

# Potential-ensrophy lengthscale for the turbulent/non-turbulent interface in stratified flow

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## Abstract

We study properties of the turbulent/non-turbulent interface (TNTI) between two layers of stratified fluids through direct numerical simulations (DNS). Zero mean shear forcing creates moderate turbulence in one of the layers with the Taylor microscale Reynolds numbers in the mixed region of  $Re_\lambda = 35, 44$ . We focus on the similarities and differences of the properties of stratified TNTIs due to two distinct types of forcing: a) convection due to a boundary heat source, and b) agitation resembling a vertically oscillating grid experiment.

Similarly to other stratified flows, the small scale dynamics of the TNTI in the present DNSs differ from what would be expected in comparable yet unstratified TNTIs. The interface cannot be indeed uniquely identified by the commonly used vorticity  $\omega$ . Instead, the potential enstrophy  $\Pi^2$  is shown to be the most appropriate marker in these flow cases. It is emphasized that the Kolmogorov lengthscale  $\eta_K \sim \sqrt{\nu/\omega}$  is not representative of the small scale dynamics of the interface. Hence, a new lengthscale,  $\eta_\Pi$ , is defined, in analogy to the Kolmogorov scale, based on the potential enstrophy,  $\eta_\Pi = (\nu^3/\Pi_*)^{1/6}$ , being  $\Pi_* = |g/\rho_0\Pi|$ . The conditionally-averaged profiles of potential enstrophy  $\Pi^2$ , enstrophy  $\omega^2$ , and turbulent kinetic energy dissipation  $\epsilon$  of the two distinctly different turbulence forcing cases collapsed when scaled by  $\eta_\Pi$  at different time instants in each simulation. This implies not only the self-similarity of the small scale statistics of the TNTI in either of the two cases, but also the similarity between the statistics of the two different turbulent flows in the proximity of TNTI.

## I. INTRODUCTION

Entrainment across turbulent/non-turbulent interfaces (TNTI) in stratified fluids is important for a vast set of applications, such as the dynamics of the ocean, atmospheric pollution dispersion, and the spread of contaminants [1]. Entrainment is responsible for the mixing and exchange of mass, energy, momentum and scalar quantities between the fluid regions [2, 3].

In unstratified cases, the turbulent flow can propagate into the irrotational region, moving the TNTI by viscous action, defined by small Kolmogorov-sized scales [4, 5]. The TNTI itself can be subdivided into viscous sublayer (VSL), as proposed by [4] with an estimated thickness of the order of the Kolmogorov lengthscale  $\eta_K$ , and turbulent sublayer (TSL) [5–7], depending on the relative magnitude of viscous diffusion and turbulent vorticity,  $\omega$ .

The VSL is a result of the process by which vorticity diffuses into the quiescent region. The lengthscale associated with this phenomenon is controlled by the viscosity  $\nu$  and the dissipation (the squared rate of strain), which is comparable in magnitude to enstrophy,  $\omega^2$ . Therefore, the lengthscale, after appropriate dimensional analysis, could be  $\sqrt{\nu/\omega}$ , that corresponds to  $\eta_K$  up to a multiplicative factor of 2 [8–10]. The thickness of the TSL, responsible for the increase in vorticity between the viscous sublayer and a fully turbulent region, is defined as the thickness of the enstrophy jump. Results in [11–14] show that the turbulent sublayer thickness is of the order of magnitude of the Taylor lengthscale,  $\lambda$ . More recently, [15] demonstrated theoretically and experimentally, that specifically in non-equilibrium turbulence the entrainment velocity scales with the Taylor velocity  $v_\lambda$ , rather than Kolmogorov velocity scale.

In general, the TNTI can be defined using the sharp change in magnitude of enstrophy, by a passive scalar or density/temperature [16, 17]. Differences may arise in the interface identification by different markers [18]. This is explained by different governing processes near the TNTI: viscous diffusion versus molecular diffusion. The differences depend on the values of Prandtl or Schmidt numbers and for high  $Pr, Sc \gg 1$  this may affect the statistics conditioned on TNTI [19–21].

In stratified fluids the flow physics is more complex because turbulence is also responsible for the irreversible mixing of the entrained fluid that changes its properties [22, 23]. Substantial insight into stratified mixing without mean shear was obtained in experiments

with employed a vertically oscillating grid in a two-fluid layer system [24–26].

A characteristic feature of stably stratified fluids is the presence of internal waves that are triggered by the turbulent agitation and propagate through the fluid at angles that are determined by the local stratification. Researchers addressed the internal waves generated by the turbulent wake of a sphere moving horizontally in a linear stratification both experimentally [27, 28] and numerically [29]. Internal waves due to turbulence mechanically activated by grids were studied in the laboratory and simulations in a linearly stratified fluid [30, 31].

Internal waves in stratified fluids can produce vorticity in the previously quiescent zone [32]. Therefore, vorticity is not anymore a reliable marker of the turbulent/non-turbulent interface [19]. Therefore, in stratified turbulent flows, the potential vorticity  $\Pi = \boldsymbol{\omega} \cdot \nabla \rho$  (where  $\rho$  is density), which is not transferred by the internal waves [33], was suggested to identify turbulent regions [31]. Even if its advantage in the study of the atmospheric convective boundary layer has been questioned [34], because the enstrophy varies several orders of magnitude between the turbulent side and the gravity waves in the free troposphere,  $\Pi$  has been successfully used to mark the non-turbulent and turbulent regions [31]. Potential enstrophy was also used in conjunction with enstrophy to identify TNTI in DNS of turbulent stratified wake [19]. Recently  $\Pi$  was effectively used to detect the TNTI in shear-driven, linearly stratified, turbulent flow DNS [35]. The authors [35] performed in-depth analysis of  $\omega$  and  $\Pi$  budgets, and estimated the interface thickness, studying flow properties near TNTI as the function of the buoyancy Reynolds number,  $Re_b = (L_O/\eta_K)^{4/3}$ , which accounts for the effects of turbulence and buoyancy, where  $L_O = \sqrt{\epsilon/N^3}$  is the Ozmidov lengthscale, and *epsilon*,  $N$  are the turbulent kinetic energy dissipation rate and buoyancy frequency, respectively.

