



Characterization methods for additive manufacturing:

Influence of processing strategies on residual stresses, microstructure and defects in AM materials and components

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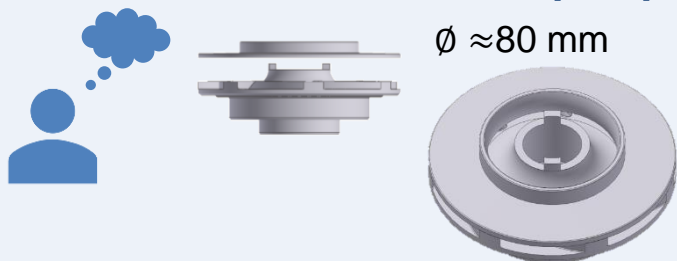
June 2nd, 2021



Knowledge for Tomorrow

Motivation – „easy printing“?!

Rocket Turbo-Pump Impeller*



Idea: printed as a single part



First result:
support cracks, deformation



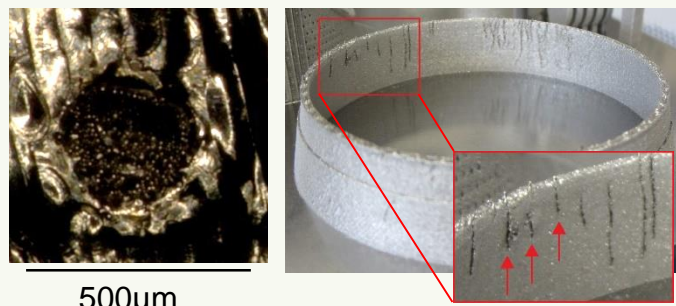
Volume Parameters Optimization

- Residual Stresses
- Porosity
- Microstructure

Injector element**



Idea: small channels
($\varnothing \approx 300\text{-}400\mu\text{m}$)



First result:
blocked channels or cracks



Contour Parameters Optimization

- Residual Stresses
- Surface Roughness

Outline

Part I – Cuboids (Ti-6Al-4V)

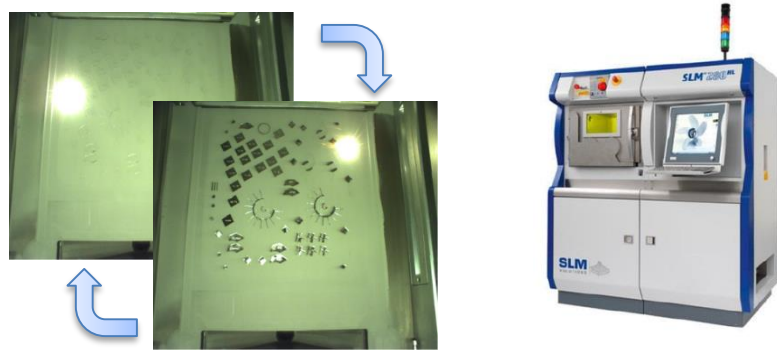
- Influence Factors for Parameter Optimization
- Residual Stress Measurement – Method
- Optimization of Volume Process Parameters
- Optimization of Contour Process Parameters

Part II – Outlook: Components (Ti-6Al-4V)

- Transferability: from Coupon to Component

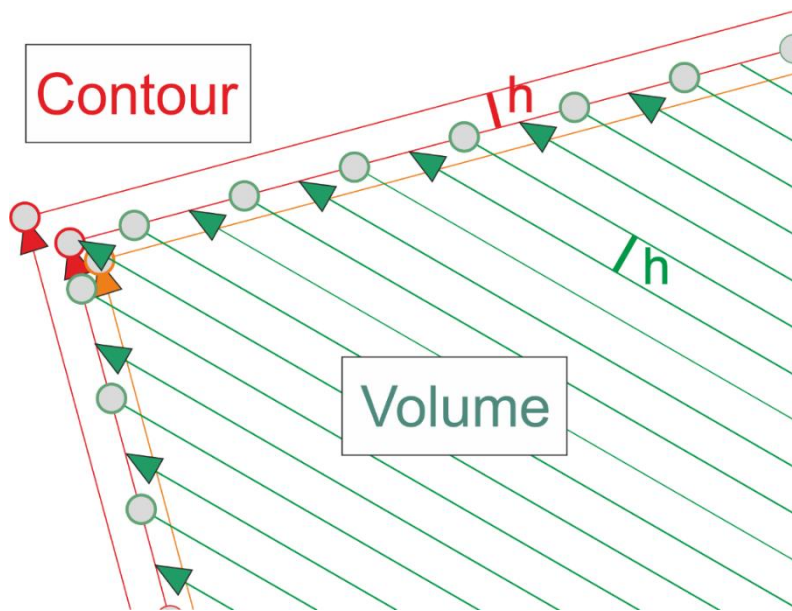


Influence factors for parameter optimization (L-PBF)



Machine used for this study:

SLM Solutions 280^{HL} single
 (280 x 280 x 300 mm³; up to 1200 °C; melt pool monitoring;
 improved: processing atmosphere and mass spectrometry)



Investigated process parameters:

- Hatch distance h
- Laser power P
- Scanning velocity v
- Number of Contour Lines
- Scan order (Volume/Contour)

Volume Energy Density

$$E_v = \frac{P}{hv}$$



Outline

Part I – Cuboids (Ti-6Al-4V)

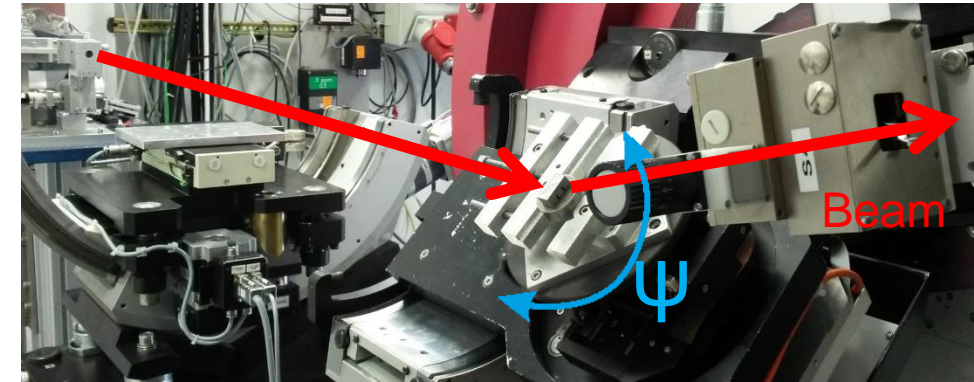
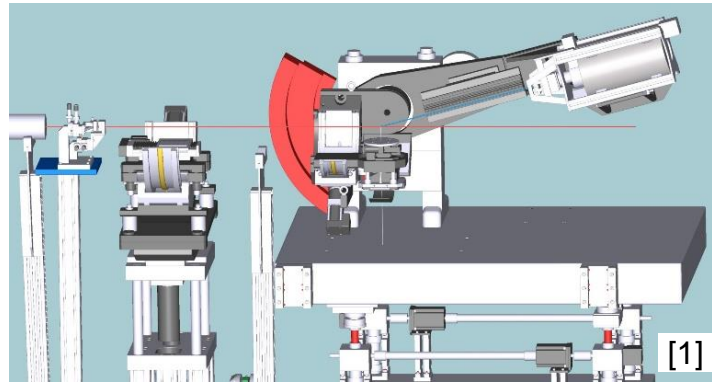
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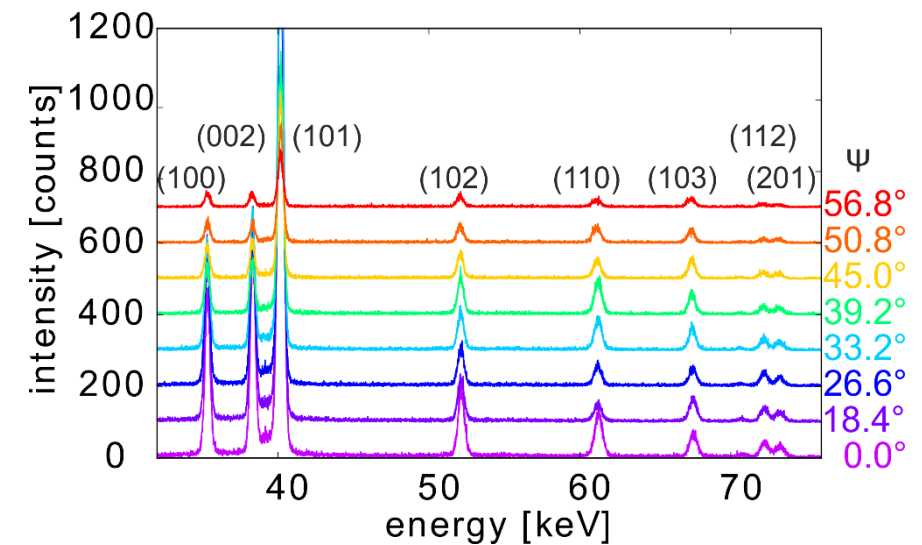
- Transferability: from Coupon to Component



Residual Stress Measurements Method



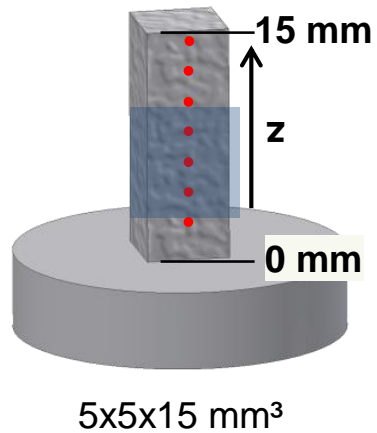
- Synchrotron source BESSY II (HZB, Berlin, Germany)
- Beamline 7T-MPW-EDDI (energy-dispersive mode of diffraction)
- Measurement in reflexion (subsurface)
- No texture near surface
 - isotropic diffraction elastic constants
- $\text{Sin}^2\psi$ -method
- Material: Ti-6Al-4V
- Peak (103) used for stress calculation



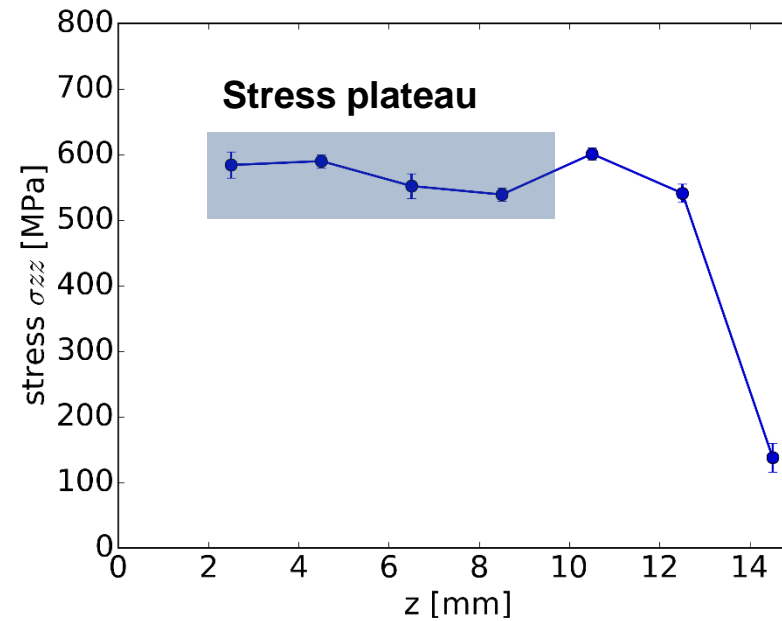
Residual Stress Measurements

Specimens

Measurement Positions



Stresses in Build Direction



- **High tensile stresses** in build direction
- **Stress plateau** in the middle
→ stress values in this region will be averaged for further comparisons



