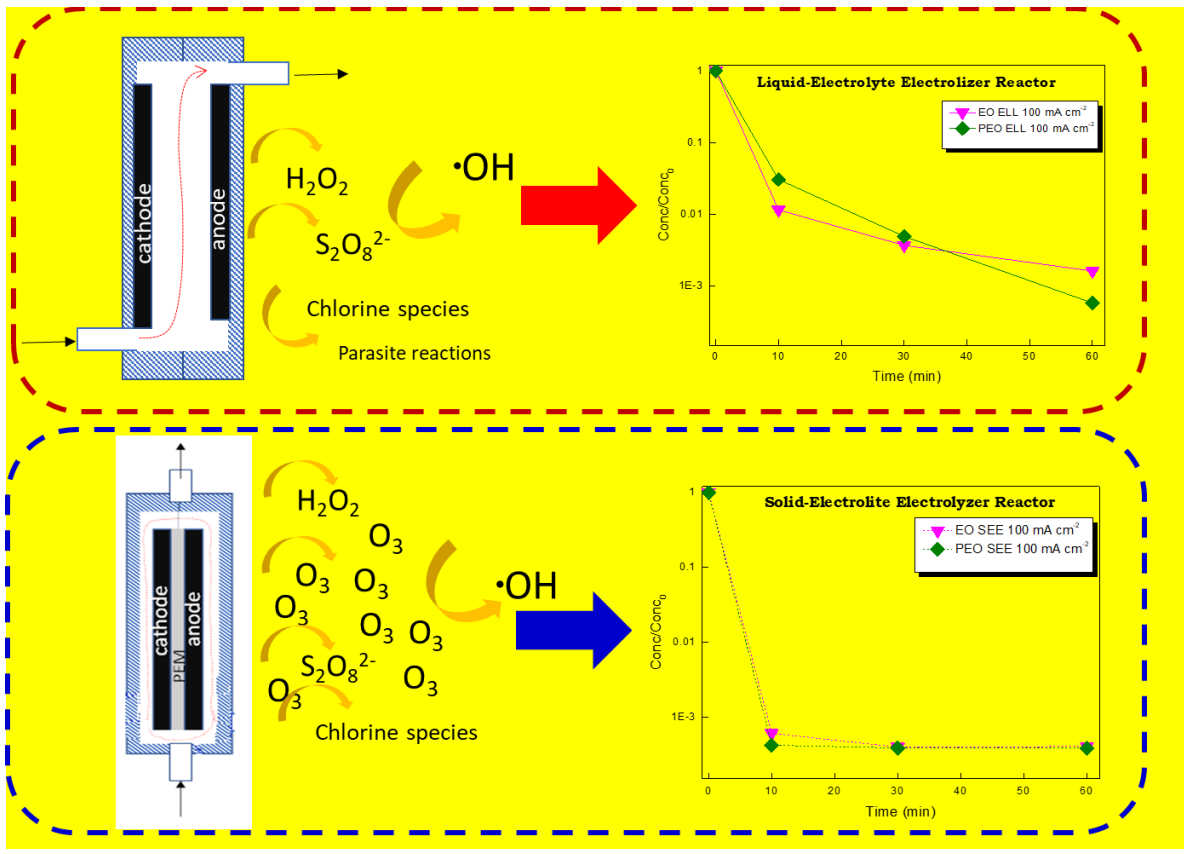


1 **Improving the degradation of low concentration of microcystin-LR with PEM**
 2 **electrolyzers and photo-electrolyzers**

3 F.L. de Souza, C. Sáez, P. Cañizares, M.A. Rodrigo*
 4 Department of Chemical Engineering, Faculty of Chemical Sciences & Technologies,
 5 Universidad de Castilla - La Mancha, Campus Universitario s/n, 13071 Ciudad Real,
 6 Spain

8 **Graphic Abstract**



9
10
11
12

13 **Abstract**

14 In this work, the performances of two electrochemical cells, a conventional liquid-
15 electrolyte electrolyzer (LEE) and a solid-electrolyte electrolyzer (SEE) were compared
16 for the treatment of two real water matrixes polluted with microcystin-LR at trace
17 concentrations. The first consists of single-compartment flow cell, while the second
18 consists of membrane-electrode assembly flow cell. Both cells can attain the removal of
19 the microcystin, although the toxin degradation was more efficient in the SEE, for both
20 water matrixes assessed, decreasing the initial concentration by 3-logs and achieving in
21 short treatment times concentrations below the guidelines of the World Health
22 Organization (WHO) for drinking water. Irradiation of UVC improves results reached by
23 the electrochemical technologies, although in lower extension than initially expected. The
24 great performance of SEE reactor is attributed to a more suitable production of oxidants
25 and a lower operation-dependence with respect to the water matrix conductivity. This cell
26 can remove pollutants also faster than the single photolysis and, in comparing its
27 performance with the other technologies assessed in this work, it is the best choice
28 requiring the less time and energy to meet the WHO standards, without being necessary
29 the coupling with photolysis.

30 **Keywords**

31 microcystin, algae toxins, hybrid processes, advanced electrochemical oxidation
32 process, electrochemical cells

33 **Highlights**

- 34 • Microcystins are efficiently degraded by electrolysis and photo-electrolysis
- 35 • Microcystin-LR is degraded photochemically by UVC irradiation
- 36 • SEE reactor obtained better performance than the LEE for the MC-LR removal

- 37 • High dependence of water matrix characteristics when using the LEE
- 38 • Irradiation of UVC improved the removal rates in both electrolyzers
- 39 • SEE without light irradiation seems to be the best choice for a full-scale
- 40 application

41

42

43 * author to whom all correspondence should be addressed: manuel.rodriigo@uclm.es

44

45

46 **1. Introduction**

47

48 In the last three decades, a very important number of works have been published aiming
49 to elucidate which was the effect of the electrode material on the degradation of hundreds
50 of organic pollutants(Martinez-Huitle et al., 2015; Sirés et al., 2014). General conclusions
51 of these papers indicate that, when using suitable electrodes, such as diamond coatings,
52 all pollutants can be completely mineralized (except for rare molecules such as the
53 reported by this group recently(Mena et al., 2018)) and this fact positioned
54 electrochemical advanced oxidation processes in the crest of the wave of the research in
55 advanced oxidation technologies (Dewil et al., 2017).

56 However, there is an important drawback of electrochemical processes: efficiency
57 decreases importantly in diluted wastes because the rate of the processes is diffusion-
58 controlled and working with concentrations under 100 mg dm^{-3} of pollutants leads to very
59 inefficient processes. Only when there is a significant contribution of the mediated
60 oxidation processes, the electrolysis becomes interesting, and reaching these conditions
61 is not always easy. These mediated processes are activated by the oxidation of species
62 naturally contained in the water or wastewater to be treated (such as sulfate, chloride,
63 carbonate, etc.) or by special designs of the electrochemical cells made to promote the
64 formation of oxidants such as hydrogen peroxide or ozone (gas diffusion electrodes,
65 membrane electrode assemblies, etc.)(Fernando Perez et al., 2019; Perez et al., 2018a;
66 Perez et al., 2018b; Perez et al., 2019).

