- 1 Modulated-laser source induction system for remote detection of
- 2 infrared emissions of high explosives using Laser-Induced Thermal
- 3 Emission (LITE)

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## Abstract

- 19 In a homeland security setting, the ability to detect explosives at a distance is a top security
- 20 priority. Consequently, the development of remote, non-contact detection systems continues to
- 21 represent a path forward. In this vein, a remote detection system for excitation of infrared
- 22 emissions using a CO<sub>2</sub> laser for generating Laser-Induced Thermal Emission (LITE) is a possible

solution. However, a LITE system using a CO<sub>2</sub> laser has certain limitations, such as the requirement of careful alignment, interference by the CO<sub>2</sub> signal during detection, and the power density loss due to the increase of the laser image at the sample plane with the detection distance. In this study, a remote chopped-laser induction system for LITE detection using a CO<sub>2</sub> laser source coupled to a focusing telescope was built to solve some of these limitations. Samples of fixed surface concentration (500 µg/cm<sup>2</sup>) of 1,3,5-trinitroperhydro-1,3,5-triazine (RDX) were used for the remote detection experiments at the distance ranging between 4 and 8 m. This system was capable of thermally exciting and capturing the thermal emissions (TEs) at different times in a cyclic manner by a Fourier Transform Infrared (FTIR) spectrometer coupled to a goldcoated reflection optics telescope (FTIR-GT). This was done using a wheel blocking the capture of TE by the FTIR-GT chopper while heating the sample with the CO<sub>2</sub> laser. As the wheel moved, it blocked the CO<sub>2</sub> laser and allowed the spectroscopic system to capture the TEs of RDX. Different periods (or frequencies) of wheel spin and FTIR-GT integration times were evaluated to find dependence with observation distance of the maximum intensity detection, minimum S/N ratio, CO<sub>2</sub> laser spot size increase, and the induced temperature increment ( $\Delta T$ ).

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# Keywords

- 40 Standoff detection; laser-induced thermal emission; highly energetic materials; mid-infrared
- 41 emission spectroscopy; carbon dioxide laser

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## 1 Introduction

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Laser-Induced Thermal Emission (LITE)<sup>1-7</sup> detection of analytes is an important remote detection technique for monitoring hazardous chemicals safely. 8-25 In a homeland security setting, the detection of high explosives (HEs) enabled by LITE spectroscopy could play an important role in maintaining safe operations while conducting real-time detection and fast analysis. 26-30 However, the limits of the detection (LOD) depend on the source to target distance, on the laser power, on the divergence of the source, as well as on the collection efficiency and detector sensitivity.<sup>31</sup> Several studies have demonstrated that the use of a CO<sub>2</sub> laser as an excitation source for LITE spectroscopy at long distances is highly suitable for stimulating strong IR emissions of analytes of interest, such as trace amounts of HEs. 1,12,32-34 This feasibility of detection and identification of small quantities of HEs on surfaces is enabled by the fact that CO<sub>2</sub> lasers operate in the mid-infrared (MIR), i.e., in the fingerprint region. HEs have strong vibrational signatures in the MIR that can lead to generate resonant absorption by the analytes. MIR radiation is strongly absorbed by the analyte, leading to relatively high local temperatures. Thus, LITE spectroscopy is a technique that has many advantages: the sample itself is the source of the analytical information, 32,35 a strong resonant infrared photothermal approach, 31 and the facility for detecting other threat chemicals regardless of size, shape, and substrate type. In a previous study developed by our research group, low surface concentrations of samples of HEs were thermally excited to higher vibrational energy levels using a CO<sub>2</sub> laser, and the radiant relaxation process was monitored using a telescope-coupled FTIR interferometer. <sup>1,36</sup> The emission spectra of HE: TNT, DNT, PETN, TATP, and RDX were successfully monitored at distances from 4 to 64 m. During these experiments, several problems were identified. First, the telescope should have been configured with a shutter to avoid blinding the detector due to the back reflection of the laser beam. Second, the spectra were collected during the time interval in which the sample was cooling after the laser was turned off. Third, the laser irradiance decreased with the source-target distance because the laser spot (LS) size increased. The induced local temperatures ( $\Delta$ T) at each laser-target range (4, 8, 16, 32, and 64 m) were 72, 20, ~7, ~3, and > 1 °C. It was proposed that better results could be obtained by collimating the laser to increase the  $\Delta$ T and obtain higher emission levels. Fourth, careful alignment of the laser-target-detector angle was necessary when the telescope and the excitation source are not part of the same device. Therefore, the main objective of this study was to develop a new experimental set-up for remote LITE detection of HEs and proposing a methodology that allows solving these four problems that affect the experimental efficiency of LITE spectroscopy.

