

1978

## **DNYCOR: An Uncertainty Dynamic Modal Analysis Program**

B. A. Dendrou

Elias N. Houstis

*Purdue University*, [enh@cs.purdue.edu](mailto:enh@cs.purdue.edu)

**Report Number:**

78-272

---

Dendrou, B. A. and Houstis, Elias N., "DNYCOR: An Uncertainty Dynamic Modal Analysis Program" (1978).  
*Department of Computer Science Technical Reports*. Paper 204.  
<https://docs.lib.purdue.edu/cstech/204>

This document has been made available through Purdue e-Pubs, a service of the Purdue University Libraries.  
Please contact [epubs@purdue.edu](mailto:epubs@purdue.edu) for additional information.

DYNCOR: An uncertainty dynamic modal analysis program

B. A. Dendrou\* and E. N. Houstis\*\*

CSD-TR 272

July 1978

Abstract

DYNCOR is a computer program which is designed to perform uncertainty dynamic modal analysis of linear elastic two-dimensional structures undergoing small displacement response. DYNCOR uses finite element techniques with triangular plane strain or stress element. The Duhamel's integral is evaluated using Newmark's procedure. The uncertainty is introduced through the physical parameters of the system and is measured using a perturbation technique.

---

\*Department of Civil engineering, Purdue University, West Lafayette, IN 47907.

\*\*Department of Computer Science, Purdue University, West Lafayette, IN 47907.

## 1. Introduction

This program handles the dynamic uncertainty analysis of linear elastic two-dimensional structures undergoing small displacement response. The medium is assumed to be a correlative field statically homogeneous and isotropic [1]. Thus the uncertainty is introduced through the following physical parameter: the modulus of Elasticity, the Poisson's ratio and the Density. Their first and second statistical moment are assumed to be known and provide the basis of the proposed uncertainty Finite Element modal analysis, with which the equations of dynamic undamped equilibrium are solved.

In section 2 the algorithm is described. It leads to the evaluation of the first and second statistical moment of the natural frequencies, the displacements field and the stress field.

A comparison of the expected natural frequencies obtained by DYNCOR, with other programs is given in [2].

## 2. Method Used

A two-dimensional Ritz-Galerkin procedure with linear triangular elements is used for the discretization of the cross section of interest.

The geometric boundaries are considered as known with certainty. The input motion is prescribed at the boundary nodes either as uniform acceleration in all base nodes or as a travelling acceleration with a given velocity.

To pursue an uncertainty dynamic analysis the following components of the algorithm are needed.

- i. Evaluation of the quasistatic displacement vector

- ii. Evaluation of the natural frequencies and their coefficient of variation performing a modal analysis coupled with a perturbation scheme as defined by Bolotin [3]. The equations are given in Appendix 1.
- iii. Evaluation of the dynamic displacement vector according to Newmark's scheme, as well as its coefficient of variation.
- iv. Evaluation of the stress vector and its coefficient of variation.

### 3. Required Input Data

Following is a description of the required format for the input data and explanations of some of the input parameters. Also an example problem is shown in figure 1. It concerns the dynamic uncertainty analysis of a [500 x 500] m square domain subjected to an input earthquake perturbation at its boundary  $y = 0$ . The boundaries  $y = 500$ ,  $x = 0$ , and  $x = 500$  are considered free.

The acceleration signal of the earthquake has a maximum acceleration of 0.5 g (g = gravity) and the increment of time is 0.01 sec. The signal is travelling at a velocity of 200 m/sec.

The physical parameters describing the geologic medium, namely the modulus of Elasticity, the Poisson's ratio, and the Density are given at each node of the 6 x 6 mesh of the discretized region  $\Omega$ . Figure 2 illustrates the displacements computed by the program at two different time intervals. The definition of the different variables is given at the beginning of the listing. The data cards are the following:

1st card

Read title of the problem (12A6)

2nd card

Read codes as specified in listing (12I5)

3rd card

Read different options as specified in listing (12I5)

4th card

Read number of elements, nodes, boundary nodes, and number of vibrational modes (12I5)

READ INPUT DATA OF FINITE ELEMENT MESH

5th card

Read the nodes constituting an element (4I4)

6th card

Read the expected value and variance of the Modulus of Elasticity (2F10.0)

7th card

Read the expected value and variance of Poisson's ratio (2F10.0)

8th card

Read the expected value and variance of the Density (2F10.0)

9th card

Read the coordinates of each node (I4, 2F10.3)

10th card

Read Boundary nodes (2I5)

READ INPUT DATA OF DYNAMIC ANALYSIS

11th card

Read number of given accelerations, number of time steps, the increment of time steps in which displacements are not printed, the time limit for the computation of a run, the time interval, and the mean velocity of the traveling perturbation (3I5, 3F10.0)

12th card

Read the given acceleration signal (8F9.6)

13th card

Read the damping value for each mode of vibration (2F10.0)

The eigenvalues and eigenvectors are computed using subroutine RSBEIG which combines BANDR, TQLRAT, and TQL2 obtained from Argonne National Laboratory as part of the EISPACK subroutine package.

References

- [1] Dendrou, B.A. and Houstis, E.N., "An Inference-finite Element Model for Field Problems," Appl. Math. Modelling, 1978, Vol. 1, June.
- [2] Dendrou, B.A. and Houstis, E.N., "Uncertainty Finite Element Dynamic Analysis," Appl. Math. Modelling. (Submitted 1978.)
- [3] Bolotin, V.V., "Statistical Methods in Structural Mechanics," Holden-Day, Inc., 1969.

APPENDIX 1

The displacement field is decomposed into:

$$\underline{d}(t) = \underline{d}^B + \underline{d}^{IN}(t)$$

Then the Syst. Equation of the undamped motion is

$$\underline{m} \ddot{\underline{d}}^{IN} + \underline{k} \underline{d}^{IN} = - \underline{m} \ddot{\underline{d}}^B$$

To uncouple the system of the differential equations, we assume the following transformation to exist.

$$\underline{d}^{IN} = \underline{A} \underline{q}$$

where  $\underline{A}$  matrix of eigenvector

We say that we transform the physical coordinates to natural coordinates.

The equation of motion becomes

$$\underline{M} \ddot{\underline{q}} + \underline{K} \underline{q} = 0$$

where  $\underline{M}, \underline{K}$  are      DIAGONAL MATRICES       $\underline{K} = \underline{A}^T \underline{k} \underline{A}$   
 $\underline{M} = \underline{A}^T \underline{m} \underline{A}$

The variability introduced through

$$\underline{K} = \underline{\bar{K}} + \sum_{i=1}^n \beta_i \underline{D}_i \underline{\bar{K}} ; i = 1, \dots, n$$

$$\tilde{M} = \bar{M} + \sum_{i=1}^n \alpha_i \tilde{D}_i \bar{M}; i = 1, \dots, n$$

where  $\alpha$  : are the Coefficient of mass variability  
for each vibration mode

Then

$$\text{VAR}^2(\tilde{M}) = \sum_{i=1}^n \text{VAR}^2(\alpha_i) \cdot \bar{M}^2 = n[\text{VAR}^2(\alpha) \cdot \bar{M}^2]$$

$$\text{VAR}^2(\tilde{K}) = n[\text{VAR}^2(\beta) \cdot \bar{K}^2]$$

Therefore

$$\text{VAR}^2(\alpha) = \frac{1}{n} \frac{\text{VAR}^2(M)}{\bar{M}^2} = \frac{1}{n\bar{M}^2} [\text{VAR}^2(\gamma) \cdot V^2 + \text{VAR}^2(v) (\bar{\gamma})^2]$$

$$\text{VAR}^2(\beta) = \frac{1}{n} \frac{\text{VAR}^2(K)}{\bar{K}^2} = \frac{1}{n\bar{K}_1^2} \left[ \text{VAR}^2(E) \left( \frac{\partial K}{\partial E} \right)^2 + \text{VAR}^2(v) \cdot \left( \frac{\partial K}{\partial v} \right)^2 \right]$$

Assuming that the natural displacements are of the form

$$\underline{q} = \underline{q} e^{j\omega_r t}$$

Thus for each vibrational mode we obtain

$$-\tilde{M} \omega_r^2 \underline{q}_r + \tilde{K} \underline{q}_r = 0$$

The perturbed values are:



$$\omega_i = \bar{\omega}_i + \sum_{r=1}^n (\omega_{ri}^M \alpha_r) + \sum_{r=1}^n (\omega_{ri}^K \beta_r)$$

$$\underline{q}_i = \bar{q}_i + \sum_{r=1}^n (\underline{q}_{ri}^M \alpha_r) + \sum_{r=1}^n (\underline{q}_{ri}^K \beta_r)$$

$$\omega_{ri}^M = - \frac{\bar{\omega}_i \underline{q}_i^T D_r^M \bar{q}_i}{z \underline{q}_i^T M \bar{q}_i}, \quad r = 1, \dots, n$$

$$\omega_{ri}^K = - \frac{\bar{q}_i^T D_r^K \bar{q}_i}{z \bar{\omega}_i \underline{q}_i^T M \bar{q}_i}$$