67 One relevant pollutant, typically found at very low concentrations, are the microcystins
68 (MC), which are associated with water polluted with cyanobacteria (Westrick et al., 2010;
69 Wood, 2016). These cyanotoxins belong to a family of hepatocyte cyclic peptides, with

70 about seventy related compounds, being the two most relevant the microcystin-LR (MC-
71 LR) and microcystin-RR (MC-RR) where L and R represent leucine and arginine,
72 respectively [11-13]. The World Health Organization (WHO) has set 1 µg/L of MC-LR
73 as a guideline value in drinking water (Guidelines for drinking-water quality and criteria
74 and other supporting information. World Health Organization, 1998), whereas recently,
75 the US Environmental Protection Agency (EPA) (Agency, 2020) added three cyanotoxins
76 (microcystin-LR, anatoxin, and cylindrospermopsin) to the Contaminant Candidate List
77 3 (CCL3) [14,15]. ~~In this context, it is worth to point out that~~ The removal of microcystins
78 is not easy and different methods have been investigated including coagulation (Şengül
79 et al., 2016), pre-oxidation (Gad and El-Tawel, 2015), photocatalytic degradation using
80 TiO₂ (Pelaez et al., 2009; Pestana et al., 2015; Yu, 2013), desalination (Boerlage and
81 Nada, 2014; Laycock et al., 2012; Seubert et al., 2012), adsorption (Pavagadhi et al.,
82 2013), application of ultrasounds (Rajasekhar et al., 2012), UV photolysis (He et al.,
83 2013; He et al., 2012; Sharma et al., 2012) and electrochemical oxidation (Shi et al., 2005;
84 Zhang et al., 2009). As pointed out before, this later technology has been demonstrated
85 to be very efficient in the removal of a large variety of compounds, being able to attain
86 their complete degradation. However, the concentrations at which these pollutants are
87 contained in the environment are a serious handicap and the use of new types of
88 electrochemical cells may be the best way to face it.

89 This work aims to compare the performance of two electrochemical cells in the treatment
90 of organic pollutants contained at very low concentrations: a conventional liquid-
91 electrolyte electrolyzer (LEE) and a solid-electrolyte electrolyzer (SEE). In the first case,
92 the water matrix acts as an electrolyte, while in the second, electrodes are connected to a
93 membrane, which behaves as the main electrolyte of the cell, and then, the system is
94 expected to be less dependent to the water matrix composition. In both cases, the water

95 to be treated is in direct contact with the electrodes and, hence, oxidants can be formed
96 from various of the ions contained (chlorides, sulfates, carbonates, etc.). Because of the
97 relevance of the matrix in terms of the oxidants that can be produced during the
98 electrochemical process, in this work, microcystins are going to be added to two real
99 water matrixes with a very different composition. Thus, because of the low concentration,
100 degradation made by direct electrolysis mechanisms is expected to be negligible as
101 compared to mediated electro-oxidation and, hence, the composition of the electrolyte is
102 expected to be extremely important. Besides, as the production of oxidants is expected to
103 be very important, both cells will be connected to a photolysis system which can also
104 degrade the microcystins or modify the degradation obtained in each of the cells.

105

106 **2. Materials and Methods**

107 **Chemicals and water samples.** Microcystin-LR purity $\geq 95\%$ (HPLC) (Enzo Life
108 Science, Inc.), Potassium iodide $\geq 99.99\%$ (Merck), Sodium thiosulfate Reagent Plus[®]
109 99% (Merck), Starch soluble (Merck), Sulfuric acid 98% (a.r., Scharlab, Spain) are of
110 analytical grade and used as received. Acetonitrile HPLC grade (Sigma-Aldrich, Spain)
111 was used for the mobile phase. Double deionized water (Millipore Milli-Q system,
112 resistivity = 18.2 M Ω cm at 25 °C) was used to prepare all solutions.

113 Fresh waters were directly collected in an agricultural irrigation well and a dump near
114 Ciudad Real (Spain). These water matrixes were subsequently filtered using Whatman[®]
115 qualitative filter paper grade 1 and used to prepare a standard solution containing 1 mg
116 dm⁻³ of MC-LR. The handling of this toxin was done with extreme care because it is
117 highly toxic and irritant and all the experiments were conducted in a full exhaust cabinet.
118 0.15 dm³ of each solution was used in each experiment as model wastewater. The initial

119 pH was the natural of each water matrix and no pH correction was performed over the
 120 tests. Table 1 shows the characteristics of the water matrixes utilized.

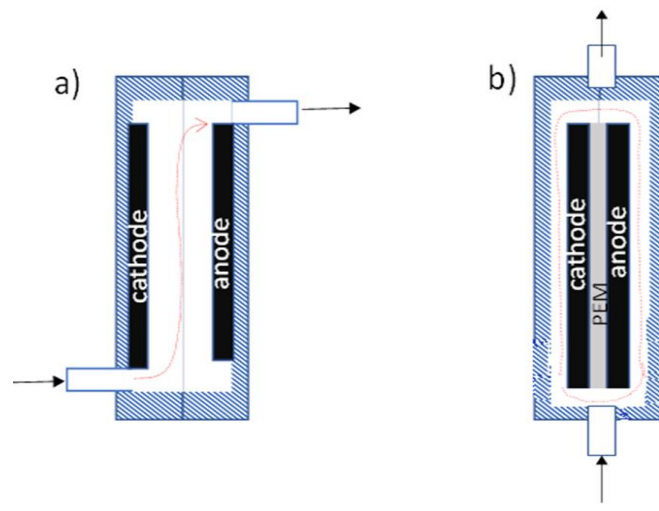
121 **Table 1.** Characteristics of the water matrixes used in the experiments.