Outline

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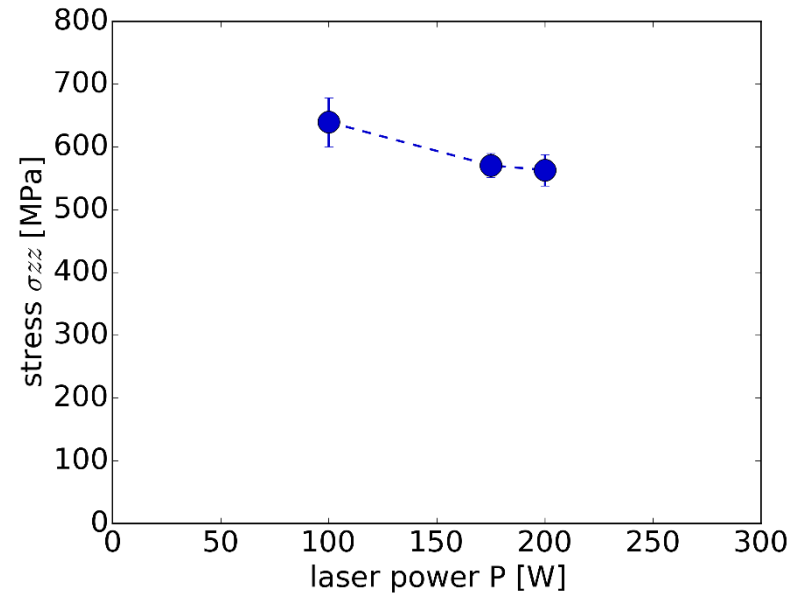


Optimization of Volume Process Parameters

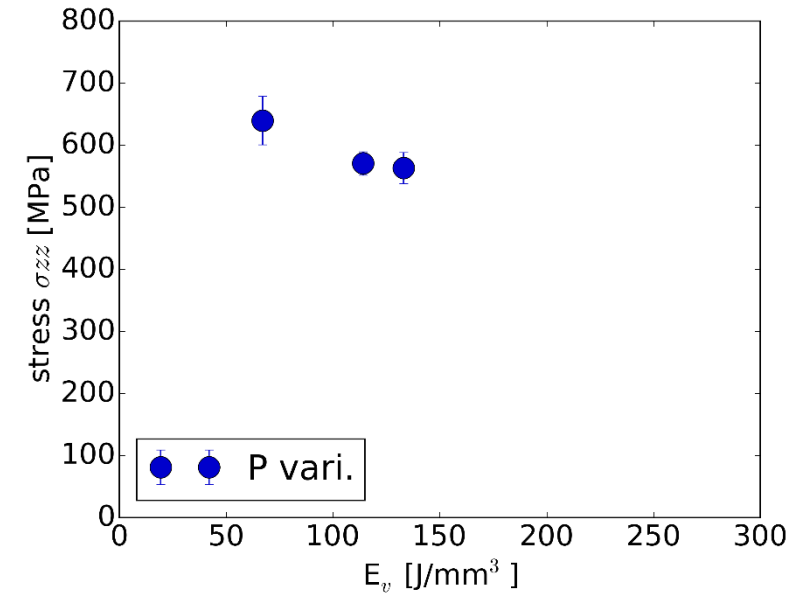
Residual Stresses

Variation of

- Laser Power P



$$E_v = \frac{P}{hv}$$

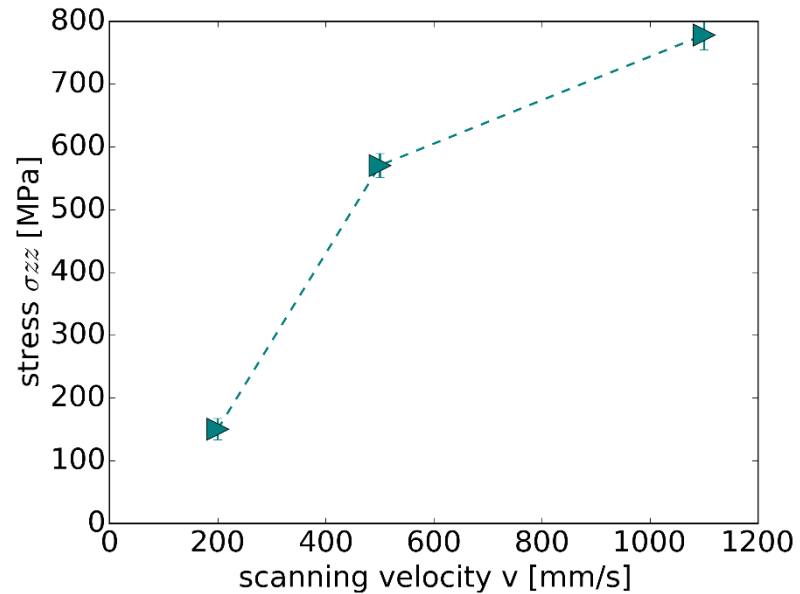


Optimization of Volume Process Parameters

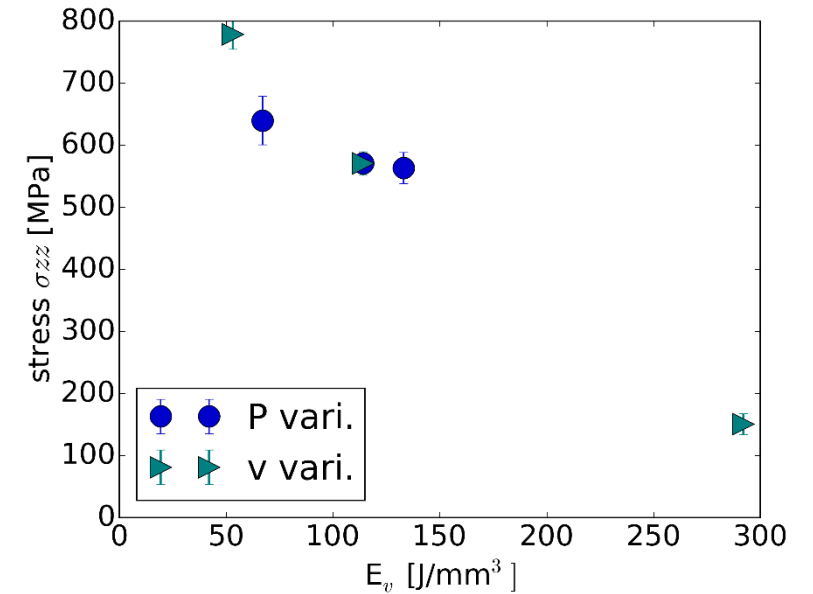
Residual Stresses

Variation of

- Laser Power P
- Scanning Velocity v



$$E_v = \frac{P}{hv}$$

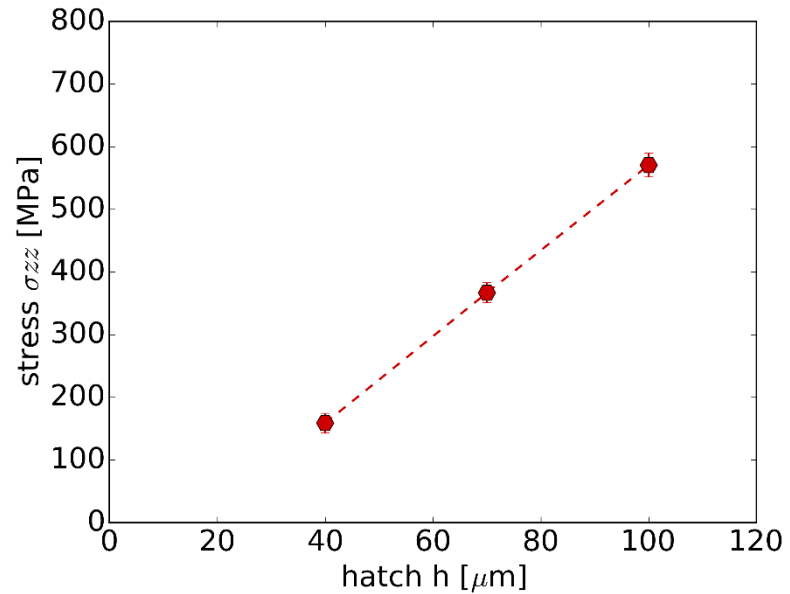


Optimization of Volume Process Parameters

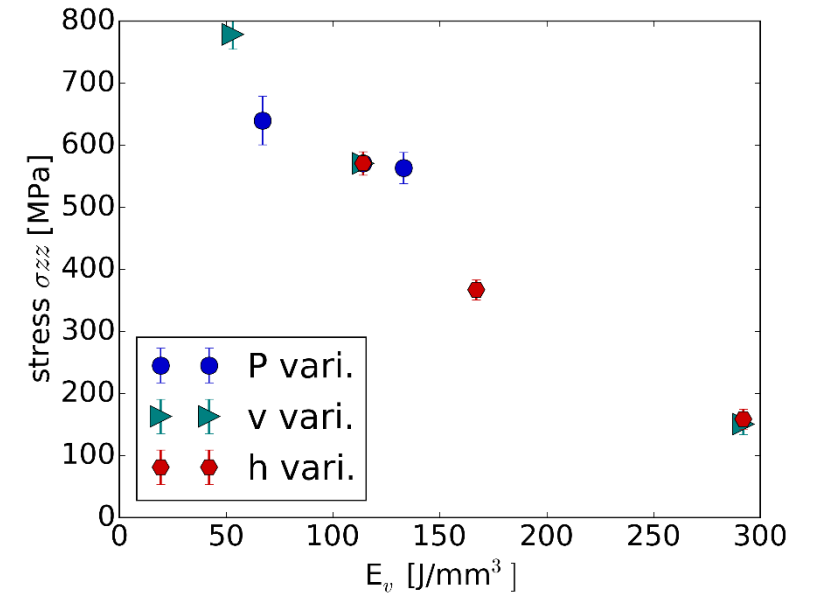
Residual Stresses

Variation of

- Laser Power P
- Scanning Velocity v
- Hatch h



$$E_v = \frac{P}{hv}$$

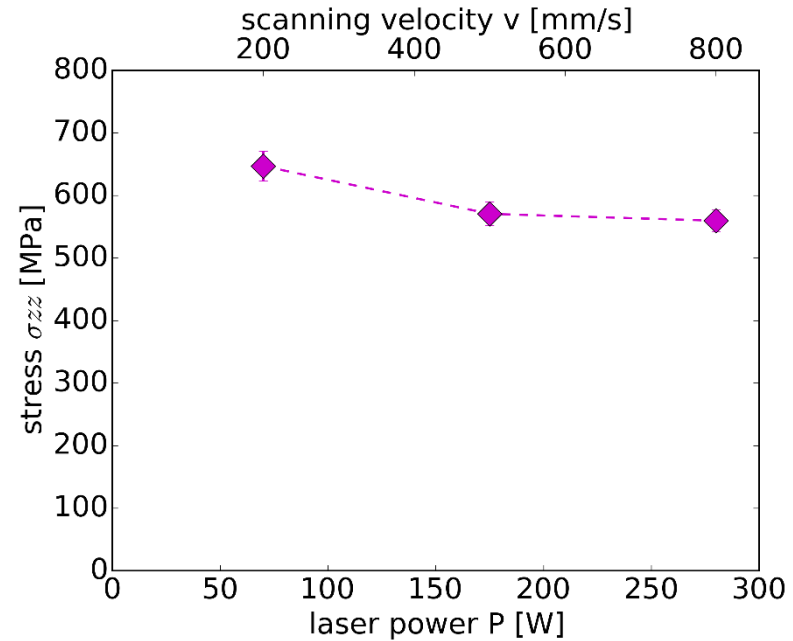


Optimization of Volume Process Parameters

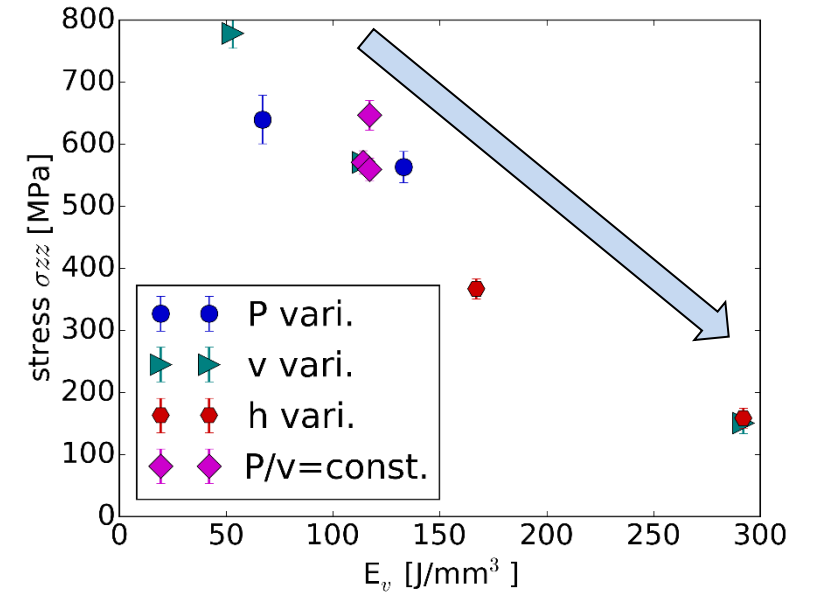
Residual Stresses

Variation of

- Laser Power P
- Scanning Velocity v
- Hatch h
- $P/v=\text{const.}$



$$E_v = \frac{P}{hv}$$



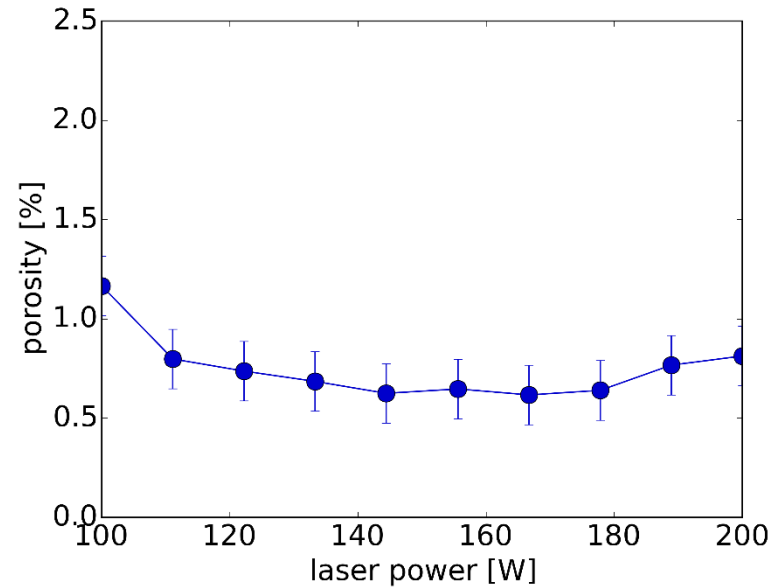
Optimization of RS for Volume Process Parameters: **High $E_v \rightarrow$ low residual stresses**

