

Four-quadrant Silicon and Silicon Carbide Photodiodes for Beam Position Monitor Applications: Electrical Characterization and Electron Irradiation Effects

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ABSTRACT: Silicon photodiodes are very useful devices as X-ray beam monitors in synchrotron radiation beamlines, as well as other astronomy and space applications. Owing to their lower susceptibility to variable temperature and illumination conditions, there is also special interest in silicon carbide devices for some of these applications. Moreover, radiation hardness of the involved technologies is a major concern for high-energy physics and space applications. This work presents four-quadrant photodiodes produced on ultrathin (10 μm) and bulk Si, as well as on SiC epilayer substrates. An extensive electrical characterization has been carried out by using current-voltage (I-V) and capacitance-voltage (C-V) techniques. The impact of different temperature (from -50 $^{\circ}\text{C}$ to 175 $^{\circ}\text{C}$) and visible light conditions on the electrical characteristics of the devices has been evaluated. Radiation effects caused by 2 MeV electron irradiation up to 1×10^{14} , 1×10^{15} and 1×10^{16} e/cm^2 fluences have been studied. Special attention has been devoted to the study of charge build-up in diode interquadrant isolation, as well as its impact on interquadrant resistance. The study of these electrical properties and its radiation-induced degradation should be taken into account for device applications.

KEYWORDS: Beam-line instrumentation (beam position and profile monitors; beam-intensity monitors; bunch length monitors); X-ray detectors; Si microstrip and pad detectors; Radiation damage to detector materials (solid state).

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46 1. Introduction

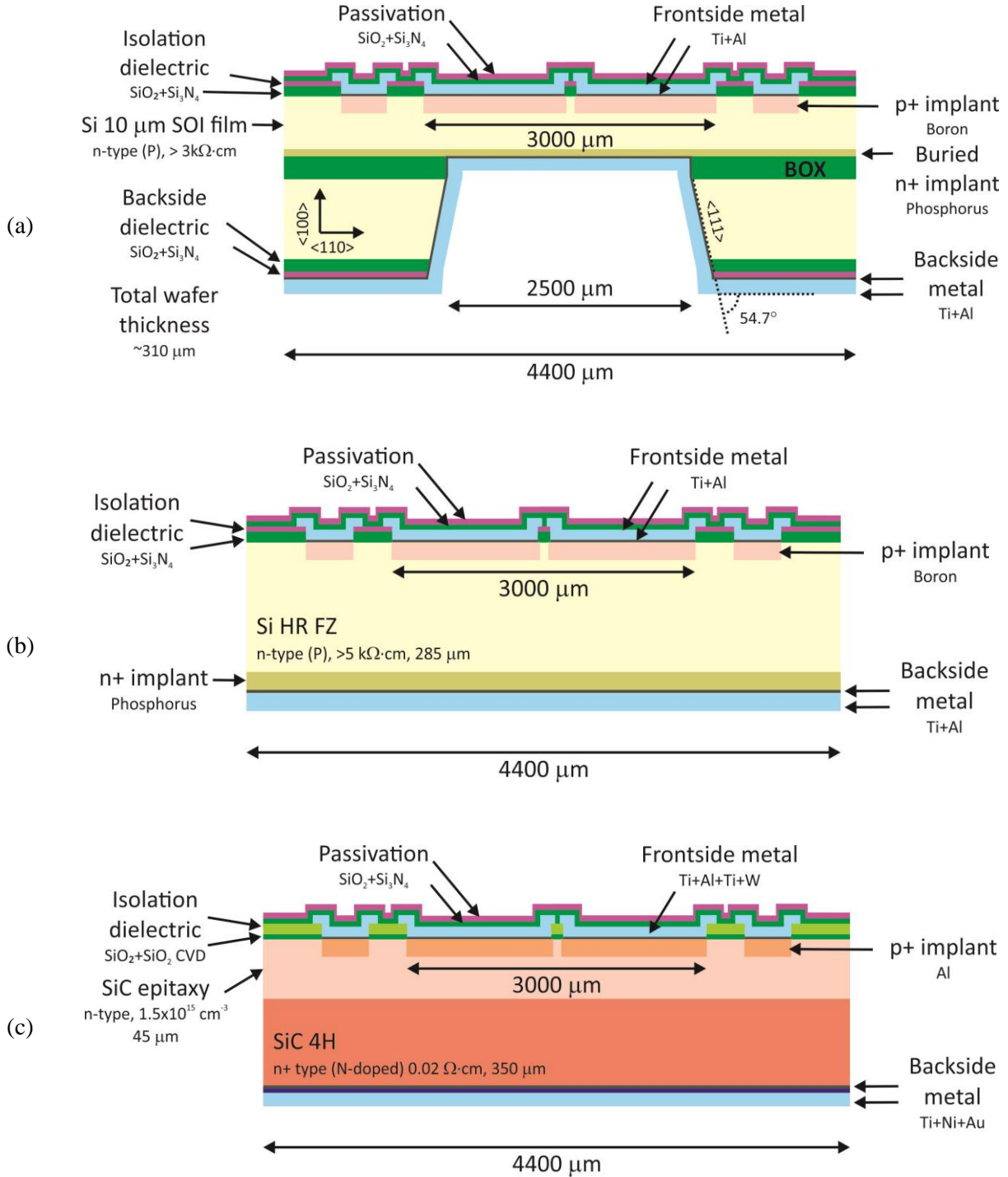
47 Silicon photodiodes are very useful devices as X-ray beam monitors in synchrotron radiation
48 beamlines. In order to be used in transmissive mode and given the absorption properties of
49 silicon, the devices must be thinner than 10 μm to achieve X-ray transmission higher than 90%
50 for photon energies above 10 keV [1-3]. On the other hand, bulk silicon segmented devices are
51 also of interest for astronomy and space applications, such as solar tracking systems [4]. Owing
52 to their lower susceptibility to variable temperature and illumination conditions, there is also
53 special interest in silicon carbide devices for some of these applications [5,6]. Superior radiation
54 resistance of SiC compared to Si was anticipated in some early works and this was attributed to
55 its higher atomic displacement threshold energy [7,8]. However, the existence of different
56 polytypes and difficulties in crystal growth have often made this difficult to assess [9,10]. Very
57 high radiation dose rates, in the range of 1 Mrad/s, are easily reached in synchrotron beams,
58 however, the X-rays maximum energy transfer to Si or SiC atoms is below the threshold energy
59 for radiation-induced dislocation of the crystalline lattice and therefore no bulk damage is
60 expected [11]. Nevertheless, the devices may still degrade owing to generation and trapping of
61 charge in dielectric layers used in their isolation and passivation, as well as surface currents
62 associated with radiation-induced interface traps [12]. The study of radiation effects on the
63 involved technologies is also of special interest for high-energy physics and space applications.