Parameter	water matrix 1	water matrix 2
pH	6.3	8.2
Conductivity ($\mu\text{S cm}^{-1}$)	222	381
F^{-} (mg dm^{-3})	1.22	0.75
Cl^{-} (mg dm^{-3})	20.18	42.99
NO_2^{-} (mg dm^{-3})	0.00	0.00
NO_3^{-} (mg dm^{-3})	0.00	1.10
SO_4^{2-} (mg dm^{-3})	40.73	49.06
PO_4^{3-} (mg dm^{-3})	17.98	1.61
Na^{+} (mg dm^{-3})	17.43	27.70
NH_4^{+} (mg dm^{-3})	0.00	0.00
K^{+} (mg dm^{-3})	6.99	18.47
Ca^{2+} (mg dm^{-3})	23.92	59.03
Mg^{2+} (mg dm^{-3})	5.70	14.40

122

123 **Experimental setup.** All the processes were carried out in a lab-scale setup described
 124 elsewhere(Souza et al., 2020a), containing 0.15 dm^3 of solution under recirculation. Two
 125 electrochemical cells were evaluated in this work. A basic scheme of the concept in which
 126 both cells are based is shown in Figure 1. In both cells, anode and cathode were diamond
 127 coatings with the same size (approx. 1 cm^2). The first cell was an in-house made single-
 128 compartment flow-pass cell in which the electrodes are faced and water pass in the gap
 129 between both. The second is a commercial cell (Mikrozon Cartridge supplied by
 130 Condias[®] GmbH (Itzehoe, Germany) and it consists of a membrane electrode assembly
 131 (MEA) in which one the faces of the electrodes is in contact with a Nafion ion exchange
 132 membrane N324 (DuPont) and the other with the water to be treated. No further details
 133 are given because the internal design is protected. Because the direct path between

134 electrodes is the proton-conducting membrane, the main electrolyte of the cell is the solid
135 electrolyte, although water passed throughout the cell also behaves as an electrolyte. In
136 this work, the first concept of cell is going to be called as liquid-electrolyte electrolyzer
137 (LEE) and the second as solid-electrolyte electrolyzer (SEE). Both mini-electrochemical
138 cells were subjected to cleaning procedure during 10 min in a 1 M Na₂SO₄ solution at 0.1
139 A before electrolysis assays.



140

141 **Figure 1.** Layout of the two electrochemical cells assessed in this work: a) Single-pass
142 flow cell: liquid-electrolyte electrolyzer (LEE) b) single-pass PEM Flow cell: solid-
143 electrolyte electrolyzer (SEE).

144

145 Continuous recirculation through the reservoir, UVC photoreactor and the
146 electrochemical cell was kept at a flow rate of 0.78 dm³ h⁻¹. Before the tests, this solution
147 was homogenized by recirculation through all the units during 10 min in the darkness.
148 During tests, the temperature kept at 20 °C.

149

150 **Analytical procedures.** Samples were taken at different time intervals to monitor the
151 oxidation process. All the samples were filtered with 0.45 µm nylon filters from Whatman
152 before their analysis. MC-LR was determined by HPLC using Mass spectrometry

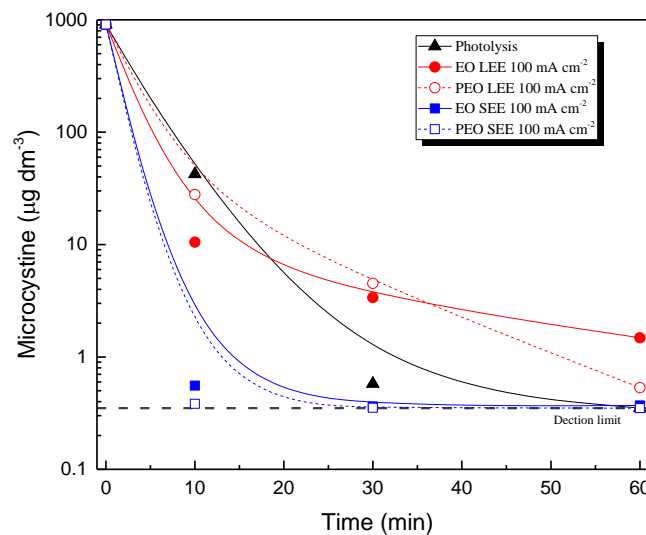
153 (HPLC/MS/MS). Agilent Technologies 1260 series LC with Agilent Technologies 6460
154 series electrospray ionization triple -quadrupole MS/MS was used. The column was a
155 Poroshell C18 (2.1 mm x 100mm x 2.7 μm). The mobile phase were (A) 0.1% formic
156 acid in methanol and (B) 0.1% formic acid in Milli-Q water. A linear gradient was applied
157 starting at 10% of (A), to 80% of (A) for 3 min over 7 min at flow rate 0.5 mL min⁻¹. MS
158 conditions were: capillary temperature of 350 °C, capillary voltage of 4.0 kV, nitrogen
159 gas at flow rates of 12 L min⁻¹. The precursor ion for MC-LR selected was m/z 135 by
160 product ion scan MS/MS mode. Finally, the multiple reaction monitoring (MRM) mode
161 (MZ = 215) was used for obtaining peak areas of the microcystin to track the reaction
162 kinetics. Positive electrospray was employed to record spectra.
163 Total oxidants, pH and conductivity were measured as described elsewhere (Souza et al.,
164 2020a).

165

166 **3. Results and discussion**

167 Figure 2 shows the changes in the MC-LR concentration contained in the Water Matrix
168 1 during the electrolysis (EO) and photo-electrolysis (PEO) with the two electrochemical
169 reactors evaluated in this work. As seen, MC-LR is destroyed by electrochemical,
170 photochemical, and photoelectrochemical technologies and MC-LR concentrations
171 decreased more than three logs in reaction times below 1 hour. Additionally,
172 concentrations reached are below (or in the nearness) the maximum recommended in the
173 guidelines of WHO (1 $\mu\text{g dm}^{-3}$ for microcystin-LR in drinking-water) in all the processes
174 studied. The good degradation results obtained by photolytic treatment can be explained
175 by microcystine structure that contain conjugated double bond and unsaturated bonds
176 responsible to UVC absorption [14] [15][19-21].

177 During the electrooxidation process employing a LEE reactor, the MC-LR concentration
 178 decreases from $1000 \mu\text{g dm}^{-3}$ down to $10.5 \mu\text{g dm}^{-3}$ during the first 10 minutes, reaching
 179 $1.4 \mu\text{g dm}^{-3}$ at the end of the treatment with a total specific current charge passed of 0.66
 180 Ah dm^{-3} . In the case of using a SEE type reactor, concentration decreased down to 0.53
 181 $\mu\text{g dm}^{-3}$, clearly below the guidelines of the WHO, in the first 10 minutes of treatment,
 182 with a total required electric charge below 0.1 A h dm^{-3} . This low energy requirement
 183 may be easily assumed for a full-scale application.



184

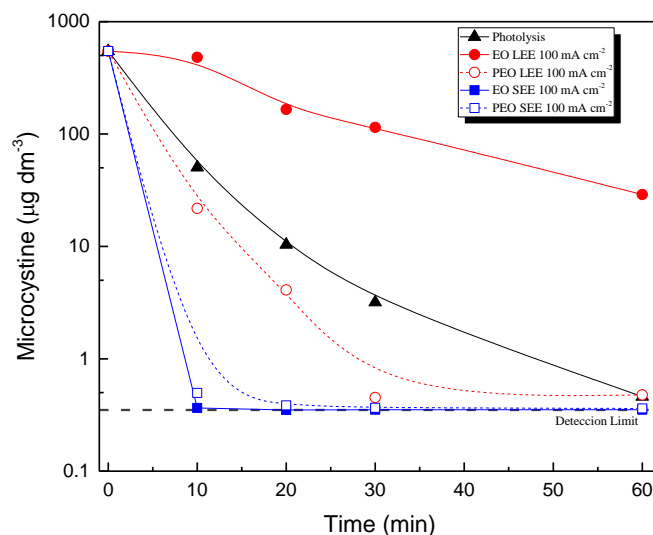
185 **Figure 2.** MC-LR concentration reduction (Log scale) as a function of reaction time for
 186 all processes studied using LEE reactor and SEE reactor. Conditions: 100 mA cm^{-2} , pH
 187 natural, $T = 20 \text{ }^\circ\text{C}$ without addition of salts. LC-MR solution prepared at Water Matrix 1.

