Increased Density to Improve Pavement Durability Demonstration Project - NDOT 3716



Image Source: University of Nevada Reno

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Abstract

The fact that Department of Transportation (DOT) specifications always include compaction provisions reflects that asphalt pavement technologists have recognized the impact of in place density on pavement performance for many decades. However, an increase in durability related performance issues in the mid 2010's placed renewed focus on it. A recent literature review summarized past lab and field work which conservatively showed a 1 percent increase in density improves pavement life by 10 percent. It included information from the WesTrack project in Nevada that showed a 1 percent increase in density resulted in an improvement in rutting performance of 7 to 66 percent and 8 to 44 percent improvement in fatigue performance. The Federal Highway Administration (FHWA) has supported an *Increased In-Place Density Initiative* since 2015 with focus on communicating and providing education on the benefits of increasing in-place density of asphalt concrete pavements that State DOTs could volunteer to participate in.

This report describes a density demonstration project conducted by the Nevada Department of Transportation (NDOT). The project scope included two test sections for the typical roadway reconstruction under special provisions that increased the NDOT standard specification in-place mat density minimum requirements by one percent and two percent, respectively. A control section was also constructed. The contractor had the flexibility to make operational and equipment changes in the two test sections to improve in place density. Collectively, use of intelligent compactors, additional density QC staff, additional roller coverages and potentially an increase in asphalt content above the JMF target led to increased mat density and improved consistency when compared to the control data.

Key Words: In-place density, in-place air voids, asphalt pavement, pavement performance

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⁽Revised March 2003)

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Introduction

The fact that Department of Transportation (DOT) specifications always include compaction provisions reflects that asphalt pavement technologists have recognized the impact of density on pavement performance for many decades. However, an increase in durability related performance issues in the mid 2010's placed renewed focus on it. A recent literature review by the National Center for Asphalt Technology (NCAT) summarized past lab and field work which conservatively showed a 1 percent increase in density improves pavement life by 10 percent (1). It included information from the WesTrack project in Nevada that showed a 1 percent increase in density resulted in an improvement in rutting performance of 7 to 66 percent and 8 to 44 percent improvement in fatigue performance. The Asphalt Institute (AI) used the 1 percent increase in density to illustrate that a typical pavement expected to last 20 years when constructed to 93 percent density, would only last 18 years if constructed to 92 percent density. Furthermore, with the 2-year increase in service life a DOT would see a life cycle cost analysis (LCCA) net present value cost savings of \$88,000 on a \$1,000,000 paving project (8.8 percent) by increasing field density 1 percent (2).

The Federal Highway Administration (FHWA) has supported an Increased In-Place Density Initiative since 2015 with focus on communicating and providing education on the benefits of increasing in-place density of asphalt concrete pavements (3). The primary activities associated with the initiative have included:

- One-day workshops for DOTs and contractors describing the significant improvement in durability and reduction in life cycle cost that can be achieved with small increases in inplace density,
- Support of DOT demonstration projects that incorporate techniques that could lead to a 1 percent increase in density, and
- Communication of the demonstration project outcomes and techniques adopted by DOTs to increase in-place density.

This report describes a density demonstration project conducted by the Nevada Department of Transportation (NDOT) on SR 160 between Las Vegas and Pahrump Nevada. The project scope included two test sections, each representing one day of paving, for the typical roadway reconstruction under special provisions that increased the NDOT standard specification in-place mat density minimum requirements by 1 percent and 2 percent, respectively (4). The special provisions, presented in Appendix A, included a potential bonus incentivizing the contractor to achieve these requirements of \$2500 per lift and \$3500 per lift for the 1 percent and 2 percent increases, respectively. Quality assurance test results obtained during construct that included asphalt content, gradation, theoretical maximum specific gravity (G_{mm}) and in-place density were used to assess how effective changes made by the contractor were at improving in-place density.

Objectives

The primary objective of the demonstration project was to determine if a 1 or 2 percent increase in the current NDOT in-place density specifications could be reasonably achieved by means within a typical NDOT contractor's control. In order to do so the following had to take place:

- A special provision had to be developed defining the demonstration project requirements and incentive payment which incorporated large enough test sections to give the contractor a reasonable opportunity to meet the requirements,
- An upcoming project had to be selected to incorporate the special provision.
- Upon award of the project to the low bidder, a demonstration project workshop had to be conducted with NDOT, FHWA and contractor representatives present,
- A pre-construction meeting had to be held on the project site, at which NDOT, FHWA and contractor representatives discussed specific actions the contractor could take to meet the primary demonstration project objective,
- The contractor had to provide a written plan to NDOT outlining the changes that would be made for each test section, and
- The test sections had to be constructed with the necessary quality control (QC) and quality assurance (QA) inspection, sampling and testing performed with the results of it analyzed to assess conformance to the special provision.
- Important information from the effort had to be documented.

Project Information

A general description of the project follows along with a description of pre-construction activities which were important to the successful construction of the demonstration project test sections.

Location and Specifications

The density demonstration test sections were included in a NDOT project by special provision. They were constructed on a portion of the NDOT contract 3716 project located west of Las Vegas Nevada. The project limits are SR 160, Blue Diamond Road, from the west edge of Mountain Springs Community to the beginning of mountainous area SR 160 Blue Diamond Road, and from 1.03 Miles North of Mountain Springs Summit to the Clark County / Nye County Line. The project site plans are presented in Appendix B. The milepost limits are CL 16.51 to CL 22.20 and CL 21.96 to NY 0.95 with a project length of 28 miles. The project was awarded to Aggregate Industries SWR, Inc. on July 9, 2018 for \$58,561,165.00. All contract details, documents and award information can be found at the following NDOT website:

https://appss.nevadadot.com/EBiddingPortalClient/Contract/ViewContractDetails.aspx?contrac tld=10400# (5). The project included 505,855 yd³ of roadbed modification, 269,911 tons of Type 2C plantmix bituminous surface, and 30,134 tons of plantmix open-grade surface. The density demonstration test sections were constructed on a portion of east bound SR 160 just east of the Nye Clark County border. The roadway width is 36 feet, consisting of two travel lanes and a shoulder all with a 2 percent cross slope to the shoulder. The pavement section was a complete reconstruction consisting of 8 inches of roadbed modification on existing subgrade covered with 6 inches of plantmix bituminous surface (placed in two 3 inch lifts) topped with ¾ inch of plantmix open-grade surface. The NDOT standard specification sections for the roadbed modification, plantmix bituminous surface and plantmix open-grade surface are 305, 402 and 403, respectively. (6). The roadbed modification consists of pulverizing the existing bituminous mixture, aggregate and in some cases subgrade to a depth of 12 inches, with four inches removed and the remaining 8 inches modified with 2 percent portland cement prior to compaction. The plantmix bituminous surface was ¾" Type 2C with 15% reclaimed asphalt pavement (RAP) defined in specification section 705. Both the plantmix bituminous surface and plantmix open-grade surface incorporated PG76-22NV asphalt binder. An "E-prime" prime coat was applied to the roadbed modification at an application rate of 0.25 gallons per square yard. An application of SS-1H is then applied to the roadbed modification at a rate of 0.05 gallons per square yard prior to paving. A tack coat of SS-1H was applied between the lifts of plantmix bituminous surface at a rate of 0.06 gallons per square yard. The NDOT standard specification section for asphalt binder, prime coat and tack coat is 703. The ³/⁴ Type 2C with 15% RAP mix design is presented in Appendix C.

Pre-planning Activities

Pre-planning activities included a 1-day workshop and preconstruction meeting. The 1-day workshop, focused on best practices for improving in-place density, was presented by Asphalt Institute staff in Las Vegas on March 14, 2017 with key NDOT, Aggregate Industries SWR, Inc., and FHWA staff present. The demonstration test section construction was originally planned for the 2018 construction season but was delayed to the 2019 construction season. So, a WebEx was held January 30, 2019 with key NDOT, Aggregate Industries SWR, Inc., FHWA, and UNR staff participating to discuss the 2019 planning.

On March 27, 2019 a preconstruction meeting was held on the project site with key NDOT, Aggregate Industries SWR, Inc., FHWA and UNR staff present. A review of best practices for improving in-place density was presented by Timothy Aschenbrener of FHWA along with examples of what techniques contractors building other demonstration projects had used to successfully increase in-place density by at least 1 percent. Aggregate Industries staff provided initial thoughts on what techniques would be used on the test sections which was followed up with a written proposal May 6, 2019. A subsequent phone call with key NDOT, Aggregate Industries SWR, Inc., and UNR staff participating refined the plan to what is presented in Table 1. In summary, for the test section number 1 (plus 1 percent density) the techniques included all new intelligent compactors (IC) and doubling of on-site QC staff. For the section number 2 (plus 2% density) the techniques planned for test section 1 would be used along with an asphalt binder content increase of 0.1 percent and an increase in roller passes. Test section number 2 was placed directly on top of test section number 1. So, test section 1 was the bottom 3-inch lift and test section 2 were the top 3-inch lift.

Test Section	Staff changes	Material changes	Equipment changes	Operational changes
1 (plus 1% density)	Increase QC density technicians from 1 to 2	None	All new Caterpillar breakdown, intermediate, and finish roller equipped with Intelligent Compaction technology	None
2 (plus 2% density)	Increase QC density technicians from 1 to 2	Increase asphalt binder 0.1%	All new Caterpillar breakdown, intermediate, and finish rollers equipped with Intelligent Compaction technology	Increase roller passes

Table 1. Pre-construction Techniques Planned for Test Section Construction

Construction

Density test section number 1 was constructed June 26, 2019, and test section number 2 was construction June 28, 2019. It was originally planned that they would be constructed over two consecutive days, but a mechanical issue at the asphalt plant on the afternoon of June 26th led to a day between the two test sections. A description of mix production and transportation follows along with a summary of placement and compaction.

Mix Production and Transportation

The Type 2C plantmix surface was produced at the Aggregate Industries AWR, Inc. Sloan Pit facility located at 5300 Sloan Road, in Sloan Nevada south of Las Vegas. Figure 1 shows the location of the Sloan Pit and density test section located between to Las Vegas and Pahrump.



