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Title: THE SALINITY EFFECTS ON THE PERFORMANCE OF A CONSTRUCTED WETLAND-  
MICROBIAL FUEL CELL

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Abstract: The objective of the present work is to study the influence of the wastewater salinity concentration on the performance of a Constructed Wetland-Microbial Fuel Cell (CW-MFC) for simultaneous water pollution control and electricity generation. The work has been carried out under the hypothesis that increasing the salinity may improve the electricity production because of a lower internal ohmic resistance, although it could damage the microbiological processes or the plants. A pilot-scale horizontal subsurface flow CW, modified to function as an MFC, was operated under a continuous operation mode over five consecutive experimental periods of approximately 2 months each. The wastewater salinity was increased in each new period by steeply increasing the NaCl concentration in the synthetic wastewater from 0.51 to 9.51 g L<sup>-1</sup>. The CW-MFC performance was monitored during every stationary period. The increasing salinity first improved the cell voltage, and the resultant maximum voltage (130 mV) under continuous operation corresponded to a salinity concentration between 4 and 5 g L<sup>-1</sup>. However, subsequently higher salinity levels caused the opposite effect. The maximum voltage was obtained in an unstable condition, as microbiological inhibition in the anode zone appeared early, at approximate salinity levels of only 3 g L<sup>-1</sup>. Batch experiments confirmed the results, and higher cell voltage values up to 600 mV were obtained if longer retention times were allowed. The wetland plants (*Phragmites australis*) were only damaged at a salinity concentration of 9.51 g L<sup>-1</sup>.

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*Ecological Engineering*  
Editor

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Dear Editor:

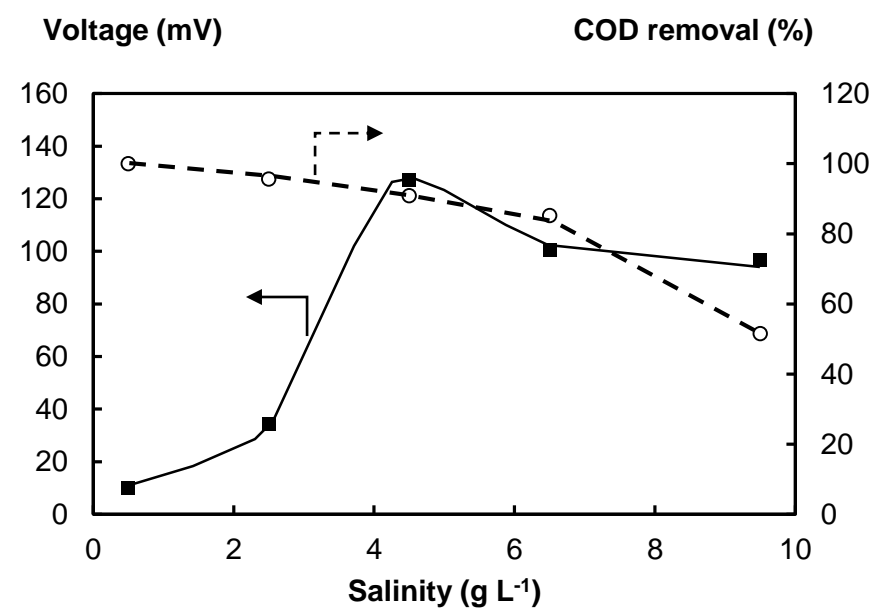
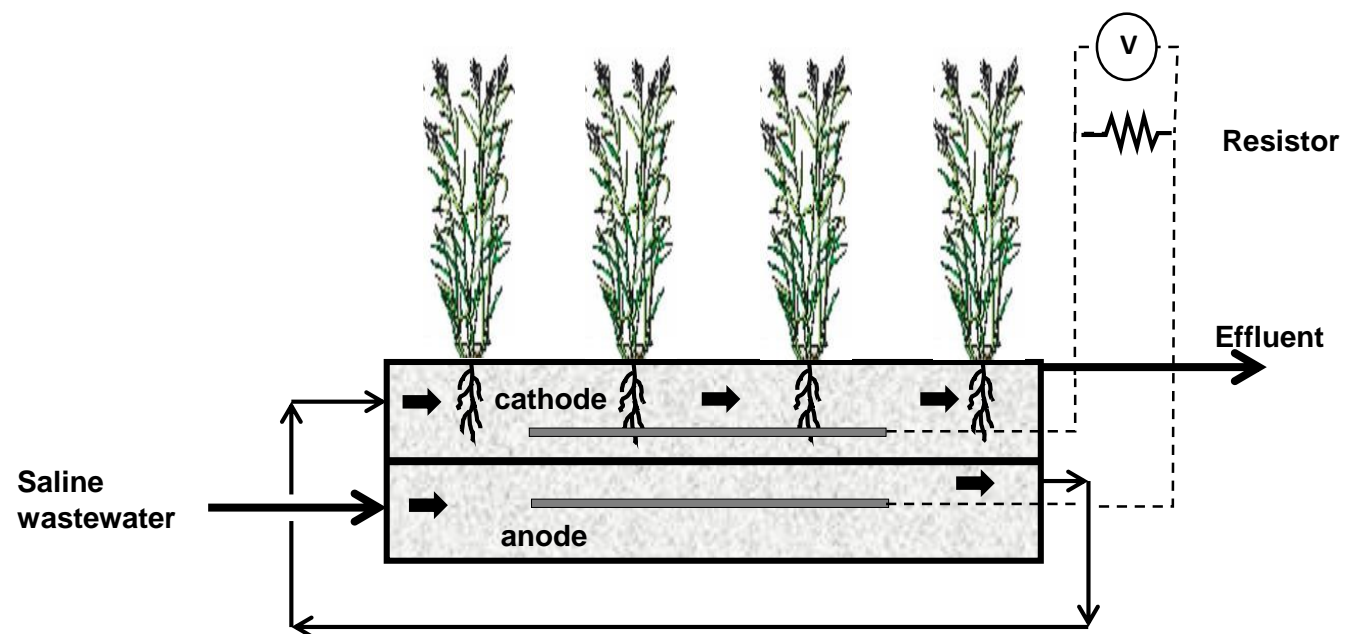
Attached you will find the REVISED manuscript ECOLENG-D-16-01038 "*The salinity effects on the performance of a constructed wetland-microbial fuel cell*", by José Villaseñor Camacho, Luis Rodríguez Romero, Carmen María Fernández Marchante, Francisco Jesús Fernández Morales and Manuel Andrés Rodrigo Rodrigo (corresponding author: jose.villasenor@uclm.es) in order to be reviewed for a possible publication as original research paper in *Ecological Engineering* (subject classification: Treatment wetlands).

The following items are included in the new submission:

- The "**Revised Manuscript**" (using MS Word).
- The "**Highlighted Revised manuscript**", that is the same revision manuscript MS Word file, using the track changes mode, where you can easily find the modifications made to the text.
- The "**Responses to reviewers**": One MS Word document containing the detailed answers to each concrete reviewer's comments. Each answer indicates the position of the modifications in the highlighted revised manuscript (MS Word file).
- Revised figure 3.

Yours sincerely

Dr. José Villaseñor Camacho



## Highlights

CW-MFCs are efficient devices used to treat wastewater and produce electricity

Salinity affects the performance of CW-MFCs

Microbiological inhibition effects can be observed at a salinity of 3 g L<sup>-1</sup>

Increasing salinity improved the cell voltage up to concentrations of 4 and 5 g L<sup>-1</sup>

Wetland plants (*Phragmites australis*) are only damaged at salinities over 9.5 g L<sup>-1</sup>

## Revision Notes: Response to Reviewers

This document shows detailed responses to the reviewer's comments. The responses indicate also the changes made in the revised manuscript. The changes are easily identifiable in the highlighted revised manuscript (revised manuscript changes marked document). The location of changes (page or line details in the responses) always refer to the highlighted revised manuscript MS Word file. Note that it is possible that the PDF generated by EES move lines.

### Reviewers' comments:

#### Reviewer #2:

The manuscript describes the performance of a pilot-scale constructed wetland-microbial fuel cell under salinities ranging from 0.5 to 9.5 mg/L. The manuscript is comprehensive and skilfully written. In my opinion, it can be published after considering the following points:

L117: Is the composition of such high salinity industrial wastewaters suitable for biological treatment? Is there sufficient organic matter present? Can the authors be more specific which industrial wastewater would be suitable for such treatment?

It is well known that high salinity can be inhibitory for biological processes. Indeed, as indicated in the abstract and introduction (line 89, original manuscript) we worked under the hypothesis of a biological damage because of increasing salinity levels, and one of the objectives of the work is to know the salinity limit that could be supported by the CW-MFC (also indicated in the original manuscript). This limit was experimentally confirmed and indicated in the discussion section and conclusions.

Regarding the organic matter concentration in wastewater, we chose an intermediate COD level (300 mgL-1) as we considered that it is sufficient concentration to perform our experimental study. COD was maintained constant in the whole experimental period. A brief sentence about this comment has been included in the revised manuscript (lines 160 - 162)

There are recent research studies about industrial wastewater treatment (including high salinity effluents) using both CW (Wu et al., 2015) and MFC (Gude, 2016). For instance, leachate from domestic landfills, or washing effluents from agro-food industries could be suitable for such combined CW-MFC technology. This information has been included in the introduction (lines 117-119)

Wu, S., Wallace, S., Brix, S., Kusch, P., Kirui, W.K., Masi, F., Dong, R., 2015. Treatment of industrial effluents in constructed wetlands: Challenges, operational strategies and overall performance. *Environ. Pollut.*, 201, 107-120.

Gude, V.G., 2016. Wastewater treatment in microbial fuel cells-an overview, *J. Cleaner Production*, 122, 287-307.

L172: 35 L d-1 instead of 35 l d-1

The change has been made (line 174 revised manuscript).

L269: "only accounts for" instead of "is only account for"

The change has been made (line 274 revised manuscript)

Figure 3: Is it possible to add error bars?

Figure 3a has been changed. Error bars for voltage measurements have been included in every period. Caption has been also changed.

L291: The cathode had a rather low DO (2 ppm). Would it be beneficial for the electricity generation to apply aeration in the cathode? Aeration is nowadays quite common in CWs.

Under the author's opinion, 2 ppm is high enough to ensure the aerobic environment in the cathode zone, and to maintain the necessary redox potential between anode and cathode (as indicated in the original manuscript line 292).

However, in the eventual case of a high organic loading, it would be possible that the organic matter could not be completely oxidized in the anode zone and it would cause depletion of DO in the cathode zone, producing anaerobic conditions which finally would cause MFC to stop working (see Villaseñor et al., 2013).

Thus, cathode aeration would be beneficial in such situation to maintain MFC working, but it must be considered also the aeration power consumption and costs in the global balance. This explanation has been included in the discussion section, lines 308-310 (revised manuscript).

L343 onwards: Could this explanation be simplified? Is the meaning that at higher salinity (4.5 mg/L) the system can obtain a higher maximum voltage but it takes longer to generate it than at lower salinity (2.5 mg/L)?

It is true, the final result is that under 4.5 mg/L it takes longer to generate voltage and (according to Figure 5b), the rate is lower. However, under the author's opinion, the reason of such behaviour must be discussed. Because of it, we stated in the original manuscript that using 4.5 mg/L is an unstable situation because of salt inhibition effects. The final sentence has been slightly modified in the revised manuscript (line 368).

L349: Could the authors summarize what the impact of these results is from practical point of view? Should one aim to obtain the highest maximum voltage or the highest average voltage generation rate? What should be the focus of further research?

According to the results, the authors considered that high salinity in industrial effluents could be a positive influence in the development of the CW-MFC technology as it improved voltage differences. However the challenge would be if halo-tolerant

microorganisms and plants could be adapted to these conditions, which may be the focus of further research.

This summary has been included at the end of discussion, line 388.

1 **THE SALINITY EFFECTS ON THE PERFORMANCE OF A CONSTRUCTED**  
2 **WETLAND-MICROBIAL FUEL CELL**

3

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19

20 **Abstract**

21 The objective of the present work is to study the influence of the wastewater salinity  
22 concentration on the performance of a Constructed Wetland-Microbial Fuel Cell (CW-  
23 MFC) for simultaneous water pollution control and electricity generation. The work has  
24 been carried out under the hypothesis that increasing the salinity may improve the



25 electricity production because of a lower internal ohmic resistance, although it could  
26 damage the microbiological processes or the plants. A pilot-scale horizontal subsurface  
27 flow CW, modified to function as an MFC, was operated under a continuous operation  
28 mode over five consecutive experimental periods of approximately 2 months each. The  
29 wastewater salinity was increased in each new period by steeply increasing the NaCl  
30 concentration in the synthetic wastewater from 0.51 to 9.51 g L<sup>-1</sup>. The CW-MFC  
31 performance was monitored during every stationary period. The increasing salinity first  
32 improved the cell voltage, and the resultant maximum voltage (130 mV) under  
33 continuous operation corresponded to a salinity concentration between 4 and 5 g L<sup>-1</sup>.  
34 However, subsequently higher salinity levels caused the opposite effect. The maximum  
35 voltage was obtained in an unstable condition, as microbiological inhibition in the  
36 anode zone appeared early, at approximate salinity levels of only 3 g L<sup>-1</sup>. Batch  
37 experiments confirmed the results, and higher cell voltage values up to 600 mV were  
38 obtained if longer retention times were allowed. The wetland plants (*Phragmites*  
39 *australis*) were only damaged at a salinity concentration of 9.51 g L<sup>-1</sup>.