188 When electrochemical and photolytic treatments are combined, results are improved at
 189 long reaction times, but the differences are not as high as pointed out in the removal of
 190 other pollutants (Souza et al., 2020b). In fact, at low reaction times, results obtained by
 191 the LEE become worse and, comparing to the photolytic process, the concentration
 192 obtained by the combined photo-electrolysis with the LEE cell is much worse. Regarding
 193 the SEE, the coupling of technologies allows to reach a decrease in the concentration of

194 MC-LR down to $0.36 \mu\text{g dm}^{-3}$, just near the detection limit of the measuring technique
195 used.

196 The semilogarithmic plot is not linear in the case of the treatments with the LEE, opposite
197 to what it can be expected in diffusion or mediated oxidation controlled processes(Aquino
198 et al., 2014). In fact, two slopes can be clearly seen, being the second lower than the first.
199 The existence of two slopes in electrochemical and photochemical degradations in
200 discontinuous mode has been associated in the literature(Dionisio et al., 2020) to a change
201 in the oxidation mechanisms. In this case, because of the extremely low concentration of
202 organics, oxidants are expected to explain this change. Regarding to photolysis and SEE-
203 electrolysis, this statement is not as clear as in the case of the photolysis and LEE-
204 electrolysis, considering that the decrease down to the detection limit ($0.3 \mu\text{g dm}^{-3}$) is
205 almost linear.

206 Figure 3 shows the MC-LR concentration decay when the treatment technologies are
207 applied to the second water matrix. Ionic conductivity of this matrix is higher and there
208 is a higher presence of chloride and sulfate anions, which may become precursors of
209 oxidants species in the reaction media. Because of that, different mechanism reactions
210 may be expected to occur. Here, there are no two slopes in the concentration vs time plot,
211 but only one, fitting well the kinetics to a pseudo-first order, as expected considering that
212 mediated oxidation and diffusion of the pollutants to the electrode surface are controlling
213 the degradation rates.



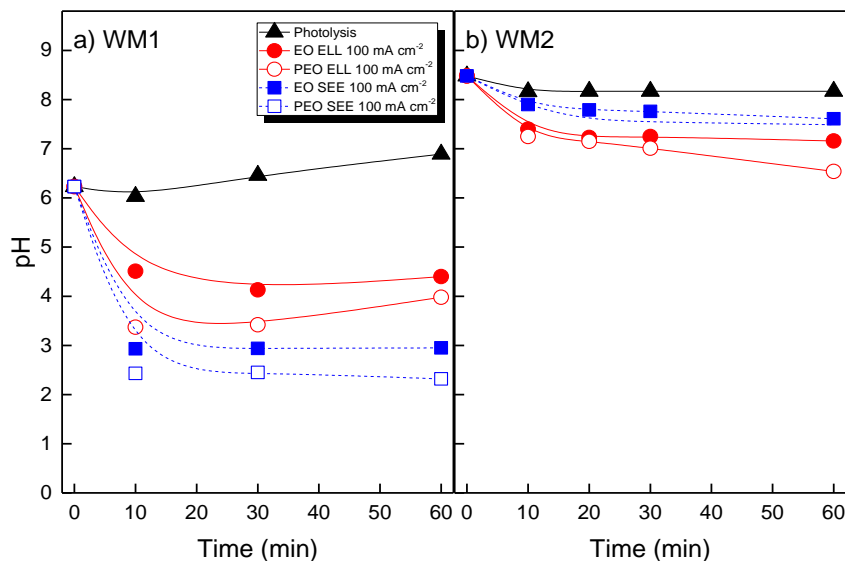
214

215 **Figure 3.** MC-LR concentration reduction (Log scale) as a function time for all processes
 216 studied using LEE reactor and SEE reactor. Conditions: 100 mA cm⁻², pH natural, T = 20
 217 °C without addition of salts. LC-MR solution prepared at water matrix 2.

218

219 Regarding the use of LEE, single electrolysis obtained slightly worse results as compared
 220 with those obtained with the first water matrix. Same can be said for UCV photolysis,
 221 which exhibited a slower removal. However, finally, after one hour of treatment, it
 222 reached 99.5 % of elimination, which corresponded to MC-LR concentrations of 0.46 µg
 223 dm⁻³. For electrolysis carried with SEE electrolyser, the MC-LR degradation results show
 224 an improvement in this water matrix compared to the water matrix 1. In addition, the
 225 combination of photolysis and electrolysis was found to be positive for the two cells
 226 studied (also if compared to the bare UVC photolysis). In case of using the LEE reactor,
 227 an improvement in the MC-LR removal of 62% was obtained when light was irradiated.
 228 However, the best results were obtained with a cell type SEE in which a quick decay is
 229 observed with 100 % of elimination (below detection limit of the technique) at 30 minutes
 230 for bare electrolysis and at only 10 minutes of treatment for combined photo-electrolysis.

231 Changes in the pH during the treatment of both water matrixes are shown in Figure 4. As
 232 seen, changes produced by photolysis are negligible in both water matrixes, which is not
 233 the case when electrolysis or photo-electrolysis are applied, for which a decrease in the
 234 pH is clearly observed. In addition, changes are more important in the case of the water
 235 matrix 1, which can be explained in terms of the lower ionic strength of the matrix and,
 236 hence, in its lowering buffering capacity. Because of these changes and considering that
 237 pH was not controlled but only monitored, the electrochemical treatment of the water
 238 matrix 1 was carried out at acidic conditions while the treatment of water matrix 2 was
 239 carried out at more neutral conditions. Worth to highlight that the acidification observed
 240 by photo-electrolysis was higher than that observed for the bare electrolysis. As well, the
 241 changes in the pH (acidification) are more important when SEE reactor is used.



242

243 **Figure 4.** Evolution of pH during the different treatments evaluated in this work
 244 employing a LEE reactor and a SEE reactor. Conditions: 100 mA cm^{-2} , pH natural, $T =$
 245 $20 \text{ }^\circ\text{C}$ without addition of salts. LC-MR solution prepared at water matrix 2.

