

Design and Analysis of 300MW Solar Configuration and its Comparison with Quaid-e-Azam Solar Park

Iqra Akram^{1,2}, Muhammad Awais^{2,3}, Adnan Bashir², Rana Abdul Jabbar Khan⁴, Jamshed Iqbal^{1,5}

¹Department of Electrical Engineering, FAST National University, Islamabad, Pakistan

²Department of Electrical Engineering, University of Engineering & Technology, Lahore, Pakistan

³Department of Electrical Engineering, Information Technology University, Lahore, Pakistan

⁴National Transmissions and Dispatch Company, Lahore Pakistan

⁵Electrical and Computer Engineering Department, University of Jeddah, Saudi Arabia

Abstract — Pakistan’s recent energy crisis demands efficient utilization of renewable energy resources. The country, being richest with respect to solar potential, is experiencing a remarkable progress in power generation from Photovoltaic sources. Quaid-e-Azam Solar Park (QASP) is an example to improve the efficiency in term of Performance Ratio (PR) and energy injected into grid. In an attempt to further elevate the efficiency, the present work proposes configuration consisting of modules and inverters with low temperature coefficient. Based on meteorological data obtained from Meteonorm/NASA, performance of the proposed configuration is simulated in PVsyst and is then compared with that of QASP. Comparative results indicate that the proposed configuration annually improves PR by a factor of 3-4% while increasing the energy injected into the grid by 4.5 MW. It is anticipated that physical realization of the proposed configuration will improve energy yield.

Keywords—PV system, Solar configuration, Energy efficiency, Performance Ratio, QASP

I. INTRODUCTION

Pakistan is facing severe energy crisis at present. Tremendous efforts are being made to offer continuous and reliable solutions by exploring renewable energy resources to overcome the crisis [1]. Solar energy is an ideal source of renewable energy having highest potential in the world [2], which offers environmental friendly [3] drastic change in the energy by reducing carbon gas emission [4]. There are two ways of harnessing solar energy to generate electricity: Photovoltaic (PV) and Concentrated Solar Power (CSP).

The later offers higher efficiency compared with the former one. However, in terms of deployment duration and costs related with installation, O & M and levelization, PV outperforms than CSP [5]. Given the financial constraints and an urge for a quick renewable solution in Pakistan, PV has been primarily the main source of generating electric power in the country. Grid connected PV systems employ direct conversion of sunlight into electricity which is then fed into the grid without involving storage batteries.

The two key factors pertinent to energy efficiency are Performance Ratio (PR) and the amount of energy injected into the grid [6]. PR depends upon several factors including ambient temperature, efficiency of the module, efficiency of the inverter, losses due to environmental effects etc. The main factor that affects PR is the ambient temperature. For regions with high temperatures (e.g. in Southern Punjab), PV panels with relatively lower temperature coefficients are preferred to minimize deficiency in efficiency due to rise in temperature.

The present work proposes a 300MW solar configuration designed in PVSyst software and analyzes its PR and injected energy. The proposed configuration is then compared with 300MW equivalent configuration of Quaid-e-Azam Solar Park (QASP) w.r.t. both key factors. Practically, QASP has a capacity of 100MW, however, for the sake of fair comparison; the equivalent configuration of

QASP is designed using same inverters and modules as being actually used. Table 1 lists the two configurations of QASP with temperature coefficient of 0.41. In contrast with JA Solar and Trina modules, the proposed configuration uses Sunpower modules to reduce the coefficient so as to improve PR.

Overall system block diagram is conceptualized in Fig 1. Parameters collected from data sources (NASA/Meteonorm) include temperature, pressure and irradiance. The collected data is used by PVsyst to analyze and compare QASP and proposed configuration w.r.t. PR, energy injected to grid and losses of the system.

