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## Mapping The In-Plane Electric Field Inside Irradiated Diodes

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## Mapping the in-plane electric field inside irradiated diodes

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### Abstract

A significant aspect of the Phase-II Upgrade of the ATLAS detector is the replacement of the current Inner Detector with the ATLAS Inner Tracker (ITk). The ATLAS ITk is an all-silicon detector consisting of a pixel tracker and a strip tracker. Sensors for the ITk strip tracker have been developed to withstand the high radiation environment in the ATLAS detector after the High Luminosity Upgrade of the Large Hadron Collider at CERN, which will significantly increase the rate of particle collisions and resulting particle tracks. During their operation in the ATLAS detector, sensors for the ITk strip tracker are expected to accumulate fluences up to  $1.6 \cdot 10^{15} \text{ n}_{\text{eq}}/\text{cm}^2$  (including a safety factor of 1.5), which will significantly affect their performance. One characteristic of interest for highly irradiated sensors is the shape and homogeneity of the electric field inside its active area. For the results presented here, diodes with edge structures similar to full size ATLAS sensors were irradiated up to fluences comparable to those in the ATLAS ITk strip tracker and their electric fields mapped using a micro-focused X-ray beam (beam diameter  $2 \times 3 \mu\text{m}^2$ ). This study shows the extension and shape of the electric field inside highly irradiated diodes over a range of applied bias voltages. Additionally, measurements of the outline of the depleted sensor areas allow a comparison of the measured leakage current for different fluences with expectations for the corresponding active areas.

*Keywords:* ATLAS, silicon strip sensors, radiation damage, active sensor area

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### 1. Introduction

Accompanying the High-Luminosity Upgrade of the Large Hadron Collider [1], the ATLAS detector [2] will be upgraded accordingly. As part of the ATLAS Phase-II Upgrade [3], the current Inner Detector of ATLAS will be

replaced with the ATLAS Inner Tracker, consisting of silicon pixel tracker and strip trackers [4].

During their operation in the ATLAS detector, sensors for the ITk strip tracker are expected to accumulate fluences up to  $1.6 \cdot 10^{15} \text{ n}_{\text{eq}}/\text{cm}^2$  (including a safety factor of 1.5), which will significantly affect their performance as semiconductors. Extensive irradiation tests

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16 have been performed using both full-size sen-  
 17 sors and test structures. Monitoring diodes in  
 18 particular are used to compare the leakage cur-  
 19 rent after irradiation for estimates of the area  
 20 factor, i.e. leakage current per unit area, and  
 21 total leakage current of full size sensors.

22 The measurements presented here were con-  
 23 ducted as a follow-up for previous studies using  
 24 the same method for un-irradiated diodes of  
 25 the same type and geometry used here [5]. Re-  
 26 peating the same measurement with irradiated  
 27 diodes allowed both to test the applicability of  
 28 the method for highly irradiated silicon struc-  
 29 tures and to study the evolution of the active  
 30 diode area with increasing fluence.

## 31 2. Experimental setup

32 Electron-hole pairs created within the de-  
 33 pleted area of a sensor lead to an increase in  
 34 the sensor current, but recombine without a  
 35 current increase in the undepleted area of a  
 36 sensor. The lateral extension of the depleted  
 37 area can therefore be mapped using the mea-  
 38 sured diode current.

39 Three diodes were studied in this measure-  
 40 ment (see figures 4a, 4c and 4e), which were  
 41 designed to have edge regions similar to full size  
 42 sensors: n-doped strip implants in a p-doped  
 43 sensor bulk were surrounded by n-doped bias  
 44 and guard ring implants, while the sensor back-  
 45 side and edge ring were p-doped. HPK diodes  
 46 used here can be assumed to have an active  
 47 thickness of 303 [6]-310 [7]  $\mu\text{m}$  and a bulk resis-  
 48 tivity of 3 k $\Omega\cdot\text{cm}$ , IFX diodes have a thickness  
 49 of 300  $\mu\text{m}$  and a bulk resistivity of 3.5 k $\Omega\cdot\text{cm}$ .  
 50 For a detailed description of the edge regions  
 51 of all ATLAS17 ([8], [7]) design diodes, see [5].

