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USING SHOT PEENING TO MULTIPLY THE LIFE OF COMPRESSOR COMPONENTS

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ABSTRACT

Fatigue life increases, by orders of magnitude, can be expected
on compressor components treated by Shot Peening -- a controlled process that involves the bombardment of the metal component by millions
of spherical particles of steel, glass or ceramic. Shot Peening is
being applied to crankshafts and con-rods of huge reciprocating com-
pressors and to

HISTORICAL BACKGROUND.

Shot Peening was first used, in a production application, to ex-
tend the life of the valve springs for the Buick and Cadillac engines
of the early 1930s (Ref. 1). The process was discovered accidentally
and, although the

FIGURE 1. EXAMPLE OF RESIDUAL STRESS PROFILE CREATED BY SHOT PEENING.

In most applications for shot peening, the benefit obtained is the direct re-
sult of the residual compressive stress produced. A typical profile of residual
compressive stress as it changes with depth is shown. It has fou

1) ss- Surface stress- The stress measured at the surface. 2) CS max - Maximum Compressive
Stress - The maximum value of the
compressive stress induced, which
normally is highest just below the
surface. 3) d - Depth - The depth of the com-
pressive stress is the point at
which the compressive stress cross-
es over the neutral axis and becomes tensile.
4). The maximum value of the tensile
stress induced. The offsetting tensile
stress induced. The core of the mate-
sile stress in the core of the mate-
compressive stress so that the part
compressive stress s

% ULTIMATE TENSILE STRENGTH

Any applied tensile loads, affirmed Alman, would have to overcome this residual compression before a crack could start. Furthermore, Almen claimed that many parts (springs, for instance, from the coiling operation) had in them, from manufacturing, residual tensile stresses, that when added upon by the tensile loads, would further contribute to the part's early failure. Shot Peening, he said, reversed the surface residual stress from tension to compression, accounting for the very great improvements in fatigue life that are
typical of the process. The academic community was almost totally The academic community was almost totally opposed to John Alman's theories since, at the time, the presence of residual stresses in metals was not recognized in engineer1ng calculations. The advent of Fracture Mechanics eventually vindicated Almen's position. Today, we not only recognize residual (or self) stresses; we are able to measure them with a considerable degree of consistency, primarily by x-ray diffraction.

consideration Of Residual Stresses

If the part is dimensionally correct, are residual stresses all
that important, in a fatigue application? A very current case is an excellent illustration. A group of engineers are developing a torsion bar for a space application (the exact nature 1s "classified"). They carefully ground the test torsion bars to produce the final profile and a smooth surface. The unpeened torsion bars, at the applied load level, averaged close to a million cycles to failure and the stress analyst in the group figured from this information, that shot peening would about double the life of the bars, to two million cycles: sufficient for the application. To his surprise, the first (and only) Shot Peened torsion bar that they tested ran for 166 million cycles when the test was discontinued.

FIGURE 2. RESIDUAL STRESS IN 4340 STEEL (HRC 50) AFTER SURFACE GRINDING.

Graph shows the stress distribution
created by different grinding tech-
niques - conventional, abusive and
gentle. It is quite evident that
conventional grinding and abusive
grinding can generate high magni-
or near the su

The stress analyst had based his calculations on the assumption that the unpeened torsion bars were in a "neutral" state of stress before any loads were applied. In reality, the grinding operation had introduced residual tensile stresses, which in extreme cases can actually exceed the yield strength of the metal (Fig. 2, Ref. 3). failures at a million cycles were actually premature failures caused by the debiting effect of the grinding stresses. When the bars were

Shot Peened, the surface residual stresses were reversed, from close
to the yield strength in tension to close to the yield strength in
compression or a delta, in this case, of over 300 KSI. The Shot Peen-
ing actually rai

the stress level applied in the testing, contributing to virtually in-
finite life. Not all applications of Shot Peening are so dramatic
but this is a good reminder that residual stresses, detrimental or
bueficial, should more specific in discussing the benefits of Shot Peening for valve
reeds and rings since our unique success in this area has propelled reeds and rings since our unique success in this area has propelled
Metal Improvement Company to become one of the leading manufactures
of these very critical components.

SHOT PEENING FOR INDUSTRIAL AND AIRCRAFT COMPRESSORS

Reciprocating Compressors

1. Crankshafts are most commonly peened in the fillets of the

pins and mains to produce increases in fatigue strength of up to 30%.

Crankshafts have also been peened in the oil holes and keyway

FIGURE 3. INCREASE IN FATIGUE STRENGTH OF SHOT PEENED CRANKSHAFTS.

