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| 1 | URANIUM REMOVAL FROM AQUEOUS SOLUTION USING MACAUBA |
|----|--|
| 2 | ENDOCARP-DERIVED BIOCHAR: EFFECT OF PHYSICAL ACTIVATION |
| 3 | |
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The main aim of this study was to evaluate options for addressing two pressing 18 challenges related to environmental quality and circular economy stemming from 19 wastage or underutilization of abundant biomass residue resources and contamination of 20 water by industrial effluents. In this study we focused on residues (endocarp) from 21 Macaúba palm (Acrocomia aculeata) used for oil production, its conversion to activated 22 biochar, and its potential use in uranium (U) removal from aqueous solutions. Batch 23 adsorption experiments showed a much higher uranyl ions (U(VI)) removal efficiency 24 25 of activated biochar compared to untreated biochar. As a result of activation, an increase in removal efficiency from 80.5 % (untreated biochar) to 99.2 % (after activation) was 26 observed for a 5 mg L⁻¹ initial U(VI) concentration solution adjusted to pH 3 using a 10 27 g L⁻¹ adsorbent dosage. The BET surface area increased from 0.83 to 643 m² g⁻¹ with 28 activation. Surface topography of the activated biochar showed a very characteristic 29 30 morphology with high porosity. Activation significantly affected chemical surface of the biochar. FTIR analysis indicated that U(VI) was removed by physisorption from the 31 aqueous solution. The adsorbed U(VI) was detected by micro X-ray fluorescence 32 technique. Adsorption isotherms were employed to represent the results of the U 33 adsorption onto the activated biochar. An estimation of the best fit was performed by 34 calculating different deviation equations, also called error functions. The Redlich-35 Peterson isotherm model was the most appropriate for fitting the experimental data, 36 suggesting heterogeneity of adsorption sites with different affinities for uranium setting 37 up as a hybrid adsorption. These results demonstrated that physical activation 38 significantly increases the adsorption capacity of macauba endocarp-derived biochar for 39 uranium in aqueous solutions, and therefore open up a potential new application for this 40 41 type of waste-derived biochar.

| 42 | |
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| 43 | |
| 44 | Keywords: biochar, activation, macauba, endocarp, uranium. |
| 45 | |
| 46 | |
| 47 | Main finding of the work: |
| 48 | This study has shown that a low-cost biomass, such as macauba palm endocarp, can be |
| 49 | successfully converted to activated biochar by physical activation and efficiently used in |
| 50 | the treatment of industrial effluents containing U(VI). |

1. INTRODUCTION

| 54 | Activated carbon can be defined as an amorphous solid of high porosity and high |
|----|---|
| 55 | specific surface area. Well-known adsorbents of widespread use, activated carbons have |
| 56 | many applications, including purification and remediation of polluted water, treatment |
| 57 | of liquid and gaseous industrial effluents, gas storage and delivery (methane and |
| 58 | hydrogen), metal recovery, catalysis, and biomedical applications, among others |
| 59 | (Bandosz, 2006; Bansal and Goyal, 2005; De Celis et al., 2009; Kwiatkowski, 2011; Le |
| 60 | Cloirec and Faur-Brasquet, 2008; Marsh and Reinoso, 2006; Mezohegyi et al., 2012; |
| 61 | Nunell et al., 2012; Ramanujan et al., 2007; Rivera-Utrilla et al., 2011; Wang and |
| 62 | Kaskel, 2012). Growing concerns surrounding environmental pollution have led to an |
| 63 | increased demand for activated carbon in water treatment and sewage treatment |
| 64 | applications. The global activated carbon market size was estimated at USD 4.72 billion |
| 65 | in 2018 and it is expected to expand at a compound annual growth rate of 17.5% |
| 66 | between 2019 and 2025 (Grand View Research, 2019; Roman et al., 2013). |
| 67 | |
| 68 | The properties of activated carbon depend on the nature of the raw material used, the |
| 69 | type of activation agent and the conditions of both the pyrolysis process and the |
| 70 | activation itself. Characteristics such as shape, particle size, pore-volume, surface area, |
| 71 | microporous structure, pore size distribution, physical and chemical characteristics of |
| 72 | the surface define the properties and applicability of the activated carbon produced. It is |
| 73 | possible to obtain different types of activated carbon with the modification of these |
| 74 | parameters, making them more specific for a particular use (Rocha et al., 2006). |

As a result of oxidation of surface functional groups, activated carbons typically have a
non-polar or weakly polar surface (Yang, 2013). This way, it is widely used to purify,
detoxify, deodorize, filter, discolor and remove a range of liquid and gaseous materials.

Almost all solid carbonaceous material can be converted to activated carbon. However, 80 81 some characteristics must be taken into account when choosing the raw material, such as carbon content. The raw material must be high in carbon and low in inorganic matter 82 (ash). Other important factors are the cost and availability of the raw material. Recently, 83 agricultural residues have aroused a great deal of interest in the production of activated 84 biochar, because they originate from renewable and low-cost resources (Chen et al., 85 86 2011; Kalderis et al., 2008). In this way, agricultural residues that would be normally discarded gained a new potential for usability, being transformed into valuable products, 87 such as activated carbons. 88

89

The process of production of activated carbon typically involves three steps: the
preparation of the raw material, carbonization, and activation. In each of these steps, the
control of the operational conditions is decisive for the structural properties of the final
product.

94

Preparation of raw material consists of removing any dirt or foreign residue that does
not belong to the material. It also involves steps of grinding, for highest homogeneity
during thermal decomposition, and oven-drying in advance of carbonization.