246 Figure 5 shows the oxidants generated during the treatments carried with the two water
 247 matrixes. For all technologies the oxidants remaining in the water are quite similar. In

248 fact, the lowest concentrations are observed for the most efficient technologies, because
249 oxidants react and disappear very rapidly, in particular the radical species, and the
250 oxidants measured are those which do not react with the organics and other oxidizable
251 compounds existing in the water matrixes. Comparing the two water matrixes the lowest
252 concentrations of oxidants were obtained for matrix 2, despite of the higher conductivity,
253 and hence the higher concentration of ions which can become precursors of oxidants.
254 Also, important to highlight that oxidants are also produced in a very important way
255 during photolysis, especially in the case of the water matrix 1.

256 This matrix from tap waters contain free available chlorine species (HClO/ClO^-) that
257 under UV irradiation are activated generating highly reactive species such as hydroxyl
258 radicals ($\text{HO}\cdot$), chlorine radicals ($\text{Cl}\cdot$) and ground-state atomic oxygen ($\text{O}(3\text{P})$). These
259 chlorine species (RCS) are responsible to inactivation of MCs [2, 14, 24][22, 23].

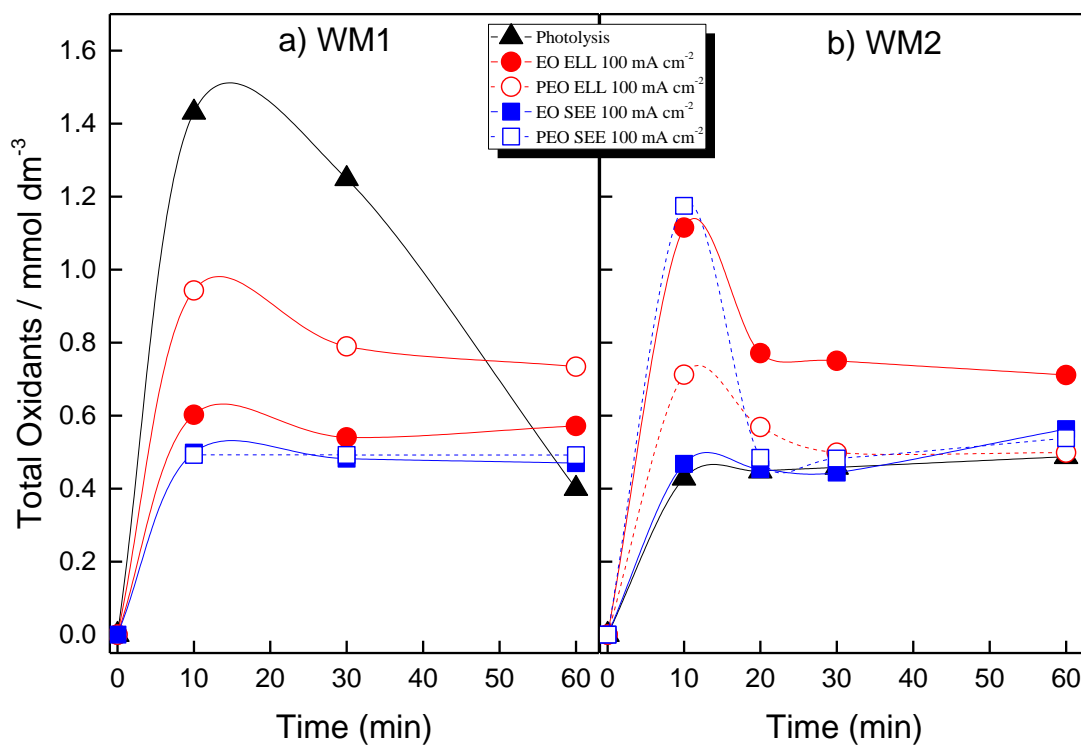
260 In addition, besides direct photochemical degradation, indirect photolysis also can occur,
261 taking in account that in these waters there is a presence of chloride. This reaction occurs
262 through free available chlorine species (HClO/ClO^-) that under UV irradiation are
263 activated generating highly reactive species such as hydroxyl radicals ($\text{HO}\cdot$), chlorine
264 radicals ($\text{Cl}\cdot$) and ground-state atomic oxygen ($\text{O}(3\text{P})$). After the generation of primary
265 radicals ($\text{HO}\cdot$ and $\text{Cl}\cdot$), they undergo subsequent reactions to produce reactive chlorine
266 species (RCS) mainly $\text{Cl}_2^{\cdot-}$ and $\text{ClO}\cdot$ as secondary radicals and $\text{O}(3\text{P})$ can react with O_2
267 and yield the ozone under oxic conditions [22, 23]. In this way, RCS have demonstrated
268 to be very important oxidants responsible to inactivation of MCs [2, 14, 24]. Zhang et al
269 2018 showed that MC-LR (initial concentration 1.0 mM) was reduced by 20.3% under
270 UV irradiation alone and at a chlorine dose of 3.0 mg L^{-1} and UV fluence of 125 mJ cm^{-2} ,
271 MC-LR was reduced by 92.5%, which was much higher than and 65.1% removal during
272 dark chlorination. Besides, the toxicity of the treated water was reduced by 75.0%, which

273 was also higher than 25.7% and 46.7% removal under UV irradiation alone and during
274 dark chlorination, respectively [24].

275 Regarding the electrolysis results, the behavior observed should be explained attending
276 to the differences between the two cells used. While in the LEE the electrolyte is the own
277 water matrix, in the SEE type reactor the electrolyte is the Nafion membrane. In the first
278 case, the generation of hydroxyl radicals and many other oxidants on the diamond surface
279 depends on speciation and quantity of salts in the water matrix. In fact, the cell voltages
280 are higher than those observed in the SEE, especially in the Water Matrix 1, because of
281 the lower ionic conductivity of this matrix. Because of the use of boron doped diamond
282 electrodes, apart from a significant production of hydroxyl radicals, many other powerful
283 oxidants can be formed, such as hydrogen peroxide, ozone and others, such as
284 peroxosalts(Canizares et al., 2009; Moraleda et al., 2019; Velazquez-Pena et al., 2013).
285 Thus, for the LEE, it is expected the production of peroxosulfates from sulfates and
286 chlorine from chloride ions. Under UVC irradiation these species can be activated
287 forming sulfate and chlorine radicals, with a higher oxidation capacity, which can explain
288 that coupling UV-C photolysis to electrolysis improved the MC-LR removal significantly
289 [33, 51-55]. These species can also be formed when oxidants interact among them and,
290 hence, the production of other oxidants such as ozone or hydrogen peroxide is expected
291 to influence on results.