Finally, the variance of the frequency is:

$$\text{VAR}^2(\omega_i) = \sum_{r=1}^n \left[ \text{VAR}^2(\alpha_i) \cdot (\omega_{ri}^M)^2 + \text{VAR}^2(\beta_i) \cdot (\omega_{ri}^K)^2 \right]$$



```

C      NPJ = NODAL POINT NUMBER 2
C      NPK = NODAL POINT NUMBER 3
C
C      E( ) = MODULUS OF ELASTICITY IN KG/(CM)2
C      POIS( ) = POISSONS RATIO
C      DEN( ) = UNIT WEIGHT IN GR/(CM)3
C
C      VE( ) = VARIANCE OF MODULUS OF ELASTICITY
C      UPOIS( ) = VARIANCE OF POISSON S RATIO
C      VDEN( ) = VARIANCE OF DENSITY
C
C      XORD( ) = X-ORDINATE IN METERS
C      YORD( ) = Y-ORDINATE IN METERS
C
C      NNB( ) = NUMBER OF NODE AT BOUNDARIES
C
C      NGAC = NUMBER OF GIVEN ACCELERATIONS
C              AT THE BOUNDARY NODES
C      NTSTEP = NUMBER OF TIME STEPS
C      NTDC = INCREMENT OF TIME STEPS IN WHICH
C              DISPLACEMENTS AND STRESSES ARE NOT PRINTED
C      TLIMIT = TIME LIMIT FOR THE COMPUTATION OF A RUN
C      DT = TIME INTERVAL FOR ACCELERATION VALUES SEC
C      RMVEL = MEAN VELOCITY OF THE TRAVELING
C              PERTURBATION AT THE BOUNDARIES
C
C-----
C
C      OUTPUT
C
C      STATIC DISPLACEMENTS OF NODES
C      N - FIRST FREQUENCIES, AND CORRESPONDING MODE SHAPES
C      GROUND VELOCITY
C      TOTAL DISPLACEMENTS OF NODES
C      STRESSES AND THEIR PEAK VALUES
C      VARIANCE OF THE FREQUENCY
C      VARIANCE OF DISPLACEMENTS
C      VARIANCE OF STRESSES
C
C-----
C
C      COMMON /COD1/ ICOD1, ICOD2, ICOD3, ICOD4
C      COMMON /COD2/ ICOD5, ICOD6, ICOD7, ICOD8
C      COMMON /FLAG/ IFLAG1, IFLAG2, IFLAG3, IFLAG4, IFLAG5, IFLAG6
C      COMMON /MESH/ NNODE, NELEM, NODBC, NN, NBAND
C      COMMON /DYNA/ NMODE, KOUNT, FLAG, TIME, RMVEL, DT
C      COMMON /DYNAL/ NTSTEP, NTDC, LK, NC, TLIMIT
C      COMMON /VOLM/ AREA
C      COMMON /MXSTR/ SMAX(50), SMIN(50), IMAX(50), IMIN(50), SMAXD(50), SMIND
C      1(50), IMAXD(50), IMIND(50)
C
C      REAL ST(100,100), STI(100,20), SMASS(100), B(100), R(260,10), W(100), EU
C      1(100), UCXX(50), UCYY(50)
C      INTEGER NEBC(40)
C
C
C      DIMENSION XORD(50), YORD(50), NNB(15), NPI(50), NPJ(50), NPK(50),
C      1E(50), POIS(50), AJ(50), BJ(50), AK(50), BK(50), DEN(50), A1(6,6),
C      2 B1(6,6), S(6,6), AEIG(100,15), ACC(800), U(110), DIS(100), YH(50)
C      3, YU(50), DSX(50), DSY(50), BINF(15,15), MK(15), F(15), C4(15), C5
C      4(15), ACCEL(15), VEL(15), LM(3), DAMP(15), STRXI(50), STRYI(50), S
C      TRXYI(50), DXZERO(100)
C
C      REAL VALFA(50), VBETA(50), KST(50), OMEGAM(15,15), OMEGAK(15,15), UH(15
C      1), UOL(50)
C
C      DIMENSION TITLE(12)
C      DIMENSION VE(100), UPOIS(100), VDEN(100)
C      REAL UDM(15,15), UD(15), UACH(15), UACD(15), UHDR(50), UVER(50), UDD(260
C      1,10), UDW(260,10), DSUX(50), DSUY(50)
C
C-----
C

```

```

A 730
A 740
A 750
A 760
A 770
A 780
A 790
A 800
A 810
A 820
A 830
A 840
A 850
A 860
A 870
A 880
A 890
A 900
A 910
A 920
A 930
A 940
A 950
A 960
A 970
A 980
A 990
A 1000
A 1010
A 1020
A 1030
A 1040
A 1050
A 1060
A 1070
A 1080
A 1090
A 1100
A 1110
A 1120
A 1130
A 1140
A 1150
A 1160
A 1170
A 1180
A 1190
A 1200
A 1210
A 1220
A 1230
A 1240
A 1250
A 1260
A 1270
A 1280
A 1290
A 1300
A 1310
A 1320
A 1330
A 1340
A 1350
A 1360
A 1370
A 1380
A 1390
A 1400
A 1410
A 1420
A 1430
A 1440

```

	READ 106, TITLE	A 1450
	READ 107, ICOD1, ICOD2, ICOD3, ICOD4, ICOD5, ICOD6, ICOD7, ICOD8	A 1460
	READ 107, IFLAG1, IFLAG2, IFLAG3, IFLAG4, IFLAG5, IFLAG6	A 1470
	READ 107, NELEM, NNODE, NODBC, NMODE	A 1480
C		A 1490
	PRINT 108, TITLE, NELEM, NNODE, NODBC, NMODE	A 1500
	PRINT 109, ICOD1, ICOD2, ICOD3, ICOD4, ICOD5, ICOD6, ICOD7, ICOD8	A 1510
C		A 1520
	PRINT 110, IFLAG1, IFLAG2, IFLAG3, IFLAG4, IFLAG5, IFLAG6	A 1530
C		A 1540
	IDEBU=ICOD1	A 1550
	NNODED=NNODE	A 1560
	NELEMD=NELEM	A 1570
	NODBCD=NODBC	A 1580
	NBCD=2*NODBC	A 1590
	NMODED=NMODE	A 1600
	NDGRFD=2*NNODE	A 1610
	NWDTHD=20	A 1620
	NGACD=800	A 1630
	IDEBU=1	A 1640
C		A 1650
C		A 1660
C		A 1670
	CALL INPMESH (NPI, NPJ, NPK, E, POIS, DEN, UE, UPOIS, UDEN, NNODED, XORD, YORD, NNB, NODBCD, NELEMD)	A 1680
C		A 1690
	-----	A 1700
C		A 1710
C		A 1720
C		A 1730
C		A 1740
	CALL INPDYN (ACC, NGACD, DAMP, STRXI, STRYI, STRXYI, NELEMD, NMODED, UD)	A 1750
C		A 1760
	-----	A 1770
C		A 1780
	NEU=NMODE	A 1790
	NN=2*NNODE	A 1800
C		A 1810
	-----	A 1820
C		A 1830
	CALL MASS (NPI, NPJ, NPK, XORD, YORD, DEN, AJ, AK, BJ, BK, NNODED, SMASS, NDGRFD, NNB, NELEMD, VOL, IDEBU)	A 1840
C		A 1850
	-----	A 1860
C		A 1870
	CALL STIFF (E, POIS, COMM, NPI, NPJ, NPK, AJ, AK, BJ, BK, NNODED, ST, NDGRFD, NWDTHD, NELEMD, NODBCD, IDEBU)	A 1880
C		A 1890
	-----	A 1900
C		A 1910
	CALL STATDIS (NNB, STI, ST, B, NDGRFD, NWDTHD, NODBCD, IDEBU)	A 1920
C		A 1930
	-----	A 1940
C		A 1950
	CALL MFREQ (NNB, NEBC, NODBCD, ST, STI, NNODED, NWDTHD, EU, W, BINF, NMODED, 1AEIG, NDGRFD, SMASS, R, NBCD, UE, UDEN, E, UW, VALFA, UBETA, KST, OMEGAM, OMEGA2K, VOL, UDM, IDEBU)	A 1960
C		A 1970
	-----	A 1980
C		A 1990
	TIME SHIFTS OF BASE DEGREES OF FREEDOM	A 2000
C		A 2010
	NTSTEPD=NTSTEP+3	A 2020
	IF (IFLAG2) 103, 101, 103	A 2030
C	101 KK=NNB(1)	A 2040
	-----	A 2050
C		A 2060
	XD=XORD(KK)	A 2070
	DO 102 K=1, NODBC	A 2080
C		A 2090
	MK(K)=0	A 2100
		A 2110
		A 2120
		A 2130
		A 2140
		A 2150
		A 2160

```

      KK=NNB(K)
      DIST=ABS(XORD(KK)-XD)
      TK=DIST/RMUEL
      XMK=TK/DT
C
C
102 MK(K)=XMK
      NC=MK(NODBC)
      GO TO 105
103 DO 104 K=1,NODBC
104 MK(K)=0
      NC=1
105 LK=NC+1
      LLKU=LK
C
C
      -----
      CALL DYNDIS (NPI,NPJ,NPK,POIS,COMM,E,STI,AEIG,W,DAMP,BINF,ACC,NMOD
1ED,STRXI,STRYI,STRXYI,NELEMD,AJ,AK,BJ,BK,NNODED,MK,NTSTEPD,NODBCD,
2NGACD,NDGRFD,NWDTHD,DSX,DSY,VEL,C4,CS,F,ACCEL,DXZERU,U,DIS,YH,YU,R
3,UOL,UH,UD,UE,UPOIS,VDEN,UDM,UACD,UACH,UBD,UDW,UHOR,UVER,DSUX,DSUY
4,LLKU,UCXX,UCYY)
C
C
      -----
      FORMAT STATEMENT
C
C
      STOP
C
106 FORMAT (12A6)
107 FORMAT (12I5)
108 FORMAT (1H112A6///,5X,51H NUMBER OF ELEMENTS-----
1-----,I3/,5X,51H NUMBER OF NODAL POINTS-----
2-----,I3/,5X,51H NUMBER OF BASE NODES-----
3-----,I3/,5X,51H NUMBER OF VIBRATIONAL MODES-----
4--,I3/)
109 FORMAT (5X,6BHCOB1 COD2 COD3 COD4 COD5 CJD6 COD7 CO
108 ,/,7X,12(I2,5X))
110 FORMAT (5X,6OHIFLAG1 IFLAG2 IFLAG3 IFLAG4 IFLAG5
1 IFLAG6,/,7X,12(I2,5X))
C
      END
      SUBROUTINE INPMESH (NPI,NPJ,NPK,E,POIS,DEN,UE,UPOIS,VDEN,NNODED,XO
1RD,YORD,NNB,NODBCD,NELEMD)
C
C
      *****
C
      READ INPUT DATA OF FINITE ELEMENT MESH
C
      REAL E(NNODED),POIS(NNODED),DEN(NNODED),UE(NNODED),UDEY(NNODED),UP
1OIS(NNODED),XORD(NNODED),YORD(NNODED)
      INTEGER NNB(NODBCD),NPI(NELEMD),NPJ(NELEMD),NPK(NELEMD)
C
      COMMON /MESH/ NNODE,NELEM,NODBC,NN,NDAND
C
      PRINT 111
      DO 101 M=1,NELEM
        READ 112, K,NPI(M),NPJ(M),NPK(M)
        PRINT 115, K,NPI(M),NPJ(M),NPK(M)
C
101 CONTINUE
C
C
      DO 102 I=1,NNODE
102 READ 108, E(I),UE(I)
      DO 103 J=1,NNODE
103 READ 108, POIS(J),UPOIS(J)
      DO 104 K=1,NNODE
104 READ 108, DEN(K),VDEN(K)
C
C

