

Power Electronics- The Enabling Technology for Renewable Energy Integration

Zhongting Tang, *Student Member, IEEE*, Yongheng Yang, *Senior Member, IEEE*,
and Frede Blaabjerg, *Fellow, IEEE*

Abstract— The drastically increased integration of renewable energy in the power grid is of significance in the transition to a sustainable energy future. The grid integration of renewables will be continuously enhanced in the future. According to the International Renewable Energy Agency (IRENA), renewable technology is the main pathway to reach zero carbon dioxide (CO₂) emissions by 2060. Power electronics have played and will continue to play an important role in this energy transition by providing efficient electrical energy conversion, distribution, transmission and utilization. Consequently, the development of power electronics technologies, i.e., new semiconductor devices, flexible converters and advanced control schemes, is promoted intensively across the globe. Among various renewables, wind energy and photovoltaic (PV) are the most widely used, and thus these are explored in this paper to demonstrate the role of power electronics. The development of renewable energies and demands of power electronics are reviewed first. The power conversion and control technologies as well as grid codes for wind and PV systems are then discussed. Future trends in terms of power semiconductors, reliability, advanced control, grid-forming operation and security issues for large-scale grid integration of renewables, and intelligent and full user engagement are especially presented at the end.

Index Terms— Grid integration, power electronics, wind turbine system (WTs), photovoltaic (PV) system, grid codes, advanced control, reliability

I. INTRODUCTION

THE raw material shortage and environmental pollution due to traditional energy sources (e.g., coal and oil) are the main obstacles to the global sustainable strategic plans. Following the Paris Agreement, it is required to achieve the energy-transition by the development and utilization of renewable energy sources (RESs). Many countries have thus made great efforts to change their energy paradigms by intensively integrating RESs, e.g., wind, solar photovoltaic (PV), bioenergy, and ocean wave energy [1]-[3]. For instance, Denmark plans to be 100% independent of fossil fuels and 100%

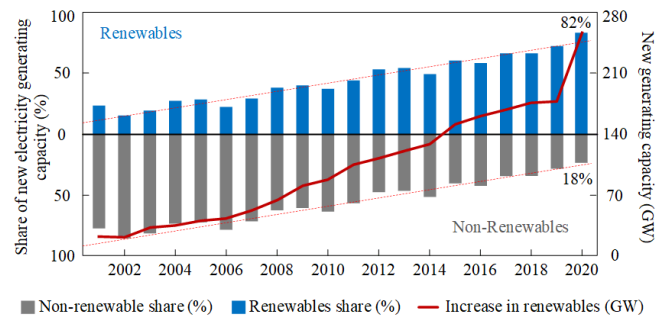


Fig. 1. Comparison of RESs and non-RESs as a share of the net total annual additions, where the net increase in global renewable generation reached 261 GW in 2020 [4].

carbon-neutral based on RESs by 2050 [2]. It is reported in [3] that Germany has rapidly increased the share of renewable energy in its electricity generation in past years, driven by strong policy support. Seen from the global landscape of renewable energy, the RES capacity has grown remarkably in the past two decades, as shown in Fig. 1 [4]. In addition, the development of global RESs from 2000 to 2020 has been depicted in Fig. 2, where wind and solar PV sources have the highest growth rates [4].

There are mainly two challenges along with the high penetration of RESs. One is how to friendly integrate large-scale RESs into the electrical grid, ensuring the network stability when injecting varying renewable power and also under grid disturbances. The other is how to achieve efficient, intelligent and reliable power conversion, transmission, distribution and utilization of the electrical energy by using power electronics. Accordingly, power electronics technologies have been developed at a fast pace, and the grid-integration standards are continuously being updated for RESs, especially wind and PV systems [5]-[12].

Regarding power electronics technology, many advancements have been done along with the development of power semiconductor devices, as shown in Fig. 3 [14]. From the first-generation power semiconductor devices (i.e., thyristors) in 1957 to the third generation of fully controlled power switches, e.g., insulated gate bipolar transistor (IGBT) and metal-oxide-semiconductor field-effect transistor (MOSFET) in the 2000s [15], [16], research efforts have mainly been put on gate drivers, circuit topologies, modeling and control strategies to achieve high switching frequencies (for high power density), low losses and high power handling capability in the power converter. As demonstrated in Fig. 3,

Manuscript submitted April 12, 2021. (Corresponding author: Yongheng Yang.)

Z. Tang and F. Blaabjerg are with the Department of Energy Technology, Aalborg University, Aalborg DK-9220, Denmark (e-mail: zta@et.aau.dk; fb@et.aau.dk).

Y. Yang is with the College of Electrical Engineering, Zhejiang University, Hangzhou 310027, China (e-mail: yang_yh@zju.edu.cn).

DOI: xxxxxxxxxxxxxxxx

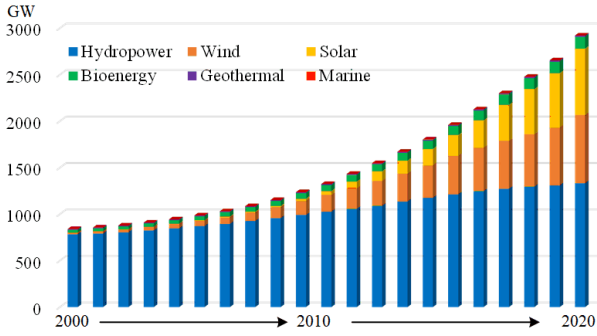


Fig. 2. Global accumulative capacity of RESs from 2000-2020 based on the data available from IRENA [4], in which hydropower covers pumped storage and mixed plants, wind contains both onshore and offshore wind energy, solar includes photovoltaics and solar thermal, and marine includes tide, wave and ocean energy.

the development of wide-bandgap (WBG) devices, e.g., silicon carbide (SiC) and gallium-nitride (GaN) power devices, brings the second revolution due to their superior performances in terms of high voltage/current stress, low power losses, high switching frequencies and high-temperature operation capability [17], [18]. On the other hand, opportunities of the WBG devices are usually accompanied by new challenges, e.g., packaging, thermal management and electromagnetic interference (EMI). Nevertheless, the advancement of semiconductor technologies has enhanced the large-scale grid integration of RESs, while lowering the system costs is still of concern, as always.

In the past, power converter topologies for low power RESs mainly focused on high power density and high efficiency, and must satisfy the requirement of the electrical isolation between the low voltage side and the grid [19]. Generally, such grid-connected converters can be classified into transformer-based and transformerless topologies. By comparison, the transformerless ones are more efficient, more compact, smaller in size, and less costly than the transformer-based converters. In addition, micro-inverters employed for low-power PV systems have the advantages of high voltage gain, plug-and-play and maintaining the maximum power point tracking (MPPT) for each PV panel [20]. On the contrary, power converters for large-scale RESs, e.g., wind power plants, pay more attention to high power level, high voltage and high reliability [21]. It has been seen in practical industrial applications that the use of power electronics in wind turbine systems has been shifted from partial-scale to full-scale levels, bringing more flexibilities and controllability in the system. Furthermore, to enhance the grid-integration of renewable energy, multiport converters are being studied to integrate energy storage devices [22]. Due to system cost limitations, these mainly focus on low power grid-connected RESs.

With the relatively small installation capacity of renewable energy in the past, the motivation of the control strategies for RESs is to satisfy the grid-following demands, e.g., high power quality and grid synchronization [6], [9]. Additionally, grid-supportive control is increasingly demanded. Moreover, protection is mainly designed to ensure stable and safe

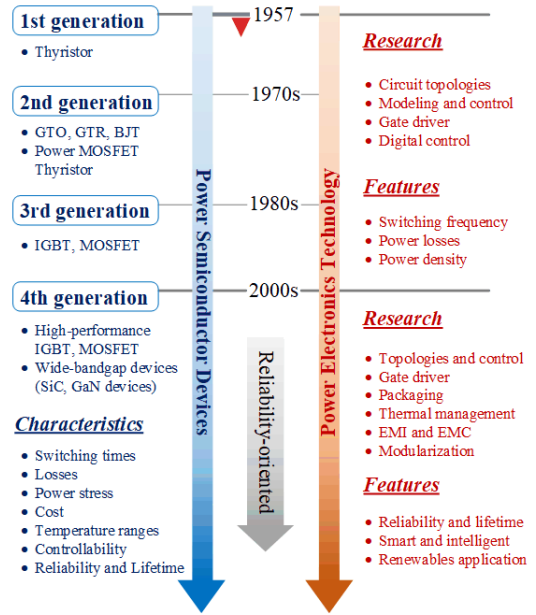


Fig. 3. Development of the power electronics technology along with the evolution of RESs and power semiconductor devices.

operation of RESs. However, with the continuous increase of grid-connected renewable energy, the stability of the grid is challenged in some areas. Consequently, control strategies for large-scale grid-connected RESs are now focusing on grid-forming capabilities, in order to enhance grid resiliency [5]. Furthermore, the RES with power converters should also intelligently respond to global management commands from system operators (e.g., limited power injection) as well as specific demands from the end-users (e.g., uninterrupted power supply). In addition, reliability-oriented control will be more and more significant to consolidate the grid integration.

This paper overviews the development of power electronics for efficient and reliable energy conversion from RESs, where wind and PV technologies will be focused on. In Section II, the typical architecture of RESs is briefly introduced, followed by a comprehensive review of the demands on wind and PV power systems, respectively. Then, technologies for wind and PV power systems are reviewed in terms of converter topologies and control strategies in Section III. In Section IV, challenges and research trends on future power electronics technologies for large-scale grid-integration of RESs are presented. Finally, Section V gives the conclusions.