The most highly stressed area of a crankshaft is the crank pin bearing fillet.
The high stress point is the boottom side of the fillet when the pin is in the top
dead center position during the firing cycle. It is common f

2. Connecting Rods are usually peened prior to machining, to pre-
vent fatigue failures in the I-beam section but some large ones are
also peened in the oil holes and in the fillets by the bolts. Fret-
ting fatigue is prev

5. Tail Rod Cylinders are peened at the intersections of cross- bores to prevent crack initiation.

very high pressure (approaching 50,000 PSI) compressors. The Shot
Peening retards failures from bending and fretting fatigue.
7. Ring and Strip Valves are edge finished and peened for very
high cycle fatigue.

Cantrifygal Comprassors

Impellers have been Shot Peened that range in size from less than 2.inches in diameter for a spaca application to 48 inches for process air. Turbochargers fall under this classification and many are shot peened against blade failure. One unique application involved thermal cracking at some locating serrations on the back face of aluminum impellers for locomotive diesel turbochargers. Of concern was the heat that might relieve the compressive stresses form Shot Peening. However, peening solved the problem, using glass beads to avoid fer rous contamination of the aluminum.

Most of the smaller turbines employed in aircraft, sometimes for propulsion, but most often as auxiliary power units, air starters,
propulsion, but most often as auxiliary power units, air starters, etc., use Shot Peened impellers, as do the engines for the Cruise Missile. Significant weight reductions are possible by including the benefits of Shot Peening in the design calculations. Materials for impellers, incidentally, may be sand cast iron or aluminum, welded steel, forged aluminum or titanium; even investment cast superalloys: all respond well to Shot Peening.

Axial Compressors

Many are used in stationary applications (a good one is for making snow on the ski slopes), but most axial compressors are used in combination with a gas turbine to form a jet engine and provide propulsion for planes, boats and trains, and some experimental trucks. puision for pianes, buzes and virtual, axial and vibrational forces act-
Because of the extreme centrifugal, axial and the stigles are typi-
ing on the rotating components, a and fratting fatigue. In fact, cally Shot Peened against bending and fretting fatigue. In fact, there are very few components of a high performance jet engine that are not peened, both during original manufacture and again at periodic overhaul intervals, and include less obvious components such as gears and fuel lines.

Diaphragm Compressors
Diaphragm compressors are quite uncommon and are used in applications where absolutely no contamination (from lubricating oils, for instance) of the compressed gas is permitted. The critical component is a large (up to 30 inches diameter by d.030 inch thick) stainless steel diaphragm that is clamped around the edges in the compressor head. Because the diaphragm moves up and down under hydraulic pressure, cracks initiate just inside of the bolt hole ring. Typically, a chemical company, compressing Freon, used to replace these diaphragms every 16 hours of service. Peening the diaphragm with glass phragms every is nours of service. See the service life to 6 months.
beads (on stainless steel) extended the service life to 6 montagm and
The difficulty here is to peen the large but very that is encountered still maintain flatness: exactly the same problem that is encountered in peening the small valve reeds with which you are all fam1liar.

COMPRESSOR VALVE COMPONENTS

To quote D. N. Lal, Research Engineer at the Carrier Corporation: "The valve, suction or discharge, is one of the most critical components of a comoressor. A flapper valve is required to have high flexibil1ty to allow unrestricted fluid passage through the ports for achieving high efficiency and capacity of the compressor, but at the same time it is also expected to have enough stiffness to return back same time it is also expected to have energy motion subjects the valve
in time to seal the ports completely. The make the situation worse. to severe cyclic stresses and strains. To make the situation worse, to severe cyclic stresses and various here increases have irregular geometry as unavoidable design re-
quirements. This increases the possibility of localized stress con-
centration and premature failure by fatigue" (Ref. dispute Lal's statement but it leaves the designer of a compressor with having to make a serious compromise between the efficiency of with having to make a serious compromine. The more the flapper reed
the compressor and the life of the valve. The more the shorter will
flexes, the more passage of fluid it will permit but the shoaking. be the number of flexures the flapper will sustain before breaking. It is incumbent on the designer to seek a reed that will allow the maximum passage of fluid without breakage during the expected life of the compressor at, let's not forget, a cost that is within budget.