TABLE 1
CONFIGURATIONS FOR PV SYSTEM DESIGN AND ANALYSIS

Configuration (System)	Inverter	Module		
		Name	Temp. Coeff.	Efficiency (%age)
Conf. 1 (QASP)	Sungrow	JA Solar	0.41	15.28
Conf. 2 (QASP)	TBEA	Trina	0.41	14.84
Conf. 3 (Proposed)	Sungrow	Sunpower	0.38	20.1

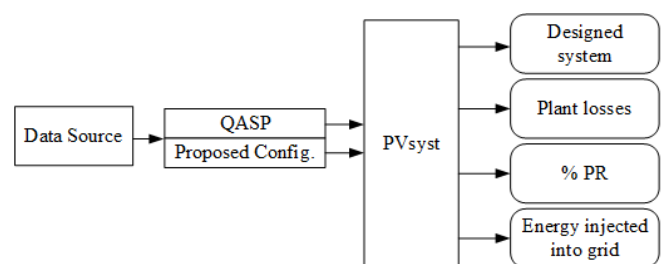


Fig. 1. Functional block diagram.

The remaining paper is organized as follows; Section II reports state-of-the-art on PV systems from grid perspectives. Section III presents design and simulation results of the proposed configuration while Section IV discusses its comparative analysis with reference to QASP. Finally Section V comments on conclusion.

II. LITERATURE REVIEW

An in-depth review of literature reported during the last decade revealed the potential of standalone solar PV systems as well as grid-connected systems. This is primarily driven by ‘green’ nature of solar energy that is catching wider interest of scientific community at domestic and commercial levels.

Hasimah *et al.* have simulated various modular technologies for Malaysian sites to meet the energy demand [7]. Based on the results obtained from ‘RETScreen Clean

Energy Management' software and PVsyst, they concluded that mono-crystalline and poly-crystalline give higher returns of energy. Karki *et al.* compared two PV systems; one installed in Berlin while other located in Kathmandu [8]. They observed that the later system comparatively generates 70% more energy due to higher solar irradiations on the solar module. Another study by Raj *et al.* considered 100 kW_p system and investigated that the simulation results obtained using PVsyst are reasonably close to the actual data measured from sunny web box [9].

Putra *et al.* simulated three different demands (1kW, 5kW, 10kW) for three Indian sites [10]. Using three types of modules, they estimated the available energy and cost of the generated energy. They highlighted technical feasibility of hybrid PV systems from physical perspectives.

Truong *et al.* designed a system with a demand of 15kW_p [11]. With a peak power generation range of 9-5.5kW_p, the presented system produces annual energy of 19348 kWh. Another study [12] conducted by Yadav *et al.* simulated 1kW_p PV system using PVsyst for Hamipur (India) site. The system produces energy of 1356kWh per year with a PR of 72.4%.

Another simulation study conducted on a 19.8kW_p British site by Pillai *et al.* deduced that PV system is not economically feasible as a backup [13]. Srivastava and Giri also simulated PV system for a site in Gorakhpur (India) for a demand of 150kW_p. The energy injected into grid is 901.22kWh per year with a PR of 83.1% [14]. Irwan *et al.* simulated a PV system for a 150kW_p site located in Kangar (Malaysia) and showed results for standalone PV system [15].

Quesada *et al.* carried out simulation for a 7.2 KW_p PV system based on data from different sources and concluded that different data sources produced different results [16]. Tallab and Malek simulated 1MW_p system for Algerian site and concluded that tilt angle should be changed in summer and winter to enhance efficiency [17]. Compared with fixed modules, this change increases the energy by 5%. Morshed *et al.* simulated PV system for a demand of 2kW_p using three tools; PVsyst, Homer and SolarMAT. They concluded that PVsyst is a better tool for designing a PV system compared to other two softwares [18].

Table 2 summarizes up-to-date literature review of demands and energy injected into grid for various locations.