Optimization of Volume Process Parameters

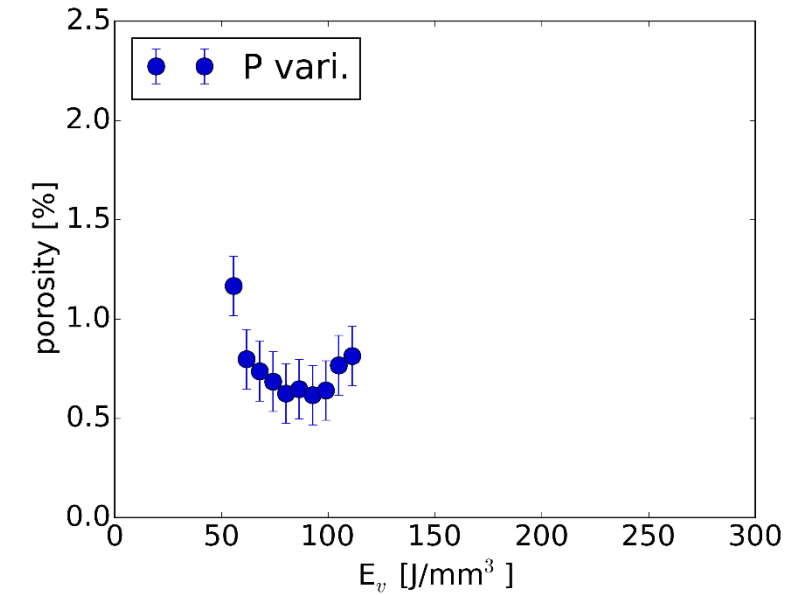
Porosity

Variation of

- Laser Power P



$$E_v = \frac{P}{hv}$$

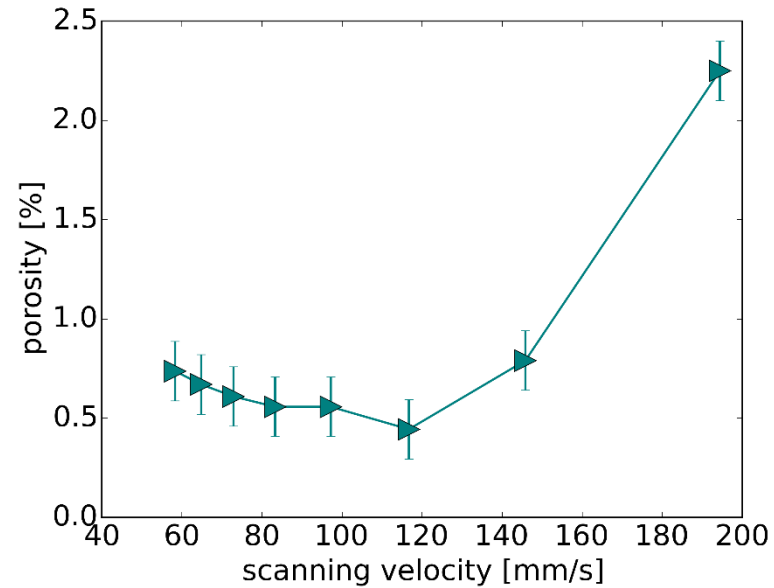


Optimization of Volume Process Parameters

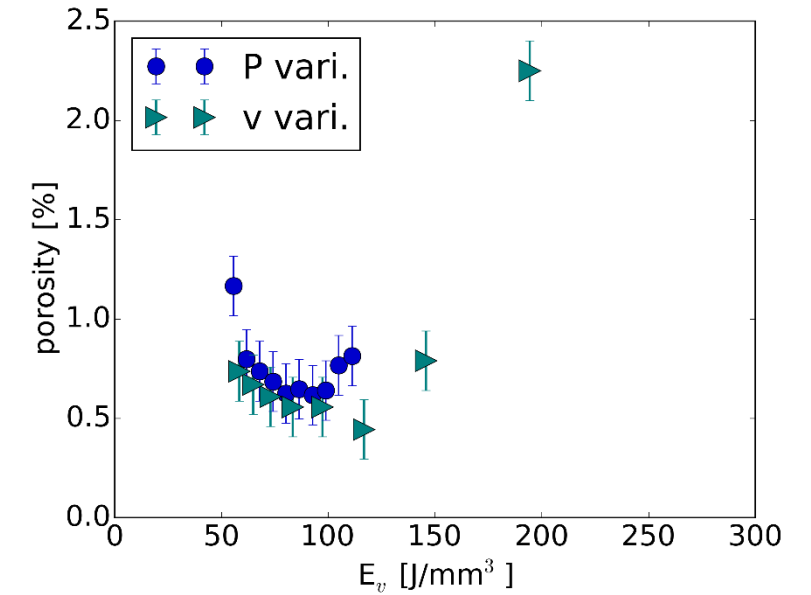
Porosity

Variation of

- Laser Power P
- Scanning Velocity v



$$E_v = \frac{P}{hv}$$

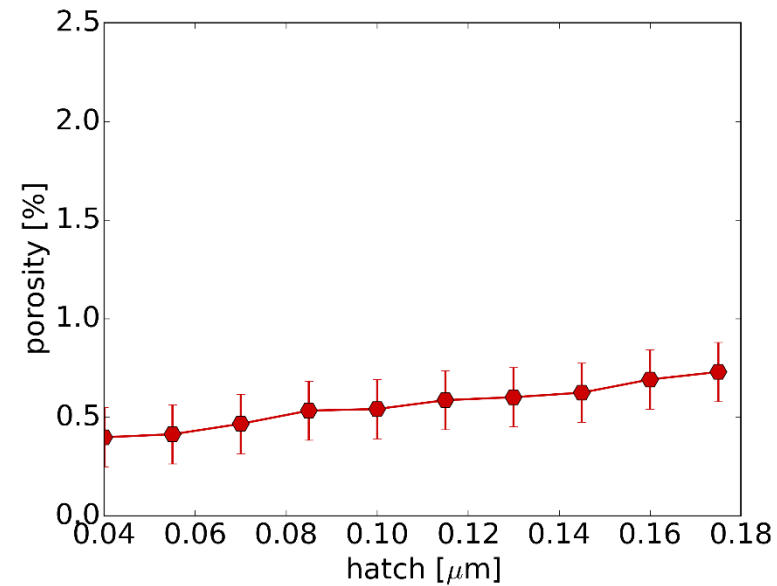


Optimization of Volume Process Parameters

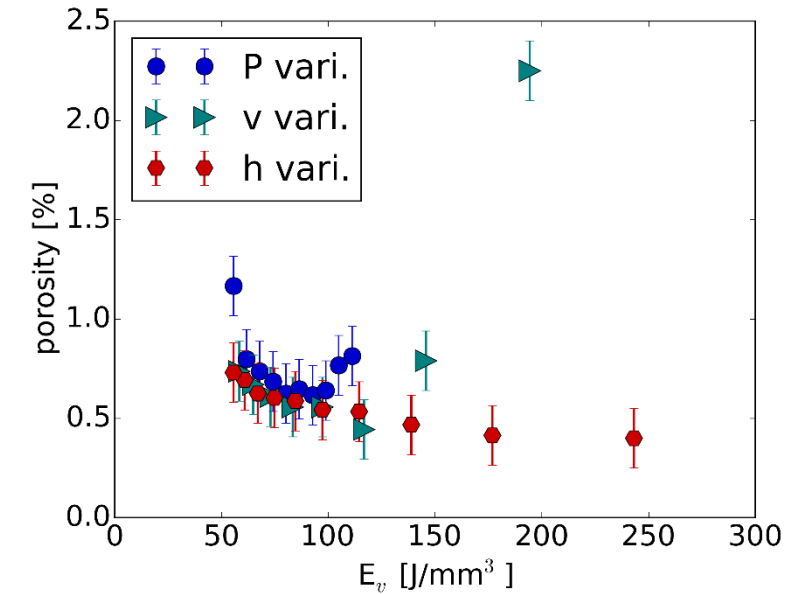
Porosity

Variation of

- Laser Power P
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$$E_v = \frac{P}{hv}$$

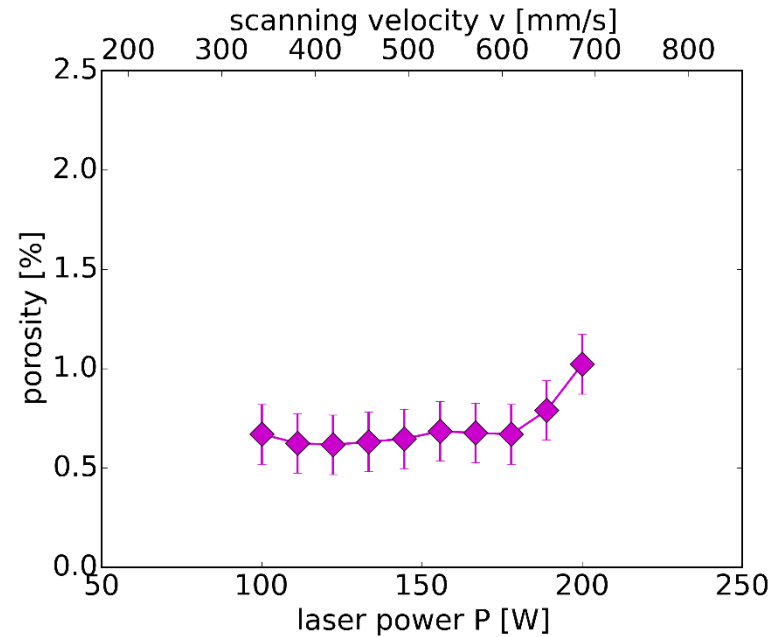


Optimization of Volume Process Parameters

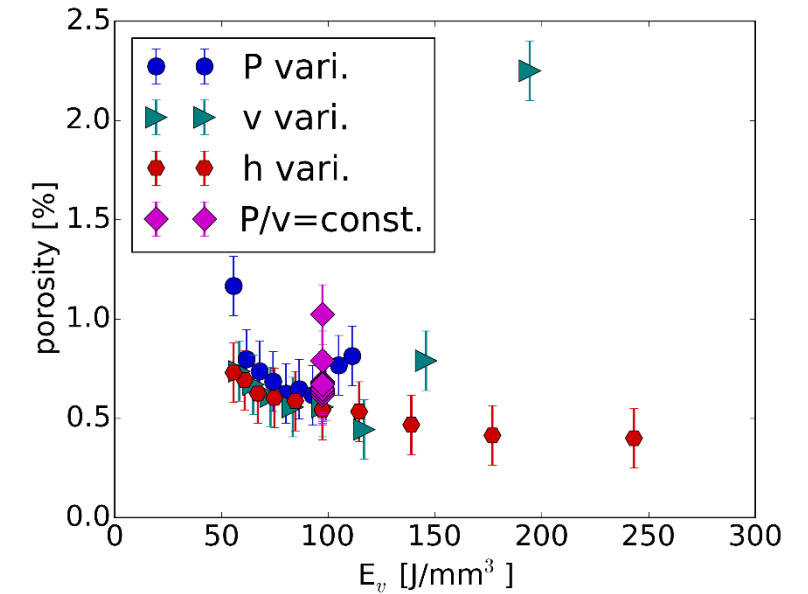
Porosity

Variation of

- Laser Power P
- Scanning Velocity v
- Hatch h
- $P/v=\text{const.}$



$$E_v = \frac{P}{hv}$$



Optimization of Porosity for Volume Process Parameters:

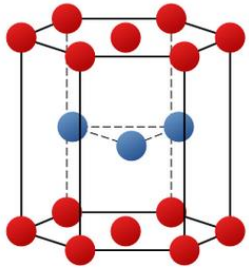
- P & v : Optimum exists for $E_v \sim 80\text{-}150 \text{ J/mm}^3$
- h : Porosity decreases with decreasing hatch distance (high E_v)



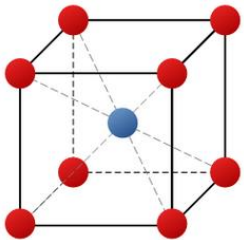
Optimization of Volume Process Parameters

Microstructure

α -phase / α' martensite:
hcp \rightarrow brittle

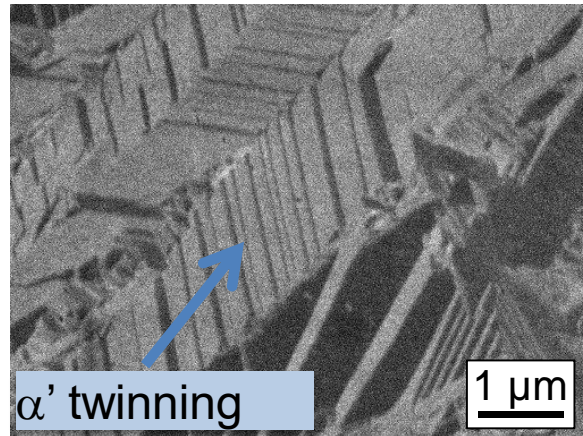


β -phase: bcc
 \rightarrow ductile

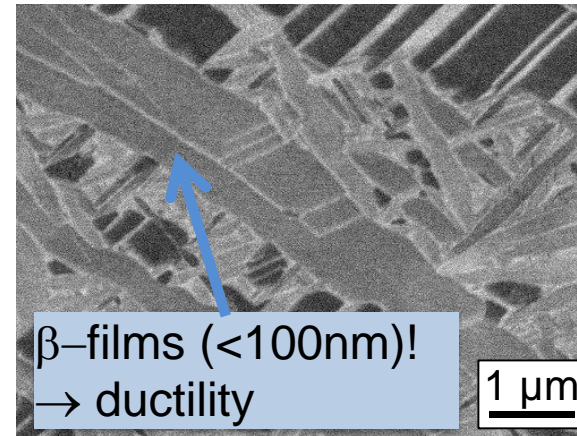


Lattice structures:
www.tec--science.com

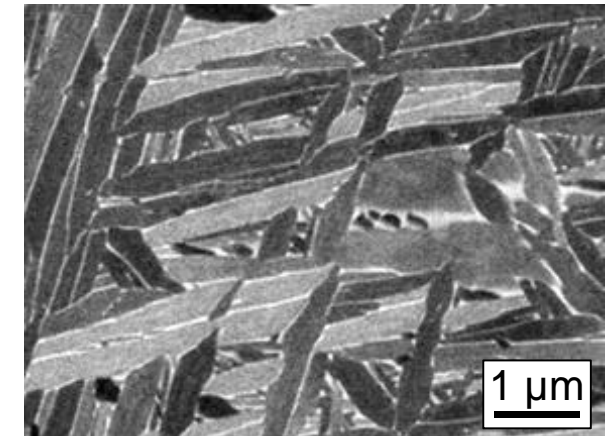
Low E_v (77 J/mm³)



Intermediate E_v (145 J/mm³)

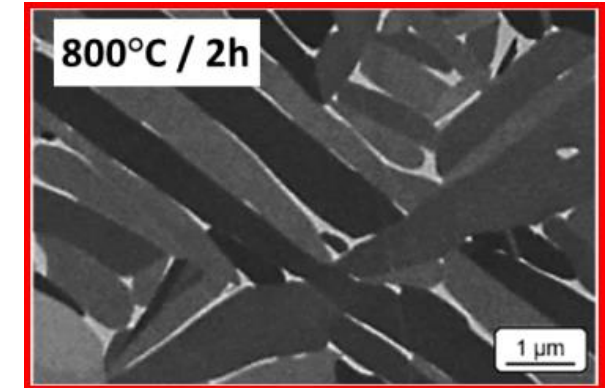


High E_v (243 J/mm³)



- \rightarrow Microstructure dependent on E_v
- \rightarrow E_v increase \Rightarrow increase in β volume fraction
- \rightarrow stabilized $\alpha+\beta$ microstructure possible at high E_v
- \rightarrow **Post-Processing:**
Heat treatment or Hot-Isostatic Pressing

800°C / 2h

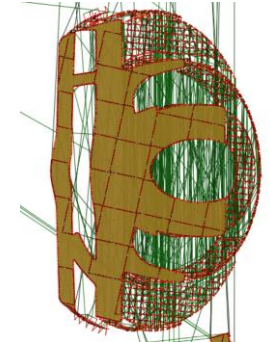


Optimization of Process Parameters

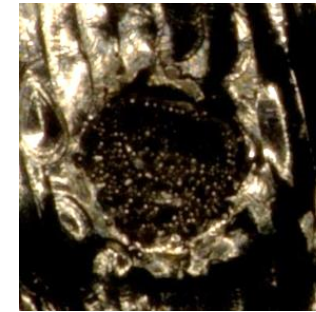
Summary I

Recommendation – Volume Process Parameters:

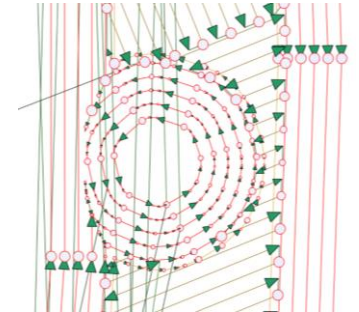
- **Hatch distance** ↓ ⇒ **Minimal stresses + porosity** (- higher build time)
- Post-processing: Heat treatment for ductile microstructure
→ solution for the impeller?



Recommendation – Contour Process Parameters?
Solution for the injector element?



500µm



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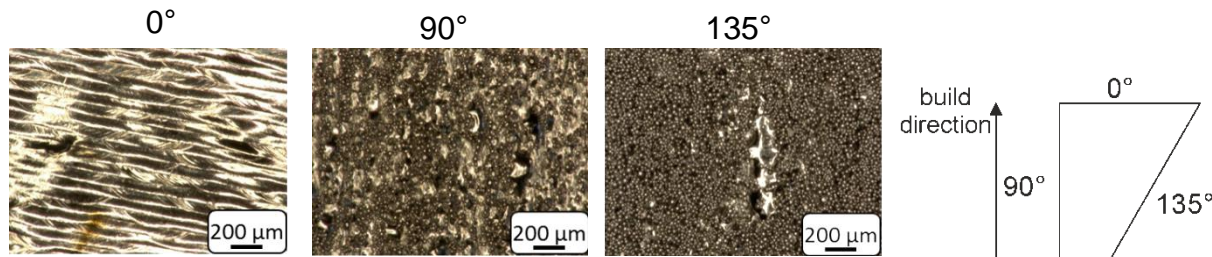
- Transferability: from Coupon to Component



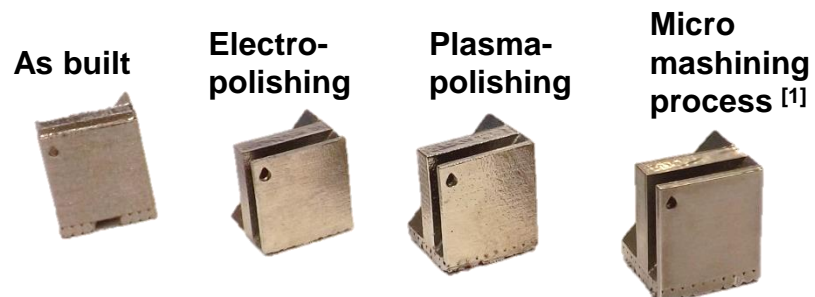
Optimization of Contour Process Parameters

Surface Roughness

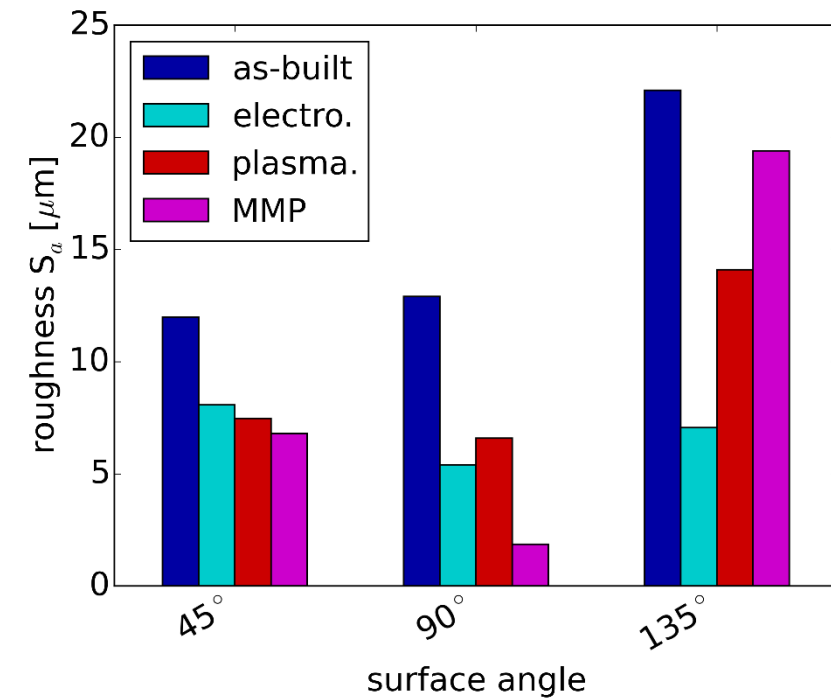
Roughness strongly dependent on orientation



Post-Processing: surface finishing

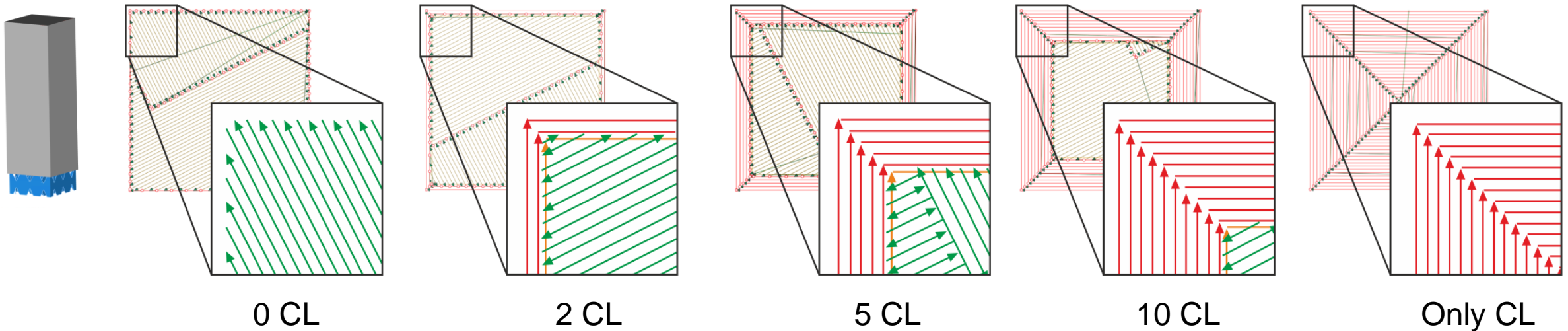


Example for S_a -values



Optimization of Contour Process Parameters

Scan Strategy

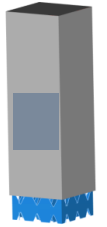


Standard Process:

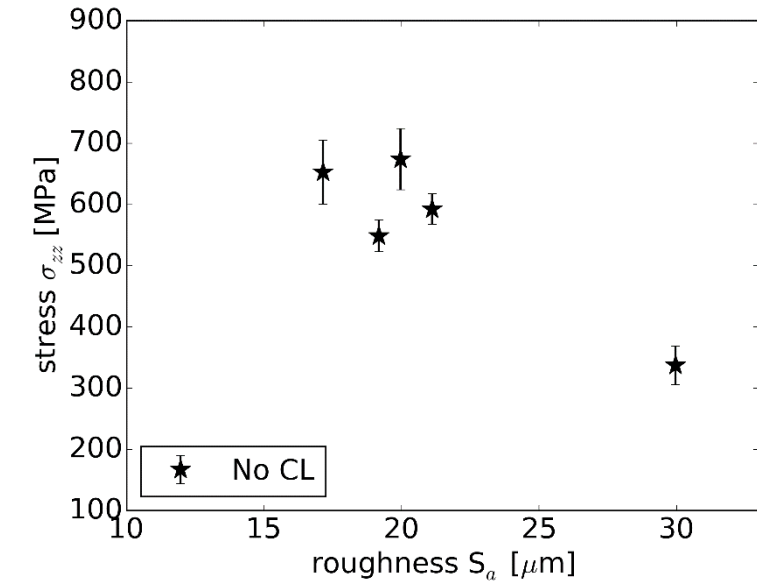
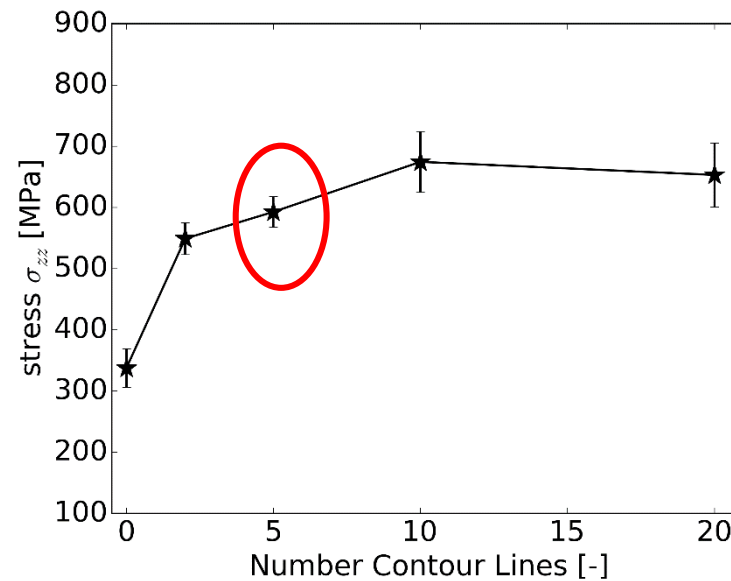
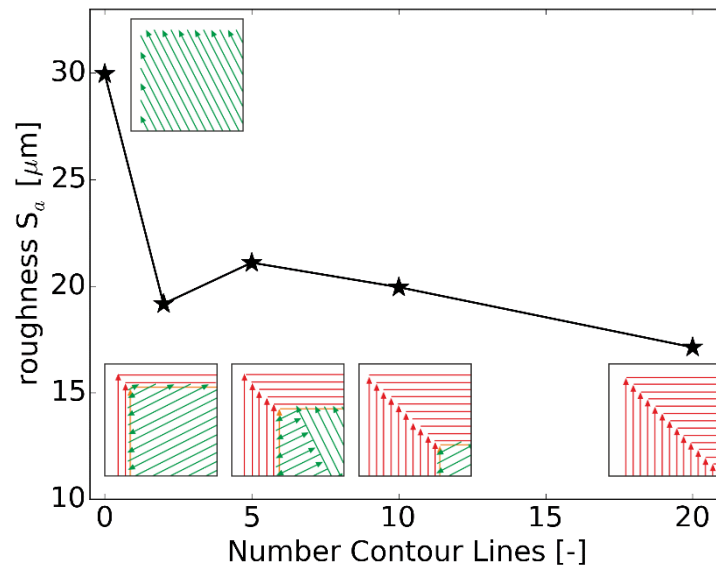
- 2 Contour Lines
- Scan order: Contour (out → in) → Volume



Optimization of Contour Process Parameters



Contour Line Number Variation

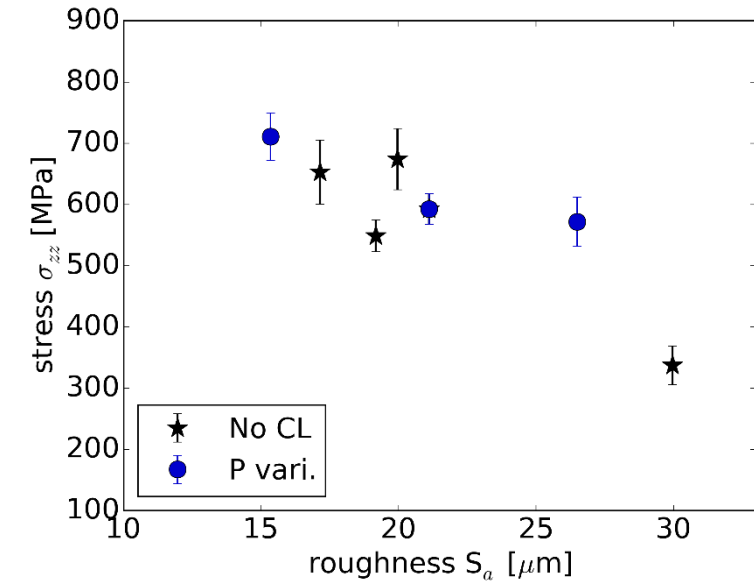
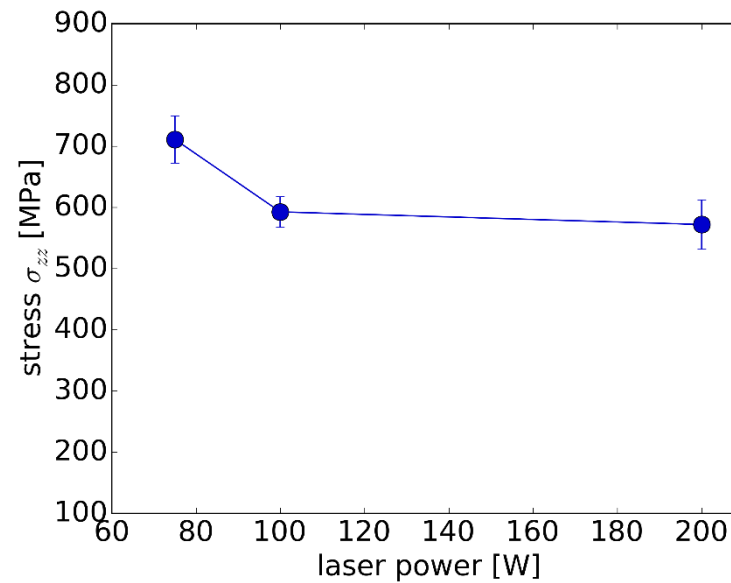
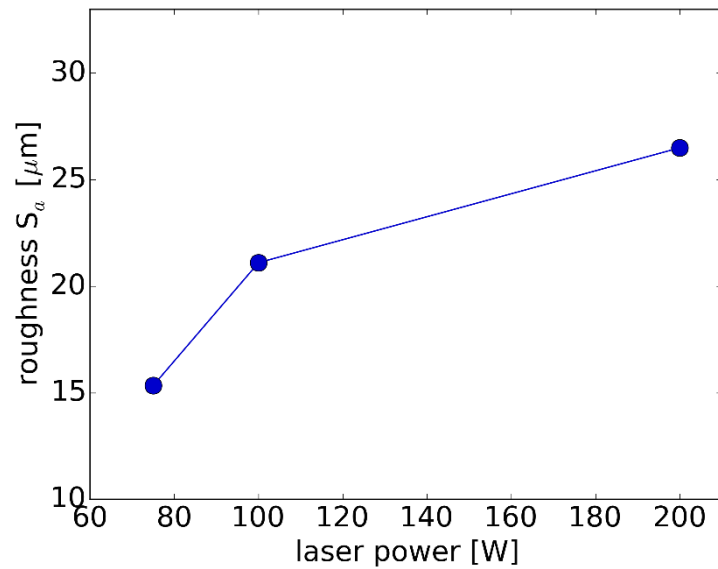


For Residual Stress Measurements:

- 5 Contour Lines; Standard Scan Order;
- Volume process parameters kept constant, contour parameters (P, h, v) are varied

Optimization of Contour Process Parameters

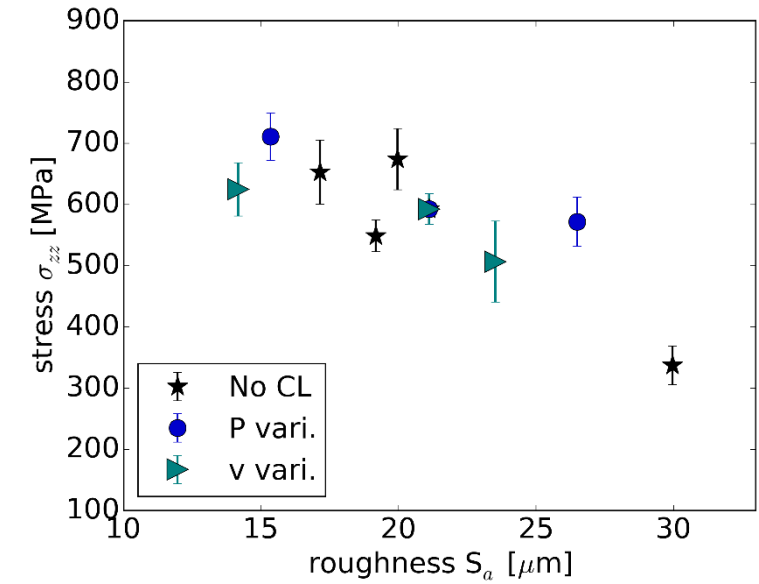
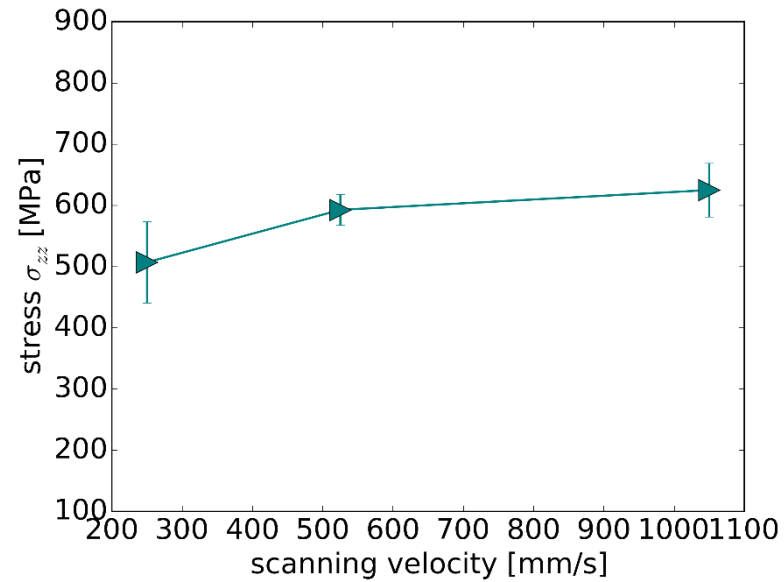
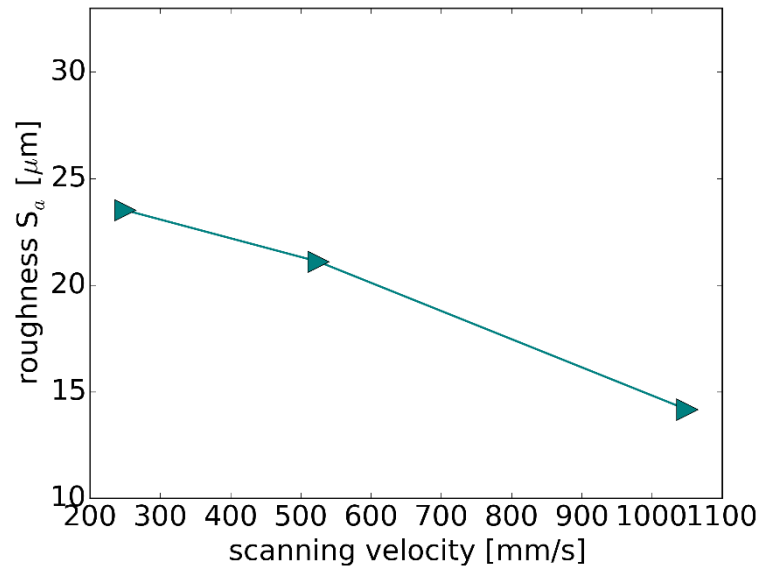
Laser Power Variation



