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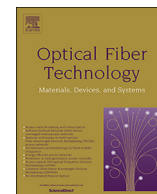
Simultaneous measurement of displacement and temperature based on two cascaded balloon-like bent fibre structures

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ARTICLE INFO	ABSTRACT
	A low-cost optical fibre sensor based on two cascaded balloon-like bent fibre (BBF) structures for simultaneous displacement and temperature measurement is reported. The sensor is fabricated by cascading two balloon-like bent single-mode fibres (SMFs) which with different bending radii, generating two separate interference dips within a limited wavelength range. The wavelength of the two interference dips exhibits different responses to external displacement and temperature variations, hence simultaneous measurement of displacement and temperature is realized. Experimental results show that the proposed optical fibre sensor achieves a displacement sensitivity of -318.8 pm/μm and a temperature sensitivity of 47.4 pm/°C. Taking advantage of its low-cost, ease of fabrication, and experimentally determined high sensitivity, the sensor in this investigation can be potentially applied in both displacement and temperature measurement fields.

1. Introduction

Monitoring of displacement is a key requirement in many measurement application fields, such as microimaging, robotics, astronautics, and structural health monitoring (SHM) [1,2]. In order to meet a variety of different measurement demands, various types of displacement sensors have been reported in recent years. Among them, optical fibre displacement sensors have regularly gained an edge over conventional electronic sensors due to their particular advantages including light weight, compact size, electromagnetic immunity and remote sensing capability. To date, several different fibre configurations have been adopted to realize displacement measurement, including fibre grating structures e.g. fibre Bragg gratings (FBGs) [3,4], tilted FBGs [5], long-period gratings (LPGs) [6], and various fibre interferometers including singlemode-multimode-singlemode (SMS) structures [7,8], Mach-Zehnder interferometers (MZIs) [9,10], a Sagnac interferometer [11], and a Fabry-Perot interferometer (FPI) [12]. Compared with fibre-grating-based displacement sensors, fibre-interferometer-based displacement sensors normally provide higher

measurement accuracy and a wider measurement range. However, in the case of many fibre interferometer devices, the complicated fabrication process and fragile structure may hinder their widespread application in industrial or commercialized optical fibre displacement sensing.

Recently, an easy-to-fabricate, structurally robust balloon-like interferometer has been reported and has attracted a great deal of research attention. However, this structure has proven to have a relatively high temperature dependence of up to 418 pm/°C [13], and in the absence of a stripped coating process, its temperature sensitivity can reach -2465 pm/°C [14]. This means that an undesirable cross-sensitivity induced by temperature is inevitable in the application of such a structure for measurement of other parameters. In order to eliminate temperature induced cross-sensitivity, simultaneous multi-parameter measurement is the most commonly used method [15]. Based on previous research, simultaneous measurement usually requires the incorporation of two separate measurement elements to introduce active sensing and reference (temperature based) interference patterns. Several fibre configurations are frequently chosen to realize the goal of

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simultaneous measurement, such as FBGs [16–19], LPGs [20,21], polarization maintaining fibre (PMF) [22], and photonics crystal fibre (PCF) [23,24]. However, combining these fibre configurations further increases the complexity and cost of the overall sensor system. Therefore, there is a clear need to develop a simple and cost-effective optical fibre sensor structure for simultaneous measurement of displacement and temperature.

In this article, a low-cost optical fibre sensor based on two cascaded balloon-like bent fibre (BBF) structures for simultaneous measurement of displacement and temperature is experimentally demonstrated. The sensor is fabricated by simply bending a standard SMF into a balloon shape with the help of a capillary tube, without the requirement for any expensive equipment. Through cascading two balloon-like bent SMFs with different bending radii, two separate interference dips can be obtained within the wavelength domain of the detector and used for simultaneous measurement of displacement and temperature. Benefiting from its advantages of low-cost, ease of fabrication and high measurement sensitivity, the sensor of this investigation may therefore find use in applications in accurate displacement and temperature measurement fields.