The geometry of the reed is usually the first consideration and
one over which the manufacturer of the reed has little control. Actu-
ally, the designers are much better served if they include the manu-
facturer at an earl

that will impact both on the life and the cost of a reed. The reed
maker must have a complete knowledge of materials; stresses (applied
and residual; beneficial and detrimental); how life is affected by
edge geometry, surf reed's ability to close totally. Overcoming this difficulty is the
province of a good reed maker and much has been done in this area.
Pursuing all of the above items to the maximum of current technology
will produce a reed ressor. Designers need to be aware of the options available to them.

Choice of Material
There is much information published by the suppliers of valve steels and it is not our province to review it in detail. High car-
bon strip is the choice for thin reeds and is supplied and stamped in
the pre-hardened condition. Nickel-alloyed steel is usually used for
thicker valves

FIGURE 4. STRESS CORROSION CRACKING.

Effect *of* shot peening with 40-80 m glass shot on the times to failure to type 304 and 347 stainless steels in a bo1ling 42S magnesium chloride solution,

Stamped Edges

A fatigue failure will always nucleate at the point of greatest stress concentration: somet1mes at an inclusion in the steel, but in the case of valve reeds, almost always at a surface defect created by the stamping operation (Ref. 7). All subsequent operations, i.e., edge rounding, removal of defects and introduction of beneficial stresses, are all performed primarily to remove or offset these sur face defects from stamping. The technology of producing good reeds tace defects from stamping.
is totally tied to the technique of producing stamped edges that are
as free from defects as possible. The importance of this will become
more apparent as we look at the subsequent operations.

Removal of Defects and Detrimental Stresses

There are a variety of processes available to the reed maker to, essentially, wear away the stamped edges and smooth out the stress concentrating defects. All are very time-consuming (and cost raising) and have limitations, especially from reed geometry. For instance, rough edges of narrow slots and small holes are very difficult to smooth out without loosing dimensions on the more exposed edges. starting with stamped edges that are essentially free of defects is paramount here. Also, the stamping operation introduces res1dual paramount nere. Theo, one over the reed. A good edge finishing
tensile stresses at the edges of the reed. A good edge finishing
process, such as STRESS-LITE, (Fig. 5, Ref. 8) will reverse these
detrimental residual tensile stresses but, again, starting with a near perfect stamping makes the stress reversal process not only more effective but, in some cases, even possible.

FIGURE 5. LCF OF SUCTION VALVE, IN THREE CONDITIONS.

The bar chart shows the performance of a particular valve for which filed fail-
ure data have been statistically related to a low cycle/high stress condition,
thereby permitting accelerated life testing. This suction valve

Edge Rounding

sending and torsional stresses are concentrated not only by notch es (surface defects) but also at sharp outside corners. Therefore, even if we had a theoretically perfect stamped edge, it would still be necessary to use processes that wi11 round the edges and distribute the applied stresses over a greater area. Here, again, the quality of the stamped edge is key: to the degree that the as-stamped edge is smooth, less edge-rounding is necessary. Too much edge finishing can produce a taper in the thickness of the reed on the sealing surface so that the reed will not close off the port. This may be difficult or even impossible to prevent if large defects from stamping must be removed in narrow slots to avoid fatigue.

Depth and Magnitude of Compressive Stresses

compressive stresses can be 1ntroduced by the correct edgefinishing process. They will be very shallow and of relatively low
magnitude but, in many cases, are sufficient for the application,
particularly if the stamped edges are near-perfect. magnitude but, in many cases, are sufficient for the application, particularly if the stamped edge are near-perfect are near-perfections of shot peening will, as we have seen in the earlier sections of

this paper, introduce much deeper residual compressive stresses and

of a magnitude approaching the yield strength of the steel. It does
so by indenting the surface so that the compressive stress is created
in the subsurface layer that can be thought of as trying to push the
indentation bac fatigue life, particularly if any are deeper than the layer of residu-
al compressive stress (Fig. 6).

FIGURE 6. STRESS-LITE **AND** SHOT PEENING.

STRESS-LITE is a proprietary process developed to control edge radius, improve
surface finish and to induce a high magnitude of residual compressive stress for in-
cheased fatigue life. The illustration is of a 2-cycle out

On a relatively thick part, say a quarter inch (6mm) or more, it
is quite easy to peen to a depth of 0.010 inch (0.25mm) to get below
surface discontinues. Peening very thin vally ereeds is an entirely
different propositi (Ref. 11). These and other tools and techniques are applied today to gain great improvements and repeatability in the fatigue life of modern valve reeds.

CONCLUSION

Controlled Shot Peening is used very effectively in the manufac-
ture of many components of both large and small compressors. Very
significant increases in life of valve reeds and rings can be
achieved with Shot Peening bu

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