Carbonization consists of thermal treatment (pyrolysis) of the precursor material (raw 99 100 material) in an inert atmosphere, at a temperature above 200 °C. In this step, the volatile 101 components and light gases (CO, H₂, CO₂ and CH₄) are removed, leaving behind a 102 porous carbon structure amenable to subsequent activation (Claudino, 2003). Biochars obtained from lignocellulosic materials are essentially microporous. However, these 103 104 pores are often fully or partially filled by thermal decomposition products, such as tar 105 (Rodriguez-Reinoso and Silvestre-Albero, 2016). Activation promotes the removal of organic compounds as well as other residues that can obstruct the pores of the biochar, 106 forming sites with enhanced adsorptive capacity (Rocha et al., 2006). 107

108

The activation process impacts on the basic characteristics of the material, such as pore
distribution and volume, density, specific surface area, and mechanical strength.
Activation exposes the aromatic groups to the oxidizing agents and initiates the
development of the microporous structure, characterizing the first phase of the process.
In the second phase, the decomposition of the walls among adjacent pores promotes
pore increase and the creation of large pores (Yang, 2013).

115

116 Activation can be carried out by chemical and physical processes. Chemical activation

relies on the action of inorganic additives, such as H₃PO₄, HNO₃, ZnCl₂, H₂SO₄, NaOH,

among others, to degrade and dehydrate the lignocellulosic material and,

simultaneously, inhibit contraction during carbonization (Mestre and Carvalho, 2018). It

120 consists of the impregnation of these activating agents into the not yet carbonized

121 material. The impregnated material is then carbonized (between 400-800 °C) in the

absence of oxygen (Contescu et al., 2018).

Activating agents generally have a dehydrating property, providing the formation of 124 125 crosslinks, rendering the material less prone to volatilization when heated to elevated temperature. In this way, the formation of bituminous compounds inside the pores is 126 127 inhibited. The product is cooled and washed to remove the remainder of the activating agent. In calcination, the chemical agents dehydrate the carbonaceous matter, resulting 128 in the creation of the pores. Peng et al. (2017) managed to enhance Cu(II) and Cd(II) 129 adsorption by modifying biochars with H₃PO₄. Trakal et al. (2014) used KOH activating 130 agent to enhance Cu(II) adsorption onto brewers draft biochar. Hadjittofi and Pashalidis 131 (2015) used HNO₃ oxidation in cactus fibers biochar for U(VI) adsorption from aqueous 132 133 solutions. Wu et al. (2019) used Fe(II, III) modified rice straw-derived biochar in soils 134 to retain phosphorous. The authors found that the adsorption capacity of Fe(II)-biochar was 2.4 times higher than biochar without any Fe. Recently, Teng et al. (2020) 135 136 employed pinecone biochar as an adsorbing material. They found that this material has great potential to adsorb Cd(II), reaching a maximum of 92.7 mg g⁻¹ of capacity. The 137 review from Xiong et al. (2019) highlighted that biochar is considered an emerging low-138 139 cost adsorbent, already been used to remove toxic elements such as Cr, Cu, As, and Pb 140 from water sources.

141

Physical activation, also called thermal activation, is the process of slow oxidation of
the char, through which it develops a porous structure, increasing its surface area. This
type of activation is performed after the carbonization process at a temperature between
700-1000 °C under appropriate flow of oxidizing gas (water steam or CO₂, used
individually or in combination). This process is also known as partial gasification
(Schettino Junior, 2004).

After physical or chemical activation, the activated biochar is subjected to subsequent
steps, such as cooling, sieving, washing, drying, polishing, granulometric separation and
packing.

152

Although chemical activation provides a greater yield, since it employs lower 153 154 temperatures and shorter activation time (Maciá-Agulló et al., 2004), the cost of activating agents, combined with the additional washing step, may favor the use of 155 physical activation. The advantages of physical activation are the possibility of 156 developing a more porous structure with a larger active area, besides having a smaller 157 environmental impact in terms of secondary pollution generation. Rajapaksha et al. 158 159 (2015) reported the enhanced removal of sulfamethazine (SMT) from water by steamactivated biochar synthesized from an invasive plant (Sicvos angulatus L.). Franciski et 160 al. (2018) used CO₂ activated biochar from solid wastes of a beer industry for 161 162 methylene blue adsorption. As reported by Zhang et al. (2019), sludge-based biochar activated with CO₂ enhanced Pb(II) adsorption. 163

164

Activation is an essential tool for the production of biochar with higher specific surface area and highly developed porosity, promoting the increase in the adsorption capacity (Gorgulho et al., 2008). In the process of activation, it is desirable to obtain a product with high internal surface area. In general, the product of activation presents a large total pore volume and a high internal surface area in the range between 300 and 2500 m² g^{-1} (Yang, 2013).

Water molecules are much smaller than CO₂ molecules, which facilitates vapor
diffusion through the porous network. As a result, steam activation yields both
micropores and mesopores with a wider range of pore size distribution, whereas CO₂
activation essentially forms and widens micropores (Dalai and Azargohar, 2007; Feng
et al., 2018). Also, CO₂ activated biochar tends to be more thermally stable (MolinaSabio et al., 1996).

178

179 IEA-R1, the largest research nuclear reactor in Brazil, is located at the Nuclear and 180 Energy Research Institute (IPEN-CNEN/SP). Currently, the reactor's fuel elements are 181 composed of low enriched uranium (LEU), i.e., up to < 20 % enriched uranium (²³⁵U 182 isotope), assembled as fuel plates of U₃Si₂ dispersed in Al. This fuel is manufactured in 183 IPEN's Nuclear Fuel Center, in sequential steps of the nuclear fuel cycle.

184

During the step of precipitation of uranium tetrafluoride (UF₄), the effluent is collected 185 and subjected to an initial treatment for prior removal of stannous ions (Sn^{2+}) and 186 fluoride ions (F⁻), which are present at very high concentrations, about 50 g L^{-1} of Sn 187 and 56 g L⁻¹ of F. This previous treatment involves sequential precipitation as Sn(OH)₄ 188 and CaF₂, decreasing these species' concentrations in the effluent to acceptable 189 regulatory levels of $< 4.0 \ \mu g \ L^{-1}$ for Sn and $< 10.0 \ \mu g \ L^{-1}$ for F, according to Brazil's 190 191 National Council for the Environment, CONAMA (CONAMA, 2011). The first precipitation step is performed by adding Na₂CO₃ to hydrolyze Sn as Sn(OH)₄. At this 192 step, part of the uranium is adsorbed on the precipitate because uranium forms a soluble 193 194 complex with the carbonate. In the second step, CaO is added for F removal as CaF₂ and U, in the form of uranyl fluoride (UO_2F_2) , is concomitantly precipitated as calcium 195 196 diuranate (CaU₂O₇).