2. Principle and fabrication

The schematic diagram of the cascaded balloon-like bent SMF structures is illustrated in Fig. 1. The sensor consists of two balloon-like bent SMFs, but with different bending radii of r_1 and r_2, and different lengths of L_1 and L_2. As depicted in Fig. 1, the light from an optical source initially propagates along the core of the input SMF in fundamental mode. When the light arrives at the first balloon-like section, owing to the bend of the waveguide, a portion of the light from the SMF core is coupled into the cladding and excites the cladding modes. These modes propagate within the SMF cladding, and after passing through the bend region, part of them are recoupled back to the SMF core. Interference therefore occurs because of the effective RI differences of the core and cladding modes and the optical path difference (OPD) experienced by the light signals. When the light arrives at the second balloon-like bent section, the above-mentioned interference occurs again. In the case of a two-mode modal interferometer, the output intensity can be expressed as [25]

$$I = I_{co} + I_{cl} + 2\sqrt{I_{co}I_{cl}} \cos(\frac{2\pi}{\lambda}L_{eff}\Delta n_{eff})$$

(1)

where I_{co} and I_{cl} represent the intensity of the core mode and cladding modes, λ is the free space wavelength, L_{eff} is the effective interference length and $\Delta n_{eff} = n_{co}\text{-}n_{cl}$ denotes the effective RI difference between the core and cladding modes. When the phase difference meets an odd multiple of π, the center wavelength of the interference dip can be expressed as [26]

$$\lambda_s = \frac{2}{(2s + 1)}L_{eff}\Delta n_{eff}$$

(2)

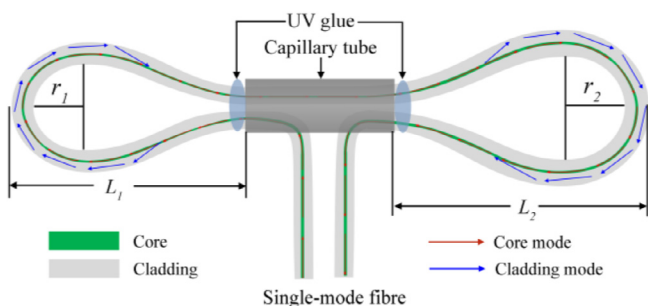where s is an integer ($s = 1, 2, 3…$). The free spectral range (FSR) of the transmission spectrum can be calculated from Eq. (2) as

$$FSR = \frac{\lambda_s^2}{L_{eff}\Delta n_{eff}}$$

(3)

Since the two BBFs have different bending radii, their effective interference length of L_{eff} and the effective RI difference (Δn_{eff}) are different, resulting in different resonance wavelengths according to Eq. (2). When the external displacement or temperature change, the value of L_{eff} and Δn_{eff} also change which leads to a shift in the resonance wavelengths. Therefore, in principle the BBF structure can be used for simultaneous measurement of displacement and temperature.

Additionally, due to the existence of the elasto-optical effect, the bend also effects the physical RI distribution inside the SMF. For a bent SMF, its originally symmetric radial RI distribution becomes asymmetrical, and the redistributed RI status can be equivalent to a distribution superimposed on that of a straight SMF, which can be expressed as

$$n_1 = n_0(1 + \frac{x}{r_{eff}})$$

(4)

where n_0 is the RI of the straight fibre, x is the displacement in the normal direction to the bent fibre axis, and r_{eff} is the equivalent bending radius which can be calculated as follows [27]:

$$r_{eff} = \frac{r}{1 - n_0^2/2[P_{12} - \nu(P_{11} + P_{12})]}$$

(5)

where r is the bending radius of the fibre, P_{11} and P_{12} are components of the photoelastic tensor, and ν is the Poisson ratio.