One of the open questions in respect to the physics of the stratified fluids interfaces, is whether a large-scale forcing on the turbulent side affects small-scale TNTI properties. We studied this aspect numerically through a comparative analysis of two stratified turbulent flows: one generated by a convective forcing through a boundary buoyancy flux, and another using a mechanical type of forcing, analogous to a vertically oscillating grid, both without mean shear.

We demonstrate that the statistics in the VSL scaled with the lengthscale  $\eta_k$  [4] has to be adjusted for the stratified turbulent cases. At least in the range of the Reynolds numbers

of this work and for shearless forcing types we present. Another small-scale lengthscale,  $\eta_{\Pi}$ , defined with  $\nu$  and  $\Pi$ , is developed. We then present the statistics scaled with  $\eta_{\Pi}$ , that show the small-scale self-similarity in the TNTI region for the two different flow cases, irrespective of their large scale forcing type.

## II. METHODS

Two cases with shearless turbulence are simulated: an oscillating grid turbulence case (hereafter denoted as **G**) and a convective boundary layer case (**C**). The direct numerical simulation is performed using the SPARKLE software, which integrates the incompressible Navier-Stokes equations in the Boussinesq approximation [36, 37]:

$$\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} = -\frac{1}{\rho_0} \frac{\partial p}{\partial x_i} + \nu \frac{\partial^2 u_i}{\partial x_j^2} + b \delta_{i3} \quad (1)$$

$$\frac{\partial b}{\partial t} + u_j \frac{\partial b}{\partial x_j} = \kappa \frac{\partial^2 b}{\partial x_j^2} \quad (2)$$

$$\frac{\partial u_i}{\partial x_i} = 0 \quad (3)$$

where  $u_i$  is the velocity vector,  $b = g(\rho_0 - \rho)/\rho_0$  is the buoyancy,  $\nu$  is the kinematic viscosity and  $\kappa$  the molecular diffusivity,  $g$  is the gravitational acceleration and  $\rho_0$  is a reference density. Eqs. (1)-(3) use Einstein notation, where  $i = 1, 2$  represent the horizontal components,  $x, y$ , and  $i = 3$  is the vertical direction,  $z$ . The code is fully parallelised, making use of domain decomposition in two directions. The spatial differential operators are discretised using second-order, symmetry preserving central difference [38] and time integration is carried out with an adaptive second-order Adams-Bashforth method [36].

Both simulations have periodic boundary conditions applied at the lateral walls and free-slip conditions at the upper and bottom boundaries. At  $t = 0$ , the fluid is at rest and has a two-layer stratification with its interface at  $z = h_0 \equiv h(t = 0)$ .  $h$  corresponds to the mixing layer depth, described in Section IID. We choose  $\rho_0$  to be the density of the bottom layer, which leads to  $b_0 = 0$  for  $z < h_0$  and  $b_{\text{ref}} = \Delta b$  for  $z > h_0$ .

### A. Grid turbulence simulation

The grid-generated turbulent flow (case **G**) is a DNS in a cuboidal domain of size  $L_x \times L_y \times L_z = h_0 \times h_0 \times 2h_0$ , on the  $360 \times 360 \times 720$  mesh. The oscillating grid is implemented

using a standard immersed boundary method, with a motion of the form

$$z_{\text{grid}}(t) = z_{\text{grid}_0} + 0.5S \sin(2\pi ft), \quad w_{\text{grid}} = 0.5S 2\pi f \cos(2\pi ft), \quad (4)$$

which is imposed by setting the velocity in the region occupied by the grid equal to  $(0, 0, w_{\text{grid}})$ , a qualitative representation of case **G** is showed in fig. 1a. To preserve the incompressibility of the fluid, the Poisson solver for pressure is called right after the computation of eq. 4. Similar simulations with this forcing type were implemented several times in different contexts [39–41].

Key parameters of the oscillating grid case are the mid-stroke position of the grid,  $z_{\text{grid}_0}/h_0 = -0.467$ , the stroke length  $S/h_0 = 0.267$  and the dimensionless oscillation frequency  $f t^* = 42$ , where  $t^* = L/u'_{\text{RMS}}$  is the turnover time,  $u'_{\text{RMS}}$  the horizontal (longitudinal  $u'$  and transverse  $v'$ ) velocity fluctuations root mean square, and  $L$  is the integral length-scale [42]. The thickness and the mesh size of the grid are  $a/h_0 = 0.03$  and  $M/h_0 = 0.2$ , respectively. These were chosen to resemble an oscillating grid with solidity of 0.31, similar to the experiments performed in [43]. The parameters are set to develop a well mixed turbulent layer in proximity of the initial buoyancy discontinuity located at  $h_0$ .

The Reynolds number is computed similarly to the experimental studies as  $Re = u'_{\text{RMS}}L/\nu = K_g\beta_g/\nu$  [42, 43], where  $K_g$  is the so-called grid action, and  $\beta_g$  is an empirical constant that depends on the grid characteristics  $S, f, M$  [44]. This approach is based on empirical relationships that define  $u'_{\text{RMS}}$  and  $L$  with the oscillating grid characteristics:  $u'_{\text{RMS}} = K_g/d$ ,  $L = \beta_g d$ , where  $d \equiv z - z_{\text{grid}_0}$  is the distance from the grid mid-stroke position. The results of the model [42] for  $K_g$  and  $\beta_g$  are shown in Fig. 1.b-c, respectively.