TABLE 2
DEMANDS AND ENERGY INJECTED INTO GRID FOR VARIOUS LOCATIONS

No.	Location(s)	Country	Latitude (N)	Longitude (E)	Module name	Demand (W _p)	Energy injected into grid (KWh/yr)
1	Senai	Malaysia	1.4°	103.4°	1) Shell Ultra 85-P 2) BP Solar-380X 3) BP Solar-Millenia MST	500-600M	1) 136.4 2) 69.2 3) 65.5 [7]
2	1) Berlin 2) Kathmandu	1) Germany 2) Nepal	1) 52.3° 2) 27.5°	1) 13.2° 2) 58°	250W _p sayoHIT-H250E01	60k	1) 53813 2)91154 [8]
3	1)Aceh Singkil 2) Alor 3) Raja Amapt	Indonesia	1) 2°21.5° 2) 8°17.6° (3) 0°23°	1) 97°52.3° 2) 124°33.2° 3) 130°52.5°	1) Honda highlander 2) Honda EG6500CXS 3) Honda Highlander SF7000-DXE	1k-5k-10k	1) 4.644-7.591-14.230 2) 4.777-10.469-18.71 3) 4.916-7.519-15.057 [10]
4	Jaipur	India	26.9124°	75.7873°	STP25000TL-30	1k	437.92 (Forecasted) 421.242 (Recorded) [9]
5	Hanoi	Vietnam	21°	-	XL-SW-335	15k	19348 [11]
6	Hamipor	India	31°2'	76°5'	STP 150-24B	1k	1356.0 [12]
7	Gorakhpur	India	26.7°	83.4°	SU-250	500k	901220 [14]
8	Kangar	Malaysia	6.43°	100.19°	Unisolar	252	735.84 [15]
9	M'sila	Algeria	34.8°	4.2°	YL250P-32b	1M	1805000 [17]

III. SIMULATION OF PROPOSED CONFIGURATION

In case of grid-connected system, the grid provides battery backup [19]. The proposed system consists of three main stages; PV array, Inverter and Output interface. PV array is a source of DC power. To handle variations in the power generated by PV system, a combiner box is used to permit injection of fixed voltage into the next stage. In inverter, DC voltage is converted into AC for consumption in grid. A central inverter resides in the proposed configuration. The third stage provides output interface and handles injection of the generated energy into grid as shown in Fig. 2.

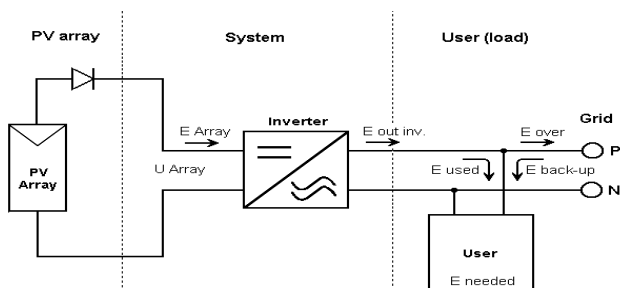


Fig. 2. Schematic diagram of the system.

In case of heavy or commercial loads, the energy can also be directly obtained from PV system instead of grid. A standard configuration also includes a protection phase; however, due to its insignificant impact on the output, we have not shown this phase in the schematics.

The process of designing a PV system for the proposed configuration starts with the selection of geographical site. Entering longitude, latitude and azimuthal information in PVsyst automatically permits data acquisition from NASA/Meteonorm. This is followed by selection of inverter and module in PVsyst for the configuration 3 listed in Table 1 and Fig. 3. We have used poly-crystalline technology in PV modules due to its better yield as reported in [7]. PVsyst automatically collects all the specifications and ratings of the selected components from the specified libraries.

PVSYS V6.39		29/01/16 Page 1/5	
Grid-Connected System: Simulation parameters			
Project :	Grid-Connected Project at Dahrnwala		
Geographical Site	Dahrnwala	Country	Pakistan
Situation	Latitude 29.6°N	Longitude	72.9°E
Time defined as	Legal Time Time zone UT+5	Altitude	152 m
Meteo data:	Albedo 0.20	Dahrnwala Synthetic - Meteonorm 7.1 (1981-1990), Sat=97%	

Fig. 3. Geographical information of site.

The next step in simulation is to specify power requirement or area. Based on user's input, the software

computes number of modules, inverters and their arrangement and determines best operating points. It also suggests tilt angle of the modules, area required and other related factors as illustrated in Fig. 4.

