University of Memphis University of Memphis Digital Commons

Electronic Theses and Dissertations

11-4-2019

Assessment of The Seismic Vulnerability of West Tennessee School Buildings

Christine Maurice Moore

Follow this and additional works at: https://digitalcommons.memphis.edu/etd

Recommended Citation

Moore, Christine Maurice, "Assessment of The Seismic Vulnerability of West Tennessee School Buildings" (2019). *Electronic Theses and Dissertations*. 2043. https://digitalcommons.memphis.edu/etd/2043

This Thesis is brought to you for free and open access by University of Memphis Digital Commons. It has been accepted for inclusion in Electronic Theses and Dissertations by an authorized administrator of University of Memphis Digital Commons. For more information, please contact khggerty@memphis.edu.

ASSESSMENT OF THE SEISMIC VULNERABILITY OF WEST TENNESSEE SCHOOL BUILDINGS

by

Christine Maurice Moore

A Thesis Submitted in Partial Fulfillment of the Requirements for the Degree of Master of Science

Major: Civil Engineering

The University of Memphis December 2019

ACKNOWLEDGMENTS

I would like to thank my co-advisors and committee members:

- Co-advisor: Dr. Charles Camp
- Co-advisor: Dr. Shahram Pezeshk
- Committee member: Dr. Chris Cramer

From handing me the initial list of schools to the submission of this document, they have truly

been there for me every step of the way. I would like to thank the school directors, maintenance

directors, and safety directors of each of the following school districts that participated in this

study:

- Bradford Special School District
- Dyer County Schools
- Dyersburg City Schools
- Gibson County Special School District
- Humboldt City Schools
- Lauderdale County Schools
- Milan Special School District
- Obion County Schools
- Trenton Special School District
- Union City Schools

Accommodating researchers can be difficult, and many of these school districts immediately recognized the benefits this study could produce for their school buildings. I would like to thank the West TN Seismic Safety Commission (WTSSC) for funding this project. I would also like to thank my mom, my dad, my brother, and my husband (I love you, Andrew!) for their support, patience, and love throughout this process. Being the parent, spouse, or sibling of a graduate student is not easy, but they make it look like a breeze. I thank God for being my source of strength, perseverance, and all good things (James 1:17).

ABSTRACT

West Tennessee is considered a Moderately High to Very High Region of Seismicity according to the Federal Emergency Management Agency (FEMA), and within the New Madrid Seismic Zone (NMSZ). However, West Tennessee has been building large structures long before strides in earthquake engineering were made. FEMA hired the Applied Technology Council (ATC) to develop a procedure entitled the "Rapid Visual Screening (RVS) Method" to quickly determine if a structure is likely to suffer major damage in an earthquake or not. This is done by documenting aspects of the structure and its site and then calculating a score for the building. The score is compared to a cut-off score. If the score of the building is less than the predetermined cut-off score, then the building is likely to collapse in the event of an earthquake resulting in a high risk of loss of life. The procedure is relatively inexpensive due to the lack of qualification necessary from the screener and the short time it takes to complete the survey. A more sophisticated government software called Hazus-MH (Hazard United States- Multi-Hazard) was developed to produce results with five damage categories: None, Slight, Moderate, Extensive, and Complete. Since Hazus-MH requires a significant amount of time to input data and find additional information from the site, it costs more to run an investigative team using Hazus-MH as opposed to the RVS Method. The West Tennessee Seismic Safety Commission has funded a project for The University of Memphis to assess the seismic resistance of West Tennessee school buildings and to investigate the correlations between the RVS Method and the results of the Hazus-MH software if any. If there is a strong correlation in data, then perhaps RVS Method is a reliable method to investigate buildings for earthquake resistance quickly.

iii

List	of Tables v	i
Lis	of Figuresvi	i
Lis	of Variablesiz	X
1.	Introduction	1
S	tudy Region Characteristics	1
	Dyer County	2
	Gibson County	2
	Lauderdale County	3
	Obion County	3
A	pproach	3
L	iterature Review	5
	FEMA P-154	5
	Previous Research	5
	Hazus Technical and User's Manuals	6
2.	Methodologies	6
F	apid Visual Screening (RVS)	5
	Pre-field Planning Activities: Location, Region of Seismicity, and Soil Type	7
	Site Observations: FEMA Building Type and Score Modifiers	0
	Post-Field Assessment	2
H	lazus-MH 4.2 Analysis	2
	Comprehensive Data Management System (CDMS)	3
	Generating a Study Region	6
	Scenarios and Hazard Maps1'	7
	Fragility Curves	8
3.	Results	0
F	VS Results	0
H	azus-MH 4.2 Results	5
	Dyer, Gibson, Lauderdale and Obion County: Coarse Map Results	1
	Dyer County: Coarse Map Results	5
	Dyer County: Finer Map Results	
Γ	Discussion and Conclusions	0

TABLE OF CONTENTS

4. Appendices	
Appendix A: Region of Seismicity's Effect on Level 1 Data Collection Form	
Appendix B: FEMA Building Type Descriptions and Compatible Hazus-MH 4.2 Type	es 47
Appendix C. Procedure for CDMS Data Entry	
Appendix D: Procedure for Creating Ground Motion Maps from Text File Compatible Hazus-MH 4.2	
Importing Points into ArcMap	
Creating a Fishnet in ArcMap	61
Joining the Point Data with the Fishnet to Create a Useable Map	63
Appendix E: Seismic Hazard Maps Used	67
Appendix F: Ancillary Data from RVS	
Appendix G. Hazus-MH 4.2 Results: Damage State Probabilities	80
Appendix H. Hazus-MH 4.2 Results: Ancillary Data	89
Appendix I: Case 1 Ranking	
Appendix J: Case 2 Ranking	
Appendix K: Case 3 Ranking	100
Appendix L. Level 1 Data Collection Form Results	101
References	102