II. REQUIREMENTS FOR RES

A. Typical RES architecture

A typical RES architecture is shown in Fig. 4, in which the power electronics converter is a critical interface to connect the renewable energy, the utility grid, the end-users and even the energy storage devices. As shown in Fig. 4, the power electronics converter undertakes the mission of transferring varying renewable energy into the utility grid with a constant voltage amplitude and a fixed frequency, and/or provide energy to local users. Therefore, demands to the power electronics are diverse and complex. It can be generally summarized as: 1)

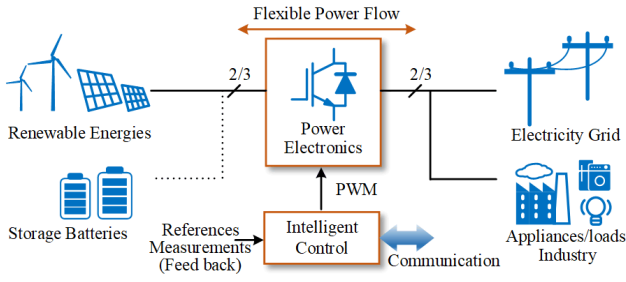


Fig. 4. Configuration of a typical grid-connected RES with power electronics converters and intelligent control.

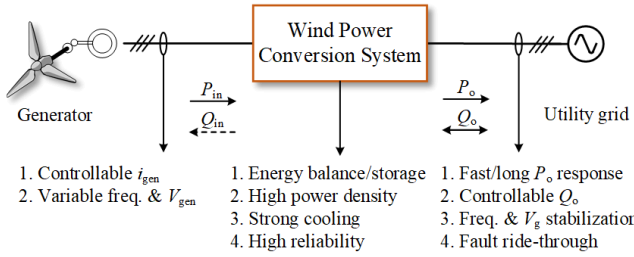


Fig. 5. Common demands on wind power systems, where P_{in} and Q_{in} are the active and reactive power transferred from the generator to the power converter, respectively, i_{gen} and V_{gen} are the generator current and voltage, respectively, P_o and Q_o are the active power and reactive power exchange between the power converter and the utility grid, respectively, and V_g is the grid voltage.

harvesting the maximum energy according to the characteristics of renewable energy; 2) producing the most energy with the least cost through power converters (related to power semiconductor devices and topologies), i.e., being high efficiency, high power density, low cost, and high reliability; 3) grid supporting capability (e.g., flexible power control and power management). The specific demands for wind and PV power systems are discussed in the following as well as certain grid integration requirements.

B. Demands on wind power systems

For wind power systems, a wind turbine harvests the wind energy as mechanical energy, and a generator converts it to electrical energy. Then, a power converter regulates the electrical energy to meet the requirements of the utility grid and/or local loads [23]-[25]. The specific demands on wind power systems are shown in Fig. 5, which can be summarized into three aspects:

(1) **Wind generator side** – The generator rotor or stator current is controlled by the power electronics converter to regulate the electromagnetic torque of the generator. The demands of the generator side current control are not only to harvest the maximum energy, but also to ensure energy balance when there is an inertia mismatch between the mechanical and the electrical power [23].

(2) **Utility grid side** – The requirements for wind energy grid-integration, including grid synchronization, response under abnormal grid conditions and grid supporting, aim to ensure safe operation with high integration of wind energy [5], [8], [26]. The most widely concerned demands are power quality, reactive power injection, frequency regulation, and fault ride-through operation. Furthermore, communication, power forecasting, ramp rate

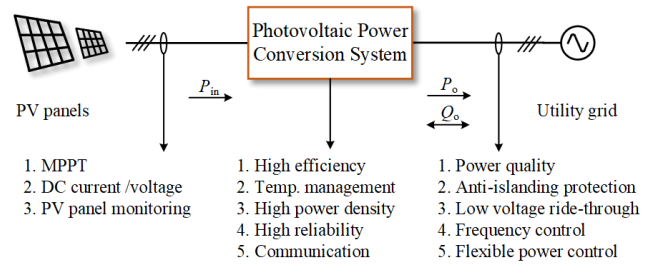


Fig. 6. Common demands on PV systems, where P_{in} is the active power from the PV panels to the power converter, and P_o and Q_o are the active and reactive power injected into the grid.

limitation and other requirements for offshore wind power plants are seen in practice [27].

(3) **Wind power conversion system side** – As being the core of the wind power system, failures of the power conversion stage will affect the entire system operation and lead to high maintenance costs, especially with a relatively large wind power capacity. Therefore, reliability becomes more and more significant in wind power systems [28], [29]. Furthermore, to ensure normal power transmission when connected to the grid, a transformer is usually adopted to boost the voltage level. In that case, power density and heat dissipation issues should be well addressed due to the limited physical space of the nacelle and tower in wind power systems. Moreover, energy storage/balancing capability should be integrated into the power conversion stage to avoid additional costs caused by the power mismatch between the wind turbine and the utility grid in very short term [23], [30].

C. Demands on PV power systems

Being different from wind power systems, solar PV energy is directly obtained through PV cells/panels using the *photovoltaic effect* in PV power systems without the mechanical energy conversion stage. As a result, the demands on PV power systems are less tough than wind power systems, although far stricter requirements should be complied with due to the remarkable expansion of solar PV installation [31]-[34]. The demands for PV power systems can be categorized as shown in Fig. 6.

(1) **PV panels side** – Similarly, maximum energy harvesting and good maintenance of the PV panels (i.e., PV panel monitoring) should be ensured to enhance high energy utilization as well as long lifetime of the system. Generally, a DC-DC converter employed as the first stage of PV inverters enhances the flexibility of power tracking [31]. Also, it extends the operation hours to some extent.

(2) **Utility grid side** – The requirements of PV systems have also been enhanced in terms of power quality, voltage/frequency regulation, and abnormal grid voltage protection and recovery, as illustrated in Fig. 6. For instance, the total harmonic distortion (THD) of the grid current must be lower than 5% [7], [12], [32]. Moreover, many existing grid-supporting demands in wind power systems become mandatory for PV systems, as the power capacity is increasing. For example, low-voltage ride-through (LVRT), frequency regulation and reactive power injection demands are now seen in IEEE Std. 1547-2018 (i.e., revision of IEEE Std. 1547-2003) [5], [35]-[38].

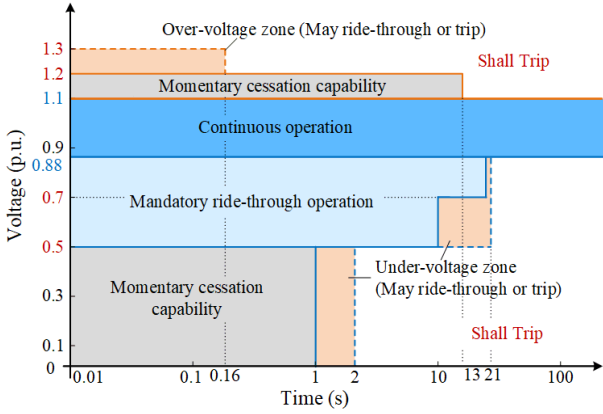


Fig. 7. Response for distributed energy resources (DERs) to abnormal grid voltages in the IEEE Std. 1547-2018 [5], including voltage ride-through requirements.

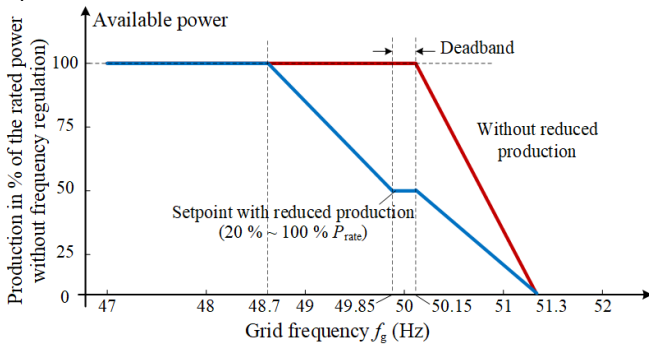


Fig. 8. Frequency regulation requirements for wind turbines connected to the grid [26], where f_g represents the grid frequency, and the wind turbine production can be limited to any power setpoint in the range of 20% ~ 100% of the rated power P_{rate} .

(3) **PV power conversion system side** – Although the price of PV panels is continuously decreasing, the cost-efficiency of the power capacity per generating unit in PV systems is relatively low. Power converters should be specially considered to lower the overall costs while increasing the efficiency. The transformerless PV inverters at low power levels are very promising alternatives with high efficiency as well as high power density [31], [39]. In that case, the leakage current issue becomes critical due to the parasitic capacitance between the PV panels and the ground. Accordingly, grid codes in [6] and [40] require that the leakage current should be suppressed below the limit (e.g., the root mean square (RMS) value should be lower than 300 mA) to ensure the safety of equipment and personnel. It is worth noting that reliability, directly affecting the stable operation and indirectly the system cost, becomes more important in power electronics for PV systems [41], [42]. Since the PV inverter always being the exposure in harsh environments or smaller housing, thermal management should be considered to enhance the reliability.

D. Grid integration requirements

It is well known that the most inherent characteristic of wind and solar energy is the weather-dependency, which means uncertainty and unpredictability are expected. In order to alleviate the impact of intermittency, the RESs, e.g., wind and PV power systems, should support the grid [11]. The main pathway includes predicting power production, flexible power

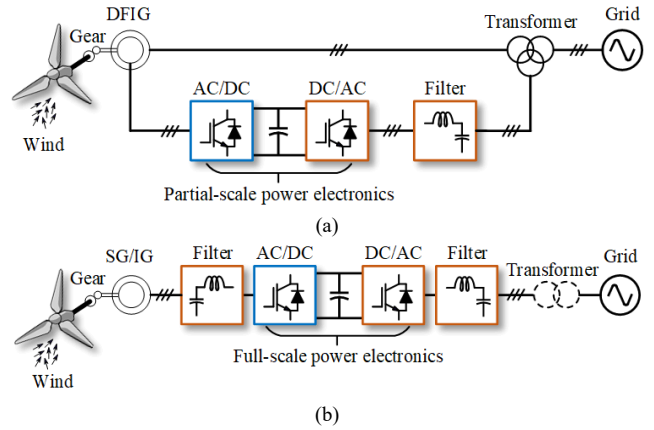


Fig. 9. Configurations of wind power systems based on variable speed wind turbines: (a) partial-scale power converter with a doubly-fed induction generator (DFIG) and (b) full-scale power converter with a synchronous generator (SG)/induction generator (IG).

control capability, and fast dynamics to the varying weather and operation conditions.

