

Structural Evolution in Iron-Catalyzed Graphitization of Hard Carbons

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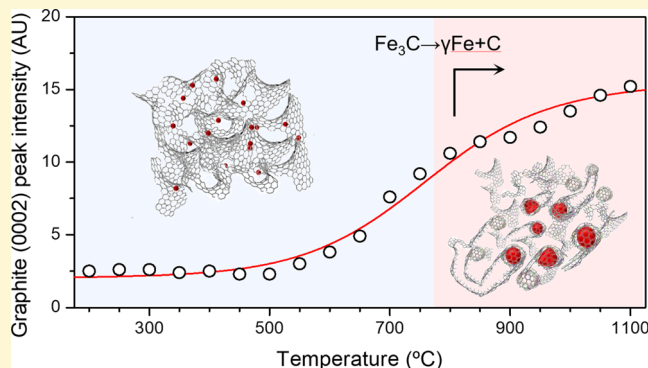


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ABSTRACT: Despite the recent interest in catalytic graphitization to obtain graphite-like materials from hard-carbon sources, many aspects of its mechanism are still poorly unknown. We performed a series of *in situ* experiments to study phase transformations during graphitization of a hard-carbon precursor using an iron catalyst at temperatures up to 1100 °C and *ex situ* total scattering experiments up to 2000 °C to study the structural evolution of the resulting graphitized carbon. Our results show that upon heating and cooling, iron undergoes a series of reductions to form hematite, magnetite, and wüstite before forming a carbide that later decomposes into metallic iron and additional graphite and that the graphitization fraction increases with increasing peak temperature. Structural development with temperature results in decreasing sheet curvature and increased stacking, along with a decrease in turbostratic disorder up to 1600 °C. Higher graphitization temperatures result in larger graphitic domains without further ordering of the graphene sheets. Our results have implications for the synthesis of novel biomass-derived carbon materials with enhanced crystallinity.



1. INTRODUCTION

An effective approach to accelerate the development of graphitic domains in non-graphitizing carbons at moderate temperatures (below 1600 °C) is the use of finely divided catalysts. This so-called *catalytic graphitization* involves the addition of foreign species to the carbon precursor that, upon heating, can induce the precipitation of ordered carbon regions and thus a decrease in the activation energy for crystallization.

The catalytic graphitization process received much attention in the 80s^{1,2} due to the possibility of synthesizing graphite from hard carbons at temperatures far below what was conventionally required (3000 °C) by soft carbons, resulting in significant cost and energy savings. Similar approaches were later used extensively to grow carbon nanotubes (CNTs) by chemical vapor deposition (CVD).³ However, despite the large body of work devoted to employing this method for the synthesis of carbon materials, the mechanisms of catalytic graphitization are still unclear and limited progress has been made in this direction. Currently, the attention is focused on the application of catalytically graphitized carbons in different advanced fields such as electrodes for supercapacitors,^{4–6} anode materials for lithium-ion batteries,⁷ and others^{8,9} owing to their outstanding properties, including enhanced crystallinity¹⁰ and electronic conductivity.¹¹

Among the different catalysts employed, IV–VIII transition metals and especially Fe, Co, and Ni have stood out for their good graphitization efficiency. In this regard, of particular

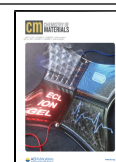
interest are previous studies from Maldonado-Hódar *et al.*,¹² Yan *et al.*,¹³ Thambiliyagodage *et al.*,¹⁴ and Sevilla *et al.*^{15–17} evaluating the graphitization effectiveness of different transition metals with the same concentration on a certain carbon precursor. According to these studies, Fe shows the highest catalytic activity; however, transition metal oxides such as Fe₂O₃ and Fe₃O₄ and alloys such as Fe–Ni and Co–Ni have also proven to be effective catalysts.^{18–20}

In graphitization, the peak heat treatment temperature is a key parameter.^{10,21} From *in situ* XRD experiments from Hoekstra *et al.*,²² the onset of the graphitization by Fe occurs from 715 °C, while Ni and Co require temperatures above 800 °C. From this temperature on, several authors have reported an increase in the degree of graphitization with increasing heat treatment temperature (HTT). Most studies are limited to low treatment temperatures and give no clear correlations between microstructural parameters and HTT,^{23,24} but Ramirez-Rico *et al.*²⁵ reported an increase in the degree of crystallinity using Fe as a catalyst from 27 to 63% as treatment temperature

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increases from 850 to 1600 °C, as calculated from Raman analysis. The increase in crystallinity was more pronounced in the 1100–1400 °C temperature range. A similar trend was also reported by Kakunuri *et al.*,²⁶ showing the largest extent of graphitization occurring between 900 and 1200 °C. So far, there is no clear evidence of a saturation point in the degree of crystallinity obtained from catalytic graphitization at a given catalyst loading.

Several mechanisms have been proposed for catalytic graphitization of carbon/iron mixtures, depending on the temperature range. At temperatures higher than the melting point of pure iron (~1540 °C), graphite is known to form by a “solution-precipitation” mechanism, in which the molten iron becomes supersaturated with carbon that precipitates upon cooling as essentially defect-free graphite, as is the case with the graphite flakes that float on the liquid metal surface in blast furnace iron casting.²⁷ Since catalytic graphitization can take place at much lower temperatures, other mechanisms have been invoked,^{28–30} involving the formation of highly supersaturated liquid droplets of Fe_xC_y.³¹ According to this theory, droplets dissolve amorphous domains from the carbon matrix and precipitate as more ordered graphitic structures due to the associated reduction in free energy. Then, these droplets tunnel through the carbon matrix, as observed in *in situ* TEM experiments⁽²⁹ and the Supporting Information in ref 30), resulting in hollow graphitic tubes or channels.^{15,28,32–35} Surprisingly, these droplets would form at temperatures much lower than the eutectic temperature of Fe–C (~1150 °C) due to size effects and the structure of the amorphous carbon itself.³⁶ In many cases, X-ray diffraction of Fe-graphitized carbon samples reveals the presence of crystalline Fe₃C, whereas other authors report only the presence of metallic Fe (alpha-iron with a bcc structure) after cooling.

In this work, we carry out a series of experiments to shed light on the graphitization mechanism of hard carbon using Fe as a catalyst. First, we perform thermogravimetric (TGA)/differential scanning calorimetry (DSC) measurements of FeCl₃-impregnated biomass pyrolysis while simultaneously monitoring the composition of the released gases by mass spectrometry to precisely determine the onset temperature for graphitization. Then, we perform *in situ* synchrotron and laboratory X-ray diffraction experiments during pyrolysis to monitor the extent of graphitization and the evolution of the chemical state of the Fe catalyst. Finally, we perform total scattering experiments of carbon graphitized at different temperatures to determine the structural evolution of the resulting carbon material as a function of peak pyrolysis temperature by analyzing its pair distribution function.