LIST OF TABLES

Table 1. Seismicity Region from MCE _R Spectral Acceleration Response	
Table 2. Soil Type Definitions	9
Table 3. Seismic Design Level	
Table 4. FEMA Building Types	
Table 5. SLI Score Distribution	
Table 6. Design Year of Buildings	
Table 7. Irregularities of Buildings	
Table 8. Damage State Probabilities for TN002548	
Table 9. Percent Loss Parameters: EDU1	
Table 10. Case 1: Summary of Result Variables	
Table 11. Case 1: Correlational Coefficient Matrix	
Table 12. Case 2: Summary of Result Variables	
Table 13. Case 2: Correlational Coefficient Matrix	
Table 14. Case 3: Summary of Result Variables	
Table 15. Case 3: Correlational Coefficient Matrix	
Table 16. Percent of Structures in Each County Ranking	
Table F1. Ancillary Building Data	74
Table F2. Ancillary School Data	77
Table G1. Damage State Probabilities: Case 1	
Table G2. Damage State Probabilities: Case 2	
Table G3. Damage State Probabilities: Case 3	
Table H1. Case 1: Predicted Casualties	89
Table H2. Case 1: Predicted Economic Losses	
Table H3. Case 2: Predicted Casualties	
Table H4. Case 2: Predicted Economic Losses	
Table H5. Case 3: Predicted Casualties	
Table H6. Case 3: Predicted Economic Losses	
Table I1. Case 1 Structures Ranked by Predicted Performance	
Table J1. Case 2 Structures Ranked by Predicted Performance	
Table K1. Case 3 Structures Ranked by Predicted Performance	

LIST OF FIGURES

TABLE OF CONTENTS	. iv
Figure 1. Seismicity Regions (Contiguous United States)	1
Figure 2. Study Site Locations	2
Figure 3. UBC Seismic Zones	15
Figure 4. Example Calculation of Damage State Probability	19
Figure 5. Example Fragility Curve with Various β values	19
Figure 6. Example Fragility Curve	
Figure 7. Level of Seismicity Across Study Region	21
Figure 8. Building Score vs. Year Built	24
Figure 9. Examples of Buildings with a Reentrant Corner	25
Figure 10. Case 1: BRC vs. MD	32
Figure 11. Case 1: BRC vs. IO	
Figure 12. Case 1: BRC vs. S _{L1}	34
Figure 13. Rank and Coarse Map PGA Values	35
Figure 14. Case 2: BRC vs. MD	37
Figure 15. Case 2: <i>BRC</i> vs. <i>S</i> _{<i>L1</i>}	37
Figure 16. Case 2: S _{L1} vs. MD	38
Figure 17. Case 1: S _{L1} Versus Rank	41
Figure A1. Basic Score and Modifiers for Low Seismicity Region	44
Figure A2. Basic Score and Modifiers for Moderate Seismicity Region	44
Figure A3. Basic Score and Modifiers for Moderately High Seismicity Region	44
Figure A4. Basic Score and Modifiers for High Seismicity Region	45
Figure A5. Basic Score and Modifiers for Very High Seismicity Region	45
Figure A6. Level 1 Data Collection Form	46
Figure C1. CDMS Home Screen	52
Figure C2. Import into CDMS Repository from File Page	53
Figure C3. Import into CDMS Repository Screen	54
Figure C4. Data Field Matching Window	55
Figure C5. Category Value Matching Window	56
Figure D1. Importing Data into Microsoft Excel	58
Figure D2. Imported Text Data in Microsoft Excel	59
Figure D3. Display XY Data Window	60
Figure C4. Export Data Window	60
Figure D5. Create Fishnet Window	62
Figure D6. Fishnet Over Point Data	63
Figure D7. Join Data Window	64
Figure D8. Dissolve Window	65
Figure D9. Feature Class to Feature Class Window	
Figure E1. PGA Values (g), Coarse Ground Motion Maps, Entire Study Region	68
Figure E2. PGV Values (in/s), Coarse Ground Motion Maps, Entire Study Region	
Figure E3. 0.3s S _a Values (g), Coarse Ground Motion Maps, Entire Study Region	69

Figure E4. 1.0s Sa Values (g), Coarse Ground Motion Maps, Entire Study Region	69
Figure E5. PGA Values (g), Coarse Ground Motion Maps, Dyer County	70
Figure E6. PGV Values (in/s), Coarse Ground Motion Maps, Dyer County	70
Figure E7. 0.3s Sa Values (g), Coarse Ground Motion Maps, Dyer County	71
Figure E8. 1.0s Sa Values (g), Coarse Ground Motion Maps, Dyer County	71
Figure E9. PGA Values (g), Fine Ground Motion Maps, Dyer County	72
Figure E10. PGV Values (in/s), Fine Ground Motion Maps, Dyer County	72
Figure E11. 0.3s Sa Values (g), Fine Ground Motion Maps, Dyer County	73
Figure E12. 1.0s Sa Values (g), Fine Ground Motion Maps, Dyer County	73

LIST OF VARIABLES

- B lognormal standard deviation value
- MCE_R Maximum Considered Earthquake Response
- *N* Standard Blow Count
- N.T.S. Drawing is not to scale
- PGA Peak Ground Acceleration
- PI-Plasticity Index of Soil
- P_{Ll} Plan Irregularity Score Modifier
- r correlational coefficient
- S_a Spectral Acceleration
- S_b Basic Score
- Sco Cut-off Score
- S_{L1} Building Score, Level 1 Score
- Spb Post-Benchmark Score Modifier
- Spc Pre-Code Score Modifier
- S_s Short-Period Spectral Acceleration, or 0.2 seconds Spectral Acceleration
- Ssoil Soil Type Score Modifier
- S_u Undrained Shear Strength of the upper 100ft
- S₁ Long-Period Spectral Acceleration, or 1.0 second Spectral Acceleration
- V_{L1M} Moderate Vertical Irregularity Score Modifier
- VL1S Severe Vertical Irregularity Score Modifier
- V_s^{30} Shear Wave Velocity
- w Moisture Content of Soil

1. INTRODUCTION

Study Region Characteristics

Earthquakes are of significant concern to residents of West Tennessee. In addition to the location of the infamous earthquakes of 1811 and 1812, West Tennessee is also in a highly seismically active area of the contiguous United States (see Figure 1, Figure A-1 of FEMA P-154 (2015)). This study focuses on 50 public schools, comprised of 85 public school buildings and/or significant additions in Tennessee, specifically in Dyer County, Gibson County, Lauderdale County, and Obion County. All four counties fall within the area of Figure 1 that is shaded in purple that is generally considered a "Very High" Region of Seismicity. The school sites and counties are shown in more detail in Figure 2.