198 Although uranium gets partially removed in this two-step precipitation stage, a remnant concentration of approx. 5 mg L^{-1} of uranium persists in solution, exceeding regulatory 199 levels (CNEN, 2014) and, therefore, it cannot be discharged into the environment as an 200 201 industrial effluent. The dispersion of radionuclides such as uranium in the aqueous 202 media (surface water and groundwater) can cause serious consequences linked to water 203 consumption. Radionuclides can be taken up and concentrated by aquatic plants and 204 animals, thereby posing a potential risk to animals higher in the food chain, including 205 humans. Also, the radionuclides can deposit in the bottom sediments and concentrate over time, increasing their long term availability to bottom feeders. All of these can 206 207 have larger implications in particular ecosystems with consequent impacts in

208 biodiversity (IAEA, 2005).

209

210 To date, a variety of carbon-based adsorbents has been investigated for U removal from wastewater including activated carbons (Abbasi and Streat, 1994; Kütahyalı and Eral, 211 2010; Mellah et al., 2006; Öter and Selçuk Zorer, 2019; Saputra et al., 2019) and 212 213 biochars (Dai et al., 2020; Guilhen et al., 2019a; Guilhen et al., 2019b; Hadjittofi and Pashalidis, 2015; Zhang et al., 2013; Ding et al., 2018). Previous investigations have 214 215 demonstrated the efficiency of the non-activated macauba biochar in the removal of uranium (Guilhen et al., 2018, 2019a; 2019b). However, since activated biochars have 216 previously indicated improved sorption capacities, the study of activated macauba 217 218 biochar for the removal of uranium is justified. To the best of our knowledge, systematic investigations on the effects of physical activation on uranium removal from 219 aqueous solution using macauba endocarp-derived biochar are virtually inexistent in the 220 221 literature, despite the prevalence of this biomass in tropical regions of the Americas.

Macauba is used for production of oil and can also be used for production of biodiesel 222 (Rivera-Utrilla et al., 2011). As a result, large quantities of discarded endocarp 223 accumulate and can pose environmental problems. Identifying an effective use for this 224 material would therefore bring about not only environmental, but also economic 225 benefits (as a result of reduced demand for unsustainable and costly activated carbon). 226 According to our previous investigation (Guilhen et al., 2019b), the low-temperature 227 biochar, namely BC350, was identified as the most promising sorbent among those 228 229 assessed. Thus, this paper focuses on exploring further improvements that can be achieved by doing the activation of this selected material. 230

231 2. MATERIALS AND METHODS

2.1. Materials

| 235 | The endocarp from the macauba palm coconut was supplied by SOLEÁ BRASIL (João |
|-----|---|
| 236 | Pinheiro, MG, Brazil). A standard solution of 1000 mg L ⁻¹ of uranium was prepared |
| 237 | through the dissolution of U_3O_8 certified reference material (CRM 129-A, natural ²³⁸ U), |
| 238 | supplied by New Brunswick Laboratory (New Brunswick, NJ, USA). This solution was |
| 239 | used to prepare both adsorption and calibration solutions. All solutions were prepared |
| 240 | with ultrapure water (18.2 M Ω cm resistivity) and analytical grade nitric acid (Merck, |
| 241 | Darmstadt, HE, Germany). |
| 242 | |
| 243 | 2.2. Sample preparation |
| 244 | |
| 245 | After an initial selection step for the removal of dirt and unbroken coconuts, the clean |
| 246 | shells were ground in a cutting mill FA300 (Rone Ind. Com. De Máquinas Ltda., |
| 247 | Carapicuíba, SP, Brazil) passing over a 3/8 mesh screen and subsequently air-dried at |
| 248 | 100 °C for 3 h. |
| 249 | |
| 250 | 2.3. Biochar production |
| 251 | |
| 252 | A Thermo Fisher Scientific (Asheville, NC, USA), Lindberg Blue M, horizontal tubular |

steel reactor, with a heating range from 100 to 1100 $^{\circ}$ C, was used to perform the

pyrolysis (Fig. 1). The pyrolysis temperature was set by a central temperature controller
and a type K thermocouple was used as secondary control inside the reactor, in the same
heating zone where the sample was placed. The samples were placed in an alumina
vessel and inserted in the reactor's tube with 0.055 m internal diameter through watercooled flanges.

259

Before initiating the pyrolysis, the reactor was purged with argon (Ar) for 20 min. Once
the targeted temperature was adjusted, the heating took place under inert argon
atmosphere. The carbonized samples were denominated as "BCT", in which "T"
corresponds to the highest treatment temperature (HTT); for instance: BC350 is the
biochar obtained at the HTT of 350 °C.

265

Approximately 30 g of dry endocarp was processed at a time, applying an argon gas flow of 40 mL min⁻¹ and a 5 °C min⁻¹ heating rate. The sample was kept at a specific HTT for 1 h (residence time). Finally, the cooled biochar was ground in a cutting mill passing over a 120 mesh screen.

270

271 2.4. Adsorption experiments

272

273 Batch technique was used for the equilibrium adsorption experiments, which were

274 performed at room temperature (25 °C) in a rotary shaker MA140 (Marconi

275 Equipamentos para Laboratórios, Piracicaba, SP, Brazil) using 100 mL glass Beckers at

- 276 120 rpm stirring rate for 24 h. The adsorbent was separated by filtration using an SCP
- 277 Science 0.45 microns Teflon membrane filter (Baie-D'Urfé, QC, Canada) and the U(VI)

278 concentration in the reminiscent filtrate solution was determined using a Spectro279 ARCOS ICP OES (Kleve, NRW, Germany).