Figure 1. Sloan Pit and Density Test Section Locations (Google Earth)

Image Source: Google Earth

There are aggregate, hot mix asphalt and ready-mix concrete production at this location which is south of Las Vegas. The hot plant on site is an Astec Double Barrel Drum plant with six storage silos. Figure 2 is a picture of the hot plant type used to produce the Type 2C plantmix that was typically operated at 300 tons per hour.



Image Source: Adam Hand

Figure 2. Astec Double Barrel Drum Plant

Consistent with NDOT requirements, the plant was calibrated in January 2019 and an inspector visited the plant during the test section production. Production at the plant started each day at 1:30am with the first truck loading out at 3:00am. This allowed adequate haul time for paving to begin at 5:00am each day. The target mix production temperature was 330°F and was typically with 10°F of this. Only bottom dump haul trucks were used, with most having two trailers carrying approximately 38 tons per truck. All 27 trucks used were tarped to help retain mix temperature during the haul. The haul distance from the hot plant to the test section location was approximately 50 miles. There is a significant grade between the plant and test section location which resulted in an average haul time of about 90 minutes.



Image Source: University of Nevada

Figure 3. Typical Bottom Dump Haul Trucks

Placement and Compaction

The test sections were placed on a divided section of SR160 in the eastbound direction. The roadway width is 36 feet, consisting of two travel lanes and a shoulder. For both test sections the plantmix was placed in 3 passes in the eastbound direction, starting with the shoulder which was located at the bottom of the 2 percent cross slope. Figure 4 is a diagram of the paving which was repeated for each lift (test section) with the longitudinal joints offset by 6 to 12 inches.



Figure 4. Test Section Pavement Lane Layout and Approximate Dimensions

The equipment used for the test section construction is presented in Table 2. All of the same equipment was used for both test sections. The Caterpillar compactors were all brand new and equipped with intelligent compaction (IC) technology. The roller weights are included in Table 2. Note that ballast was not added to the CW34 pneumatic rollers. An intelligent compactor is a compactor equipped with the addition of the following capabilities:

- GPS based location mapping,
- Compaction surface temperature measurement,
- Compaction measurement value determination if a vibratory compactor, and
- On-board monitor/controller/data collection system

IC utilizes the Global Navigation Satellite System (GNSS) to correlate measurements to a physical location. Using a base station at the project location with a GPS receiver and transmitter improves precision of the positioning with real time kinematics (RTK). Figure 5 shows an onsite base station

with a GPS receiver and transmitter. Post processing of IC data can be performed using Vela software which is available at http://www.intelligentcompaction.com/veta/ (7). IC temperature and mapping features were used for the test section compaction. Representatives from Caterpillar and Sitech were on-site to provide roller operator training and GPS setup and support the day prior to and during construction of the test sections.

Equipment	Model	Units	Use/Notes
BearCat Distributor		1	Prime and tack coat
Roadtec Material Transfer Vehicle	SB2500	1	With windrow pickup
Caterpillar Paver	AP1055F	1	With automated grade controls and hopper extension
Caterpillar Steel Drum Roller	CB66B (14.5 ton)	1	Breakdown rolling with IC
Pneumatic Tire Roller with IC	CW34 (11 ton)	2	Intermediate rolling with IC, No additional ballast
Caterpillar Steel Drum Roller	CB66B (14.5 ton)	1	Finish rolling with IC
Volvo Steel Drum Roller	DD25B (2.8 ton)	1	Transverse joint construction only
Blaw Knox Kick Broom	CB-90	1	Sweeping prior to prime and tack coats

Table 2. Placement and Compaction Equipment



Image Source: University of Nevada Reno

Figure 5. GPS with RTK for Location Positioning to Generate Accurate Mapping

Prior to placement of the 3-inch bottom lift Type 2C plantmix a prime coat was applied with the BearCat asphalt distributor shown in Figure 6. The prime coat was uniformly applied.



Image Source: University of Nevada Reno

Figure 6. Asphalt Distributor Applying Prime Coat

Paving was initiated at 5am and completed by 3:30pm each day. Weather conditions during test section construction are summarized in Table 3. Paving initiated in the eastbound direction. Trucks dumped plantmix in a windrow and the Roadtec MTV was used to pick it up and mix it prior to discharging into the hopper on the Caterpillar AP1055F paver as shown in Figure 7. Breakdown rolling initiated immediately behind the paver with the Caterpillar CB66B roller using both vibratory and static compaction modes. A pair of tandem Caterpillar CW34 intermediate rollers followed the breakdown roller as shown in Figure 8. Finish rolling was accomplished with a second Caterpillar CB66B roller. Longitudinal joints were compacted from the cold side first as illustrated in Figure 9. It is important to note that joint density requirements were not included in the test section specifications. Roller coverages and plantmix temperatures during compaction are summarized in Table 4. Table 5 contains the stationing identifying the beginning and ending of paving along tonnage placed and plantmix loose mix sampling locations testing frequencies.

Test Section	Date Constructed	Ambient Temperature Range (°F)	Relative Humidity Range (%)	Wind Speed (mph)	Cloud Cover
1	06/26/19	73-102	low	5-18	none
2	06/28/19	71-101	low	5-10	none

Table 3. Weather Conditions During Test Section Construction



Image Source: University of Nevada Reno

Figure 7. Windrow pickup, Discharge into the Paver Hopper and Breakdown Compaction



Image Source: University of Nevada Reno

Figure 8. Tandem Intermediate Pneumatic Rollers

			· · · · · · · · · · · · · · · · · · ·	
Operation	Location	Temperature Coverages and m		Coverages and mode
Operation	LOCATION	Range (°F)	(Test section no. 1)	(Test section no. 2)
Asphalt Plant	Discharge	325-355	n/a	n/a
Dumping	Windrow	300-320	n/a	n/a
Breakdown	Behind	nd	2.5 vibratory	3 vibratory
rolling	paver	290-300	0.5 static	1 static
Intermediate rolling	multiple	200-290	4	4
Einich rolling			2 vibratory	2 vibratory
FILIISH FOILING	multiple	172-192	2 static	3 static

Table 4. Plantmix Temperatures, Roller Coverages and Modes

Table 5. Important Project Stations and Tonnage.

Test Section	Shoulder Stationing	Lane 2 Stationing	Lane 1 Stationing	Plantmix Tonnage	Density Lots / Sublots per	Plantmix Lots / Sublots per	Plantmix Mat Sample Stations
					Lot	Lot	otations
1	LE 300+15	LE 304+20	LE 304+20	2/21	2/5	1/2	LE 286+00,
1	to 233+16	to 236+50	to 238+68	2431	5/5	1/5	LE 286+50
2	LE 300+15	LE 300+15	LE 300+15	2200	2/5	1/2	LE 252+00,
Z	to 233+16	to 233+16	to 233+16	2360	5/5	1/3	LE 257+00



Image Source: University of Nevada Reno

Figure 9. Longitudinal Joint Compaction

Quality Control and NDOT Acceptance Sampling and Testing

NDOT performs all acceptance sampling and testing on its projects. Contractors perform quality control (QC) testing, though it does not have to be reported to NDOT. NDOT typically performs asphalt content, gradation and theoretical maximum specific gravity tests on loose mix sampled from the mat behind the paver as illustrated in Figure 10. On this project NDOT performed these tests in a field lab located not far from the project. One exception on this project was that gradations were performed on coldfeed samples taken at the asphalt plant. The reason for this is the aggregate has a tendency to breakdown excessively in the ignition oven. Aggregate Industries SWR, Inc. performed the same tests on mixture sampled at the Sloan Pit asphalt plant location and on split samples taken with NDOT from the mat.



Image Source: University of Nevada Reno

Figure 10. NDOT and Contractor Staff Obtaining Plantmix Samples from the Mat

Each test section represented a lot of plantmix. For each plantmix lot 3 sublot samples were obtained and tests performed. Per the special provisions each test section included 3 density lots randomly selected by NDOT during the paving operations. The selection of locations and nuclear density testing were performed in accordance with Test Method Nev. T335, which includes a

correlation with drilled cores (8). For each lot 5 mat density tests were performed using a calibrated nuclear density gage. Density is reported in percent relative to theoretical maximum specific gravity of the plantmix, which is determined in accordance with Test Method Nev. T325B (8). Each test section was a plantmix lot which included 3 sublots. Theoretical maximum specific gravity tests were performed on 2 of the sublot samples per test section. Both NDOT and contractor personnel used Troxler 4640B nuclear density gauges.

The contractor had two QC density technicians on the project full time, which is one more technician than normal. This made it possible for one technician to always be working with paver operator and the roller operators, with primary focus being on monitoring the breakdown compaction. The second technician worked with the other roller operators and assisted NDOT staff with mat sampling. Although the contractor does not formally report QC test results, Aggregate Industries staff did share results verbally and by writing them on the mat next to nuclear density gauge test locations as they were performed. At the first density test location the NDOT and contractor technicians performed density tests next to each other as an informal means of comparing nuclear gage performance/calibration at the start of the day.

Results

The NDOT quality assurance plantmix test reports are presented in Appendix D. The plantmix test reports include asphalt content (%AC), gradation, and theoretical maximum specific gravity. For each test section (day of paving one lift) three plantmix samples were obtained. Table 6 is a summary of plantmix test results. Note that theoretical maximum specific gravities were measured on the first two sublot samples each day of paving and were the basis for reported percent relative density. Individual gradation test results for each sample are presented in the appendix only. All asphalt and gradation test results were within specification tolerances. One of the actions the contractor planned to improve density was to increase asphalt content by 0.1 percent on test section 2. The JMF target was 4.2 percent. The average asphalt content observed on both test sections was 4.5 percent, so the actual increase was greater than planned and the same for both test sections.