```

```

A 2170
A 2180
A 2190
A 2200
A 2210
A 2220
A 2230
A 2240
A 2250
A 2260
A 2270
A 2280
A 2290
A 2300
A 2310
A 2320
A 2330
A 2340
A 2350
A 2360
A 2370
A 2380
A 2390
A 2400
A 2410
A 2420
A 2430
A 2440
A 2450
A 2460
A 2470
A 2480
A 2490
A 2500
A 2510
A 2520
A 2530
A 2540
A 2550
A 2560
A 2570
A 2580
B 10
B 20
B 30
B 40
B 50
B 60
B 70
B 80
B 90
B 100
B 110
B 120
B 130
B 140
B 150
B 160
B 170
B 180
B 190
B 200
B 210
B 220
B 230
B 240
B 250
B 260
B 270
B 280
B 290
B 300

```

C	PRINT 109	B	310
C	DO 105 I=1,NNODE	B	320
C	105 PRINT 110, E(I),POIS(I),DEN(I)	B	330
C	PRINT 116	B	350
C	DO 106 M=1,NNODE	B	360
C	READ 113, K,XORD(M),YORD(M)	B	370
C	XORD(M)=XORD(M)*100.	B	380
C	YORD(M)=YORD(M)*100.	B	390
C	PRINT 117, K,XORD(M),YORD(M)	B	400
C	106 CONTINUE	B	410
C	PRINT 118	B	420
C	DO 107 K=1,NODBC	B	430
C	READ 114, M,NNB(K)	B	440
C	PRINT 119, M,NNB(K)	B	450
C	107 CONTINUE	B	460
C	RETURN	B	470
C	108 FORMAT (2F10.0)	B	480
C	109 FORMAT (//5X, 22HMOD.EL. POIS. DEN.,//)	B	490
C	110 FORMAT (5X,3(E15.3,2X))	B	500
C	111 FORMAT (2X, 28H ELEM.=I J K ,//)	B	510
C	112 FORMAT (4I4,3E12.4)	B	520
C	113 FORMAT (1I4,2F10.3)	B	530
C	114 FORMAT (1I5,1I5)	B	540
C	115 FORMAT (2X,4I4,3E12.4)	B	550
C	116 FORMAT (5X, 25H NODE X-ORD Y-ORD ,//)	B	560
C	117 FORMAT (5X,14,2F10.3,2X)	B	570
C	118 FORMAT (5X, 32H NODAL POINTS ON THE BASE )	B	580
C	119 FORMAT (5X,2I5)	B	590
C	END	B	600
C	SUBROUTINE INPBYN (ACC,NGACD,DAMP,STRXI,STRYI,STRXYI,NELEMD,NMODED	B	610
C	1,UD)	B	620
C	*****	B	630
C	READ INPUT DATA OF DYNAMIC ANALYSIS	B	640
C	REAL ACC(NGACD),STRXI(NELEMD),STRYI(NELEMD),STRXYI(NELEMD),DAMP(NM	B	650
C	1ODED),UD(NMODED)	B	660
C	COMMON /COD2/ ICOD5,ICOD6,ICOD7,ICOD8	B	670
C	COMMON /MESH/ NNODE,NELEM,NODBC,NN,NBAND	B	680
C	COMMON /DYNA/ NMODE,KOUNT,FLAG,TIME,RMUEL,DT	B	690
C	COMMON /DYNA1/ NTSTEP,NDTC,LK,NC,TLIMIT	B	700
C	PRINT 105	B	710
C	READ 106, NGAC,NTSTEP,NDTC,TLIMIT,DT,RMUEL	B	720
C	PRINT 110, NGAC,NTSTEP,NDTC,TLIMIT,DT,RMUEL	B	730
C	READ 107, (ACC(J),J=1,NGAC)	B	740
C	DO 101 I=1,NGAC	B	750
C	101 ACC(I)=ACC(I)*1000.	B	760
C	READ 108, (DAMP(N),UD(N),N=1,NMODE)	B	770
C	PRINT 111, (N,DAMP(N),N=1,NMODE)	B	780
C	DO 102 N=1,NELEM	B	790
C	STRXI(N)=0.	B	800
C	STRYI(N)=0.	B	810
C	102 STRXYI(N)=0.	B	820
C	IF (ICOD5) 104,103,104	B	830
C		B	840

```

103 READ 109, (M,STRXI(N),STRYI(N),STRXYI(N),N=1,NELEM) C 330
104 PRINT 112, (M,STRXI(N),STRYI(N),STRXYI(N),N=1,NELEM) C 340
RETURN C 350
C C 360
105 FORMAT (5X, 30HINPUT DATA OF DYNAMIC ANALYSIS,/) C 370
106 FORMAT (3I5,3F10.0) C 380
107 FORMAT (8F9.6) C 390
108 FORMAT (2F10.0) C 400
109 FORMAT (1I4,3F15.4) C 410
110 FORMAT (5X, 49H NGAC NTSTEP NDTL TLIMIT DT RMVEL,/, C 420
1, 14X, 3I5, 3F10.4) C 430
111 FORMAT (5X, 16H MODE DAMPING ,1X/, (15,1FB.5)) C 440
112 FORMAT (5X, 18H INITIAL STRESSES,1X/, 47H ELEMENT X-STRESS C 450
1 STRYRESS XY-STRESS,/, 5X, (1I10, 3F15.4)) C 460
C C 470
END C 480
SUBROUTINE MASS (NPI, NPJ, NPK, XORD, YORD, DEN, AJ, AK, BJ, BK, NNODED, SMAS D 10
S, NDGRFD, NELEMD, UOL, IDEBUG) D 20
C C 30
C ***** D 40
C C 50
C EVALUATION OF LUMPED MASSES AT NODES D 50
C C 55
C C 60
C COMMON /COD1/ ICOD1, ICOD2, ICOD3, ICOD4 D 80
COMMON /FLAG/ IFLAG1, IFLAG2, IFLAG3, IFLAG4, IFLAG5, IFLAG6 D 90
COMMON /MESH/ NNODE, NELEM, NODBC, NN, NBAND D 100
C D 110
REAL XORD(NNODED), YORD(NNODED), DEN(NNODED), AJ(NELEMD), AK(NELEMD), B D 120
J(NELEMD), BK(NELEMD), SMASS(NDGRFD), UOL(NNODED) D 130
INTEGER NPI(NELEMD), NPJ(NELEMD), NPK(NELEMD) D 140
C D 150
C C 160
C CALCULATING MASSES D 170
C D 180
C D 190
NN=2*NNODE D 200
DO 101 I=1, NN D 210
101 SMASS(I)=0. D 220
DO 104 N=1, NELEM D 230
I=NPI(N) D 240
J=NPJ(N) D 250
K=NPK(N) D 260
C D 270
DENS=(DEN(I)+DEN(J)+DEN(K))/3. D 280
AJ(N)=XORD(J)-XORD(I) D 290
AK(N)=XORD(K)-XORD(I) D 300
BJ(N)=YORD(J)-YORD(I) D 310
BK(N)=YORD(K)-YORD(I) D 320
AREA=(AJ(N)*BK(N)-BJ(N)*AK(N))/2. D 330
IF (AREA) 102, 102, 103 D 340
102 PRINT 108, N D 350
GO TO 106 D 360
103 DL=AREA*DENS/3. D 370
ROW=DL/10000. D 380
II=2*I-1 D 390
JJ=2*J-1 D 400
KK=2*K-1 D 410
SMASS(II)=SMASS(II)+ROW D 420
SMASS(JJ)=SMASS(JJ)+ROW D 430
SMASS(KK)=SMASS(KK)+ROW D 440
SMASS(II+1)=SMASS(II+1)+ROW D 450
SMASS(JJ+1)=SMASS(JJ+1)+ROW D 460
SMASS(KK+1)=SMASS(KK+1)+ROW D 470
C D 480
C ***** DEBUG ***** D 490
C D 500
IF (IDEBUG.EQ.1) GO TO 104 D 510
C D 520
PRINT 107, SMASS(II), SMASS(JJ), SMASS(KK), SMASS(II+1), SMASS(JJ+ D 530
1 ), SMASS(KK+1) D 540
104 CONTINUE D 550
C D 560

```

```

DO 105 I=1,NNODED
  II=2*I-1
105 VOL(I)=SMASS(II)*1000./DEN(I)
C
106 RETURN
C
107 FORMAT (5X,6(F10.3,2X)/)
108 FORMAT (2X, 37H ZERO OR NEGATIVE AREA, EL. NO. = ,I4)
C
END
SUBROUTINE STIFF (E,POIS,COMM,NPI,NPJ,NPK,AJ,AK,BJ,BK,NNODED,ST,ND
1GRFD,NWDTHD,NELEMD,IDEBUG)
C
*****
C
EVALUATION OF STIFFNESS MATRIX
C
REAL E(NNODED),POIS(NNODED),AJ(NELEMD),AK(NELEMD),BJ(NELEMD),BK(NE
1LEMD),ST(NDGRFD,NWDTHD)
C
COMMON /COD1/ ICOD1,ICOD2,ICOD3,ICOD4
COMMON /FLAG/ IFLAG1,IFLAG2,IFLAG3,IFLAG4,IFLAG5,IFLAG6
COMMON /MESH/ NNODE,NELEM,NODBC,NN,NBAND
COMMON /VOLM/ AREA
C
REAL A1(6,6),B1(6,6),S(6,6)
INTEGER NPI(NELEMD),NPJ(NELEMD),NPK(NELEMD),LM(3)
C
STIFFNESS MATRIX
C
DO 107 N=1,NELEM
C
  I=NPI(N)
  J=NPJ(N)
  K=NPK(N)
  EMO= (E(I)+E(J)+E(K))/3.
  POISR=(POIS(I)+POIS(J)+POIS(K))/3.
C
  IF (IFLAG1.GT.0) GO TO 101
  EMO=EMO/(1.-POISR**2)
  POISR=POISR/(1.-POISR)
101 CONTINUE
C
  AREA=(AJ(N)*BK(N)-AK(N)*BJ(N))*5
  COMM=.25*EMO/((1.-POISR**2)*AREA)
  A1(1,1)=BJ(N)-BK(N)
  A1(1,2)=0.
  A1(1,3)=BK(N)
  A1(1,4)=0.
  A1(1,5)=-BJ(N)
  A1(1,6)=0.
  A1(2,1)=0.
  A1(2,2)=AK(N)-AJ(N)
  A1(2,3)=0.
  A1(2,4)=-AK(N)
  A1(2,5)=0.
  A1(2,6)=AJ(N)
  A1(3,1)=AK(N)-AJ(N)
  A1(3,2)=BJ(N)-BK(N)
  A1(3,3)=-AK(N)
  A1(3,4)=BK(N)
  A1(3,5)=AJ(N)
  A1(3,6)=-BJ(N)
  B1(1,1)=COMM
  B1(1,2)=COMM*POISR
  B1(1,3)=0.
  B1(2,1)=COMM*POISR
  B1(2,2)=COMM
  B1(2,3)=0.
  B1(3,1)=0.
  B1(3,2)=0.