280

281 The adsorption capacity (mg g^{-1}) of the adsorbent was calculated using Eq. (1):

282

$$q_t = \frac{(C_0 - C_t) \times V}{M}$$
 Eq. (1)

283

where " q_t " is the adsorbed amount of adsorbate per gram of adsorbent at any time "t", " C_0 " and " C_t " the concentrations of the adsorbate in the initial solution and at any time "t", respectively (mg L⁻¹); "V" the volume of the adsorbate solution added (L) and "M" the amount of the adsorbent used (g).

288

289 The extraction efficiency was determined through the following equation (Eq. (2)):

290

$$R(\%) = \left(\frac{C_o - C_t}{C_o}\right) \times 100$$
 Eq. (2)

291

where "R" is the extraction efficiency or retention percentage, " C_0 " (mg L⁻¹) is the initial concentration of each adsorbate and " C_t " (mg L⁻¹) represents the concentration of the adsorbate at time "t".

296 2.4.1. Adsorption using activated BC

297

| 298 | Although BC350 performed very promisingly in the removal of uranium from aqueous |
|-----|---|
| 299 | solutions (Guilhen et al., 2019b), the remaining solution still exceeded regulatory levels |
| 300 | (CNEN, 2014). In order to verify if activation enabled the improvement in the |
| 301 | adsorption capacity of the macauba biochar, experiments were conducted, comparing |
| 302 | both activated (BC350A) and non-activated biochar (BC350), considering various |
| 303 | initial uranium concentrations. |
| 304 | |
| 305 | To do so, independent duplicates with different $U(VI)$ concentrations, ranging from 1 to |
| 306 | 200 mg L^{-1} , were prepared in pH 3 and put in contact with a 10 g L^{-1} dosage of the |
| 307 | adsorbents (BC350-A and BC350). The system was subjected to a 120 rpm stirring rate |
| 308 | at room temperature for 24 h. These adsorption parameters have been previously |
| 309 | established through experimentation and optimized for maximum uranium removal |
| 310 | (Guilhen et al., 2019a). |
| 311 | |
| 312 | 2.5. Physical activation |
| 313 | |
| 314 | The process of physical activation, also known as partial degasification (Contescu et al., |
| 315 | 2018), was applied to the BC350. When CO_2 is used as activating agent, the activation |
| 316 | equation can be described according to the reverse-Boudouard reaction: |

$$C + CO_2 \rightleftharpoons 2CO$$
 Eq. (3)

319 $\Delta H \cong +170 \text{ kJ mol}^{-1} \text{ at } 298 \text{ K}.$

320

321 The reaction is endothermic, i.e., the product is higher in energy than the reactants.

322 Therefore, the change in enthalpy is positive and heat must be supplied to favor the

reaction. Temperatures above 700 °C are required to promote the reaction.

324

325 The activation was carried out by heating the BC350 up until 850 °C under Ar

atmosphere at a 10 °C min⁻¹ heating rate. Once the sample reached 850 °C, the Ar

supply was interrupted and a 20 mL min⁻¹ flow of CO_2 was introduced in the pyrolysis

reactor (Castro, 2009), replacing the Ar flow. The sample was kept under these

conditions for 2 h.

330

After activation, the sample was acid washed using 0.5 mol L^{-1} of HCl to remove

impurities from inside the pores, followed by subsequent washes with warm and cool

distilled water. The activated sample, denominated "BC350-A", was oven-dried at 110

³³⁴ °C and stored in a desiccator before further use.

335

336 **2.6.** N₂ adsorption analysis

| 338 | The N_2 adsorption analysis at 77 K was performed using Micromeritics, TriStar II 3020 |
|-----|---|
| 339 | V1.03 (Norcross, GA, USA), surface, and porosity analyzer. |
| 340 | |
| 341 | 2.7 Adsorption isotherm models |
| 342 | |
| 343 | Four isotherm models (Langmuir, Freundlich, Toth and Redlich-Peterson) were tested |
| 344 | for modeling the adsorption isotherms by nonlinear method. See the supplementary |
| 345 | material for further details on the isotherm models. |
| 346 | |
| 347 | 2.8 Parameter estimation |
| 348 | A "search method" called <i>Downhill Simplex</i> was used to optimize the parameters in |
| 349 | order to adjust the mathematical models that most accurately represent the observed |
| 350 | date. See the supplementary material for a full description of the method. |
| 351 | |
| 352 | 2.9 Characterization |
| 353 | |
| 354 | Nitrogen adsorption analysis was used to characterize the biochar's specific surface area |
| 355 | and adsorption isotherms were obtained to assess the $U(VI)$ adsorption onto the |
| 356 | activated biochar. Surface analysis was evaluated by Fourier-Transform infrared |
| 357 | spectroscopy (FTIR), the morphology of the activated and non-activated biochars was |
| 358 | observed by scanning electron microscopy (SEM) analysis and the presence of $U(VI)$ |
| 359 | was detected by micro X-ray fluorescence spectrometry. |
| 360 | |