Test Section	Sublot	Asphalt Content (%)	Theoretical Maximum Specific Gravity (pcf)			
1	1	4.4	160.9			
1	2	4.4	160.9			
1	3	4.6	-			
1	Average	4.5	160.9			
2	1	4.4	160.7			
2	2	4.6	160.6			
2	3	4.6	-			
2	Average	4.5	160.7			

Table 6.	NDOT OA	Plantmix Tes	t Result Summai	v
10010-01	11001 001		c nesanc samma	y

The NDOT quality assurance density test reports are presented in Appendix E. Table 7 is a summary of mat density results for both test sections showing individual sublot and the lot average values. The sublot values ranged from 93 to 95 percent relative density and all lot averages were 94 percent, with the exception of test section 1 lot 1. This is positive since the standard specification lower density limit is 92 percent.

Table 8 shows the percent within limits (PWL) and pay factors calculated for each lot with the standard specification and both test section special provision mat density requirements applied. Note that the values in bold and italic are the actual values for the two test sections. The other data is simply presented for those curious what the PWL and pay factors would be with each of the different specifications applied. It is important to recognize that when the standard specification is applied the pay factors for five of the six lots are 100 percent and the corresponding pay factors are all 105 percent with the except of one lot which is 99 percent. This illustrates that what the contractor did on both test sections to increase density led a very good quality per the current NDOT standard specifications. Appendix E Table E1, Table E2 and Table E3 show the four readings for each of the five individual sublot density test results reported along with lot averages for test section 1 and Table E4, Table E5 and Table E6 show the four readings for each of the five individual sublot density test results reported along with lot averages for test section 2.

Close review of Table 8 reveals that when the lower density specification limit was raised by 1.0% (test section 1) the observed PWL values were 69 to 95 percent and averaged 80 percent. The corresponding pay factors were 90 to 103 percent and averaged 97 percent. When the lower density specification limit was raised by 2.0% (test section 2) the observed PWL values were 19 to 60 percent and averaged 41 percent. The corresponding pay factors were 64 to 85 percent and averaged 75 percent. One could interpret the test section 2 data to suggest that an increase in mat density lower specification limit of 2 percent would be unreasonable, especially with the extra effort placed on test section 2. Interestingly though, when the test section 1 special provision is applied to the test section 2 observed densities it appears that a 1 percent increase in mat density lower specification limit might be reasonable. This statement is based on the observed PWL values of 87 to 100 percent and average of 91 percent. The corresponding pay factors were similar among the test sections, the only real operational difference between the test sections was additional breakdown and finish roller coverages.

		Sublot	Sublot	Sublot	Sublot	Sublot	Lot	
Tost		1	2	3	4	5	Average	Standard
Soction	Lot	Relative	Relative	Relative	Relative	Relative	Relative	Doviation
Section		Density	Density	Density	Density	Density	Density	Deviation
		(pcf)	(pcf)	(pcf)	(pcf)	(pcf)	(pcf)	
1	1	93.2	93.2	93.5	94.4	93.0	93.5	0.57
1	2	94.3	93.1	95.2	93.8	94.3	94.1	0.75
1	3	94.8	96.0	92.8	94.2	92.7	94.1	1.41
1	Average	94.1	94.1	93.8	94.1	93.3	93.9	0.91
2	1	94.4	93.1	93.1	93.9	94.8	93.9	0.78
2	2	93.3	93.5	94.3	93.0	93.7	93.6	0.49
2	3	93.7	94.6	93.8	93.8	94.3	94.1	0.41
2	Average	93.8	93.8	93.7	93.6	94.3	93.8	0.56

Table 7. Test Section QA Density Test Results Summary

Table 8. Test Section Percent Within Limits and Pay Factor Summary by Specification Type

Test	Lot	Standard	Standard	Special	Special	Special	Special
Section		Spec.	Spec.	Provision 1	Provision 1	Provision 2	Provision 2
		PWL	Pay Factor	PWL	Pay Factor	PWL	Pay Factor
		92-96%	92-96%	93-96%	93-96%	94-96%	94-96%
1	1	100	105	79	95	21	65
1	2	100	105	<i>99</i>	105	54	82
1	3	95	102	71	91	47	79
1	Average	98	104	83	97	41	75
2	1	100	105	88	99	46	78
2	2	100	105	91	100	23	66
2	3	100	105	100	105	58	84
2	Average	100	105	93	101	42	76

One of the objectives of the density demonstration projects is to compare the density that was being achieved by the contractor, under its normal operations, prior to applying the techniques planned for the demonstration project test section construction. Recall that the techniques select were to use all IC compactors, add a density technician and increase asphalt content (see Table 1 for more detail). The density being achieved under normal operations is referred to as a "Control" section. Table 9 is a summary of 28 density lots obtained on the same project using the same paving crew, asphalt plant and mixture prior to construction of the density demonstration test section. Individual sublot values range from 92 to 96 percent and the lot averages are 93 to 94 percent. The average for all Control lots is 94 percent.

	Sublot 1	Sublot 2	Sublot 3	Sublot 4	Sublot 5	Lot	
Lot	Relative	Relative	Relative	Relative	Relative	LUL Average	Standard
	Density	Density	Density	Density	Density	(ncf)	Deviation
	(pcf)	(pcf)	(pcf)	(pcf)	(pcf)	(per/	
1	92.4	92.9	92.6	92.7	94.0	92.9	0.62
2	92.7	93.6	93.1	93.9	93.5	93.4	0.49
3	94.2	92.7	94.4	94.2	94.4	94.0	0.74
4	94.0	94.9	94.3	92.4	93.3	93.8	0.96
5	94.2	92.9	93.9	93.5	93.5	93.6	0.46
6	93.3	93.7	93.9	94.3	92.9	93.6	0.53
7	92.3	92.5	92.9	93.8	93.2	92.9	0.59
8	93.3	94.8	93.6	94.6	93.9	94.1	0.63
9	94.5	94.8	93.5	94.3	94.4	94.3	0.46
10	93.4	93.4	93.9	93.4	94.2	93.7	0.37
11	93.6	93.3	93.8	95.7	93.3	93.9	0.99
12	94.2	93.0	93.9	93.3	92.6	93.4	0.64
13	93.6	93.1	93.8	94.0	94.2	93.7	0.44
14	93.4	95.0	92.8	94.5	93.4	93.8	0.88
15	92.7	93.1	93.8	92.9	92.8	93.1	0.42
16	93.3	92.6	94.0	95.3	95.1	94.1	1.16
17	93.7	94.2	93.9	94.7	93.8	94.0	0.41
18	94.3	95.2	95.9	93.2	93.2	94.3	1.20
19	93.4	93.3	93.1	93.9	93.2	93.4	0.32
20	94.4	92.5	93.2	93.0	93.0	93.2	0.70
21	92.8	93.4	93.0	92.8	92.6	92.9	0.32
22	94.0	93.9	93.4	94.0	94.2	93.9	0.28
23	92.8	93.8	95.2	95.1	94.7	94.3	1.03
24	94.0	93.9	92.9	92.6	92.6	93.2	0.69
25	93.0	93.7	94.4	93.1	94.0	93.7	0.58
26	94.6	93.7	93.6	93.9	92.6	93.7	0.72
27	93.2	93.1	92.8	93.2	93.1	93.1	0.18
28	93.3	93.0	92.1	94.7	91.8	93.0	1.14
29	94.0	91.8	91.9	93.1	93.0	92.8	0.89
Average	93.5	93.5	93.6	93.8	93.5	93.6	0.65

Table 9. Control Relative Densities Prior to Density Demonstration Project Test Sections

Table 10 shows a summary of the percent within limits (PWL) and pay factors calculated for the control and both test sections with the standard specification and special provision mat density requirements applied. Under the standard specification the PWL and pay factor for the control are slightly higher than test section 1 and slightly lower than test section 2. Under special provision 1 (+1 percent) the techniques used by the contractor resulted both test section 1 and test section 2 having higher PWL and pay factors than the control section. The same observation is made under special provision 2. The PWL increases from 77 to 91 and the corresponding pay factor increases from 94 to 101 percent under special provision 1. The PWL increases from 27 to 41 percent and the pay factor increases from 69 to 75 percent under special provision 2. The reason for the improved test section 1 and test section 2 PWL and pay factors is the densities observed in the test sections are more consistent than those observed for the control, which in turn positively impacts PWL and pay factor. If one only looks at the average density between the control and test sections 1 and 2 they appear to be the same. It is particularly interesting to note the significant difference in PWL and pay factors between the control and test section 2 under special provision 1, as this data also suggests that it may be reasonable to consider increasing the minimum density specification by 1.0%.

	Standard	Standard	Special	Special	Special	Special
	Spec.	Spec.	Provision 1	Provision 1	Provision 2	Provision 2
Test Section	PWL	Pay Factor	PWL	Pay Factor	PWL	Pay Factor
	92-96%	92-96%	93-96%	93-96%	94-96%	94-96%
Control	98	104	78	94	28	69
Test Section 1	98	104	83	97	41	75
Test Section 2	100	105	93	101	42	76

Table 10. Comparison of Control and Test Section Percent Within Limits and Pay Factors

Summary and Conclusions

A density demonstration project with a primary objective of determining if a 1 or 2 percent increase in the current NDOT in-place density specifications could be reasonably achieved by means within a typical NDOT contractor's control was performed. The special provisions for the project included significant bonus potential opportunity to incentivize the contractor to increase density. Different techniques were used by the contractor to try to meet the increased density levels on two test sections, each representing a day of paving (approximately 2500 tons). For the 1 percent increase all rollers were equipped with intelligent compaction technology and two, rather than one, QC density technicians were on the project fulltime. For the 2 percent increase these same techniques were used along with an increase in roller coverages and a planned increase in asphalt content.

NDOT acceptance test results showed that all plantmix properties were within specification tolerance and that the asphalt binder content measured during production was 0.3 percent above the job mix formula target value for both test sections. Mat density sublot values ranged

from 93 to 95 percent relative density and all but one lot averages were 94 percent. This is very positive since the lot averages were typically 2 percent higher than the NDOT standard specification lower limit of 92 percent.