52 At the time of the measurements, investiga-  
 53 tions into the full depletion voltage of the used  
 54 diodes after different levels of irradiation were  
 55 still in progress. It was therefore decided to  
 56 conduct all diode measurements presented here  
 57 with an applied bias voltage of -500 V. Since  
 58 IFX MD2 and HPK MD2 diodes were designed  
 59 with similar edge structures as full ATLAS ITk

Fluence, [n <sub>eq</sub> /cm <sup>2</sup> ]	V <sub>fD</sub> , [V]	Current at -20 °C [A]	Induced current [nA]
1 · 10 <sup>14</sup>	300 [8]-400 [9],	5.0 · 10 <sup>-7</sup>	17-18
5 · 10 <sup>14</sup>	300 [8]-500 [9]	1.5 · 10 <sup>-6</sup>	14-15
1 · 10 <sup>15</sup>	> 600 [9]	2.9 · 10 <sup>-7</sup>	12-13
3 · 10 <sup>15</sup>	> 800 [9]	5.2 · 10 <sup>-6</sup>	9

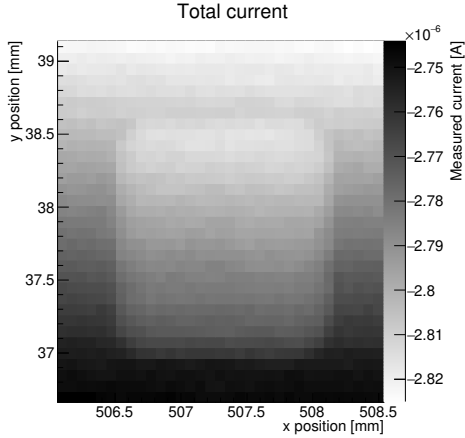
Table 1: Parameters of the diodes under investigation: full depletion voltages V<sub>fD</sub>, total diode leakage current (measured for all three diodes irradiated to the same fluence together for technical reasons) and average photo current induced by X-ray beam for an individual diode.

strip sensors, which are foreseen to be operated  
 at -500 V, this working point was chosen to pro-  
 vide information about the development of the  
 depleted sensor at the sensor edge at realistic  
 operating conditions. Information about deple-  
 tion voltages from later measurements [8], [9]  
 is summarised in table 1.

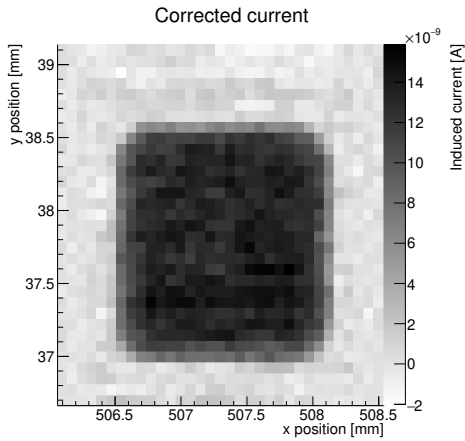
The test setup was flushed with nitrogen to  
 prevent condensation on the diodes. During  
 measurements, diodes were cooled down to -  
 20 °C with measured variations of unit[±0.1]°C  
 using a peltier-element cooling jig inside a  
 light-sealed cold box. Precision stages allowed  
 to move diodes under investigation with re-  
 spect to an X-ray beam pointed normal to the  
 diode's top surface in order to obtain 2D maps.  
 A Keithley 2410 high voltage power supply was  
 used to both bias diodes under investigation  
 and measure the corresponding current.

## 3. Performed measurements

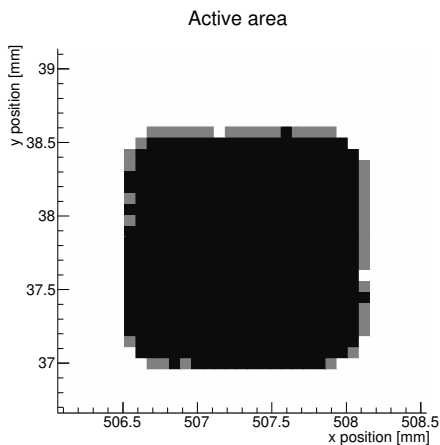
Measurements were conducted using an X-  
 ray beam focused to a beam size of 2 × 3  $\mu\text{m}^2$   
 with a monochromatic beam energy of 15 keV  
 (beamline B16 at the Diamond Light Source).  
 Within a diode of 300  $\mu\text{m}$  thickness, each  
 15 keV photon has a 51 % chance to interact  
 with a silicon atom. The interaction produces  
 one 15 keV electron, which travels up to 20  $\mu\text{m}$   
 within silicon, which determines the limit of  
 the achievable position resolution.