## B. Convective boundary layer simulation

The convective case (**C**) is simulated with a steady vertical heat flux  $q_w = -\kappa\partial\theta/\partial z$  applied at the bottom boundary. The three-dimensional volume has  $L_x \times L_y \times L_z = 4h_0 \times 4h_0 \times 2h_0$  size, with a computational resolution of  $N_x \times N_y \times N_z = 720 \times 720 \times 360$ . Similarly to **G**, this case also develops a fully mixed region between the turbulence source at the boundary and the initial density jump at  $h_0$ . In the case **C** the characteristic velocity of the convective mixed layer is  $U = (\beta g q_w h_0)^{1/3}$  [45], with  $\beta$  the thermal expansion coefficient, and the characteristic lengthscale is  $L = h_0$ . The Reynolds number for the case **C** is

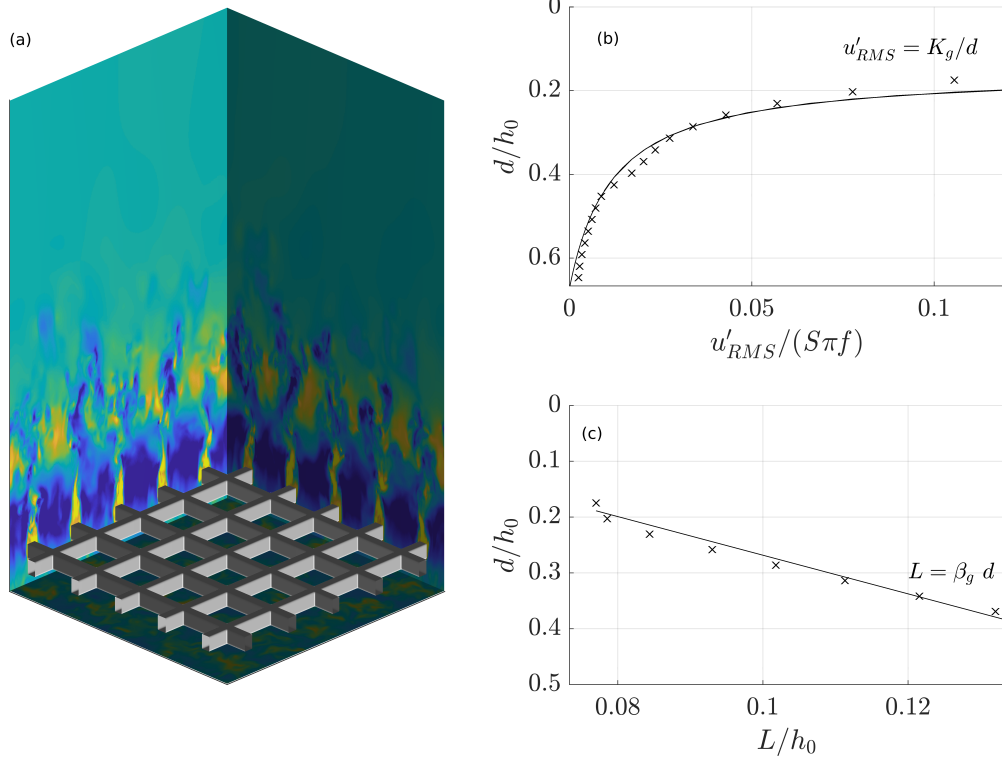


FIG. 1. Oscillating grid DNS case **G**: (a) 3D representation of the grid within the domain at  $t/t^* = 3.8$ , the colored fields represent the fluid vertical velocity; (b) spatial distribution of  $u'_{RMS}$  and (c) longitudinal integral length scale as function of the distance from the grid  $d$ .

$$Re = UL/\nu = 1260.$$

### C. Further simulation details

Both simulations were performed for a period  $t_{run}$ , but all the results in section-III are computed after  $t_{run}/2$  in order for the system to reach quasi-stationary condition. Details are summarized in table I. In addition to the domain sizes  $N_{i=x,y,z}, L_{i=x,y,z}$  and the large scale Reynolds number  $Re$ , table I reports other key parameters: the Taylor micro-scale Reynolds number,  $Re_\lambda = u_T \lambda / \nu$ , and buoyancy Reynolds number,  $Re_b$ , which are more relevant for comparison of the well mixed layers due to different large scale forcing, and near the TNTI, respectively. Both parameters are given for two locations: at  $z = h$ , and closer to the turbulence source, in the well mixed region, where stratification effect is negligible ( $L_O \gg \eta_K$ ).  $Re_\lambda$  is computed using the Taylor micro-scales  $u_T \approx \sqrt{2k/3}$  and  $\lambda = \sqrt{10\nu k/\epsilon}$ , utilising

TABLE I. The DNS cases main features.

	$N_x N_y N_z$	$L_x L_y L_z/h_0^3$	$Pr$	$Re$	$t_{\text{run}}/t^*$	$Re_\lambda(z = h)$	$Re_\lambda(z = 0.7h)$	$Re_b(z = h)$	$Re_b(z = 0.7h)$	$Ri$	$\Delta z/\eta_K$
<b>C</b>	$720^2 \times 360$	$4^2 \times 2$	1.25	1260	16	13	44	0.210	105	240	0.91
<b>G</b>	$360^2 \times 720$	$1^2 \times 2$	1.25	92	6	8	35	0.125	21000	30	1.44

the turbulent dissipation rate,  $\epsilon$ , and the turbulent kinetic energy  $k = \frac{1}{2}(\overline{u'^2} + \overline{v'^2} + \overline{w'^2})$ . The buoyancy Reynolds number  $Re_b$ , commonly representing turbulence intensity in stratified flows relates the influence of buoyancy and small-scales turbulence. The Ozmidov scale is computed with the frequency  $N$  defined as  $(g \overline{db}/dz)^{1/2}$ . The strength of the stratification is estimated with the bulk Richardson number  $Ri$ . It is defined as  $Ri = \Delta bh/k$ , where  $k = k(z = 0.7h)$ . The Prandtl number is set to  $Pr = 1.25$ , for both (**G**) and (**C**), to increase viscosity over molecular diffusivity.

#### D. Horizontally-averaged statistics

Before presenting the conditional analysis, the basic statistics of the two cases are discussed. Fig. 2 shows the spatial distributions of key flow properties of the two DNSs emphasizing their common features and differences. The horizontally-averaged profiles of buoyancy  $b$ , turbulent kinetic energy  $k$ , the diffusive flux  $\kappa\phi_B$  (being  $\phi_B = \overline{db}/dz$ ), and the turbulent buoyancy flux  $\overline{w'b'}$ , are shown for the two DNSs (**C** in the top row and case **G** in the bottom row). The quasi-stationary temporal evolution of these quantities is shown by color shades as explained in the legends. The profiles are horizontally averaged, with further averaging over one turn-over time scale  $t^*$ . Since the emphasis of this paper is on the entrainment properties of different flows, the profiles are normalised by the value at the mixed layer depth  $h$ . The mixed layer depth  $h$  is diagnosed via the minimum of the diffusive buoyancy flux  $\phi_B$  (or equivalently the inflection point of the mean buoyancy).  $b_{\phi_E}$  and  $k_{\phi_E}$  are then the buoyancy and the turbulent kinetic energy, sampled at  $z = h$ . The entrainment flux  $\phi_E$  was determined following [46] by extrapolating the linear profile of the total buoyancy flux to the boundary layer depth  $h$ .