For instance, an unexpected disconnection may be triggered by a sudden grid voltage decrease, threatening the equipment and grid security, or even leading to a large-scale outage under a high-level penetration of renewable. To tackle this, the RESs must remain connected during this short period, which is exemplified as the mandatory ride-through operation area in Fig. 7. As shown in Fig. 7, the response time and voltage ride-through requirements for distributed energy resources (DERs) (including wind and solar PV energies) in IEEE Std. 1547-2018 are demonstrated [5]. It can be illustrated that the response for the abnormal voltage conditions becomes more flexible and controllable.

Furthermore, the RESs should have the voltage/frequency support during the fault ride-through operation, including the voltage-reactive power regulation and frequency-active power regulation [5], [32]. More specifically, in the case of LVRT operation, RESs can operate with the following regulation modes of reactive power: 1) constant power factor mode; 2) voltage-reactive power mode; 3) active power-reactive power mode; 4) constant reactive power mode [5]. Moreover, the transmission system operator can send commands for the reactive power injection to regulate and support the grid voltage. Notably, this reactive power control should be realized slowly (e.g., under the time constant of minutes) in steady-state. Referring to the requirements for the active power, the RESs should regulate the active power according to the grid frequency at the Point-of-Common-Coupling (PCC). As exemplified in Fig. 8, the production of the wind turbine can be limited to any power setpoint remotely. When the production is 100% of the rated power, the frequency control can only reduce the output power (see the red line in Fig. 8). In contrast, when the wind turbine operates with a certain level of power reduction, the output power can both be increased and decreased to regulate the frequency flexibly (see the blue curve in Fig. 8) [26]. In all, grid codes in many countries have been modified to ensure the reliability and stability of the large-scale

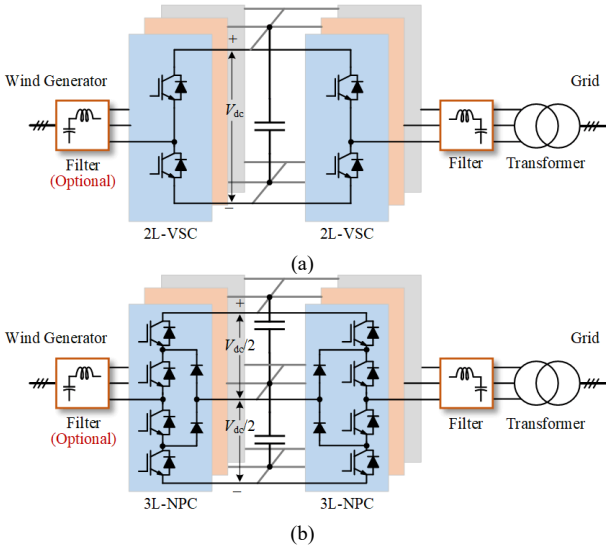


Fig. 10. Common power converters for wind power systems: (a) 2L-VSC back-to-back topology and (b) 3L-NPC back-to-back topology.

integration of renewables and will be more stringent and intelligent in the future.

III. POWER ELECTRONICS FOR RES INTEGRATION

As mentioned previously, the power electronics for RES grid-integration should not only consider the inherent characteristics of renewable sources, but also the grid requirements and energy transmission/distribution demands. Furthermore, more end-users preferences will be integrated to provide intelligent energy management, e.g., uninterrupted power supply. As one of the typical RESs, wind power systems have experienced from non-power-electronics-based concepts to full-scale power converter-based systems with the power rating per turbine being significantly increased [24], [43]. At the same time, the power electronics for PV systems have a remarkable evolution in terms of topologies and control strategies [31], [44]-[47]. Especially, the reliability-oriented control and the inertia enhancement strategies are popularly researched for both large-scale wind and solar PV power converters.

A. Wind power systems

1) System configurations

There exist several wind power system concepts depending on the types of generators, power electronics, speed controllability, and the way in which the aerodynamic power flows. Correspondingly, the power converters are various in those wind power systems with different generators and power rating levels. Till present, the Doubly-Fed Induction Generator (DFIG) with partial-scale power converters is still the mainstream configuration of wind power systems, as presented in Fig. 9(a) [23]. To develop efficient, reliable and compact wind turbine systems, full-scale power converter-based synchronous generators (SG)/permanent magnet synchronous generators (PMSG) or induction generators (IG) have taken an increasing part in the wind power system market, which is shown in Fig. 9(b). It is anticipated that the full-scale configuration will further cover the market of wind power

systems in the future along with the fast development of power electronics [23], [28].

2) Power converter topologies

Depending on the wind turbine system concepts, the power converter topologies vary. For instance, the most common power converter in the DFIG wind power systems is the two-Level Voltage Source Converter (2L-VSC), which has a simple structure with a limited power rating [23]. As depicted in Fig. 10 (a), the structure of a back-to-back (BTB) 2L-VSC is introduced, where the advantage is the full power controllability with a relatively simple structure and few components. This converter is a well-proven, robust and reliable solution to low-voltage wind power systems.

Comparatively, multi-level power converters are promising in wind power systems with higher voltages and higher power ratings [24], [25]. A three-Level Neutral Point Clamped (3L-NPC) BTB power converter is exemplified in Fig. 10 (b). Compared to the 2L-BTB converter, the 3L-NPC BTB topology can achieve less dv/dt stresses on the semiconductor devices and smaller filter inductors due to the multi-level output voltages. In that case, multi-level power converters are suitable to achieve the medium-voltage (MV) level power conversion with lower currents. It is worth noting that the mid-point voltage fluctuation of the DC-link should be well addressed for reliable operation, as investigated in [25], [48]. With the continuous expansion of the installed capacity in wind power systems, multi-cell converter configurations (i.e., converter unit modules are connected to be an array) are also becoming promising and will be further used in the wind turbine systems as the power level is increasing [21], [49]-[51].

3) Control

For wind power systems, the mechanical turbine and the power converters need to be controlled, where the time scales are different for various motivations [11]. According to the special demands in Fig. 5, the control of wind power systems typically includes three levels, as shown in Fig. 11. The control functions for the power converter system, i.e., the power interface between the wind turbine and the grid, are detailed in the following.

(1) **Basic control** – Like all the grid-connected converters, the basic control for wind power converters mainly considers current regulation, stabilization of the DC-link voltage, and grid synchronization [9]. The objective is to obtain efficient and reliable power conversion. In addition, the basic control should provide good steady-state and dynamic performances to ensure stable and safe operation.

(2) **Specific control** – Since the wind speed is varying, the generated power is also fluctuating. Therefore, the mechanical system and power converter should be properly controlled to maximize the energy harvesting by adjusting the rotational speed of the turbine. When the wind speed is lower than the rated value, the wind turbine can find an optimal pitch angle to achieve power optimization. If the wind speed exceeds the rated value, the pitch angle should be regulated to limit the generated power. In the normal grid-connected operation, the wind power systems should adopt proper current controllers to meet the power quality requirements.

(3) **Advanced control** – Notably, many advanced control functions for wind power converters are becoming introduced to enable an intelligent, reliable and grid-supportive system.

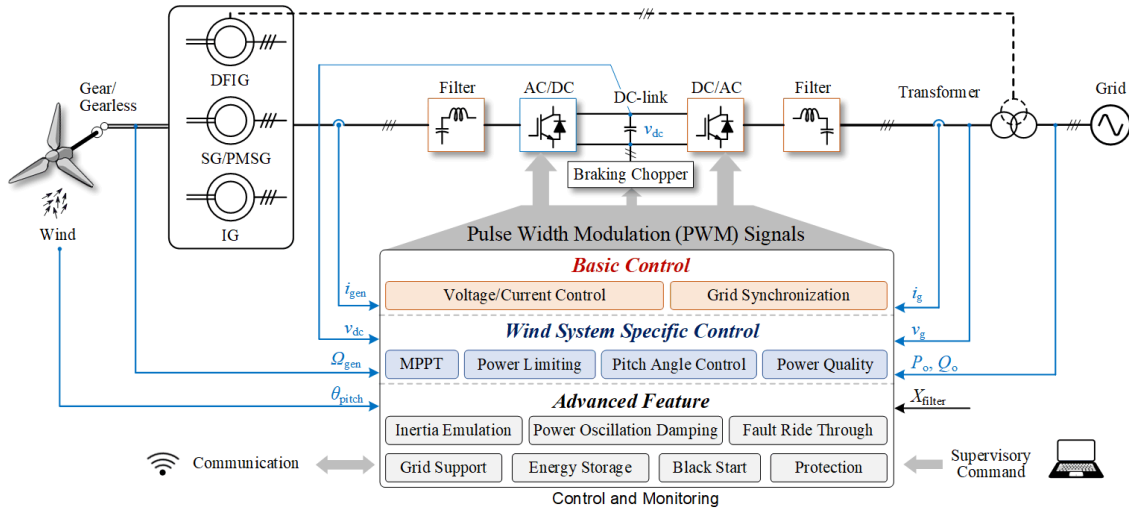


Fig. 11. General control structure for wind power systems.

For instance, the reliability-oriented control may be considered to ensure high availability and low maintenance costs, lowering the cost of energy in a long run, such as thermal control and the reliability evaluation approach for the wind power converter with energy storage [52], [53]. The response to grid faults (e.g., voltage ride-through operation) and grid support capability (injecting or absorbing reactive power) should be provided to ensure grid-friendly wind power systems. Subsystems in the wind turbine, e.g., generator/grid side converters, braking chopper/crowbar, and pitch angle controller, also need to be coordinated to ride through abnormal grid conditions, such as damping power oscillation and increasing the power inertia for recovery [55]-[54]. In addition, wind power systems should also enhance the resiliency to tolerate, adapt and recover from extreme events. This will become essential in future power electronics-based systems.