| 361 | Surface analysis was carried out using a Perkin Elmer Spectrum One FTIR |
|---|--|
| 362 | spectrophotometer (PerkinElmer Inc., Waltham, USA). High-resolution imaging of both |
| 363 | activated and non-activated biochars were obtained using a FEI Quanta 650FEG |
| 364 | scanning electron microscope (FEI Company, Hillsboro, USA). A Shimadzu Micro X- |
| 365 | ray fluorescence spectrometer μ -EDX 1300 (Shimadzu Corporation, Kyoto, Japan) was |
| 366 | used to confirm the presence of uranium in the activated biochar. A Spectro ARCOS |
| 367 | inductively coupled plasma optical emission spectrometer (Spectro Analytical |
| 368 | Instruments Co., Kleve, Germany) and a Thermo iCAP inductively coupled plasma |
| 369 | mass spectrometer (Thermo Fisher Scientific, Waltham, USA) were employed for |
| 370 | multi-element analysis. |
| 371 | |
| 372 | 2.10 Application in treatment of $U(VI)$ effluent |
| 572 | |
| 373 | |
| | |
| 374 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and |
| 374 375 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such |
| 374 375 376 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such amounts that could interfere or compete in the process of U(VI) adsorption. Also, the |
| 374 375 376 377 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such amounts that could interfere or compete in the process of U(VI) adsorption. Also, the residual effluent is alkaline (pH approx. 8) and a previous study with BC350 showed |
| 374 375 376 377 378 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such amounts that could interfere or compete in the process of U(VI) adsorption. Also, the residual effluent is alkaline (pH approx. 8) and a previous study with BC350 showed that a better performance was achieved when U(VI) solution was adjusted to pH 3 |
| 374 375 376 377 378 379 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such amounts that could interfere or compete in the process of U(VI) adsorption. Also, the residual effluent is alkaline (pH approx. 8) and a previous study with BC350 showed that a better performance was achieved when U(VI) solution was adjusted to pH 3 (Guilhen et al., 2019a). The adsorption parameters have been optimized using the |
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| 374 375 376 377 378 379 380 381 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such amounts that could interfere or compete in the process of U(VI) adsorption. Also, the residual effluent is alkaline (pH approx. 8) and a previous study with BC350 showed that a better performance was achieved when U(VI) solution was adjusted to pH 3 (Guilhen et al., 2019a). The adsorption parameters have been optimized using the biochar obtained at 350 °C (BC350), because it was the temperature at which the gravimetric yield factor provided the best compromise between fixed carbon and |
| 374 375 376 377 378 379 380 381 382 | A multi-elemental analysis of the residual effluent, previously treated to remove Sn and F, was performed in order to determine which other elements were present in such amounts that could interfere or compete in the process of U(VI) adsorption. Also, the residual effluent is alkaline (pH approx. 8) and a previous study with BC350 showed that a better performance was achieved when U(VI) solution was adjusted to pH 3 (Guilhen et al., 2019a). The adsorption parameters have been optimized using the biochar obtained at 350 °C (BC350), because it was the temperature at which the gravimetric yield factor provided the best compromise between fixed carbon and gravimetric yield (Guilhen et al., 2019b). |

- 384 The removal of U(VI) from the aqueous pre-treated UF₄ effluent using BC350-A was
- evaluated by testing three sub-samples, with solution pH values adjusted from 8 to 3
- before addition of the adsorbent (Guilhen et al., 2019a). Inductively coupled plasma
- mass spectrometry (ICP-MS) was used for the determination of the remaining U(VI) in
- 388 solution.

390 3. RESULTS AND DISCUSSION

391

392 3.1. Activation

393

Uranium adsorption onto BC350-A was evaluated for a wide range of solution
concentrations between 1 and 200 mg L⁻¹, adjusted to pH 3, using an adsorbent dosage
of 10 g L⁻¹. The results are shown in Fig. 2.

397

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398 The uranium removal was significantly higher on the activated biochar (BC350-A),
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achieving over 99 % removal for an initial concentration of 5 mg L^{-1} , whereas for the

400 non-activated biochar (BC350), the removal efficiency achieved was of 80.5 % at the

401 same initial concentration (Guilhen et al., 2019b). The average remaining concentration

402 of U(VI) was 0.041 mg L⁻¹ (41 μ g L⁻¹) and the final pH measured was 5.7. Additionally,

403 the removal efficiency was over 90 % and practically constant for a wider range of

404 concentrations (2.5 to 25 mg L^{-1}) when the activated BC was used.

405

| 406 | The adsorption | capacity (q) | of BC350-A | increased with | increasing | initial | uranium |
|-----|----------------|----------------|------------|----------------|------------|---------|---------|
|-----|----------------|----------------|------------|----------------|------------|---------|---------|

407 concentrations. At an initial uranium concentration of 5 mg L^{-1} , the adsorption capacity

408 was 422.0 mg g^{-1} for BC350 (Guilhen et al., 2019b) and 488.7 mg g^{-1} for BC350-A

409 (Table S3). The highest uranium adsorption capacity ($q = 11,750 \text{ mg g}^{-1}$) in the range

- 410 investigated was achieved at an initial concentration of 200 mg L^{-1} when BC350-A was
- 411 used.

The BC350-A behavior can be explained in terms of exchangeable sites in the activated adsorbent structure, evidencing that the activation process successfully increased the adsorption sites in the biochar structure. According to Gulnaz et al. (2004), the initial increase in the adsorbate's concentration will increase the driving force of the concentration gradient, causing an increase in adsorption capacity.

418

As the ratio of uranium to BC350-A ($[U]/m_{BC350-A}$) increases, the exchangeable sites in the BC structure get saturated, resulting in decreasing driving force and removal efficiency. In contrast, the adsorption capacity increased with initial uranium concentration (constant mass of adsorbent), which may be due to an increase in the driving force of the concentration gradient as the initial adsorbate concentration increased.

425

426 The adsorption capacity achieved for an initial uranium concentration of 5 mg L^{-1} (qe =

427 488.7 mg g^{-1}) was used to compare the efficiency of BC350-A with other materials,

428 which have been previously tested as adsorbents for U(VI). When compared to other

429 organic, inorganic and biological adsorbents reported in literature, BC350-A is among

430 the highest performing adsorbents for U(VI) adsorption (Table S1).