40

#### 41 **Keywords**

42 Constructed Wetland; Microbial Fuel Cell; bioelectrogenic; salinity.

43

#### 44 **1. Introduction**

45 Microbial Fuel Cells (MFCs) are electrochemical devices that can obtain electricity  
46 from organic matter by means of the activity of bioelectrogenic microorganisms. As  
47 conventional fuel cells, they also have two chambers, with electrodes working under a  
48 difference of electric potential. However, what makes MFCs unique is the fact that

49 active microorganisms in the anode chamber are capable of oxidizing the organic matter  
50 using electric current instead of oxygen by various complementary mechanisms,  
51 becoming the real biological catalyst of the electrochemical device. MFCs have been  
52 extensively studied, and many scientific papers and books have been published in recent  
53 years. Because organic waste can be used as fuel for MFCs, this technology has been  
54 proposed for environmental remediation purposes, and the concept of  
55 bioelectrochemical wastewater treatment is currently receiving significant attention  
56 (Gude, 2016).

57 In this context, currently, a very promising variety of MFCs is being studied, consisting  
58 of integrating MFC technology into natural ecosystems or low-cost environmental  
59 remediation technologies. There are currently three of these technologies, including the  
60 Sediment Microbial Fuel Cells (SMFCs), also called Benthic MFCs; the Plant-type  
61 Microbial Fuel Cells (PMFCs); and MFCs coupled to Constructed Wetlands (CW-  
62 MFCs), and they all are based on the redox potential differences that naturally exist  
63 between the top water-air interface and the anaerobic bottom of these ecosystems. There  
64 is also a large amount of literature on the subject. All of these technologies have been  
65 described in a recent review (Fernández et al., 2015).

66 One of the most interesting options of these low-cost technologies for wastewater  
67 treatment are constructed wetlands (CWs). These systems are wetlands, isolated from  
68 the underground below them, that receive wastewater. Wastewater treatment in CWs is  
69 the result of a combination of natural physical, chemical, and biological phenomena  
70 (Zhi and Ji, 2012). There are different types of CWs; subsurface flow wetlands are one  
71 of the most implemented types (García et al., 2010). Basically, they consist of a  
72 wastewater subsurface flux flowing through a porous gravel bed, which includes

73 macrophyte plants growing on the top surface and a mixed microbial population in the  
74 form of biofilms attached to the gravel and roots.

75 The study of the combination of CWs and MFCs is recent. The first work was published  
76 by Yadav (2010), and although the number of papers is still low, it is increasing  
77 exponentially in the last 5 years (Doherty et al., 2015a). The works studied the influence  
78 of the type or concentration of the organic pollutants (Corbella et al., 2015; Fang et al.,  
79 2015; Liu et al., 2014; Srivastava et al., 2015; Wu et al., 2015a), the role of plants and  
80 the effect of the position of the roots (Corbella et al., 2014; Fang et al., 2013; Liu et al.,  
81 2014), the water flow configuration (Corbella et al., 2014; Corbella et al., 2015;  
82 Doherty et al., 2015b), the type of cathode (Liu et al., 2014; Srivastava et al., 2015) and  
83 the distance between the electrodes (Doherty et al., 2015b; Doherty et al., 2015c). The  
84 works usually aimed to improve the cell efficiency through maintaining a high redox  
85 potential between the electrodes and reducing the internal resistance.

86 To the authors' knowledge, wastewater salinity may be an important aspect influencing  
87 the CW-MFC performance, and its effect has not yet been studied. Initially, wastewater  
88 salinity is expected to have a contradictory effect on the two main processes (biological  
89 and electrochemical) occurring in the device: negative in the biological process and  
90 positive in the electrochemical process. Regarding the possible biological effects,  
91 constructed wetlands have been extensively applied for industrial wastewater treatment  
92 (Gao et al., 2015; Wu et al., 2015b), and there are some works focused on high salinity  
93 wastewater treatment by CWs (Gao et al., 2015; Karajić et al., 2010). Klomjek and  
94 Nitorisavut (2005) reported that some plant species used in CWs were adversely  
95 affected by high salinity in wastewater. Gao et al. (2015) tested twelve different plants  
96 species and detected a salinity level at which the treatment efficiency begins to fall.

97 Regarding the microbial role in wetlands, Gao et al. (2012) reported that the increase in  
98 salinity strongly reduced the microorganism concentration, while Lin et al. (2008)  
99 reported inhibition of the microbial activity.

100 Regarding the electrochemical performance, Logan (2008) and Rozendal et al. (2008)  
101 described the expected positive effect of increasing the wastewater salinity in an MFC  
102 and explained it in terms of the increase in the electrical conductivity of the electrolyte,  
103 which reduces the internal ohmic resistance and results in an ohmic drop of the fuel cell.  
104 However, they also stated the expected negative effect in the microbial activity at high  
105 salinity levels. Likewise, Lefebvre et al. (2012) reported increased power and decreased  
106 internal resistances using increasing salinity levels but found a drastic power reduction  
107 at a NaCl level of 20 g/L because of the inhibition of microbial growth.

108 In this context, it could be considered that the wastewater salinity could be an important  
109 factor to be tested in the performance of the combined CW-MFC system, and this paper  
110 aims to describe and discuss the results of the study of a pilot-scale CW-MFC treating  
111 wastewater with a steeply increasing salinity. Until now, this subject has not been  
112 tested, and it is hypothesized that a moderate salinity could produce a positive effect on  
113 the fuel cell performance, although it could also negatively affect the role of plants or  
114 microorganisms in the subsurface system. Because of the complexity of the CW-MFC  
115 mechanisms, the global effect and the salt tolerance limit are still unknown. The results  
116 could be of great relevance because of their potential applicability to the treatment of  
117 high salinity industrial wastewater. For instance, leachate from domestic landfills, or  
118 washing effluents from agro-food industries could be suitable for such combined CW-  
119 MFC technology.

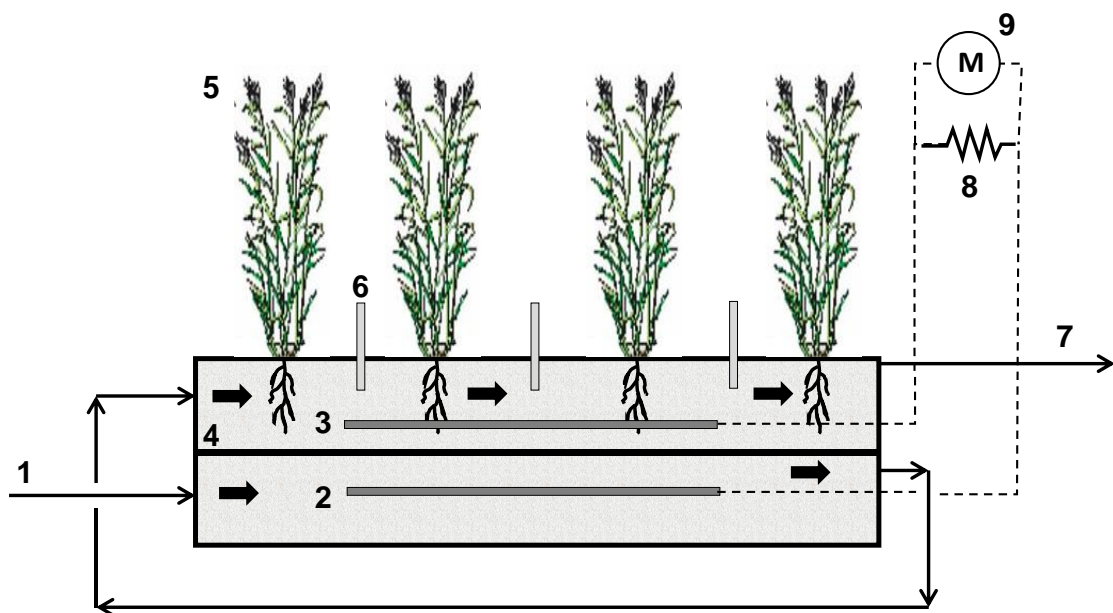
120

121 **2. Materials and Methods**

122 The materials, experimental procedures, and analytical methods have been described  
123 thoroughly elsewhere (Villaseñor et al., 2013; Villaseñor Camacho et al., 2014). The  
124 following subsections only describe the important details.

125 **2.1. Constructed wetland - microbial fuel cell microcosm.**

126 The experimental installation consisted of a pilot-scale horizontal subsurface flow CW  
127 for wastewater treatment, modified to function as an MFC (figure 1).



128

129

Figure 1

130 The installation was located in the greenhouse facility of the Institute for Chemical and  
131 Environmental Technology of the University of Castilla La Mancha, Ciudad Real  
132 (Spain). The wetland consisted of a 115 cm × 47 cm plastic channel with a bed depth of  
133 50 cm, and it was filled with gravel with an average particulate diameter of 9 mm and  
134 bed porosity of 0.4. Sampling points were placed along the wetland, and they made it  
135 possible to introduce temperature or dissolved oxygen probes. *Phragmites australis*,  
136 which was purchased from a commercial greenhouse, was planted in the wetland in

137 autumn 2011 (20 plants m<sup>-2</sup>), although this work was performed in the period February-  
138 October 2014, and the plants were completely developed during the experimental work.  
139 Regarding the MFC elements, rectangular (each was 70 cm × 15 cm and 3 cm thick)  
140 graphite plate electrodes were located in the gravel bed, and the distance between them  
141 was 26 cm. The anode plate was located 12 cm above the bottom of the wetland, and an  
142 identical graphite cathode plate was also located 12 cm below the wetland surface. Both  
143 electrodes were located in the subsurface water flow. The anode and cathode were  
144 connected by a 120 Ω resistor.

145 A 2-cm-thick layer of calcium bentonite (*Bentonil A*, from *Süid-Chemie*) separated the  
146 anode and cathode compartments in order to limit the growth of roots to the upper area  
147 only, where the cathode was located. The raw wastewater flow passed through the  
148 anode compartment, and subsequently, the outlet flow was pumped to the cathodic  
149 compartment via horizontal subsurface flow and finally left the wetland.

## 150 **2.2 Synthetic wastewater**

151 The synthetic domestic wastewater composition included glucose (175 mg L<sup>-1</sup>),  
152 CH<sub>3</sub>COONa·3H<sub>2</sub>O (175 mg L<sup>-1</sup>), NaHCO<sub>3</sub> (144 mg L<sup>-1</sup>), KH<sub>2</sub>PO<sub>4</sub> (58 mg L<sup>-1</sup>),  
153 MgCl<sub>2</sub>·6H<sub>2</sub>O (48 mg L<sup>-1</sup>), CaCl<sub>2</sub>·2H<sub>2</sub>O (39 mg L<sup>-1</sup>), (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> (146 mg L<sup>-1</sup>), and  
154 (NH<sub>4</sub>)<sub>2</sub>Fe(SO<sub>4</sub>)<sub>2</sub>·6H<sub>2</sub>O (109 mg L<sup>-1</sup>). The resulting main inlet wastewater parameters of  
155 this synthetic wastewater were as follows: total suspended solids (TSS): 0-5 mg L<sup>-1</sup>,  
156 chemical oxygen demand (COD): 300 mg L<sup>-1</sup>, inorganic salt concentration: 515 mg L<sup>-1</sup>,  
157 and electrical conductivity: 0.9 mS cm<sup>-1</sup>. Over the course of the experiment, the salinity  
158 concentrations were modified as described later in this paper. It was considered that the  
159 COD level was high enough, but not excessive, to perform the experimental study, and  
160 it was always maintained constant.

161 **2.3. Experimental procedure.**

162 A start-up period was not necessary because the wetland had been continuously  
163 working since autumn 2011, using synthetic wastewater (Villaseñor Camacho et al.,  
164 2014). The wetland worked under a continuous operation mode over five consecutive  
165 experimental periods of approximately 2 months each. The wastewater salinity was  
166 increased in each new period by increasing the NaCl concentration in the synthetic  
167 wastewater. The salinity was the only variable under study, so all the others parameters  
168 were kept constant. The CW-MFC performance was monitored during every stationary  
169 period. Also, a batch experiment was performed at the end of each period by stopping  
170 the water flow during 9 days. Table 1 shows the NaCl concentration, the total inorganic  
171 salt concentration and the electrical conductivity of the wastewater used in every period.  
172 A constant wastewater flow of 35 L d<sup>-1</sup> was used to maintain a hydraulic residence time  
173 of 2.75 days (except at the end of each period in which the batch experiment was  
174 performed). The wastewater pH was always maintained at approximately 7.4 by means  
175 of the buffer capacity of the synthetic medium, and the air-conditioning system  
176 available in the greenhouse maintained the room temperature between 19 and 27°C.

177

178 Table 1. Salinity concentration and wastewater conductivity during the consecutive  
179 experimental periods.

Period	NaCl added to wastewater (g L <sup>-1</sup> )	Total inorganic salt concentration (g L <sup>-1</sup> )	Average electrical conductivity (mS cm <sup>-1</sup> )
I	0	0.51	0.9
II	2	2.51	4.7
III	4	4.51	9.1
IV	6	6.51	11.7
V	9	9.51	15.1

180 **2.4. Sampling, analysis, and electrochemical monitoring.**

181 The whole system was monitored twice every week. Samples of the influent and  
182 effluents of the two electrode compartments were taken, and the soluble COD, TSS and  
183 volatile suspended solids (VSS) concentrations were analysed in the laboratory  
184 according to standard methods (A.P.H.A., 1998). The dissolved oxygen (DO) level in  
185 the anodic compartment was measured in the anodic effluent, and the DO was also  
186 measured in the cathodic compartment *in situ* using the sampling points. The DO was  
187 measured using a YSI-5000 dissolved oxygen probe. The potentials between the edges  
188 of the external resistance were continuously monitored by a multimeter in order to  
189 continuously monitor the value of the cell potential.