The horizontal dotted lines in **G** case (Fig. 2e-h, at -0.6 and -0.33), mark the stroke of the grid. Since the fluid velocity in this region is directly affected by the oscillating grid motion, the corresponding volume is excluded from the conditional analysis in section III B.



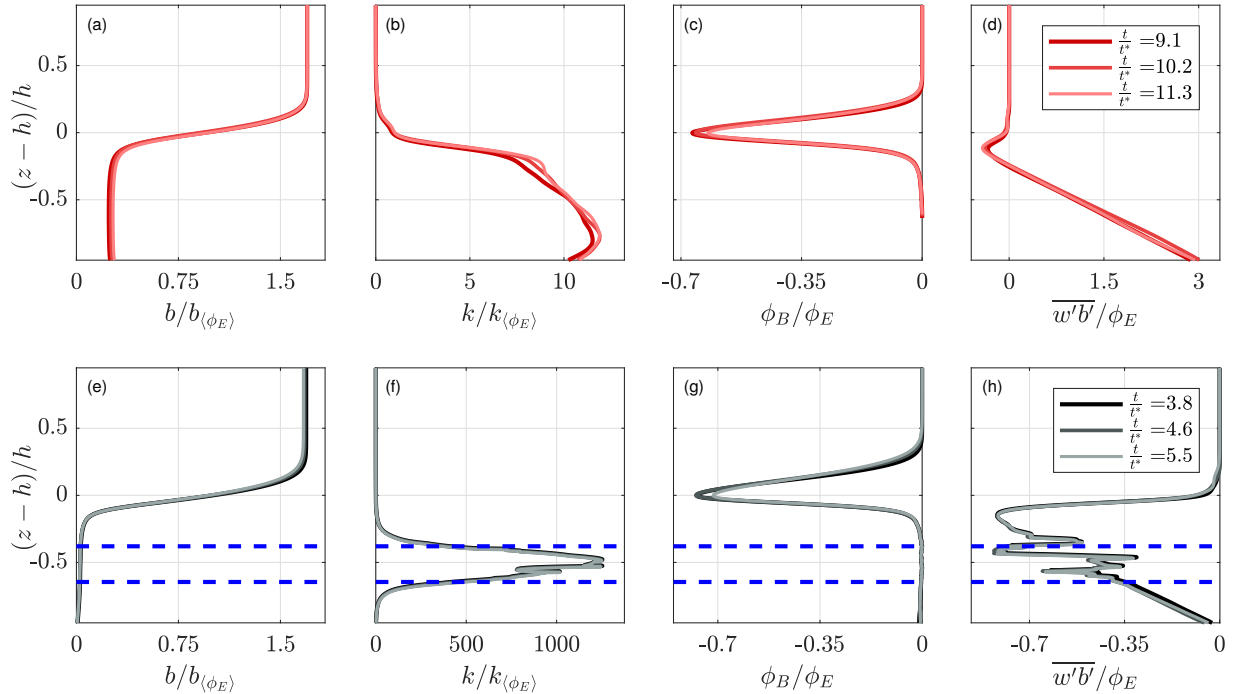


FIG. 2. Vertical profiles of case **C** (upper row), and **G** (lower row) over time: (a)-(e) buoyancy; (b)-(f) turbulent kinetic energy; (c)-(g) diffusive flux; (d)-(h) turbulent flux.

The negligible differences between the curves with different shades, corresponding to the prescribed time intervals emphasize that the systems have reached their quasi-steady state regimes, for all the relevant quantities. Moreover, Fig. 2a,e and 2c,g show that both simulation results have similar profiles for buoyancy and diffusive fluxes. This is one of the key similarity points of the two cases. It is also clear that, in the time needed to reach quasi-steady condition, the molecular diffusion causes the buoyancy profile to transition from the initial step function profile, with discontinuity at  $z = h_0$ , to a continuous profile with a transitional region at about  $z \approx h$ . The existence of this layer supports a region in which internal waves can propagate.

Despite the similarity in flux profiles, the two cases are different in their mechanisms: the convective **C** case produces turbulence via buoyancy  $\overline{w'b'}$  over the entire mixed layer (apart from the entrainment zone in which  $\overline{w'b'}$  is negative), whilst for the grid case **G**, the turbulence is generated at the grid and then transported through the mixed layer. Here, the buoyancy flux is negative throughout the mixed layer, which goes at the expense of the turbulence kinetic energy. This is evident in the profiles of turbulence kinetic energy,

which are substantially different (Fig. 2b,f). Fig. 2b presents relatively large values of  $k$  throughout the bottom half of the domain before a sharp drop at  $(z - h)/h < -0.2$ . For the **G** case, Fig. 2f, TKE decays with the reciprocal of the distance from the grid as  $k^{1/2} \sim u'_{\text{RMS}} = K_g/(z - z_{\text{grid}_0})$  [42, 47], right below the region of the direct agitation by the oscillating grid.

### III. RESULTS

#### A. Definition of the turbulent/non-turbulent interface position

As mentioned in the introductory section, there are several possible definitions of TNTI. In unstratified cases, vorticity is used to separate rotational from irrotational fluid, based on either vorticity or enstrophy thresholds,  $\omega^2 \geq \omega_{\text{th}}^2$ . An appropriate threshold is chosen such that the conditional statistics near the TNTI do not significantly depend on its value, e.g. [5, 8]. It is typically supported by the plot of the turbulent volume as a function of enstrophy, which exhibits a plateau at a properly chosen  $\omega_{\text{th}}^2$ . It is also possible to visualize the interface position; its shape that should not vary strongly depending on the value of  $\omega_{\text{th}}^2$ , see e.g. [6, 48].