```

```

D 570
D 580
D 590
D 600
D 610
D 620
D 630
D 640
D 650
D 660
E 10
E 20
E 30
E 40
E 50
E 60
E 70
E 80
E 90
E 100
E 110
E 120
E 130
E 140
E 150
E 160
E 170
E 180
E 190
E 200
E 210
E 220
E 230
E 240
E 250
E 260
E 270
E 280
E 290
E 300
E 310
E 320
E 330
E 340
E 350
E 360
E 370
E 380
E 390
E 400
E 410
E 420
E 430
E 440
E 450
E 460
E 470
E 480
E 490
E 500
E 510
E 520
E 530
E 540
E 550
E 560
E 570
E 580
E 590
E 600
E 610
E 620

```



C	B1(3,3)=COMM*(1.-POISR)*.5	E	630
	DO 102 J=1,6	E	640
	DO 102 I=1,3	E	650
	S(I,J)=0.	E	660
	DO 102 K=1,3	E	670
102	S(I,J)=S(I,J)+B1(I,K)*A1(K,J)	E	680
	DO 103 J=1,6	E	690
	DO 103 I=1,3	E	700
103	B1(J,I)=S(I,J)	E	710
	DO 104 J=1,6	E	720
	DO 104 I=1,3	E	730
	S(I,J)=0.	E	740
	DO 104 K=1,3	E	750
104	S(I,J)=S(I,J)+B1(I,K)*A1(K,J)	E	760
C		E	770
	LM(1)=NPI(N)	E	780
	LM(2)=NPJ(N)	E	790
	LM(3)=NPK(N)	E	800
DO	107 L=1,3	E	810
	I=2*LM(L)-1	E	820
	II=2*L-1	E	830
DO	107 M=1,3	E	840
	IF (LM(L).GT.LM(M)) GO TO 107	E	850
	J=2*(LM(M)-LM(L))+1	E	860
	JJ=2*M-1	E	870
	ST(I,J)=ST(I,J)+S(II,JJ)	E	880
	ST(I,J+1)=ST(I,J+1)+S(II,JJ+1)	E	890
	IF (L-M) 105,106,105	E	900
105	ST(I+1,J-1)=ST(I+1,J-1)+S(II+1,JJ)	E	910
106	ST(I+1,J)=ST(I+1,J)+S(II+1,JJ+1)	E	920
107	CONTINUE	E	930
C		E	940
C		E	950
C	DETERMINATION OF THE HALF BAND WIDTH	E	960
C		E	970
	NB=2	E	980
DO	110 N=1,NELEM	E	990
	I=IABS(NPI(N)-NPJ(N))	E	1000
	J=IABS(NPI(N)-NPK(N))	E	1010
	K=IABS(NPJ(N)-NPK(N))	E	1020
	N1=MAX0(I,J,K)	E	1030
	IF (N1-15) 109,108,108	E	1040
108	PRINT 115, N	E	1050
	GO TO 113	E	1060
109	IF (N1.GT.NB) NB=N1	E	1070
110	CONTINUE	E	1080
C		E	1090
	NBAND=2*NB+2	E	1100
	MM=NBAND	E	1110
	PRINT 116, NBAND	E	1120
C		E	1130
	IF (ICOD2) 113,111,113	E	1140
111	REHIND 1	E	1150
	WRITE (1) ((ST(I,J), I=1,NN), J=1,NBAND)	E	1160
C		E	1170
C	***** DEBUG *****	E	1180
C		E	1190
	IF (IDDEBUG.EQ.1) GO TO 113	E	1200
C		E	1210
	DO 112 I=1,NN	E	1220
	PRINT 114, (ST(I,J), J=1,NBAND)	E	1230
C		E	1240
C	PUNCH 20, (ST(I,J), J= 1, NBAND )	E	1250
C		E	1260
	112 CONTINUE	E	1270
C		E	1280
C	PUNCH 20, ( SMASS(I), I = 1.NN )	E	1290
C		E	1300
113	RETURN	E	1310
C		E	1320
	114 FORMAT (2X,8(F10.3,2X))	E	1330
		E	1340



C		F	690
	DO 107 I=1,NN	F	700
107	STI(I,K)=B(I)	F	710
108	CONTINUE	F	720
C		F	730
	IF (ICOD3) 109,111,109	F	740
C		F	750
109	DO 110 K=1,NODBC	F	760
	PRINT 112, K	F	770
	PRINT 113	F	780
	DO 110 N=1,NNODE	F	790
	NI=2*N-1	F	800
110	PRINT ,14, N,STI(NI,K),STI(NI+1,K)	F	810
111	RETURN	F	820
C		F	830
112	FORMAT (2X, 91H STATIC DISPL. DUE TO A UNIT DISPL. AT	F	840
	1 BASE NODE ORDERED NUMBER =,113/)	F	850
113	FORMAT (2X, 23H NP X-ORD Y-ORD )	F	860
114	FORMAT (2X,11B,2E20.6)	F	870
C		F	880
	END	F	890
	SUBROUTINE SOLVE (KKK,A,B,NUMEQD,NWDTHD)	G	900
C		G	910
C	*****	G	920
C		G	930
C	SOLUTION OF LINEAR SYSTEM OF EQUATIONS	G	940
C		G	950
C	REAL A(NUMEQD,NWDTHD),B(NUMEQD)	G	960
C		G	970
C	COMMON /MESH/ NNODE,NELEM,NODBC,NN,NBAND	G	980
C		G	990
C		G	1000
	MM=NBAND	G	1010
	IF (KKK.EQ.2) GO TO 104	G	1020
	MM=NBAND	G	1030
	IF (KKK.EQ.2) GO TO 104	G	1040
C		G	1050
C		G	1060
	NRS=NN-1	G	1070
	NR=NN	G	1080
	IF (KKK-1) 101,101,104	G	1090
101	DO 103 N=1,NRS	G	1100
	M=N-1	G	1110
	MR=MIN0(MM,NR-M)	G	1120
	PIVOT=A(N,1)	G	1130
	DO 103 L=2,MR	G	1140
	C=A(N,L)/PIVOT	G	1150
	I=M+L	G	1160
	J=0	G	1170
	DO 102 K=L,MR	G	1180
	J=J+1	G	1190
102	A(I,J)=A(I,J)+C*A(N,K)	G	1200
103	A(N,L)=C	G	1210
	GO TO 107	G	1220
104	DO 105 N=1,NRS	G	1230
	M=N-1	G	1240
	MR=MIN0(MM,NR-M)	G	1250
	C=B(N)	G	1260
	B(N)=C/A(N,1)	G	1270
	DO 105 L=2,MR	G	1280
	I=M+L	G	1290
105	B(I)=B(I)-A(N,L)*C	G	1300
	B(NR)=B(NR)/A(NR,1)	G	1310
	DO 106 I=1,NRS	G	1320
	N=NR-I	G	1330
	M=N-1	G	1340
	MR=MIN0(MM,NR-M)	G	1350
	DO 106 K=2,MR	G	1360
	L=M+K	G	1370
106	B(N)=B(N)-A(N,K)*B(L)	G	1380
107	RETURN	G	1390
C		G	1400

```

SUBROUTINE MFREQ (NNB,NEBC,NODBCD,ST,STI,NNODED,NWDTHD,EU,W,BINF,N
H 10
1MODE,AEIG,NDGRFD,SMASS,R,NBCD,VE,VDEN,E,UW,UALFA,UBETA,KST,OMEGAM
H 20
2,OMEGAK,UOL,UDM,IDEBUG)
H 30
C
H 40
C
*****
H 50
C
EVALUATION OF VIBRATIONAL MODES
H 60
C
COMMON /COD1/ ICOD1,ICOD2,ICOD3,ICOD4
H 80
COMMON /COD2/ ICOD5,ICOD6,ICOD7,ICOD8
H 90
COMMON /FLAG/ IFLAG1,IFLAG2,IFLAG3,IFLAG4,IFLAG5,IFLAG6
H 100
COMMON /MESH/ NNODE,NELEM,NODBC,NN,NBAND
H 120
COMMON /DYNA/ NMODE,KOUNT,FLAG,TIME,RMUEL,DT
H 130
COMMON /VOLM/ AREA
H 140
C
C
*****
H 150
C
REAL STI(NDGRFD,NWDTHD),EU(NMODED),W(NMODED),AEIG(NDGRFD,NMODED),B
H 160
1INF(NMODED,NODBCD),SMASS(NDGRFD),KST(NDGRFD),ST(NDGRFD,NWDTHD),R(N
H 170
2DGRFD,NWDTHD),E(NMODED),VE(NMODED),VDEN(NMODED),UW(NMODED),UALFA(N
H 180
3MODED),UBETA(NMODED),OMEGAM(NMODED,NMODED),OMEGAK(NMODED,NMODED),U
H 190
4OL(NMODED),UDM(NMODED,NODBCD)
H 200
C
H 210
C
INTEGER NNB(NODBCD),NEBC(NBCD)
H 230
C
H 240
C
COMPUTE AND PRINT FREQUENCIES
H 250
*****
H 260
C
IF (ICOD2) 110,101,110
H 270
101 CONTINUE
H 280
DO 102 I=1,NODBC
H 290
II=2*I-1
H 300
NEBC(II)=2*NNB(I)-1
H 310
102 NEBC(II+1)=NEBC(II)+1
H 320
C
H 330
REWIND 1
H 340
READ (1) ((ST(I,J),I=1,NN),J=1,NBAND)
H 350
C
H 360
-----
H 370
CALL BEING (AEIG,ST,R,W,SMASS,EU,NMODED,NDGRFD,NWDTHD),NEBC,NBCD,IDEBUG)
H 380
H 390
-----
H 400
C
H 410
PRINT 122
H 420
DO 103 J=1,NMODE
H 430
EU(J)=ABS(EU(J))
H 440
W(J)=SQRT(EU(J))
H 450
103 PRINT 123, J,W(J)
H 460
C
H 470
IF (ICOD8) 106,104,106
H 480
104 DO 105 N=1,NMODE
H 490
PRINT 124, N,W(N)
H 500
PRINT 125
H 510
DO 105 M=1,NMODE
H 520
KK=2*M-1
H 530
105 PRINT 125, M,AEIG(KK,N),AEIG(KK+1,N)
H 540
C
H 550
PUNCH OF FREQUENCIES AND MODE SHAPES
H 560
C
H 570
106 IF (ICOD7) 107,112,107
H 580
107 DO 108 N=1,NMODE
H 590
108 PUNCH 126, N,W(N)
H 600
DO 109 M=1,NMODE
H 610
DO 109 M=1,NMODE
H 620
KK=2*M-1
H 630
109 PUNCH 127, M,AEIG(KK,N),AEIG(KK+1,N)
H 640
GO TO 112
H 650
C
H 660
H 670
H 680
H 690
H 700
H 710
H 720