Numerical simulations based on the Beam Propagation Method (BPM) have been carried out to investigate the optical field distribution within the bent fibre. According to Eq. (4), the RI distribution of the bent fibre can be established in a straight fibre model. To simplify the simulation process, only the section with the largest curvature (the top of the balloon-like structure) was considered because this section has a uniform bending radius. The simulation geometry/RI parameters were set as: the diameters and RIs for the SMF core/cladding are 8.3/125 μm and 1.4504/1.4447, respectively, and the simulation length of the SMF is 1 cm. When the bending radii were set to 10 mm, 8 mm, 6 mm and 4 mm, for an incident wavelength of 1550 nm, the simulation results are shown in Fig. 2. It can be observed from Fig. 2 that optical field is mainly concentrated on the outside of the bent fibre. With a decrease in the bending radius from 10 mm to 4 mm, the optical field intensity of the cladding modes excited in the SMF cladding layer increases. The optical field intensity distribution of the core and cladding mode due to modal interference results in a difference in the extinction ratio (ER) of the interference dips. Therefore, a suitable range of bending radii needs to be determined experimentally to obtain an effective interference pattern.

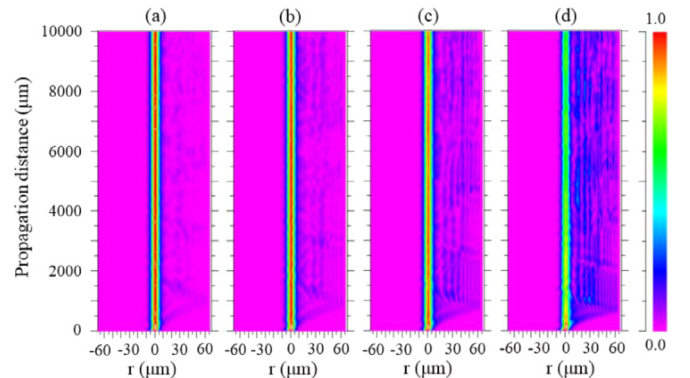Fig. 3 shows the measured transmission spectra in the range of

Fig. 1. Schematic diagram of the cascaded BBF structures.

Fig. 2. Simulated optical field distribution of the BBF structure with different bending radii (a) $r = 10$ mm; (b) $r = 8$ mm; (c) $r = 6$ mm; (d) $r = 4$ mm.
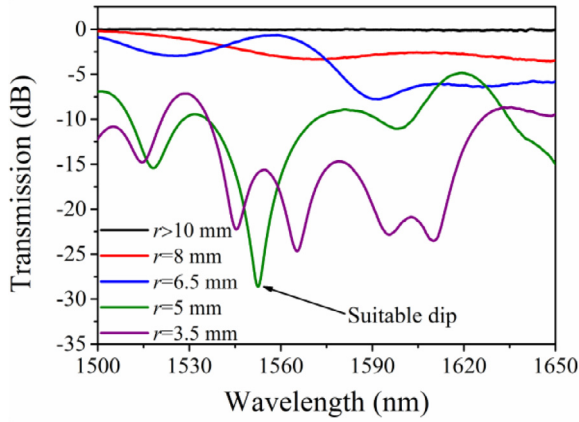
Fig. 3. Measured transmission spectra of the BBF structure with different bending radii.

Fig. 4. Transmission spectra of the BBF1, BBF2 and the cascaded fibre structures.

1500–1650 nm of a BBF structure with different bending radii. It can be seen that when the bending radius is greater than 10 mm, no clear interference dips were observed since very little light propagating in the SMF core is coupled into the cladding. As the bending radius decreases, more light is coupled into the cladding, resulting in an increase of transmission loss. Interference patterns appear when the bending radius was 8 mm and 6.5 mm, and the resulting interference dips do not have a good ER. When the bending radius was further decreased to 5 mm, an interference dip with enhanced ER (more than 18 dB) occurred at 1552 nm. With further decreases in the bending radius to 3.5 mm, more interference dips were detected, but the induced interference dips possess a smaller ER compared with the 5 mm bending case. If the bending radius continues to decease below 2.5 mm, the SMF is more susceptible to fracture, and the light signal in this case is weak because excess light is not only coupled into the cladding, but also out the cladding, resulting in large power loss. Therefore, based on the initial results obtained in this experiment, an appropriate bending radius for balloon-like structure to form an effective interference pattern should be in the region of 5 mm.