2. EXPERIMENTAL SECTION

2.1. Sample Preparation. A commercial artificial medium density fiberboard (MDF) was chosen as a representative carbon precursor due to its low cost and homogeneity. As a route to homogeneously deposit fine iron particles into the resulting carbon, we chose to impregnate the biomass directly using an iron chloride solution that decomposes into iron upon heating. Iron-catalyzed graphitized carbon can thus be produced in a single high-temperature process: heating the impregnated precursor results in both the formation of a carbon scaffold and the decomposition of the catalyst precursor into metallic iron that then promotes carbon graphitization at higher temperatures.

In a typical synthesis process, cut and dried MDF wood pieces were impregnated with 1.0 M iron (III) chloride solution (FeCl₃, anhydrous 97% purity, *Panreac*) in isopropanol under vacuum for 2

h to ensure a homogenous impregnation. After impregnation, samples were then dried at 80 °C until complete solvent evaporation and constant weight are obtained. The mass gain was about 7 ± 2% with no external volume change.

Pyrolysis was carried out in a single-step process in a tube furnace under nitrogen flowing at 0.2 L·min⁻¹. Impregnated samples were placed on alumina crucibles and then heated at a rate of 1 °C·min⁻¹ up to 500 °C and then at 5 °C·min⁻¹ up to the desired peak temperature (ranging from 850 to 1600 °C) followed by a holding time of 30 min and then cooled down at 10 °C·min⁻¹ to room temperature. This temperature program was chosen to avoid cracks due to gas release during pyrolysis and to obtain defect-free monoliths. Samples pyrolyzed up to 2000 °C were also obtained in a two-step process: first carbonized up to 1000 °C as described above and then heated up to 2000 °C (5 °C·min⁻¹, holding time 30 min) in a vacuum furnace (LHTG 200-300/30-2G—*Carbolite Gero GmbH & Co. KG*) under flowing argon. After pyrolysis, remaining Fe particles were removed by stirring in concentrated HNO₃ (69%, *Panreac*) followed by washing in deionized water until neutral pH.

2.2. Thermogravimetric Analysis Coupled with Mass Spectrometry. The thermal behavior of raw precursors during pyrolysis processes was characterized by thermogravimetric analysis (TGA) and differential scanning calorimetry (DSC) experiments, in which the weight and heat flow changes are measured *versus* a reference as a function of temperature. All measurements were carried out using a dual system (SDT Q-600, *TA Instruments*) between room temperature and 1000 °C at a heating rate of 10 °C·min⁻¹ under a constant nitrogen flow rate of 100 mL·min⁻¹. The instrument was coupled to a mass spectrometer (GSD 320 OmniStar, *Pfeiffer*) to evaluate the composition of evolved gases during pyrolysis. Mass/charge ratios between 10 and 50 u.m.a were considered, with a scan rate of 200 ms·(u.m.a)⁻¹ and a secondary electron multiplier detector working at a voltage of 970 V.

2.3. In Situ X-ray Diffraction during Graphitization. The graphitization reaction was followed *in situ* using X-ray diffraction in the Material Science Powder Diffraction (MSPD) beamline of the ALBA-CELLS synchrotron (Cerdanyola del Vallés, Spain). Beam energy was 30 keV (wavelength $\lambda = 0.4133$ Å as confirmed using a Si standard) and scattering was measured up to $2\theta = 60^\circ$ using an array of position-sensitive detectors (*Dectris Mythen*). Samples were contained in sealed quartz capillaries of 0.7 mm diameter. Since the release of volatiles during pyrolysis could break the containing capillaries, samples were prepared in a two-step process: MDF pieces were first carbonized to 1000 °C without any catalyst, as described in the previous section, and the obtained carbon pieces were then impregnated with 1 M FeCl₃ solution in isopropanol as explained before. This powder was then ground and sealed under vacuum in quartz capillaries for diffraction experiments. Diffraction patterns were obtained isothermally as a function of temperature in 50 °C increments from 300 to 800 °C and then back to 300 °C. The sample was heated using a hot-air blower, using a heating rate of 50 °C/min between isotherms.

Since the maximum temperature reached at the MSPD beamline was 800 °C, we carried out additional experiments at higher temperatures using a laboratory X-ray diffractometer equipped with a high-temperature reaction chamber (D8 Discover with a HIGH-temp furnace chamber, *Bruker*). The same sample was used in this case but under flowing nitrogen and at temperatures between 300 and 1100 °C. Additional details can be found in the [Supporting Information](#).

2.4. Total Scattering Experiments. Total scattering experiments were performed at the MSPD beamline using the same conditions as described above. In this case, data were collected up to $2\theta = 120^\circ$, resulting in a usable scattering vector range of $Q \sim 0.5\text{--}25$ Å⁻¹. The measurement time was 45 min per sample. Powdered graphitized carbon samples free of residual iron were contained in 0.7 mm polyimide tubes; an empty tube was also measured, and its background scattering signal was subtracted from the data. The pair distribution function (PDF) of each sample was calculated by Fourier transforming the coherently scattered signal using an *ad hoc*