292 In the SEE, oxidants are not only produced on the faces of the electrodes in contact with
293 the water, but they are also produced on the surface that faces the membrane. Thus, it has
294 been demonstrated an important promotion in the production of ozone(Isidro et al., 2019;
295 Isidro et al., 2020; Isidro et al., 2018) in the SEE as compared to LEE. Various studies
296 have concluded that ozone is very effective at much lower concentrations than chlorine
297 and the disinfection occur quite rapidly once a critical residual level is reached [26]. Thus,

298 it is known that mixture of ozone or hydrogen peroxide with peroxosulfate or with
299 chlorine promote the formation of several radicals, which may be the responsible for the
300 much better performance of the SEE system. In addition, when SEE was employed, lower
301 concentrations of surplus oxidants are detected. This means that a significant amount of
302 the oxidants produced in the medium was consumed in the oxidation of microcystin and
303 then, they are not detected in the solution. However, it is important to consider that the
304 presence of these radicals is not always positive. Lifetime of radicals is very short, and
305 they are only effective when the concentration of organics to be oxidized is high.
306 Otherwise, they are deactivated reactivating the non-radical peroxosalts or forming
307 oxygen and other species with lower oxidation capacity. This can help to understand the
308 two slopes observed in the concentration vs time semilogarithmic decay, with a much
309 lower rate when the concentrations of microcystin are almost negligible and thus, the
310 possibilities of interactions between radicals and pollutants decrease. Other important
311 observation is the pH variation during the experiments. The pH initial of the solution
312 varied more importantly with the SEE reactor. This behavior can explain the better results,
313 once that in according to Farook et al. acidic conditions provided better disinfection than
314 alkaline because of greater ozone stability, and thus higher ozone residuals that can act
315 on the oxidation of MC-LR (Farook, 1977).



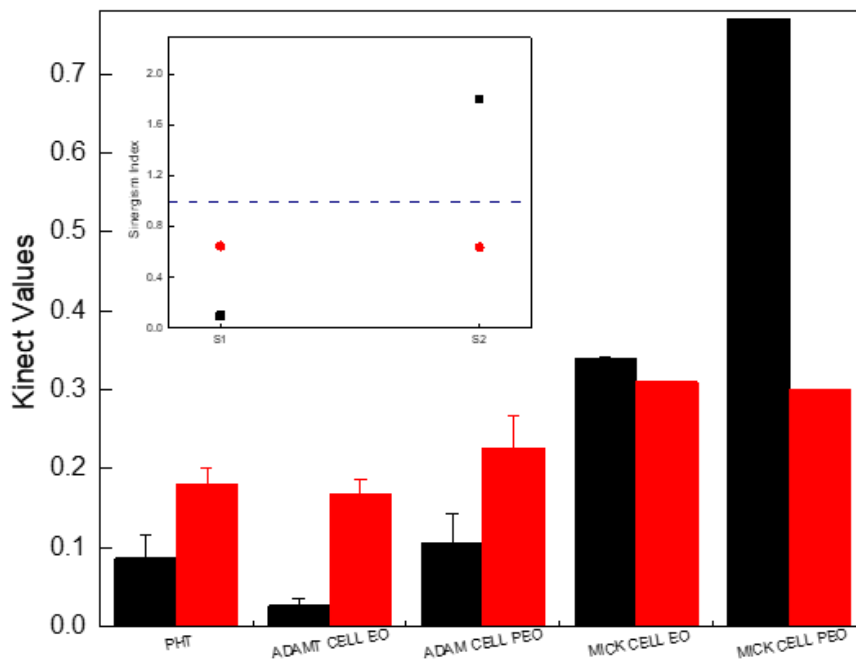
316

317 **Figure 5.** Total oxidants generated in Water Matrix 1 (part a) and WM2 (part b) as a
 318 function time for different treatments evaluated in this work employing a LEE reactor and
 319 a SEE reactor. Conditions: 100 mA cm^{-2} , pH natural, $T = 20 \text{ }^\circ\text{C}$ without addition of salts.

320

321 Figure 6 shows the kinetic constants obtained after fitting the first zone of the
 322 experimental degradation results to a first order kinetic model for all experiments carried
 323 out in both water matrixes. Regarding to reactors employed, as can be seen, highest rates
 324 were obtained when SEE type reactor was employed. This means that the generation of
 325 oxidants was huge compared to other oxidants in the LEE reactor. The first order kinetic
 326 can be explained because of the pseudo-steady state approach proposed by the group of
 327 Palmas (Mascia et al., 2007) and later verified in other works(Aquino et al., 2014;
 328 Dionisio et al., 2019a; Dionisio et al., 2019b), which confirm the mediated oxidation as
 329 the main mechanisms of oxidation.

330 The Figure also shows that there was a great improvement in the reaction rate when light
 331 irradiation was coupled to EO system, especially when SEE reactor was used. However
 332 the effect is not synergistic but antagonistic with values of the synergistic coefficient
 333 (calculated according to the procedure describe elsewhere (Souza et al., 2019)) below 1.0,
 334 except for the case of the SEE operating in the photoelectrochemical mode, for which a
 335 value slightly over 1 is found. Thus, the inset of the Figure shows the synergy index of
 336 the combined system which S1 represent the synergism when light irradiation was couple
 337 to EO when LEE reactor was used and S2 correspond to UV-C couple to EO-SEE. As
 338 can be seen, because of the high efficiency of the single processes and also because of the
 339 negative effects of the presence of many radicals when the concentration of organics is
 340 very low their combinations do not result in a synergistic but in antagonistic values.

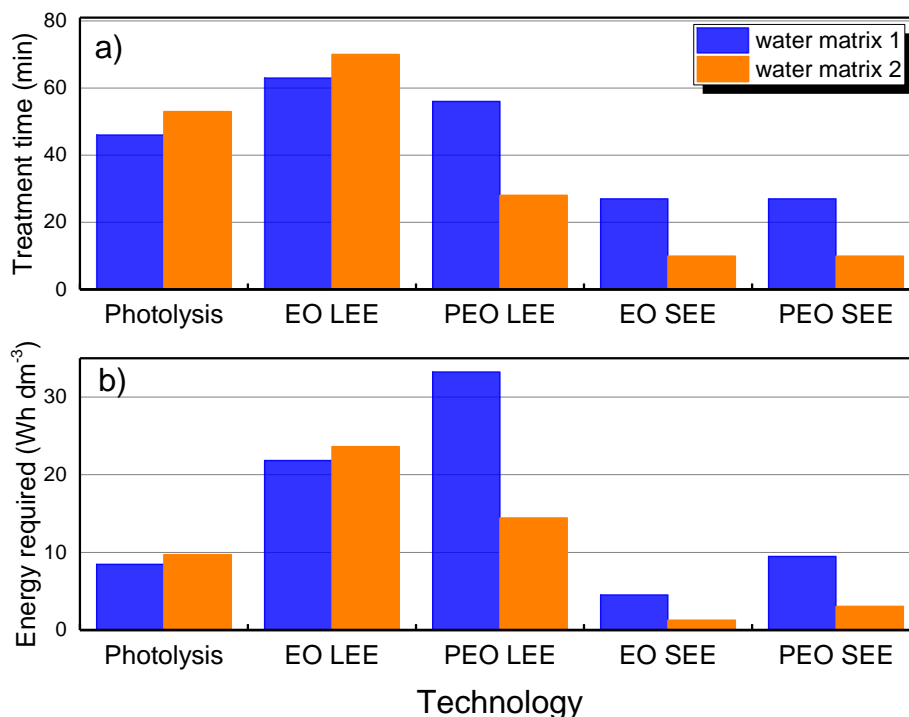


341

342 **Figure 6.** Kinect constants obtained after fitting the experimental degradation LC-MR
 343 results to a first-order kinetic reaction model. Inset: Synergistic effect calculated at S1
 344 using processes using a liquid electrolyte electrolyzer (LEE) and a Solid electrolyte
 345 electrolyzer (SEE). (■) LC-MR solution prepared at pore water matrix and (●) LC-MR

346 solution prepared at surface water matrix. Conditions: pH natural, T 20 °C without
347 addition of salts.