431

432 **3.2** N₂ adsorption analysis

433

434 N₂ adsorption analysis allowed the determination of the specific surface area (BET),

435 pore volume and mean pore size for the activated and non-activated biochar samples,

436 BC350-A and BC350, respectively. The results obtained are presented in Table S2.

| 438 | As expected, the BET surface area increased with activation. Biochar activation took |
|-----|--|
| 439 | place at 850 °C, 500 degrees higher than the pyrolytic temperature employed to produce |
| 440 | the BC350 sample. Surface area increased with increasing temperatures due to the |
| 441 | escape of volatile substances and the formation of channels in the biochar structure. The |
| 442 | porosity development is further promoted by the gasification process during physical |
| 443 | activation with CO ₂ . The activation results are consistent with what has been described |
| 444 | in the literature (Ahmad et al., 2012; Chen et al., 2012; Kim et al., 2013). |
| 445 | |
| 446 | The N_2 adsorption-desorption isotherm for BC350 and BC350-A are shown in Fig. S1. |
| 447 | Type II-isotherm best fits the BC350, according to the IUPAC's classification (Martín- |
| 448 | Martínez, 1990; Thommes et al., 2015). Type II isotherms are observed for nonporous |
| 449 | or macroporous materials. |
| 450 | |
| 451 | Generally, isotherms obtained for physically activated charcoals tend to correspond to |
| 452 | the Type IV, traditionally attributed to mesoporous solids with a significant |
| 453 | microporous fraction (Crini and Badot, 2011). However, the isotherm obtained for |
| 454 | BC350-A is compatible with Type I isotherms, according to the IUPAC's classification |
| 455 | (Thommes et al., 2015), which represent microporous solids. |
| 456 | |
| 457 | Type I isotherms show a rapid increase in adsorbed gas pressure as pressure increases |

until reaching a plateau. This is due to the great ease of adsorption in pores with

diameters smaller than 2 nm. After micropore filling, there are virtually no other regions

| 460 | where adsorption is significant. The curve, therefore, exhibits an almost constant region |
|-----|---|
| 461 | and grows back when condensation begins to take place (Teixeira et al., 2001). |

| 463 | The isotherm shown in Fig. S1 (BC350-A) exhibits a hysteresis cycle. The upward |
|-----|--|
| 464 | curve represents the measurements obtained by progressive addition of the adsorbent |
| 465 | gas (adsorption) until saturation, while the downward curve represents the progressive |
| 466 | withdrawal (desorption) (Rouquerol et al., 1999). According to the IUPAC's |
| 467 | classification (Martín-Martínez, 1990), this cycle has the aspect of "H4", being |
| 468 | associated with narrow slit pores with wedge shapes, cones and/or parallel plates and |
| 469 | cylindrical capillaries open at both ends (Lowell et al., 2012; Sing, 1985; Thommes, |
| 470 | 2010; Thommes et al., 2015, 2013). |

471

It is also observed that for low relative pressure values ($P/P_0 \approx 0,1$), the volume of N_2 472 adsorbed by BC350-A is 3×10^{-1} cm³ g⁻¹, which is much higher compared to the volume 473 adsorbed by BC350 (1.4×10^{-3} cm³ g⁻¹). This increase in adsorbed volume at low 474 relative pressures is due to a higher microporous development (< 2 nm), which leads to 475 a larger specific surface area in the BC350-A. When $P/P_0 \approx 1$, the volume of adsorbed 476 gas is also higher for the activated sample and, in this case, this is related to the 477 maximum capacity of total gas adsorption by the solid, evidencing the highest porosity 478 479 in the activated biochar.

480

Pore size distribution for BC350 is shown in Fig. S2. A predominance of medium-sized
porous, characteristic of mesoporous materials (2 to 50 nm), with an average pore size
of 30 nm was observed. However, a significant macroporous fraction (> 50 nm) was

484 observed, which is consistent to the surface area of 0.83 m² g⁻¹ (0.5 to 2 m² g⁻¹) as 485 shown in Table S2.

486

Pore size distribution for BC350-A is shown in Fig. S2. A prevalence of micropores can
be observed as a consequence of the physical activation, contributing to the increase of
micropore volume (Table S2). The average pore size of BC350-A was 2.9 nm and the
pore volume was 0.3 cm³ g⁻¹, characterizing the activated material as essentially
microporous. Therefore, the isotherm data were adjusted by the t-plot method.
Comparison of the porous structure of activated and non-activated samples indicates

that the activation process clearly led to an increase in porosity of activated samples.

495 The porosity (P) of BC350-A was determined as the volume of voids in the biochar,

496 calculated according to Eq. (4):

497

498

BC350-A's true (1.98 g cm⁻³) and bulk densities (0.74 g cm⁻³) were applied in Eq. (4) and the calculated porosity (P) is approximately 63 %. Therefore, BC350-A can be classified as a material of very high porosity (P > 50 %) (Fiori and Carmignani, 2001).

503 **3.3 Adsorption isotherms**

505 The results of the U adsorption on the activated biochar, BC350-A, are presented in

506 Table S3 and could be mathematically represented by isotherms. Langmuir, Freundlich,

507 Toth and Redlich-Peterson isotherms were employed in the study of the U/BC350-A

508 system. The obtained graphs are shown in Fig. 3.

509

510 The respective parameters, obtained by non-linear regression for each isotherm model,511 are shown in Table 1.

Table 1. Experimental parameters of the adsorption isotherm models of the U/BC350-A
system.

| Langmuir | $Q_{max} (mg g^{-1})$ | | $K_L (L mg^{-1})$ | | $R^2_{adj.}$ |
|------------|--|------------------------------------|-------------------------------|------|--------------|
| | 107.08 | | 2.12 | | 0.883 |
| Freundlich | $K_F ((mg g^{-1})(mg L^{-1})^{-1/nF})$ | | n _F | | $R^2_{adj.}$ |
| | 69.94 | | 2.09 | | 0.927 |
| Toth | $K_T (L mg^{-1})$ | a _T (L mg ⁻¹ |) | t | $R^2_{adj.}$ |
| | 2.22 | 0.47 | | 0.02 | 0.872 |
| R-P | $K_{RP} (L g^{-1})$ | a _{RP} (mg L | ⁻¹) ^{-β} | β | $R^2_{adj.}$ |
| | 93.59 | 16.48 | | 0.19 | 0.955 |
| | | | | | |

However, the R² values for Freundlich and Redlich-Peterson are very close to each
other, making it difficult to use this parameter as a selection criterion. Thus, an estimate
of the best fit for the isotherm model was performed by calculating different equations
for deviation estimate, also called "error functions" (Foo and Hameed, 2010) as shown
in Table S4.