- Laser Power: $P \uparrow \Rightarrow S_a \uparrow, \sigma \downarrow$

Optimization of Contour Process Parameters

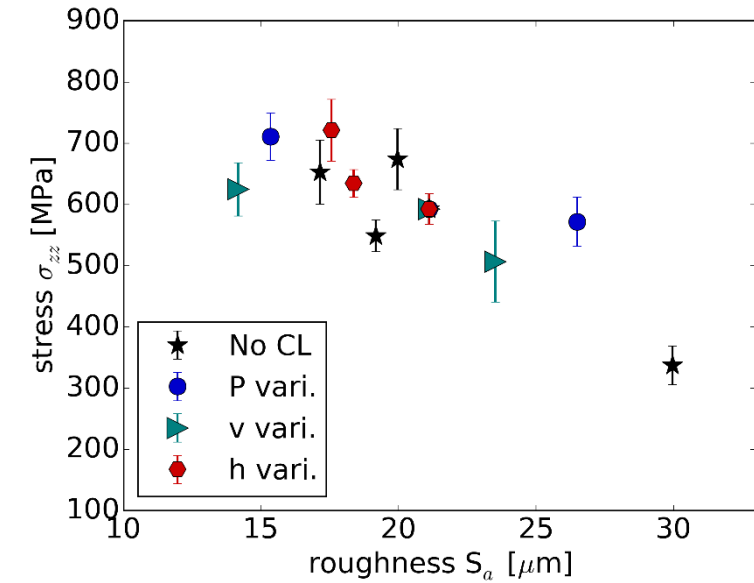
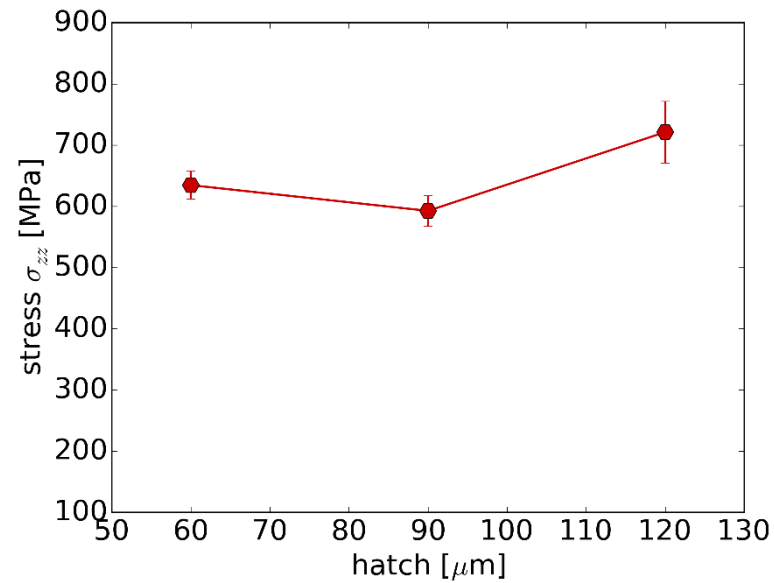
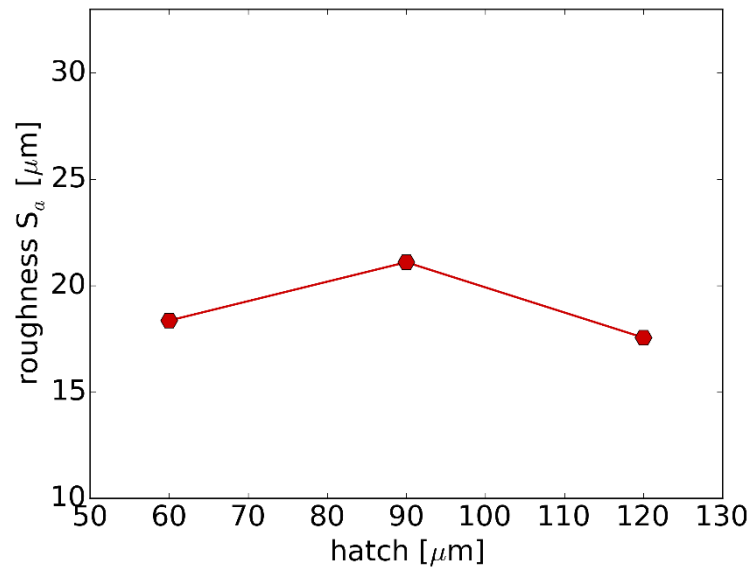
Scanning Velocity Variation



- Laser Power: $P \uparrow \Rightarrow S_a \uparrow, \sigma \downarrow$
- Velocity: $v \uparrow \Rightarrow S_a \downarrow, \sigma \uparrow$

Optimization of Contour Process Parameters

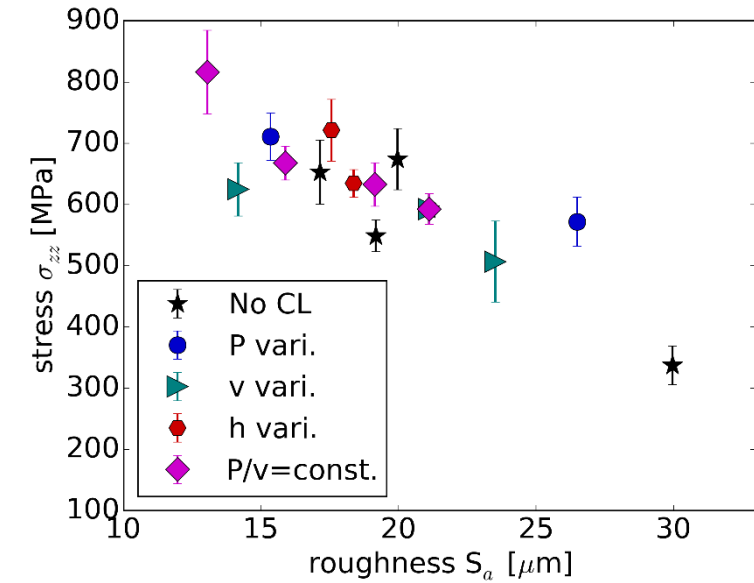
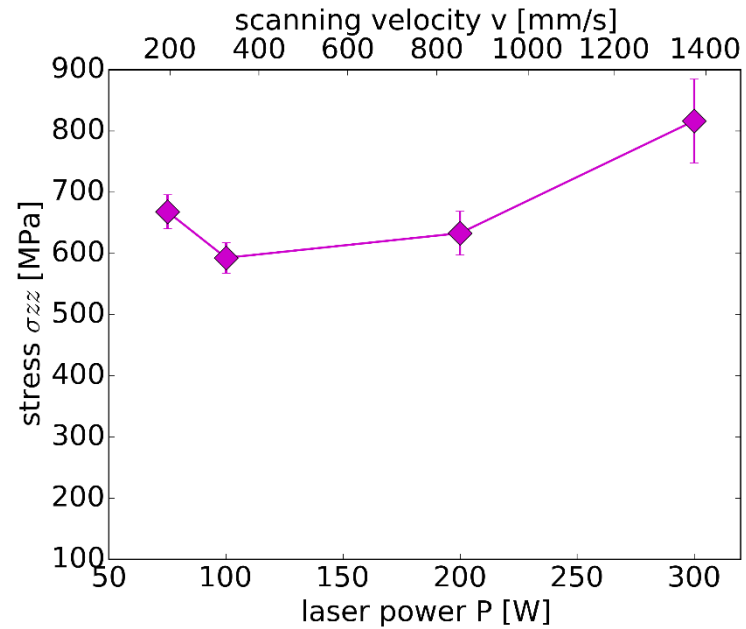
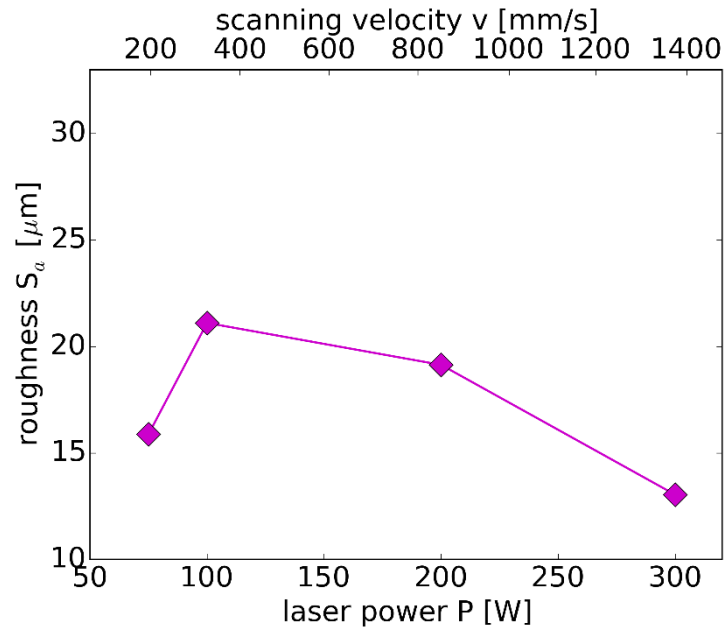
Hatch Variation



- Laser Power: $P \uparrow \Rightarrow S_a \uparrow, \sigma \downarrow$
- Velocity: $v \uparrow \Rightarrow S_a \downarrow, \sigma \uparrow$
- Hatch: $h \uparrow \Rightarrow$ no clear influence

Optimization of Contour Process Parameters

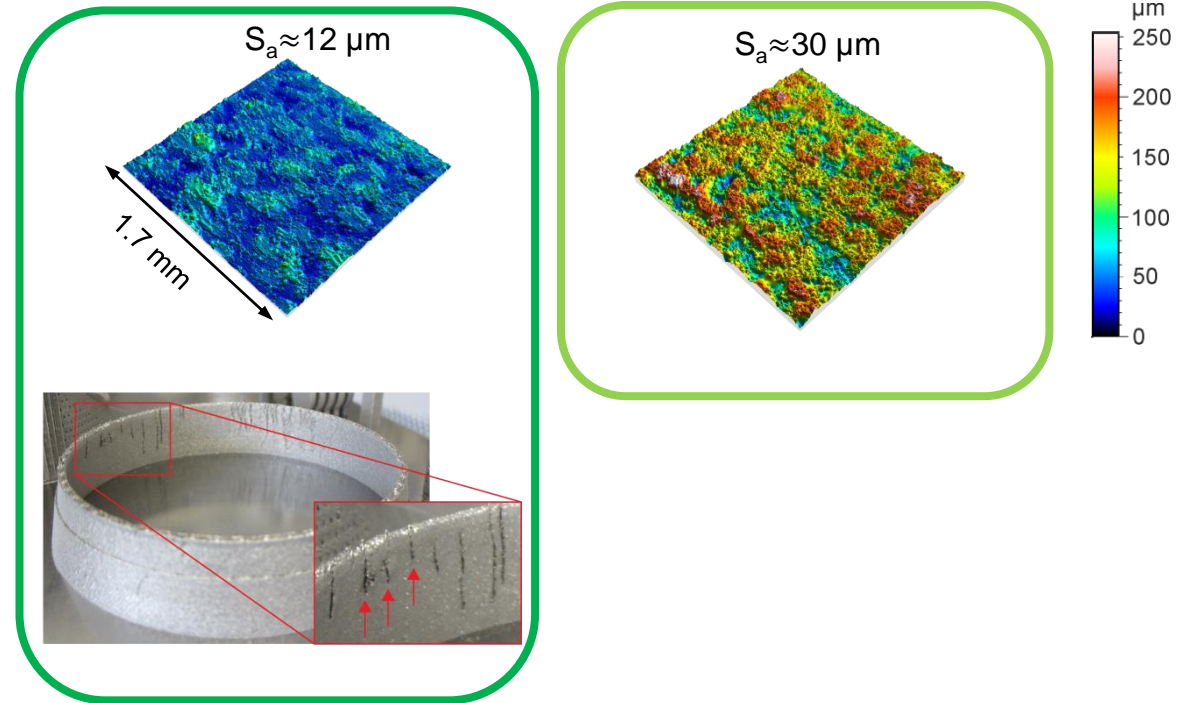
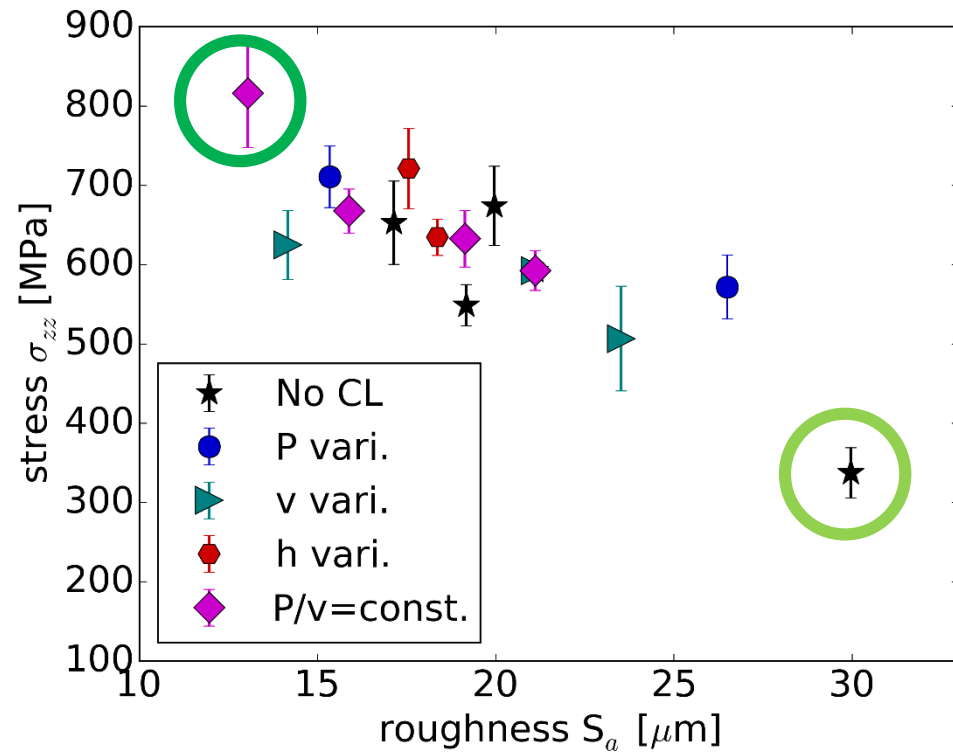
P/v=const.