Collector Plane Orientation		Tilt	30°	Azimuth	0°
Models used		Transposition	Perez	Diffuse	Erbs, Meteorom
Horizon		Average Height	5.8°		
Near Shadings		No Shadings			
PV Array Characteristics					
PV module		Si-mono	Model	SPR-X20-250-BLK	
Original PV/syst database		Manufacturer	SunPower		
Number of PV modules		In series	16 modules	In parallel	75000 strings
Total number of PV modules		Nb. modules	1200000	Unit Nom. Power	250 Wp
Array global power		Nominal (STC)	300000 kWp	At operating cond.	277480 kWp (50°C)
Array operating characteristics (50°C)		U mpp	629 V	I mpp	441248 A
Total area		Module area	1492898 m²	Cell area	1324512 m²
Inverter					
Characteristics		Model	SG500MX	Manufacturer	Sungrow
Inverter pack		Operating Voltage	500-820 V	Unit Nom. Power	500 kWac
		Nb. of inverters	501 units	Total Power	250500 kWac
PV Array loss factors					
Array Soiling Losses		Uc (const)	20.0 W/m²K	Loss Fraction	1.0 %
Thermal Loss factor		Uv (wind)	0.0 W/m²K / m/s	Loss Fraction	0.0 %
Wiring Ohmic Loss		Global array res.	0.023 mOhm	Loss Fraction	1.5 % at STC
Module Quality Loss				Loss Fraction	-1.3 %
Module Mismatch Losses				Loss Fraction	1.0 % at MPP
Incidence effect, user defined profile					
		0°	50°	60°	65°
		70°	75°	80°	85°
		90°			
		1.00	1.00	0.99	0.97
				0.94	0.89
				0.77	0.62
				0.50	0.00
System loss factors					
Unavailability of the system		Wires: 3x30000.0 mm²	10 m	Loss Fraction	1.9 % at STC
		5.5 days, 3 periods		Time fraction	1.5 %

Fig. 4. Parameters values for proposed configuration.

Main parameters of the system (Fig. 4 and Fig. 5) include; nominal AC and DC power, total number of modules, number of inverters, arrangement of modules in series and parallel combinations, annual energy, PR etc.

Main system parameters		System type	Grid-Connected
Horizon		Average Height	5.8°
PV Field Orientation		tilt	30°
PV modules		Model	SPR-X20-250-BLK
PV Array		Nb. of modules	1200000
Inverter		Model	SG500MX
Inverter pack		Nb. of units	501.0
User's needs		Unlimited load (grid)	
Main simulation results		Produced Energy	502979 MWh/year
System Production		Performance Ratio PR	80.2 %
		Specific prod.	1677 kWh/kWp/year

Fig. 5. System energy and PR for proposed configuration.

Detailed monthly results include power produced per month, system losses, PR and energy injected into the grid as shown in Fig. 6 and Fig. 7. Irradiation (global horizontal and global diffused), ambient temperature and system efficiency etc. on monthly basis are tabulated in Table 3. Fig. 8 presents the power lost due to auxiliary losses.

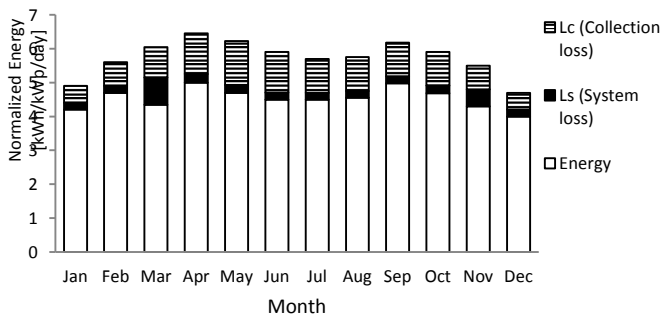


Fig. 6. Normal power per month for proposed configuration.

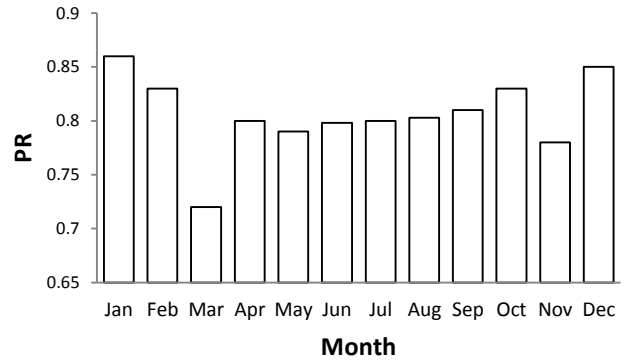


Fig. 7. PR for proposed configuration.