B. PV power systems

1) System configurations

Grid-connection PV configurations can be summarized into three types according to the power level, as presented in Fig. 12 [47], [57]. As shown in Fig. 12(a) and (b), considering an AC grid with the RMS voltage of 230 V per phase and the fundamental frequency of 50 Hz, the DC bus voltage for the two-stage PV inverters is typically 400 V for single-phase systems, and 700 V for three-phase systems where a tradeoff between the power quality and switching stress is also taken into account. Referring to the central PV inverters in Fig. 12(c), a wide range of the DC bus voltage up to 1500 V is required for PV systems to minimize the costs [58]. For low-power PV systems (e.g., below 1 kW), module-level converters are usually adopted to achieve the high MPPT efficiency of each PV panel, as demonstrated in Fig. 12(a). However, system costs are relatively high, and more power losses are generated when adopting a large number of module converters with a high voltage gain.

Consequently, string inverters are often preferred in residential and commercial grid-connected PV systems. As shown in Fig. 12(b), the configuration of the string inverter is demonstrated. Each string of PV panels employs a DC-DC

power optimizer and it is then connected to a string inverter. Although the MPPT efficiency for PV panels has a certain compromise, the PV systems can obtain high cost-effective performances in terms of conversion efficiency, power density, reliability and flexible control. Notably, multiple strings can be adopted to increase the overall system power.

As for large-scale PV power systems (e.g., commercial and utility-scale PV stations), the central inverter is widely employed due to its simple structure and control with lower overall system costs [47], as depicted in Fig. 12(c). For such a configuration, there are several challenges: (1) high voltage and current stresses on PV panels due to the high DC-link voltage and power level; (2) risk of low efficiency due to a global MPPT and mismatch of PV panels; (3) lower reliability caused by the high power diodes and one central inverter. To address the above issues, many central inverters adopted multi-level power converters for large-scale PV power systems with high voltage and high power, as well as parallel central inverters [59]. This, to some extent, might complicate the entire system.

2) Power converter topologies

Correspondingly, there are various inverter topologies in different grid-connected PV configurations, as shown in Fig. 14 [44]-[46], [59], [60]. As mentioned previously, different from wind power systems, PV systems harvest solar PV energy through PV panels. The parasitic capacitor between the PV panel and the ground should be carefully considered in practice. All grid codes/requirements for PV systems have a strict limitation on the leakage current, e.g., the RMS leakage current limitation and sudden leakage current limitation according to DIN VDE 0126 [40], [45]. Generally, PV inverters can adopt transformers to provide isolation having low leakage currents, while the overall system efficiency is low. Thus, transformerless inverters have been introduced in the PV industry, where the leakage current issue must be well addressed [45].

Micro-inverters are increasingly used to directly interface PV modules to the utility grid [44], [60]. These can enhance the energy harvesting per PV module. Micro-inverters have to boost the PV module voltage for grid-connection. High-frequency transformers are used in practice, such as the

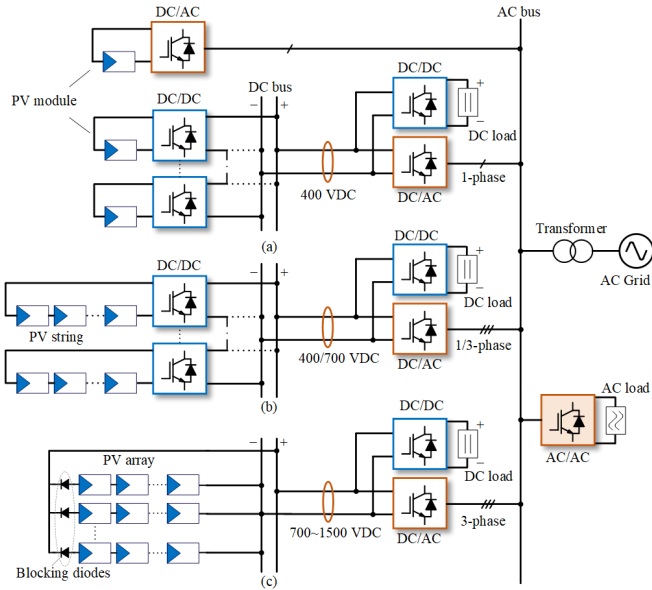


Fig. 12. Grid-connected PV configurations: (a) module-level converters for low-power applications (micro-inverters), (b) string inverters for medium or high-power PV systems, and (c) central inverters for utility-scale PV power stations, where DC-DC converters are optional to provide a wide range of PV input voltages.

commercial inverters of Sun-Sine and Dorfmueller DMI series [61], [62]. On the other hand, many step-up transformerless micro-inverters have been introduced [44]. The buck-boost integrated full-bridge micro-inverter is exemplified in Fig. 13(a) [63].

To process high power, while maintaining high efficiency, many advanced transformerless inverters have been developed [45], [46] for PV strings. Transformerless PV string inverters can be divided into two groups, i.e., DC-decoupling and AC-decoupling converters. For instance, the H5 inverter is a typical DC-decoupling inverter, while its leakage current suppression is affected by the parasitic capacitors of the power switches [45]. The highly efficient and reliable inverter concept (HERIC), as shown in Fig. 13(b), is an excellent AC-decoupling topology with good performance in leakage current suppression, conversion efficiency and reliability [64].

Several PV power plants have come into service for several years using central inverters (e.g., SMA Sunny Central CP XT inverter) and more are under construction. As mentioned previously, multilevel inverters are employed to tackle the issue of high voltage stresses, e.g., the 3L-NPC inverter adopted as the central PV inverter in Fig. 13(c) [59]. In addition, several central inverters are connected in parallel to share the current stresses and provide flexible power management. It should be noted that the line-frequency LV/MV transformers may be considered when being connected to the grid.

3) PV system control

Most of the demands on PV systems depicted in Fig. 6 should be achieved by controlling the PV inverter. Especially with the remarkable growth in the installation capacity, more and more advanced features have been required in addition to basic control of grid-connected inverters and PV system specific control. The multi-layer control functions, as presented in Fig. 14, are detailed in the following.

(1) **Basic Control** – Similar to wind power systems, the

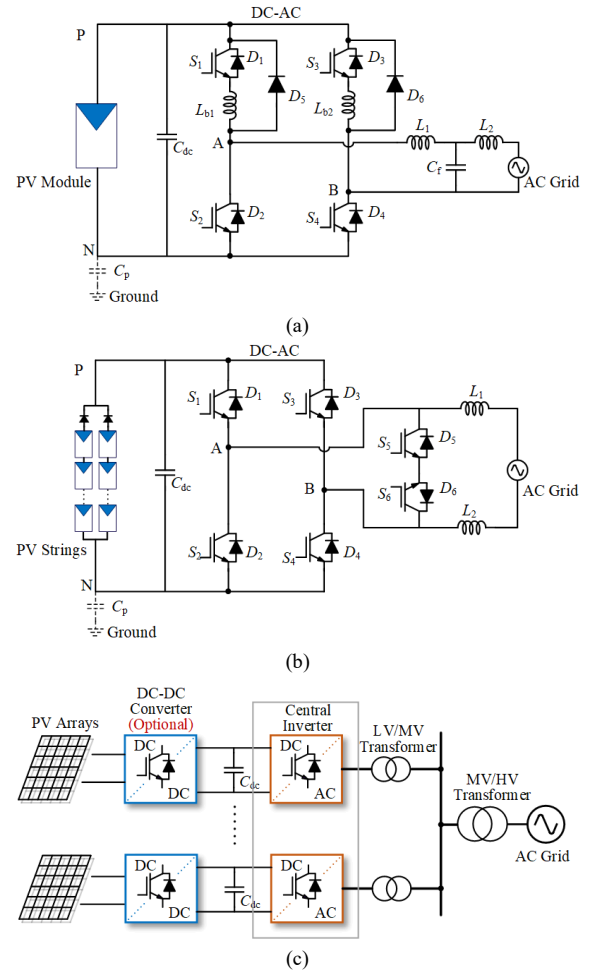


Fig. 13. Power converters for PV systems: (a) buck-boost integrated full-bridge micro-inverter, (b) transformerless PV string inverter (HERIC), and (c) central PV inverters (3L-NPC).

common basic control include voltage/current control and grid synchronization. Moreover, the basic control is generally to achieve good steady-state and dynamic performances, guaranteeing the power quality of the grid-connected PV system [65]. The basic controls are fundamental to PV system specific controls and advanced features.

(2) **Specific Control** – Power generation from solar PV systems is also uncertain and highly dependent on the weather/climate conditions. Thus, specific controls of inverters applied in PV systems contain the MPPT control, islanding protection, and seamless transition. In addition, the specific controls for wind systems are now mandatory in PV systems, as presented in IEEE 1547-2018 [5].

(3) **Advanced Feature** – Nowadays, reliability, fault ride-through and grid supporting capability are emphasized in PV systems. Correspondingly, more flexible power control is required [66], e.g., reactive power to regulate the grid voltage and active power to regulate the frequency. To achieve a long lifetime as well as high reliability, PV panels are employing system-level condition monitoring. Besides, reliability-oriented controls (e.g., power limiting control with weather forecasting and junction temperature control in the power modules [69]) are considered to enhance the reliability and lifetime.