An analysis of PWL and pay factors when applying the NDOT standard specification and two project special provisions was performed. When the standard specification was applied the pay factors for five of the six lots were 100 percent and the corresponding pay factors were all 105 percent with the except of one lot which was 99 percent. This illustrates that what the contractor did on both test sections to increase density led to good quality per the current NDOT standard specifications. When the lower density specification limit was raised by 1.0% (test section 1) the observed PWL values were 69 to 95 percent and averaged 80 percent. The corresponding pay factors were 90 to 103 percent and averaged 97 percent. When the lower density specification limit was raised by 2.0% (test section 2) the observed PWL values were 19 to 60 percent and averaged 41 percent. The corresponding pay factors were 64 to 85 percent and averaged 75 percent.

Even though it is a limited data set, the test section 2 data suggests that an increase in mat density specification limit of 2 percent would be unreasonable, especially with the extra effort placed on test section 2 by this contractor. Interestingly though, when the test section 1 special provision is applied to the test section 2 observed densities it appears that a 1 percent increase in mat density lower specification limit may be reasonable. This statement is based on the observed PWL values of 87 to 100 percent and average of 91 percent with corresponding pay factors of 98 to 105 percent, averaging 101 percent. A comparison of a control section consisting of 29 density lots, obtained on the same project prior to the density demonstration test section construction, showed that similar average density values were obtained between the control and test sections, but the test section data was less variable resulting in higher PWL and pay factor values.

Because asphalt contents were similar among the test sections, the only real operational difference between the test sections was additional breakdown and finish roller coverages. Collectively, use of intelligent compactors, additional density QC staff, additional roller coverages and potentially an increase in asphalt content above the JMF target led to increased mat density and improved consistency when compared to the control data. Other factors that contributed to improved density were the production per shift was relatively low (≈2500 tons) and equipment manufacture support was on site because all compactors used were brand new. With the resources available the time needed to achieve the required compaction did not slow down paving operations. Trucking was the limit factor on production rate.

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Appendices

Appendix A - Special Provision Excerpt

402.03.06 Compaction. Perform compaction according to "Method B."

The reference to Test Method No. Nev. T324 in the last sentence of the fourth paragraph on page 163 of the Standard Specifications is hereby changed to Test Method No. Nev. T325.

From station "XE2" 1144+42.70 to station "XE2" 1250+02.70, the third paragraph on page 163 of the Standard Specifications is hereby deleted and the following substituted therefore:

Each lift of each course of bituminous material will be divided into six "Test Sections" with three test sections located between station "XE2" 1144+42.70 and station "XE2" 1197+22.70 and three test sections located between station "XE2" 1197+22.70 and station "XE2" 1250+02.70.

From station "XE2" 1144+42.70 to station "XE2" 1197+22.70, the fourth paragraph on page 163 of the Standard Specifications is hereby deleted and the following substituted therefore:

 Compaction Requirements of Test Sections. The density of each test section will be evaluated based on the results of 5 nuclear tests taken at randomly selected locations within the sections as described in Test Method No. Nev. T335. The mean density of the 5 nuclear tests shall not be below 93% nor above 96% (with no single test below 91% nor above 97%) of the "Target" density achieved in the Department's Field Laboratory using Test Method No. Nev. T325. The Contractor will receive an additional \$2,500 per lift for each test section (3 total) meeting these requirements.

From station "XE2" 1197+22.70 to station "XE2" 1250+02.70, the fourth paragraph on page 163 of the Standard Specifications is hereby deleted and the following substituted therefore:

 Compaction Requirements of Test Sections. The density of each test section will be evaluated based on the results of 5 nuclear tests taken at randomly selected locations within the sections as described in Test Method No. Nev. T335. The mean density of the 5 nuclear tests shall not be below 94% nor above 96% (with no single test below 92% nor above 97%) of the "Target" density achieved in the Department's Field Laboratory using Test Method No. Nev. T325. The Contractor will receive an additional \$3,500 per lift for each test section (3 total) meeting these requirements.

Appendix B - Project Site Plans



Figure B.1. Project Site Plan Sheet 1.



Figure B.2. Project Site Plan Sheet 2.

Appendix C- Type 2C with 15% RAP Job Mix Formula

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STATE OF NEVADA DEPARTMENT OF TRANSPORTATION

> District One 123 East Washington Avenue Las Vegas, NV 89101 (702) 486-6677 FAX (702) 486-6680

Steve Sisolak Governor

March, 2019

Kristina Swallows, P,E. Director

Mr. Ron Adair, Project Manager Aggregate Industries SWR Inc. 4675 Teco Ave, Suite 140 Las Vegas, NV 89118 Contract No.3716 Project No. NHP-160-1(028) and NHP-160-1(029) Plantmix Surfacing (Type 2C)(Wet) w/RAP Mix Design No. BF19-013 Job Mix Formula No. 2

Dear Sir:

The following is **Job-Mix Formula No. 2** for the Plantmix Surfacing (Type 2) (Wet) to be used on Contract No. 3716. The hot plant is owned and operated by Aggregate Industries and is located in Sloan Pit. The mix design represents aggregates sampled in December 2018 from Sloan Pit mixed with PG 76-22NV supplied by **Alon**. Any modifications to the job-mix formula must be approved by the Engineer.

Sieve Size	Percent Passing	Job-Mix Range	Specification Range
1-Inch	100	100	100
¾-Inch	93	88-95	88-95
½-Inch	81	74-85	70-85
3/8-Inch	72	65-78	60-78
No. 4	53	46-60	43-60
No. 10	31	30-35	30-44
No. 40	14	12-18	12-22
No.200	7	5-8	3-8

The bitumen ratio to be added shall be <u>3.6%</u> (\pm 0.4% operational tolerance, Subsection 401.02.02) Alon Asphalt Cement, Grade PG 76-22 NV. The bitumen ratio of the recycled asphalt pavement (RAP) shall be 0.6%. The total bitumen ratio (after the ignition oven) shall be <u>4.2%</u>. Do not use the \pm 0.4% operational tolerance as a means to alter the bitumen ratio target value.

All aggregates with the exception of the recycled asphalt pavement (RAP) shall be marinated per Standard Specification Subsection 401.03.08 (Marination Method), using 1% lime for coarse aggregates and 2% lime for fine aggregates. The combined lime for the above bin percentages shall be 1.5%.

The Bin percentages shall be as follows:

19mm (3/4")	10% Sloan Pit
12.5mm (1/2")	20% Sloan Pit
9.5mm (3/8")	12% Sloan Pit
Chips	13% Sloan Pit
Crusher Fines	30% Sloan Pit
1/2" RAP	15% Agg Industries

Appendix D - NDOT Plantmix Quality Assurance Test Results

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Mr. Ron Adair, Project Manager Aggregate Industries SWR Inc. March 7, 2019 Contract No.3716 Project No. NHP-STP-0160(028), (029) Plantmix Surfacing (Type 2C)(Wet) w/Rap Mix Design No. BF17-13 Job Mix Formula No. 2

No baghouse fines are allowed to be introduced into the mix, until that material is included in the plant calibration. If included in the plant calibration, the baghouse fines will not exceed 2% by dry mass of the aggregate and must remain consistent.

Target temperature of the mixture in the hauling vehicle leaving the plant shall be a minimum of 320 °F, although a higher temperature may be advisable for better workability and compaction, with a maximum temperature at the plant of 350 °F, and a maximum 20 °F drop in temperature from the time the mix leaves the plant until arriving at the paver drop.

The minimum temperature at the site of placement shall not be below 300 °F.

All percentages are based on dry weight of aggregate and RAP.

Should you have any questions, please contact this office.

Sincerely,

DocuSigned by Don Unistiansen P.E.

Don J. Christiansen, P.E. Resident Engineer

> pc: Sami Lompa, P.E., Assistant Construction Engineer; Mario Gomez, P.E., Assistant District Engineer; Darin Tedford, P.E., Chief Materials Engineer; Las Vegas Progress Lab; Jayson Vorce, Quality Assurance; District One Lab; PBS2C J1 /BF19-013 3716

THEORETICA	L MAXIMUM SPECIFIC GRAVITY OF E	BITUMINOUS PAVING MIXTURES (FIELD METHOD)	
Material Type: Tested By: Sampled By: Sampled From Station: Lot / Sublot:	TYPE 2 C W/GLAP D. VALLEDOR D. VALLEDOR "LF" 2016 400	Date: 6/26/19 Contract Number: 37/6 Test Number (same as burn-off): 7-1-48 Time of Day: 7:30 AM	

FIELD RICE RESULTS

2642.3
7745.7
9363.4

APPARENT SPECIFIC GRAVITY

A/[(A+B)-C]=	2.579
--------------	-------

DENSITY

S.G. x 1 Mg/m³ = $\frac{2.579}{160.9}$ Mg/m³ S.G. x 62.4 ibs/ \hbar^3 = $\frac{160.9}{100.9}$ ibs/ \hbar^3

Resident Engineer:

0 DON CHRISTIANSEN, P.E.

NDOT 040-030 08/10 RESIDENT ENGINEER Distribution: Headquarters Construction, District, Resident Engineer, Contractor

THEORETICAL MAXIMUM SPECIFIC GRAVITY OF BITUMINOUS PAVING MIXTURES (FIELD METHOD)

Material Type:

Tested By:

Sampled By:

Sampled From Station:

Lot / Sublot:

TYPE 21 WEAP
D. VAUEDON
D. BUT LER
"LE" 206+50
- POPTSU

Date:	6/26/19
Contract Number:	3716
Test Number (same as	s burn-off): 7-2-48
Time of Day:	10:15 Am

FIELD RICE RESULTS

"A" = Mass of sample in air

"B" = Mass of pycnometer and water

"C" = Mass of evacuated sample, pycnometer and water

APPARENT SPECIFIC GRAVITY

A/[(A+B)-C]=

2.578

2681

9

5

DENSITY

S.G. x 1 Mg/m³ =

S.G. x 62.4 lbs/ft3 =

.578 Mg/m³ 160.9 lbs/ft³

Resident Engineer:

DON CHRISTIANSEN, P.E. RESIDENT ENGINEER

NDOT 040-030 08/10

Distribution: Headquarters Construction, District, Resident Engineer, Contractor

THEORETICAL MAXIMUM SPECIFIC GRAVITY OF BITUMINOUS PAVING MIXTURES (FIELD METHOD)