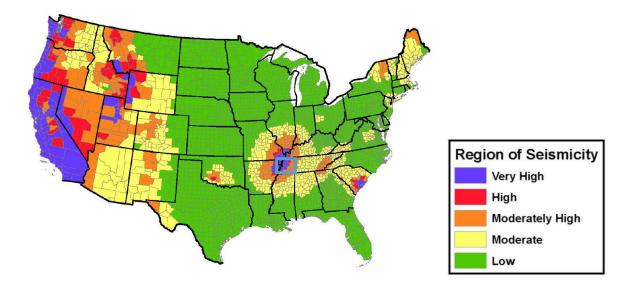


Figure 1. Seismicity Regions (Contiguous United States)

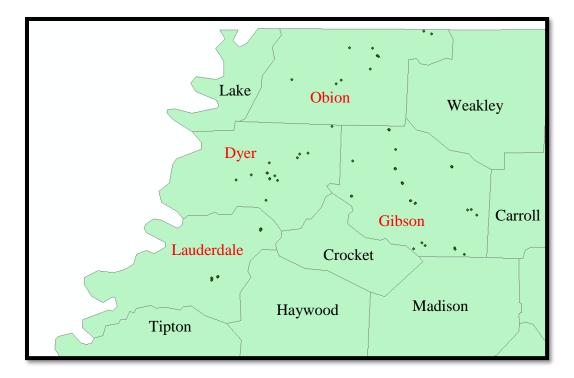


Figure 2. Study Site Locations

Dyer County

Dyer County contains 17 (20%) of the studied structures and/or significant additions. The median household income in Dyer County is \$44,386. In 2018, Dyer County had an estimated population of 37,320, which is a 2.6% decrease from the 2010 Census estimates. 17.7% of the population, or 6,606 people are between 5 and 18 years of age (U.S. Census Bureau, 2018). According to the Tennessee Report Card, the schools studied account for 6,815 students and teachers occupying the school buildings during each school year. 1,279,945 square feet of school buildings were studied in Dyer County.

Gibson County

Gibson County contains 43 (50.6%) of the studied structures and/or significant additions. The median household income in Gibson County is \$41,315. In 2018, Gibson County had an estimated population of 49,045, which is a 1.3% decrease from the 2010 Census estimates.

17.9% of the population, or 8,779 people are between 5 and 18 years of age (U.S. Census Bureau, 2018). According to the Tennessee Report Card, the schools studied account for 10,169 students and teachers occupying the school buildings during each year. 1,602,837 square feet of buildings were studied in Gibson County.

Lauderdale County

Lauderdale County contains 14 (16.5%) of the studied structures and/or significant additions. The median household income in Lauderdale County is \$35,551. In 2018, Lauderdale County had an estimated population of 25,825, which is a 7.2% decrease from the 2010 Census estimates. 16.8% of the population, or 4,338.6 people are between 5 and 18 years of age (U.S. Census Bureau, 2018). According to the Tennessee Report Card, the schools studied account for 4,706 students and teachers occupying the school buildings during each year. 744,257 square feet of school buildings were studied in Lauderdale County.

Obion County

Obion County contains 11 (12.9%) of the studied structures and/or significant additions. The median household income in Lauderdale County is \$38,063. In 2018, Obion County has an estimated population of 30,267, which is a 4.8% decrease from the 2010 Census estimates. 16.0% of the population, or 4,843 people are between 5 and 18 years of age (U.S. Census Bureau, 2018). According to the Tennessee Report Card, the schools studied account for 5,479 students and teachers occupying the school buildings each year. 911,366 square feet of school buildings were studied in Obion County.

Approach

Rapid Visual Screening (RVS) is a method of evaluating buildings based on simple characteristics to inexpensively determine if it is resistant or vulnerable to seismic forces. RVS

3

was developed by the Applied Technology Council (ATC) for the Federal Emergency Management Agency (FEMA). Some advantages of RVS is that anyone with a background related to construction or engineering can be trained to screen buildings, which makes the process extremely inexpensive as opposed to hiring private structural engineering firms to retrofit a building without knowing how seismically vulnerable or resistant the building is. One disadvantage of the RVS method is that it can only come to one of two conclusions: The building either "may be seismically hazardous and should receive a detailed structural evaluation" or not. The conclusion is arrived upon by calculating a score for the building, S_{L1} , and comparing it to a cut-off score for the region, S_{co} . If the building's score is above the cut-off score, the building is not considered potentially seismically hazardous. Another methodology used for this study is using Hazus-MH 4.2, which takes similar information collected from the RVS form, and computes probabilities that the surveyed building will fall into the following damage states: None, Slight, Moderate, Extensive, and Complete. A noticeable benefit in using Hazus-MH 4.2 over RVS for evaluating buildings is that there are clearly more detailed results. However, a major drawback of Hazus-MH 4.2 is that there are a much higher computation time and time used for data entry. The main objective of this study is to evaluate seismic vulnerability of the schools in the study and to develop a prioritized list of schools following both the RVS and Hazus-MH 4.2 approaches. Another objective of this study is to compare the RVS results with the Hazus-MH 4.2 results to see if using Hazus-MH 4.2 would be necessary for determining if a building needs a detailed structural evaluation. Many parties could benefit from this study in terms of prioritizing which school buildings should be considered for a more detailed structural engineering evaluation and retrofit versus which school buildings could be considered a storm

shelter location. A few of the school campuses have a tornado shelter that could also serve as a shelter in the event of an earthquake, as those buildings have also been screened.