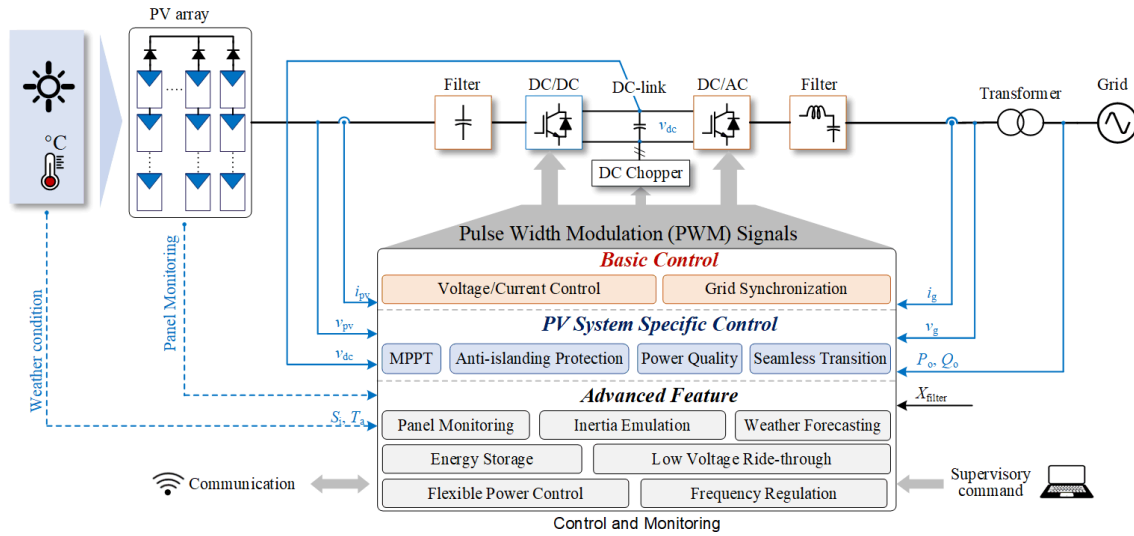


Fig. 14. General control structure for grid-connected PV systems, where many advanced schemes, e.g., delta power production control, virtual inertia controls, black start, power oscillation damping, implementation of virtual synchronous generators by energy storage, have been adopted to enhance the grid integration capability [67]-[72].

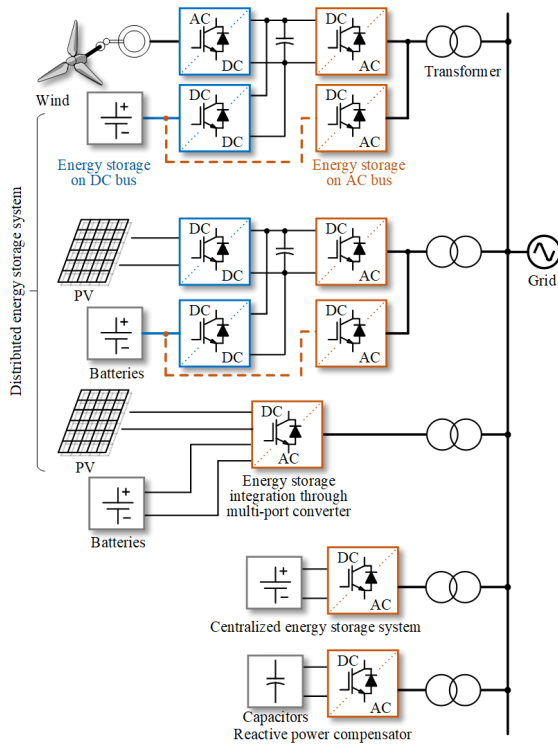


Fig. 15. Energy storage integration and reactive power compensator for grid support of wind and PV power systems.

C. Grid Support

To realize the “carbon neutrality” strategy [1] and the energy-transition, the grid support capability is very critical to achieve stable and reliable grid-integrated RESs. That means the energy must be balanced between the generators and the loads under any conditions, such as uncertain and non-dispatchable renewables, abnormal grid conditions and special demands from the operator or end-users. Consequently, many active and reactive power control strategies have been

studied to improve grid integration [72]-[76]. For instance, the power references can be obtained intuitively through the power control based on the PQ theory [66]. Droop control with the reactive power injection function is usually adopted when the line impedance is inductive [76].

In addition to controlling the power generation of renewable energies [70], [75], the energy storage system is a feasible option to enhance the active power control capability [72]-[74]. In California, energy storage must be required when installing grid-connected RESs [76]. To provide reactive power, the reactive power management capability has been integrated into RESs [76], [78]. Moreover, the centralized reactive power compensator is also a common device. Fig. 15 shows that wind and PV power systems adopt batteries and capacitors to achieve active and reactive power regulation, respectively. As demonstrated in Fig. 15, the distributed energy storage systems can be connected to both the DC-link and AC bus of wind and PV power systems by DC/DC converters or DC/AC converters, respectively. Recently, many stand-alone multiport converters have been developed to integrate energy storage batteries into RESs, achieving flexible configurations, high system efficiency, high power density, low device-count and simple control. Moreover, the centralized energy storage device and the reactive power compensator are directly connected to the AC grid. The above auxiliary devices, i.e., energy storage batteries and reactive power compensators in Fig. 15, can obtain an optimal operation point between cost and revenue growth [74]. In all, grid-friendly RESs have to minimize the impact on the grid operation, while also providing additional services.

IV. TRENDS IN POWER ELECTRONICS FOR RES INTEGRATION

A. Power devices

Power semiconductor devices are the key components to achieve energy conversion in terms of system cost, efficiency, power density, reliability, and modularity. The further development of power semiconductor devices can be

concluded in the following aspects:

(1) **Materials** – High-power silicon-based semiconductors have been the main components in power converters of RESs for several decades, e.g., IGBT and Integrated Gate Commutated Thyristor (IGCT). With the development of WBG devices, e.g., SiC and GaN power devices, more challenges are coming as well as advantages. On one hand, high switching frequencies and low power losses of WBG devices can improve the power density of power converters. On the other hand, challenges in the design of gate drivers and EMI issues should be considered, especially when the switching frequency of the WBG devices is becoming much higher, e.g., several MHz.

(2) **Packaging** –The conventional packaging technology for IGBT, which has the soldering and bond-wire connection of internal chips, has the disadvantages of larger thermal resistance, lower power density and higher failure rates [79], [80]. In order to increase the lifetime of the IGBT modules, improved technologies include the press-pack-based plate soldering, sinter technology to avoid the chip soldering, as well as replaced bond wire material to reduce the coefficient of thermal expansion [81], [82]. The press-pack technology improves the connection of chips by directly press-packing the contact, leading to low short-circuit failure, high power density and better cooling capability. Consequently, the press-pack devices, including the silicon-based and WBG devices, can be expected to become more utilized in the future [83].

Packaging technologies are significantly relevant to the lifetime of power semiconductor devices, further affecting the applications in RESs. Power semiconductors of power converters with high power levels in future large-scale grid-integrated RESs require high voltage/current stress. In addition to thermal management, compactness and failure rates, packaging technologies should have more considerations on the performance in terms of parasitic parameters (e.g., especially for WBG devices with high switching frequencies), explosion resistance and costs. Moreover, the better connection of power semiconductor devices in series or parallel is also an option to handle high power and high currents.

B. Reliability

One of the main goals of power converters for RESs is to achieve the highest energy conversion efficiency with the lowest system cost. Therefore, high reliability draws more and more attention [28], [29], and this will continue in the future as RES has to operate for 25~30 years [14]. In addition to improving the power converter structure and developing more advanced semiconductor devices (e.g., WBG devices), reliability-oriented control strategies are also promising to enhance the reliability performance.

Reliability-oriented design and control, including effective thermal management, robustness design and validation with the knowledge of mission profiles are gaining much interest. For instance, many attempts have been made on the thermal modeling of power devices and power converters to estimate the lifetime of the system, enabling the reliability-oriented design [53], [84]-[86]. Moreover, many control strategies aiming to improve thermal performance have been developed,

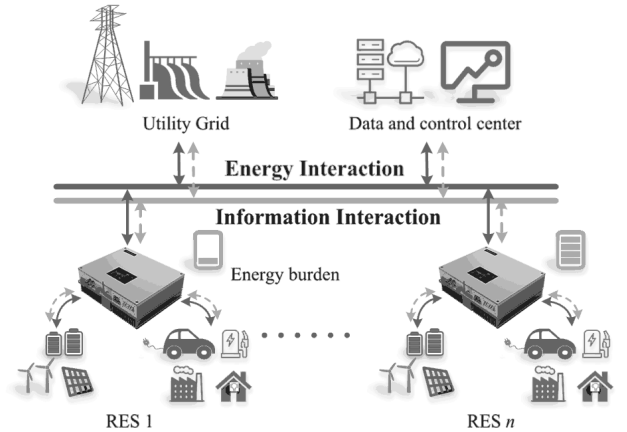


Fig. 16. Intelligent energy architecture for large-scale renewable energy grid integration.

such as junction temperature control during LVRT operation and hybrid control to reduce the thermal loading by flexible power regulation [84], [86]. In a word, the reliability will be more and more considered in future large-capacity renewable energy systems, and it will be more and more power electronics-based dependent.

C. Advanced control

The further deep integration of RESs and energy storage is an efficient path to realize energy balance, fault-tolerant and grid support capability, tackling issues caused by renewable fluctuation and abnormal grid conditions [87]. In addition, RESs with energy storage can be taken as an energy hub in the concept of energy Internet, which has intelligent cooperation management with the end-users and operators [88], [89]. In that case, power electronics will be equipped with many advanced control strategies, enabling thermal analysis and control, and energy cooperated control strategies (e.g., artificial intelligence-based and data-driven controls [90]).

Fig. 16 exemplified an energy Internet architecture, where the future power grid has a high penetration level of RESs. In such a system, energy storage must be integrated, which can be electric vehicles or stationary batteries. The infrastructure of the energy Internet contains the physical energy (e.g., RESs and the utility grid operator) and information networks (e.g., communication, data and control center). With comprehensive information and flexible power control capability, global, efficient and optimal energy management can be achieved for better power generation, transmission and distribution. With further integration of storage, the development of energy storage materials is also important [91].

D. Grid integration

To continue the energy transition with large-scale RESs, more stringent demands in terms of grid integration, cooperation, protection and end-user engagement are being updated. This makes RESs with 100% power electronic operate in the grid-forming mode or become more flexible [92]. As exemplified in Fig. 16, those RESs (e.g., consisting of wind/PV energies, converters, storage devices and loads) should thus consider such aspects in the future.