64 In this work, four-quadrant photodiodes produced on ultrathin (10 μm) and bulk Si, as well
65 as on SiC epilayer substrates are studied. The devices have been fabricated with different design
66 parameters along with auxiliary technology test structures (single diodes and MOS capacitors).
67 Electrical characterization has been carried out by using current-voltage (I-V) and capacitance-
68 voltage (C-V) techniques. The impact of different temperature, from -50 $^{\circ}\text{C}$ to 175 $^{\circ}\text{C}$, and
69 visible light conditions on the electrical characteristics of the devices has been evaluated.
70 Finally, the effects of 2 MeV electron irradiation, up to 1×10^{14} , 1×10^{15} and 1×10^{16} e/cm²
71 fluences, have been also studied.

72

73 **2. Four quadrant diodes fabrication**

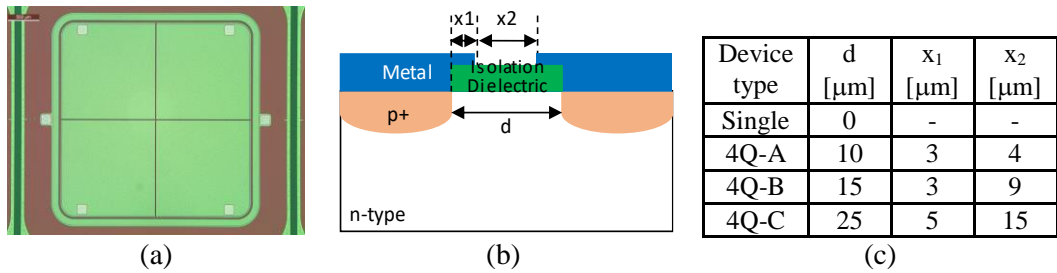
74 Device fabrication is based on IMB-CNM p-on-n diode processing experience on both high
 75 resistivity silicon [13] and silicon carbide substrates [6].
 76