To fabricate the cascaded BBF structures, a length of standard SMF (SMF-28, Corning) was initially stripped of its polymer coating over an appropriate length. Next, both free ends of the SMF were inserted into a Teflon capillary tube for which the length and inner diameter are 1.5 cm and 800 μm, respectively. By moving this capillary tube along the fibre, the bending radius of the balloon-like structure can be flexibly adjusted. Based on this method, two balloon-like structures with different bending radii were obtained, and the entire structure was finally immobilized using ultraviolet (UV) glue.

The bending radius and the length of the two balloon-like structures was measured. The smaller balloon-like structure (BBF1) has an r_1 of 4.96 mm and L_1 of 17.58 mm, the larger balloon-like structure (BBF2) has an r_2 of 5.37 mm and L_2 of 19.18 mm. The transmission spectra of the individual BBF1, BBF2, and the cascaded structure were measured and are shown in Fig. 4. It can be seen that two interference dips with high ER values were detected in the cascaded structure over the wavelength range of 1500–1650 nm. The central wavelength of dip 1 and dip 2 were located at 1550.8 nm and 1605.8 nm, respectively. Benefiting the high interference visibility of dip 1 and dip 2, these two interference dips formed by BBF1 and BBF2 were chosen for the measurement of this investigation.

Based on the above discussions, when the external displacement and temperature change, the resulting wavelength shift of dip 1 and dip 2 can be expressed as follows:

$$\Delta\lambda_{dip1} = K_{D1}\cdot\Delta D + K_{T1}\cdot\Delta T \qquad (6)$$

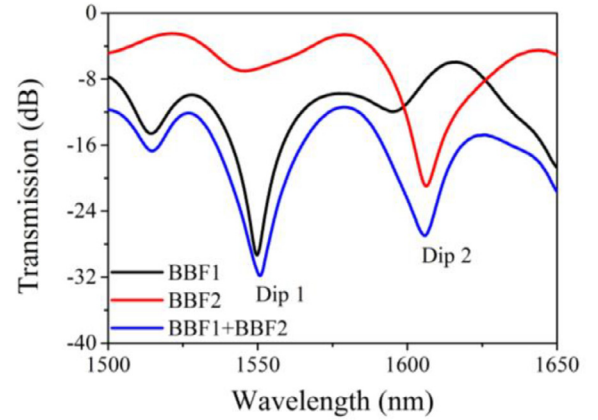$$\Delta\lambda_{dip2} = K_{D2}\cdot\Delta D + K_{T2}\cdot\Delta T \qquad (7)$$

where ΔD and ΔT denote the variation of displacement and temperature; K_{D1}, K_{D2}, K_{T1} and K_{T2} are the sensitivity coefficients of dip 1 and dip 2 in response to displacement and temperature, respectively. Once these coefficients are determined experimentally, and based on Eqs. (6) and (7), a demodulation matrix can be established to realize the goal of simultaneous measurement of displacement and temperature.

3. Experimental results and discussions

The experimental setup for micro-displacement test is illustrated in Fig. 5, where a supercontinuum light source (SCS, YSL SC-series, China) was used to provide broadband light and an optical spectrum analyzer (OSA, YOKOGAWA AQ6370D, Japan) with a spectral resolution of 20 pm was used to monitor the spectral response of the sensor. The sensor sample was mounted horizontally and fixed on a lifting stage of adjustable height. A linear translation stage with a displacement resolution of 10 μm was used to accurately change the displacement applied to the balloon-like section. The smaller balloon-like bent SMF was placed in contact with the translation stage and used for displacement measurement, thus while the larger radius balloon-like bent SMF was entirely free from external displacement change and therefore was subject only to temperature changes.