In stratified cases, vorticity can be produced in the environment by internal waves [32, 49]. This situation complicates the use of  $\omega_{\text{th}}^2$  as a TNTI marker. This may be especially relevant for low and moderate Reynolds numbers [34]. Conversely to  $\omega^2$ ,  $\Pi^2$  is produced by viscous and diffusive effects [19]. Initially irrotational fluid regions, may acquire potential enstrophy only by turbulence-related mechanisms (like entrainment) but not through internal waves.

Figs. 3.a-b and 3.d-e show a 2D vertical cross-section (**C**) and (**G**) simulations, respectively, presenting the potential enstrophy (fig. 3.a-d, and enstrophy (fig. 3.b-e with the former exhibiting a clear boundary between the turbulent and non-turbulent fluids. Note that the vertical axis is relative to the mixed layer depth  $h$  defined in the previous section, and it is clear that the instantaneous TNTI is situated about 20% higher than  $h$ . The instantaneous values of  $\omega^2$  can be seen to extend even further up, and are a result of the smooth stratification produced by molecular diffusion and to the relatively low values of  $Re$  which allow internal waves to propagate into this region. We experimented with a large number of indicators for TNTI, including enstrophy, and hybrid indicators [19], but in all

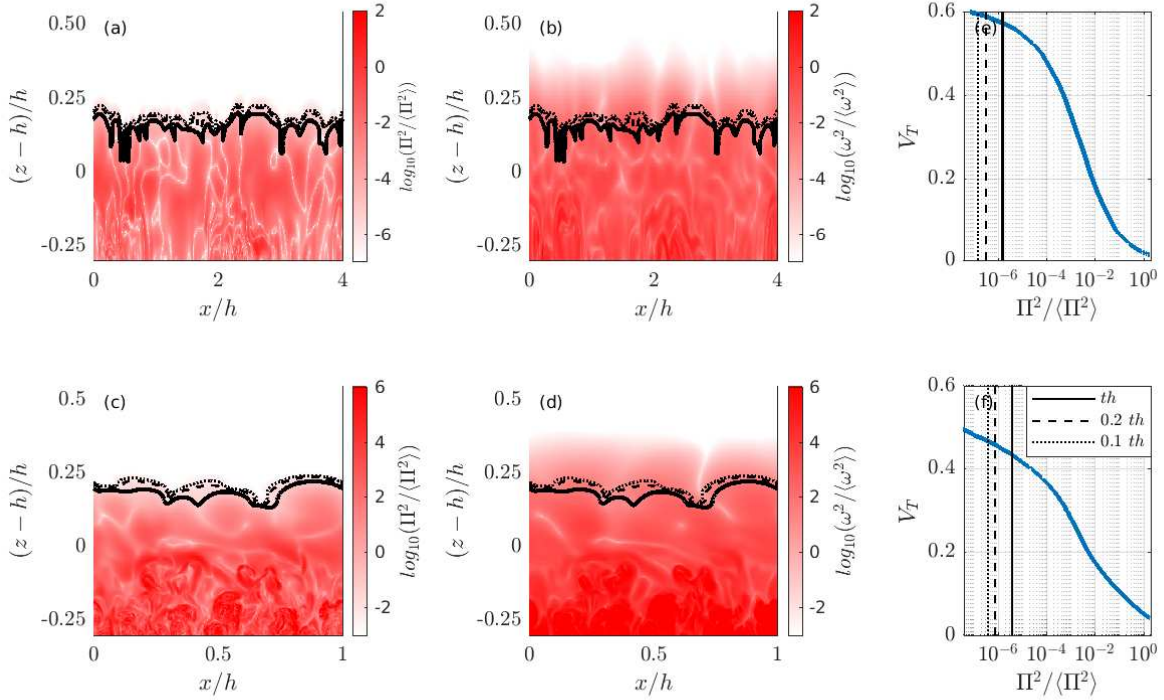


FIG. 3. Case **C** (upper row) and **G** (lower row): vertical cross-section of (a)-(d) normalised  $\Pi^2$ , (b)-(e) normalised  $\omega^2$ , (c)-(f) turbulent volume fraction as function of  $\Pi^2$ . Black lines mark: threshold (solid), 1/5 of threshold (dashed), 1/10 of threshold (dotted)

other cases the results were unacceptably sensitive to the chosen threshold. Only potential enstrophy turns out to be a robust indicator for the TNTI, provided that the threshold is chosen sufficiently small. Fig. 3.c-f shows the turbulent volume fraction  $V_T$  as a function of  $\Pi^2$ , normalized by its mean value  $\langle \Pi^2 \rangle$  computed over the turbulent and quiescent regions (excluding the volume spanned by the oscillating grid in **G**). It is clear that  $V_T$  is only weakly dependent on the exact value near the chosen threshold:  $4 \times 10^{-6} \langle \Pi^2 \rangle$  for case **C** DNS and  $1.6 \times 10^{-6} \langle \Pi^2 \rangle$  for case **G**.

## B. Comparison of the near-interface dynamics between the two cases

It is generally expected that the significant properties for the near- interface turbulent dynamics, driven by the viscous diffusion of vorticity into the irrotational region, are the

kinematic viscosity  $\nu$  and vorticity  $\omega$  [4, 8, 9]. The most relevant lengthscale in this region is the Kolmogorov scale,  $\eta_K \sim \sqrt{\nu/\omega}$  (derivable from the more common expression  $\eta_K = (\nu^3/\epsilon)^{1/4}$  using the relation:  $\epsilon = 2\nu\omega^2$ , valid in homogeneous isotropic turbulence [50, 51]). Therefore, for the following comparison of the small-scale near-interface dynamics of the two DNS cases in Fig. 4-5 we normalize the distance to the interface,  $z_* = z - z_I$  where  $z_I$  is the interface position, by  $\eta_K$  computed at the TNTI. We want to check if some similarities in the conditional profiles of  $\Pi^2$ ,  $\omega^2$ ,  $k$ , and  $\epsilon$  in Fig. 4(a,c,e,g) can be found. These quantities, scaled by  $\eta_K$  do exhibit good self-similarity in time for each DNS separately. The conclusion one has to draw from these results is that the two simulations – despite both being driven by shearless turbulence - do not produce the same dynamics near the TNTI, with the turbulent quantities in **C** changing much more slowly as a function of  $z^*/\eta_K$  than **G**.