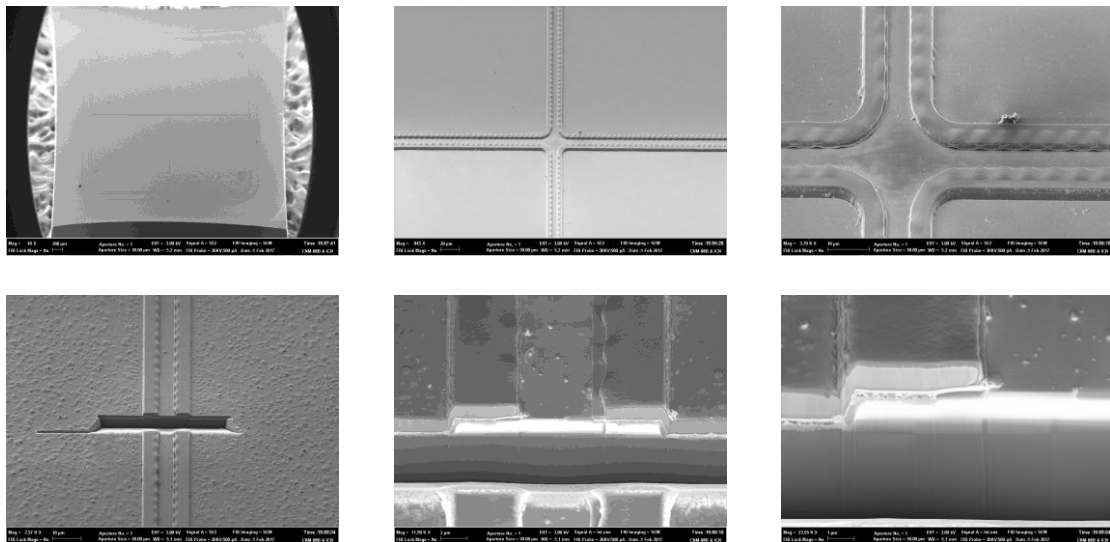
77 **Figure 1.** Schematic cross sections (not drawn to scale) of a four-quadrant diode with its guard
 78 ring fabricated on (a) ultrathin (10 μm) Si layer, (b) bulk Si and (c) epitaxied SiC substrates.

79 For the case of the ultra-thin silicon devices, a combination of direct wafer bonding, wafer
 80 thinning, p-on-n device processing and backside deep anisotropic etching processes has been
 81 used [2,3,14]. The mask design basically includes single diodes (not segmented in four
 82 quadrants) and four-quadrant diode variants implementing different space gap between
 83 quadrants as well as various geometries for the front side metal layer. A fixed size die (4400 μm
 84 \times 4400 μm) is used for all devices. Furthermore, metal-oxide-semiconductor (MOS) capacitors
 85 using as gate dielectric the interquadrant isolation oxide used for the four-quadrant diode
 86 structures are also available. Figure 1 shows schematic cross sections of the four-quadrant
 87 diodes fabricated on ultrathin (10 μm) silicon layer, bulk Si and epitaxied SiC substrates.

91 Figure 2 shows an optical microscopy picture of a fabricated four-quadrant diode, together
 92 with a sketch presenting the definition of the interquadrant distance (d), as well as the metal
 93 overlapped and non-overlapped isolation regions (x_1 and x_2 , respectively). For the case of both
 94 thin film and bulk Si devices, the interquadrant isolation dielectric represented in Fig. 2(b) is a
 95 dielectric stack composed by a thermally grown SiO_2 layer of 520 nm plus a deposited 180 nm
 96 Si_3N_4 layer, which was also used as a mask for the wafer backside thinning process in the case
 97 of the 10 μm -thick Si devices. For the case of the SiC devices, a dielectric stack composed of a
 98 30 nm thermally grown SiO_2 layer plus a 1000 nm deposited SiO_2 layer was used.
 99



100 **Figure 2.** (a) Optical microscopy picture of a fabricated four-quadrant diode, (b) sketch with the
 101 definition of the interquadrant distance “ d ”, as well as the metal overlapped and non-overlapped
 102 isolation regions (x_1 and x_2 , respectively), (c) device types used in the present work.
 103



104 **Figure 3.** SEM pictures of a SiC four-quadrant diode (4Q-A type) subjected to ion milling with
 105 focused ion beam (FIB) in a localized area across the diode interquadrant region.

106 Post-fabrication inspection of the devices on the different substrates was carried out by
107 means of Optical Microscopy, Scanning Electron Microscopy (SEM), Energy Dispersive X-ray
108 Spectroscopy (EDX) and Focused Ion Beam (FIB) techniques. Figure 3 shows SEM pictures of
109 a SiC four-quadrant diode subjected to FIB ion milling in a localized area across the diode
110 interquadrant region.