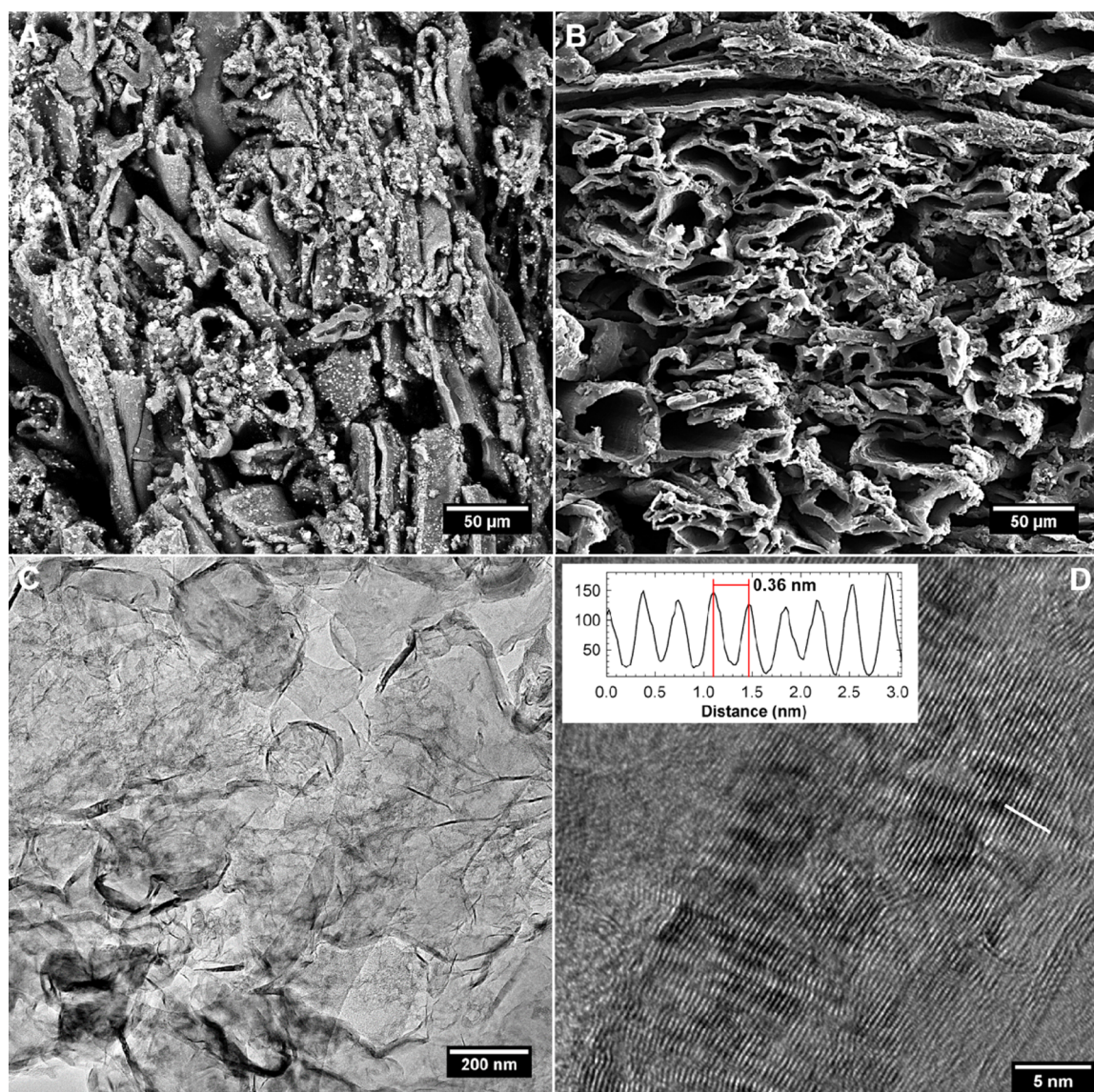


Figure 1. (A) Scanning electron micrograph of pyrolyzed, FeCl₃-impregnated medium density fiberboard. (B) Fe-catalyzed carbon derived from MDF-pyrolysis, after removal of Fe particles. (C) Transmission electron micrograph of Fe-graphitized carbon processed at 1600 °C and (D) high-resolution TEM micrograph showing detailed (002) lattice fringes of ordered graphitic regions.

polynomial correction as implemented in PDFGetX3 software.³⁷ Further analysis of the obtained PDFs was performed using PDFGui.³⁸

3. RESULTS AND DISCUSSION

3.1. Electron Microscopy. The microstructure of Fe-graphitized carbon from the pyrolysis of the MDF is shown in Figure 1. The structure of the original wood precursor, made of hollow, pressed cellulose fibers, is maintained after graphitization. The obtained carbon material is decorated with Fe nanoparticles (panel A) that are removed after etching with concentrated HNO₃ (panel B). The weight content of Fe within the carbon was ~11% after graphitization and below 0.5% after acid etching, as measured using ICP-OES. Under a transmission electron microscope (panel C), flat ordered regions are observed and so are hollow carbon spheres, as has been reported previously for this material.²¹ The high-resolution micrograph of panel D confirms the appearance of a graphitic structure. A line profile across stacked graphene layers allows us to estimate the interplanar distance between

layers as (0.36 ± 0.01) nm, slightly larger than the theoretical interplanar spacing of graphite (0.336 nm, ICDD card 41-1487).

3.2. TGA and Mass Spectroscopy Analysis. Thermogravimetric and differential scanning calorimetry analyses coupled with mass spectrometry were carried out to study the thermal behavior of catalyzed/non-catalyzed MDF samples and evolved gases while heating under flowing nitrogen. Furthermore, FeCl₃ powders were also characterized for comparison purposes. Figure 2 shows TGA and DSC analysis under an inert atmosphere of the raw MDF precursor without a catalyst (a), FeCl₃ powder (c), and MDF impregnated with 1.0 M FeCl₃ solution (e). Right panels in Figure 2 (b,d,f) show associated mass spectrometry representation (treatment temperature vs mass/charge ratio) where the signal intensity is represented in log units, indicating the evolution of gas products during thermal decomposition. A constant background signal on the mass spectrum due to nitrogen ($m/z = 14, 28, 29$ a.m.u), water vapor ($m/z = 18$ a.m.u), oxygen ($m/z =$

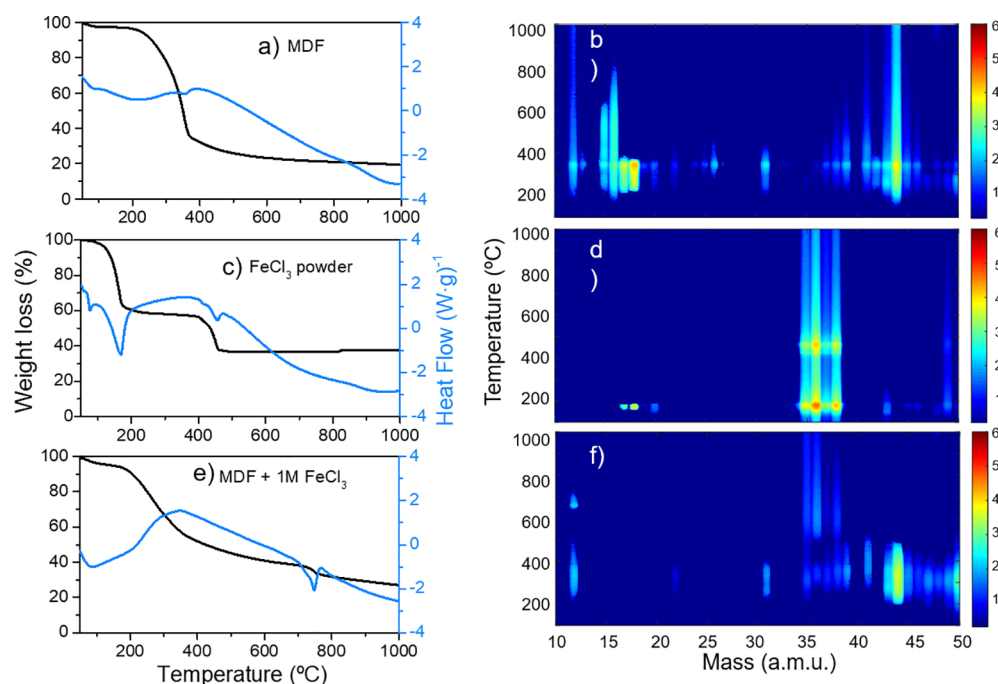


Figure 2. TGA and DSC analysis along with mass spectrum of evolved gases (treatment temperature *vs* mass/charge ratio) of a raw MDF (a,b), FeCl₃ powder (c,d), and MDF impregnated with 1.0 M FeCl₃ solution (e,f) heating at 10 °C·min⁻¹ under an inert atmosphere. Normalized mass spectra are represented as a function of pyrolysis temperature for different mass values in terms of the logarithm of the ion current in arbitrary units.

= 16, 32 a.m.u), and carbon dioxide ($m/z = 44$ a.m.u) from the vacuum chamber and sealing was subtracted from the data.