Literature Review

While conducting this research, documents and papers were referenced to help better understand the problem and solutions. FEMA P-154 (2016) and its supporting documentation FEMA P-155 (2016) explain how to develop a Rapid Visual Screening (RVS) program and complete an RVS, as well as many resources for using RVS results for seismic advocacy. Seismic Vulnerability Evaluation of Essential Facilities in Memphis and Shelby County, Tennessee (Chang et al, 1995), Assessment of the Seismic Vulnerability of the University of Memphis Main Campus Buildings (Mize, 2006), Assessment of the Seismic Vulnerability of Shelby County Mass Emergency Shelters (Boling, 2009), and Statistical Assessment of the Seismic Vulnerability of Mid-South Building Structures (Assadollahi, 2010) are all previous projects including this type of research conducted in West Tennessee. They each serve unique purposes in addition to comparing the RVS Method and Hazus-MH software output. The Hazus-MH 2.1 Advanced Engineering Building Module (AEBM) Technical and User's Manual (FEMA, 1999) and Earthquake Model: Hazus-MH 2.1 User Manual (FEMA, 1999) are tools developed to help researchers properly use Hazus-MH for earthquake loss estimation. Currently, those are the two most recent and relevant manuals available on FEMA's website, despite Hazus-MH 4.1 being the most up-to-date version of the software.

FEMA P-154

FEMA 154 was first developed by the ATC for FEMA in 1988, then revised in 2002, and again in 2015 when the document was re-named FEMA P-154. Since 1988, several improvements have been made. One difference is the distinguishing of five regions of seismicity

is now recognized, as opposed to three in the first two editions. The first edition identified 12 Building Classifications, the second edition recognized 15 Building Classifications, and the most recent edition recognizes 17 FEMA Building Types, formerly called "Building Classifications." Due to these changes, comparing this study to previous versions done before 2015 is not an apples-to-apples comparison. One must consider that a building previously under one building classification is now under a different FEMA building type, resulting in a different score.

Previous Research

Reviewing similar studies in this region helped notice the numerous changes made by ATC and FEMA over the last 20 years. There is more differentiation in geological information and structural information, and that is noticeable in the previous research material compared to now. This is the first study in West TN since the third edition of FEMA P-154 in 2016.

Hazus Technical and User's Manuals

Hazus-MH 4.2 does not yet have a user or technical manual available for the earthquake hazard; nonetheless, the technical and user manuals for Hazus-MH 2.1 have proven to be helpful. FEMA also released a series of videos on Youtube.com in Summer 2019 that helped with selecting hazard maps, defining scenarios, and running analyses.

2. METHODOLOGIES

Rapid Visual Screening (RVS)

RVS is one of the two methodologies used in this study to assess the seismic vulnerability of structures. While FEMA P-154 details the gathering of the investigative team, the different ways of obtaining and collecting data, and how to use the results for seismic

advocacy, this section outlines the details of how this specific study was performed. For more details on alternative implementations of RVS, consult FEMA P-154.

To calculate the score for a building, S_{L1} , one must fill out the Level 1 Data Collection form. There are five versions of this form based on the level of seismicity. Once the form is selected, a basic score is determined from the FEMA building type; then, any score modifiers are added or subtracted from the basic score to result in the final Level 1 score or score for the building, S_{L1} . Appendix A shows the form for a building in a Very High region of seismicity, as well as the "Basic Score, Modifiers, and Final Level 1 Score, S_{L1} " section for each region of seismicity, and explains how the basic score and score modifiers change based on the region of seismicity of the building.

The RVS procedure is first begun by identifying which buildings to survey. It is ideal to know most or all the buildings at the beginning of the study so that preliminary research can be performed for all the buildings at once. Once most of the buildings are determined, pre-field planning may commence.

Pre-field Planning Activities: Location, Region of Seismicity, and Soil Type

Data collected during the pre-field planning activities are primarily found in the upper right portion of the Level 1 Data Collection Form shown in Appendix A, Figure A6. First, determine the Latitude and Longitude of each structure to at least six decimal places; this allows the user to distinguish between adjacent buildings.

While one can technically determine the level of seismicity by using the county-level maps shown in Figure 1, it is recommended to determine the region of seismicity by entering the following parameters into <u>https://seismicmaps.org/</u>: The design code reference is "2013 ASCE

7

41", the earthquake hazard level to "BSE-2N", and the soil site classification is the soil site class "B". The location can be determined by using the Latitude and Longitude of the site found previously. By inputting these various parameters, the maximum considered earthquake response, *MCE_R*, and spectral accelerations may be determined. The results from the USGS seismic maps may be interpreted using Table 1 (Table 2-2 FEMA P-154). This region determines which Level 1 Data Collection Form you choose. Once the form is selected, recording other identifying data such as the address, building name, and building use is helpful so that once site visits commence, one knows how to locate the building for the sidewalk survey. For the sites in this study, buildings were found to be in Moderately High, High, and Very High seismicity regions. If the original county-wide map were used, all buildings would have been in the Very High seismicity region. Taking extra measures, such as using the recommended procedure above, helps the screener avoid making overly conservative assumptions since the base score for each building significantly decreases with each higher level of seismicity on the Level 1 Data Collection forms.