526

527 Since mathematical models are only an attempt to describe reality (Ncibi, 2008), the 528 deviation estimates are better suited to obtain a more accurate fit. The deviation 529 estimates, shown in Table S4, compare the experimental q_e (q_{eexp}), described in Table 530 S3, with the calculated q_e (q_{ecalc}) using the equations shown in Table S4. The lower 531 values of these estimates indicate the best fitting isotherms.

532



534 U/BC350-A system is based on the highest determination coefficient (R^2) and the

lowest values of RAE, SSR, MPSD, HYBRID, SAE and X^2 altogether.

536

As can be seen in Table S5, the Redlich-Peterson model provided the best fit of the

experimental data, suggesting heterogeneity of adsorption sites (Olivelli et al., 2013),

539 with different affinities for uranium, or the existence of a cooperative effect (Hinz,

540 2001), which increases the affinity between uranyl ions and adsorption sites.

541

Since the Redlich-Peterson equation is a hybrid isotherm, that incorporates
functionalities of both the Langmuir and the Freundlich isotherms (Foo and Hameed,
2010), it was expected that the fit of the experimental data for this equation would be
better than that obtained with the Langmuir and Freundlich equations. The modeling
reveals, thus, a hybrid adsorption mechanism.

547

548 This supports previous findings in recent literature. For instance, Li et al. (2019)

549 employed biochar derived from *Ficus microcarpa* aerial root and also compared raw

and modified biochar. Their findings also indicated the Redlich-Peterson to be the best

fitting isotherm for both biochars ($R^2 = 0.96$ for raw biochar, $R^2 = 0.98$ for modified

biochar). Another example is the work of Vieira et al. (2019), who studied the

adsorption of U(VI) onto macrophytes. For *Pistia stratiotes*, the Redlich-Peterson

equation provided the best fit for the experimental data ($R^2 = 0.86$, corrected Akaike

555 information criterion = -175.2).

556

557 **3.4 Characterization**

558

A comparison of FTIR spectra of BC350 and BC350-A is shown in Fig. 4. The FTIR

spectra for BC350 have been already discussed in a previous study (Guilhen et al.,

561 2019b) and Fig. 4 contrasts it against that of activated biochar.

| 563 | The absorption bands attributed to the -OH stretching of hydroxyl and carboxylic acid |
|-----|--|
| 564 | groups (3600–3300 cm ⁻¹) and to the C=C stretching of aromatic structures (1650–1520 |
| 565 | cm ⁻¹), that are practically non-existent in the BC350-A spectrum, are much more |
| 566 | pronounced in the BC350 spectrum. Previous findings (Guilhen et al., 2019b) showed |
| 567 | that the uranyl ions were adsorbed onto BC350 by chemisorption, enabled by hydroxyl |
| 568 | and carboxylic acid surface groups. Other bands corresponding to the -CH ₂ and -CH ₃ |
| 569 | stretching of aliphatic chains (2942 cm ⁻¹) and aromatic –CO and phenolic –OH at 1270 |
| 570 | cm ⁻¹ were also considerably reduced in the BC350-A sample. |
| | |

These spectra are in agreement with previous observations (Guilhen et al., 2019b) and are the result of the process of thermal decomposition, in which the increase in the pyrolytic temperature causes loss of surface functional groups and subsequent decrease in acidity and polarity of the surface (Kim et al., 2013), indicating that physisorption is the ruling mechanism of adsorption in the U/BC350-A system and was enabled because of the increased specific surface area of the BC350-A.

578

The micrographs shown in Figs. 5 and 6 correspond to the topography images of the
BC350 and BC350-A, respectively.

581

582 Despite the high heterogeneity of the surfaces, the morphology of BC350 is very

583 characteristic of chars, with porous cavities and intertwined channels formed by the

transport of water vapor and volatiles to the surface of the material (Bandosz, 2006).

In the micrographs of BC350-A (shown in Fig. 6) it is possible to observe a morphology that is characteristic of activated chars. The release of volatile components promoted the formation of a structure with vascular bundles or channels that provide greater permeability to the material due to the increased surface area.

590

These microscopic images evidence the role of activation in removing residues that 591 remained from the biomass decomposition and the volatilization of bituminous 592 substances and tars during the process of carbonization, in which rudimentary pores are 593 already created. On physical activation, these residues react with the flow of gases (in 594 595 this case, CO₂) at elevated temperatures (850 °C), getting oxidized. As a result, the pre-596 existing pores get cleared and widened (because CO₂ oxidizes the carbonaceous 597 material present inside the pores as well), increasing the surface area. An increased surface area exposes more surface groups, favoring chemical and physical interactions 598 with uranyl ions. 599

600

Energy-dispersive micro X-ray fluorescence spectrometry (Micro-XRF) was employed
to detect the presence of adsorbed uranium in BC350-A. This technique was selected
over the conventional XRF because of its sensitivity, capable of detecting uranium in
lower concentrations. Therefore, this technique provides evidence that the uranium was
actually absorbed onto BC350-A. The results are shown in Table S6.

606

607 The characteristic X-rays emitted by the innermost layers of a given element are 608 grouped under the name K_{α} and K_{β} , resulting from electronic transitions $L \rightarrow K$ and M 609 $\rightarrow K$, respectively (Lyman series). Similarly, the characteristic X-ray emission lines L_{α} 610 and L_{β} originate from the electronic transition of the layers $M \rightarrow L (L_{\alpha 1}, L_{\alpha 2} e L_{\beta 1})$ and 611 $N \rightarrow L (L_{\beta 2})$ (Balmer series) (Khoury Asfora, 2010).