The raw MDF precursor (Figure 2a,b) exhibits two main weight loss stages in the TGA curve. The first one, which takes place at temperatures below 200 °C, corresponds to the water desorption, while the second stage between 250 and 500 °C is due to the thermal decomposition of polysaccharide chains and breakdown of C–O, C–C, and C–H bonds, leaving a solid carbon template of about 20–25% of the original weight precursor at temperatures above 600–700 °C. Most evolved gases are released in the same temperature range, between 200 and 500 °C. The main evolved gases upon pyrolysis are⁴ CO₂ ($m/z = 12, 22, 44$ a.m.u), CO ($m/z = 12, 14, 28$), O₂ ($m/z = 16, 32$ a.m.u), and H₂O ($m/z = 16, 17, 18, 32$ a.m.u) and signals from hydrocarbons such as CH₄, C₂H₄, and C₂H₆ (at $m/z = 12–16, 24–27, 38–44$ a.m.u).³⁹ From the DSC curves (blue color), the pyrolysis process is mainly endothermic, as energy is required to break the polysaccharide chains.

FeCl₃ powder (Figure 2c,d) decomposes in two stages until reaching 460 °C.⁴⁰ These two stages are attributed to the loss of chlorine (as confirmed by the mass spectrum and the increased ion current at $m/z = 35–38$ a.m.u) due to the decomposition of FeCl₃, leaving behind a 35 wt % of remaining Fe. At 150 °C, the release of adsorbed water ($m/z = 16–18$ a.m.u) is also observed. Reference work indicates that hydrated FeCl₃ decomposes in the 200–500 °C range to produce iron oxide or hydroxide species^{41–43} due to the decomposition of (1) FeCl₃ \rightleftharpoons FeCl₂ + 1/2Cl₂ (~200 °C) and then (2) FeCl₂ \rightleftharpoons Fe + Cl₂ (460 °C), leaving behind 35 wt % of remaining Fe, similar to our observations. It is therefore reasonable to assume that the loss of chlorine indicates decomposition of the FeCl₃ precursor to produce the catalyst precursor nanoparticles in our system.

The MDF impregnated with 1.0 M FeCl₃ solution (Figure 2e,f) exhibits a similar behavior during pyrolysis to that of the

raw MDF but shows a narrower main weight loss of the cellulosic-based precursor at temperatures ranging between 200 and 500 °C, as seen in the mass spectra. The thermal decomposition of the catalytic agent is detected by the release of chlorine ($m/z = 35–38$ a.m.u; Figures 2f and 3a) that occurs over a wider temperature range (with peak rates at 337 and 600 °C) when compared to FeCl₃ powder (with maximum rate decomposition at 177 and 462 °C; Figure 3b) upon heat treatment. At 700–750 °C, we observe an additional weight loss and an endothermic peak on the heat flow curve, which can be attributed to the carbothermic reduction of iron oxide and subsequent formation of iron carbide (Figure 2e). This can be correlated with the release of CO₂ species ($m/z = 44$ a.m.u; Figures 2f and 3c) that does not occur on the raw MDF without a catalyst (Figure 3d).

3.3. In Situ XRD Experiments. Figure 4a shows scattered intensity from synchrotron X-ray diffraction experiments as a function of the temperature and diffraction angle recorded *in situ* during heating of a carbon sample impregnated with FeCl₃ up to 800 °C, whereas Figure 4b shows selected diffraction patterns at specific temperatures with marks corresponding to the main observed reflections. At 300 °C, a shoulder or bump at $2\theta \sim 6^\circ$ ($\lambda = 0.4134$ Å) related to amorphous carbon areas can be observed, along with diffraction reflections of hematite (Fe₂O₃—ICDD card 39-1346), which is consistent with the thermal decomposition of FeCl₃ in air at this temperature.⁴⁴ Fe₂O₃ reflections are observed upon heating up to 400 °C, at which point it transforms into magnetite (Fe₃O₄; ICDD card 76-0955). A further increase in the treatment temperature up to 700 °C subsequently transforms Fe₃O₄ into wüstite (FeO; ICDD card 03-0968), which finally undergoes carbothermic reduction to form an intermediate carbide, cementite (Fe₃C; ICDD card 35-0772). At 750 °C, the apparition of a broad asymmetric peak at $2\theta \sim 7^\circ$ indicates the presence of graphite—(002) reflection and thus the onset of graphitization. This

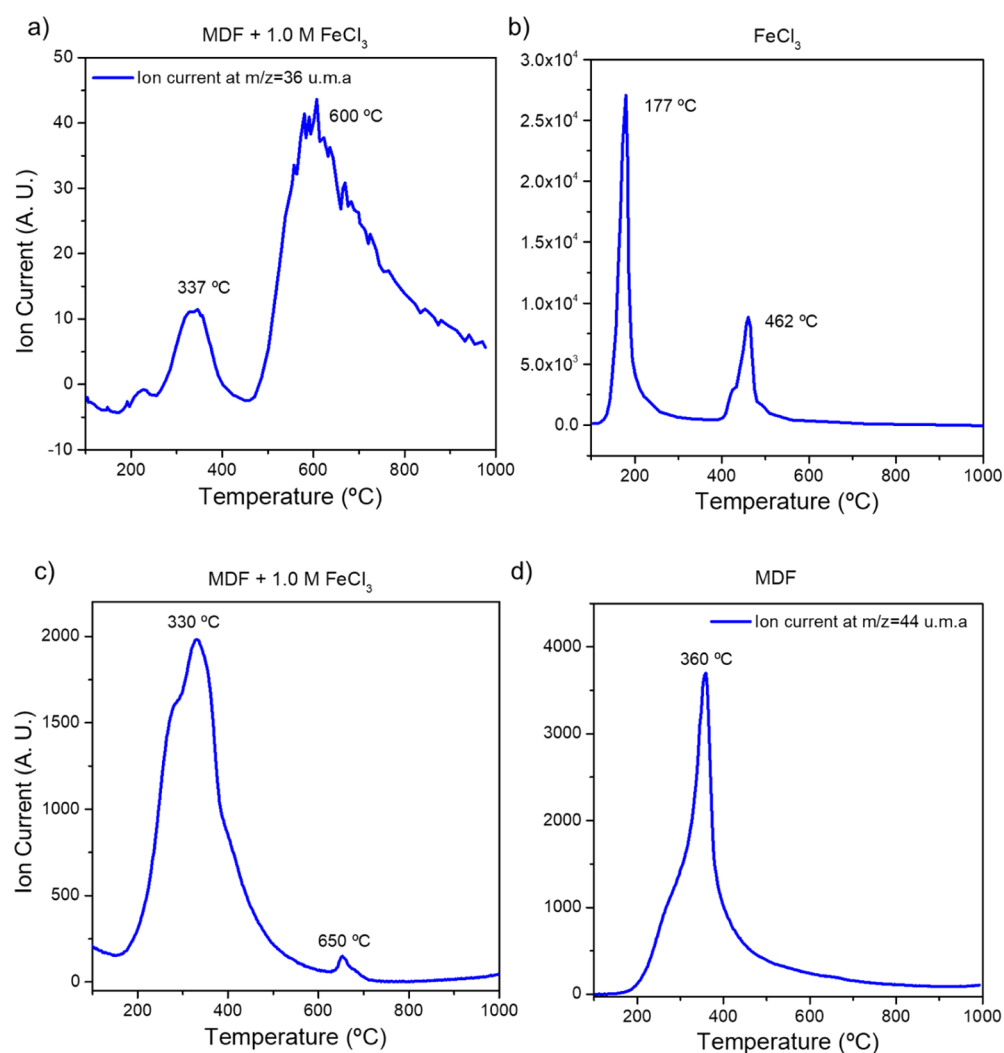


Figure 3. Mass spectra. Top panels: ion current signal vs treatment temperature at $m/z = 36$ u.m.a related to evolved Cl_2 gases for (a) MDF impregnated with 1.0 M FeCl_3 and (b) FeCl_3 powder. Bottom panels: ion current signal vs treatment temperature at $m/z = 44$ u.m.a related to evolved CO_2 gases for (c) MDF impregnated with 1.0 M FeCl_3 and (d) MDF without Fe.