However, in the choice of the threshold indicator, it was quite clear that the enstrophy was not suitable for these cases. Since the potential enstrophy  $\Pi^2$  was shown to be a robust TNTI indicator, it stands to reason to define a new local lengthscale

$$\eta_{\Pi} = \left( \frac{\nu^3}{\Pi'} \right)^{1/6} \quad (5)$$

where  $\Pi'$  is defined as

$$\Pi_* = |\bar{\omega} \cdot \nabla b| = \left| \frac{g}{\rho_0} \Pi_I \right| \quad (6)$$

and  $\Pi_I$  the square root of the threshold of potential enstrophy.  $\eta_{\Pi}$  defines the relevant scale in cases when the vorticity evolves not only through viscous diffusion, but also by stratification effects. In stratified cases  $\Pi^2$  can only enter the non-turbulent region via molecular effects. Therefore, applying a dimensional analysis using  $\Pi$  and  $\nu$  to obtain a length-scale,  $\eta_{\Pi}$  is the natural small-scale lengthscale.

The flow properties scaled with  $\eta_{\Pi}$  for both DNSs are reported in Fig. 4(b,d,f,h). The key result is that the two simulations exhibit remarkably similar behaviour near the TNTI, when scaled based on  $\eta_{\Pi}$ . Indeed, for  $\Pi^2$ ,  $\omega^2$  and  $\epsilon$ , the profiles of (G) and (C) are nearly indistinguishable for  $z^*/\eta_{\Pi} > -10$ . Only the kinetic energy for the two cases deviates deeper into the non-turbulent layer ( $z^*/\eta_{\Pi} > 5$ ).

Comparison of profiles of potential enstrophy and enstrophy in Fig. 4b,d further highlights the effectiveness of the proposed method for TNTI detection and the use of the new lengthscale. Not only  $\Pi^2$  presents a larger magnitude in the “jump” across the interface as in [35],  $\Pi^2$  curves also show a clear change in slope, with the presence of the inflection point

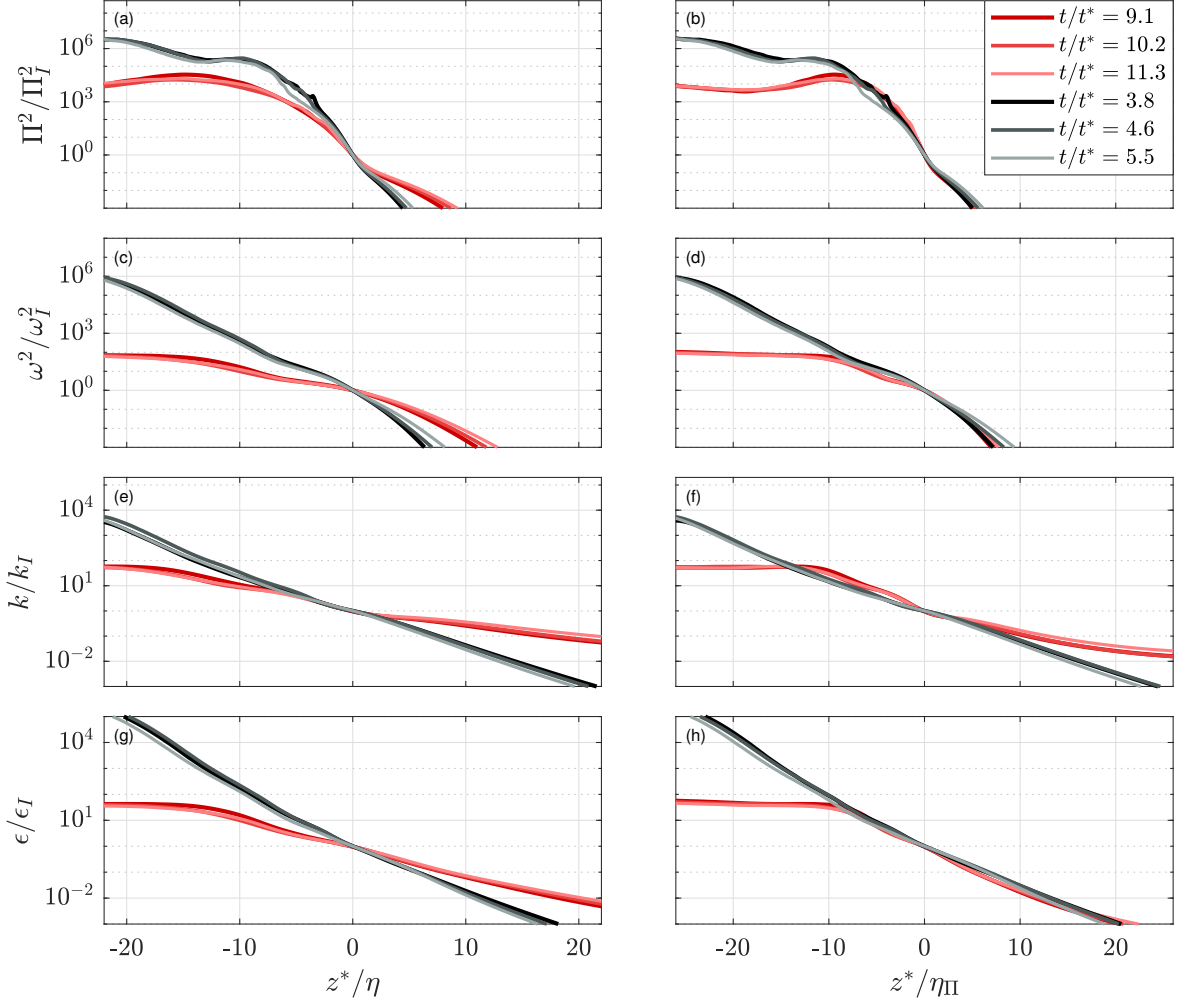


FIG. 4. Vertical conditional profiles of: (a)-(b)  $\Pi^2$ , (c)-(d)  $\omega^2$ , (e)-(f)  $k$ , (g)-(h)  $\epsilon$  scaled with  $\eta_K$  (left column) and  $\eta_{\Pi}$  (right column). **G**: black curves; **C**: red curves.

at  $z^* \approx 0$ , and a distinct boundary between the turbulent and the non-turbulent regions which is sharper as compared to  $\omega^2$ .