190

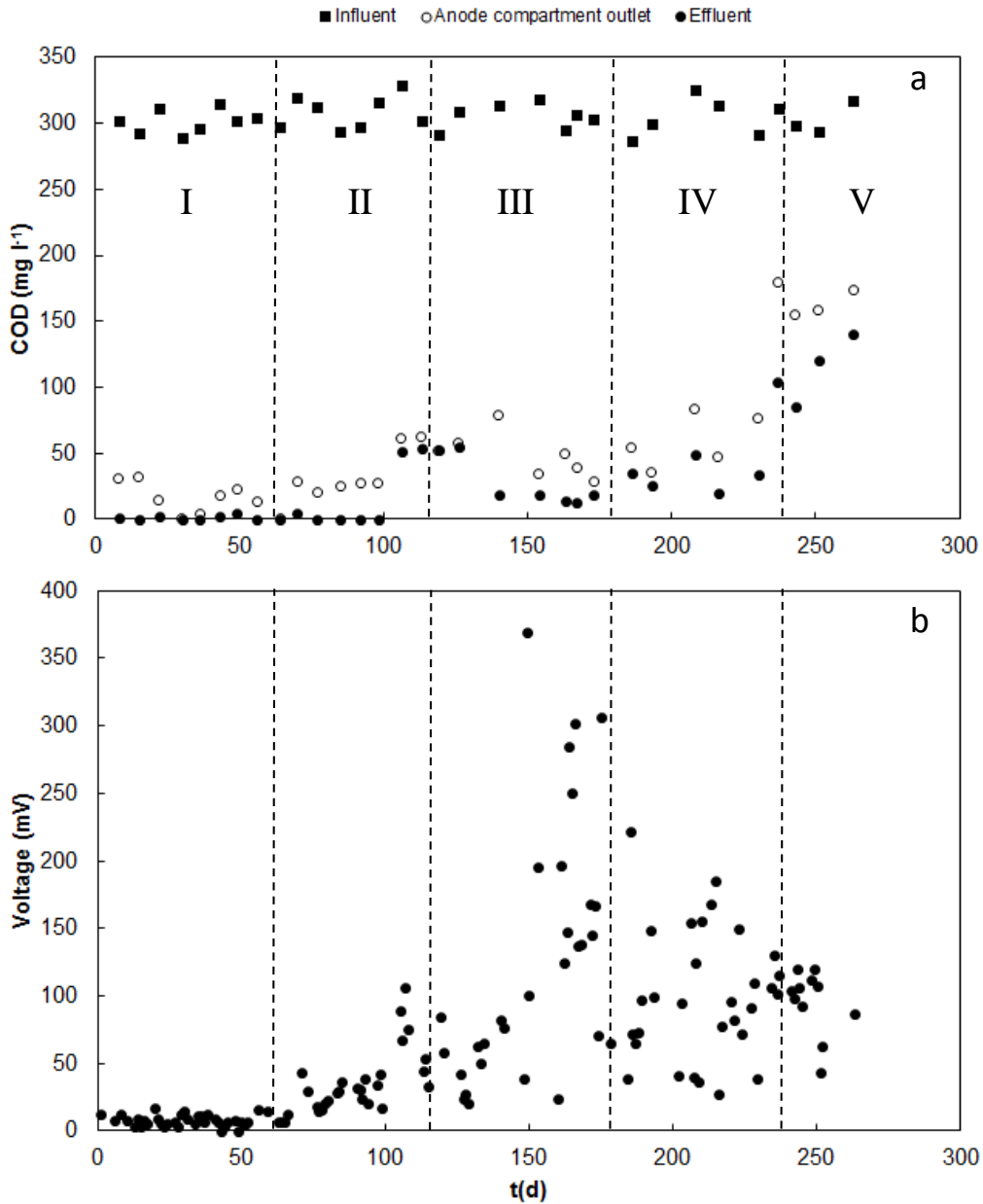
191 **3. Results and Discussion**

192 Figure 2 shows the changes in the performance of the CW-MFC over the five periods of  
193 study, for which increasing salinity (with step disturbances) was fed to the  
194 bioelectrochemical device. The COD and cell voltage were monitored in order to  
195 determine the changes in performance of the CW-MFC. COD, the first parameter,  
196 describes the operation of the device as an environmental remediation technology, while  
197 the cell voltage describes its performance as an energy production technology.

198 The CW-MFC functioned for over approximately 2 months in the first experimental  
199 period, showing stationary and stable performance. As expected, the wastewater  
200 treatment results were successful. The soluble COD at the anode compartment outlet  
201 was approximately 25 ppm, while the soluble COD concentration at the cathode  
202 compartment outlet (the final effluent) was negligible. The VSS concentration in the  
203 effluent varied between 0 and 10 ppm, and this variation was caused by the probable



204 detachment and drag of organic material from inside the wetland because the VSS  
205 concentration of the inlet wastewater was negligible.



206

207

Figure 2.

208 From an electrochemical point of view, the CW also worked as an MFC over period I,

209 and it generated electricity. However, the voltage values monitored were not as high as

210 expected (average cell voltage was 10 mV with a load of 120 ohm), in particular when

211 this result is compared with the results obtained in previous operation periods, for which

212 the wetland worked under very similar conditions. At this point, it is important to note  
213 that the CW-MFC had been operating uninterrupted for more than three years. Thus,  
214 over the first stationary operation period (2012), the CW-MFC generated approximately  
215 18 mV per unit of the influent wastewater organic loading rate ( $\text{g}_{\text{COD}} \text{m}^{-2} \text{d}^{-1}$ )  
216 (Villaseñor et al., 2013), and over the second operation period (2013), it generated  
217 approximately 13 mV per unit of the organic loading rate (Villaseñor Camacho et al.,  
218 2014). The results shown in the present work (obtained over the 3<sup>rd</sup> year of continuous  
219 operation) reached only 0.6 mV per unit of the organic loading rate. Thus, the MFC  
220 efficiency strongly decreased over three years, although a high wastewater treatment  
221 efficiency remained. Some previous research suggested that it is important to study the  
222 long-term performance of these types of MFCs based on natural ecosystems. The  
223 decrease in the efficiency has been previously related to the deterioration of the cathode  
224 (Zhang et al., 2012) or to the clogging phenomena in the cathode zone (Zhang et al.,  
225 2011). It must be noted that clogging is one of the classical problems associated with  
226 the long-term operation of subsurface constructed wetlands (García et al., 2010). The  
227 reasons for such a low efficiency are unknown, although the system showed stable  
228 operation, which is necessary for continued study in this work.

229 Figure 2a shows the COD concentrations in the inlet wastewater, the anode  
230 compartment outlet and the cathode compartment outlet (final effluent) over the  
231 consecutive step disturbances as a function of the value of the salinity. The increase in  
232 salinity between periods I and II (from 0.51 to 2.51  $\text{g L}^{-1}$ ) was observed to cause a slight  
233 decrease in the efficiency of the anodic oxidation of the organic matter, but the COD  
234 concentration in the final effluent remained negligible. Moreover, an increasing  
235 progressive deterioration can be observed in the anodic oxidation in periods III to V, but

236 in this case, it adversely affected the final effluent COD concentrations as the values  
237 measured were increasingly higher. This observation points out the influence of the  
238 salinity on the metabolic activity of the microorganisms and that high values of the  
239 salinity negatively affect the application of CW as environmental remediation  
240 technology. Therefore, high salinity values should be prevented in order to assure a  
241 good performance with regards to wastewater treatment.

242 Figure 2b shows the cell voltages (120 ohm resistance) generated by the CW-MFC over  
243 the entire experimental period. The cell voltage increased as the wastewater salinity  
244 increased. Although there were some variability and fluctuations in the data, a clear  
245 increasing trend was observed until the end of period III (150 d). However, the  
246 fluctuations became very large from that point onwards. High cell voltages were  
247 observed, although they were unstable. Instability would be probably associated with  
248 the declining performance of the microbial metabolism caused by the higher salinity.  
249 Finally, a clear decreasing trend was observed in the last period (marked as V).

250

251 Figure 3a summarizes the average values of the cell voltage measured during each  
252 period of this experimental study and the “electrogenic ratio”, that is, the percentage of  
253 the COD consumed by bioelectrogenic microorganisms. The electrogenic ratio is  
254 calculated by eq. 1.  $r_{\text{COD-electrogenic}}$  is the COD consumption rate by bioelectrogenic  
255 microorganisms and is calculated by eq. 2, where  $j$  is the current density,  $A$  is the anode  
256 area,  $n$  is the number of electrons donated per mol of COD consumed, and  $F$  is the  
257 Faraday constant.  $r_{\text{COD}}$  is the total COD consumption rate at the anode outlet, which can  
258 be calculated by the mass balance shown in eq. 3, which takes into account the flow-

259 pattern of the CW-MFC, where  $q$  is the volumetric flow rate. Figure 3b shows the  
260 values calculated by equations 2 and 3.

$$261 \quad \text{electrogenic ratio (\%)} = (r_{\text{COD-electrogenic}}/r_{\text{COD}}) \cdot 100 \quad (1)$$

$$262 \quad r_{\text{COD-electrogenic}} = (jA/4F) \quad (2)$$

$$263 \quad q\text{COD}_{in} - q\text{COD}_{out} + r_{\text{COD}} \cdot V = V(d\text{COD}/dt) \quad (3)$$

264

265 Figure 3b shows that the  $r_{\text{COD-electrogenic}}$  increased when the salinity increased from 0.5 to  
266  $4.5 \text{ g L}^{-1}$ , and almost remained unchanged up to  $9.5 \text{ g L}^{-1}$ , while the  $r_{\text{COD}}$  decreased with  
267 increase in salinity, resulting in high electrogenic ratio at high salinity levels. It seems  
268 that the electrogens could be more tolerant to salinity increase than other COD  
269 degradation microorganisms. Moreover, the percentage  $r_{\text{COD-electrogenic}}$  only accounts for a  
270 small part of the COD removal, indicating that the MFC functioning would not be well  
271 established in the test CW-MFC system.

272 Taking all these points into account, figure 3a shows that the best electric current  
273 generation result (130 mV) was obtained when using a wastewater salinity  
274 concentration between 4 and  $5 \text{ g L}^{-1}$ . Regarding the efficiency in the use of the COD by  
275 electrogenic microorganisms, figure 3a also shows an optimal salinity between 4 and 5  
276  $\text{g L}^{-1}$ . Upward of these concentrations, the efficiency of the degradation of the COD in  
277 the anode decreases (figure 3b). This phenomenon caused a relatively high percentage  
278 for the electrogenic ratio (figure 3a, using  $9.51 \text{ g L}^{-1}$  salinity), but as will be discussed  
279 later, the authors consider that this is not a stable condition.

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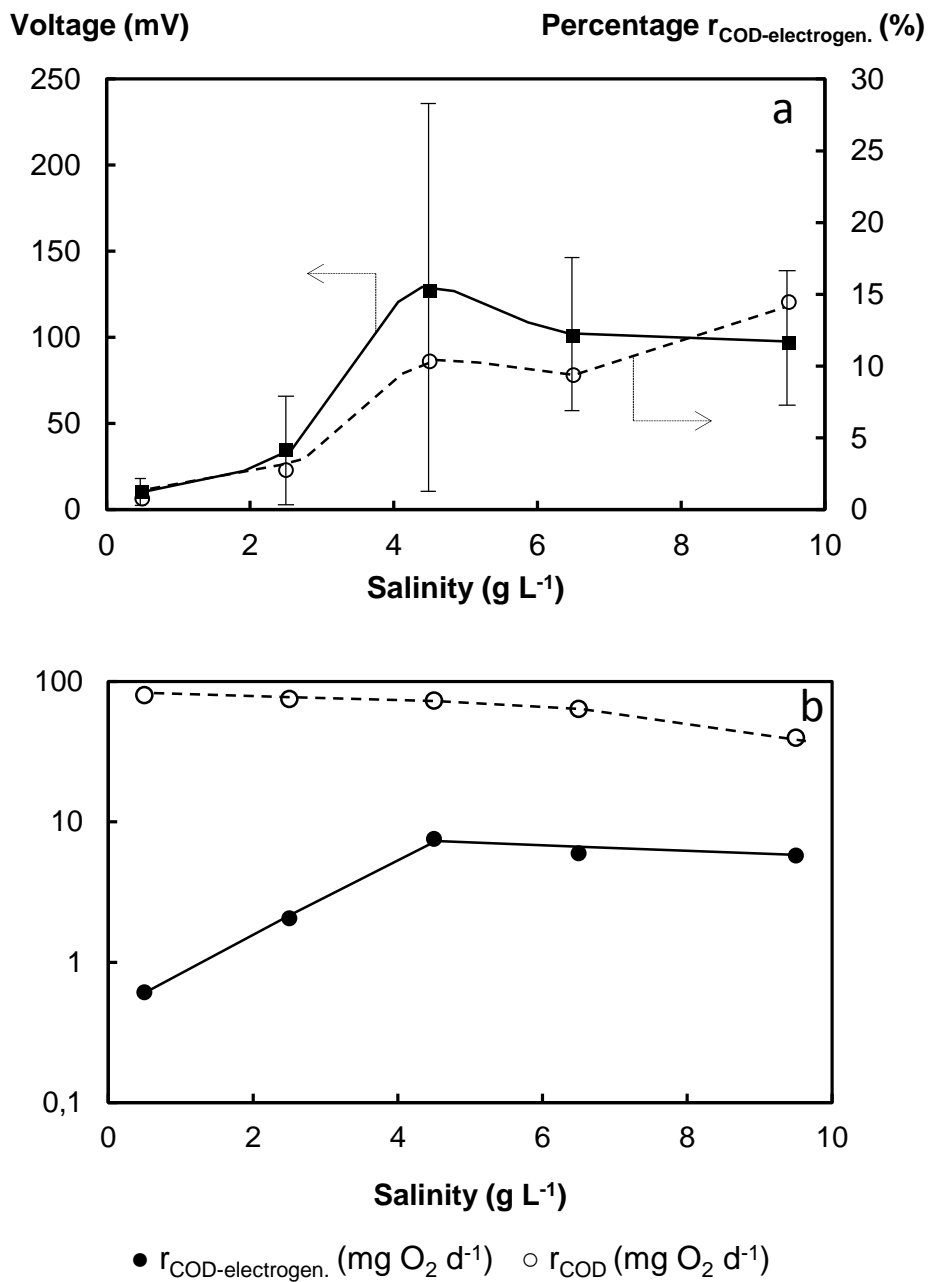