phase reflects the uptake of carbon into iron oxide nanoparticles and reaches its maximum intensity at 800 °C. At 800 °C, Fe_3C and fcc iron phases ($\gamma\text{-Fe}$; ICDD card 52-0512) coexist. As the sample is cooled down, the Fe_3C phase decomposes into $\gamma\text{-Fe}$, which then transforms at 700 °C (close to the theoretical transformation temperature, 727 °C) into ferrite ($\alpha\text{-Fe}$; ICDD card 06-0696).⁴⁵ After cooling down to room temperature, the only large reflections apart from those of graphite correspond to $\alpha\text{-Fe}$. More details about the phase composition as a function of temperature as determined from Rietveld refinement can be found in the [Supporting Information](#) (Figures S1–S5).

To reach higher temperatures, we used a laboratory diffractometer equipped with a high-temperature chamber and carried out experiments between 300 and 1100 °C. Most important results are shown in [Figure 5](#) (full results in the [Supporting Information](#)). At 750 °C, a mixture of Fe_3C and metallic $\gamma\text{-Fe}$ (fcc) is observed, in agreement with synchrotron XRD data. Upon further heating, the carbide decomposes and only metallic $\gamma\text{-Fe}$ is observed, apart from some small peaks due to the alumina sample holder ([Figure 5a](#)). The intensity of the (002) reflection of graphite monotonically increases with

the temperature up to 1100 °C ([Figure 5b](#)), even though cementite decomposition starts at ~ 800 °C.

3.4. Total Scattering Experiments and Pair Distribution Function Analysis. Diffraction measurements up to $Q \sim 0.5\text{--}25 \text{ \AA}^{-1}$ were performed on carbon samples graphitized at temperatures from 850 to 2000 °C, after the removal of Fe, as described in the material section. [Figure 6](#) shows the normalized scattering factors (related to the diffracted intensity) as a function of Q , zooming into the $1.6\text{--}2.2 \text{ \AA}^{-1}$ region (panel a), where the (002) peak from graphite is located. A qualitative assessment of these data reveals an increased crystallinity with increasing graphitization temperature, as evidenced by the sharpening of the diffraction peaks. Fourier transforming these data allowed us to calculate and further analyze the pair distribution function (PDF) to extract information on the degree of structural development of biomass-derived carbon upon graphitization using the Fe catalyst.

The PDF is a very powerful tool for the study of materials that show limited crystallinity and only local ordering,⁴⁶ especially for carbon materials. One of the earliest examples is from R. Franklin,^{47,48} who studied the structural differences between graphitizable and non-graphitizable carbon from

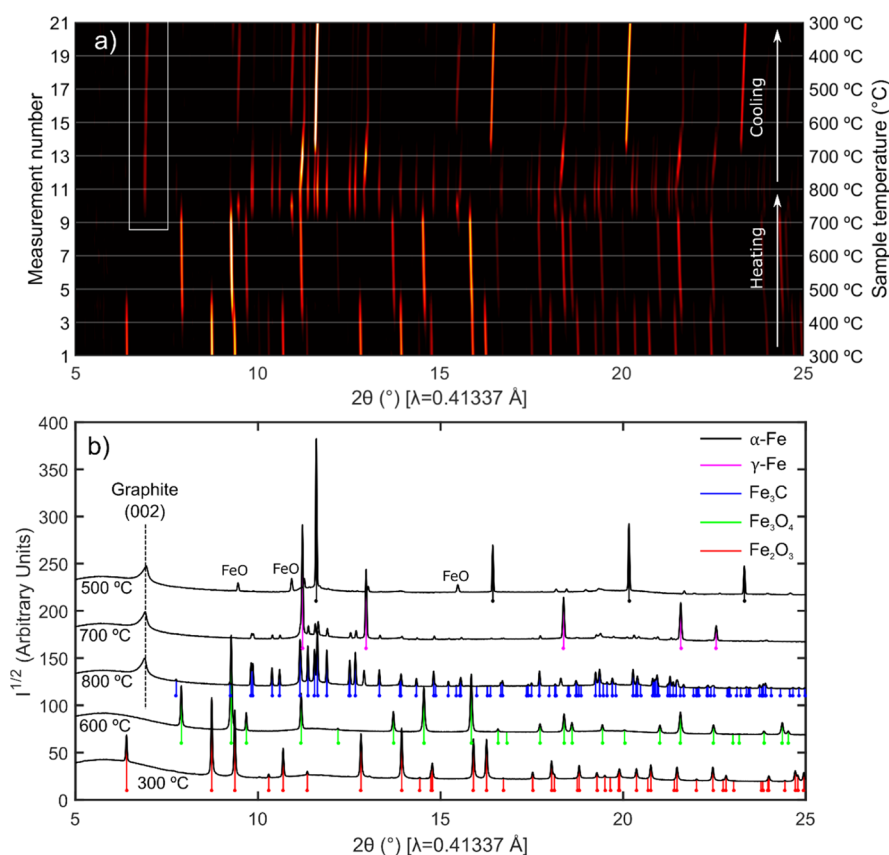


Figure 4. Graphitization measured *in situ* using synchrotron X-ray diffraction. (A) Two-dimensional plot showing diffracted intensity as a function of temperature and scattering angle 2θ . In this experiment, the temperature first rises from 300 to 800 °C (measurements 1–11) and then decreases back to 300 °C (measurements 12–21). The (002) reflection from graphite is marked with a white line. (B) Line plots of diffracted intensity as a function of angle 2θ for selected temperatures, along with the position of reflections of the crystalline phases identified at each temperature. The formation of graphitic regions results in the appearance of an asymmetric peak at a position close to the (002) reflection of graphite (marked with a dashed line).

different polymeric precursors. Several applications of the PDF to the study of carbon obtained by pyrolysis^{49,50} and other turbostratic layered materials can be found in the literature.⁵¹

The PDF contains information regarding the interatomic distances in a solid, irrespectively of its crystalline or amorphous character. For X-rays, it is defined as

$$G(r) = \frac{1}{r} \sum_{ij} \frac{b_i b_j}{b^2} \delta(r - r_{ij}) - 4\pi\rho_0 \quad (1)$$

where r_{ij} represents the interatomic distance between atoms i and j and b_i is the scattering length of atom i and ρ_0 is the average atomic density. It can be computed from the scattered intensity $S(Q)$ of a powdered (isotropic) material by means of the following relationship

$$G(r) = \frac{2}{\pi} \int_0^\infty Q[S(Q) - 1] \sin(Qr) dQ \\ \approx \frac{2}{\pi} \int_{Q_{\min}}^{Q_{\max}} Q[S(Q) - 1] \sin(Qr) dQ \quad (2)$$

with Q being the modulus of the scattering vector. Since the available Q -range is limited in any diffractometer, the obtained function approximates the real one due to truncation effects. In the PDF, each atomic pair distance manifests as a peak that is centered on the average distance and has a finite width since interatomic distances may vary due to at least atomic thermal

motion. For very crystalline materials, the PDF oscillates around zero and exhibits peaks up to very large interatomic distances (>100 Å), its range being limited only by the diffractometer angular resolution. In nanomaterials or materials with limited long-range ordering, the amplitude of the PDF decays with increasing interatomic distances, and this decay allows for estimation of the crystalline domain or crystallite size.