348 Hence, important differences are found in the degradation of microcystins associated to
349 the reactor type and light application. Here, it is important to compare the technologies in
350 order to make a first applicability estimation, regardless the TRL of this work is not high
351 enough to make a complete and rigorous economic analysis. This comparison is shown
352 in Figure 7, in terms of the treatment time required and energy consumed by each
353 technology to decrease the concentrations from 1 ppm down to the 1 ppb level
354 recommended by WHO for drinking water.



355

356 **Figure 7.** a) Treatment time and b) Energy required by each technology to achieve 1 μg
357 dm^{-3} recommended by WHO for drinking water.

358 Results demonstrate that the selection of a PEM electrolyzer is advisable not only from
359 the point of view of contact times required for the depletion of the hazardous pollutant

360 but also because of the cost, as this system allows to reach the target with the minimum
361 energy demand. In this case the combination with UCV irradiation is not recommended,
362 because despite for the conventional cell (LEE) clear advantages are noticed, in the case
363 of the PEM electrolyzer (SEE) it leads to an unnecessary increase in the energy consumed.
364 The results shown in the Figure, also point out the significance of the water matrix. Thus,
365 in the best case (photo-electrolysis with SEE), energy demanded for the removal of the
366 same amount of MC-LR is more than the double required for a water with higher
367 conductivity (and hence more oxidants precursors).

368

369 **4. Conclusions**

370 From this work, the following conclusion can be drawn:

- 371 • Microcystin-LR can be destroyed by electrochemical, photochemical and
372 photoelectrochemical technologies. The initial concentration of this toxin can be
373 decreased more than three-logs in less than 1 hour of treatment, attaining values
374 below the recommended in the guidelines of WHO for drinking water ($1 \mu\text{g dm}^{-3}$).
375 ³).
- 376 • Better performances were obtained employing a SEE reactor as compared to LEE
377 reactor for both water matrixes. UCV photolysis was more effective than
378 electrochemical treatment with the LEE but not with the SEE. Combining
379 photolysis with electrolysis leads to improvement in the treatment.
- 380 • The best results obtained to SEE can be explained in terms of a more suitable
381 production of oxidants. This reactor is also less dependent on the conductivity of
382 the treated water because the main electrolyte is a polymer exchange membrane.

383 • SEE reactor is the best choice for water treatment with low conductivity and very
384 low pollutant concentration from the point of view of contact times required for
385 your complete depletion as well of the energy required.

386

387 **Acknowledgements**

388 Financial support from the Agencia Estatal de Investigación and European Union through
389 projects CTQ2017-91190-EXP, PID2019-107271RB-I00 and PID2019-110904RB-I00 is
390 gratefully acknowledged. Also, financial support from Coordenação de Aperfeiçoamento
391 de Pessoal de nível Superior (CAPES) process 88881.171154/2018-01 for the scholarship
392 awarded to Fernanda L. Souza is gratefully acknowledged.

393

394

395 **5. References**

- 396 Agency USEP. Contaminant Candidate List (CCL) and Regulatory Determination. 2020, 2020.
397 Aquino JM, Rocha-Filho RC, Saez C, Canizares P, Rodrigo MA. High efficiencies in the
398 electrochemical oxidation of an anthraquinonic dye with conductive-diamond anodes.
399 Environmental Science and Pollution Research 2014; 21: 8442-8450.
400 Boerlage S, Nada N. Algal toxin removal in seawater desalination processes. Desalination and
401 Water Treatment 2014; 55: 2575-2593.
402 Canizares P, Saez C, Sanchez-Carretero A, Rodrigo MA. Synthesis of novel oxidants by
403 electrochemical technology. Journal of Applied Electrochemistry 2009; 39: 2143-2149.
404 Dewil R, Mantzavinos D, Poullos I, Rodrigo MA. New perspectives for Advanced Oxidation
405 Processes. Journal of Environmental Management 2017; 195: 93-99.
406 Dionisio D, Motheo AJ, Saez C, Canizares P, Rodrigo MA. Competitive Anodic Oxidation of
407 Methyl Paraben and Propylene Glycol: Keys to Understand the Process.
408 Chemelectrochem 2019a; 6: 771-778.
409 Dionisio D, Motheo AJ, Saez C, Rodrigo MA. Effect of the electrolyte on the electrolysis and
410 photoelectrolysis of synthetic methyl paraben polluted wastewater. Separation and
411 Purification Technology 2019b; 208: 201-207.
412 Dionisio D, Santos LHE, Rodrigo MA, Motheo AJ. Electro-oxidation of methyl paraben on DSA
413 (R)-Cl-2: UV irradiation, mechanistic aspects and energy consumption. Electrochimica
414 Acta 2020; 338.
415 Farook S, Chian, E. S. N. ; Englebrecht, R. S., . Basic Concepts in Disinfection with Ozone.
416 Journal Water Pollution Control Federation 1977; 49.

417 Fernando Perez J, Llanos J, Saez C, Lopez C, Canzares P, Andres Rodrigo M. Towards the scale
418 up of a pressurized-jet microfluidic flow-through reactor for cost-effective electro-
419 generation of H₂O₂. *Journal of Cleaner Production* 2019; 211: 1259-1267.

420 Gad AAM, El-Tawel S. Effect of pre-oxidation by chlorine/permanganate on surface water
421 characteristics and algal toxins. *Desalination and Water Treatment* 2015; 57: 17922-
422 17934.

423 Guidelines for drinking-water quality neAtVH, criteria and other supporting information. World
424 Health Organization G, 1998. Guidelines for drinking-water quality. 2020, 1998.

425 He X, de la Cruz AA, Dionysiou DD. Destruction of cyanobacterial toxin cylindrospermopsin by
426 hydroxyl radicals and sulfate radicals using UV-254nm activation of hydrogen peroxide,
427 persulfate and peroxymonosulfate. *Journal of Photochemistry and Photobiology A:
428 Chemistry* 2013; 251: 160-166.