111 **3. Electrical characterization of non-irradiated devices**

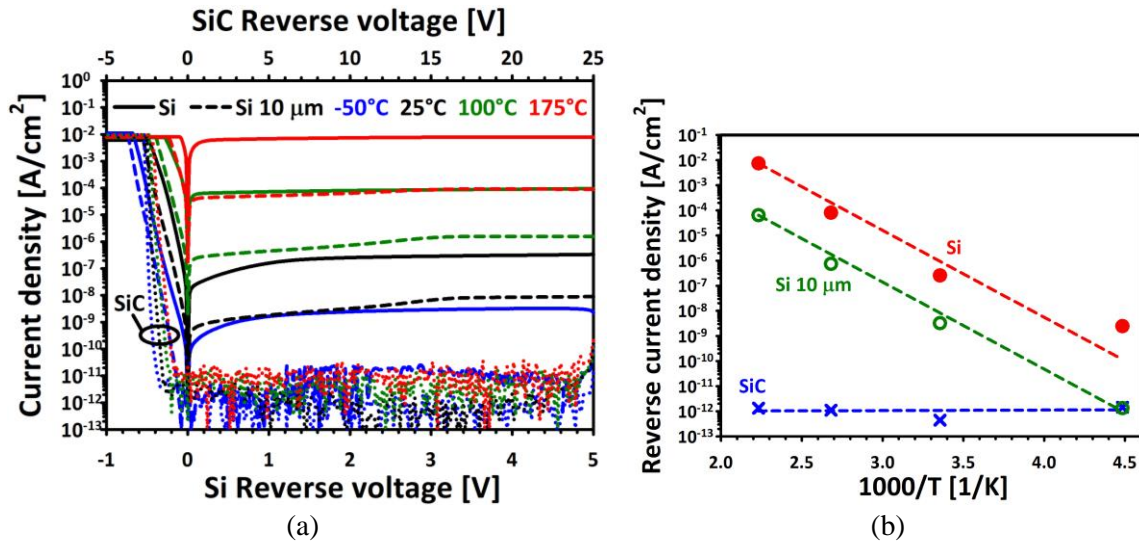
112 Current-voltage (I-V) and Capacitance-Voltage (C-V) measurements were carried out in a
113 Summit 11000B-M light-proof and electrically shielded probe station by using an HP 4155B
114 semiconductor parameter analyzer and an Agilent 4284A Precision LCR Meter.

115 **3.1 Temperature effects**

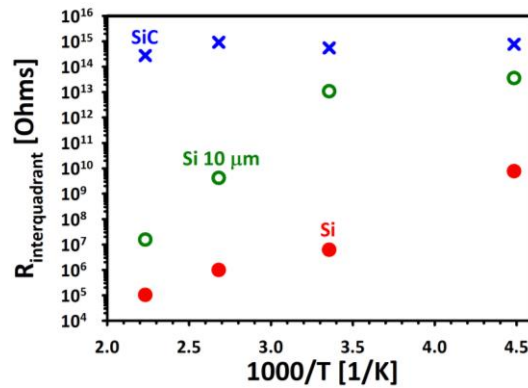
116 In order to evaluate the electrical characteristics of the devices fabricated on the different
117 substrates, diode I-V curves were measured at different temperatures by using an Espec ETC-
118 200L thermal system with the wafer prober thermal chuck. The I-V characteristics were
119 measured with three independent HP 4155B source monitor units (SMUs) connected to the
120 diode, ring and backside terminals. While zero potential was applied to the diode and ring
121 terminals, a voltage sweep was performed on the backside terminal.

122 Figure 4(a) shows the current density measured for bulk Si, 10 μm -thick Si and epilayer
123 SiC single diodes at four different temperatures (-50 $^{\circ}\text{C}$, 25 $^{\circ}\text{C}$, 100 $^{\circ}\text{C}$ and 175 $^{\circ}\text{C}$). From the
124 figure, a clear increase in both, reverse and forward bias current levels is observed on bulk Si
125 and 10 μm -thick Si diodes when increasing measurement temperature. Lower conduction levels
126 are observed for the 10- μm thick Si diodes compared to their thicker bulk Si counterparts. In
127 particular, the reverse leakage current at -50 $^{\circ}\text{C}$ for the thin Si diodes is found to be in the range
128 of the experimental set-up resolution ($\sim\text{pA}$). For what concerns the reverse bias breakdown
129 voltage, all devices have been tested up to 100 V, and only for the 10- μm thick Si diodes
130 breakdown has been observed at 40 V. Interestingly for potential applications, no significant
131 increase is observed for the reverse current in SiC diodes when increasing the measurement
132 temperature, this can be attributed to its wider bandgap energy (3.2 eV) compared to silicon (1.1
133 eV), reducing the thermal generation of carriers. Only some increase in forward bias current
134 levels is observed, what can be indeed regarded as a diode threshold voltage lowering. This is
135 due to junction built-in potential decrease as a result of semiconductor intrinsic carrier
136 concentration increase with temperature. Finally, the observed forward bias current density
137 saturation corresponds to a fixed 1×10^{-3} A SMU current compliance.

138 The reverse current dependence on temperature can be better appreciated in Fig. 4(b),
139 where the current density values corresponding to some fixed reverse bias conditions (2 V for
140 bulk Si and 10 μm -thick Si devices and 10 V for epitaxied SiC diodes) have been plotted against
141 measuring temperature. From Fig. 4(b), Arrhenius-law dependences can be drawn for Si
142 devices, with corresponding activation energies about 0.56 eV and 0.66 eV for the bulk Si and
143 10 μm -thick Si devices, respectively. These values about half of the silicon bandgap energy
144 point to generation current as the dominant contribution to the reverse current, especially for the
145 bulk Si devices. On the other hand, the slightly higher activation energy extracted for the 10
146 μm -thick Si devices may suggest some slight contribution of diffusion mechanism in these
147 thinner devices [15]. In contrast, under the studied measurement conditions, no appreciable
148 temperature dependence is observed for the SiC diodes reverse current.