Further insight into the atomic ordering from the analysis of PDFs requires a structural model that can be fitted to the observed data, from which structural parameters can be refined. Although several approaches exist, we have performed the so-called *small-box* modeling using the crystalline structure of graphite as a starting point. This approach has been successfully employed in the past to study hard carbons and starts by postulating a crystalline structure that contains the basic short-range atomic unit (hexagonal carbon rings in this case) and smoothing out the long-range correlations by introducing *long-range* disorder. We introduce this disorder through anisotropic *atomic displacement parameters* (ADPs), which are allowed to take unphysical values describing *static* disorder, as opposed to thermal motion.⁴⁹ In our analysis, we refined the lattice parameters a and c and anisotropic displacement parameters U_{ii} and an average crystallite size and a global scale factor.⁵² To maintain consistency with the in-plane symmetry of the graphene layers, we fixed $U_{22} = U_{11}$

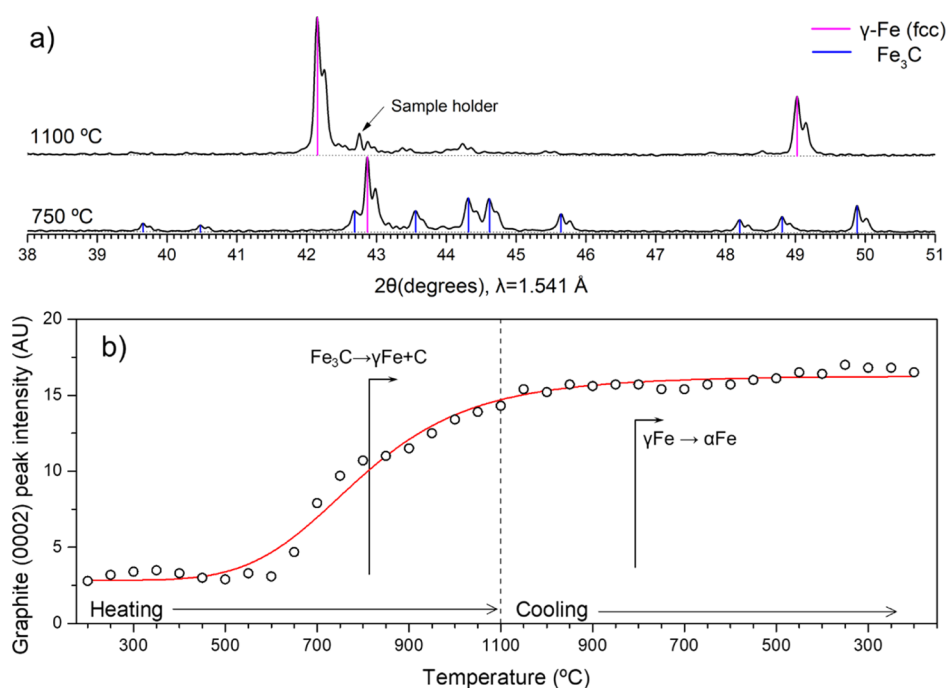


Figure 5. (a) High-temperature diffraction experiments in a laboratory diffractometer. The bottom diffraction pattern was obtained at 750 °C and shows reflections from both Fe_3C and metallic $\gamma\text{-Fe}$. Upon further heating, the carbide decomposes, leaving only metallic $\gamma\text{-Fe}$ at 1100 °C (upper diffraction pattern). (b) Evolution of the (002) reflection intensity of graphite as a function of temperature (laboratory diffractometer). The temperatures at which the cementite decomposition and the fcc-to-bcc transformation of iron are observed are marked. The red line is only included as a visual aid and does not imply any particular model to fit the data.

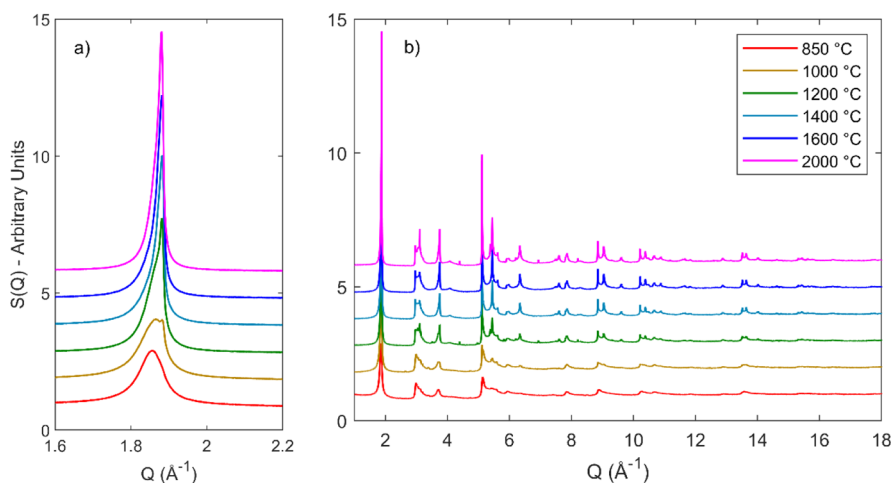


Figure 6. Normalized scattering factor for the Fe-graphitized MDF at different carbonization temperatures. Panel A shows a magnified view of the region containing the reflection from the (002) planes in graphite.

and $U_{12} = 1/2 U_{11}$ and independently refined U_{11} and U_{33} to probe both in-plane and out-of-plane disorder in the structure.

The observed PDFs along with the fitting to the calculated PDFs from the refined structural model and the difference between the two are shown in Figure 7a,b for carbons obtained at 850 and 2000 °C. In all cases, the number of fitting parameters was restricted to six (a , c , U_{11} , U_{33} , crystallite size, and a global scale factor) and refinement was performed in the range 0.5–20 Å for r . Agreement factors R_w were generally below 20%.^b While this number might appear high when compared to typical R_{wp} values attainable in Rietveld refinements, goodness-of-fit metrics cannot be directly compared between the two methods, and R_{ws} greater than 15% are common in real-space refinements of well-crystallized

materials.⁵¹ In general, a good correspondence between measured data and the model PDF could be obtained, as can be seen from the fits. The parameters from the refinements are shown as a function of graphitization temperature in Figure 7c–f.