To provide a precise value for the TNTI thickness  $\delta_I$  we followed the procedure proposed in [35] based on a fit of Gaussian shape to  $\partial\Pi^2/\partial z$ . This procedure yields  $\delta_I \sim 10\eta_{\Pi}$  for both **C** and **G**. It is noteworthy that, in the stratified shear driven flow [35]  $\delta_I$  increased with decreasing  $Re_b$ , as the flow evolved in time. It remains to be studied whether this effect is present in shearless stratified cases on a larger range of  $Re_b$ .

For completeness, we also computed the TNTI thickness with the Kolmogorov length  $\eta_K$  scaling: both DNSs present constant behaviour in time, however the difference in  $\delta_I$  is larger

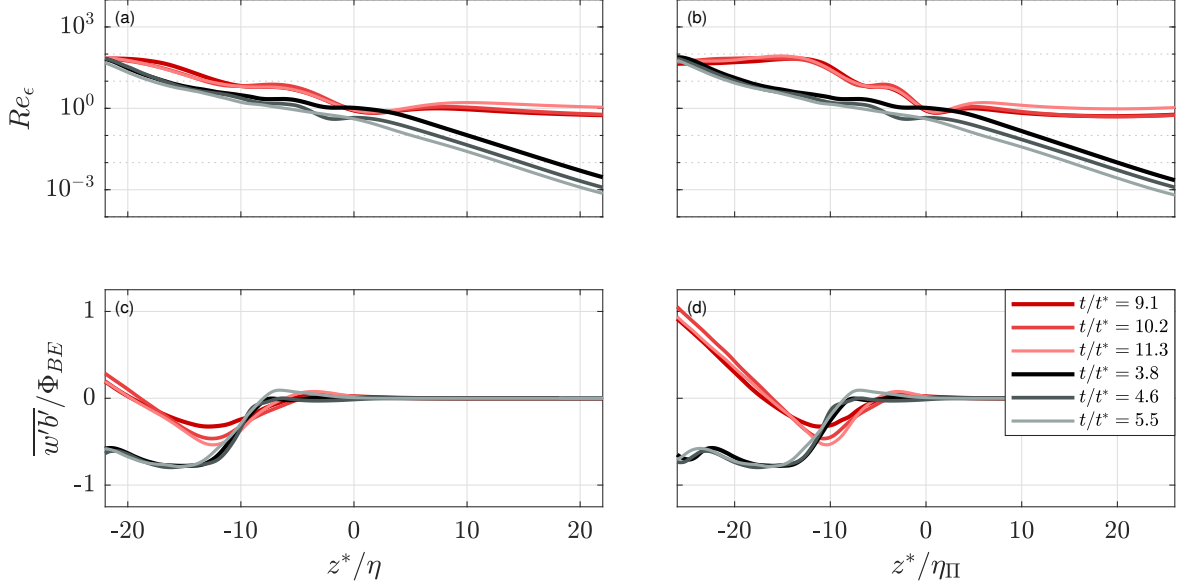


FIG. 5. Vertical conditional profiles of: (a)-(b)  $Re_\epsilon$ , (c)-(d)  $\overline{w'b'}$  scaled with  $\eta_K$  (left column) and  $\eta_\Pi$  (right column). **C**: red curves; **G**: black curves.

between **C** and **G** than the results obtained from the  $\eta_\Pi$ . In case **G**  $\delta_I = 10\eta_K$ , while in **C** we obtain  $\delta_I = 15\eta_K$ .

We further compare the two cases and the scaling with the viscous lengthscale versus the new lengthscale in Fig. 5 presenting the turbulent Reynolds number  $Re_\epsilon = k^2/(\nu\epsilon)$  and the turbulent buoyancy flux  $\overline{w'b'}$ . Here, no collapse is observed in either of the lengthscales. Both turbulence Reynolds numbers are  $O(1)$  at the TNTI; the convective driven case **C** is more strongly agitated compared to the grid case **G** in the turbulent region, leading to higher values of  $Re_\epsilon$ . This is possibly caused by the different nature of forcing type. The turbulent fluxes shown in Fig. 5c-d reflect, similarly to  $Re_\epsilon$ , the different types of turbulent agitation of the two cases in the turbulent regions and the change from negative to positive values of  $\overline{w'b'}$  that leads to a local maxima in the interfacial layer.

### C. Vorticity structure in the near TNTI region

One of the key questions is whether the vorticity dynamics is different between the two cases. We address this question by studying the alignment of vorticity vectors with the TNTI isosurface, conditionally sampled at different distances from the interface. The alignment of two three-dimensional vector fields can be characterised through the alignment angle  $\theta$ , which is defined as  $\cos \theta = \boldsymbol{\omega} \cdot \mathbf{n} / |\boldsymbol{\omega}| |\mathbf{n}|$ , where  $\mathbf{n}$  is the normal to the TNTI surface [52]. The alignment is analysed through the conditional mean profiles and PDFs of  $\cos \theta$ , in Fig. 6.

We observe a strong alignment between vorticity and the TNTI surface, similar to the results in [52]. This is expected at the TNTI interface, including stratified flow cases, since according to Helmholtz second theorem a vortex filament either extends to the fluid boundaries or forms a closed path [53], hence vortical tube-like structures, associated to turbulence, could not end inside the fluid. Evidence for the above statement is shown in Fig. 6a: a plateau at  $-10 < z^*/\eta_{\text{II}}$  where the minimum value of  $\langle \cos \theta \rangle$  is approximately 0.3 for both DNSs.

The PDFs of  $\cos \theta$  at three distance intervals are shown in Fig. 6b,c,e. The PDFs in the interval  $[-20, -15]\eta_{\text{II}}$  show that in the turbulent regions the vorticity angles are almost uniformly distributed and there is no preferential alignment. A lower Reynolds number in the **G** case compared to the **C** case is probably the reason for the small bias in the alignment. However, when getting closer to the TNTI, as in panels Fig. 6c,d that represent the intervals  $[-10, -5]\eta_{\text{II}}$  and  $[-2.5, 2.5]\eta_{\text{II}}$  respectively, we observe that the most frequent angle between  $\boldsymbol{\omega}$  and  $\mathbf{n}$  is  $\cos \theta = 0$  similarly to [52], confirming a tendency of  $\boldsymbol{\omega}$  to align with the TNTI.