429 He X, Pelaez M, Westrick JA, O'Shea KE, Hiskia A, Triantis T, et al. Efficient removal of
430 microcystin-LR by UV-C/H₂O₂(2) in synthetic and natural water samples. *Water Res*
431 2012; 46: 1501-10.

432 Isidro J, Brackemeyer D, Saez C, Llanos J, Lobato J, Canzares P, et al. Operating the CabECO (R)
433 membrane electrolytic technology in continuous mode for the direct disinfection of
434 highly fecal-polluted water. *Separation and Purification Technology* 2019; 208: 110-
435 115.

436 Isidro J, Brackemeyer D, Saez C, Llanos J, Lobato J, Canzares P, et al. Electro-disinfection with
437 BDD-electrodes featuring PEM technology. *Separation and Purification Technology*
438 2020; 248.

439 Isidro J, Llanos J, Saez C, Brackemeyer D, Canzares P, Matthee T, et al. Can CabECO (R)
440 technology be used for the disinfection of highly faecal-polluted surface water?
441 *Chemosphere* 2018; 209: 346-352.

442 Laycock MV, Anderson DM, Naar J, Goodman A, Easy DJ, Donovan MA, et al. Laboratory
443 desalination experiments with some algal toxins. *Desalination* 2012; 293: 1-6.

444 Martinez-Huitle CA, Rodrigo MA, Sires I, Scialdone O. Single and Coupled Electrochemical
445 Processes and Reactors for the Abatement of Organic Water Pollutants: A Critical
446 Review. *Chemical Reviews* 2015; 115: 13362-13407.

447 Mascia M, Vacca A, Palmas S, Polcaro AM. Kinetics of the electrochemical oxidation of organic
448 compounds at BDD anodes: modelling of surface reactions. *Journal of Applied
449 Electrochemistry* 2007; 37: 71-76.

450 Mena IF, Cotillas S, Diaz E, Saez C, Rodriguez JJ, Canzares P, et al. Electrolysis with diamond
451 anodes: Eventually, there are refractory species! *Chemosphere* 2018; 195: 771-776.

452 Moraleda I, Cotillas S, Llanos J, Saez C, Canzares P, Pupunat L, et al. Can the substrate of the
453 diamond anodes influence on the performance of the electrosynthesis of oxidants?
454 *Journal of Electroanalytical Chemistry* 2019; 850.

455 Pavagadhi S, Tang AL, Sathishkumar M, Loh KP, Balasubramanian R. Removal of microcystin-LR
456 and microcystin-RR by graphene oxide: adsorption and kinetic experiments. *Water Res*
457 2013; 47: 4621-9.

458 Pelaez M, de la Cruz AA, Stathatos E, Falaras P, Dionysiou DD. Visible light-activated N-F-
459 codoped TiO₂ nanoparticles for the photocatalytic degradation of microcystin-LR in
460 water. *Catalysis Today* 2009; 144: 19-25.

461 Perez JF, Llanos J, Saez C, Lopez C, Canzares P, Rodrigo MA. Development of an innovative
462 approach for low-impact wastewater treatment: A microfluidic flow-through
463 electrochemical reactor. *Chemical Engineering Journal* 2018a; 351: 766-772.

464 Perez JF, Llanos J, Saez C, Lopez C, Canzares P, Rodrigo MA. The pressurized jet aerator: A new
465 aeration system for high-performance H₂O₂ electrolyzers. *Electrochemistry
466 Communications* 2018b; 89: 19-22.

467 Perez JF, Llanos J, Saez C, Lopez C, Canizares P, Rodrigo MA. On the design of a jet-aerated
468 microfluidic flow-through reactor for wastewater treatment by electro-Fenton.
469 Separation and Purification Technology 2019; 208: 123-129.

470 Pestana CJ, Edwards C, Prabhu R, Robertson PKJ, Lawton LA. Photocatalytic degradation of
471 eleven microcystin variants and nodularin by TiO₂ coated glass microspheres. J Hazard
472 Mater 2015; 300: 347-353.

473 Rajasekhar P, Fan L, Nguyen T, Roddick FA. A review of the use of sonication to control
474 cyanobacterial blooms. Water Res 2012; 46: 4319-29.

475 Seubert EL, Trussell S, Eagleton J, Schnetzer A, Cetinic I, Lauri P, et al. Algal toxins and reverse
476 osmosis desalination operations: laboratory bench testing and field monitoring of
477 domoic acid, saxitoxin, brevetoxin and okadaic acid. Water Res 2012; 46: 6563-73.

478 Sharma VK, Triantis TM, Antoniou MG, He X, Pelaez M, Han C, et al. Destruction of microcystins
479 by conventional and advanced oxidation processes: A review. Separation and
480 Purification Technology 2012; 91: 3-17.

481 Shi HX, Qu JH, Wang AM, Ge JT. Degradation of microcystins in aqueous solution with in situ
482 electrogenerated active chlorine. Chemosphere 2005; 60: 326-33.

483 Sirés I, Brillas E, Oturan MA, Rodrigo MA, Panizza M. Electrochemical advanced oxidation
484 processes: today and tomorrow. A review. Environmental Science and Pollution
485 Research 2014.

486 Souza FL, Rocha RS, Ferreira NG, Rodrigo MA, Lanza MRV. Effects of coupling hybrid processes
487 on the treatment of wastewater containing a commercial mixture of diuron and
488 hexazinone herbicides. Electrochimica Acta 2019; 328.

489 Souza FL, Saez C, Canizares P, Rodrigo MA. Improving photolytic treatments with
490 electrochemical technology. Separation and Purification Technology 2020a; 235.

491 Souza FL, Sáez C, Cañizares P, Rodrigo MA. Improving photolytic treatments with
492 electrochemical technology. Separation and Purification Technology 2020b; 235.

493 Velazquez-Pena S, Saez C, Canizares P, Linares-Hernandez I, Martinez-Miranda V, Barrera-Diaz
494 C, et al. Production of oxidants via electrolysis of carbonate solutions with conductive-
495 diamond anodes. Chemical Engineering Journal 2013; 230: 272-278.

496 Westrick JA, Szlag DC, Southwell BJ, Sinclair J. A review of cyanobacteria and cyanotoxins
497 removal/inactivation in drinking water treatment. Anal Bioanal Chem 2010; 397: 1705-
498 14.

499 Wood R. Acute animal and human poisonings from cyanotoxin exposure - A review of the
500 literature. Environ Int 2016; 91: 276-82.

501 Yu HJ. Progress of TiO₂ Photocatalytic Oxidation Technology in Algae Removal.
502 Advanced Materials Research 2013; 631-632: 246-253.

503 Zhang C, Fu D, Gu Z. Degradation of microcystin-RR using boron-doped diamond electrode. J
504 Hazard Mater 2009; 172: 847-53.

505 Şengül AB, Tüfekçi N, Aktan S. The use of alum as coagulant for removing cyanobacterial cells
506 in drinking water. Desalination and Water Treatment 2016; 57: 25610-25616.

507

508