(1) **Storage**– Without synchronous generators, RESs with

100% power electronics have low inertia, resulting in poorer voltage and frequency regulation capability. Thus, storage energy devices should be integrated to replace the role of synchronous generators in grid regulation. This energy storage can be provided by specific batteries, electric vehicles and loads with certain energy storage. In this context, how to size the integrated energy storage devices in the design phase and, then how to better control the entire system to enhance the active/reactive power regulation capability to achieve enough inertia are of interest in future power grids. Coordinative operation of multiple energy sources should be optimal to maximize the economic benefit.

(2) **Converters** – As shown in Fig. 16, power converters for RESs with grid-forming operation should integrate energy storage devices into RESs. Multiport converters are promising solutions that enable flexible power control, high system efficiency, high power density and high reliability [22]. At the same time, many challenges, e.g., high power ratings and strong intermittency, should be considered when developing multiport converters for large-scale grid-integration of RESs.

(3) **Control** – To realize the operation of RESs with 100% power electronics, the frequency and voltage controls may significantly differ from the grid-following ones. The power converters should be controlled to be operating in the grid-forming mode, where the frequency and voltage control can be achieved as conveniently as that in the synchronous generators. In that case, the frequency and voltage control in the grid-forming mode should be properly addressed considering the utility grid stability and interaction with other sources and loads. Correspondingly, the operation range of the frequency and voltage may be redefined as well as future power systems stability indices. Moreover, the cooperation and communication with the distribution/transmission operators should be re-prioritized according to the time scale. Compared to the traditional grid-following RESs, the future grid-forming controls can achieve fast and intelligent voltage/frequency control and realize power dispatch without communication. In that case, the coordinative operation needs to consider the impacts of voltage/frequency controls under grid-forming operation [92].

(4) **Resiliency** – With large-scale RES integration, the unintentional disconnection of RESs will affect the stability of the grid (e.g., power outage). Thus, the grid resilience should be enhanced for RESs, which should have a strong tolerance of fault conditions, effective protections and emergency management for recovery. For instance, the updated IEEE 1547-2018 requires voltage/frequency ride-through [5]. Those fault-ride through operations and protections (e.g., current fault protections, anti-islanding protection and power swing blocking protection) should be flexibly and reasonably improved for the grid-forming operation of RESs with low inertia. Then, it becomes possible to minimize the disconnection incidents of RESs, increasing the security of power supply by RESs. After the elimination of faults, the voltage regulation should be enhanced for grid voltage recovery under the large-scale integration of RESs (i.e., weak grid conditions).

In all, with the further development of power electronics and the increasing demand for environmental-friendly energy generation, it can easily be anticipated that more and more

RESs will be integrated into the power grid. In such a landscape of energy, the power electronics are like the skeletons of human beings and underpinned by advanced control and information technologies, like the brain, and the grid integration will be more flexible and cost-effective. Eventually, it will help to reach global sustainability.

V. CONCLUSION

The development of renewable energy and power electronics (e.g., semiconductors and power converter systems) has been explored in this paper. Among those, grid-connected wind and PV systems have been discussed as the dominant RESs. Before reviewing power electronics technologies, stringent demands for wind and PV power systems have been summarized. Correspondingly, typical power converter topologies for wind and PV power systems were reviewed, as well as general control strategies. The investigation illustrated that the performance of reliability, conversion efficiency, grid resilience and system cost can be improved by enhancing the power converter topologies and control strategies. Finally, the challenging issues and research trends were introduced, i.e., power semiconductor devices (e.g., WBG devices), reliability aspects, advanced control and system operation. To conclude, power electronics are playing an essential role (will still do so) in the grid integration of renewable energy and realizing the energy transition for a sustainable and green society. This will be underpinned by advanced control and information technologies.

REFERENCES

- [1] International Renewable Energy Agency (IRENA), Reaching zero with renewables: Eliminating CO₂ emissions from industry and transport in line with the 1.5°C climate goal, Sep. 2020, https://www.irena.org/-/media/Files/IRENA/Agency/Publication/2020/Sep/IRENA_Reaching_zero_2020.pdf, last accessed Apr. 06, 2021.
- [2] DAMVAD & Kariros Future, "DK2050: Green growth in Denmark towards 2050 – Four future scenarios," Tech. Rep., 2nd edition, http://www.dac.dk/media/54231/Damvad_english_1007.pdf, last accessed Apr. 06, 2021.
- [3] International Energy Agency (IEA), Germany 2020: Energy policy review, https://www.bmwi.de/Redaktion/DE/Downloads/G/germany-2020-energy-policy-review.pdf?__blob=publicationFile&v=4, last accessed Apr. 06, 2021.
- [4] International Renewable Energy Agency (IRENA), Renewable capacity statistics 2021, Mar. 2021, https://www.irena.org/-/media/Files/IRENA/Agency/Publication/2021/Apr/IRENA_RE_Capacity_Statistics_2021.pdf, last accessed Apr. 06, 2021.
- [5] IEEE Standard Committee, *IEEE standard for interconnection and interoperability of distributed energy resources with associated electric power systems interfaces*, IEEE Std 1547-2018, pp. 1-138, Apr. 2018.
- [6] VDE-AR-N 4105, *Power generation systems connected to the low voltage distribution network-Technical minimum requirements for the connection to and parallel operation with low-voltage distribution networks*, Verband der Elektrotechnik, Aug. 2011.
- [7] Y. K. Wu, J. H. Lin and H. J. Lin, "Standards and guidelines for grid-connected photovoltaic generation systems: A review and comparison," *IEEE Trans. Ind. Appl.*, vol. 53, no. 4, pp. 3205-3216, July-Aug. 2017.
- [8] Y. Wu, S. Chang and P. Mandal, "Grid-connected wind power plants: A survey on the integration requirements in modern grid codes," *IEEE Trans. Ind. Appl.*, vol. 55, no. 6, pp. 5584-5593, Nov.-Dec. 2019.
- [9] F. Blaabjerg, R. Teodorescu, M. Liserre, and A.V. Timbus, "Overview of control and grid synchronization for distributed power generation