Figure 3

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286 Figure 4 shows the time-course of the dissolved oxygen and VSS concentrations at the

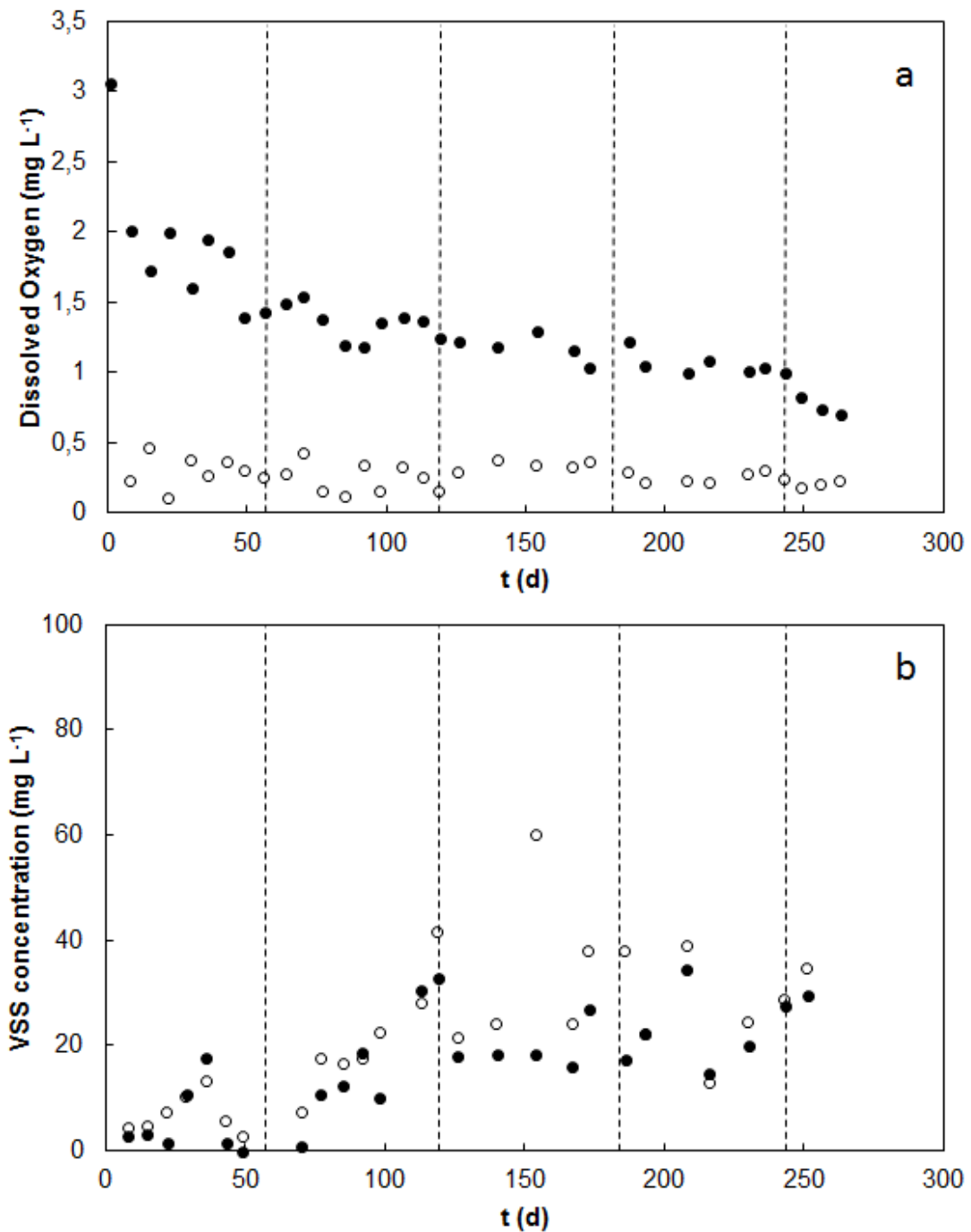
287 outlet of the anode and cathode compartments over the five stages. As expected, the

288 anode compartment worked under nearly completely anaerobic conditions, while the

289 cathode compartment showed concentrations very close to 2 ppm, which are similar to  
290 the DO concentrations previously reported in this system (Villaseñor et al., 2013). This  
291 condition ensures enough oxygen for the proper operation of the cathode reduction  
292 process. Subsequently, a continuous DO concentration decrease was observed as the  
293 salinity increased. There may be several reasons for this decline, such as the decrease of  
294 oxygen solubility in water or a negative impact in the plants' growth and, hence, a  
295 decrease in the roots' aeration potential. However, according to the COD profile  
296 observed in figure 2a, it may be hypothesized that the DO level decreased because of  
297 the salinity inhibitory effect on the anode microbiological performance, as the organic  
298 matter was not completely oxidized, and it produced an oxygen demand in the cathode  
299 compartment. Thus, the aeration potential of the plants would not be high enough to  
300 replace the oxygen consumption. Then, cathode aeration could be beneficial in such  
301 situation to maintain DO level and so maintain MFC working, but it must be considered  
302 also the aeration power consumption and costs in the global balance.

303 Figure 4b shows a progressive increase in the VSS concentration in the outlet of both  
304 compartments, especially in period II. The VSS could be related to the detachment  
305 phenomenon, which is usually associated with the deterioration of a biofilm due to the  
306 inhibition of microbial growth. It is assumed again that the inhibition occurred in the  
307 anode zone because both VSS profiles were very similar, and sometimes, even higher  
308 VSS concentrations were measured at the outlet of the anode compartment.

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Figure 4

314 Some previous works have reported the influence of high salinity levels on the  
 315 performance of CWs or MFCs. Regarding MFCs, Lefebvre et al. (2012) tested an MFC  
 316 treating wastewater under high NaCl concentrations. They observed a decrease in the  
 317 internal ohmic resistance and an increase in the electric power generation, but they also

318 found problems in the anodic biological process. They concluded that the antagonistic  
319 effect of NaCl on the anolyte conductivity and biofilm growth made bioelectricity  
320 production advantageous at salinity concentrations of up to 20 g L<sup>-1</sup> of NaCl, but the  
321 inhibition of anodophilic microorganisms began at a concentration of 10 g L<sup>-1</sup> NaCl. Liu  
322 et al. (2005) tested an MFC using NaCl concentrations of up to 400 mM, and the  
323 electric power generation always increased. They estimated that the maximum  
324 concentration of NaCl at which the microbial growth inhibition would occur is  
325 approximately 3%. Regarding CWs, there are some works that reported salinity  
326 inhibition of the microbial processes inside the wetland (Gao et al., 2012; Lin et al.,  
327 2008). Regarding the possible negative impact of the high salinity on the plants, in the  
328 present work, only a clear deterioration during the last period has been observed, that is,  
329 under 9.51 g L<sup>-1</sup> of salt. Different macrophyte plants in constructed wetlands treating  
330 high salinity wastewater have been tested in previous reported works. Gao et al. (2012)  
331 tested 12 different plants and observed that high salinity damaged their growth and  
332 decreased their nutrient uptake capacity and aeration potential in the roots zone.  
333 However, *Phragmites australis* was the most resistant species, and it functioned  
334 correctly up to a salt concentration of 20 g L<sup>-1</sup>.  
335 According to our results and previous research, it is assumed that higher salinity levels  
336 would reduce the internal ohmic resistance and, thus, increase the electric power  
337 generation, although there is a maximum admissible level for plants and  
338 microorganisms. The maximum level is between 4 and 5 g L<sup>-1</sup> under the continuous  
339 operation mode. However, lower salt concentrations (approximately 3 g L<sup>-1</sup>) begin to  
340 damage the anodic biological process. We assumed that the role of the plants remained  
341 constant, and plant damage was only observed from salinity concentrations of 9.51 g L<sup>-1</sup>



342 and higher. The electric power generation under  $9.51 \text{ g L}^{-1}$  is high, although we consider  
343 that this condition is unstable.

344 Figure 5a shows the results of the batch experiments performed at the end of each  
345 continuous period. The wastewater inflow was stopped in the batch experiments in  
346 order to allow enough retention time to oxidize the organic matter in the anode  
347 compartment. A voltage increase up to a maximum value can be observed in every  
348 experiment, and subsequently, there is a decrease until the “fuel” is depleted. Figure 5b  
349 shows the maximum cell voltage measured and the average voltage generation rate  
350 (calculated from the beginning to the maximum value). The figure also shows that the  
351 positive effect of the salinity increases as higher voltage differences are measured until  
352 the salt concentration reaches  $4.51 \text{ g L}^{-1}$ . Above this concentration, the maximum  
353 voltage decreases. Additionally, it can be observed that the voltage values are much  
354 higher than the values obtained under continuous operation, and this result suggests that  
355 higher retention times would be advisable. Figure 5b shows that the higher voltage  
356 generation rate corresponds to a relatively low salinity concentration of  $2.51 \text{ g L}^{-1}$ ,  
357 although the maximum cell voltage ( $600 \text{ mV}$ ) corresponds to  $4.51 \text{ g L}^{-1}$ . This result  
358 would confirm the results obtained under continuous operation; that is, under  $4.51 \text{ g L}^{-1}$ ,  
359 it is possible to obtain transiently higher potential differences in the MFC, although it  
360 takes longer to generate electricity because it is an unstable condition, as the  
361 microbiological process would begin to deteriorate at a concentration of approximately  
362  $3 \text{ g L}^{-1}$ .

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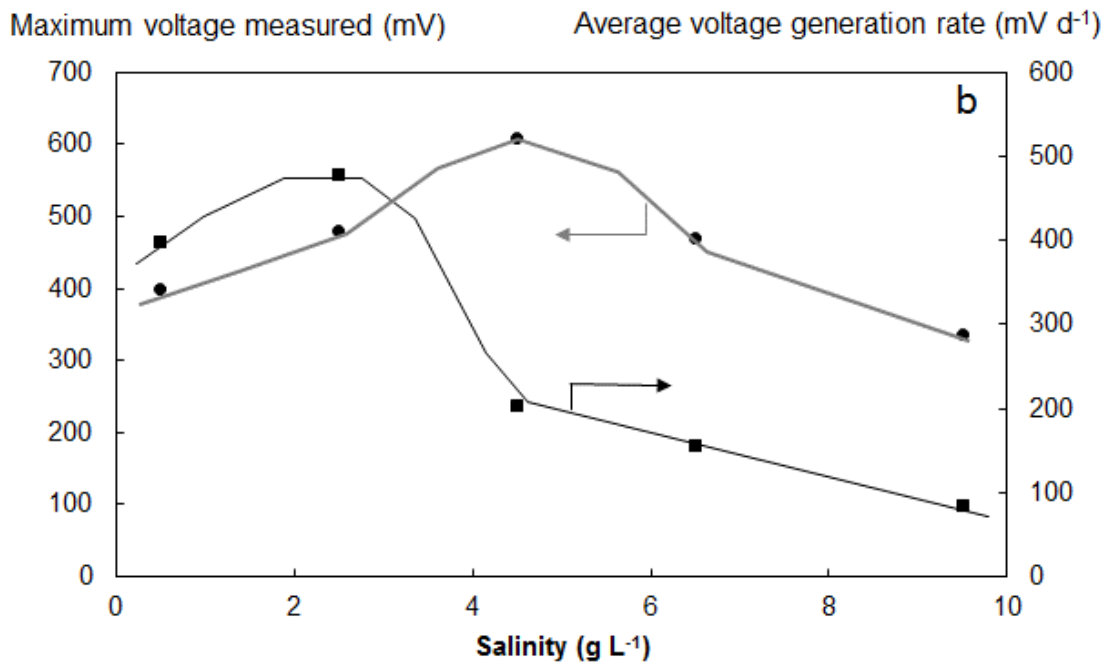
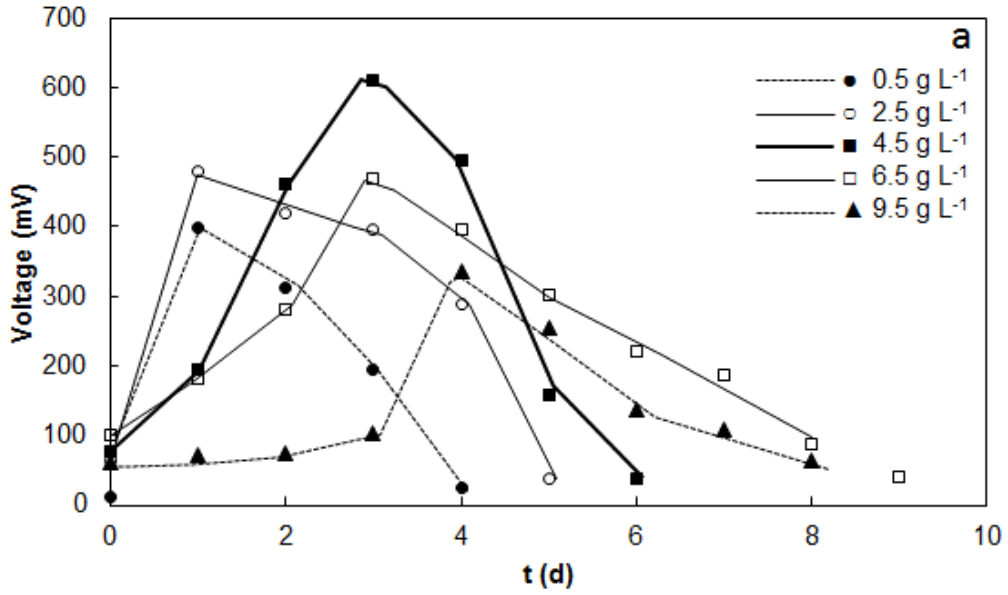