(a) Total diode current read out per stage position



(b) Diode current map after subtracting diode leakage current line by line



(c) Active area of diode calculated from bins in diode plateau: bins above the calculated threshold plus  $\sigma$  were counted towards the active area (black), bins at the threshold, but within  $\sigma$  were counted towards the active area uncertainty (grey bins, see figure 3).

90 Diodes were scanned in a grid with a step  
 91 size of  $75 \times 75 \mu\text{m}^2$  to provide good spatial  
 92 resolution while minimising the beam time re-  
 93 quired per diode measurement. During mea-  
 94 surements, the total diode current was read  
 95 out. For irradiated diodes, the measured cur-  
 96 rent was dominated by the sensor leakage cur-  
 97 rent (see figure 1a), which varied with the sen-  
 98 sor temperature. At a sensor temperature of  
 99 about  $-20^\circ\text{C}$ , actual fluctuations in the sen-  
 100 sor leakage current, i.e. fluctuations independent  
 101 of temperature changes, were small compared  
 to the X-ray beam induced current. Figure 2

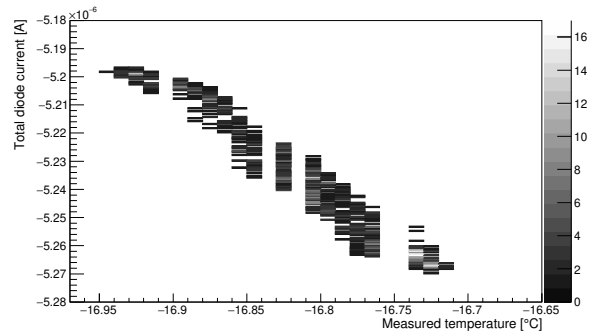


Figure 2: Correlation between measured temperature and diode leakage current for a sample irradiated up to  $3 \cdot 10^{15} \text{ n}_{\text{eq}}/\text{cm}^2$ : while temperature changes of about  $0.25^\circ\text{C}$  change the overall current by  $\pm 40 \text{ nA}$ , temperature-independent changes are significantly smaller (while including additional, beam-induced currents).

102

103 In order to map the depleted diode area,  
 104 the measured diode leakage current was sub-  
 105 tracted from the total measured current. Scans  
 106 were performed in horizontal scan lines, taken  
 107 within about 3 min per line, which can there-  
 108 fore be assumed to show only small fluctuations  
 109 in diode temperature and overall leakage cur-  
 110 rent. Therefore, a linear fit was performed for  
 111 each scan line, where the un-depleted edge re-  
 112 gions of the diode were used to calculate the to-  
 113 tal diode current per position. By subtracting  
 114 the diode leakage current per bin, the underly-  
 115 ing depleted area inside the diode was obtained  
 116 (see figure 1b for an image of IFX MD2, irra-  
 117 diated up to  $1 \cdot 10^{15} \text{ n}_{\text{eq}}/\text{cm}^2$ ). The resulting

118 association of bins with the active or inactive  
 119 diode area allowed to map this area directly  
 120 (see figure 1c).

121 The active sensor area was calculated from  
 122 the resulting corrected current map: bins in  
 123 the main pedestal (within fluctuations) were  
 124 counted towards the active area, bins within  
 125 a window within  $\sigma$  between background and  
 126 pedestal were counted towards the uncertainty  
 127 of the active area (see figure 3).

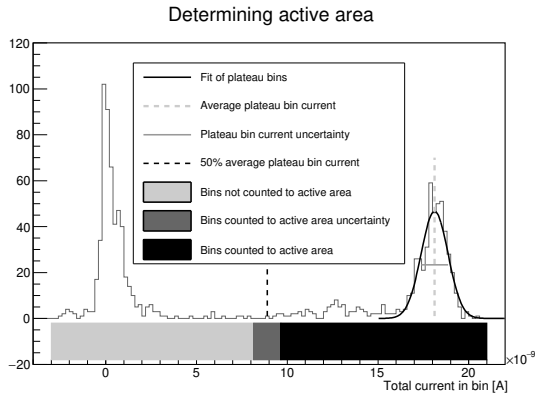


Figure 3: Determining the active area of an irradiated diode from currents measured per bin: the average current measured within the active diode area was measured. Bins were counted to the active diode area if their measured current was higher than half the average plateau current.