150 **Figure 4.** (a) Diode current-voltage characteristics and (b) reverse current density as a function of temperature for bulk Si, 10 μm-thick Si and epitaxied SiC diodes measured at four different
 151 temperatures (-50 °C, 25 °C, 100 °C and 175 °C). Diode area is 0.09 cm².
 152
 153



154 **Figure 5.** R_{interquadrant} versus measuring temperature for different substrate four-quadrant diodes.
 155
 156

157 In order to investigate possible temperature effects on interquadrant resistance of the
 158 segmented diodes, electrical measurements on four-quadrant devices fabricated on the different
 159 semiconductor substrates were also carried out at different temperatures. Three independent HP
 160 4155B source monitor units (SMUs) were connected to the first quadrant, to the second, third
 161 and fourth quadrants shorted together and to the backside terminal. Current versus voltage
 162 curves were measured by applying a limited V₂ voltage sweep (from -1 V to +1 V and -5 V to
 163 +5 V for Si and SiC devices, respectively) to the three connected neighbour quadrants while
 164 measuring the I₁ current in the other quadrant that was kept at zero potential. These curves were
 165 measured for several diode backside reverse voltages. An estimation of interquadrant resistance
 166 was obtained from the slope of I₁ versus V₂ characteristics ($R_{interquadrant} = 1 / |(dI_1/dV_2)|$). The slopes
 167 were obtained by means of linear curve fits of the measured characteristics at the various diode
 168 backside reverse biases.

169 Figure 5 shows R_{interquadrant} as a function of measuring temperature for a set of bulk Si, 10
 170 μm-thick Si and epitaxied SiC four-quadrant devices (4Q-A type). The interquadrant resistance
 171 values correspond to high substrate reverse bias conditions (100 V for bulk Si and epitaxied SiC

172 diodes and 10 V for 10 μm -thick Si devices). From the figure, lower $R_{\text{interquadrant}}$ values are
173 clearly extracted for bulk silicon devices when increasing the measurement temperature.
174 Although higher values are obtained for the diodes fabricated on the 10 μm -thick silicon
175 membranes, $R_{\text{interquadrant}}$ temperature dependence is also observed for these thinner Si devices.
176 The highest $R_{\text{interquadrant}}$ values are clearly obtained for the SiC four-quadrant diodes, with no
177 appreciable temperature dependence for the studied conditions.
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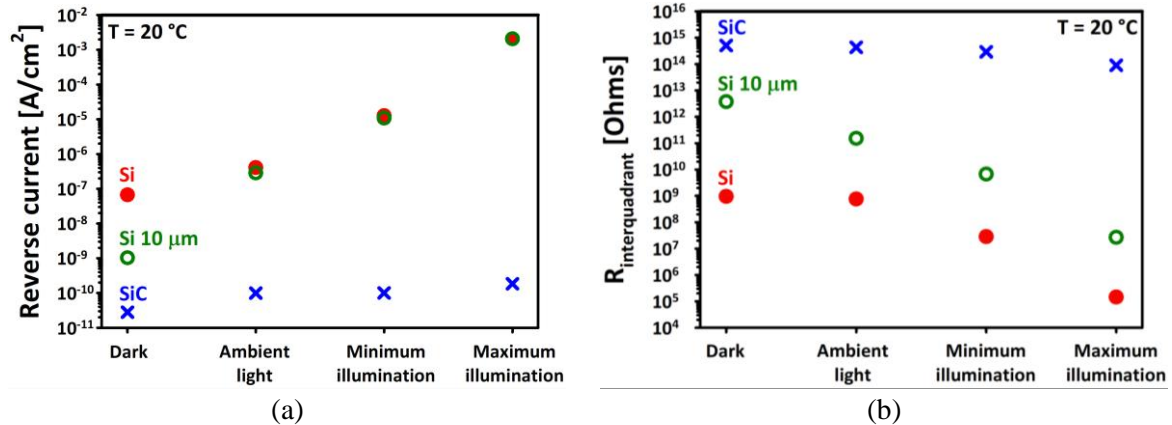
179 **3.2 Visible light effects**

180 Due to the larger SiC 4H bandgap energy (3.2 eV) compared to Si (1.1 eV), visible light, with
181 wavelengths in the range of 400 nm to 700 nm and corresponding photon energies between 3.1
182 eV and 1.65 eV, is not expected to generate electron-hole pairs in the SiC material. Owing to
183 this lower susceptibility to visible light, which may be present in real operation applications,
184 there is interest in SiC devices, which could simplify some of the experiments.