Figure 5

370 From the results in the present work, it could be argued that the CW-MFC would  
371 improve the electric power generation while treating wastewater with high salinity,  
372 although there is a maximum salt level that first inhibits the microbial process. Later,  
373 the salt level damages the plants' performance. Some researchers proved previously that  
374 it is possible to use halotolerant plant species (Webb et al., 2012) or to inoculate  
375 halotolerant microorganisms (Karajić et al., 2010) in CWs. Regarding MFC, Monzon et  
376 al. (2015) proposed using extreme halophilic microbes. The authors of the present work  
377 consider that the application of such halotolerant microbes and plants could allow for  
378 the application of CW-MFC to simultaneously treat high salinity industrial wastewater  
379 and produce electricity.

380 According to these results, the authors considered that high salinity in industrial  
381 effluents could be a positive influence in the development of the CW-MFC technology  
382 as it improved voltage differences. However the challenge would be if halo-tolerant  
383 microorganisms and plants could be adapted to these conditions, which may be the  
384 focus of further research.

385

#### 386 **4. Conclusions**

387 The increasing salinity first improved the cell voltage under continuous operation, and  
388 the maximum voltage corresponded to a salinity concentration between 4 and 5 g L<sup>-1</sup>,  
389 while subsequently higher salinity levels caused the opposite effect. However,  
390 according to the COD, DO and VSS measurements, microbiological inhibition in the  
391 anode zone appeared early at an approximate salinity of 3 g L<sup>-1</sup>. The batch experiments  
392 confirmed this behaviour. The wetland plants remained without apparent damage up to  
393 salinity levels of 9.51 g L<sup>-1</sup>.

394 **Acknowledgements**

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512 Figure 1. Experimental installation. (1) Wastewater feeding; (2) Anode; (3) Cathode; (4)  
513 Bentonite layer; (5) Reed plants; (6) Sampling points; (7) Treated effluent; (8)  
514 Resistance; and (9) Multimeter.

515

516

517 Figure 2. Influent and effluent COD concentrations (a) and voltage generation (b)  
518 during the entire experimental period.

519

520

521 Figure 3. (a) Average voltage generation values and error bars, and percentage of the  
522 COD consumed by bioelectrogenic microorganisms in the MFC depending on the  
523 salinity of the wastewater and (b) the total and electrogenic COD consumption rates.

524

525

526 Figure 4. Dissolved oxygen concentrations (a) and VSS concentrations (b) in the anode  
527 ( $\circ$ ) and the cathode ( $\bullet$ ) effluents.

528

529

530 Figure 5. Cell voltage generated (a) and the maximum and average cell voltage change  
531 rates (b) in the batch experiments.

532

1 **THE SALINITY EFFECTS ON THE PERFORMANCE OF A CONSTRUCTED**  
2 **WETLAND-MICROBIAL FUEL CELL**

3

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19

20 **Abstract**

21 The objective of the present work is to study the influence of the wastewater salinity  
22 concentration on the performance of a Constructed Wetland-Microbial Fuel Cell (CW-  
23 MFC) for simultaneous water pollution control and electricity generation. The work has  
24 been carried out under the hypothesis that increasing the salinity may improve the

25 electricity production because of a lower internal ohmic resistance, although it could  
26 damage the microbiological processes or the plants. A pilot-scale horizontal subsurface  
27 flow CW, modified to function as an MFC, was operated under a continuous operation  
28 mode over five consecutive experimental periods of approximately 2 months each. The  
29 wastewater salinity was increased in each new period by steeply increasing the NaCl  
30 concentration in the synthetic wastewater from 0.51 to 9.51 g L<sup>-1</sup>. The CW-MFC  
31 performance was monitored during every stationary period. The increasing salinity first  
32 improved the cell voltage, and the resultant maximum voltage (130 mV) under  
33 continuous operation corresponded to a salinity concentration between 4 and 5 g L<sup>-1</sup>.  
34 However, subsequently higher salinity levels caused the opposite effect. The maximum  
35 voltage was obtained in an unstable condition, as microbiological inhibition in the  
36 anode zone appeared early, at approximate salinity levels of only 3 g L<sup>-1</sup>. Batch  
37 experiments confirmed the results, and higher cell voltage values up to 600 mV were  
38 obtained if longer retention times were allowed. The wetland plants (*Phragmites*  
39 *australis*) were only damaged at a salinity concentration of 9.51 g L<sup>-1</sup>.

40

#### 41 **Keywords**

42 Constructed Wetland; Microbial Fuel Cell; bioelectrogenic; salinity.

43

#### 44 **1. Introduction**

45 Microbial Fuel Cells (MFCs) are electrochemical devices that can obtain electricity  
46 from organic matter by means of the activity of bioelectrogenic microorganisms. As  
47 conventional fuel cells, they also have two chambers, with electrodes working under a  
48 difference of electric potential. However, what makes MFCs unique is the fact that

49 active microorganisms in the anode chamber are capable of oxidizing the organic matter  
50 using electric current instead of oxygen by various complementary mechanisms,  
51 becoming the real biological catalyst of the electrochemical device. MFCs have been  
52 extensively studied, and many scientific papers and books have been published in recent  
53 years. Because organic waste can be used as fuel for MFCs, this technology has been  
54 proposed for environmental remediation purposes, and the concept of  
55 bioelectrochemical wastewater treatment is currently receiving significant attention  
56 (Gude, 2016).

57 In this context, currently, a very promising variety of MFCs is being studied, consisting  
58 of integrating MFC technology into natural ecosystems or low-cost environmental  
59 remediation technologies. There are currently three of these technologies, including the  
60 Sediment Microbial Fuel Cells (SMFCs), also called Benthic MFCs; the Plant-type  
61 Microbial Fuel Cells (PMFCs); and MFCs coupled to Constructed Wetlands (CW-  
62 MFCs), and they all are based on the redox potential differences that naturally exist  
63 between the top water-air interface and the anaerobic bottom of these ecosystems. There  
64 is also a large amount of literature on the subject. All of these technologies have been  
65 described in a recent review (Fernández et al., 2015).

66 One of the most interesting options of these low-cost technologies for wastewater  
67 treatment are constructed wetlands (CWs). These systems are wetlands, isolated from  
68 the underground below them, that receive wastewater. Wastewater treatment in CWs is  
69 the result of a combination of natural physical, chemical, and biological phenomena  
70 (Zhi and Ji, 2012). There are different types of CWs; subsurface flow wetlands are one  
71 of the most implemented types (García et al., 2010). Basically, they consist of a  
72 wastewater subsurface flux flowing through a porous gravel bed, which includes

73 macrophyte plants growing on the top surface and a mixed microbial population in the  
74 form of biofilms attached to the gravel and roots.

75 The study of the combination of CWs and MFCs is recent. The first work was published  
76 by Yadav (2010), and although the number of papers is still low, it is increasing  
77 exponentially in the last 5 years (Doherty et al., 2015a). The works studied the influence  
78 of the type or concentration of the organic pollutants (Corbella et al., 2015; Fang et al.,  
79 2015; Liu et al., 2014; Srivastava et al., 2015; Wu et al., 2015a), the role of plants and  
80 the effect of the position of the roots (Corbella et al., 2014; Fang et al., 2013; Liu et al.,  
81 2014), the water flow configuration (Corbella et al., 2014; Corbella et al., 2015;  
82 Doherty et al., 2015b), the type of cathode (Liu et al., 2014; Srivastava et al., 2015) and  
83 the distance between the electrodes (Doherty et al., 2015b; Doherty et al., 2015c). The  
84 works usually aimed to improve the cell efficiency through maintaining a high redox  
85 potential between the electrodes and reducing the internal resistance.

86 To the authors' knowledge, wastewater salinity may be an important aspect influencing  
87 the CW-MFC performance, and its effect has not yet been studied. Initially, wastewater  
88 salinity is expected to have a contradictory effect on the two main processes (biological  
89 and electrochemical) occurring in the device: negative in the biological process and  
90 positive in the electrochemical process. Regarding the possible biological effects,  
91 constructed wetlands have been extensively applied for industrial wastewater treatment  
92 (Gao et al., 2015; Wu et al., 2015b), and there are some works focused on high salinity  
93 wastewater treatment by CWs (Gao et al., 2015; Karajić et al., 2010). Klomjek and  
94 Nitorisavut (2005) reported that some plant species used in CWs were adversely  
95 affected by high salinity in wastewater. Gao et al. (2015) tested twelve different plants  
96 species and detected a salinity level at which the treatment efficiency begins to fall.

97 Regarding the microbial role in wetlands, Gao et al. (2012) reported that the increase in  
98 salinity strongly reduced the microorganism concentration, while Lin et al. (2008)  
99 reported inhibition of the microbial activity.

100 Regarding the electrochemical performance, Logan (2008) and Rozendal et al. (2008)  
101 described the expected positive effect of increasing the wastewater salinity in an MFC  
102 and explained it in terms of the increase in the electrical conductivity of the electrolyte,  
103 which reduces the internal ohmic resistance and results in an ohmic drop of the fuel cell.  
104 However, they also stated the expected negative effect in the microbial activity at high  
105 salinity levels. Likewise, Lefebvre et al. (2012) reported increased power and decreased  
106 internal resistances using increasing salinity levels but found a drastic power reduction  
107 at a NaCl level of 20 g/L because of the inhibition of microbial growth.

108 In this context, it could be considered that the wastewater salinity could be an important  
109 factor to be tested in the performance of the combined CW-MFC system, and this paper  
110 aims to describe and discuss the results of the study of a pilot-scale CW-MFC treating  
111 wastewater with a steeply increasing salinity. Until now, this subject has not been  
112 tested, and it is hypothesized that a moderate salinity could produce a positive effect on  
113 the fuel cell performance, although it could also negatively affect the role of plants or  
114 microorganisms in the subsurface system. Because of the complexity of the CW-MFC  
115 mechanisms, the global effect and the salt tolerance limit are still unknown. The results  
116 could be of great relevance because of their potential applicability to the treatment of  
117 high salinity industrial wastewater. For instance, leachate from domestic landfills, or  
118 washing effluents from agro-food industries could be suitable for such combined CW-  
119 MFC technology.  
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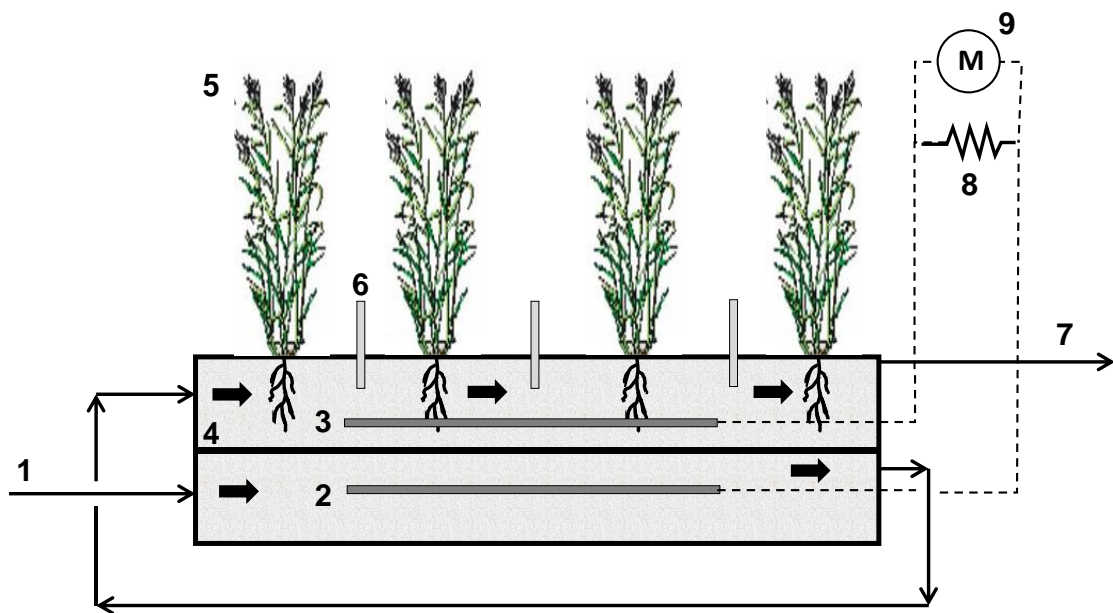
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## 123 2. Materials and Methods

124 The materials, experimental procedures, and analytical methods have been described  
125 thoroughly elsewhere (Villaseñor et al., 2013; Villaseñor Camacho et al., 2014). The  
126 following subsections only describe the important details.