# 2 Methodology

80 2.1 Sample preparation

Only one HE was used in the experiments: 1,3,5-trinitroperhydro-1,3,5-triazine (RDX) which was synthesized in the laboratory. Acetone (99.5%, GC grade, Thermo-Fisher Scientific, Waltham, MA, USA) was used as the solvent. RDX samples were deposited on aluminum plates substrates (Al:  $2.54~\rm cm \times 2.54~cm$ ) at a nominal surface concentration of  $500~\mu g/cm^2$ . A sample-smearing technique was used to deposit the RDX samples. A stock solution of RDX was prepared in acetone. A Teflon® stub (3 cm wide and 0.04 cm thick) was used to smear a fixed volume (10  $\mu$ L) of the solutions containing the analytes onto the metal surface. The smearing was performed quickly, tilting the Teflon® sheet to the right or left in a single-pass operation. A

minimal adhesion of 500 μg/cm<sup>2</sup> to the Teflon was assumed. The plates were first cleaned with acetone followed by air-drying before the desired RDX surface loading was deposited.

## 2.2 Apparatus

The experimental setup used is illustrated in Fig. 1. It consisted of an intermittent excitation system of the thermal emissions (TE) induced by a CO<sub>2</sub> laser as the excitation source. This system was capable of thermally exciting and acquiring the TE at different times in a cyclic manner using a Fourier transform infrared (FTIR) spectrometer coupled to a gold-coated optics reflective telescope (GT). The chopping of the laser beam was accomplished using a wheel to block the laser and the capture of the TE by the FTIR-GT while heating the sample with the CO<sub>2</sub> laser. As the wheel moved, it blocked the CO<sub>2</sub> laser and allowed the acquisition of the TEs by the FTIR-GT. The sample temperature was measured with a thermocouple thermometer. On the back of the aluminum plate that was used as sample substrate, a cylindrical cavity was drilled close to the surface of the samples and the thermocouple head was fixed in place. This reduced the temperature difference between the sample and thermocouple by less than 0.5 °C.

## 2.2.1 Telescope

The catadioptric telescope used was an Argunov-Cassegrain design, equipped with gold-coated mirrors. The primary and secondary mirrors were 15 cm and 5 cm in diameter, respectively. The telescope was modified by allowing the secondary mirror to move and form an image at the focal plane from infinite distance to less than 4 m. This was possible by placing the secondary mirror in a movable optical mount (movement represented by a dotted arrow in Fig. 1) with a linear displacement resolution of 1 µm to allow the decreased focal point of the reflective system.<sup>1</sup>

#### 2.2.2 Spectrometer

The infrared spectrometer used was an open-path-FT-IR interferometer, model EM27 (Bruker Optics, Billerica, MA, USA). The optical bench consisted of a compact, enclosed, and desiccated Michelson-type interferometer equipped with ZnSe windows, an internal blackbody (BB) calibration source, a KBr beamsplitter, a very fast native focal ratio of f/0.9 with a field of view (FOV) of 30 mrad (1.7°). The FOV was reduced to 10 mrad (0.6°) by the receiver telescope, which had an infinite focal point magnification of 3×.

The optical chopper wheel (OCW) used consisted of an aluminum plate cut to a radius of 15.2

### 2.2.3 Optical chopper wheel (OCW)system

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cm which had a two-and-a-half arc-shaped opening (slightly larger than the spectrometer window) and an angle of 153.5° (Fig. 1(a)). The wheel contained a counterweight on the side of the opening with its center of mass at the center of the wheel so that when turning, it would not pivot. CO<sub>2</sub> laser: The target surface was heated using a CO<sub>2</sub> laser with 36 W as maximum output power (Firestar vi30, Synrad, Inc., Mukilteo, WA, USA), and an emission band from 926 to 980 cm<sup>-1</sup>. The laser beam was aligned with the center of the spectrometer window in an imaginary line called "the horizon." The center of the telescope mirror was aligned with the center ray of the laser beam. The laser radiation was reflected by two plane gold-coated mirrors to enter the telescope. Then, the laser beam was reflected towards the secondary mirror of the telescope and then to the primary mirror and then onto the sample (Fig. 1). This strategy of using the telescope to focus the laser light ensures that the LS on the sample was small and the laser power was high to ensure a strong heating effect. Thus, the telescope assumed two roles, focusing the laser and collecting the emission. Moreover, the alignment with respect to the sample was minimal and was only necessary to point at the sample plane. A 532 nm laser pointer was used to align the