TABLE 3
ANNUAL ENERGY AND ARRAY EFFICIENCY OF PROPOSED CONFIGURATION

	G_H kWh/ m²	Ta °C	G_I kWh/ m²	G_Ef kWh/ m²	Eary MWh	E_G MWh	Ef_A %	Ef_S %
January	105.4	14.55	149.8	144.0	40054	38629	17.91	17.27
February	120.7	18.94	156.8	150.2	41067	39576	17.54	16.90
March	163.2	25.09	187.4	179.0	47705	40539	17.05	14.49
April	184.0	30.41	188.6	179.5	47030	45350	16.71	16.11
May	201.8	35.13	190.0	180.1	46559	44937	16.42	15.85
June	192.2	34.35	173.9	164.3	42843	41378	16.50	15.94
July	189.1	33.33	174.3	164.5	43189	41719	16.60	16.04
August	180.9	32.14	178.4	169.1	44410	42857	16.67	16.09
September	171.2	30.80	188.5	179.8	47219	45513	16.78	16.18
October	146.9	28.24	182.8	175.2	46264	44591	16.95	16.34
November	119.0	21.78	171.8	165.2	44616	40011	17.40	15.60
December	99.9	16.73	148.7	142.1	39264	37880	17.69	17.07
Yearly	1874	26.83	2091	1993	530219	502979	16.99	16.11

G_H Horizontal global irradiance
Eary Effective energy at the output of the array
Ta Ambient Temperature
E_G Energy injected into grid
G_I Global incident coll.plane
Ef_A Effic.Eout array/rough area
G_Ef Effective Global corr,for IAM and shading
Ef_S Effic.Eout system/rough area

Grid-Connected System: Simulation parameters (continued)	
User's needs :	Unlimited load (grid)
Auxiliaries loss	Constant (fans) 10 W ... from Poper thresh. 0.8 kW Proportional to Poper 10.0 W/kW... from Poper thresh. 3.0 kW

Fig. 8. 300MW system auxiliary losses.

IV. COMPARISON BETWEEN THREE CONFIGURATIONS

Results obtained corresponding to the three configurations mentioned in Table 1 are then compared. Comparison parameters include PR, energy injected into grid and losses.

Comparing efficiency/area given in Table 3 for various configurations, it is found that in case of QASP, configurations 1 and 2, this value is 11.83% and 11.37% respectively. The proposed configuration over-performs since it offers an efficiency of 16.11%. Also, the amount of energy injected into the grid is higher in case of the proposed configuration as compared to QASP configurations as listed in Tables 3-5.

TABLE 4
ANNUAL ENERGY AND ARRAY EFFICIENCY FOR QASP CONFIGURATION 1

	G_H kWh/ m²	Ta °C	G_I kWh/ m²	G_Ef kWh/ m²	Eary MWh	E_G MWh	EA_G MVAh	Ef_S %
January	156.0	14.15	222.7	213.8	58574	56074	59025	12.43
February	120.7	18.94	156.8	150.2	39828	38144	40152	12.01
March	163.2	25.09	187.4	179.0	45665	43797	46102	11.54

April	184.0	30.41	188.6	179.5	44667	38799	40841	10.16
May	201.8	35.13	190.0	180.1	44061	42344	44572	11.01
June	192.2	34.35	173.9	164.3	40864	39268	41335	11.15
July	189.1	33.33	174.3	164.5	41375	39755	41847	11.26
August	180.9	32.14	178.4	169.1	42400	40714	42857	11.27
September	171.2	30.80	188.5	179.8	44855	43049	45315	11.28
October	146.9	28.24	182.8	175.2	44067	42280	44506	11.42
November	119.0	21.78	171.8	165.2	42968	41189	43357	12.84
December	99.9	16.73	148.7	142.1	38404	33074	34814	10.98
Year	1925	26.26	2164	2063	530219	498487	524724	11.37