### 127 2.1. Constructed wetland - microbial fuel cell microcosm.

128 The experimental installation consisted of a pilot-scale horizontal subsurface flow CW  
129 for wastewater treatment, modified to function as an MFC (figure 1).



130

131

Figure 1

132 The installation was located in the greenhouse facility of the Institute for Chemical and  
133 Environmental Technology of the University of Castilla La Mancha, Ciudad Real  
134 (Spain). The wetland consisted of a 115 cm × 47 cm plastic channel with a bed depth of  
135 50 cm, and it was filled with gravel with an average particulate diameter of 9 mm and  
136 bed porosity of 0.4. Sampling points were placed along the wetland, and they made it

137 possible to introduce temperature or dissolved oxygen probes. *Phragmites australis*,  
138 which was purchased from a commercial greenhouse, was planted in the wetland in  
139 autumn 2011 (20 plants m<sup>-2</sup>), although this work was performed in the period February-  
140 October 2014, and the plants were completely developed during the experimental work.  
141 Regarding the MFC elements, rectangular (each was 70 cm × 15 cm and 3 cm thick)  
142 graphite plate electrodes were located in the gravel bed, and the distance between them  
143 was 26 cm. The anode plate was located 12 cm above the bottom of the wetland, and an  
144 identical graphite cathode plate was also located 12 cm below the wetland surface. Both  
145 electrodes were located in the subsurface water flow. The anode and cathode were  
146 connected by a 120 Ω resistor.

147 A 2-cm-thick layer of calcium bentonite (*Bentonil A*, from *Süd-Chemie*) separated the  
148 anode and cathode compartments in order to limit the growth of roots to the upper area  
149 only, where the cathode was located. The raw wastewater flow passed through the  
150 anode compartment, and subsequently, the outlet flow was pumped to the cathodic  
151 compartment via horizontal subsurface flow and finally left the wetland.

## 152 **2.2 Synthetic wastewater**

153 The synthetic domestic wastewater composition included glucose (175 mg L<sup>-1</sup>),  
154 CH<sub>3</sub>COONa·3H<sub>2</sub>O (175 mg L<sup>-1</sup>), NaHCO<sub>3</sub> (144 mg L<sup>-1</sup>), KH<sub>2</sub>PO<sub>4</sub> (58 mg L<sup>-1</sup>),  
155 MgCl<sub>2</sub>·6H<sub>2</sub>O (48 mg L<sup>-1</sup>), CaCl<sub>2</sub>·2H<sub>2</sub>O (39 mg L<sup>-1</sup>), (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> (146 mg L<sup>-1</sup>), and  
156 (NH<sub>4</sub>)<sub>2</sub>Fe(SO<sub>4</sub>)<sub>2</sub>·6H<sub>2</sub>O (109 mg L<sup>-1</sup>). The resulting main inlet wastewater parameters of  
157 this synthetic wastewater were as follows: total suspended solids (TSS): 0-5 mg L<sup>-1</sup>,  
158 chemical oxygen demand (COD): 300 mg L<sup>-1</sup>, inorganic salt concentration: 515 mg L<sup>-1</sup>,  
159 and electrical conductivity: 0.9 mS cm<sup>-1</sup>. Over the course of the experiment, the salinity  
160 concentrations were modified as described later in this paper. It was considered that the



161 | COD level was high enough, but not excessive, to perform the experimental study, and  
162 | it was always maintained constant.

165 | **2.3. Experimental procedure.**

166 | A start-up period was not necessary because the wetland had been continuously  
167 | working since autumn 2011, using synthetic wastewater (Villaseñor Camacho et al.,  
168 | 2014). The wetland worked under a continuous operation mode over five consecutive  
169 | experimental periods of approximately 2 months each. The wastewater salinity was  
170 | increased in each new period by increasing the NaCl concentration in the synthetic  
171 | wastewater. The salinity was the only variable under study, so all the others parameters  
172 | were kept constant. The CW-MFC performance was monitored during every stationary  
173 | period. Also, a batch experiment was performed at the end of each period by stopping  
174 | the water flow during 9 days. Table 1 shows the NaCl concentration, the total inorganic  
175 | salt concentration and the electrical conductivity of the wastewater used in every period.  
176 | A constant wastewater flow of 35  $\text{L d}^{-1}$  was used to maintain a hydraulic residence time  
177 | of 2.75 days (except at the end of each period in which the batch experiment was  
178 | performed). The wastewater pH was always maintained at approximately 7.4 by means  
179 | of the buffer capacity of the synthetic medium, and the air-conditioning system  
180 | available in the greenhouse maintained the room temperature between 19 and 27°C.

181 |  
182 | Table 1. Salinity concentration and wastewater conductivity during the consecutive  
183 | experimental periods.

---

Period	NaCl added to	Total inorganic salt	Average electrical
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	wastewater (g L <sup>-1</sup> )	concentration (g L <sup>-1</sup> )	conductivity (mS cm <sup>-1</sup> )
I	0	0.51	0.9
II	2	2.51	4.7
III	4	4.51	9.1
IV	6	6.51	11.7
V	9	9.51	15.1

184 **2.4. Sampling, analysis, and electrochemical monitoring.**

185 The whole system was monitored twice every week. Samples of the influent and  
186 effluents of the two electrode compartments were taken, and the soluble COD, TSS and  
187 volatile suspended solids (VSS) concentrations were analysed in the laboratory  
188 according to standard methods (A.P.H.A., 1998). The dissolved oxygen (DO) level in  
189 the anodic compartment was measured in the anodic effluent, and the DO was also  
190 measured in the cathodic compartment *in situ* using the sampling points. The DO was  
191 measured using a YSI-5000 dissolved oxygen probe. The potentials between the edges  
192 of the external resistance were continuously monitored by a multimeter in order to  
193 continuously monitor the value of the cell potential.

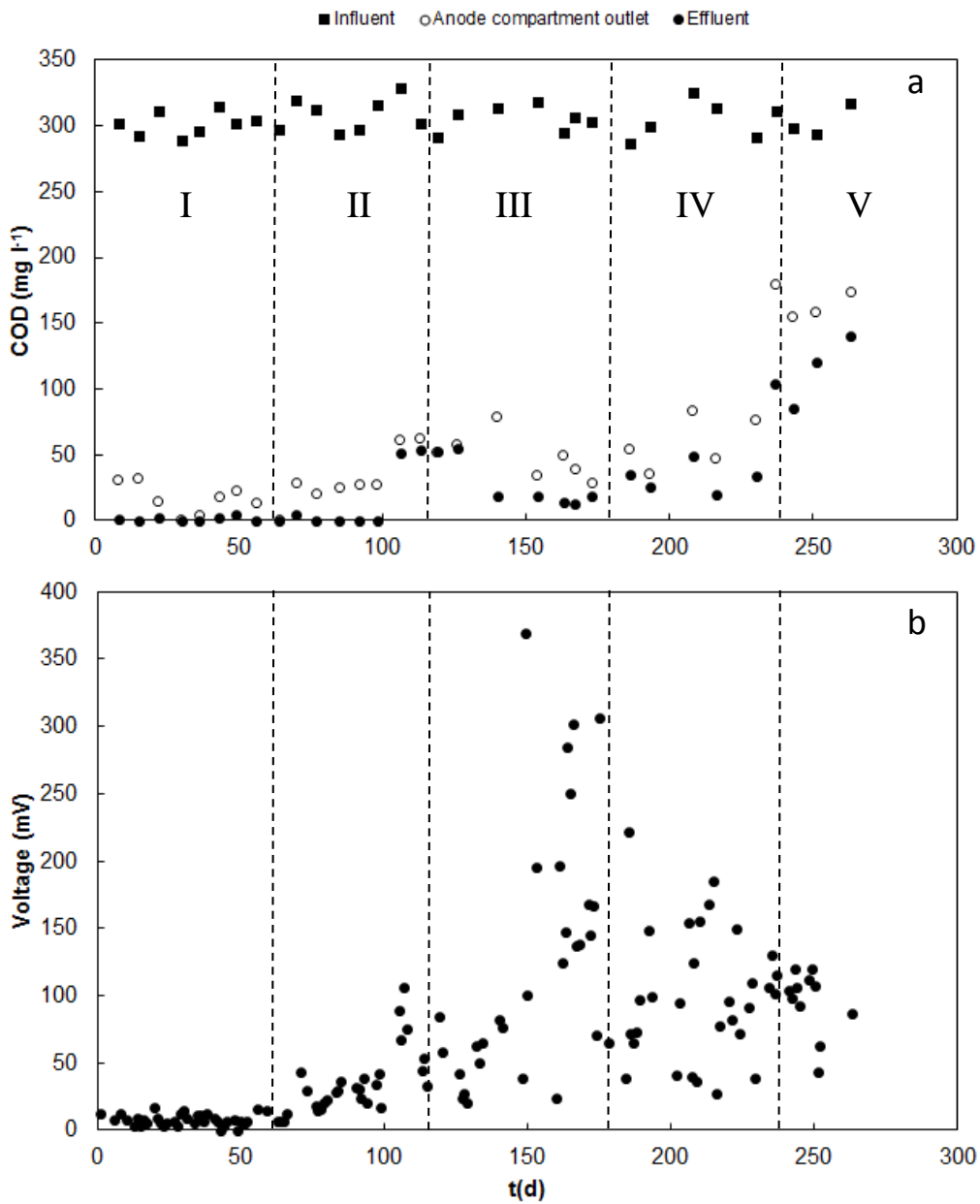
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195 **3. Results and Discussion**

196 Figure 2 shows the changes in the performance of the CW-MFC over the five periods of  
197 study, for which increasing salinity (with step disturbances) was fed to the  
198 bioelectrochemical device. The COD and cell voltage were monitored in order to  
199 determine the changes in performance of the CW-MFC. COD, the first parameter,  
200 describes the operation of the device as an environmental remediation technology, while  
201 the cell voltage describes its performance as an energy production technology.

202 The CW-MFC functioned for over approximately 2 months in the first experimental  
203 period, showing stationary and stable performance. As expected, the wastewater

204 treatment results were successful. The soluble COD at the anode compartment outlet  
205 was approximately 25 ppm, while the soluble COD concentration at the cathode  
206 compartment outlet (the final effluent) was negligible. The VSS concentration in the  
207 effluent varied between 0 and 10 ppm, and this variation was caused by the probable  
208 detachment and drag of organic material from inside the wetland because the VSS  
209 concentration of the inlet wastewater was negligible.



210

211

Figure 2.

212 From an electrochemical point of view, the CW also worked as an MFC over period I,  
213 and it generated electricity. However, the voltage values monitored were not as high as  
214 expected (average cell voltage was 10 mV with a load of 120 ohm), in particular when  
215 this result is compared with the results obtained in previous operation periods, for which  
216 the wetland worked under very similar conditions. At this point, it is important to note  
217 that the CW-MFC had been operating uninterrupted for more than three years. Thus,  
218 over the first stationary operation period (2012), the CW-MFC generated approximately  
219 18 mV per unit of the influent wastewater organic loading rate ( $g_{\text{COD}} \text{ m}^{-2} \text{ d}^{-1}$ )  
220 (Villaseñor et al., 2013), and over the second operation period (2013), it generated  
221 approximately 13 mV per unit of the organic loading rate (Villaseñor Camacho et al.,  
222 2014). The results shown in the present work (obtained over the 3<sup>rd</sup> year of continuous  
223 operation) reached only 0.6 mV per unit of the organic loading rate. Thus, the MFC  
224 efficiency strongly decreased over three years, although a high wastewater treatment  
225 efficiency remained. Some previous research suggested that it is important to study the  
226 long-term performance of these types of MFCs based on natural ecosystems. The  
227 decrease in the efficiency has been previously related to the deterioration of the cathode  
228 (Zhang et al., 2012) or to the clogging phenomena in the cathode zone (Zhang et al.,  
229 2011). It must be noted that clogging is one of the classical problems associated with  
230 the long-term operation of subsurface constructed wetlands (García et al., 2010). The  
231 reasons for such a low efficiency are unknown, although the system showed stable  
232 operation, which is necessary for continued study in this work.

233 Figure 2a shows the COD concentrations in the inlet wastewater, the anode  
234 compartment outlet and the cathode compartment outlet (final effluent) over the  
235 consecutive step disturbances as a function of the value of the salinity. The increase in

236 salinity between periods I and II (from 0.51 to 2.51 g L<sup>-1</sup>) was observed to cause a slight  
237 decrease in the efficiency of the anodic oxidation of the organic matter, but the COD  
238 concentration in the final effluent remained negligible. Moreover, an increasing  
239 progressive deterioration can be observed in the anodic oxidation in periods III to V, but  
240 in this case, it adversely affected the final effluent COD concentrations as the values  
241 measured were increasingly higher. This observation points out the influence of the  
242 salinity on the metabolic activity of the microorganisms and that high values of the  
243 salinity negatively affect the application of CW as environmental remediation  
244 technology. Therefore, high salinity values should be prevented in order to assure a  
245 good performance with regards to wastewater treatment.