Material Type: Tested By: Sampled By: Sampled From Station: Lot / Sublot:	74PE 2 C W / FAP D. VALLEOUR D. VALLEDOR "LE" 257 +20	Date: Contract Number: Test Number (same as b Time of Day:	6/28/19 3716 num-off): <u>7-1-49</u> 7:18 AM
	FIELD R	ICE RESULTS	
"A" = Mass of "B" = Mass of "C" = Mass of	f sample in air f pycnometer and water f evacuated sample, pycnometer and	$\frac{2654.6}{7748.1}$ d water $\frac{9372.2}{7}$	
APPARENT S	SPECIFIC GRAVITY A/[(A+B)	-c]= <u>2-576</u>	
DENSITY			
	S.G. x 1 Mg/m ³ =	2.576 Mg/m ³ (60.7 lbs/ft ³	
Resident Eng)	

DON CHRISTIANSEN, P.E. RESIDENT ENGINEER

NDOT 040-030 08/10

Distribution: Headquarters Construction, District, Resident Engineer, Contractor

JRG

THEORETICAL MAXIMUM SPECIFIC GRAVITY OF BITUMINOUS PAVING MIXTURES (FIELD METHOD)

Material Type:	TYPE 2C W/PAP	Detry	(do D)19
Tested By:	D. VAUEDOR	Date;	
Sampled By:	DIBUTVER	Contract Number:	3716
Sampled From Station:	"VE" 252 +00	Test Number (same a	ss burn-off): <u>7-2-49</u>
Lot / Sublot:	100	Time of Day:	10:40 Am

FIELD RICE RESULTS

"A" = Mass of sample in air

"B" = Mass of pycnometer and water

"C" = Mass of evacuated sample, pycnometer and water

APPARENT SPECIFIC GRAVITY

A/[(A+B)-C]=

2.574

2636.6

C360

3

JEG

5

DENSITY

S.G. x 1 Mg/m³ = 2.574 Mg/m³ S.G. x 62.4 lbs/ft³ = 60.6 lbs/ft³

Resident Engineer:

DON CHRISTIANSEN, P.E. RESIDENT ENGINEER

NDOT 040-030 08/10

Distribution: Hoodquarters Construction, District, Resident Engineer, Contractor

Elapsed Time: 85:00 Sample Weight: 2539s Weight Loss: 137.7s Percent Loss: 5.42% Temp Comp: 0.07% Calib. Fator: 1.02% Bitumen Ratio: 4.64% _____ Calibrated Asphalt Ctnt 4.33% Filter Set Pt: 750 C Chember Set Pt: 482 C Tested By: D.VA.VAPON MIX Type: TYPE 26 W/ CAP Sample 10:1-1- 48 Time: 6:06:53 Date: 06-26-19

and the second se
Elapsed Time: 86:00 Sample Weight: 2586s Weight Loss: 133.79 Percent Loss: 5.17% Temp Comp: 0.09% Calib. Factor: 1.02% Bitumen Ratio: 4.35%
Calibrated Asphalt Ctnt 4.07%
Et Li es Cab Dh 750 C
Filter Set Pt: 750 C
Chamber Set Pt: 402 L
Tested By: D. VAULANOP
MIX Type: Type 20 W/CA
Sample 10: 7-2-78 Time: 10:38:06 Date: 06-26-19

Elapsed Time Sample Weigh Weight Loss: Percent Loss Temp Comp: Calib. Facto Bitumen Rati	13 14:22 13 13 14:25 14	96:00 26209 35.79 5.18% 0.06% 0.06%	
Calibrated A 4.1	spha O%	It C	t nt
Filter Set P Chamber Set	t: Pt:	750 (482	==== C
Tested By:	J.F	bres	5
MIX Type: Typ	pe Z	cw/	AP
Sample 1D: Time: 16:47:2 Date: 06-26-1	29	3-4	8

Rev. 10/17

10 STATE OF NEVADA DEPARTMENT OF TRANSPORTATION Report No.: Contract No. 3716 DAILY PLANT REPORT OF ASPHALT MIXTURES Contractor: 4 INDUSTRIES FIELD TESTER'S REPORT 62619 PLANT INSPECTOR'S REPORT STREET INSPECTOR'S REPORT Date: Sampled/Tested by: P.V. P.B J.F 26 19 Contract No.: 3716 Date: 6: 26.19 Contract No.: 3716 SIEVE ANALYSIS SAMPLES D. Kalling by: Inspection by: Specification References: **105.03.01.101.05.01.101.02.02** Mix Design No.: **BF 19-13** Job-Mix Formula No.: **02** CJU) Dover Drum Type of plant: Weather Conditions: _____ Job-Mix Formula No.: 02 b-Mix Bitumen Ratio: 4-2 ocation of plan Type of mix: TIPE 2C-W PAP ocation of plant: Aggregation (Sloan Atmospheric temps: Job-Mix Bitumen Ratio: Low: 67 Alon P6 76-22 High: 97 ce temps: Low: 109 High: 134 Sample Number Job-Mix Type of asphall coment: Specificatio NU RUNNING YIELD CHECKS Limits Source of coarse agg.: Agreete Bitumen Ratio ype of mineral filler. Hydro tod ± 0,4 % Moisture (belt) 0.00 0.00 0.00 100 100 100 100 63 90 93 88-95 177 43 47 71-85 43 69 72 65-78 -4 56 46-60 -2.25 Type of mineral filler. % Moisture (mix) hime 1% Max Type of Mix: 2c W / RAP Pass 1" Mix Design No.: BF 19-13 00 Mix Design reo... Job-Mix Formula No.: 02. toh-Mix Bitumen Ratio: 4.2 1/0 93 90 47 43 43 69 57 54 32 3 304+20 5272+50 Pass 3/4" 4:30 88-95 Pasa 1/2" Pass 3/8" 3170 30.64 29.93 102.2 70-85 43-60 REPORT OF ASPHALT QUANTITIES Pass No. 4 56 54 mix produced (before waste): 2431.06 (one Pass No. 10 TPB Field + Length x Witth x Dep TPS Field + Length x Witth x Depi Yield % + TPS Field + TPS Field x Plantmix wasted/rejected at plant: 30.35 30-44 -0 Pass No. 16 eason for waster Pass No. 40 REPORT OF ASPHALT QUANTITIES 15 15 16 12-18 12-22 Pass No. 200 Total plantmix delivered to paver: 7 17 B 3-8 5-8 2431.590 Total plantmix wasted at paver: Sample Nun REPORT OF TEMPERATURES AT PLANT Job-Mit cification 52. 47 long Total plantmix placed: (delivered) led minimum asphalt cement temp: _______ G Range Limits 2378.59 ion JMF Mix temp. range: Resson for waste: Truck Bilumen Ralio 320 to E ± 0.4 350 broke. donte, Test Time Asphalt Plantmix Time % Moisture (belt) and End of the day excess Asphalt Plantmix % Moisture (mix) 1140A 345'F 1% Max. 2: 10 A 341 "F 3: 10 A 346 "F Pass 1" REPORT OF TEMPERATURES AT PAVER Pass 3/4" IMF Minimum mix temperature at paver: Time Plantmix Time Plantmix Time Plantmix Pass 1/2" 4:30 A 344 "F 5:00 328 10:20 334 4:30 327 5:45 335 11:02 332 Pass 3/8" 5:35A 340"F Pass No. 4 6:54A 334" F Pass No. 10 6:25 331 1:20 335 7: 16A 338'F 715 332 7:05 334 Pass No. 16 8:28 # \$40'F 8:45 327 7:55 331 Pass No. 40 91254 355 "F Pass No. 200 9.05 329 3.25 329 9:50 328 3:55 329 Remarks: 7-2-48 ON YZ' STEVE FALLED SCREEN Remarks: Remarks: Shoulder 10 width 3" depth Lana 1 16 width 3" depth 140.9 am 160.9 000 Distribution: HQ Construction, District, Resident Engeer, Contractor 'NUUT '040-011 Resident Engine

RESIDENT ENGINEER

Elapsed Time: 85:00 Sample Weight: 25379 Weight Loss: 130.38 Percent Loss: 5.14% Temp Comp: 0.05% Calib. Factor: 1.02% Bitumen Ratio: 4.35% Calibrated Asphalt Ctnt 4.07% Filter Set Pt: 750 C Chamber Set Pt: 482 C Tested By: D. AUDOP MIX Type: TYPE 26 N/R 7-1 Sample ID: Time: 6:02:50 Date: 06-28-19

Elapsed Time: 86:00 Sample Weisht: 25509 Weisht Loss: 138.29 Percent Loss: 5.42% Temp Comp: 0.07% Calib. Factor: 1.02% Bitumen Ratio: 4.64% *********************** Calibrated Asphalt Ctnt 4.33% == Filter Set Pt: 750 C Chamber Set Pt: 482 C Tested By: D. VAUEDON TYPE 20 WRAP Mix Type: Sample 10:1-2 40 Time: 9:09:56 Date: 06-28-19

Elapsed Time: 98:00 Sample Weight: 27489 Weight Loss: 148.49 Percent Loss: 5.40% Temp Comp: 0.05% Calib. Factor: 1.02% Bitumen Ratio: 4.63% Calibrated Asphalt Ctnt 4.33% Filter Set Pt; Chamber Set Pt; 750 C 482 C Tested By:_ J.F Mix Type: LVD 20 1 Sample 10: Time: 13:55:55 Date: 06-28-19