Fig. 6 shows the measured spectral response of the sensor when subjected to a 0–90 μm displacement range at a constant temperature of 20 °C. A complete measurement cycle was performed to test the hysteresis of the sensor for displacement measurement. In this case, the displacement was initially increased from 0 to 90 μm and then decreased from 90 μm back to 0 with a step of 10 μm. The corresponding spectral evolution results are shown in Fig. 6(a) and (b), respectively. From the results presented in Fig. 6(a), it is clear that the two separate interference dips exhibit different individual responses to external
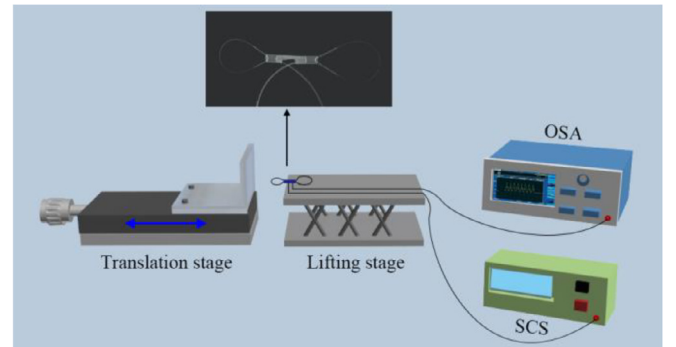

Fig. 5. Schematic diagram of the experimental setup for the displacement test.
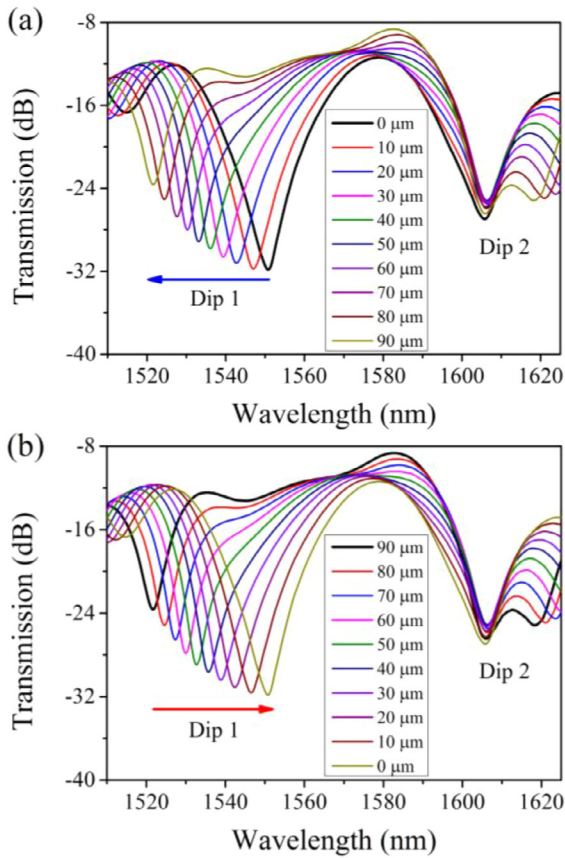
Fig. 6. Measured spectral responses at different displacement values (a) displacement increasing; (b) displacement decreasing.

Fig. 8. Dip wavelength versus temperature and the linear fitting (a) result of dip 1 and its spectral evolution inset in the figure; (b) result of dip 2 and its spectral evolution inset in the figure.

displacement change. The smaller balloon-like bent SMF dip 1 exhibits a clear blue-shift in the wavelength domain, while the larger balloon-like bent SMF dip 2 shows no wavelength shift as the displacement was increased from 0 to 90 μm. For the second half of the cycle when the applied displacement was reduced, the evolution of dip 1 of Fig. 6(b) shows a clear red-shift and is therefore opposite to the displacement increasing case.