```

```

C      READ FREQUENCIES AND MODE SHAPES
C
110 READ 121, (W(N),N=1,NMODE)
    DO 111 N=1,NMODE
    DO 111 M=1,NMODE
        KK=2*M-1
111 READ 127, K,AEIG(KK,N),AEIG(KK+1,N)
    IF (ICOD8) 112,104,112
C
112 IF (ICOD6) 120,113,120
C
C      INFLUENCE COEFFICIENT MATRIX A(N,K)
C
113 DO 114 N=1,NMODE
    DO 114 K=1,NODBC
114 BINF(N,K)=0.
    DO 116 N=1,NMODE
    DO 116 K=1,NODBC
        TERM=0.
        UT=0.
        DO 115 L=1,NN
            UT=UT+AEIG(L,N)*STI(L,K)
C
115 TPART=TPART+AEIG(L,N)*SMASS(L)*STI(L,K)
C
        UDM(N,K)=UT
C
116 BINF(N,K)=TPART
    IF (ICOD3) 117,120,117
117 PRINT 128
    DO 118 N=1,NMODE
118 PRINT 130, (BINF(N,K),K=1,NODBC)
C
    DO 119 N=1,NMODE
119 PRINT 130, (UDM(N,K),K=1,NODBC)
C
C      -----
C
CALL EIGUNCR (SMASS,AEIG,ST,OMEGAM,OMEGAK,W,KST,UE,UBEN,UW,NDGRFD,
INWDTHD,NNODED,NMODED,UALFA,UBETA,E,UOL,IDEBUG)
C
C      -----
C
120 CONTINUE
    RETURN
C
121 FORMAT (12X,F15.8)
122 FORMAT (2X, 29H          MODE NO   FREQUENCY)
123 FORMAT (2X,1I12,1F15.5)
124 FORMAT (2X, 29H THE FREQUENCY OF MODE NUMBER,I4, 7H IS =,F10.4/
1)
125 FORMAT (2X,1I12,2E15.6)
126 FORMAT (1I12,1F15.8)
127 FORMAT (1I12,2E15.6)
128 FORMAT (2X, 40H PARTICIPATION COEFFICIENTS A(K,N) S )
129 FORMAT (2X, 43H NODAL POINT X-EIGEN COORD Y-EIGEN COORD )
130 FORMAT (2X,8F15.6)
C
    END
SUBROUTINE BEING (AEIG,A,R,W,SMASS,EU,NMODED,NDGRFD,NWDTHD,NEBC,NB
ICD,IDEBUG)
C
C      *****
C
C      EVALUATION OF THE NATURAL FREQUENCIES
C
    REAL SMASS(NDGRFD),AEIG(NDGRFD,NMODED),EU(NMODED),W(NDGRFD),R(NDGR
1FD,NWDTHD),A(NDGRFD,NDGRFD)
C
    COMMON /MESH/ NNODE,NELEM,NODBC,NN,NBAND

```

```

H 730
H 740
H 750
H 750
H 770
H 780
H 790
H 800
H 810
H 820
H 830
H 840
H 850
H 860
H 870
H 880
H 890
H 900
H 910
H 920
H 930
H 940
H 950
H 960
H 970
H 980
H 990
H 1000
H 1010
H 1020
H 1030
H 1040
H 1050
H 1060
H 1070
H 1080
H 1090
H 1100
H 1110
H 1120
H 1130
H 1140
H 1150
H 1160
H 1170
H 1180
H 1190
H 1200
H 1210
H 1220
H 1230
H 1240
H 1250
H 1260
H 1270
H 1280
H 1290
H 1300
H 1310
H 1320
H 1330
I 10
I 20
I 30
I 40
I 50
I 60
I 70
I 80
I 90
I 100
I 110

```

C	COMMON /DYNA/ NMODE,KOUNT,FLAG,TIME,RMUEL,DT	I 120
C	INTEGER NEBC(NBCD)	I 130
C	-----	I 140
C		I 150
C		I 160
C	INITIALIZE	I 170
C		I 180
C		I 190
C	MM=NBAND	I 200
C	IFLAG=0	I 210
C	NEU=NMODE	I 220
C		I 230
C		I 240
C		I 250
C	EIGENVALUE PROBLEM	I 260
C	-----	I 270
C		I 280
C	TRACE=0.	I 290
C	DO 102 I=1,NN	I 300
C	TRACE=TRACE+ABS(A(I,1))	I 310
C	X=SMASS(I)	I 320
C	IF (X.GT.0.) GO TO 101	I 330
C	PRINT 116, I	I 340
C	IFLAG=1	I 350
C	GO TO 102	I 360
C	101 SMASS(I)=1./SQRT(X)	I 370
C	102 CONTINUE	I 380
C	IF (IFLAG.NE.0) STOP	I 390
C	DO 103 I=1,NN	I 400
C	L=I-1	I 410
C	MR=MINO(MM,NN-I+1)	I 420
C	DO 103 J=1,MR	I 430
C	K=L+J	I 440
C	103 A(I,J)=A(I,J)*SMASS(I)*SMASS(K)	I 450
C		I 460
C	IMPOSE BOUNDARY CONDITIONS ON A	I 470
C		I 480
C	IF (NBCD.LE.0) GO TO 115	I 490
C	DO 104 N=1,NBCD	I 500
C	I=NEBC(N)	I 510
C	A(I,1)=100.*TRACE	I 520
C	DO 104 J=2,MM	I 530
C	A(I,J)=0.	I 540
C	L=I-J+1	I 550
C	IF (L.LE.0) GO TO 104	I 560
C	A(L,J)=0.	I 570
C	104 CONTINUE	I 580
C		I 590
C	***** DEBUG *****	I 600
C		I 610
C	IF (IDEBUG.EQ.1) GO TO 106	I 620
C		I 630
C	DO 105 I=1,NN	I 640
C	PRINT 117, (A(I,J),J=1,MM)	I 650
C	105 CONTINUE	I 660
C		I 670
C	MATRIX IN SYMETRIC MODE	I 680
C		I 690
C	106 DO 107 J=1,MM	I 700
C	N1=0	I 710
C	DO 107 I=MM-J+1,NN	I 720
C	R(I,J)=A(1+N1,MM-J+1)	I 730
C	N1=N1+1	I 740
C	107 CONTINUE	I 750
C		I 760
C		I 770
C	***** DEBUG *****	I 780
C		I 790
C	IF (IDEBUG.EQ.1) GO TO 109	I 800
C		I 810
C	DO 108 I=1,NN	I 820
C		I 830

```

          PRINT 117, (R(I,J),J=1,MM)
108 CONTINUE
109 CONTINUE
C
      IND=2
      NM=NDGRFD
C
C-----
C
      CALL RSBEIG (NM,MM,MM,R,IND,W,A)
C-----
C
***** DEBUG *****
C
      IF (IDBUG.EQ.1) GO TO 112
C
      DO 110 I=1,NN
110 PRINT , #W=#,W(I)
C
      DO 111 I=1,NN
111 PRINT 117, (A(I,J),J=1,NN)
C
112 CONTINUE
C
      DO 113 J=1,NEU
C
          EU(J) = W(J+NBC)
C
          EU(J)=W(J)
113 CONTINUE
C
      DO 114 I=1,NN
          X=SMASS(I)
          SMASS(I)=1./X**2
          DO 114 J=1,NEU
114 AEIG(I,J)=A(I,J)*X
C
115 RETURN
C
116 FORMAT (2X, 20H ONEG. OR ZERO MASS EQUATION, I5)
117 FORMAT (2X, 10(F10.3, 2X))
C
      END
      SUBROUTINE DYNDIS (NPI, NPJ, NPK, POIS, COMM, E, STI, AEIG, W, DAMP, BINF, AC
J 10
      IC, NNODED, STRXI, STRYI, STRXYI, NELEMD, AJ, AK, BJ, BK, NNODED, MK, NTSTEPD, N
J 20
      20DBCD, NGACD, NDGRFD, NWDTHD, DSX, DSY, VEL, C4, C5, F, ACCEL, DXZERO, U, DIS, Y
J 30
      3H, YU, R, UOL, UW, UD, UE, UPOIS, UDEN, UDM, VACD, UACH, UDD, UDW, UHOR, UVER, DSU
J 40
      4X, DSUY, LLKU, UCXX, UCYY)
J 50
C
C-----
C
*****
C-----
C
      EVALUATION OF DYNAMIC DISPLACEMENTS
C-----
C
      COMMON /FLAG/ IFLAG1, IFLAG2, IFLAG3, IFLAG4, IFLAG5, IFLAG6
J 120
      COMMON /MESH/ NNODE, NELEM, NODBC, NN, NBAND
J 130
      COMMON /DYNA/ NMODE, KOUNT, FLAG, TIME, RMVEL, DT
J 140
      COMMON /DYNA1/ NTSTEP, NDT, LK, NC, TLIMIT
J 150
      COMMON /MXSTR/ SMAX(50), SMIN(50), IMAX(50), IMIN(50), SMAXD(50), SMIND
J 160
      1(50), IMAXD(50), IMIND(50)
J 170
C
      REAL AJ(NELEMD), AK(NELEMD), BJ(NELEMD), BK(NELEMD), E(NELEMD), POIS(NN
J 180
      10DED), STRXI(NELEMD), STRYI(NELEMD), STRXYI(NELEMD), DSX(NNODED), DSY(N
J 190
      2NODED), ACC(NGACD), DAMP(NMODED), BINF(NMODED, NODBCD), AEIG(NDGRFD, NMO
J 200
      3DED), W(NMODED), VEL(NMODED), C4(NMODED), C5(NMODED), F(NMODED), ACCEL(N
J 210
      4MODED), DXZERO(NTSTEPD), U(NTSTEPD), DIS(NTSTEPD), STI(NDGRFD, NWDTHD),
J 220
      5YH(NNODED), YU(NNODED), R(LLKU, NNODED), UOL(NNODED), UOL(NNODED), UDEN(NNODED), UPOI
J 230
      6S(NNODED), UE(NNODED), UH(NNODED), UD(NMODED), UDM(NMODED, NODBCD), VACD
J 240
      7(NMODED), UACH(NMODED), UDD(LLKU, NMODED), UDW(LLKU, NMODED), UHOR(NNODE
J 250
      260