612

613 The emission line K_{α} characteristic of "Fe" has a very low intensity, indicating its

- 614 presence as a probable impurity in the material. The K_{α} and $K_{\alpha C}$ (Compton) lines of Rh
- are due to the Rh tube (the X-ray source).

| 617 | Exposure of the sample to the X-ray beam promotes the excitation of the L layers in the |
|-----|--|
| 618 | adsorbed U. The β transition lines of U (16.48 keV and 17.23 keV) are the least likely to |
| 619 | occur and have higher energy than the α transition line (13.66 keV). The indices "1" and |
| 620 | "2" in the transitions $L_{\beta 1}$ and $L_{\beta 2}$ indicate the transition between the sublayers M-IV \rightarrow |
| 621 | L-II and N-V \rightarrow L-III. The most intense transition occurs in L _a . Since uranium has |
| 622 | electrons distributed in layers of orders higher than M, it is also possible to identify a |
| 623 | transition U M _{β} referring to the transition N-V (O) \rightarrow N-3 (M) (Paschen series). |
| 624 | |
| 625 | Micro-XRF analysis provided an efficient way to identify the U present in the |
| 626 | adsorbent, thus proving the effective adsorption onto BC350-A. |
| 627 | |
| 628 | 3.5 Application in UF4 effluent treatment |
| 629 | |
| 630 | As can be seen in Table 2, the sequential initial treatment reduced the concentration of |
| 631 | Sn and F species in solution to values lower than the allowable limits according to the |
| | |

- 632 Resolution nº 430 of the Brazilian National Council for the Environment, CONAMA
- 633 (CONAMA, 2011).
- 634
- **Table 2.** Sn, U and F levels after the pre-treatment in the Nuclear Fuel Center.

| Element | Effluent | Effluent | Maximum | | |
|--------------------|---------------------------------------|-------------|----------------------|-------------------|--|
| $(\mu g m L^{-1})$ | (Initial) | (Final) | levels | Regulatory Agency | |
| Sn | $5\times10^4\pm1.6\times10^2$ | < LOD | 4 | CONAMA (2011) | |
| U | $7.6\times10^1\pm3\times10^{-1}$ | 5.1 ± 0.6 | 2.2×10^{-1} | CNEN (2014) | |
| F | $5.6 \times 10^4 \pm 1.4 \times 10^2$ | 5.7 ± 0.5 | 10 | CONAMA (2011) | |

 $*LOD = 0.5 \ \mu g \ mL^{-1}$

637

However, CONAMA's Resolution Nº 430 (CONAMA, 2011) does not include the

639 maximum values for U release. Therefore, the liberation of effluents containing U must

640 comply with CNEN's resolution CNEN-NN-8.01 (CNEN, 2014), for which the

641 maximum limit for the mixture of U isotopes in the UF₄ effluent (80.25 % for 238 U and

642 19.75 % ²³⁵U isotopic ratio) was calculated according to their respective specific

- 643 activities, considering an allowable discharge level of 5.6 kBq m^{-3} for both isotopes (see
- section 3.5 of the supplementary Material).
- According to the results presented in Table 2, the two-step treatment resulted in a
- solution in which the remaining U concentration was 5 mg L^{-1} , therefore, not efficient
- enough to comply with the regulatory demands (CNEN, 2014).

| 649 | A complementary treatment of this solution, initially at pH 8, was performed using the |
|-----|--|
| 650 | activated biochar (BC350-A) and the pH of the solution was adjusted to 3. After |
| 651 | adsorption, the remaining U concentration in solution was $1.1 \times 10^{-1} \ \mu g \ mL^{-1}$ (2.8 kBq |
| 652 | m ⁻³) The presence of Na ⁺ ions in the solution ($2.7 \times 10^3 \ \mu g \ mL^{-1}$) has likely influenced |
| 653 | the adsorption process, decreasing the removal efficiency initially achieved for the |
| 654 | aqueous solution (Na^+ free) from 99.2% (4.1 \times 10^{-2} μg mL^-1) to 97.9% (1.1 \times 10^-1 μg |
| 655 | mL ⁻¹). Other elements such as Mg, B, Zn, Ni, As, Cu, Ba, Cr, Pb, Mn, Se, Fe, Cd and |
| 656 | Ag were also determined in the UF4 effluent by ICP OES, but none of them scored |
| 657 | higher than $1 \times 10^{-1} \ \mu g \ mL^{-1}$, therefore, their influence were considered negligible |
| 658 | regarding coexistence interactions. Moreover, the U concentration in the treated solution |
| 659 | was below the maximum allowable limits of 5.6 kBq m ⁻³ (CNEN, 2014). |
| | |

661 4. CONCLUSION

662

663 CO₂ physical activation significantly enhanced the adsorption capacity of macauba endocarp-derived biochar for uranyl ions in aqueous solutions, achieving over 99 % 664 removal for an initial concentration of 5 mg L^{-1} . The activation process led to an 665 increase in porosity with a specific surface area increasing from 0.83 to 643 m² g⁻¹. 666 Chemical surface of the biochar was significantly affected by activation. According to 667 668 the FTIR analysis, the activation process increased the aromaticity of the biochar, 669 indicating that the uranium adsorption was carried out by physical interactions. The 670 adsorption of uranyl ions onto the activated biochar was confirmed by µ-EDX analysis. 671 The Redlich-Peterson three-parameter equation isotherm model was the most

appropriate for fitting the experimental data, suggesting heterogeneity of adsorption
sites with different affinities for uranium setting up as a hybrid adsorption mechanism.
Finally, treating an actual U-containing effluent with BC350-A has proven to be
efficient in meeting the regulatory requirements. This study has therefore shown that an
ubiquitous low-cost biomass material such as macauba palm endocarp can be
successfully converted to activated biochar and used in treatment of industrial effluents,
specifically those containing uranyl ions.

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687

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884 Figure Captions

- **Fig. 1**. Scheme of the biochar/activated biochar production apparatus.
- **Fig. 2**. Removal efficiency (a) and adsorption capacity (b) for BC350 and BC350-A.
- **Fig. 3**. Adsorption isotherms of the U onto BC350-A.
- **Fig. 4.** FTIR/UATR vibrational spectrum of BC350 and BC350-A.
- **Fig. 5.** BC350 micrographs obtained by SEM in different magnifications.
- **Fig. 6.** BC350-A micrographs obtained by SEM in different magnifications.