path of the CO<sub>2</sub> laser to aim the sample. This part of the system contained a moving mirror that allowed pointing to the sample. This mirror is removed to start the LITE detection.

#### 2.2.4 Time-step

The OCW system divided the cycle into four-time steps (Fig. 1(b)). The first step was the acquisition time. In this time, the OCW rotated  $153.5^{\circ}$  allowing the telescope to capture the emissions and then passing through to the spectrometer and, at the same time, blocking the  $CO_2$  laser. The second step was a transition time. In this period, the OCW opened to a  $26.5^{\circ}$  arc and completely blocked the  $CO_2$  laser letting the spectrometer window partially. In the third time step, the OCW rotated by  $153.5^{\circ}$ , letting the laser light pass towards the telescope and blocking the window of the spectrometer so that it did not detect the laser light when it was heating the sample. Finally, in the fourth step consisted of a secondary transition time in which the OCW turned by  $26.5^{\circ}$ , remaining to block the  $CO_2$  laser while the spectrometer window was partially closed.

### 3 Results

## 3.1 Relative IR thermal emission of the OCW

In the first set of experiments, samples of RDX of  $500 \,\mu\text{g/cm}^2$  nominal surface loading were placed at a target distance 4 m from the cyclic induction system. The target samples were focused by the telescope using the laser pointer. Next, the OCW was adjusted to a wheel frequency ( $f_w$ ) of 0.1 Hz, and the spectra were acquired with an integration time ( $t_i$ ) of 2.0 s, continuously. Fig. 2 (a) shows the profiles of the emission spectra. Two types of spectra were acquired, emission spectra of the samples with the OCW switched off (Off), and sample

emission spectra of the samples with the OCW switched on (On). These are illustrated in Fig. 2 (a) by red and black traces, respectively. The ratios between these two types spectra were calculated and called relative emission spectra (On/Off ratios or e<sub>A</sub>) with respect to the aluminum OCW at room temperature used as background.

In Fig. 2(a), the e<sub>A</sub> spectrum of RDX (purple trace) reveals the characteristic spectral pattern for RDX as can be observed in relation to an emissivity spectrum of RDX used reference to a standard of RDX (green trace). Usually, the relative emission spectrum is obtained by dividing the emission of the sample by the emission of the blackbody at the same temperature as the sample. This situation generates an inverted signal spectrum since the blackbody emission is always higher than the sample emission, but in this case, e<sub>A</sub> spectra were obtained with respect to the emission of the aluminum OWC. However, the chopper wheel material does not behave as a blackbody, and its emission temperature is lower than the sample emission temperature. This has the effect that the vibrational features in the spectrum are shown upward looking (as if it were an absorption spectrum). This practical form of detection is convenient since, in the case of remote detection in the field, the temperature of the sample is unknown. For that reason, this work has been focused on making the detection considering the possibility of applications in real scenarios.

The MIR signals for RDX that stand out include the band at 1234 cm<sup>-1</sup> and the band at 1034 cm<sup>-1</sup> for N-C-N stretch, the signals at 1016 cm<sup>-1</sup>, and 943 cm<sup>-1</sup> for the combination N-NO<sub>2</sub> stretch and in-plane C–H bending, respectively. Other RDX signatures identified are 919 cm<sup>-1</sup> out-of-plane CH<sub>2</sub> bending, the ring breathing mode at 881 cm<sup>-1</sup>, the band at 850 cm<sup>-1</sup> for C-N-C stretch, and the band at 779 cm<sup>-1</sup> for N-C-N stretch.<sup>39,40</sup> The band at 1321 cm<sup>-1</sup> for N-NO<sub>2</sub> symmetric

stretch and the signal at 1593 cm<sup>-1</sup> for the N-NO<sub>2</sub> asymmetric stretch were not observed because water vapor signals overshadowed them (Fig 1(a)).