	Table 1. Seismicity Region from <i>MCE_R</i> Spectral Acceleration Response				
Seismicity Region			Spectral Acceleration	Spectral Acceleration	
		eismicity Region	Response, S _s (short-period,	Response, S_1 , (long-period,	
			or 0.2 seconds)	or 1.0 second)	
		Low	$S_s < 0.250 { m g}$	$S_1 < 0.250$ g	
		Moderate	$0.250g \le S_s < 0.500g$	$0.250g \le S_1 < 0.500g$	
		Moderately High	$0.500g \le S_s < 1.000g$	$0.500g \le S_1 < 1.000g$	
		High	$1.000g \le S_s < 1.500g$	$1.000g \le S_1 < 1.500g$	
		Very High	$S_s \ge 1.500$ g	$S_1 \ge 1.500$ g	

Table 1. Seismicity Region from MCE_R Spectral Acceleration Response

After the region of seismicity for each building site is determined, the soil type may be determined. Use the following link to determine the shear wave velocity, V_s^{30} , near each of the buildings:<u>https://usgs.maps.arcgis.com/apps/webappviewer/index.html?id=8ac19bc334f747e486</u> <u>550f32837578e1</u>. If the data is no longer available at the link provided, find other sources to obtain the average shear wave velocity, average standard blow count, or average undrained shear strength of the upper 100 feet of soil to help deduce the site class of the soil surrounding each structure using Table 2, (Table 2-5 FEMA P-154 (2015)). The soil type only influences the score of the building if the soil type is A, B, or E. Surprisingly if the soil type is F, a detailed structural evaluation is recommended, but the score of the building is not affected. Soil type F is considered an "other hazard" present (FEMA, 2015). All the buildings in this study fall within soil type C or D.

Soil Type/Site	Shear Wave Velocity1, V_s^{30}	Standard Blow	Undrained Shear Strength	
Class		Count1, N	of the upper 100ft', S_u	
A. Hard Rock	$V_s^{30} > 5000 \text{ ft/s}$	N/A	N/A	
B. Rock	$2500 \text{ ft/s} < V_s^{30} < 5000 \text{ ft/s}$	N/A	N/A	
C. Very Dense				
Soil and Soft	$1200 \text{ ft/s} < V_s^{30} < 2500 \text{ ft/s}$	N > 50	S > 2000 psf	
Rock				
D. Stiff Soil	$600 \text{ ft/s} < V_s^{30} < 1200 \text{ ft/s}$	15 < N < 50	$1000 \text{ psf} < S_u < 2000 \text{ psf}$	
	$V_s^{30} \le 600 \text{ft/s}$	<i>N</i> < 15	$S_u < 1000 \text{ psf}$	
E. Soft Clay Soil	More than 10 feet of soft soil with plasticity index, $PI > 20$, water content,			
	$w > 40\%$, and $S_u < 500 \text{ psf}$			
	Soils Requiring Site-Specific Evaluations			
	Soils vulnerable to potential failure or collapse under seismic			
	loadings, such as liquefiable soils, quick and highly sensitive clays,			
F. Poor Soil	collapsible weakly-cemented soils.			
	Thicker than 10 feet of peat or highly organic clay			
	> Very high plasticity clays (25 feet with $PI > 75$).			
	More than 120 feet of soft or medium stiff clays			

Table 2. Soil Type Definitions

During the pre-field planning activities, a few other decisions regarding RVS are made. Firstly, a cut-off score is determined. Chapter 2 of FEMA P-154 suggests a cut-off score of 2 to be used for most cases, so for this study, the cut-off score is 2.0 (FEMA, 2016). Additionally, the code year and benchmark year should be selected. In previous versions of FEMA P-154, the benchmark year is the only year of significance. However, the third edition of FEMA P-154 distinguishes between a code year and a benchmark year. The code year is the year that seismic codes were initially adopted and enforced locally, and the benchmark year is the year that seismic codes were significantly improved (FEMA, 2016). It was determined that West Tennessee only has a code year, and that is 1991 (Mize, 2006).

Site Observations: FEMA Building Type and Score Modifiers

Once the pre-field planning activities for a site are complete, the site visit may begin. The best department to contact at any facility is the maintenance office, or a plant manager if applicable. The maintenance offices generally have floor plans, evacuation maps, and reliable dates that buildings were constructed. The single most important characteristic of the building to determine is the FEMA building type.

Briefly mentioned earlier, and described in Appendix B, the FEMA building type is determined by the material the building is constructed with and the main seismic-resisting system in place. Materials that buildings could be constructed with are wood, steel, concrete, steel encased in concrete, and masonry. Seismic-resisting systems include moment frames, braced frames, and shear walls. Appendix B describes each FEMA building type in detail as well as the Hazus-MH 4.2 software-equivalent model building type. FEMA P-154 has guidance for screeners on how to identify the FEMA building type in Section 3.14 (FEMA, 2016). Once the FEMA building type is determined, the building has a basic score, *S*_b. For example, in Appendix A: Figure A6, the basic score for a W1 building in a Very High region of seismicity is 2.1. Once the basic score is determined, the building should be scoped for plan irregularities, vertical irregularities, and other score modifiers.

The basic score has score modifiers that lower or raise the basic score underneath it. The first score modifier addressed is the soil type score modifier, S_{soil} , since it can be determined

before the site visit. If the soil type is A or B, then it has a positive effect on the building's score. Soil type E reduces the building's score, and soil types C and D have no effect. The year the building was designed and/or constructed is extremely important; depending on how old or new the building is, the basic score can be lowered by 0.3 or raised by 2.0 in the Very High region of seismicity. The year the building was designed and/or constructed can be determined by the maintenance office, older staff members, or placards present at the entrance of the building or addition. If it is known when the building was constructed, a year is subtracted from that and is called the code year. The year the building was designed is that building's code year, and it is compared to the code year for the region. If the building was built before the code year for the region, the building is considered pre-code, S_{pc} , and it is a negative score modifier. If the building is younger than the code year (or benchmark year, if applicable), then it is considered "post-benchmark" and it is a positive score modifier. Vertical irregularities and plan irregularities are the last set of score modifiers to discuss.