246 Figure 2b shows the cell voltages (120 ohm resistance) generated by the CW-MFC over  
247 the entire experimental period. The cell voltage increased as the wastewater salinity  
248 increased. Although there were some variability and fluctuations in the data, a clear  
249 increasing trend was observed until the end of period III (150 d). However, the  
250 fluctuations became very large from that point onwards. High cell voltages were  
251 observed, although they were unstable. Instability would be probably associated with  
252 the declining performance of the microbial metabolism caused by the higher salinity.  
253 Finally, a clear decreasing trend was observed in the last period (marked as V).

254

255 Figure 3a summarizes the average values of the cell voltage measured during each  
256 period of this experimental study and the “electrogenic ratio”, that is, the percentage of  
257 the COD consumed by bioelectrogenic microorganisms. The electrogenic ratio is  
258 calculated by eq. 1.  $r_{\text{COD-electrogenic}}$  is the COD consumption rate by bioelectrogenic  
259 microorganisms and is calculated by eq. 2, where  $j$  is the current density,  $A$  is the anode

260 area,  $n$  is the number of electrons donated per mol of COD consumed, and  $F$  is the  
 261 Faraday constant.  $r_{COD}$  is the total COD consumption rate at the anode outlet, which can  
 262 be calculated by the mass balance shown in eq. 3, which takes into account the flow-  
 263 pattern of the CW-MFC, where  $q$  is the volumetric flow rate. Figure 3b shows the  
 264 values calculated by equations 2 and 3.

$$265 \quad \text{electrogenic ratio (\%)} = (r_{COD-electrogenic}/r_{COD}) \cdot 100 \quad (1)$$

$$266 \quad r_{COD-electrogenic} = (jA/4F) \quad (2)$$

$$267 \quad qCOD_{in} - qCOD_{out} + r_{COD} \cdot V = V(dCOD/dt) \quad (3)$$

268

269 Figure 3b shows that the  $r_{COD-electrogenic}$  increased when the salinity increased from 0.5 to  
 270  $4.5 \text{ g L}^{-1}$ , and almost remained unchanged up to  $9.5 \text{ g L}^{-1}$ , while the  $r_{COD}$  decreased with  
 271 increase in salinity, resulting in high electrogenic ratio at high salinity levels. It seems  
 272 that the electrogens could be more tolerant to salinity increase than other COD  
 273 degradation microorganisms. Moreover, the percentage  $r_{COD-electrogenic}$  is only accounts for  
 274 a small part of the COD removal, indicating that the MFC functioning would not be  
 275 well established in the test CW-MFC system.

276 Taking all these points into account, figure 3a shows that the best electric current  
 277 generation result (130 mV) was obtained when using a wastewater salinity  
 278 concentration between 4 and  $5 \text{ g L}^{-1}$ . Regarding the efficiency in the use of the COD by  
 279 electrogenic microorganisms, figure 3a also shows an optimal salinity between 4 and 5  
 280  $\text{g L}^{-1}$ . Upward of these concentrations, the efficiency of the degradation of the COD in  
 281 the anode decreases (figure 3b). This phenomenon caused a relatively high percentage

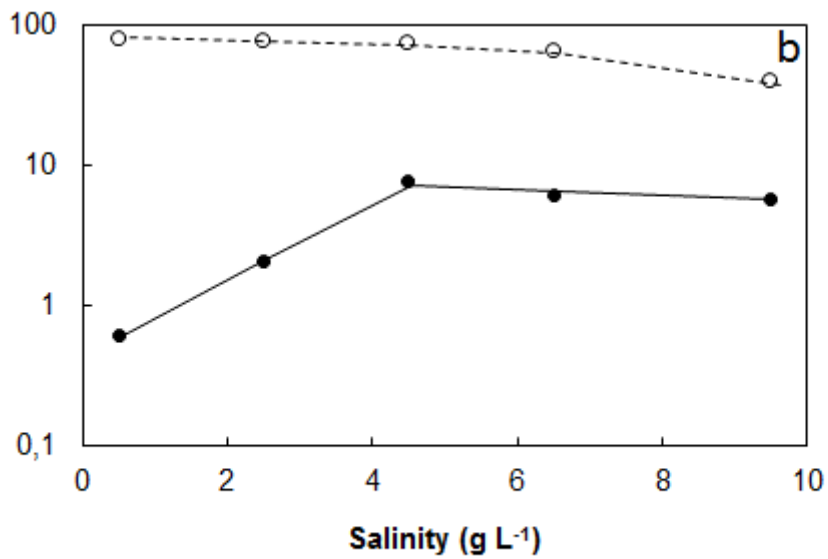
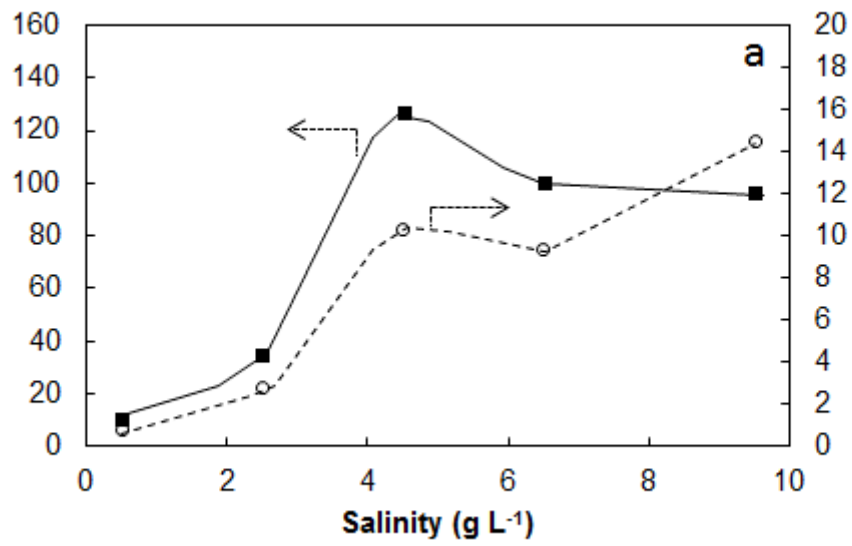
282 for the electrogenic ratio (figure 3a, using  $9.51 \text{ g L}^{-1}$  salinity), but as will be discussed  
283 later, the authors consider that this is not a stable condition.

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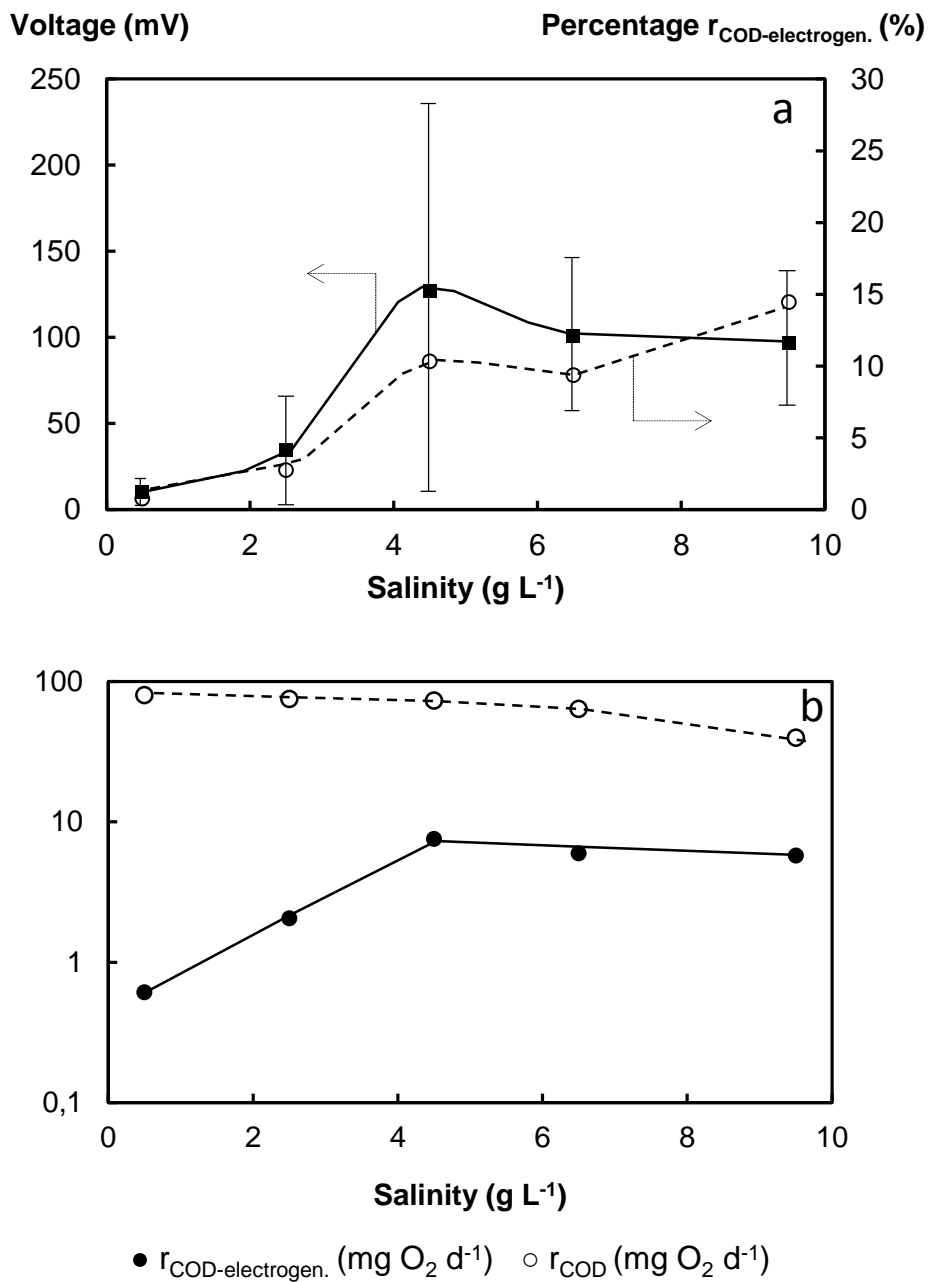
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**Voltage (mV)** **Percentage  $r_{\text{COD-electrogen.}}$  (%)**



●  $r_{\text{COD-electrogen.}}$  (mg O<sub>2</sub> d<sup>-1</sup>) ○  $r_{\text{COD}}$  (mg O<sub>2</sub> d<sup>-1</sup>)





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292 Figure 4 shows the time-course of the dissolved oxygen and VSS concentrations at the

293 outlet of the anode and cathode compartments over the five stages. As expected, the

294 anode compartment worked under nearly completely anaerobic conditions, while the

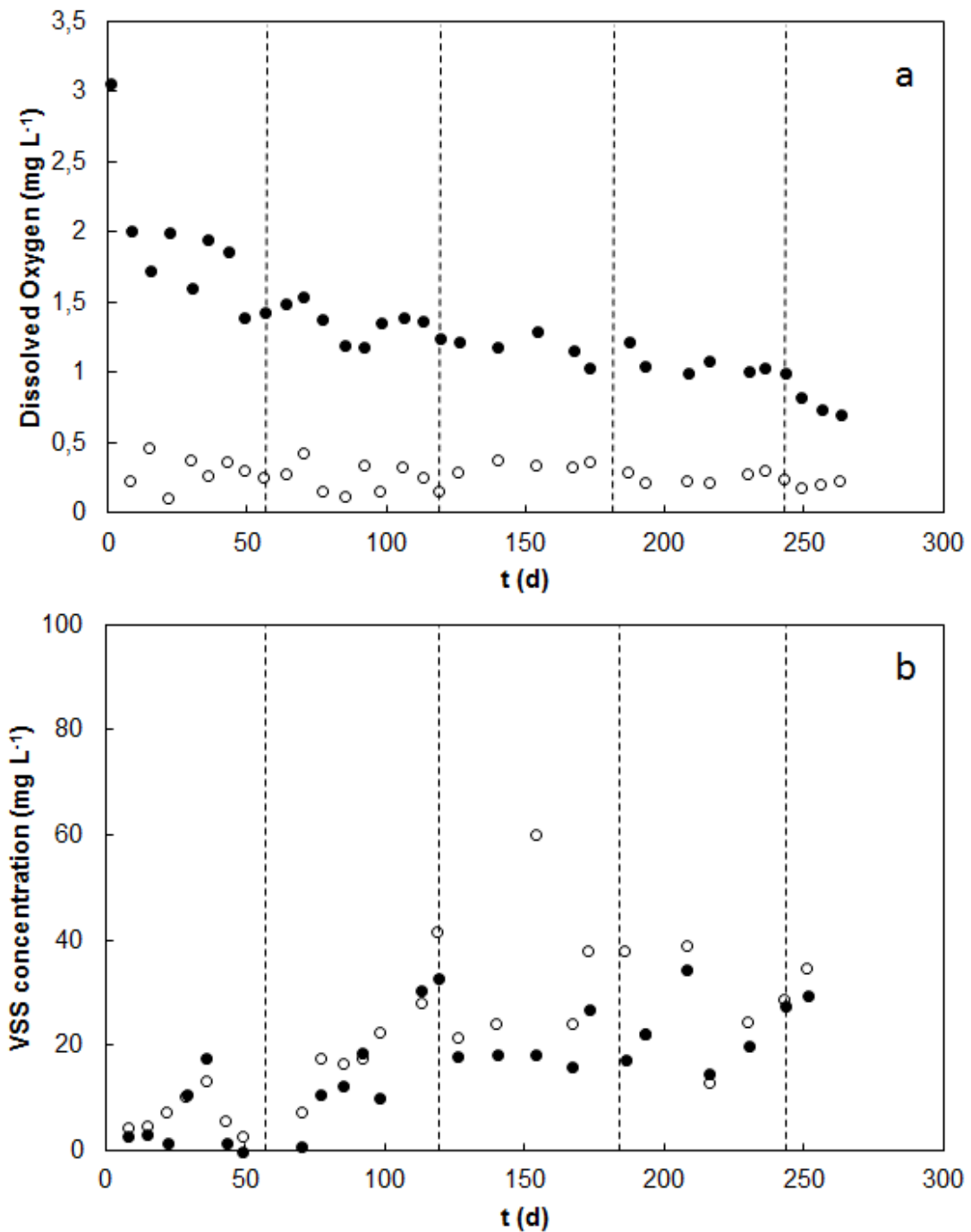
295 cathode compartment showed concentrations very close to 2 ppm, which are similar to  
296 the DO concentrations previously reported in this system (Villaseñor et al., 2013). This  
297 condition ensures enough oxygen for the proper operation of the cathode reduction  
298 process. Subsequently, a continuous DO concentration decrease was observed as the  
299 salinity increased. There may be several reasons for this decline, such as the decrease of  
300 oxygen solubility in water or a negative impact in the plants' growth and, hence, a  
301 decrease in the roots' aeration potential. However, according to the COD profile  
302 observed in figure 2a, it may be hypothesized that the DO level decreased because of  
303 the salinity inhibitory effect on the anode microbiological performance, as the organic  
304 matter was not completely oxidized, and it produced an oxygen demand in the cathode  
305 compartment. Thus, the aeration potential of the plants would not be high enough to  
306 replace the oxygen consumption. Then, cathode aeration could be beneficial in such  
307 situation to maintain DO level and so maintain MFC working, but it must be considered  
308 also the aeration power consumption and costs in the global balance.