Standard State	9 Sa	mpled/Tes	ited by:	V. p.B/=	S.F. D.1	1	PLANT INS	PECTOR'S	REPORT		STR	EETIN	SPECT	OR'S F	REPOR	т
	SIL	VE ANAL	YSIS SAR	PLES			Cate. Graning C	onvact No.:	3/16	Date:	6.2	8.19	Contract	No.:	3710	
Specification Refe	rences: 1	105.03	014-1	02.09 V		10	inspection by:	KAlling	10 M	linspe	tion by:	C	202		210	
Mix Design No.: P	SEIN	-13	Job-N	fix Formula No	1.02.02	-lii	I speller af start	er Dru	im	Weat	er Condi	tions:	Sun	114		-
Type of mix: 1P	EZCW	PAD	Job-Mix E	Situmen Ratio:	4.2	-l#	Source of emball comes	greate	(SleAN)	Atmos	pheric ter	mps: L	.ow: 7	P	High:	100 1
a second a second second	S	ample Nu	nber	Job-Mix	Specification	-13	Tupo of period	- Alon		Surfac	e temps:	L	ow: 7	z	High:	180 1
service in the	1-1-40	17-2.4	17-34	Range	Limits	" [!]	Source of seams and	P6 76	-12 NV		R	RUNNI	IG YIEL	CHEC	KS	
Bitumen Ratio	4.4	4.0	4.6	38-46	+04	-10	Source of the age :	A 491094	2	Time	Line/	Station	Length	TPS Flet	TPR PL	Viold W
% Moisture (belt)	1.9	1.5	1.3	10.0 1.0	- 0,4	Hil	Type of mineral Sloc	Prente	1.	7:4	1 26	5+85		-	- IT OF TA	1 1010 75
% Moisture (mix)	0.00	0,00	0.00		1% May		Type of Mix:	ryarated	lime		23	3+16	32 60	10 90	10.00	
Pass 1"	100	00	100	100	100	-18	Mix Design No	19 KAP		1				1000	10.01	100
Pass 3/4"	13	90	91	88-95	80.9-	-11	Job-Mix Formula No	17-13		1:30	14 2T	2+50	1.		f	<u> </u>
² 888 1/2"	79	76	75	74-85	20-05	-Hill	Job-Mix Bilumon Ratio	11 - 7.		E	2P 231	8+68	2282	20.7	34.0	00.0
asa 3/8"	44	42	TT	15-70	10.05	-111	REPORT OF A	9.2.11	ANTITICA				-104	49.72	-30,20	49.4
ass No. 4	58	56	55	46-60	12 1B	-111	Planimix produced (hefer	SPHALT QU	ANTITIES				_		-	
ass No. 10	34	31	30	20,25	30 41	-111	Plantmix wasted/missied	at plants	2317.80 dans	TP3 Flet	i = Longih x V	Mith x Dep	A Martin Martin State	2) x % carr	Durtina - 7	
ass No. 16		-1	70	20105	20-14	-1:11	Reason for waste:	er biaut:	tons	Vield %	TPS Field +	Vidin x Dept TP8 Pies x	100 to 100	shown in t	te plana) +	2000
ass No. 40	17	16	15	12.18	10.20	-81				11	REPOR		SPHALT			
ass No. 200	0	G	2	12-10	12-22	-!!!		_		Total pla	ntmix del	livered t	o navo-	JUAN	THES	
	Sa	unie Num	her	Job Mile	30	lill	PEROPT OF THE	DEDATIN		Total pla	nimix wa	steri at :	v paver.	_	2379	80 lons
State 1	50	upo ridil		JOD-MIX	specification		Sperified minimum	PERATURES	AIPLANT	Total pla	númix ela	ced: and	pernet:		<u> </u>	80 lons
lumen Ratio	1997			Range	Limits		JMF Mix temp, range-	a coment tem	320	Reason	or waste		L_		2370	lons
Moisture (belt)			-		± 0.4	1168	Time Asphall Ct.	520	10 350 C	day	P. P. C	<u>165</u>	Tand	end	<u> </u>	the.
Moisture (mix)	-				1.42. 7	li li	1'40 A OPLIC	nix Time	Asphalt Plantmix	13				_		
and the second		-	-		1% Max.	1:II	1. 1. A 936 F			P	FRORT 4		00040			
358 1 [*]	1.00	-	_		1.5. 1.4.		2. 30M 3:4/P	1-1		JME Mint		Inmaci	PERATU	RES AT	PAVE	R
ass 3/4"	ALC: NO. 1011				62.54		2. 2A 337/P	+ +	_	Time	Dianta	ampen	anne al b	aver:	30	0 F
155 1" 158 3/4"			2.00		1	11FF	1. 2 A 231 P			Cine	- Janumb	Time	Plan	mix 7	ime I	Plantmix
155 1* 155 3/4* 155 1/2*						a : 11 P P										
ass 3/4" ass 3/4" ass 1/2" ass 3/8" as No. 4		-					5:34 A 338 P			5.00	205	10.4	0 33	2		1
ass 1* ass 3/4* iss 1/2* iss 3/8* ass No. 4 ass No. 4	_	-					5:34 A 338 P			5:45	379	11:30	33	2		
aas 1" ass 3/4" ass 1/2" iss 3/8" iss No. 4 iss No. 10							5:34A 338"P 6:264 335"F 7:544 336"P			5:45	379	11:30	330	2		_
aas 1" ass 3/4" ass 1/2" ass 3/8" ass No. 4 ass No. 10 ass No. 16							5:34 338 P 6:264 355 F 7:544 356 P 8:25 A 357 P			5:45	379 379 340 339	11:30	0 33 330 320 329	2		
ass 3/4" ass 3/4" ass 3/8" ass 3/8" ass No. 4 ass No. 10 as No. 16 ass No. 40							5:34A 338'P 6:2ca 355'F 7:54 355'F 8:25A 357'P 8:25A 337'P 9:354 342'P			5:00 5:45 6:30 7:25 8:20	379 379 349 339 325	11:30	330 330 320 320 376			
ass 1" ass 3/4" ass 1/2" ass 1/2" ass No. 4 ass No. 4 ass No. 10 ass No. 10 ass No. 10 ass No. 200							5:34A 338 'P 6:264 335 'F 7:544 332 'P 8:25A 337 'P 7:354 342 'P			5:00 5:45 6:30 7:25 8:20 8:50	329 379 339 325 332	10:9 11:30 12:10 12:5 1:55 2:35	330 330 370 370 370 370			
sss 1" sss 3/4" sss 1/2" sss 3/8" sss No. 4 sss No. 10 sss No. 10 sss No. 10 sss No. 200 marks: Matter							5:34 338 P 4:24 335 P 7:34 38(1) 8:25 A 537 P 7:354 342 P Remarks:			5:00 5:45 4:30 7:25 8:20 8:50 9:50	325 379 347 325 325 332 332	10:9 11:30 12:54 1:55 2:35	330 330 329 329 329 338			
ass 1/2 ass 3/4" ass 3/2" ass 1/2" ass No. 4 ass No. 10 ass No. 10 ass No. 10 ass No. 10 ass No. 20 marks: <u>Marke</u>		met	911	regained	Specs.	Re	5:3*A 338"F 4:2cA 355"F 7:5*A 35(') 8:25A 337"F 1:35A 342"F Remarks: marks:			5:00 5:45 4:30 7:25 8:20 8:50 9:50 8:50 8:50	325 379 327 325 325 332 339 5km	10:9 11:30 12:50 12:50 1:55 2:35	330 330 320 370 370 370			
ass 3/4" ass 3/4" ass 3/7" ass 3/8" ass 3/8" ass No. 1 ass N		met	911	regeired	specs.	Re	5134A 338 P 612ca 355 P 612ca 355 P 7594 552 P 8125A 357 P 9125A			5:00 5:45 4:30 7:25 8:20 9:20 9:20 Remarks:	325 339 339 325 332 332 339 5hould	10:9 11:30 12:10 12:5 1:55 2:35	0 33 330 320 370 370 370 370			
ass 3/4" ass 3/4" ass 3/2" ass 1/2" ass 1/2 ass 1		met	م(ا	regoired	Specs.	Re	51344 338 P 41244 335 P 4124 335 P 334 P 81254 357 P 81254 257 P			5:00 5:45 4:30 7:25 8:20 8:50 9:20 Remarks:	325 379 339 325 339 339 339 5hould 16 Wid	10:9 11:30 12:10 12:55 1:55 2:35 2:35	0 33 330 330 370 370 370 370 370 370 370 3			

RESIDENT ENGINEER

Appendix E - NDOT Density Quality Assurance Test Results

Tables E1 through E6 show the four readings for each of the five individual sublot density test results reported along with lot averages.

Test #	133-PM-	133-PM-	133-PM-	133-PM-	133-PM-	Average
	1	2	3	4	5	0
Station (nearest 25	295+75	289+00	281+00	277+00	271+50	n/a
ft.)						
Distance from Edge	2	7	1	2	7	4
(ft)						
Left or Right	Left	Left	Left	Left	Left	Left
Reading #1 (pcf)	149.5	149.7	149.7	152.0	149.8	150.1
Reading #2 (pcf)	150.6	149.4	150.3	151.1	150.5	150.4
Reading #3 (pcf)	149.7	150.0	150.1	152.4	148.9	150.2
Reading #4 (pcf)	149.9	150.6	151.8	152.2	149.2	150.7
Average (pcf)	149.9	149.9	150.5	151.9	149.6	150.4
Correction Factor	1.0	1.0	1.0	1.0	1.0	1.0
Corrected Density	149.9	149.9	150.5	151.9	149.6	150.4
(pcf)						
% Relative	93	93	94	94	93	93
Compaction						

Table E1. Test Section 1 Lot 1 Mat Density Test Results (06/26/19).

Table E2. Test Section 1 Lot 2 Mat Density Test Results (06/26/19).