Vertical irregularities and plan irregularities are found at the site and are basic characteristics of the shape of the building that cause it to perform worse in an earthquake event as opposed to buildings without an irregularity present. Vertical irregularities are further subdivided into moderate and severe; while both are negative score modifiers, moderate vertical irregularities have a lower magnitude than severe vertical irregularities. The seven vertical irregularities found in buildings from FEMA P-154 Chapter 3 (2016) are: sloping site, unbraced cripple wall, weak and/or soft story, out-of-plane setback, in-plane setback, short column/pier, and split levels. Plan irregularities mostly deal with the symmetry of the building in the plan dimension. A list of the five plan irregularities found in buildings from FEMA P-154 Chapter 3 (2016) is: torsion, non-parallel systems, reentrant corner, diaphragm openings, and beams that do

11

not align with columns. Descriptions and of the vertical and plan irregularities are found in FEMA P-154.

Post-Field Assessment

After the site visit has been completed, the score for the building, S_{LI} , may be calculated by using Equation 1a:

$$S_{L1} = S_b + S_m \tag{1a}$$

where S_b is the basic score, and S_m is the sum of the score modifiers. The sum of the score modifiers is calculated in Equation 1b:

$$S_m = V_{L1S} + V_{L1M} + P_{L1} + S_{pc} + S_{pb} + S_{soil}$$
(1b)

where V_{LIS} is the severe vertical irregularity score modifier, V_{LIM} is the moderate vertical irregularity score modifier, P_{LI} is the plan irregularity score modifier, S_{pc} is the pre-code score modifier, S_{pb} is the post-benchmark score modifier, and S_{soil} is the soil type score modifier. Once the Level 1 Score is known, it is compared to the benchmark score of 2.0 to determine if the building needs a detailed structural evaluation. Then, the RVS data may be entered into a Microsoft Excel spreadsheet, and slightly modified to enter information into Hazus-MH 4.2.

Hazus-MH 4.2 Analysis

Hazus-MH 4.2 is a software application within ArcGIS used for risk estimation in the event of several natural disasters: earthquake, flood, hurricane, and tsunami. Hazus-MH 4.2 estimates the physical, social, and economic losses due to an earthquake event. This study primarily focuses on the damage states of the buildings after an earthquake event. While Hazus-MH 4.2 is a very powerful tool, it also has many limitations. The detail of a study performed in Hazus software used to be measured by Level 1, Level 2, and Level 3 analyses. Level 1 was all default information, Level 2 included some building survey data (custom inventory) and some unique hazard information- such as soil type or local PGA, PGV, 0.3s spectral acceleration, and 1s spectral acceleration, and Level 3 included user-developed fragility curves (ESRI 2006). It was generally recommended to use Level 2 analysis since user-developed fragility curves are difficult to make and must be made individually for each building. So, even if a user-developed fragility curve was developed correctly, it would only show results for one individual building, yielding an insignificant sample size (number of observations less than 30). Since Level 3 analysis was not recommended, Hazus-MH 4.2 now splits analyses into two categories: Basic and Advanced. A basic analysis is based mainly on default (Hazus-provided) data. Some new information may be provided by the user, but the hazard is defined by Hazus. An advanced analysis includes any custom inventory that is not provided by Hazus but generally focus is given to hazard information collected by geologists and seismologists in the local area (FEMA 2019). It is also useful to have specific building inventory information collected by engineers for a more accurate building type information. This study considers only local probabilistic ground motion maps, so it is considered an advanced analysis. All the inventory in the study has been surveyed, so user-developed information is being used for all the building types, the number of stories, etcetera to be defined in Hazus-MH 4.2. For every piece of information desired, specific data input is required. CDMS was developed to validate data entering Hazus-MH 4.2 to ensure that all the necessary inputs are present.

Comprehensive Data Management System (CDMS)

CDMS is a tool that is downloaded and installed in conjunction with Hazus-MH 4.2 and exists only to help import data into and export data from Hazus-MH 4.2. First, a state database is downloaded from the FEMA website, and selected for the region. Then, data may be imported

into the repository from a Microsoft Excel spreadsheet, geodatabase, or shapefile file. Different hazards, "Hazus-MH Inventory Categories." and "Hazus-MH Inventory Datasets (layers)" have different required inputs. Once the proposed input file, hazard, inventory category, and inventory dataset are selected, CDMS will display the required fields. The hazard for this study is "Earthquake." The inventory category selected for this study is "Advanced Engineering Building Module (AEBM)," and the only inventory dataset under that category is also "AEBM." There are four required fields: area (square feet), earthquake building type, earthquake design level, and occupancy type. Remember that the earthquake building type is not necessarily the FEMA building type; the designation for low-rise, mid-rise, and high-rise described in Appendix B must be used.

The earthquake design level is an indicator of how a building will perform based on the codes of that region. There are three seismic design levels: High-Code, Moderate-Code, and Low-Code. An additional category, Pre-Code, is applicable to all buildings constructed before 1941. While separating buildings into these categories may seem arbitrary, each of the categories is associated with a damage function within Hazus-MH 4.2. The earthquake design level is determined using Figure 3 and Table 3. Figure 3 is a map of the 1994 Uniform Building Code's (UBC) seismic zones. Table 3 is a map within the Hazus-MH 2.1 User's Manual.

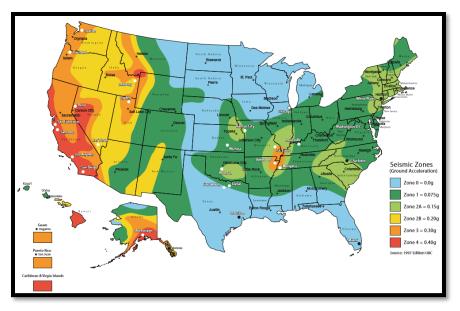


Figure 3. UBC Seismic Zones

From the figure above, the study region is within Zone 3. So, all buildings in this study are either Moderate-Code or Pre-Code according to Table 3, which is Table 2.2 in the Hazus-MH 2.1 AEBM Manual (FEMA 2012). Upon further inspection, 80 of the 85 buildings surveyed are considered Moderate-Code, and the 5 remaining are considered Pre-Code.