309 Figure 4b shows a progressive increase in the VSS concentration in the outlet of both  
310 compartments, especially in period II. The VSS could be related to the detachment  
311 phenomenon, which is usually associated with the deterioration of a biofilm due to the  
312 inhibition of microbial growth. It is assumed again that the inhibition occurred in the  
313 anode zone because both VSS profiles were very similar, and sometimes, even higher  
314 VSS concentrations were measured at the outlet of the anode compartment.

315

316

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318

319

Figure 4

320

Some previous works have reported the influence of high salinity levels on the

321

performance of CWs or MFCs. Regarding MFCs, Lefebvre et al. (2012) tested an MFC

322

treating wastewater under high NaCl concentrations. They observed a decrease in the

323

internal ohmic resistance and an increase in the electric power generation, but they also

324 found problems in the anodic biological process. They concluded that the antagonistic  
325 effect of NaCl on the anolyte conductivity and biofilm growth made bioelectricity  
326 production advantageous at salinity concentrations of up to 20 g L<sup>-1</sup> of NaCl, but the  
327 inhibition of anodophilic microorganisms began at a concentration of 10 g L<sup>-1</sup> NaCl. Liu  
328 et al. (2005) tested an MFC using NaCl concentrations of up to 400 mM, and the  
329 electric power generation always increased. They estimated that the maximum  
330 concentration of NaCl at which the microbial growth inhibition would occur is  
331 approximately 3%. Regarding CWs, there are some works that reported salinity  
332 inhibition of the microbial processes inside the wetland (Gao et al., 2012; Lin et al.,  
333 2008). Regarding the possible negative impact of the high salinity on the plants, in the  
334 present work, only a clear deterioration during the last period has been observed, that is,  
335 under 9.51 g L<sup>-1</sup> of salt. Different macrophyte plants in constructed wetlands treating  
336 high salinity wastewater have been tested in previous reported works. Gao et al. (2012)  
337 tested 12 different plants and observed that high salinity damaged their growth and  
338 decreased their nutrient uptake capacity and aeration potential in the roots zone.  
339 However, *Phragmites australis* was the most resistant species, and it functioned  
340 correctly up to a salt concentration of 20 g L<sup>-1</sup>.  
341 According to our results and previous research, it is assumed that higher salinity levels  
342 would reduce the internal ohmic resistance and, thus, increase the electric power  
343 generation, although there is a maximum admissible level for plants and  
344 microorganisms. The maximum level is between 4 and 5 g L<sup>-1</sup> under the continuous  
345 operation mode. However, lower salt concentrations (approximately 3 g L<sup>-1</sup>) begin to  
346 damage the anodic biological process. We assumed that the role of the plants remained  
347 constant, and plant damage was only observed from salinity concentrations of 9.51 g L<sup>-1</sup>

348 and higher. The electric power generation under  $9.51 \text{ g L}^{-1}$  is high, although we consider  
349 that this condition is unstable.

350 Figure 5a shows the results of the batch experiments performed at the end of each  
351 continuous period. The wastewater inflow was stopped in the batch experiments in  
352 order to allow enough retention time to oxidize the organic matter in the anode  
353 compartment. A voltage increase up to a maximum value can be observed in every  
354 experiment, and subsequently, there is a decrease until the “fuel” is depleted. Figure 5b  
355 shows the maximum cell voltage measured and the average voltage generation rate  
356 (calculated from the beginning to the maximum value). The figure also shows that the  
357 positive effect of the salinity increases as higher voltage differences are measured until  
358 the salt concentration reaches  $4.51 \text{ g L}^{-1}$ . Above this concentration, the maximum  
359 voltage decreases. Additionally, it can be observed that the voltage values are much  
360 higher than the values obtained under continuous operation, and this result suggests that  
361 higher retention times would be advisable. Figure 5b shows that the higher voltage  
362 generation rate corresponds to a relatively low salinity concentration of  $2.51 \text{ g L}^{-1}$ ,  
363 although the maximum cell voltage ( $600 \text{ mV}$ ) corresponds to  $4.51 \text{ g L}^{-1}$ . This result  
364 would confirm the results obtained under continuous operation; that is, under  $4.51 \text{ g L}^{-1}$ ,  
365 it is possible to obtain transiently higher potential differences in the MFC, although it  
366 takes longer to generate electricity because it is an unstable condition, as the  
367 microbiological process would begin to deteriorate at a concentration of approximately  
368  $3 \text{ g L}^{-1}$ .

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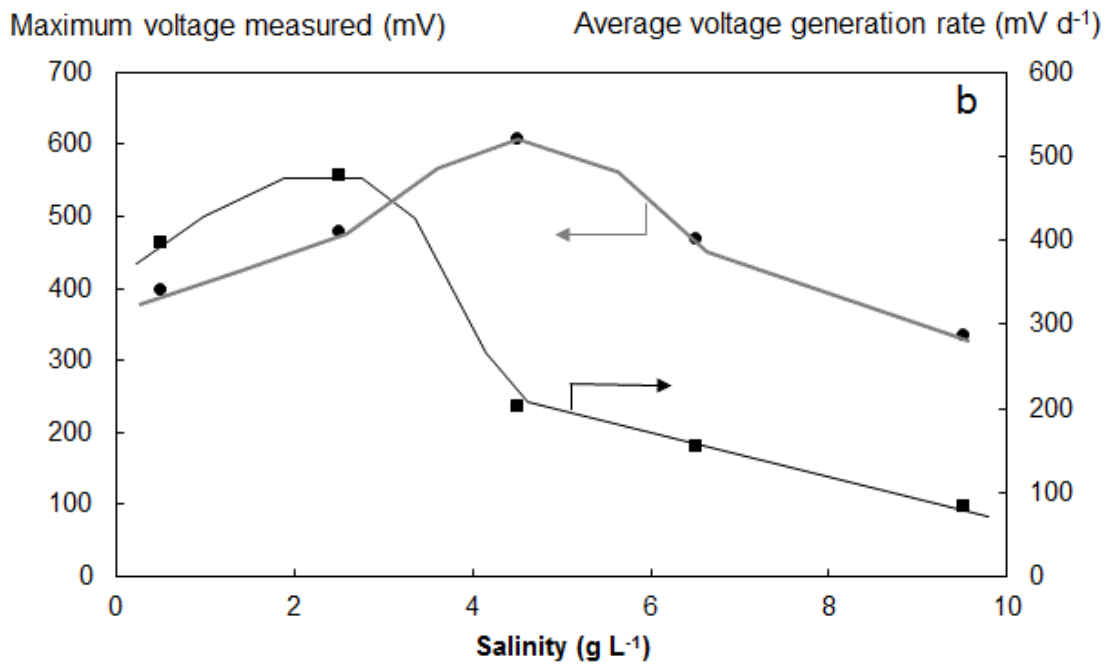
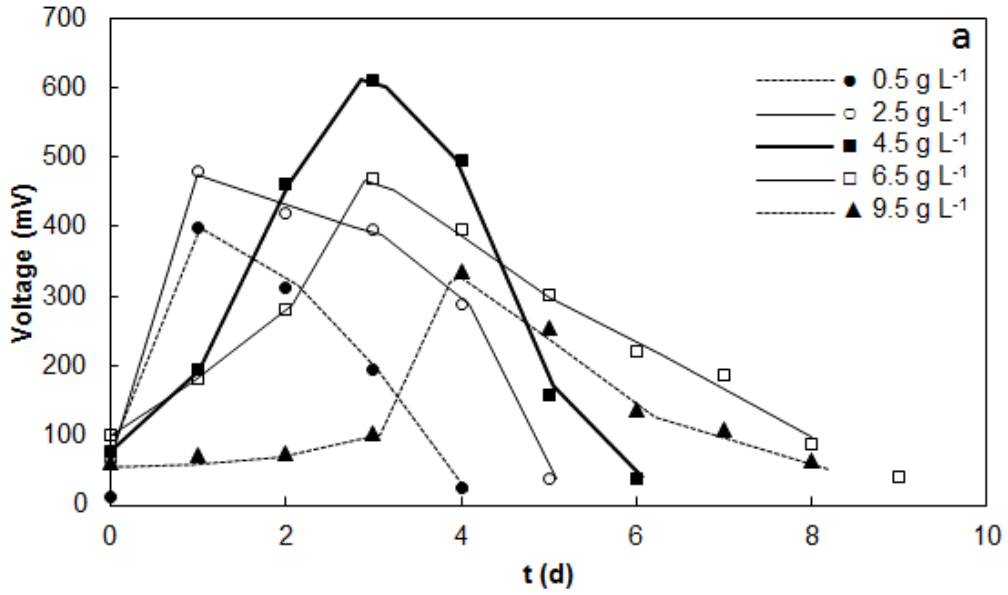


Figure 5

376 From the results in the present work, it could be argued that the CW-MFC would  
377 improve the electric power generation while treating wastewater with high salinity,  
378 although there is a maximum salt level that first inhibits the microbial process. Later,  
379 the salt level damages the plants' performance. Some researchers proved previously that  
380 it is possible to use halotolerant plant species (Webb et al., 2012) or to inoculate  
381 halotolerant microorganisms (Karajić et al., 2010) in CWs. Regarding MFC, Monzon et  
382 al. (2015) proposed using extreme halophilic microbes. The authors of the present work  
383 consider that the application of such halotolerant microbes and plants could allow for  
384 the application of CW-MFC to simultaneously treat high salinity industrial wastewater  
385 and produce electricity.

386 According to these results, the authors considered that high salinity in industrial  
387 effluents could be a positive influence in the development of the CW-MFC technology  
388 as it improved voltage differences. However the challenge would be if halo-tolerant  
389 microorganisms and plants could be adapted to these conditions, which may be the  
390 focus of further research.

391

#### 392 **4. Conclusions**

393 The increasing salinity first improved the cell voltage under continuous operation, and  
394 the maximum voltage corresponded to a salinity concentration between 4 and 5 g L<sup>-1</sup>,  
395 while subsequently higher salinity levels caused the opposite effect. However,  
396 according to the COD, DO and VSS measurements, microbiological inhibition in the  
397 anode zone appeared early at an approximate salinity of 3 g L<sup>-1</sup>. The batch experiments  
398 confirmed this behaviour. The wetland plants remained without apparent damage up to  
399 salinity levels of 9.51 g L<sup>-1</sup>.

400

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520 Figure 1. Experimental installation. (1) Wastewater feeding; (2) Anode; (3) Cathode; (4)  
521 Bentonite layer; (5) Reed plants; (6) Sampling points; (7) Treated effluent; (8)  
522 Resistance; and (9) Multimeter.

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525 Figure 2. Influent and effluent COD concentrations (a) and voltage generation (b)  
526 during the entire experimental period.

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529 Figure 3. (a) Average voltage generation values and error bars, and percentage of the  
530 COD consumed by bioelectrogenic microorganisms in the MFC depending on the  
531 salinity of the wastewater and (b) the total and electrogenic COD consumption rates.

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534 Figure 4. Dissolved oxygen concentrations (a) and VSS concentrations (b) in the anode  
535 (○) and the cathode (●) effluents.

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538 Figure 5. Cell voltage generated (a) and the maximum and average cell voltage change  
539 rates (b) in the batch experiments.

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