```

```

C      8D), UVER(NNODED), DSUX(NNODED), DSUY(NNODED)
C      DIMENSION UCXX(NNODED), UCYY(NNODED)
C      INTEGER NPI(NELEMD), NPJ(NELEMD), NPK(NELEMD), MK(NMODED)
C
C      INTEGRATION OF GROUND DISPLACEMENT USING SIMPSON RULE
C      *****
C      PRINT 150, DT
C      PRINT 153, (ACC(I), I=1, NTSTEP)
C      IF (IFLAG2) 105, 101, 105
101  DT2=DT/2.
      LIM=NT3STEP+2
      U(1)=DT2*(ACC(1)+ACC(2))
      DO 102 I=2, LIM
102  U(I)=U(I-1)+DT2*(ACC(I)+ACC(I+1))
      PRINT 154, DT
      PRINT 153, (U(I), I=1, NTSTEP)
      DT3=DT/3.
      DIS(1)=DT3*U(1)
      DO 103 I=3, LIM, 2
          L=(I+1)/2
103  DIS(L)=DIS(L-1)+DT3*(U(I-2)+4.*U(I-1)+U(I))
      LMAX=L-1
      DO 104 I=1, LMAX
          II=I*2-1
          DXZERO(II)=DIS(I)
104  DXZERO(II+1)=(DIS(I)+DIS(I+1))/2.
      PRINT 155, DT
      PRINT 153, (DXZERO(I), I=1, NTSTEP)
105  CONTINUE
C
C      KOUNT=0
C      KPRINT=0
C
C      CALCULATING RESPONSES OF NORMAL VIBRATIONAL MODES
C      MATRIX R
C      *****
C
C      DO 106 I=1, LK
C      DO 106 J=1, NMODE
106  R(I, J)=0.
      IND=0
      C1=DT/2.
      BETA=1./6.
      C2=BETA*DT**2
      C3=(.5-BETA)*DT**2
C
C      CASE OF TRAVELING BOUNDARY CONDITIONS
C
C      DO 108 N=1, NMODE
C      C4(N)=W(N)**2
C      C5(N)=2.*DAMP(N)*W(N)
C      F(N)=1.+C1*C5(N)+C2*C4(N)
C      VEL(N)=0.
C      ACCEL(N)=-ACC(1)
C      Y=6.
C      DO 107 NN=1, LK
C      AA=VEL(N)+C1*ACCEL(N)
C      BB=Y+DT*VEL(N)+C3*ACCEL(N)
C      ACCEL(N)=(-ACC(NN+1)-C5(N)*AA-C4(N)*BB)/F(N)
C      VEL(N)=AA+C1*ACCEL(N)
C
C      UACD(N)=-((C5(N)*AA)/DAMP(N))/F(N)**2
C      UACH(N)=-((C5(N)*AA)/W(N))-(2.*C4(N)/W(N))*BB)/F(N)**2
C      UDD(NN, N)=C2*UACD(N)
C      UDW(NN, N)=C2*UACH(N)

```

```

J 270
J 2
J 2.0
J 3.0
J 310
J 370
J 33
J 340
J 350
J 360
J 370
J 380
J 390
J 400
J 410
J 420
J 430
J 440
J 450
J 460
J 470
J 480
J 490
J 500
J 510
J 520
J 530
J 540
J 550
J 560
J 570
J 580
J 590
J 600
J 610
J 620
J 630
J 640
J 650
J 660
J 670
J 680
J 690
J 700
J 710
J 720
J 730
J 740
J 750
J 760
J 770
J 780
J 790
J 800
J 810
J 820
J 830
J 840
J 850
J 860
J 870
J 880
J 890
J 900
J 910
J 920
J 930
J 940
J 950
J 960
J 970
J 980

```



```

      Y=BB+C2*ACCEL(N)
107   R(NN,N)=Y
108   CONTINUE
C
C
109   KOUNT=KOUNT+1
      KPRINT=KPRINT+1
C
      IF (KOUNT-NC) 113,113,110
C
C       CASE OF NON TRAVELING BOUDARY CONDITIONS
C
110   DO 111 I=1,NC
      DO 111 J=1,NMODE
111   R(I,J)=R(I+1,J)
      DO 112 N=1,NMODE
          AA=VEL(N)+C1*ACCEL(N)
          BB=R(NC,N)+DT*VEL(N)+C3*ACCEL(N)
          ACCEL(N)=(-ACC(KOUNT+1)-C5(N)*AA-C4(N)*BB)/F(N)
          VEL(N)=AA+C1*ACCEL(N)
112   R(NC+1,N)=BB+C2*ACCEL(N)
          IND=IND+1
C
C       CALCULATION TOTAL DISPLACEMENT OF NODAL POINTS
C
113   IKOUNT=KOUNT-IND
C
      IF (KPRINT-NMTC) 139,114,114
114   KPRINT=0
      DO 117 KK=1,NMODE
          N=2*KK-1
          L=N+1
          YH(KK)=0.
          YU(KK)=0.
C
          UHOR(KK)=0.
          UVER(KK)=0.
C
          DO 116 K=1,NODBC
C
C              IF (KOUNT-MK(K)) 117,117,115
115          MM=IKOUNT-MK(K)
C
          DO 116 NI=1,NMODE
C
          HM=UDM(NI,K)*AEIG(N,NI)*R(MM,NI)
          HN=BINF(NI,K)*AEIG(N,NI)*UDH(MM,NI)
          HD=BINF(NI,K)*AEIG(N,NI)*UDD(MM,NI)
C
          URM=UDM(NI,K)*AEIG(L,NI)*R(MM,NI)
          URW=BINF(NI,K)*AEIG(L,NI)*UDW(MM,NI)
          URD=BINF(NI,K)*AEIG(L,NI)*UDD(MM,NI)
C
          UDX=HM**2*UDL(KK)*UDEN(KK)+HW**2*UW(NI)+HD**2*UD(NI)
          UDY=URM**2*UDL(KK)*UDEN(KK)+URW**2*UW(NI)+URD**2*UD(NI)
C
          UHOR(KK)=UHOR(KK)+UDX
          UVER(KK)=UVER(KK)+UDY
          HT=BINF(NI,K)*AEIG(N,NI)*R(MM,NI)
          YH(KK)=YH(KK)+HT
          UT=BINF(NI,K)*AEIG(L,NI)*R(MM,NI)
116   YU(KK)=YU(KK)+UT
117   CONTINUE
      DO 118 N=1,NMODE
C
          DSUX(N)=UHOR(N)
          DSUY(N)=UVER(N)
C
          DSX(N)=YH(N)

```

```

J 107
J 108
J 109
J 110
J 111
J 112
J 113
J 114
J 115
J 116
J 117
J 118
J 119
J 120
J 121
J 122
J 123
J 124
J 125
J 126
J 127
J 128
J 129
J 130
J 131
J 132
J 133
J 134
J 135
J 136
J 137
J 138
J 139
J 140
J 141
J 142
J 143
J 144
J 145
J 146
J 147
J 148
J 149
J 150
J 151
J 152
J 153
J 154
J 155
J 156
J 157
J 158
J 159
J 160
J 161
J 162
J 163
J 164
J 165
J 166
J 167
J 168
J 169
J 170