From the above spectral response results, it is clearly demonstrated that dip 2 is immune to external displacement change, which means its displacement sensitivity can be expressed as 0. Conversely, external displacement variations strongly influence the location of the central wavelength of dip 1. Fig. 7 shows the wavelength of dip 1 as a function of displacement for the displacement increasing and decreasing cases. From the linear fitting results, the sensor exhibits an excellent linear
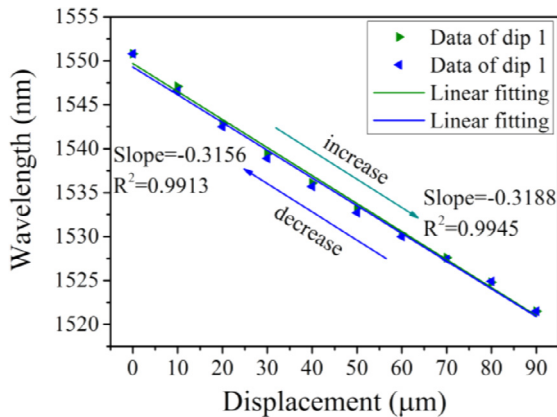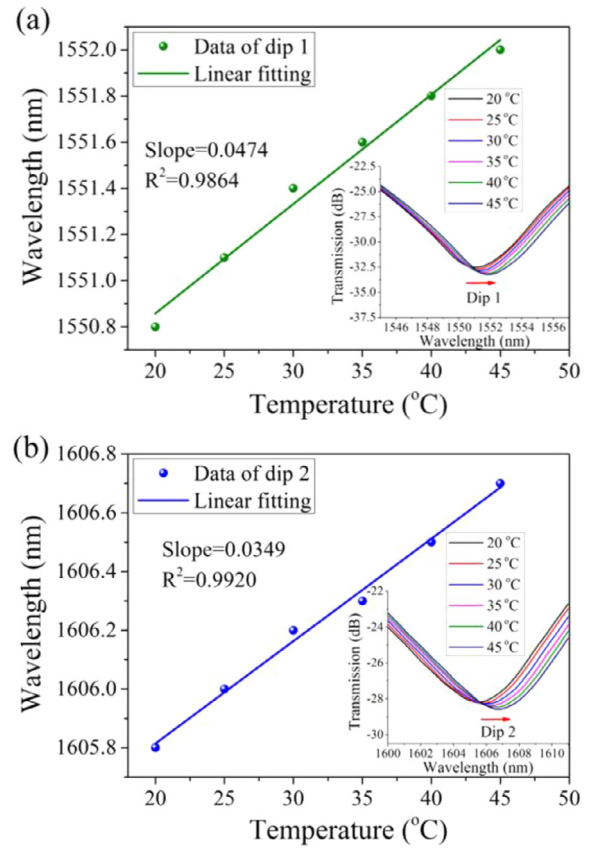

Fig. 7. Dip 1 wavelength versus displacement and the linear fitting.

response to external displacement variation, and the displacement sensitivities within the displacement range cases were calculated to be −318.8 pm/μm (increasing) with an R^2 of 0.9945 and −315.6 pm/μm (decreasing) with an R^2 of 0.9913, respectively. Based on the observed spectral response characteristics and the calculated displacement sensitivities, it is also evident that there is no discernible hysteresis present for the displacement measurement.

To investigate the temperature response of the sensor, the sensor was placed in a temperature-controlled chamber (ESPEC SH-222, Japan), in which the inside temperature could be easily adjusted by altering the set value on an external operating panel. In this case, the temperature was increased from 20 °C to 45 °C with a step of 5 °C, and the corresponding spectral response and data fitting results of dip 1 and dip 2 are shown in Fig. 8(a) and (b), respectively. It can be seen from the insets in Fig. 8(a) and (b) that both dip 1 and dip 2 exhibit a red-shift in the wavelength domain as the temperature increases. The linear fitting results show these two dips exhibit a good linear response to temperature change, and the temperature sensitivities of dip 1 and dip 2 were determined to 47.4 pm/°C with R^2 of 0.9864 and 34.9 pm/°C with R^2 of 0.9920, respectively.