185 In order to get a rough idea about the impact of visible light conditions on the electrical
186 characteristics of the devices fabricated on the different substrates, the illumination system of
187 the wafer prober microscope was used. While performing the electrical measurements, four
188 different visible light conditions for the set-up were considered: “dark”, “ambient”, “minimum”
189 and “maximum” illumination. In the “dark” condition the device under test (DUT) was
190 measured in the light-proof wafer prober microchamber (using a metal piece to prevent any light
191 entering through the microscope glass window). In the “ambient” condition, the metal piece was
192 not used, so that room ambient light was allowed to illuminate the DUT. Under the “minimum”
193 and “maximum” illumination conditions, the LEDs of the microscope illumination system were
194 switched on, so that additional light than in the “ambient” condition reached the DUT. It has to
195 be commented here that no calibrated regulation was available for the LEDs illumination system
196 and this could have affected especially the “minimum” light condition (in some cases the LEDs
197 could have been a bit more or less active). On the other hand, the “maximum” illumination
198 condition is thought to be more precise, as it corresponded to the maximum illumination power
199 of the system.

200 Figure 6(a) shows reverse current for bulk Si, 10 μm -thick Si and epitaxied SiC diodes
201 exposed to the different visible light conditions. To better allow illumination, the data was taken
202 for single diodes with a 0.09 cm^2 area and without metal layer on most of the diode, only a
203 metal ring around it. From Figure 6(a) a clear increase in reverse current levels is observed for
204 the bulk Si and 10- μm thick Si devices when increasing the visible light illumination conditions.
205 In contrast, no significant visible light dependence is observed for the SiC diodes reverse
206 current under the studied illumination conditions.

207 In order to investigate possible visible light effects on the interquadrant resistance of the
208 segmented diodes, electrical measurements on four-quadrant devices fabricated on the different
209 semiconductor substrates were also carried out. Four-quadrant diodes (4Q-C type) without
210 metal layer on most of the diode quadrants were used for these measurements. Figure 6(b)
211 shows the obtained $R_{\text{interquadrant}}$ results as a function of illumination condition. From the figure,
212 lower $R_{\text{interquadrant}}$ values are clearly obtained for bulk silicon and 10- μm thick Si when increasing
213 the visible light illumination. The highest $R_{\text{interquadrant}}$ values are clearly obtained for the SiC
214 four-quadrant diodes, with no significant visible light dependence under the studied
215 illumination conditions.
216
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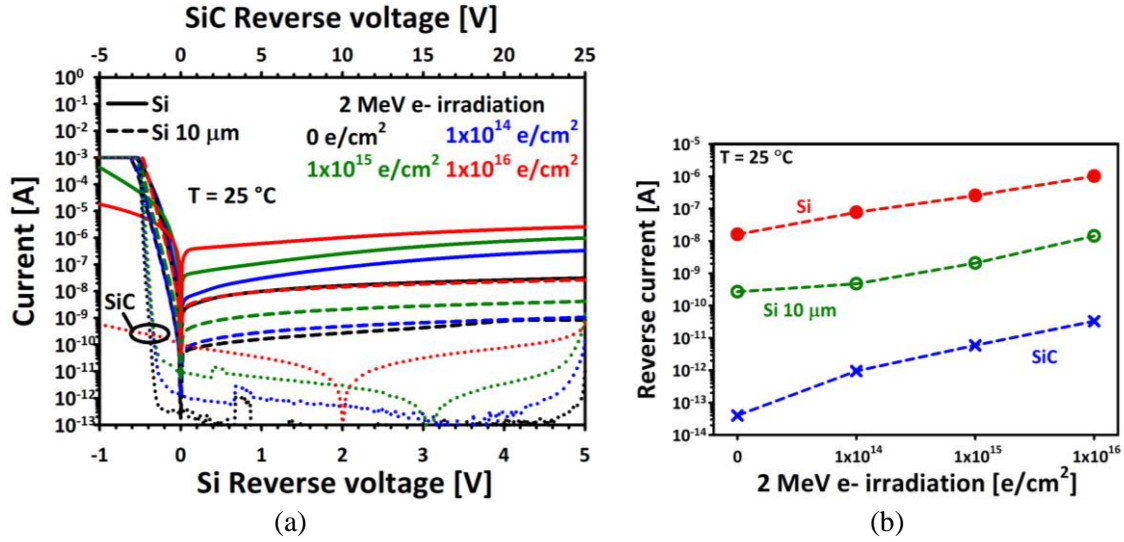
218 **Figure 6.** (a) Diode reverse current density and (b) Extracted $R_{\text{interquadrant}}$ for bulk Si, 10 μm -
 219 thick Si and epitaxied SiC diodes exposed to different visible light conditions.
 220