```

	DSY(N)=YU(N)	J 1710
C		J 1720
C		J 1730
C	118 CONTINUE	J 1740
C		J 1750
C	FLAG=0	J 1760
	119 IF (FLAG) 120,128,120	J 1770
	120 IF (IFLAG3) 137,121,137	J 1780
	121 IF (IFLAG4) 123,122,123	J 1790
	122 PRINT 156	J 1800
	123 DO 126 N=1,NNODE	J 1810
	DC 125 K=1,NODBC	J 1820
	IF (KOUNT-MK(K)) 126,126,124	J 1830
	MI=KOUNT-MK(K)	J 1840
C		J 1850
	YH(N)=STI(2*N-1,K)*DXZERO(MI)	J 1860
	YU(N)=STI(2*N,K)*DXZERO(MI)	J 1870
C		J 1880
	DSX(N)=DSX(N)+YH(N)	J 1890
	125 DSY(N)=DSY(N)+YU(N)	J 1900
	126 CONTINUE	J 1910
C		J 1920
	DO 127 I=1,NNODE	J 1930
	UCXX(I)=SQRT(ABS(DSUX(I)))/DSX(I)	J 1940
	UCYY(I)=SQRT(ABS(DSUY(I)))/DSY(I)	J 1950
	127 CONTINUE	J 1960
C		J 1970
	GO TO 130	J 1980
	128 EN=KOUNT	J 1990
	TIME=EN*DT	J 2000
	IF (TIME-TLIMIT) 129,129,137	J 2010
	129 PRINT 157, TIME	J 2020
C		J 2030
	IF (IFLAG4) 137,130,137	J 2040
	130 CONTINUE	J 2050
	IF (FLAG) 142,131,133	J 2060
C		J 2070
	131 PRINT 143	J 2080
	PRINT 144	J 2090
	PRINT 159	J 2100
	DO 132 I=1,NNODE	J 2110
	132 PRINT 158, I,DSX(I),DSY(I)	J 2120
C		J 2130
	133 CONTINUE	J 2140
	PRINT 145	J 2150
	PRINT 144	J 2160
	PRINT 159	J 2170
	DO 134 I=1,NNODE	J 2180
	134 PRINT 158, I,DSX(I),DSY(I)	J 2190
C		J 2200
	PRINT 146	J 2210
	DO 135 I=1,NNODE	J 2220
	135 PRINT 147, I,DSUX(I),DSUY(I)	J 2230
	PRINT 148	J 2240
	DO 136 J=1,NNODE	J 2250
	136 PRINT 147, J,UCXX(J),UCYY(J)	J 2260
C		J 2270
	IF (FLAG) 137,138,137	J 2280
C		J 2290
C	-----	J 2300
C		J 2310
C		J 2320
	137 CALL STRESS (NPI,NPJ,NPK,NELEMD,AJ,AK,BJ,BK,E,POIS,COIM,NNODED,STR	J 2330
	IXI,STRYI,STRXYI,DSX,DSY,UE,UW,UPDIS,DSUX,DSUY,NMODED)	J 2340
C		J 2350
C	-----	J 2360
C		J 2370
	GO TO 139	J 2380
	138 FLAG=1	J 2390
	GO TO 119	J 2400
	139 IF (KOUNT-NTSTEP) 109,140,140	J 2410
C		J 2420



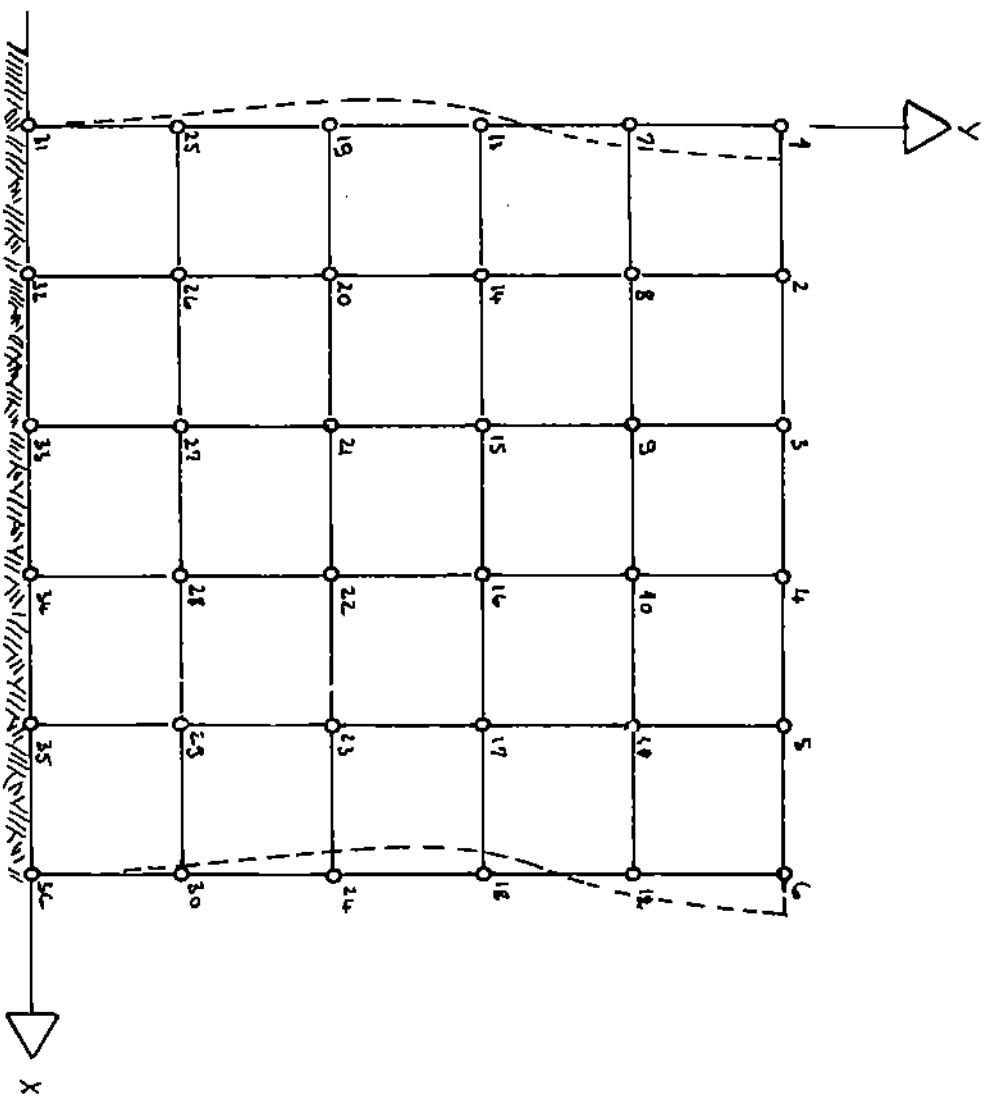
	SMAX(N)=CENT+RAD	K	370
	SMIN(N)=CENT-RAD	K	380
	SMAXD(N)=SMAX(N)	K	390
	SMIND(N)=SMIN(N)	K	400
	101 CONTINUE	K	410
C		K	420
	FUH=0.	K	430
	DO 102 I=1,NMODE	K	440
	102 FUH=FUH+UW(I)	K	450
C		K	460
C		K	470
	DO 111 N=1,NELEM	K	480
	I=NPI(N)	K	490
	J=NPJ(N)	K	500
	K=NPK(N)	K	510
C		K	520
	EMOD=(E(I)+E(J)+E(K))/3.	K	530
	POISR=(POIS(I)+POIS(J)+POIS(K))/3.	K	540
	FUE=(UE(I)+UE(J)+UE(K))/3.	K	550
	FUPOIS=(UPOIS(I)+UPOIS(J)+UPOIS(K))/3.	K	560
C		K	570
C		K	580
	EPSILX=(BJ(N)-BK(N))*DSX(I)+BK(N)*DSX(J)-BJ(N)*DSX(K)	K	590
	EPSILY=(AK(N)-AJ(N))*DSY(I)-AK(N)*DSY(J)+AJ(N)*DSY(K)	K	600
	GAMA=(AK(N)-AJ(N))*DSX(I)-AK(N)*DSX(J)+AJ(N)*DSX(K)+(BJ(N)-BK(N)	K	610
1	))*DSY(I)+BK(N)*DSY(J)-BJ(N)*DSY(K)	K	620
	COMM=EMOD/((1.-POISR**2)*(AJ(N)*BK(N)-AK(N)*BJ(N)))	K	630
	STRX=COMM*(EPSILX+POISR*EPSILY)+STRXI(N)	K	640
	STRY=COMM*(EPSILY+POISR*EPSILX)+STRYI(N)	K	650
	STRXY=COMM*GAMA*(1.-POISR)*.5+STRXYI(N)	K	660
C		K	670
C		K	680
C		K	690
C		K	700
	EVALUATION OF STATISTICAL CHARACTERISTICS OF STRESSES	K	680
		K	690
		K	700
	EXW=(BJ(N)-BK(N))*DSUX(I)+BK(N)*DSUX(J)-BJ(N)*DSUX(K)	K	710
	EYW=(AK(N)-AJ(N))*DSUY(I)-AK(N)*DSUY(J)+AJ(N)*DSUY(K)	K	720
	GW=(AK(N)-AJ(N))*DSUX(I)-AK(N)*DSUX(J)+AJ(N)*DSUX(K)+(BJ(N)-BK(N)	K	730
1	))*DSUY(I)+BK(N)*DSUY(J)-BJ(N)*DSUY(K)	K	740
C		K	750
C		K	760
	SXW=COMM*(EXW+POISR*EYW)	K	770
	SYW=COMM*(EYW+POISR*EXW)	K	780
	SXYW=COMM*GW*(1.-POISR)*.5	K	790
C		K	800
C		K	810
	SXE=COMM*(EPSILX+POISR*EPSILY)/EMOD	K	820
	SYE=COMM*(EPSILY+POISR*EPSILX)/EMOD	K	830
	SXYE=COMM*GAMA*(1.-POISR)*.5/EMOD	K	840
C		K	850
C		K	860
	DCOM=(1.-POISR)*2.*AREA	K	870
	SXN=COMM*EPSILY+(EPSILX+POISR*EPSILY)*(EMOD*2.*AREA*2.*POISR)/D	K	880
1	COM**2	K	890
	SYN=COMM*EPSILX+(EPSILY+POISR*EPSILX)*(EMOD*2.*AREA*2.*POISR)/D	K	900
1	COM**2	K	910
	SXYN=-COMM*GAMA*.5-GAMA*POISR*(EMOD*2.*AREA*2.*POISR)/DCOM**2	K	920
C		K	930
C		K	940
	USTX=(FUH*SXW**2)+(FUE*SXE**2)+(FUPOIS*SXN**2)	K	950
	USTY=(FUH*SYW**2)+(FUE*SYE**2)+(FUPOIS*SYN**2)	K	960
	USTXY=(FUH*SXYW**2)+(FUE*SXYE**2)+(FUPOIS*SXYN**2)	K	970
C		K	980
C		K	990
	CENT=(STRX+STRY)/2.	K	1000
	RAD=SQRT(((STRY-STRX)/2.)**2+STRXY**2)	K	1010
	SIGMAX=CENT+RAD	K	1020
	SIGMIN=CENT-RAD	K	1030
	TAUMAX=(SIGMAX-SIGMIN)/2.	K	1040
	IF (TIME-TLIMIT) 103,103,111	K	1050
C		K	1060
103	CONTINUE	K	1070
	COFSTX=SQRT(ABS(USTX))/STRX	K	1080

```

C          COFSY=SQRT(ABS(USTY))/STRY                                K 1090
C          PRINT 114, N, STRX, STRY, STRXY, SIGMAX, SIGMIN, TAUMAX   K 1100
C          PRINT 112, USTX, USTY                                    K 1110
C          IF (FLAG) 104, 111, 104                                  K 1120
104         IF (SMAXD(N)-SIGMAX) 105, 106, 106                      K 1130
105         SMAXD(N)=SIGMAX                                         K 1140
C          IMAXD(N)=KOUNT                                           K 1150
106         IF (SMIND(N)-SIGMIN) 111, 111, 107                     K 1160
107         SMIND(N)=SIGMIN                                         K 1170
C          IMIND(N)=KOUNT                                           K 1180
C          IF (SMA(N)-COFSTX) 108, 109, 109                       K 1190
108         SMA(N)=COFSTX                                           K 1200
C          IMAX(N)=KOUNT                                           K 1210
109         IF (SMIN(N)-COFSY) 110, 111, 111                      K 1220
110         SMIN(N)=COFSY                                           K 1230
C          IMIN(N)=KOUNT                                           K 1240
111        CONTINUE                                               K 1250
C                                                                    K 1260
C          RETURN                                                  K 1270
C                                                                    K 1280
C                                                                    K 1290
112        FORMAT (2X, 10HUARIANCE ,3E14)                          K 1300
113        FORMAT (5X,103H ELEMENT X-STRESS Y-STRESS XY-STRESS   K 1310
1         MAX-STRESS MIN-STRESS MAX-SHEAR )                      K 1320
114        FORMAT (5X,1110,3F15.4,5X,4F15.2)                      K 1330
C                                                                    K 1340
C          END                                                    K 1350
C          SUBROUTINE EIGUNCR (SMASS,AEIG,ST,OMEGAM,OMEGAK,W,KST,VE,VDEN,UW,N
1DGRFD,NWTHD,NNODED,NMODED,VALFA,UBETA,E,UOL,IDEBUG)             L 10
C                                                                    L 20
C                                                                    L 30
C          *****                                               L 40
C                                                                    L 50
C          UNCERTAINTY ANALYSIS OF NATURAL FREQUENCIES           L 60
C                                                                    L 70
C                                                                    L 80
C          COMMON /MESH/ NNODE,NELEM,NODBC,NN,NBAND               L 90
C          COMMON /DYNA/ NMODE,KOUNT,FLAG,TIME,RMUEL,DT           L 100
C                                                                    L 110
C          REAL SMASS(NDGRFD),AEIG(NDGRFD,NMODED),ST(NDGRFD,NWTHD),W(NMODED)
1,VE(NMODED),VDEN(NMODED),UW(NMODED),VALFA(NMODED),UBETA(NMODED),KS
2T(NDGRFD),OMEGAM(NMODED,NMODED),OMEGAK(NMODED,NMODED),E(NMODED),UO
3L(NMODED)                                                         L 120
C                                                                    L 130
C                                                                    L 140
C                                                                    L 150
C          REAL NUMERM,NUMERK                                     L 160
C                                                                    L 170
C                                                                    L 180
C          STIFNESS + MASS TERMS                                  L 190
C                                                                    L 200
C          REWIND 1                                               L 210
C          READ (1) ((ST(I,J),I=1,NN),J=1,NBAND)                 L 220
C                                                                    L 230
C          DO 101 I=1,NNODED                                       L 240
C             II=I*2-1                                             L 250
C                                                                    L 260
C                                                                    L 270
C             KST(I)=ST(II,1)                                       L 280
101        CONTINUE                                               L 290
C                                                                    L 300
C          DO 102 J=1,NMODE                                         L 310
C             L=2*J-1                                               L 320
C             L2=2*J                                                L 330
C                                                                    L 340
C                                                                    L 350
C          AA=2./(NMODE*SMASS(L)**2)                               L 360
C          A2=2./(NMODE*SMASS(L2)**2)                              L 370
C          VALFA(L)=AA*VDEN(J)*(UOL(J)**2)                         L 380
C          VALFA(L2)=A2*VDEN(J)*(UOL(J)**2)                       L 390
C                                                                    L 400
C          BB=2./(NMODE*KST(L)**2)                                 L 410
C          B2=2./(NMODE*KST(L2)**2)                                L 420
C          UBETA(L)=BB*VE(J)*(KST(L)/E(J))**2                     L 430
C          UBETA(L2)=B2*VE(J)*(KST(L2)/E(J))**2*10000000.        L 440
102        CONTINUE                                               L 450