The above experimental results clearly show that dip 1 and dip 2 have different response characteristics for displacement and temperature. The smaller BBF dip1 is sensitive to external displacement and temperature variation, while the larger BBF dip 2 is independent of displacement change which enables the combination of the two BBFs to be used for simultaneous measurement of displacement and temperature. Based on Eqs. (6) and (7) and the displacement and temperature sensitivity coefficients determined above, the demodulation matrix can be written as follows:

Table 1

Comparison of the sensing performance of different sensors for displacement and temperature measurement.

Measurement configuration	Displacement sensitivity (pm/ μm)	Temperature sensitivity (pm/ °C)	Simultaneous measurement
FBG [3]	0.0643	16.9	Yes
FBG [4]	0.058	–	No
Tilted FBG [5]	− 0.0086 (m^{-1})	–	No
LPG [6]	220	–	No
MMI [7]	35.5	–	No
MMI [8]	0.51 (dB/μm)	− 0.365 (dB/°C)	No
MZI [9]	835	46–85	No
MZI [10]	− 0.385 (dB/ μm)	− 0.036 (dB/°C)	No
Sagnac interferometer [11]	–	–	No
FPI [12]	–	–	No
Bent fibre with LPG [20]	− 306	42.9	Yes
Cascaded balloon-like fibre structures (this work)	**− 318.8**	**47.4**	**Yes**

$$\begin{bmatrix} \Delta D \\ \Delta T \end{bmatrix} = \begin{bmatrix} -318.8 pm/\mu m & 47.4 pm/^{\circ}C \\ 0 & 34.9 pm/^{\circ}C \end{bmatrix}^{-1} \begin{bmatrix} \Delta \lambda_{Dip1} \\ \Delta \lambda_{Dip2} \end{bmatrix} \qquad (8)$$

Moreover, according to the OSA with a resolution of 20 pm used in the experiments and assuming a suitable calibration, the displacement and temperature measurement resolution of the optical fibre sensor of this investigation were calculated to be 0.06 μm and 0.42 °C, respectively.

Table 1 includes a direct comparison of the displacement and temperature sensing performance between the sensor described in this investigation and the other sensors cited in this article. It can be seen that the cascaded balloon-like bent fibre structures has competitive displacement and temperature sensitivity compared to the previous cases. Moreover, the sensor of this investigation can achieve simultaneous measurement of displacement and temperature, which supports its potential applications in the field of displacement and temperature measurement.

4. Conclusion

In summary, a low-cost optical fibre sensor based on two cascaded balloon-like bent fibre structures for simultaneous displacement and temperature measurement has been presented. The sensor was simply fabricated by cascading two balloon-like bent SMFs to generate independent interference dips in the transmission spectrum. The smaller balloon-like bent SMF interference dip was sensitive to both displacement and temperature variation, while the larger balloon-like SMF was entirely strain relieved and hence introduced a reference dip to realize unambiguous displacement and temperature measurement. Experimental results show a displacement sensitivity of − 318.8 pm/μm over the displacement range of 0–90 μm and a temperature sensitivity of 47.4 pm/°C over the temperature range of 20–45 °C were achieved. Such a low-cost optical fibre sensor is highly sensitive and is without hysteresis, which provides great application potential for use in many robust displacement and temperature measurement scenarios.

CRediT authorship contribution statement

Ke Tian: Conceptualization, Methodology, Validation, Investigation, Data curation, Writing - original draft. **Ruoning Wang:** Methodology, Investigation. **Meng Zhang:** Methodology, Investigation. **Xianfan Wang:** Software. **Xin Wang:** Visualization. **Guoyong Jin:** Writing - review & editing. **Elfed Lewis:** Writing - review & editing.

Gerald Farrell: Writing - review & editing. **Pengfei Wang:** Writing - review & editing, Supervision.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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