Test #	134-PM-	134-PM-	134-PM-	134-PM-	134-PM-	Average
	1	2	3	4	5	
Station (nearest 25	303+50	291+00	286+50	276+50	271+25	n/a
ft.)						
Distance from Edge	3	4	8	5	4	5
(ft)						
Left or Right	Left	Left	Left	Left	Left	Left
Reading #1 (pcf)	151.7	149.9	152.6	150.1	150.3	150.9
Reading #2 (pcf)	150.9	150.3	153.9	151.8	152.5	151.3
Reading #3 (pcf)	152.3	150.0	152.8	150.8	152.2	151.6
Reading #4 (pcf)	151.7	149.0	153.2	150.8	151.7	151.3
Average (pcf)	151.7	149.8	153.1	150.9	151.7	151.4
Correction Factor	1.0	1.0	1.0	1.0	1.0	1.0
Corrected Density	151.7	149.8	153.1	150.9	151.7	151.4
(pcf)						
% Relative	94	93	95	94	94	94
Compaction						

Tost #	12E DM	125 DM	12E DM	125 DM	125 DM	Average
Test #	132-5161-	132-5101-	132-5101-	132-5101-	132-5101-	Average
	1	2	3	4	5	
Station (nearest 25	300+25	292+25	289+00	281+00	278+00	n/a
ft.)						-
Distance from Edge	9	15	1	6	5	7
(ft)						
Left or Right	Left	Left	Left	Left	Left	Left
Reading #1 (pcf)	152.7	153.9	148.9	150.8	148.2	150.9
Reading #2 (pcf)	152.2	155.9	149.7	151.2	149.2	151.6
Reading #3 (pcf)	153.3	154.2	149.7	152.6	149.8	151.9
Reading #4 (pcf)	151.8	154.0	148.8	151.7	149.3	151.1
Average (pcf)	152.5	154.5	149.3	151.6	149.1	151.4
Correction Factor	1.0	1.0	1.0	1.0	1.0	1.0
Corrected Density	152.5	154.5	149.3	151.6	149.1	151.4
(pcf)						
% Relative	95	96	93	94	93	94
Compaction						

Table E3. Test Section 1 Lot 2 Mat Density Test Results (06/26/19).

Table E4. Test Section 2 Lot 1 Mat Density Test Results (06/28/19).

Test #	136-PM-	136-PM-	136-PM-	136-PM-	136-PM-	Average
	1	2	3	4	5	
Station (nearest 25	259+75	253+25	251+75	245+00	236+75	n/a
ft.)						
Distance from Edge	2	10	10	3	2	5
(ft)						
Left or Right	Left	Left	Left	Left	Left	Left
Reading #1 (pcf)	153.9	149.0	149.4	152.6	154.1	151.8
Reading #2 (pcf)	150.8	148.9	148.8	151.3	150.5	150.9
Reading #3 (pcf)	151.4	149.1	150.9	149.6	153.7	150.6
Reading #4 (pcf)	150.8	151.3	149.3	150.2	151.3	150.8
Average (pcf)	151.7	149.6	149.6	150.9	152.4	150.8
Correction Factor	1.0	1.0	1.0	1.0	1.0	1.0
Corrected Density	151.7	149.6	149.6	150.9	152.4	150.8
(pcf)						
% Relative	94	93	93	94	95	94
Compaction						

Test #	137-PM-	137-PM-	137-PM-	137-PM-	137-PM-	Average
	1	2	3	4	5	
Station (nearest 25	266+25	257+50	251+75	244+00	237+00	n/a
ft.)						
Distance from Edge	1	3	6	4	4	4
(ft)						
Left or Right	Left	Left	Left	Left	Left	Left
Reading #1 (pcf)	149.4	150.6	152.2	149.0	150.5	150.3
Reading #2 (pcf)	149.8	151.1	151.1	149.3	150.2	150.3
Reading #3 (pcf)	149.9	149.1	151.2	149.9	150.7	150.2
Reading #4 (pcf)	150.8	150.4	151.4	149.4	150.9	150.6
Average (pcf)	149.9	150.3	151.5	149.4	150.6	150.3
Correction Factor	1.0	1.0	1.0	1.0	1.0	1.0
Corrected Density	149.9	150.3	151.5	149.4	150.6	150.3
(pcf)						
% Relative	93	94	94	93	94	94
Compaction						

Table E5. Test Section 2 Lot 2 Mat Density Test Results (06/28/19).

Table E6. Test Section 2 Lot 3 Mat Density Test Results (06/28/19).

Test #	138-PM-	138-PM-	138-PM-	138-PM-	138-PM-	Average
	1	2	3	4	5	
Station (nearest 25	267+75	260+25	256+50	249+75	240+75	n/a
ft.)						
Distance from Edge	11	16	12	10	9	12
(ft)						
Left or Right	Left	Left	Left	Left	Left	Left
Reading #1 (pcf)	151.4	152.8	150.5	150.3	152.5	151.5
Reading #2 (pcf)	150.9	152.2	150.1	151.2	150.8	151.0
Reading #3 (pcf)	150.7	151.6	151.5	150.5	150.9	151.0
Reading #4 (pcf)	149.9	151.8	151.1	151.2	152.2	151.2
Average (pcf)	150.5	152.1	150.8	150.8	151.6	151.2
Correction Factor	1.0	1.0	1.0	1.0	1.0	1.0
Corrected Density	150.5	152.1	150.8	150.8	151.6	151.2
(pcf)						
% Relative	94	95	94	94	94	94
Compaction						

Material Type Lift, Lane & Direction Width and Depth Lot/Sublot	PBS Type	e 2C W/RAP ane 3 shoulder, ED 3° D	Contract Nu Date Gauge Set N Tested By	mber <u>37/0</u> 6/20 lumber <u>148</u> D. 30	6 /19 +les	
Sta. 29	5+79 Sta.	288+97 Sta.	SECTION	ta. 277+10	Sta. 271+45	
1.	-					7
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8	¢.		<u>्</u> र			0
3	5	5	5		6 6	4
Random Number Blo	ck:	Beg	inning Station	10"300+15	7	-
		End	Ing Station	26" 265+85		
(A x length = longitudinal ,	B x width = transverse	e)	_			
686 .	0120	[Had al	В			
626	0.636	436.3	10	x 0.193	= 2.0	
686	12 804	732.2	10	x 0.673	5 = 6.7	1
686 8	0.310	201.0	10	x 0.112		1.8
686 x	0.183	1255	10	X 0.19	= 1.9	- 103
		163.2		A 10,05	- <u>6.</u> S	-
TARGET DENSITY N	la/m ³ (net)	602 9	Error (BIOE)		1 110	
TEET#			From (RICE) t	est number	-1-48	_ 323
IESI#	135PM- 1	133 -PM- 2	133-PM- 3	133-PM- 4	133-PM- 5	1993
STATION	295+75	289400	281+00	277 +00	271+50	
Distance (control la	2 1				211700	1. 13. 2
Ulstance from edge	- Joint	7 * Joint	Joint	2 * Join	t 7 * Joint	
Left of Right	LUAC	47	61	LT	LT	1.31
DENSITY	160%	149.1	149.7	157.0	149,8	-
READINGS	1497	199.9	150.5	151.1	150.5	
READING0	149 9	150.0	120.1	152.4	198.9	
Averane Denelty	149 9	149.0	151.0	1510	147.4	1
Corrected Density	149.9	149 9	150.5	151.7	149.6	-
% Relative Compartion	93	92	94	94	92	-
Minimum compaction	1131		1.17	77	73	
Correction Factor		1.00				
		1.00	F	temarks: Test	section meets	
* Mean Test Section	Density, Mg/m ³ (p	of)= (50.4	4 Special	Provision requir	ed spec plus	
* Mean Percent relati	ve Compaction=	93	spec.	AT Specie	1 Provisions	
* Not Applicable	to Partial Test Se	actions or Joint Densiti	es Single: 71	SPEC	402.03.06	
24 - P			Mean : 93	3-96	A. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	
Joint Test Specificati	on	Min. 90	V.			
Single Test Specifica	ition	Min. 90	Max. 97		arrest r	
Mean Test Section S	pecification	Min. 92	Max. 96		a second second	- 1 C
		- · · A				
Desident Frankright		EN/U	1	Accepte	ad V Rejected	
Resident Engineer	signature	Jun	TNI DC		249473	
	D	ON CHRISTIANS	EN, P.E.			
NDOT		RESIDENT ENGI	NEER			
040 047	Distaliant and the state	unders Construction Product	and Englander Director Co.	Casherina		
Dev EIDE	Distribution; Heado	venera construction, Hesid	ent engineer, District Eng	meer, Contractor		
NGN. 6/05						
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			5			V

PBS Type 2C W/RAT Ist Lift, Lance 2. EB 12' W x 3' D Material Type Contract Number Lift, Lane & Direction Date 26/19 Width and Depth Gauge Set Number 148 Lot/Sublot Tested By 5 Butles TEST SECTION 303+492 Sta. 290+92. Sta Sta. 286+473 Sta. 276+602 Sta. 271+36 8 202 21 900 년 서 اد £ 5 297+17 440 +062 . 4 283+ 5 269 (P 5 Random Number Block: 24 Beginning Station "LE" 304+20 4 269+07 Ending Station (A x length = longituding), B x width = transverse) A R 70.3 702.6 0.100 х = 12 0.259 х = 702.6 х 0.890 = 12 x 0,317 = 3.8 702-6 х 0.523 367.5 1 2 х 0.665 = 8.0 0.928 702.6 х = 652.0 12 x 0,404 4.8 = 7026 73 х 0.6 = 472 ١Z R x 0.305 3 TARGET DENSITY Mg/m3 (pcf) 160.9 From (RICE) test number 7- 2- 48 TEST # 134 -PM-7 134 -PM- 2 134-PM- 3 134-PM- 4 134-PM- 5 8TATION 291+00 303+50 286+50 276+50 271+25 nearest 10m (25 ft.) 4 3 Distance from edge * Joint ខ * Joint 4 * Joint 5 * Joint * Joint Left or Right 47 27 67 67 1.7 47 27 27 ۷ 4T 1480 149.9 149.4 NUCLEAR 151.7 148.0 152.6 148.5 150.1 149.2 150. 150.9 151.2 150.3 149.0 153.9 149.9 DENSITY 151.8 148.4 152.5 152.3 152.8 READINGS 150.0 152.2 150.8 153.2 149.0 151.7 150.8 151.7 149.6 149.2 153.1 149.2 150.7 149.2 153.1 149.2 150.9 Average Density 149.8 148.8 146.2 151,7 149.6 1498 151.7 146. **Corrected Density** 1485 151 94 9 94 9 92 9 % Relative Compaction 93 **Correction Factor** 1.00 Remarks: Test section meets Special Provision 51.4 * Mean Test Section Density, Mg/m³ (pcf)= required spec plus SPEC 94 * Mean Percent relative Compaction= Special Provisions SPEC Single: 91-97 * Not Applicable to Partial Test Sections or Joint Densities 402.03.06 Mean: 93-96 Joint Test Specification 90 Min. 90 Single Test Specification Min. Max. 97 Mean Test Section Specification 92 Min. Max. 46 Accepted V Rejected **Resident Engineer Signature**