```

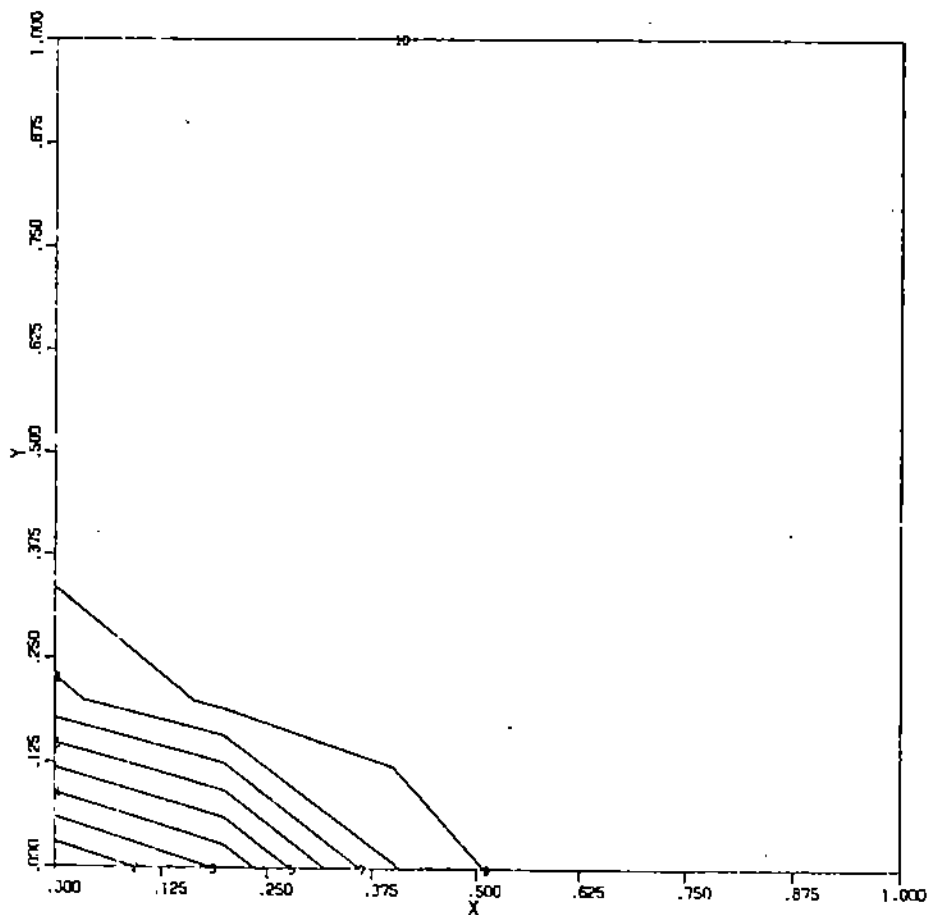
C		L	480
	COEF=0.	L	481
	DO 103 I=1,NMODE	L	480
	DO 103 J=1,NMODE	L	490
	COEF=COEF+(AEIG(J,I)**2)*SMASS(J)	L	500
C	103 CONTINUE	L	510
C		L	520
	K1=1	L	530
C	104 IF (K1.GT.NMODE) GO TO 106	L	540
C		L	550
	DO 105 I=1,NMODE	L	560
C		L	570
		L	580
	NUMERM=-(AEIG(I,K1)**2)*SMASS(K1)*W(K1)	L	590
	DENOMM=2.*COEF	L	600
C		L	610
	OMEGAM(K1,I)=NUMERM/DENOMM	L	620
C		L	630
	NUMERK=-(AEIG(I,K1)**2)*KST(K1)	L	640
	DENOMK=2.*W(K1)*COEF	L	650
C		L	660
	OMEGAK(K1,I)=NUMERK/DENOMK	L	670
C		L	680
	105 CONTINUE	L	690
C		L	700
	K1=K1+1	L	710
	GO TO 104	L	720
C	106 CONTINUE	L	730
C		L	740
	UMASS=0.	L	750
	USTIF=0.	L	760
	UWW=0.	L	770
	NMM=NMODE/2	L	780
C		L	790
	DO 108 II=1,NMM	L	800
	I=2*II-1	L	810
	DO 107 JJ=1,NMM	L	820
	J=2*JJ-1	L	830
	UWW=UWW+(OMEGAM(I,J)**2*VALFA(J)+OMEGAK(I,J)**2*UBETA(J))	L	840
C		L	850
	UMASS=UMASS+(OMEGAM(I,J)**2*VALFA(J))	L	860
	USTIF=USTIF+(OMEGAK(I,J)**2*UBETA(J))	L	870
C		L	880
	107 CONTINUE	L	890
C		L	900
	PRINT , UMASS,USTIF,UMASS,USTIF	L	910
	UW(I)=UWW	L	920
C	108 CONTINUE	L	930
C		L	940
	*****DEBUG*****	L	950
C		L	960
	IF (IDEBUG.EQ.1) GO TO 111	L	970
	PRINT , OMEGAM	L	980
C		L	990
		L	1000
	DO 109 I=1,NMODE	L	1010
C	109 PRINT 112, (OMEGAM(I,J),J=1,NMODE)	L	1020
	PRINT , OMEGAK	L	1030
	DO 110 I=1,NMODE	L	1040
C	110 PRINT 112, (OMEGAK(I,J),J=1,NMODE)	L	1050
C		L	1060
	111 CONTINUE	L	1070
C		L	1080
	PRINT , UARIANCEOFEIGENVALUES	L	1090
	PRINT 112, (UW(I),I=1,NMODE)	L	1100
C		L	1110
	STOP	L	1120
C		L	1130
	RETURN	L	1140
C		L	1150
	112 FORMAT (2X,11F12.6)	L	1160
		L	1170



SPATIAL DISTRIBUTION OF THE DISPLACEMENTS

AT TIME 1.3 sec

---



SPATIAL DISTRIBUTION OF THE DISPLACEMENTS

AT TIME 2.7 sec

---