G_H	Horizontal global irradiance	Eary	Effective energy at the output of the array
Ta	Ambient Temperature	E_G	Energy injected into grid
G_I	Global incident coll.plane	EA_G	Apperent energy to the grid
G_Ef	Effective Global corr,for the IAM and shading.	Ef_S	Effic.Eout system/rough area

TABLE 5
ANNUAL ENERGY AND ARRAY EFFICIENCY FOR QASP CONFIGURATION 2

	G_H kWh/m ²	Ta °C	G_I kWh/m ²	G_Ef kWh/m ²	Eary MWh	E_G MWh	EA_G MVAh	Ef_S %
January	105.4	14.55	149.8	144.0	39423	37993	39992	12.91
February	120.7	18.94	156.8	150.2	40043	38566	40595	12.52
March	163.2	25.09	187.4	179.0	45995	44318	46650	12.04
April	184.0	30.41	188.6	179.5	45053	39298	41366	10.61
May	201.8	35.13	190.0	180.1	44456	42929	45188	11.51
June	192.2	34.35	173.9	164.3	41221	39802	41896	11.65
July	189.1	33.33	174.3	164.5	41712	40280	42400	11.77
August	180.9	32.14	178.4	169.1	42747	41243	43413	11.77
September	171.2	30.80	188.5	179.8	45237	43592	45886	11.78
October	146.9	28.24	182.8	175.2	44428	42809	45062	11.92
November	119.0	21.78	171.8	165.2	43249	41654	43846	12.35
December	99.9	16.73	148.7	142.1	38576	33473	35197	11.45
Year	1874	26.83	2091	1993	530219	485918	511492	11.83

G_H	Horizontal global irradiance	Eary	Effective energy at the output of the array
Ta	Ambient Temperature	E_G	Energy injected into grid
G_I	Global incident coll.plane	EA_G	Apperent energy to the grid
G_Ef	Effective Global corr,for IAM and shading	Ef_S	Effic.Eout system/rough area

Fig. 9 presents comparative results of the three configurations in terms of their monthly PR. It can be seen that the proposed configuration (Conf. 3) over-performs its counterparts through almost all the year. This is due to careful selection of its underlying modules which have higher efficiency and lower temperature coefficient (see Table I).

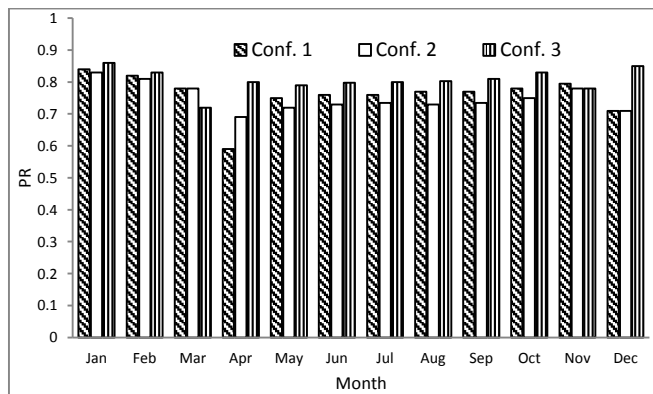


Fig. 9. PR per month for all the selected configurations.

Normalized energy for all the configurations is depicted in Fig. 10. Simulation results indicate that the monthly energy produced is comparatively larger in case of the proposed configuration in comparison with QASP

configurations. Collection losses (L_c) and System losses (L_s) are relatively less in the proposed configuration.

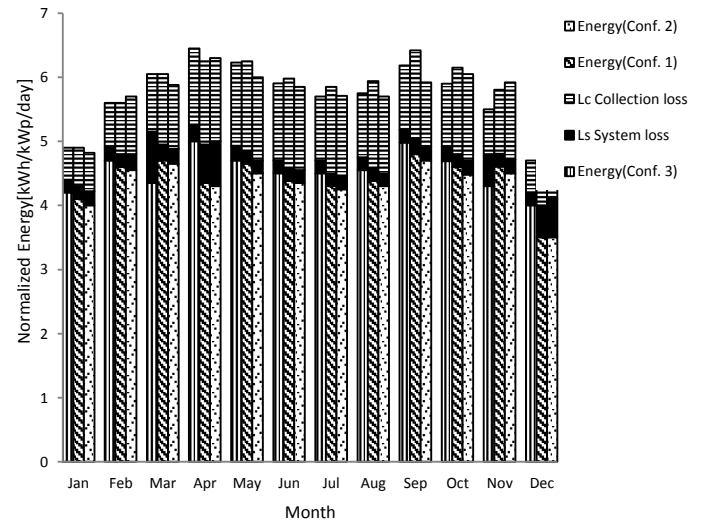


Fig. 10. Normalized energy for all the selected configurations.