Evolution of the calculated lattice parameters of the average disordered structure evidence a progressive enhancement of crystallinity with increasing graphitization temperature. By looking at the parameter a (Figure 7c), which is related to the average *in-plane* interatomic distances in the structural graphene unit, we see that at temperatures in the range 850–1200 °C, calculated lattice parameters are lower than those of ideal graphite ($a = 2.461$ Å, marked with a dashed horizontal line in panel c), which is indicative of sheet

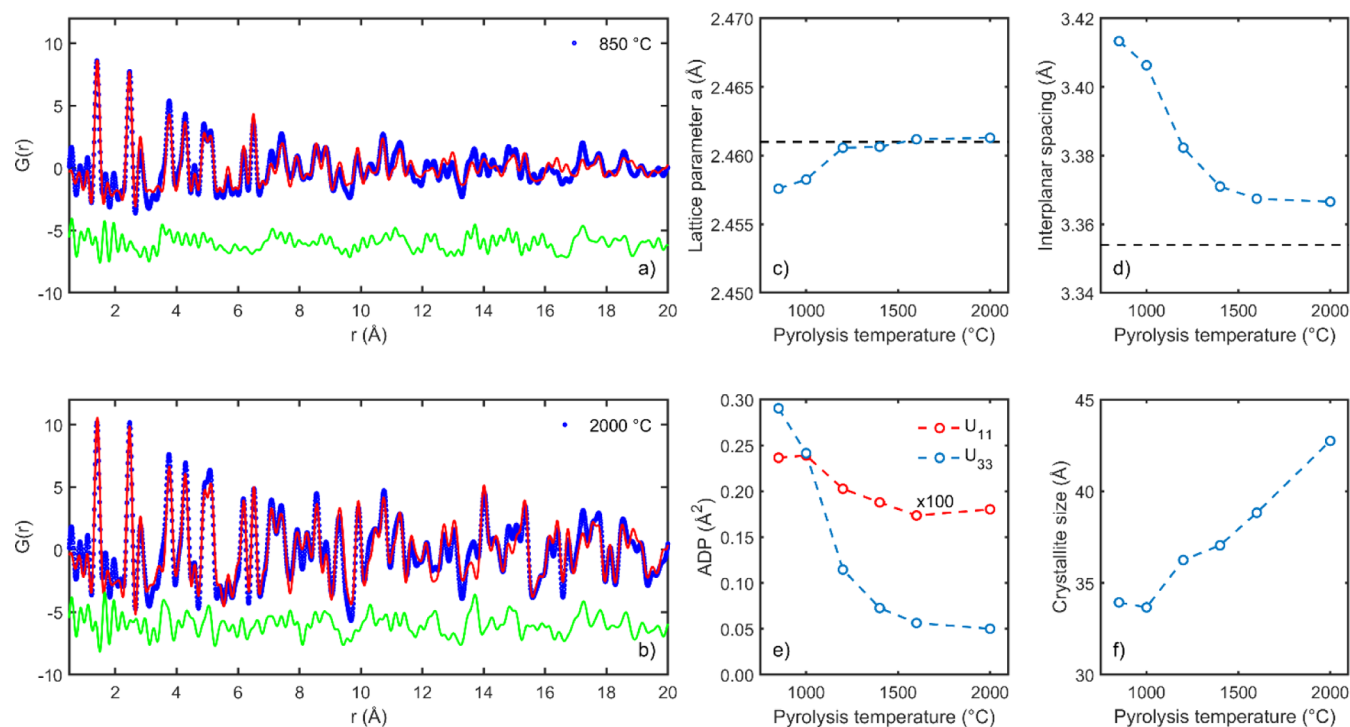


Figure 7. (a,b) Observed PDF (blue circles), fitted profile (red line), and difference (green line) for graphitized carbon at 850 °C (panel a) and 2000 °C (panel b). (c,d) Lattice parameter a and interplanar spacing ($c/2$) obtained from fitting the observed PDFs to a disordered graphite structure, as a function of temperature. Dashed black lines show the theoretical values for graphite. (e) In-plane (U_{11}) and out-of-plane (U_{33}) atomic displacement parameters from the fit as a function of temperature. Note that U_{11} is multiplied by a factor of 100. (f) Crystallite size as a function of temperature.

curvature in the stacked graphene layers.⁵³ However, the value of the lattice parameters progressively increases and reaches the theoretical value at a pyrolysis temperature of 1400 °C and remains virtually constant thereon, suggesting that increasing pyrolysis temperature decreases sheet curvature as graphene layers become planar and stacked on top of each other. The importance of the peak pyrolysis temperature can also be seen in the evolution of the interlayer or interplanar spacing between graphene sheets (theoretical value for graphite is $1/2c = 3.354$ Å, again marked with a dashed line) shown in Figure 7d. The interplanar spacing progressively decreases with increasing pyrolysis temperature until reaching a constant value of 3.36 Å for temperatures above 1400 °C.

Further evidence on this increased ordering is observed in the evolution of ADPs with increasing graphitization temperatures. The values of U_{11} (Figure 7e), related to *in-plane* disorder, progressively decrease up to 1400 °C and thereon become constant, reaching 1.8×10^{-3} Å², a value that is physically compatible with thermal motion. Similarly, the values of U_{33} decrease with the temperature up to 1600 °C as well due to the rapprochement between graphene layers and reach about 0.05 Å², a value that is 2 orders of magnitude larger than U_{11} and can be interpreted in terms of turbostratic disorder.

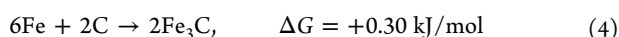
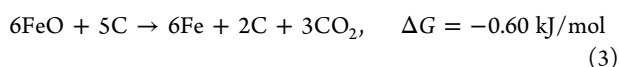
3.5. Graphitization Mechanism. It is then clear from the results that the extent of graphitization in hard carbon using Fe as a catalyst is mainly determined by the peak reaction temperature. Previous studies showed this dependence using other techniques such as Raman spectroscopy and the corresponding decreased intensity ratio between D_1 and G bands when increasing the pyrolysis temperature.^{7,21} Several authors attribute the graphitization to the initial formation of

an iron carbide phase that continuously forms and decomposes into ordered graphitic carbon. According to these studies, the formation of Fe_3C is responsible for graphitization, and the fact that only metallic Fe is observed on samples graphitized at temperatures above 1000 °C is explained by decomposition of the carbide into Fe and C upon cooling.^{29,31} Our *in situ* observations partially support this theory but also give additional insight into the process, which can be summarized as follows:

- 1 At temperatures below ~ 700 °C, Fe resulting from the thermal decomposition of $FeCl_3$ goes through several oxidation states as it is progressively reduced from Fe_2O_3 to Fe_3O_4 and finally to FeO at ~ 700 °C. Both the structure of the biomass precursor and the nature of the initial Fe source and concentration would play a key role in the graphitization process. Previous studies showed that impregnation of lignocellulosic biomass with $FeCl_3$ results in degradation of hemicellulose and selective hydrolysis of cellulose.^{54–56} This would explain the different thermal evolution and release of CO_2 and Cl_2 species upon pyrolysis of $FeCl_3$ -impregnated biomass in comparison to the decomposition of raw biomass and $FeCl_3$ separately (Figure 3).
- 2 Then, at ~ 700 °C, FeO is fully reduced into metallic Fe as observed by both X-ray diffraction and TGA/DSC/mass spectroscopy experiments. This endothermic reduction is observed in the DSC, and the carbothermic reduction is evidenced by the release of CO_2 species at such a temperature range. Immediately, Fe_3C is formed and graphitization starts, resulting in the presence of a peak close to the (002) interplanar spacing of graphite in the X-ray diffraction pattern.