## 128 4. Results

129 Mapping the active areas of all diodes under  
 130 investigation (after irradiation up to  $1 \cdot 10^{14}$   
 131  $n_{eq}/cm^2$ ) showed that the shape of the de-  
 132pleted area matched the shape of the diode im-  
 133plants (see figures 4b, 4d and 4f). Similar as  
 134 for the same diode geometries before irradiation,  
 135 the shape of the active area was found to  
 136 show rounded corners matching the shape of  
 137 the diode edge ring (see figures 4a, 4c and 4e).

138 Samples of each diode type were irradiated  
 139 up to four fluences:  $1 \cdot 10^{14}$   $n_{eq}/cm^2$ ,  
 140  $5 \cdot 10^{14}$   $n_{eq}/cm^2$ ,  $1 \cdot 10^{15}$   $n_{eq}/cm^2$  and  $3 \cdot$   
 141  $10^{15}$   $n_{eq}/cm^2$  (only for HPK MD2 due to  
 142 time constraints). One diode per fluence was

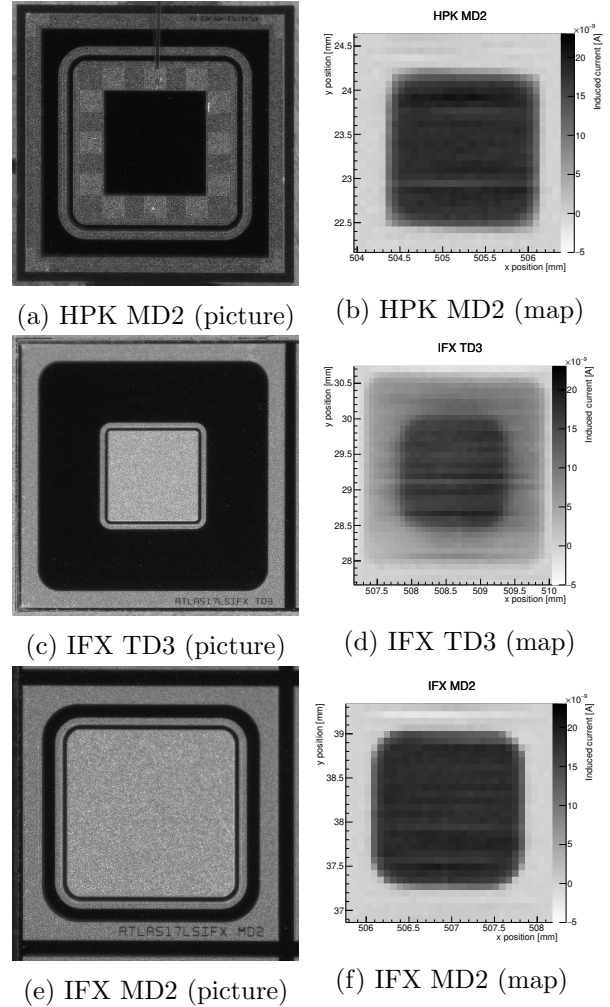
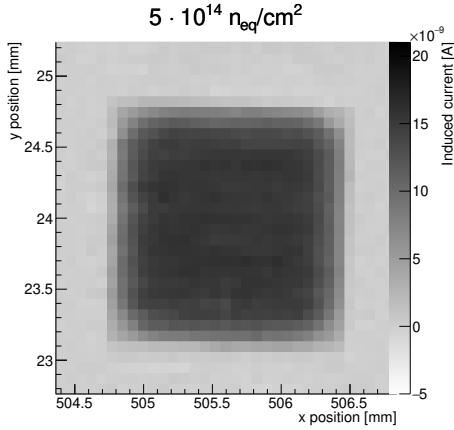
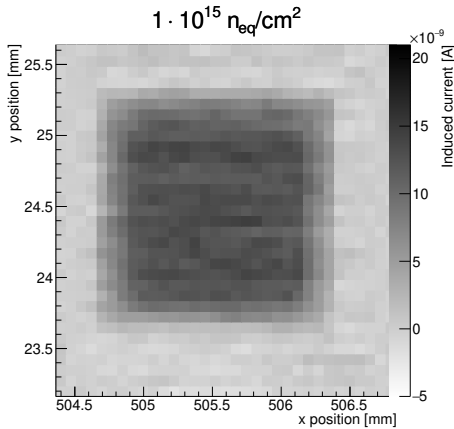


Figure 4: Pictures and maps of diodes irradiated up to  $1 \cdot 10^{14}$   $n_{eq}/cm^2$ , measured at a bias voltage of  $-500$  V each.

143 mapped in the beam, except for the highest fluence  
 144 level, where the signal-to-noise-ratio was  
 145 found to be too low to map the active area re-  
 146 liably.