Fig. 9 and 10 respectively presented monthly comparative results in terms of PR and energy injected into grid. To analyze the performance on a wider spectrum, Table 6 lists the comparison results on annual basis. Again, the proposed configuration depicts superior performance compared to QASP configurations with reference to PR as well as output energy.

TABLE 6
PR AND ENERGY PRODUCED ANNUALLY BY VARIOUS CONFIGURATIONS

Configuration	PR (%)	Energy produced (MWh)
Conf. 1	77.5	485918
Conf. 2	76.8	498487
Conf. 3	80.2	502979

The comparative results can also be stated in terms of system losses. The design which suffers from larger losses exhibit lower PR and thus lesser energy injected into the grid. In case of PV system, losses due to ambient temperature are the most dominant ones. The module efficiency and so overall PR of the system are inversely proportional to ambient temperature. Addition of energy due to module quality is higher in case of conf. 3 as compared to other configurations.

TABLE 7
LOSS DUE TO TEMPERATURE AND MODULE QUALITY LOSSES

Configuration	Loss due to temperature	Module quality loss
Conf. 1	-12.9%	+0.7%
Conf. 2	-13.4%	+0.7%
Conf. 3	-9.3%	+1.3%

Losses other than the ones due to ambient temperature have no dominant effects on changing PR and energy

injected into grid. This is obvious from Table 8 which presents global incidence on collector plane and far shading/horizon. No remarkable difference can be seen in far shading/horizon.

TABLE 8
IMPACT OF OTHER LOSSES

Configuration	Global incident on coll. plane	Far shadings/Horizon
Conf. 1	+11.6%	-2.9%
Conf. 2	+12.4%	-2.8%
Conf. 3	+11.6%	-2.9%

Tables 9-11 show that the losses due to soiling factor, irradiance level and module mismatch, ohmic wiring, inverter, auxiliaries, unavailability of system and AC ohmic are not significantly different in all the selected configurations. Thus, it is confirmed that in our case, PR is mainly dependent on temperature losses of the system.

TABLE 9
LOSSES DUE TO SOILING FACTOR AND IRRADIANCE LEVEL

Configuration	Soiling loss factor	Losses due to irradiance level
Conf. 1	-1%	-0.3%
Conf. 2	-1%	-0.4%
Conf. 3	-1%	-1.5%

TABLE 10
MODULE MISMATCHES AND OHMIC WIRING LOSSES

Configuration	Module mismatch loss	Ohmic wiring loss
Conf. 1	-1%	-1.1%
Conf. 2	-1%	-1.1%
Conf. 3	-1%	-1.1%

TABLE 11
AUXILIARIES (FAN, OTHERS), UNAVAILABILITY OF THE SYSTEM AND AC OHMIC LOSSES

Configuration	Inverter Loss	Auxiliaries Loss	Unavailability of Sys	AC Ohmic loss
Conf. 1	-1.5%	-1%	-1.6%	-1.1%
Conf. 2	-2%	-1%	-1.6%	-1.1%
Conf. 3	-1.5%	-1%	-1.7%	-1%

V. CONCLUSION

This work proposes a configuration of PV based system of 300MW capacity. Selection of inverters and modules has been carefully done to reduce losses thereby enhancing PR and energy injected into the grid. The designed configuration is then subjected to rigorous analysis in PVsyst. Finally, a comparison with a 300MW equivalent of an existing solution (i.e. QASP) is presented to validate efficacy of the proposed configuration. Our work improves %PR of QASP from 76% to 80%, enhances energy injected into grid by 4.5MW and decreases temperature losses by a factor of 4%.

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