UBC Seismic Zone	Design Vintage		
(NEHRP Map Area)	Post-1975	1941-1975	Pre-1941
Zone 4 (MA 7)	7) High-Code Moderate-Code		Pre-Code
Zone 3 (MA 6)	Moderate-Code	Moderate-Code	Pre-Code
Zone 2B (MA 5)	Moderate-Code	Low-Code	Pre-Code
Zone 2A (MA 4)	Low-Code Low-C		Pre-Code
Zone 1 (MA 2/3)	Low-Code	Pre-Code	Pre-Code
Zone 0 (MA 1)	Pre-Code	Pre-Code	Pre-Code

 Table 3. Seismic Design Level

Finally, the occupancy type should be determined. While there are many occupancy types to choose from, all buildings within this study are considered EDU1, which are all primary, elementary, and high school buildings. There are other recommended economic data that Hazus-

MH 4.2 will estimate based on the required parameters. CDMS will validate the data and allow the user to transfer data into the CDMS repository. Then, the user can return to the home screen and transfer the data into the statewide data set. Based on previous experiences, it is recommended to "Replace" the data in the statewide data-set rather than "Append" the data. This helps avoid duplicate entries. Once the data regarding the buildings are transferred to the statewide dataset, the user will now see the data input in all Hazus-MH 4.2 study regions in that state. Appendix C has a complete procedure for updating a study region using CDMS. Appendices F and L contain data necessary to run a Hazus-MH 4.2 AEBM Module.

Generating a Study Region

To create a study region, applicable hazard(s) must be selected. Since this study is only considering losses from earthquakes, only the earthquake hazard is selected. Only selecting applicable hazards helps reduce time to complete the analysis.

Study regions can be aggregated at the state, county, or census tract level for an earthquake hazard analysis. The smaller the aggregation level, the more detailed analysis is. The reason for this is economic status, living conditions, and population characteristics are recorded at the aggregation level chosen, so the smaller the aggregation level, the more variation in the population is represented (Hazus-MH 2.1 2012). This study aggregates at the census- tract level. To create the study region, the appropriate level of aggregation is selected, and then the applicable state, county, and census tracts are selected. Then, the study region is generated. To open the region, select "Open a Region." The buildings should already be present in the inventory. In addition to seeing the usual ArcMap tabs, several tabs specific to Hazus-MH 4.2 will appear to be used for inventory validation, hazard selection, and viewing results.

Scenarios and Hazard Maps

When performing a seismic risk analysis, the user must create a scenario. A scenario includes options for indicating the seismic hazard map, liquefaction susceptibility map, landslide susceptibility map, fault rupture maps, then a soil type map, and water depth map. Once the scenario is created, the analysis can be run.

Hazus-MH 4.2 has five options for selecting hazard maps. There are two deterministic options: "Historical Epicenter Event" and "Arbitrary Event." A historical epicenter event is one that is based on an earthquake in the area that has happened in the past. While it may sound like a great idea to use this option, there is no probabilistic evidence that the same exact magnitude and location of an earthquake will happen again. An arbitrary event is just as it sounds; it is a list of arbitrary magnitudes and locations of earthquakes that have been created for Hazus users. The remaining three options are a probabilistic hazard, a user-supplied hazard, and a USGS ShakeMap. A probabilistic hazard asks for the user to specify a return period in years and a magnitude driving the probabilistic event. A user-supplied hazard requires PGA, PGV, 0.3s spectral acceleration, and 1.0s spectral acceleration maps for the area of interest; the usersupplied hazard was chosen for the study region, as there is currently one local study that covers the entire study region with the required ground motion data supplied by Dhar and Cramer (2017) that has a grid spacing of 0.1°. The maps resulting from this study will be referred to as the "coarse ground motion maps" throughout this document. A more detailed ground motion map has been generated that covers only Dyer County TN with a grid spacing of 0.005°, resulting in four hundred data points for every data point that the 2017 study covers. These more detailed maps will be referred to as the "finer Dyer County ground motion maps" throughout this

17

document. Appendix D shows the user how to create Hazus-compatible ground motion maps from a text file. From the local ground motion data above, three cases are studied:

- 1. For Dyer, Gibson, Lauderdale, and Obion Counties, ground motion values with 2% in 50year exceedance using coarse ground motion maps.
- For Dyer County, ground motion values with 2% in 50-year exceedance using coarse ground motion maps.
- For Dyer County, ground motion values with 2% in 50-year exceedance using finer Dyer County ground motion maps

Appendix E shows the ground motion maps used in this study. It should be noted that the same maps are used in both the first and second cases, so the second case is just a subset of the first. More detailed maps are used in the third case, so the results should be more accurate for the third case.

Fragility Curves

A fragility curve is made up of two components: the damage median and the lognormal standard deviation value, β (FEMA-AEBM, 2012). The final fragility curve shows the probability of a structure falling into a damage state given a spectral displacement. First, the probability that a building will suffer slight, moderate, extensive, or complete damage given a spectral displacement is plotted; where each probability is equal to 0.5 is defined as the "damage state median". An example of the damage state median points is shown in FEMA's AEBM User and Technical Manual (2012), and Figure 4. After the damage state median is found, the slope is determined by the lognormal standard deviation value, β .

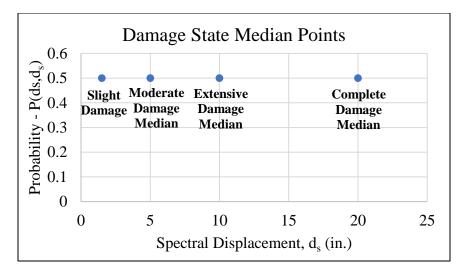


Figure 4. Example Calculation of Damage State Probability

The effect of the beta value is shown in Figure 5 (Figure 6.2 AEBM Manual) and reflected in Equation 2. Equation 2 calculates the vertical axis of a fragility curve, which is the probability of a damage state given a spectral displacement:

$$P(ds|d_s) = \varphi\left(\frac{1}{\beta}\ln\left(\frac{d_s}{\bar{d}_{s,ds}}\right)\right)$$
(2)

where φ is the standard normal cumulative distribution function (cdf), d_s is the spectral displacement, and $\bar{d}_{s,ds}$ is the median spectral displacement where the building reaches a particular damage state.