- Laser Power: $P \uparrow \Rightarrow S_a \uparrow, \sigma \downarrow$
- Velocity: $v \uparrow \Rightarrow S_a \downarrow, \sigma \uparrow$
- Hatch: $h \uparrow \Rightarrow$ no clear influence
- P/v=const: $P+v \uparrow \Rightarrow S_a$ maximum, σ minimum

Optimization of Contour Process Parameters

Correlation between residual stresses and roughness



It is not possible to optimize RS and roughness the same time → compromise necessary

Optimization of Process Parameters

Summary II

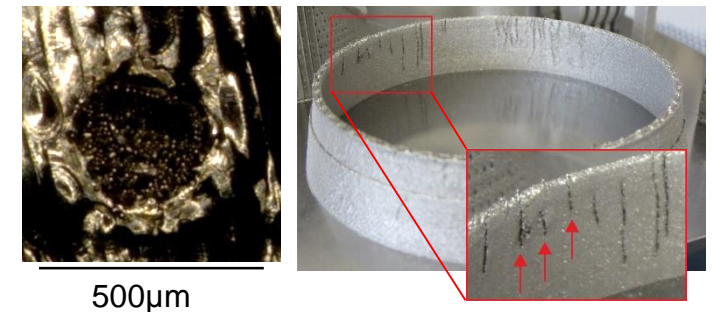
Recommendation – Volume Process Parameters:

- **Hatch distance** ↓ ⇒ **Minimal stresses + porosity** (- higher build time)
- Post-processing: Heat treatment for ductile microstructure
→ solution for the impeller?



Recommendation – Contour Process Parameters:

- Low RS: low velocity, low laser power
- Low surface roughness: high velocity
- ⇒ Residual stresses and surface roughness cannot be simultaneously optimized → compromise needed



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- Residual Stress Measurement – Method
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- Optimization of Contour Process Parameters

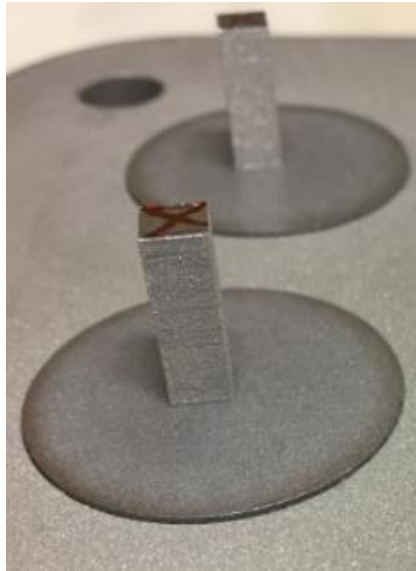
Part II – Outlook: Components (Ti-6Al-4V)

- Transferability: from Coupon to Component



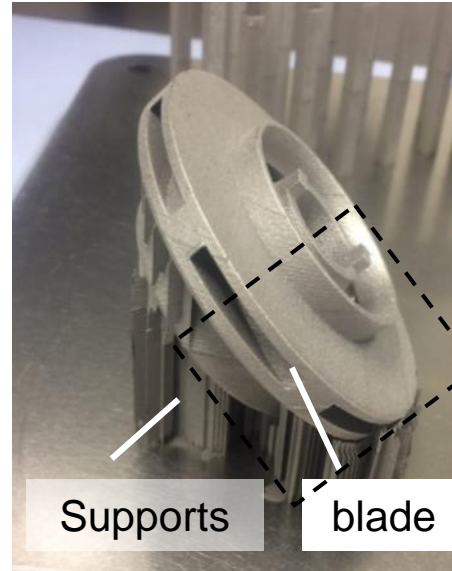
Transferability: from coupon to component

Coupon level



Columnar prior β -grains parallel to building direction

Component



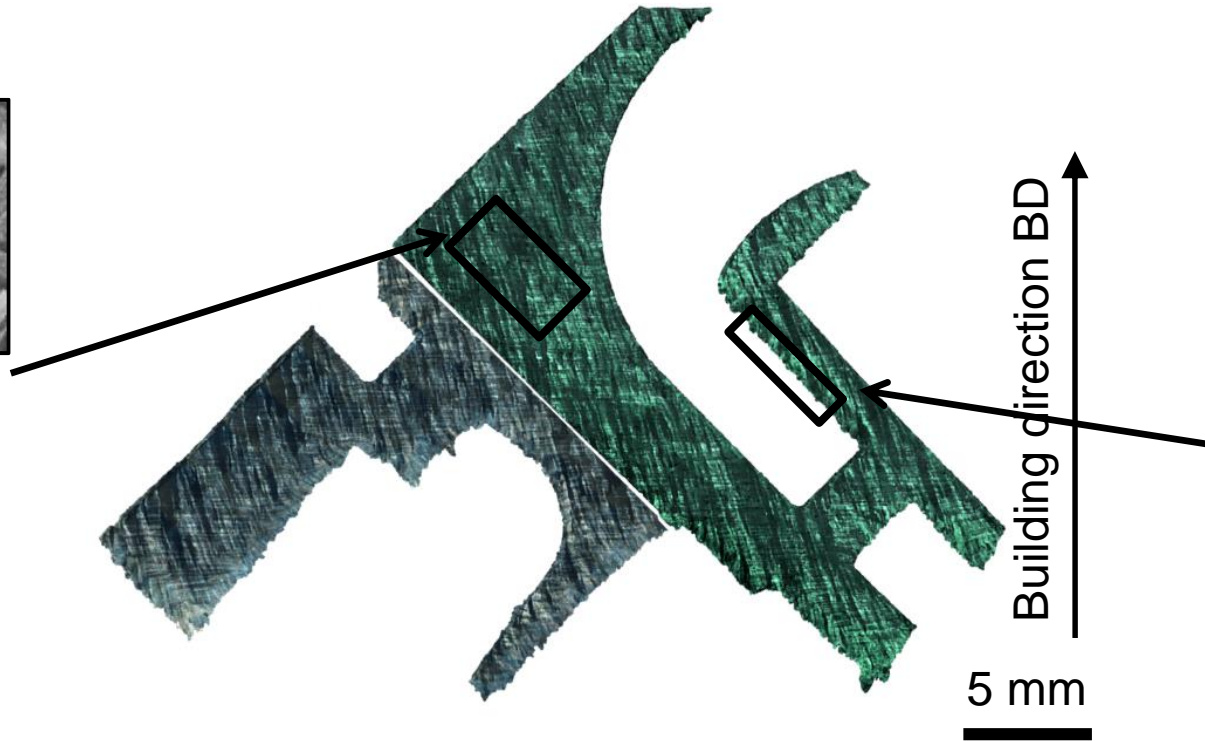
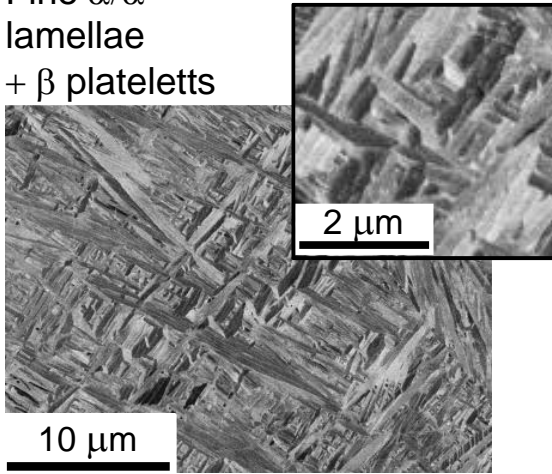
Columnar prior β -grains not parallel to building direction



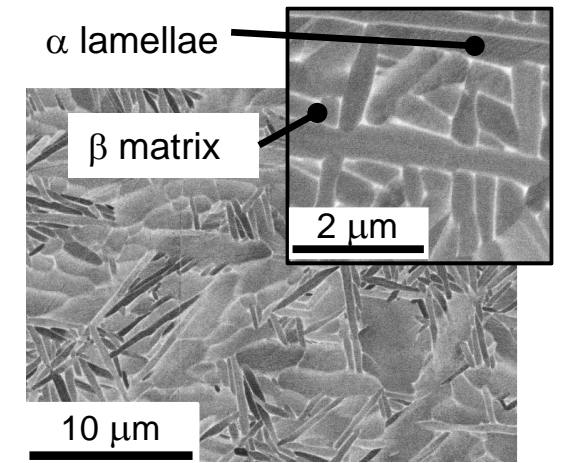
Transferability: from coupon to component

Component bulk:

Fine α/α' lamellae + β plateletts

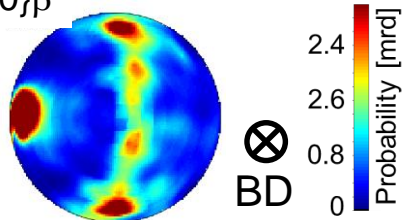


Dowskin regions (<< 1 mm):



Pronounced texture:

$\{200\}_\beta$

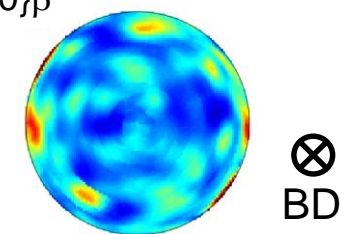


Microstructures and textures different from cuboids with same parameters!