(a) Map of diode HPK MD2, irradiated up to  $5 \cdot 10^{14} \text{ n}_{\text{eq}}/\text{cm}^2$



(b) Map of diode HPK MD2, irradiated up to  $1 \cdot 10^{15} \text{ n}_{\text{eq}}/\text{cm}^2$

Figure 5: Current maps for the same diode geometry, irradiated up to increasing fluences

147 The active area of diodes irradiated to dif- 159  
 148 ferent fluence levels was successfully mapped 160  
 149 using a micro-focused X-ray beam by reading 161  
 150 out the overall diode current. 162

## 151 5. Conclusion

152 The method was found suitable for measure- 166  
 153 ments of the active sensor area using the total 167

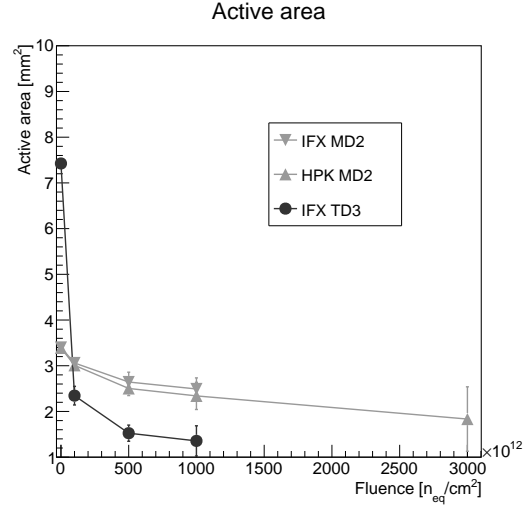


Figure 6: Reduction of the active area of different diodes with increasing fluence levels. Area of unirradiated diodes from [5]

	Width of area, [mm]		
	HPK MD2	IFX TD3	IFX MD2
Diced size	2	3	2
Bias implant	1.14	1.00	1.25
Unirradiated	$1.85 \pm 0.01$	$2.63 \pm 0.01$	$1.96 \pm 0.01$
$1 \cdot 10^{14} \text{ n}/\text{cm}^2$	$1.70 \pm 0.01$	$1.79 \pm 0.01$	$1.76 \pm 0.01$
$5 \cdot 10^{14} \text{ n}/\text{cm}^2$	$1.55 \pm 0.01$	$1.38 \pm 0.03$	$1.54 \pm 0.02$
$1 \cdot 10^{15} \text{ n}/\text{cm}^2$	$1.55 \pm 0.02$	$1.22 \pm 0.01$	$1.55 \pm 0.01$
$3 \cdot 10^{15} \text{ n}/\text{cm}^2$	$1.51 \pm 0.07$	-	-

Table 2: Measured width of active diode areas for different fluences compared to the diode design layout (distance between bias ring/bias implants and overall diced diode size).

154 diode current. The current setup with diode  
 155 temperatures of  $-20^\circ\text{C}$  provided a sufficient  
 156 signal-to-noise ratio to allow tests of diodes  
 157 up to fluences of  $1 \cdot 10^{15} \text{ n}/\text{cm}^2$  (see figures 5a  
 158 to 5b).

Measurements for all diodes showed that the  
 active diode area shrank with increasing irradi-  
 ation (see figure 6) as expected: for an unirra-  
 diated diode, the depleted diode area extends  
 laterally beyond the bias ring towards the dic-  
 ing edge. Free charge carriers generated be-  
 yond the bias ring drift towards to the collec-  
 tion area and can be read out [5]. After ir-  
 radiation, the diodes under investigation have

168 decreased bulk resistivity due to an increase of 212  
169 acceptor-like defects, therefore the same bias 213  
170 voltage decreases the lateral extension of the 214  
171 depleted zone [10]. 215

172 All diodes had depleted areas of 85-95 % 216  
173 of their diced size before irradiation, which 217  
174 matched the inner outline of the edge ring. Ir- 218  
175 radiation to  $1 \cdot 10^{15}$  n/cm<sup>2</sup> shrank the active ar- 219  
176 eas by 31 % (HPK MD2), 27 % (IFX MD2) and 220  
177 82 % (IFX TD3) of the size of the unirradiated 221  
178 diode's active area. The performed measure- 222  
179 ments indicated that the outline of the active 223  
180 area before irradiation is defined by the shape 224  
181 of the edge ring and follows the shape and size 225  
182 of bias or guard ring implants after irradiation. 226  
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