- systems," *IEEE Trans. Ind. Electron.*, vol. 53, no. 5, pp. 1398-1409, Oct. 2006.
- [10] J. M. Carrasco, L. G. Franquelo, J. T. Bialasiewicz, E. Galvan, R. C. P. Guisado, Ma. A. M. Prats, J. I. Leon, and N. Moreno-Alfonso, "Power-electronic systems for the grid integration of renewable energy sources: a survey," *IEEE Trans. Ind. Electron.*, vol. 53, no. 4, pp. 1002-1016, Jun. 2006.
- [11] F. Blaabjerg, Y. Yang, D. Yang, and X. Wang, "Distributed power generation systems and protection," in *Proc. IEEE*, vol. 105, no. 7, pp. 1311-1331, Jul. 2017.
- [12] R. Teodorescu, M. Liserre, and P. Rodriguez, *Grid converters for photovoltaic and wind power systems*. Hoboken, NJ: Wiley, 2011.
- [13] M. Liserre, T. Sauter, and J. Y. Hung, "Future energy systems: Integrating renewable energy sources into the smart power grid through industrial electronics," *IEEE Ind. Electron. Mag.*, vol. 4, no. 1, pp. 18-37, Mar. 2010.
- [14] H. Wang and F. Blaabjerg, "Power Electronics Reliability: State of the Art and Outlook," *IEEE J. Emerg. Sel. Top. Power Electron.*, early access, doi: 10.1109/JESTPE.2020.3037161.
- [15] H. F. Wolf, *Semiconductors*. New York: Wiley, 1971.
- [16] K. Shenai, R. S. Scott and B. J. Baliga, "Optimum semiconductors for high-power electronics," *IEEE Trans. Electron Devices*, vol. 36, no. 9, pp. 1811-1823, Sept. 1989.
- [17] K. Shenai, P. G. Neudeck, M. Dudley, and R. F. Davis, "High-power switching in semiconductors—What is beyond silicon thyristor?" in *Proc. of IEEE Energytech*, May 2011, pp. 1-6.
- [18] J. L. Hudgins, G. S. Simin, E. Santi, and M. A. Khan, "An assessment of wide bandgap semiconductors for power devices," *IEEE Trans. Power Electron.*, vol. 18, no. 3, pp. 907-914, May 2003.
- [19] S. Kouro, J. I. Leon, D. Vinnikov and L. G. Franquelo, "Grid-connected photovoltaic systems: An overview of recent research and emerging PV converter technology," *IEEE Ind. Electron. Mag.*, vol. 9, no. 1, pp. 47-61, Mar. 2015.
- [20] K. Alluhaybi, I. Batarseh and H. Hu, "Comprehensive review and comparison of single-phase grid-tied photovoltaic microinverters," *IEEE J. Emerg. Sel. Top. Power Electron.*, vol. 8, no. 2, pp. 1310-1329, June 2020.
- [21] B. Novakovic and A. Nasiri, "Modular multilevel converter for wind energy storage applications," *IEEE Trans. Ind. Electron.*, vol. 64, no. 11, pp. 8867-8876, Nov. 2017.
- [22] A. K. Bhattacharjee, N. Kutkut and I. Batarseh, "Review of multiport converters for solar and energy storage integration," *IEEE Trans. Power Electron.*, vol. 34, no. 2, pp. 1431-1445, Feb. 2019.
- [23] K. Ma, L. Tutelea, I. Boldea, D. M. Ionel, and F. Blaabjerg, "Power electronic drives, controls, and electric generators for large wind turbines—an overview," *Electr. Power Compon. Syst.*, vol. 43, no. 12, pp. 1406-1421, Jul. 2015.
- [24] M. Liserre, R. Cardenas, M. Molinas, and J. Rodriguez, "Overview of multi-MW wind turbines and wind parks," *IEEE Trans. Ind. Electron.*, vol. 58, no. 4, pp. 1081-1095, Apr. 2011.
- [25] K. Ma and F. Blaabjerg, "Multilevel converters for 10 MW wind turbines," in *Proc. of EPE*, pp. 1-10, 30 Aug. 2011-01 Sept. 2011.
- [26] Energinet - *Wind turbines connected to grids with voltages below 100 kV*, Regulation TF 3.2.6, Jan. 2003.
- [27] Tennen TSO GmbH, *Requirements for offshore grid connections in the crid of Tennen TSO GmbH*, Dec. 2012.
- [28] F. Blaabjerg, K. Ma, and D. Zhou, "Power electronics and reliability in renewable energy systems," in *Proc. of ISIE*, pp. 19-30, 28-31 May 2012.
- [29] H. Wang, M. Liserre, and F. Blaabjerg, "Toward reliable power electronics: challenges, design tools, and opportunities," *IEEE Ind. Electron. Mag.*, vol. 7, no. 2, pp. 17-26, Jun. 2013.
- [30] Y. Liu, W. Du, L. Xiao, H. Wang, S. Bu and J. Cao, "Sizing a hybrid energy storage system for maintaining power balance of an isolated system with high penetration of wind generation," *IEEE Trans. Power Systems*, vol. 31, no. 4, pp. 3267-3275, July 2016.
- [31] S. B. Kjaer, J. K. Pedersen, and F. Blaabjerg, "A review of single-phase grid-connected inverters for photovoltaic modules," *IEEE Trans. Ind. Appl.*, vol. 41, no. 5, pp. 1292-1306, Sept.-Oct. 2005.
- [32] Y. Yang, P. Enjeti, H. Wang, and F. Blaabjerg, "Wide-scale adoption of photovoltaic energy: grid code modifications are explored in the distribution grid," *IEEE Ind. Appl. Mag.*, vol. 21, no. 5, pp. 21-31, Sept.-Oct. 2015.
- [33] N. P. Papanikolaou, "Low-voltage ride-through concept in flyback inverter-based alternating current photovoltaic modules," *IET Power Electron.*, vol. 6, no. 7, pp. 1436-1448, Aug. 2013.
- [34] IEEE PES industry technical support leadership committee, *Impact of IEEE 1547 standard on smart inverters and the applications in power systems*, IEEE PES, pp. 1-87, Aug. 2020.
- [35] IEEE Standard Committee, *IEEE standard for interconnecting distributed resources with electric power systems*, IEEE Std 1547-2003, vol., no., pp.1-28, 28 Jul. 2003.
- [36] P. Rodriguez, A. V. Timbus, R. Teodorescu, M. Liserre, and F. Blaabjerg, "Flexible active power control of distributed power generation systems during grid faults," *IEEE Trans. Ind. Electron.*, vol. 54, no. 5, pp. 2583-2592, Oct. 2007.
- [37] G. M. S. Azevedo, G. Vazquez, A. Luna, D. Aguilar, and A. Rolan, "Photovoltaic inverters with fault ride-through Capability," in *Proc. of ISIE*, pp. 549-553, 5-8 Jul. 2009.
- [38] Y. Yang, F. Blaabjerg, and H. Wang, "Low voltage ride-through of single-phase transformerless photovoltaic inverters," *IEEE Trans. Ind. Appl.*, vol. 50, no. 3, pp. 1942-1952, May/Jun. 2014.
- [39] T. Kerekes, D. Sera, and L. Mathe, "Three-phase photovoltaic systems: structures, topologies, and control," *Electr. Power Compon. Syst.*, vol. 43, no. 12, pp. 1364-1375, Jul. 2015.
- [40] DIN VDE 0126, *Automatic disconnection device between a generator and the public low-voltage grid*, German Standard, 2010.
- [41] E. Koutroulis and F. Blaabjerg, "Design optimization of transformerless grid-connected PV inverters including reliability," *IEEE Trans. Power Electron.*, vol. 28, no. 1, pp. 325-335, Jan. 2013.
- [42] Y. Yang, H. Wang, and F. Blaabjerg, "Reliability assessment of transformerless PV inverters considering mission profiles," *Int. J. Photoenergy*, vol. 2015, 10 pages, 2015.
- [43] J. Fang, H. Li, Y. Tang and F. Blaabjerg, "On the inertia of future more-electronics power systems," *IEEE J. Emerg. Sel. Top. Power Electron.*, vol. 7, no. 4, pp. 2130-2146, Dec. 2019.
- [44] D. Meneses, F. Blaabjerg, O. Garcia, and J.A. Cobos, "Review and comparison of step-up transformerless topologies for photovoltaic AC-module application," *IEEE Trans. Power Electron.*, vol. 28, no. 6, pp. 2649-2663, Jun. 2013.
- [45] W. Li, Y. Gu, H. Luo, W. Cui, X. He and C. Xia, "Topology review and derivation methodology of single-phase transformerless photovoltaic inverters for leakage current suppression," *IEEE Trans. Ind. Electron.*, vol. 62, no. 7, pp. 4537-4551, July 2015.
- [46] M. N. H. Khan, M. Forouzesh, Y. P. Siwakoti, L. Li, T. Kerekes and F. Blaabjerg, "Transformerless inverter topologies for single-phase photovoltaic systems: A comparative review," *IEEE J. Emerg. Sel. Top. Power Electron.*, vol. 8, no. 1, pp. 805-835, March 2020.
- [47] Y. Yang, K. A. Kim, F. Blaabjerg, and A. Sangwongwanich, *Advances in Grid-Connected Photovoltaic Power Conversion Systems*. Cambridge, U.K.: Woodhead Publisher, Aug. 2018.
- [48] J. Rodriguez, S. Bernet, P.K. Steimer, and I.E. Lizama, "A survey on neutral-point-clamped inverters," *IEEE Trans. Ind. Electron.*, vol. 57, no. 7, pp. 2219-2230, Jul. 2010.
- [49] B. Andresen and J. Birk, "A high power density converter system for the Gamesa G10x 4.5 MW Wind turbine," in *Proc. of EPE*, pp. 1-7, 2-5 Sep., 2007.
- [50] M. Malinowski, K. Gopakumar, J. Rodriguez and M. A. Pérez, "A survey on cascaded multilevel inverters," *IEEE Trans. Ind. Electron.*, vol. 57, no. 7, pp. 2197-2206, July 2010.
- [51] N. Thitichaiworakorn, M. Hagiwara, and H. Akagi, "A medium-voltage large wind turbine generation system using an AC/AC modular multilevel cascade converter," *IEEE J. Emerg. Sel. Topics Power Electron.*, vol. 4, no. 2, pp. 534-546, Jun. 2016.
- [52] K. Ma and F. Blaabjerg, "Thermal optimised modulation methods of three-level neutral-point-clamped inverter for 10 MW wind turbines under low-voltage ride through," *IET Power Electron.*, vol. 5, no. 6, pp. 920-927, Jul. 2012.
- [53] Z. Qin, M. Liserre, F. Blaabjerg and P. C. Loh, "Reliability-oriented energy storage sizing in wind power systems," in *Proc. of IPEC-ECCE*, pp. 857-862, 18-21 May. 2014.
- [54] F. Blaabjerg and K. Ma, "Wind Energy Systems," in *Proc. IEEE*, vol. 105, no. 11, pp. 2116-2131, Nov. 2017.
- [55] M. Mahzarnia, M. P. Moghaddam, P. T. Baboli and P. Siano, "A review of the measures to enhance power systems resilience," *IEEE Syst. J.*, vol. 14, no. 3, pp. 4059-4070, Sept. 2020.