⇒ Strong **geometry influence!**

Less textured:

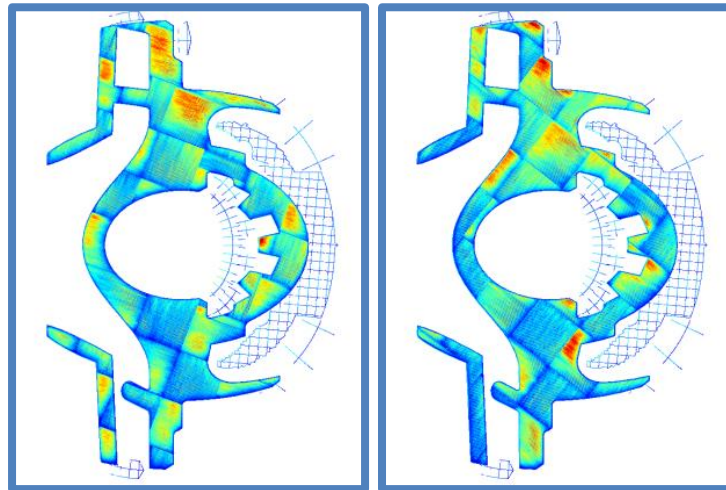
$\{200\}_\beta$



Transferability: from coupon to component

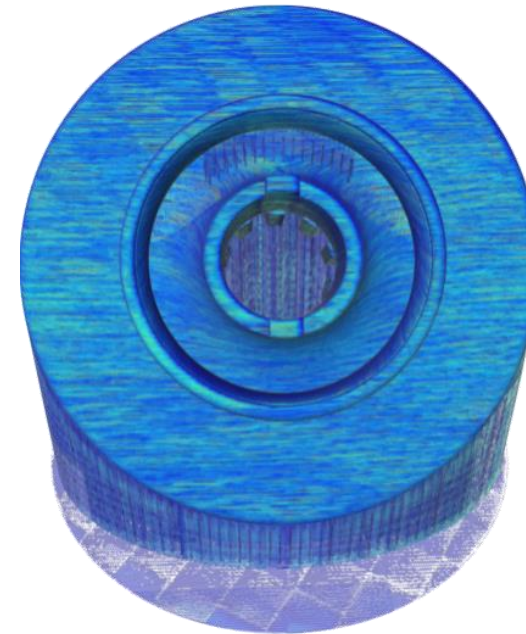
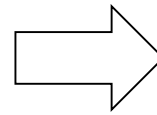
Melt Pool Monitoring (MPM)

- SLM 280^{HL} with Melt Pool Monitoring system (2 photodiodes)
- Layerwise data acquisition of emitted melt pool intensity



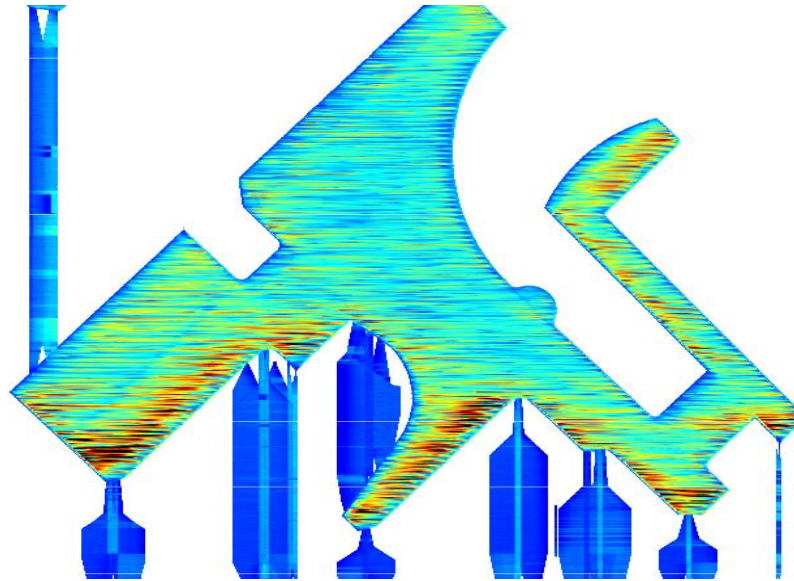
Layer n

Layer n+1

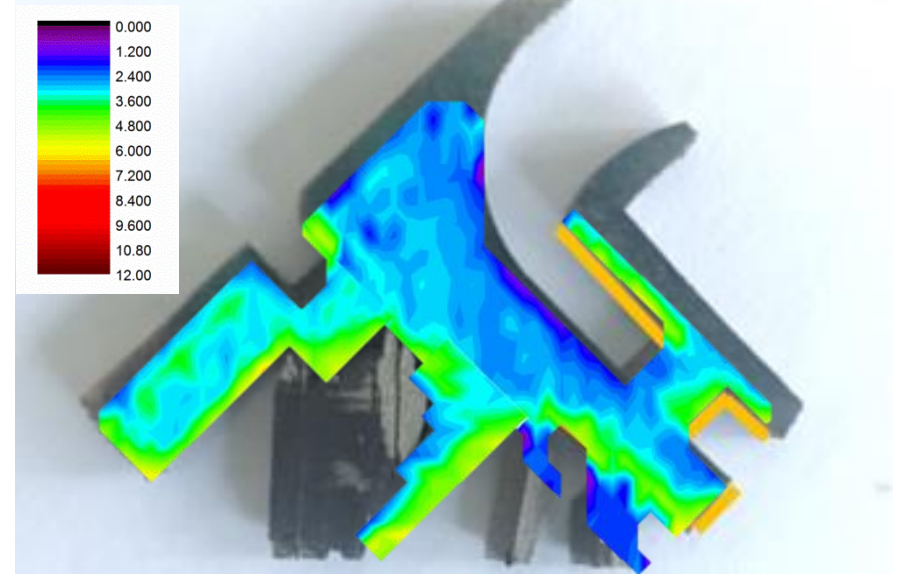


Transferability: from coupon to component

In situ Melt-pool Monitoring (MPM):



HEXRD β -volume fraction [vol.%]:

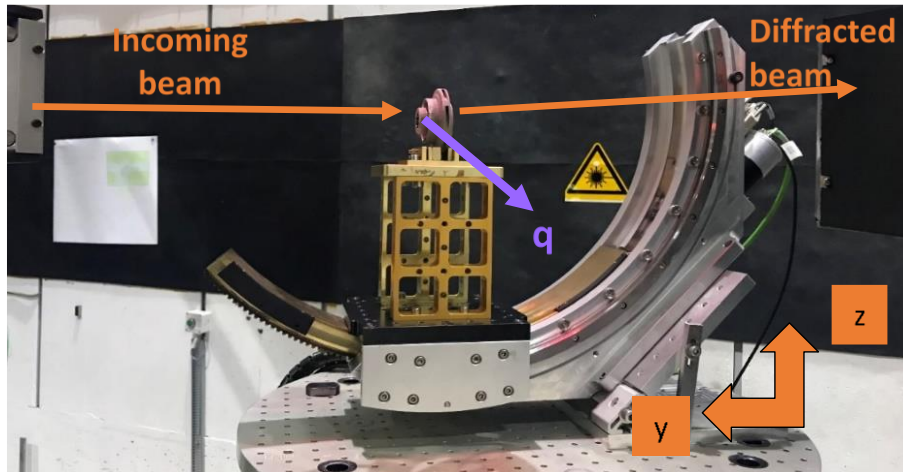


⇒ Strong **geometry influence**

⇒ β -volume fraction is reflected in Melt Pool Monitoring data

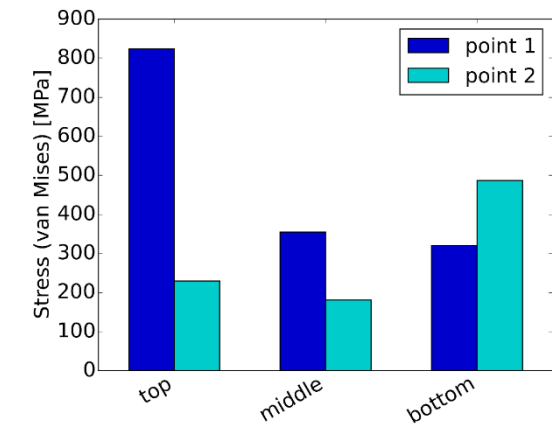
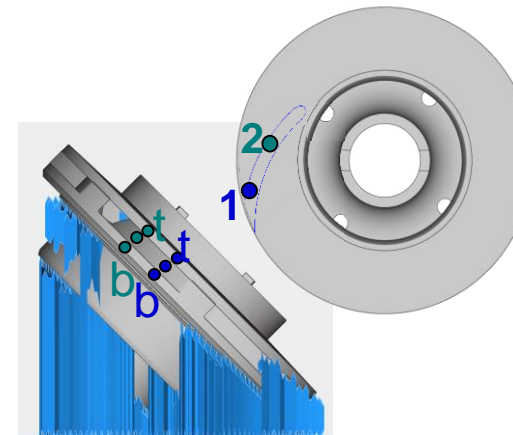
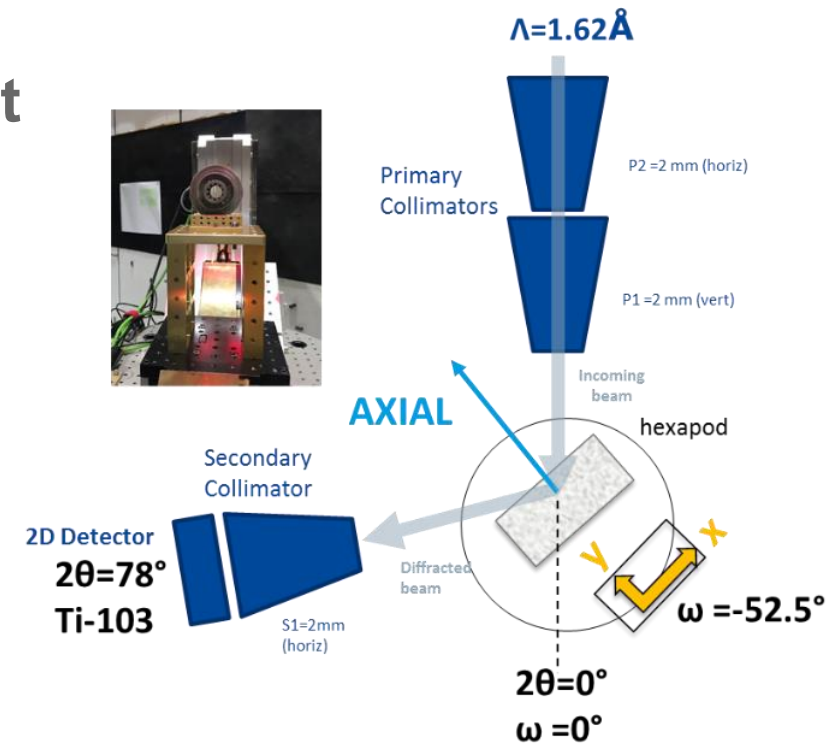
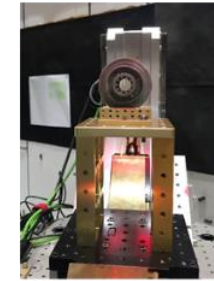
Transferability: from coupon to component

Neutron Diffraction



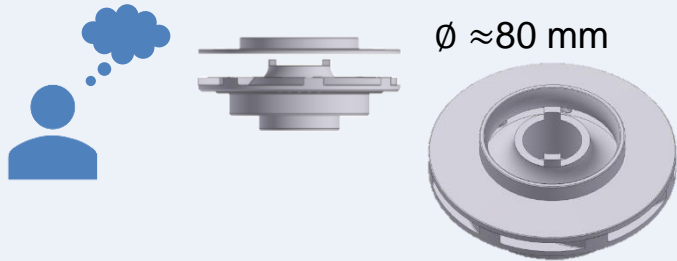
- SALSA strain diffractometer at ILL
- Neutron beam: 1.62\AA (Ti-103 at $2\theta=78^\circ$)
- Full Tensor analysis:
6 different angular conditions i.e. strain components
- LAMP software (ILL) for peak fitting (Gaussian model)
- Unstrained reference measurements

⇒ Complex stress state, further analysis required



Motivation – „easy printing“?!

Rocket Turbo-Pump Impeller*



Idea: printed as a single part



First result:
support cracks, deformation

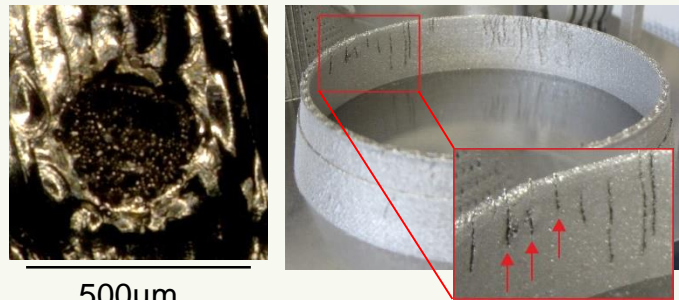


Optimized Result:
burst test - no failure

Injector element**



Idea: small channels
($\varnothing \approx 300\text{-}400\mu\text{m}$)



First result:
blocked channels or cracks



Optimized Result:
successful spray test

Thank you for your attention!!!



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