- 3 At temperatures above 750 °C, the carbide phase (Fe₃C) partially decomposes into metallic Fe with a fcc structure (austenite, γ-Fe), which is the equilibrium phase of metallic iron at temperatures higher than ~727 °C. Although the formation/decomposition of a carbide phase would play a key role in the graphitization at temperatures <800 °C upon heating, our *in situ* experiments suggest that the absence of Fe₃C reflections at temperatures above 800 °C indicates that this mechanism would not be dominant at high temperatures. Nevertheless, the Fe₃C decomposition into Fe with a bcc structure (ferrite, α-Fe) and C upon cooling gives for the first time clear evidence of the formation of additional graphitic regions, which may be explained by the decreased solubility of carbon into the metal catalyst particles with decreasing temperature and the precipitation of ordered carbon surrounding the catalyst particle core to reduce the surface energy upon cooling.^{57–59}
- 4 Our PDF results indicate that structural evolution continues from 800 °C and up to 2000 °C, not only increasing the average size of the graphitic domains but also resulting in flattening and stacking of graphene sheets. The largest degree of structural development occurs in the 1000–1600 °C range, as determined from the analysis of pair distribution functions of the resulting graphitized carbon. The decreased sheet curvature and increased stacking level of graphene sheets with lower turbostratic disorder at temperatures >1400 °C would be attributed to the precipitation of three-dimensional graphite crystals due to a higher catalyst particle size. Previous studies on catalytic graphitization using Ni as a catalyst^{35,60} have been invoked by transmission microscopy analysis that at lower temperatures, the graphitization takes place by deposition of curved graphene layers surrounding Ni particles of a few nanometers in size, while at higher temperatures (>1400 °C), the coarsening of catalyst droplets promotes the formation of three-dimensional graphite platelets by a solution precipitation mechanism. The abrupt decrease in interplanar distances and *U*₃₃ values would be related to the precipitation of less-defective graphite crystals, in comparison to lower temperatures where the carbon exhibits a higher curvature and turbostratic disorder.

Clearly, graphitization by transition metal catalysts is a complex phenomenon that can proceed by several, concurrent routes depending on the chemical state and the size of the catalyst particles. A simple calculation performed using FactSage⁶¹ yields the following Gibbs' free energies at *T* = 765 °C (normalized per mol Fe)



Therefore, the early formation of Fe₃C is thermodynamically favored when FeO is carbothermally reduced, whereas the formation of Fe₃C directly from metallic Fe (reaction 4) will only occur spontaneously at temperatures over ~820 °C. This is in agreement with the *in situ* observations of Hoekstra *et al.*²² who reported the onset of graphitization in the Fe–C system and formation of Fe₃C at temperatures as low as 715 °C. The formation of the carbide might also explain why Fe is a more

effective bulk graphitization catalyst than Ni or Co, as there is no stable carbide phase in the Ni–C and Co–C phase diagrams.⁶²

The nanosized nature of the catalyst particles resulting from the decomposition of the FeCl₃ precursor probably explains why graphitization occurs at much lower temperatures in our system than that observed by Li *et al.*⁶³ (~1200 °C), who mixed powders of milled coke carbon and iron (particle sizes <74 and <5 μm, respectively). The large particle sizes of Fe in the cited study probably limited the formation of Fe₃C due to the sluggish diffusion kinetics, and thus, graphitization only started when a liquid phase formed *via* a solution reprecipitation mechanism. Due to the large size of the particles, this liquid phase formed at temperatures above the Fe–C eutectic (~1150 °C), whereas in our system, it occurs much earlier due to the nanosized nature of the Fe particles.

4. CONCLUSIONS

Iron is an effective catalyst for the graphitization of hard carbons obtained from the pyrolysis. Understanding the graphitization mechanism by transition metals is of utmost importance for the future design of graphitic materials. A series of *in situ* experiments were herein carried out using Fe to shed light on the graphitization mechanism of a hard carbon. A homogeneous distribution of fine nanosized Fe particles within the carbon precursor was obtained after impregnation with FeCl₃. The temperature at which graphitization takes place is influenced by the local structure of the amorphous carbon and the size and initial oxidation state of the catalyst. Our results show that when deposited *in situ*, decomposition of the Fe precursor proceeds by a series of reductions, from Fe₂O₃ to FeO and finally to Fe, which favors the early formation of Fe₃C, promoting the graphitization of hard carbon at temperatures as low as 750 °C. However, Fe₃C reflections are absent at temperatures over 800 °C, indicating that the formation/decomposition of Fe₃C is not responsible for graphitization at higher temperatures. The largest structural development occurs in the 1000 °C–1600 °C temperature range. A monotonically increase in long-range ordering and decreased sheet curvature of the resulting graphitic carbon are observed at temperatures up to 1600 °C. At higher temperatures, the graphitic domains grow without an increase in local ordering: both the interplanar spacing between the graphene sheets and the turbostratic disorder remain constant up to 2000 °C.

■ ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acs.chemmater.0c04385>.

Results of Rietveld refinement of *in situ* synchrotron data and results of *in situ* diffraction experiments on a laboratory diffractometer upon heating from 200 to 1100 °C and cooling back to 200 °C (PDF)

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Notes

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ADDITIONAL NOTES

^aMass (u.m.a): 12 (C⁺ from CO, CO₂ and C_xH_y); 13 (CH⁺ from C_xH_y); 14 (CH₂⁺ and CO₂²⁺ from C_xH_y and CO); 15 (CH₃⁺ from C_xH_y); 16 (O⁺ and CH₄⁺ from H₂O and CH₄); 17 (OH⁺ from H₂O); 18 (H₂O⁺ from H₂O); 22 (CO₂²⁺ from CO₂); 24 (C₂⁺ from C_xH_y); 26 (C₂H₂⁺ from C_xH_y); 27 (C₂H₃⁺ from C_xH_y); 32 (O₂⁺ from O₂); 35 (³⁵Cl⁺ from Cl₂); 37 (³⁷Cl⁺ from Cl₂); 38 (H³⁷Cl⁺ from HCl and C₃H₂⁺ from C_xH_y); 39 (C₃H₃⁺ from C_xH_y); 41 (C₃H₅⁺ from C_xH_y); 42 (C₃H₆⁺ from C_xH_y); 43 (C₃H₇⁺ from C_xH_y); 44 (CO₂⁺ from CO₂); and 45 (¹³CO₂⁺ from CO₂).

^bThe agreement factor is defined as

$$R_w^2 = \frac{\sum (y_i^{\text{obs}} - y_i^{\text{calc}})^2}{\sum (y_i^{\text{obs}})^2} \times 100\%, \text{ where } y_i \text{ is the value at position } i.$$

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