DON CHRISTIANSEN, P.E. RESIDENT ENGINEER

NDOT 040-017 Rev. 5/05

Distribution: Headquarters Construction, Resident Engineer, District Engineer, Contractor

Material Type Lift, Lane & Direction Width and Depth Lot/Sublot	785 16+ 41 16' 2	EF, La	w/R/ me 1, EU " O	AP S	Con Date Gau Tes	itract Numi e Ige Set Nu ted By	mber	3716 6/26/ 148 D.B.H	19	
Eta Zoob	-20	-	1	TEST SEC	CTION	1		2	5%	2
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(A x length = logoitudies) . p	anadalih — i —			Fucing	Station	2	E. 512	+ 50		
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634 4	0.27	4 2	464.	-	-	-	×	1.556		5.7
A	0.101		80.3			6	x 2	.284		4.5
	-		-							
TARGET DENSITY M	g/m³ (pci)	160	.9		From	(RICE) tes	st number	Τ-	2-48	
TEST #	13SPM	1 0	C .PM	7	25 0	M 2	175-01	1 4	12004	-
STATION			13 -F W-		30 -FI	W>	100-11	g7	135-PM-	
nearest 10m (25 ft)	300	+25	292+	25	289	+00	281.	+ 00	278+	00
Distance from edge	9 1	Joint	1-	laint	1	* Joint	6	La Infint		
Left or Right	17	17	17	17	CT.	1T	17	Joint	17	Jnint
NUCLEAR 1	152.7 1	45 5 1	63.9 11	12/1	109	1226	IEAR	162 6	140 7	10-
DENSITY	157.21	45.71	55 4 10	a 1 1	49 7	151.8	151.0	153.0	140, 2	170.2
READINGS	1533		54 2	F	119 7	12.00	1000	1367	149 0	150.0
4	1518		54.0		44 9	1	1517	1	147.8	
Average Density	152.5	ACGI	545 14	1991	49 2	1522	1016	1.528	140	dia c
Corrected Density	152.5	45 G I	24 5 14	29	49 2	1522	151.6	1520	149.1	199.6
% Relative Compaction	95	90	96	92	GZ	ac	au	95	97.	97.6
The residence of the second		10	-100	12	12	10		15		-12-1
Correction Factor				00						
						Re	marks.		11	1.
* Mean Test Section (Jonelly Ma	m ³ (acf)=	15	51.4	- SP	ecial Rea	wie les	25+ 566	Tion met	15
*Mean Percent relativ	Compac	Hone		Q LL		pec	L.	equired	SPCG P	105
* Not Applicable i	to Dartial T	ost Section	n or loint l	lanellion	Sina	le: 91-	97 2	Pecial	Crovis of	s spec
nor rephilosofe (ear occurri	a di adili L	Jei Iainea	- 0	. 93-	96	102.0 5	06	
Joint Test Specificatio	n	A.flr	00		-		·			
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Mean Test Section So	non Necification	Mir	97		av C					
mean i sat decuoji op	Jecilication	PVIII	16			9		1	1	
		1	~A.1					Constant	Palacto	
Resident Engineer S	ionature	K	SPIV.	-+	Contra and		A	ccepted	rejected	"
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		DUN	SIDENT	ENGINI	EER					
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Material Type Lift, Lane & Direction Width and Depth Lot/Sublot	785 Type 2 1st 1: Ft, Lane 10'W x	<u>C W/RAP</u> 3 Shoulder, <u>G</u> B 3 ° P	Contract Num Date Gauge Set No Tested By	umber 3716 6/28/ 148 D. 6. t	ler
Sta. 259 Sta. 259 Sta. 259 Sta. 259 Sta. 259 Sta. 259 Sta. 259 Sta. 259 Sta. 259	+65 ² Ste. NI M + 5 V N	TEST 2-53+15 ³ Sta. パ ド ド ド	SECTION 251+79 ³ 11 12 14 15 17 17 17 17 17 17 17 17 17 17 17 17 17	a. 244+96- 00 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Sta. 236+769 9 +
Random Number Blo (A x length = longitudine) , A (53, 6) x (53, 6) x (53, 6) x (53, 6) x (53, 6) x (53, 6) x (53, 6) x	ck: 18 8 x width = transvese) 0.947 = 0.947 = 0.150 = 0.150 = 0.195 = 0.448 =	Beg End 614.1 615.9 98.1 127.5 292.9	B 10 10 10 10 10 10 10 10 10	x 0.169 x 0.985 x 0.985 x 0.985 x 0.985 x 0.313 x 0.215	$ \begin{array}{c} = & 1.7 \\ = & q.q \\ = & q.6 \\ = & 3.1 \\ = & 2.2 \\ \end{array} $
TARGET DENSITY N TEST # STATION nearest 10m (25 ft.) Distance from edge Left or Right NUCLEAR DENSITY READINGS	Ig/m ³ (pcf) 6 /36-PM- /- 259 + 75 2 • Joint 47 153.9 150.8 151.4 150.8	$\begin{array}{c} 0.7 \\ \hline 136 -PM-2 \\ 253+25 \\ \hline 10 & Joint \\ 27 \\ \hline 141.0 \\ \hline 149.4 \\ \hline 151.3 \\ \hline \end{array}$	From (RICE) te 736 - PM - 3 $2 \le 1 + 7 \le$ 10 = 3 Joint 47 148.8 $1 \le 0.9$ $1 \le 0.9$ 149.3	$\begin{array}{c c} \text{ist number} & T-1 \\ \hline 136 \text{-PM-} & 4 \\ 245 + 66 \\ \hline 3 & \text{Joint} \\ 47 \\ \hline 157.6 \\ \hline 157.6 \\ \hline 149.6 \\ \hline 150.2 \\ \hline \end{array}$	-49 $/3 \leftarrow PM - 5$ $236 + 75$ $2 \cdot Joint$ 47 $159, 5$ $151, 3$
Average Density Corrected Density % Relative Compaction	151.7 151.7 94	149.6	149.6 149.6 93	150.9 150.9 94	152.4 152.4 95
Correction Factor * Mean Test Section * Mean Percent relati * Not Applicable Joint Test Specificati Single Test Specificati Mean Test Section S	Density, Mg/m ³ (po ve Compaction= to Partial Test Sec on tion pecification	f)= <u>150,8</u> <u>94</u> tions or Joint Densiti Min. <u>90</u> Min. <u>90</u> Min. <u>92</u>	B Special Tre Spec. Single: 9 Mena: 97 Max. 97 Max. 96	emarks: Conpact suision 2-97 Stee p provision 4-96	meets regulated lus special is 402.03.06
Resident Engineer NDOT 040-017 Rev. 5/05	Signature Distribution: Headqu	ON CHRISTIANS RESIDENT ENG	SEN, P.E. INEER tent Engineer, District Engi	Accepted	Rejected
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Material Type Lift, Lane & Direction Width and Depth Lot/Sublot	PBS Type Z Ist Lift, Li 16'w x	C W/RAP HARE I, ED 3" D	Contract Num Date Gauge Set Nu Tested By	ber <u>3716</u> mber <u>148</u> D. Sut 1	19
Sta. 26- 05+ 212	477 ⁹ Sta. 7 Sta. 7 M ト + い い い い い い い い い い い い い	TEST MI F Sta NI F Sta NI F Sta NI F Sta NI F Sta NI F Sta NI F Sta NI F Sta NI F Sta NI Sta	SECTION 256+CIE Sta 0 N + + N N N N	1. 249+78 £ 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	sta. 240 + 72 -
Random Number Blo	ck: (5	Beg	inning Station	E"272+50 E"238+68	
A GT6.9 X GT6.4 X GT6.4 X GT6.4 X GT6.4 X GT6.4 X GT6.4 X X GT6.4 X X X X X X X X X X X X X	0.698 = 0.796 = 0.348 = 0.358 = 0.698 =	472.1 538.4 235.4 242.2 472.(B 16 16 16 16	x 0.683 x 0.996 x 0.743 x 0.595 x 0.531	= 10.9 = 15.9 = 11.9 = 9.5 = 8.6
TARGET DENSITY	Mg/m³ (pcf)	60.6	From (RICE) tes	st number <u>7 - 2</u>	- 49
TEST # STATION	138-PM- 1 267+75	138 -PM- 2 260+25	138 -PM- 3 256+50	138-PM- 4 249+75	138-PM- 5
Distance from edge	U Joint	16 * Joint	12 * loint	10 + Joint	9 A lalat
Left or Right	LT LT	LT LT	LT LT	LT LT	LT LT
NUCLEAR	1 1514 151.9	152,8 147.0	150.5 150.8	150.3 148.4	152.5 148.
DENSITY	2 149.7 153.3	152.2 145.4	150.1 149.9	151.2 148.9	150.8 147.
READINGS	150.1	151.6	151.5	150.5	150.9
Average Density	150.5 152.6	1521 146.2	150.8 150 4	150.8 149 7	151 6 148 0
Corrected Density	150.5 152.6	152.1 146.2	150.8 150.4	150.8 148.7	151.6 148 0
% Relative Compaction	94 95	95 91	94 94	94 93	94 92
Correction Factor		1.00	Re	marks: Compacts	on on test
* Mean Test Section * Mean Percent relat * Not Applicable	Density, Mg/m ³ (pd ive Compaction= to Partial Test Sec	tions or Joint Densit	2 Special Pro spec spec single: 97	1.96 HOR OT	Meets requir us special as spec
Joint Test Specificat Single Test Specifica Mean Test Section S	on tion specification	Min. 90 Min. 90 Min. 92	Max. 97 Max. 96	102.03	/
Resident Engineer	Signature	CHRISTIANS	EN, P.E.	Accepted	Rejected
NDOT 040-017	Distribution: Headqua	rters Construction, Resid	ient Engineer, District Engin	eer, Contractor	

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