Fig. 2(b) shows the  $e_A$  spectra for 18 cycles of the OCW at  $f_W = 0.1$  Hz. The inserted figure shows the time step for this experiment, where the  $t_i$  was 2.0 s. The asterisks indicate the spectrum used to obtain  $e_A$ . The increase of the characteristic emission RDX signals was observed due to the increase in sample temperature.

## 3.2 Signal monitoring of the OCW adjusted by frequency and integration time

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Samples of 500 µg/cm<sup>2</sup> of RDX were placed at 4 m of distance from the cyclic thermal induction system and focused onto the FOV of the telescope using the laser pointer. A background spectrum of aluminum of OCW was initially acquired. Next, the fw of the OCW system was adjusted to 0.1, 0.2, 0.4, 1.0, and 2.0 Hz and acquiring spectra with a t<sub>i</sub> of 2.0 s, continuously. Then, the  $f_w$  was set at 1.0 Hz, and the  $t_i$  was varied between 0.5 to 2.2 s. In Fig. 3(a-d) the  $e_A$  for the RDX signal at 1234 cm<sup>-1</sup> at 100 s are shown, with a total of 50 spectra for different f<sub>w</sub> values. Three types of points are shown: blue diamond represent spectra in Off mode (when the wheel obstructs the spectrometer window); red diamond represent spectra in On mode (when the spectrometer window is clear), and green diamond are intermediate between On and Off positions. In Fig. 3(d) when the spectra acquisition of the OCW was adjusted to  $t_i = 2.0$  s and  $f_w$ 2.0 Hz, the cyclic speed increase was evidenced. Therefore, the OCW would enable the acquisition of four spectra in the On position and four spectra in the Off position. Consequently, each green diamond represents the average of the e<sub>A</sub> at 1234 cm<sup>-1</sup> for RDX of all spectral acquisitions in On and Off (On-Off) time. Fig 3 (a) shows only the e<sub>A</sub> for the peak at 1234 cm<sup>-1</sup> in On and Off due to cyclic speed decrease.

Fig. 4(a) shows the  $e_A$  spectra #50 for different  $f_w$  in contrast with the standard spectra of RDX (solid black line). In all  $e_A$  spectra, the characteristic signals of RDX were observed. However, the best spectra  $e_A$  were observed at  $f_w$  values of 0.2 and 0.4 Hz due to the decrease of the noise in the spectra. Although RDX signals in the  $e_A$  spectra for 0.1 Hz are very intense, they also contain a higher noise compared to other spectra.

The effect of the integration time  $(t_i)$ was also evaluated. In this case, the cyclic system was set at  $f_w$  1.0 Hz and  $t_i$  was varied between 0.5 to 2.2 s. Fig. 4(b) shows the spectra with higher intensity (max) and less intensity (min) and their spectral average (Av), varying the  $t_i$ : 0.54 s, 1.08 s, and 2.16 s. In general, for all Av spectra, the  $t_i$  values evaluated showed a variation in the spectral pattern that represents the RDX spectrum was observed. However, the increase in  $t_i$  allows that the OCW acquires enough sample information to get a good signal for both max and min spectra.

3.3 Dependence of  $CO_2$  laser spot and  $\Delta T$  with the distance

The dependence of the LS diameter of the  $CO_2$  laser and the induced temperature increment ( $\Delta T$ ) by the LITE process on RDX samples was investigated. The LS diameter of the  $CO_2$  laser was determined to increase by 0.5 cm/meter without a focusing telescope (Galán-Freyle et al. 1). In contrast, when the telescope was used to focus the LS the increase in diameter was only 0.1 cm/meter. LS diameter as a function of distance was measured using thermal paper (change in color with temperature). For the measurements, thermal paper was exposed to the laser action for 5 s, leaving a stain of the size of the LS diameter. The measurements were repeated for 5 times and an average was calculated. The uncertainty of the reported diameter values was  $\pm$  0.05 cm. This reduced increment in LS diameter was reflected in the  $\Delta T$  induced and the signal dependence with source-target distance. The results are shown as insets of Fig. 5(a). Focusing

the LS with the telescope for LITE detection at 4 m induced a  $\Delta T$  lower than LITE detection without a telescope. This result is attributed to the fact that in the present optical arrangement, the induced heat transfer is an intermittent process.