221 4. Electron irradiation effects

222 In order to investigate the radiation hardness of the devices fabricated on the different
 223 substrates, some samples were subjected to unbiased 2 MeV electron irradiations (the terminals
 224 of the devices were left floating) at room temperature. The irradiations were carried out using
 225 the electron accelerator at Takasaki-JAEA in Japan for three different independent fluences ($\phi =$
 226 $1 \times 10^{14} \text{ e/cm}^2$, $1 \times 10^{15} \text{ e/cm}^2$ and $1 \times 10^{16} \text{ e/cm}^2$, with corresponding total ionizing doses about 2.5
 227 Mrad(Si), 25 Mrad(Si) and 250 Mrad(Si)). After irradiation, the samples were exposed to room
 228 temperature during two weeks and no other intentional annealing was performed.

229 Figure 7(a) shows diode current-voltage characteristics measured for bulk Si, 10 μm -thick
 230 Si and epitaxied SiC diodes at different 2 MeV electron irradiation fluences. A progressive
 231 increase of leakage current in reverse bias operation is observed for increasing e-irradiation
 232 fluence. Moreover, some radiation-induced current lowering in forward operation seems to be
 233 observed for the more irradiated bulk silicon devices, which could probably be associated to the
 234 device series resistance increase. This increasing resistivity may result from changes in the free
 235 carrier concentration due to carrier removal by the radiation-induced point defects [16]. For the
 236 case of the epitaxied SiC diodes, relatively low reverse currents are obtained for $1 \times 10^{14} \text{ e/cm}^2$
 237 and $1 \times 10^{15} \text{ e/cm}^2$ fluences, however, no clear diode characteristics have been observed for
 238 $1 \times 10^{16} \text{ e/cm}^2$ irradiated devices. This radiation-induced phenomenon in SiC devices needs to be
 239 further studied. In particular, device performance as a detector remains to be checked and the
 240 results from recent proton and neutron irradiations could shed some further light on the
 241 performance of the irradiated SiC devices.

242 Figure 7(b) shows the electron irradiation dependence of leakage current at some fixed
 243 reverse bias conditions (2 V for bulk Si and 10 μm -thick Si devices and 5 V for epitaxied SiC
 244 diodes). From these results, a value of $4.5 \times 10^{-19} \text{ A/cm}$ has been extracted for the leakage current
 245 damage rate (α) (with $I_{\text{vol}} = \alpha \cdot \phi$ and $I_{\text{vol}} \equiv I / (\text{area} \times \text{depletion depth})$). Taking into account a
 246 nonionizing energy loss (NIEL) relative hardness factor of 2.49×10^{-2} for the 2 MeV electrons
 247 with respect to 1 MeV neutrons [17], the obtained α value is in the range of published results for
 248 irradiated silicon [18]. From the 10 μm -thick Si device results, factors around 1.8, 8 and 50 have
 249 been extracted for the radiation-induced diode current degradation, being these somewhat higher
 250 than the ones obtained for gamma irradiation at comparable total ionizing doses [3].



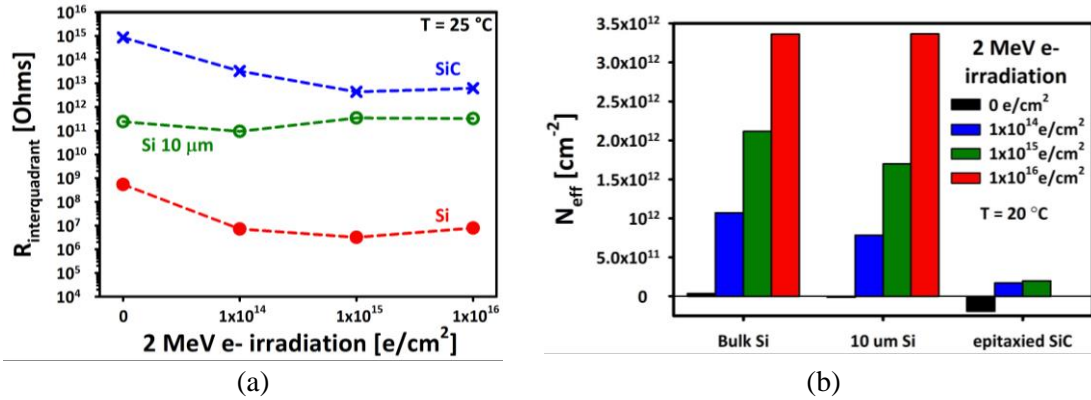
251 **Figure 7.** (a) Diode current-voltage characteristics and (b) reverse current measured for bulk Si,
 252 10 μm -thick Si and epitaxied SiC diodes (4Q-B type) at different 2 MeV electron irradiation
 253 fluences.
 254