## IV. SUMMARY AND CONCLUSIONS

We presented a DNS study of the TNTI in shearless stratified turbulent flows, with a buoyancy jump between two layers. We focus on the question of similarity at small scales in the proximity of the interface of two fluid cases, forced by two distinctly different ways: convective forcing using a constant heat flux versus an agitation resembling an oscillating grid.

We confirmed that in the stratified cases considered here, the common approach to identify the TNTI based on the enstrophy threshold is not reliable, since  $\omega^2$  is no longer repre-

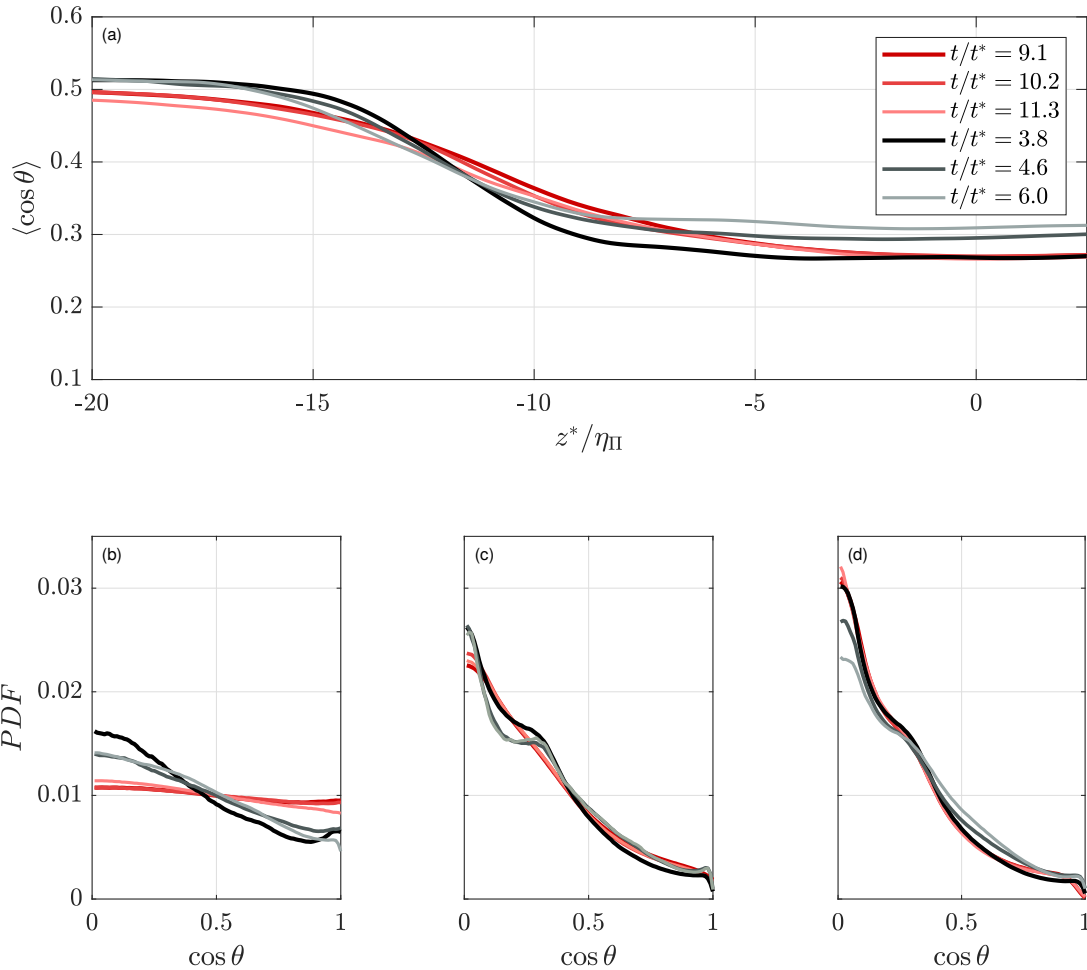


FIG. 6. Alignment of  $\boldsymbol{\omega}$  with the TNTI normal  $\mathbf{n}$ . **C**: red curves; **G**: black curves. (a) vertical profiles of  $\langle \cos \theta \rangle$ . PDFs of  $\cos \theta$  at different intervals height: (b)  $-20 < z_I/\eta_{\Pi} < -15$ ; (c)  $-10 < z_I/\eta_{\Pi} < -5$ ; (d)  $-2.5 < z_I/\eta_{\Pi} < 2.5$ .

sentative of the viscous processes across the turbulent/non-turbulent boundary alone, but can also contain contributions from internal waves. The latter were caused by the interaction of the turbulence with a stratified layer which developed due to molecular diffusion. Hence the potential enstrophy  $\Pi^2$ , which is not affected by stratification related phenomena, need to be used to define TNTI in both shearless cases, similarly to [19, 35]. Based on the analogy between the enstrophy  $\omega^2$  and potential enstrophy  $\Pi^2$  we defined a new lengthscale  $\eta_{\Pi}$ . Using this lengthscale, the basic TNTI statistics for the two cases collapsed onto each other. Furthermore, the lengthscale clearly distinguished between the turbulent region and



the near-TNTI region in the slopes of the profiles of turbulent properties. The near-TNTI region defined by the new lengthscale also reflects the fact that the vortical structures realign to the interface within this region (while being randomly oriented in the turbulent core). However, there were also indicators that did not collapse onto one curve, such as  $Re_\epsilon$  and the turbulent heat-flux  $\overline{w'b'}$ .

In light of the intriguing results for the new lengthscale  $\eta_{\Pi}$ , it will be crucial to explore the behaviour for these flow cases at higher  $Re_b$  and also for other canonical flows, such as a stratified wake. Furthermore, it may be interesting to analyse the various terms of the potential enstrophy equation, to obtain more detailed description of the physical phenomena that influence  $\Pi^2$ , similar to the study of [35]. It is also interesting to test if this scale has presence in the small-scale dynamics of turbulent linearly stratified flows.

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