When the sensing distance increased to 8 m, the effect of the increase of the LS diameter per meter is more evident. The  $\Delta T$  for LITE detection without focusing the LS decreases approximately 50 °C in comparison with focusing the LS in which the decrease in  $\Delta T$  is maintained almost to 10 °C, as shown on the right side inset of Fig. 5 (a). A fit was obtained between the  $\Delta T$  induced at the sample and the reciprocal of the LS diameter (shown on left side inset of Fig. 5 (a)). The dependence obtained is as expected because when increasing the LS diameter, the power per unit area decreases, generating a lower  $\Delta T$ .

To evaluate the effect of the telescope as a focusing tool in remote detection using a LITE intermittent induction system, a comparison was made with the report by Galán-Freyle *et al.*, <sup>1</sup> using the RDX samples deposited on Al substrates at the same nominal surface concentration (500 μg/cm<sup>2</sup>). The signal to noise ratio (S/N) for the RDX samples was measured and compared between LITE systems with and without focusing the LS with the telescope. Fig. 5(b) shows the averages of e<sub>A</sub> for RDX spectra acquired with the cyclic induction LITE system at 4, 6, and 8 m of source-target distances. The inset in Fig. 5(b) shows that at 4 m of source-target distance, a higher S/N ratio was achieved by the non-focused LITE system. However, at 8 m of source-target distance, the S/N ratio was higher for the cyclic induction LITE system focusing the LS with the telescope system.

# 4 Conclusion

The proposed methodology showed an improved efficiency in the alignment of the LITE process at the sample plane. The dependence of LITE with source-target distance was improved, solving the excessive increase in the size spot of the  $CO_2$  laser in the LITE process. The sample emission rate was measured without the interference of the  $CO_2$  laser light. The optimum conditions for the cyclic induction LITE system were adjusted to 1 Hz for the frequency of the chopper wheel and an integration time of 2.0 s. In this study, only LITE detection distances from 4 to 8 m were evaluated. For future work, it is expected to investigate at a longer detection distances, with other sources of excitation such as tunable MIR lasers (quantum cascade lasers), synchronizing the detector with the chopper.

It is emphasized that it was not necessary to measure the temperature of a blackbody or to have to turn off the laser because it saturated the detector. This is a definite advantage of cyclic induction LITE systems making it more amenable real field applications.

#### **Disclosures**

The authors declare no conflicts of interest.

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## FIGURE CAPTIONS

- Fig. 1 Experimental setup of the standoff laser-induced thermal detection (LITE) of HEMs. (a)
- Optical chopper wheel (OCW) system; (b) Schematic representation of experiment timing for the
- acquisition time and LITE.

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- 435 Fig. 2 (a) Thermal emission for 500  $\mu$ g/cm<sup>2</sup> at 4 m of RDX with  $f_w = 0.1$  Hz, d = 4 m, and  $t_i = 2$
- 436 s; (b) e<sub>A</sub> spectra for 18 cycles at 1 Hz and 4 m.

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- 438 **Fig. 3** Signal monitoring at 1234 cm<sup>-1</sup> for (a)  $f_w = 0.1$  Hz,  $t_i = 2.0$  s, and d = 4 m; (b) for  $f_w = 0.2$
- 439 Hz,  $t_i = 2$  s, and d = 4 m; (c) for  $f_w = 0.4$  Hz,  $t_i = 2.0$  s, and d = 4 m; (d) for  $f_w = 2.0$  Hz,  $t_i = 2.0$  s,
- 440 and d = 4 m.

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- 442 Fig. 4 (a)  $e_A$  spectra for various  $f_w$  values for  $t_i = 2.0$  s and d = 4 m; (b) average  $e_A$  spectra for
- various  $t_i$  for a total acquisition time of 120 s,  $f_w = 1.0$  Hz and d = 4 m. The min and max spectra
- of the experiment are shown.

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- Fig. 5 (a) Dependence of the LS diameter for various source-target distances, induced with and
- without the telescope. Insets: dependence of the temperature increase ( $\Delta T$ ) for various source-
- target distances (left); reciprocal of LS diameter (right); (b) e<sub>A</sub> spectra for various source-target
- distances for 500 µg/cm<sup>2</sup>. Inset: dependence of S/N ratio divided by the nominal surface
- 450 concentration (C<sub>s</sub>) for various source-target distances.

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