- [56] S. Ma, S. Li, Z. Wang and F. Qiu, "Resilience-oriented design of distribution systems," *IEEE Trans. Power Syst.*, vol. 34, no. 4, pp. 2880-2891, July 2019.
- [57] M. Vilathgamuwa, D. Nayanisiri and S. Gamini, *Power electronics for photovoltaic power systems*, Morgan & Claypool, 2015.
- [58] E. Serban, M. Ordonez and C. Pondiche, "DC-Bus Voltage Range Extension in 1500 V Photovoltaic Inverters," *IEEE J. Emerg. Sel. Top. Power Electron.*, vol. 3, no. 4, pp. 901-917, Dec. 2015.
- [59] X. Zhang, T. Zhao, W. Mao, D. Tan and L. Chang, "Multilevel inverters for grid-connected photovoltaic applications: examining emerging trends," *IEEE Power Electron. Mag.*, vol. 5, no. 4, pp. 32-41, Dec. 2018.
- [60] Q. Li and P. Wolfs, "A review of the single-phase photovoltaic module integrated converter topologies with three different DC link configurations," *IEEE Trans. Power Electron.*, vol. 23, no. 3, pp. 1320-1333, May 2008.
- [61] G. Kern and M. Russell, (2001 Jun.). Cost reduction and manufacture of the SunSine AC module. National Renewable Energy Laboratory [Online]. Available: <http://www.nrel.gov/docs/fy01osti/30534.pdf>.
- [62] Dorfmueller DMI series module inverter technical description. Dorfmueller Solaranlagen GMBH. [Online]. Available: http://www.dorfmueller-solaranlagen.de/images/wechselrichter_dmi_all_gemein.pdf.
- [63] C. Wang, "A novel single-stage full-bridge buck-boost inverter," *IEEE Trans. Power Electron.*, vol. 19, no. 1, pp. 150-159, Jan. 2004.
- [64] S. Heribert, S. Christoph, and K. Jurgen, "Inverter for transforming a DC voltage into an AC current or an AC voltage," Europe Patent 1 369 985 (A2), May. 2003.
- [65] C. Bao, X. Ruan, X. Wang, W. Li, D. Pan and K. Weng, "Step-by-step controller design for LCL-type grid-connected inverter with capacitor-current-feedback active-damping," *IEEE Trans. Power Electron.*, vol. 29, no. 3, pp. 1239-1253, Mar. 2014.
- [66] Y. Yang, H. Wang and F. Blaabjerg, "Reactive power injection strategies for single-phase photovoltaic systems considering grid requirements," *IEEE Trans. Ind. Appl.*, vol. 50, no. 6, pp. 4065-4076, Nov. 2014.
- [67] A. Sangwongwanich, Y. Yang and F. Blaabjerg, "A sensorless power reserve control strategy for two-stage grid-connected PV systems," *IEEE Trans. Power Electron.*, vol. 32, no. 11, pp. 8559-8569, Nov. 2017.
- [68] E. Rakhshani and P. Rodriguez, "Inertia emulation in AC/DC interconnected power systems using derivative technique considering frequency measurement effects," *IEEE Trans. Power Syst.*, vol. 32, no. 5, pp. 3338-3351, Sept. 2017.
- [69] M. Andresen, K. Ma, G. Buticchi, J. Falck, F. Blaabjerg and M. Liserre, "Junction temperature control for more reliable power electronics," *IEEE Trans. Power Electron.*, vol. 33, no. 1, pp. 765-776, Jan. 2018.
- [70] J. C. Y. Hui, A. Bakhshai and P. K. Jain, "An energy management scheme with power limit capability and an adaptive maximum power point tracking for small standalone PMSG wind energy systems," *IEEE Trans. Power Electron.*, vol. 31, no. 7, pp. 4861-4875, July 2016.
- [71] Y. Chou, C. Liu, Y. Wang, C. Wu and C. Lin, "Development of a black start decision supporting system for isolated power systems," *IEEE Trans. Power Syst.*, vol. 28, no. 3, pp. 2202-2210, Aug. 2013.
- [72] J. Fang, Y. Tang, H. Li and X. Li, "A battery/ultracapacitor hybrid energy storage system for implementing the power management of virtual synchronous generators," *IEEE Trans. Power Electron.*, vol. 33, no. 4, pp. 2820-2824, April 2018.
- [73] M. Lu, C. Chang, W. Lee and L. Wang, "Combining the wind power generation system with energy storage equipment," *IEEE Trans. Ind. Appl.*, vol. 45, no. 6, pp. 2109-2115, Nov.-Dec. 2009.
- [74] Z. Shu and P. Jirutitijaroen, "Optimal operation strategy of energy storage system for grid-connected wind power plants," *IEEE Trans. Sustain. Energy*, vol. 5, no. 1, pp. 190-199, Jan. 2014.
- [75] A. Sangwongwanich, Y. Yang and F. Blaabjerg, "High-performance constant power generation in grid-connected PV systems," *IEEE Trans. Power Electron.*, vol. 31, no. 3, pp. 1822-1825, March 2016.
- [76] J. C. Vasquez, R. A. Mastromauro, J. M. Guerrero, and M. Liserre, "Voltage support provided by a droop-controlled multifunctional inverter," *IEEE Trans. Ind. Electron.*, vol. 56, no. 11, pp. 4510-4519, Nov. 2009.
- [77] Decision adopting energy storage procurement framework and design program [Online], 2013. Available: <https://docs.cpuc.ca.gov/PublishedDocs/Published/G000/M078/K929/78929853.pdf>.
- [78] A.K. Pathak, M.P Sharma, M. Bunde, "A critical review of voltage and reactive power management of wind farms," *Renew. Sust. Energ. Rev.*, Vol. 51, pp. 460-471, Nov. 2015.
- [79] M. Ciappa, "Selected failure mechanisms of modern power modules," *Microelectron. Rel.*, vol. 42, no. 4, pp. 653-667, Jan. 2002.
- [80] U. M. Choi, F. Blaabjerg, "Separation of wear-out failure modes of IGBT modules in grid-connected inverter systems," *IEEE Trans. Power Electron.*, vol. 33, no. 7, pp. 2518-2530, Sep. 2018.
- [81] S. Gunturi and D. Schneider, "On the operation of a press pack IGBT module under short circuit conditions," *IEEE Trans. Adv. Packag.*, vol. 29, no. 3, pp. 433-440, Aug. 2006.
- [82] R. Simpson, A. Plumpton, M. Varley, C. Tonner, P. Taylor and X. Dai, "Press-pack IGBTs for HVDC and FACTS," *CSEE J. Power Energy Syst.*, vol. 3, no. 3, pp. 302-310, Sept. 2017.
- [83] Y. Chang, F. Iannuzzo, A. S. Bahman, W. Li, X. He, and F. Blaabjerg, "Compact sandwiched press-pack SiC power module with low stray inductance and balanced thermal stress," *IEEE Trans. Power Electron.*, vol. 35, no. 3, pp. 2237-2241, March 2020.
- [84] Y. Yang, H. Wang, F. Blaabjerg, and T. Kerekes, "A hybrid power control concept for PV inverters with reduced thermal loading," *IEEE Trans. Power Electron.*, vol. 29, no. 12, pp. 6271-6275, Dec. 2014.
- [85] Z. Ni, X. Lyu, O. P. Yadav, B. N. Singh, S. Zheng and D. Cao, "Overview of real-time lifetime prediction and extension for SiC power converters," *IEEE Trans. Power Electron.*, vol. 35, no. 8, pp. 7765-7794, Aug. 2020.
- [86] Y. Yang, H. Wang and F. Blaabjerg, "Reduced junction temperature control during low-voltage ride-through for single-phase photovoltaic inverters," *IET Power Electron.*, Vol. 7, No. 8, 2014-08, p. 2050-2059.
- [87] I. Batarseh and K. Alluhaybi, "Emerging opportunities in distributed power electronics and battery integration: setting the stage for an energy storage revolution," *IEEE Power Electron. Mag.*, vol. 7, no. 2, pp. 22-32, June 2020.
- [88] W. Su and A. Huang, *The energy internet-an open energy platform to transform legacy power systems into open innovation and global economic engines*, 1st ed, Woodhead Publishing, Nov. 2018.
- [89] S. Hussain, F. Nadeem, M. A. Aftab, I. Ali, and T. S. Ustun, "The emerging energy internet: architecture, benefits, challenges, and future prospects," *Electronics*, vol. 8, no. 9, p. 1037, 2019.
- [90] S. Zhao, F. Blaabjerg and H. Wang, "An Overview of Artificial Intelligence Applications for Power Electronics," *IEEE Trans. Power Electron.*, vol. 36, no. 4, pp. 4633-4658, April 2021.
- [91] Z. Yang, L. Tong, D. P. Tabor, E. S. Beh, M. Goulet, D. D. Porcellinis, A. A. Guzik, R. G. Gordon, and M. J. Aziz, "Alkaline benzoquinone aqueous ow battery for large-scale storage of electrical energy," *Adv. Energy Mater.*, vol. 8, no. 8, 1702056, 2018.
- [92] Y. Lin, J. H. Eto, B. B. Johnson, J. D. Flicker, R. H. Lasseter, H. N. Villegas Pico, G. S. Seo, B. J. Pierre, and A. Ellis, "Research roadmap on grid-forming inverters," *National Renewable Energy Laboratory: Golden, CO, USA, 2020, NREL/TP-5D00-73476*.



Zhongting Tang (S'18) was born in Sichuan, China, in 1990. She received her B.S. degree in Automation Control in 2012 and Ph.D. degree in Control Science and Engineering in 2020 from Central South University, Changsha, China. During 2018~2020, she studied as a guest Ph.D. student at the Department of Energy Technology in Aalborg University, Aalborg, Denmark. Now, she is currently working as a postdoc here.

Her research focus is on the grid integration of photovoltaics, topology and modulation technology of transformerless converter and its application and reliability in Photovoltaic system.



Yongheng Yang (SM'17) received the B.Eng. degree in electrical engineering and automation from Northwestern Polytechnical University, Shaanxi, China, in 2009 and the Ph.D. degree in electrical engineering from Aalborg University, Aalborg, Denmark, in 2014.

He was a postgraduate student at Southeast University, China, from 2009 to 2011. In 2013, he spent three months as a Visiting Scholar at Texas A&M University, USA. Dr. Yang is currently an Associate Professor with the Department of Energy Technology, Aalborg University. Dr. Yang was named on the list of world's Top 2% most-cited Scientists in 2020. His research focuses on the grid integration of renewable energy, particularly photovoltaic, power converter design, analysis and control, and reliability in power electronics.

Dr. Yang is the Chair of the IEEE Denmark Section. He serves as an Associate Editor of the CPSS Transactions on Power Electronics and Applications, the IET Electronics Letters, the IET Renewable Power Generation, the IEEE Journal of Emerging and Selected Topics in Power Electronics, and the IEEE Transactions on Industrial Electronics. He was the recipient of the 2018 IET Renewable Power Generation Premium Award, and the 2018 IEEE Transactions on Power Electronics' Outstanding Reviewers Award.



Frede Blaabjerg (S'86–M'88–SM'97–F'03) was with ABB-Scandia, Randers, Denmark, from 1987 to 1988. From 1988 to 1992, he got the PhD degree in Electrical Engineering at Aalborg University in 1995. He became an Assistant Professor in 1992, an Associate Professor in 1996, and a Full Professor of power electronics and drives in 1998.

From 2017 he became a Villum Investigator. He is *honoris causa* at University Politehnica Timisoara (UPT), Romania and Tallinn Technical University (TTU) in Estonia.

His current research interests include power electronics and its applications such as in wind turbines, PV systems, reliability, harmonics and adjustable speed drives. He has

published more than 600 journal papers in the fields of power electronics and its applications. He is the co-author of four monographs and editor of ten books in power electronics and its applications.

He has received 32 IEEE Prize Paper Awards, the IEEE PELS Distinguished Service Award in 2009, the EPE-PEMC Council Award in 2010, the IEEE William E. Newell Power Electronics Award 2014, the Villum Kann Rasmussen Research Award 2014, the Global Energy Prize in 2019 and the 2020 IEEE Edison Medal. He was the Editor-in-Chief of the IEEE TRANSACTIONS ON POWER ELECTRONICS from 2006 to 2012. He has been Distinguished Lecturer for the IEEE Power Electronics Society from 2005 to 2007 and for the IEEE Industry Applications Society from 2010 to 2011 as well as 2017 to 2018. In 2019-2020 he serves a President of IEEE Power Electronics Society. He is Vice-President of the Danish Academy of Technical Sciences too.

He is nominated in 2014-2020 by Thomson Reuters to be between the most 250 cited researchers in Engineering in the world.