255 Figure 8(a) shows interquadrant resistance results as a function of electron fluence.
 256 Whereas electron irradiation seems to reduce $R_{\text{interquadrant}}$ for bulk Si and epitaxied SiC devices,
 257 no clear trend is observed for the devices fabricated on the 10 μm silicon membranes. The
 258 previous studies with gamma irradiation on similar thin film devices [3], showed a slight
 259 increase of $R_{\text{interquadrant}}$ after gamma irradiation. $R_{\text{interquadrant}}$ increase was explained by the
 260 presence radiation-induced positive charges in the isolation dielectric, which would lead the n-
 261 type silicon surface to a deeper accumulation condition, thus improving interquadrant isolation.
 262 For the present case of 2 MeV electron irradiation, a possible explanation could be a trade-off
 263 between positive charge trapping in interquadrant isolation and semiconductor surface damage.
 264 In fact, the results from irradiated four-quadrant diodes with higher interquadrant distance (4Q-
 265 C instead of 4Q-B type devices from Figure 8) show a slight $R_{\text{interquadrant}}$ decrease with electron
 266 irradiation.
 267

268 In order to evaluate radiation-induced charge build-up in the diode interquadrant isolation
 269 dielectric, several MOS capacitors that use the same isolation oxide as gate dielectric were also
 270 irradiated. A clear stretch-out and radiation-induced shift of C-V curves towards negative gate
 271 voltages was observed for the irradiated MOS capacitors on the Si substrates. This is indicative
 272 of radiation-induced positive charge build-up. The extracted flat band voltage values (V_{fb}) have
 273 been compared with the one expected for an ideal MOS structure with 4.25 eV metal work
 274 function, corresponding to the aluminium gate electrode. From this, an estimation of the
 275 effective trapped charge density (N_{eff}), defined as a fixed charge located at the silicon/dielectric
 276 interface, has been obtained. Figure 8(b) shows the extracted N_{eff} values from irradiated MOS
 277 capacitors. From the figure, low N_{eff} values, in the range of $+3.5 \times 10^{10} \text{ cm}^{-2}$ and $-1.4 \times 10^{10} \text{ cm}^{-2}$,
 278 have been obtained for non-irradiated Bulk Si and 10 μm -thick Si devices, respectively
 279 (assuming theoretical V_{fb} values of -0.16 V and -0.32 V for MOS capacitor on their
 280 corresponding n-type silicon substrates). However, positive N_{eff} values roughly in the range of
 281 $1 \times 10^{12} \text{ cm}^{-2}$, $2 \times 10^{12} \text{ cm}^{-2}$ and $3.5 \times 10^{12} \text{ cm}^{-2}$ are obtained for the devices irradiated to 1×10^{14}
 282 e/cm^2 , $1 \times 10^{15} \text{ e/cm}^2$ and $1 \times 10^{16} \text{ e/cm}^2$, respectively. These values are in reasonable agreement

283 with previous results obtained on gamma irradiated 10 μm -thick Si devices [3], when taking
 284 into account the equivalent total ionizing dose for the 2 MeV electron irradiations.

286 For the case of the MOS capacitors on the epitaxied SiC substrate, smaller radiation-
 287 induced shift of C-V curves was observed after 1×10^{14} e/cm^2 and 1×10^{15} e/cm^2 irradiation. In
 288 principle, this could point to an improved radiation hardness for their Si_3N_4 -free interquadrant
 289 isolation stack. However, similarly to diode I-V measurements, no functional MOS C-V
 290 characteristics could be measured for 1×10^{16} e/cm^2 irradiated devices. Further studies would be
 291 needed for this radiation-induced phenomenon in SiC devices.
 292



293 **Figure 8.** (a) Extracted $R_{\text{interquadrant}}$ as a function of 2 MeV electron irradiation fluence for
 294 bulk Si, 10 μm -thick Si and epitaxied SiC four-quadrant diodes (4Q-B type). (b) effective
 295 trapped charge densities (N_{eff}) in the isolation dielectric extracted from C-V curves measured at
 296 1 kHz on electron irradiated MOS capacitors with area 8.17×10^{-3} cm^2 .
 297

298 5. Summary

299 Segmented four-quadrants diodes, intended for X-ray beam alignment, as well as other potential
 300 space or astronomy applications, have been fabricated on ultrathin (10 μm) and bulk Si, as well
 301 as on epitaxied SiC substrates. The improved performance shown by silicon carbide devices at
 302 variable temperatures and visible light illumination conditions could simplify some applications
 303 in which silicon devices are currently used. However, the radiation-induced behaviour at high
 304 irradiation fluences, as well as further SiC technology developments to process on high resistive
 305 (semi-insulating) bulk SiC substrates, need to be further studied.

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