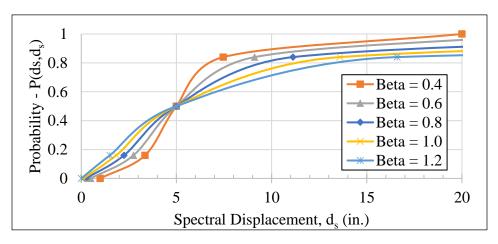


Figure 5. Example Fragility Curve with Various β values

The process above is completed four times for each building type and earthquake design level combination to yield the slight, moderate, extensive, and complete thresholds. Then, the fragility curve for the component type, building type, and earthquake design level is developed, and together it looks like Figure 6.

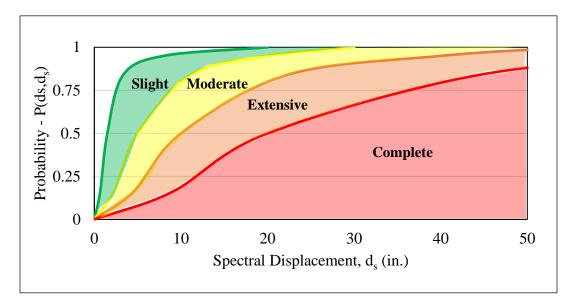


Figure 6. Example Fragility Curve

Fragility curves are automatically defined in Hazus according to the structure's building type and seismic design level.

3. **Results**

RVS Results

The basic score of a building is dependent upon the region of seismicity and building type. While the four counties all generally fall within the "Very High" region of seismicity when looking at Figure 1, using the more detailed procedure in the Methodologies Section determined that all buildings in the study fall within the "Moderately High" to "Very High" Regions of Seismicity. Figure 7 shows what region of seismicity each building falls within. 40 buildings are within the "Very High" region, 36 buildings are within the "High" region, and 9 are within the "Moderately High" region.

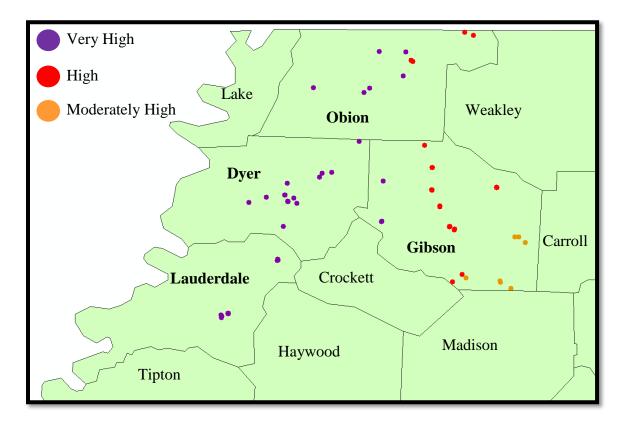


Figure 7. Level of Seismicity Across Study Region

The result in Figure 7 makes sense because the western-most parts of Tennessee are closer to the New Madrid fault line. The FEMA Building Type also helps determine the basic score, S_b , of each building. Table 4 shows the distribution of FEMA Building Types. It is evident from Table 4 that overwhelmingly the greatest number of structures in this region for primary, elementary, and secondary schools are RM1, or reinforced masonry with a flexible diaphragm. A possible reason for this is that once a school system finds an ideal architect to use, the same architect is hired for multiple projects, and the older school plans are referred to create new school plans. This situation was found to occur in several school districts during this study.

FEMA Building Type	Number of Structures	Percent of Structures
C3	9	10.59%
PC1	3	3.57%
PC2	2	2.38%
S3	3	3.57%
S5	15	17.86%
RM1	49	58.33%
RM2	1	1.19%
URM	3	3.57%

Table 4. FEMA Building Types

The basic score of an RM1 building in a "Very High" region of seismicity is only 1.1. Recall that 2.0 is the selected cut-off score. Of the RM1 structures observed, less than 30% had a score higher than the cut-off score. Of the S5 and S3 structures observed, none of them had a score above the cut-off score.

The number of most importance in the RVS procedure is the overall score for each building, S_{LI} , as this is the number that indicates which buildings are more likely or less likely to collapse in the event of an earthquake. Table 5 shows the distribution of building scores.

able J. SLI Scole Distribu		
Range of	Number of	
S_{L1}	Structures	
0.2-0.5	39	
0.6-0.9	7	
1.0-1.5	11	
1.6-1.9	7	
2.0-2.5	7	
2.6-2.9	3	
3.0-3.5	5	
3.6-3.9	6	

From Table 5, approximately 64 of the buildings are more likely to suffer extensive damage in the event of an earthquake, and 21 of the buildings are not likely to suffer extensive damage. While Table 5 gives general information, what causes the buildings to have lower scores is more important. All buildings surveyed have an estimated design year found from either from a plaque in the building, older employees, or building plans. Table 6 shows the period structures were built, and the percentage of structures designed in that decade with a score above the cut-off score.

Year Built	Number of Structures	Percent of Structures	Percent of Structures Above Cut-off Score
1910-1919	1	1.18%	0.00%
1920-1929	0	N/A	N/A
1930-1939	1	1.18%	0.00%
1940-1949	4	4.71%	0.00%
1950-1959	6	7.06%	0.00%
1960-1969	4	4.71%	0.00%
1970-1979	17	20.00%	0.00%
1980-1989	12	14.12%	0.00%
1990-1999	16	18.82%	37.50%
2000-2009	14	16.47%	46.15%
2010-2019	10	11.76%	90.00%

Table 6. Design Year of Buildings

According to Table 5, no buildings built before 1990 have a score above the cut-off score of 2.0. Recall that 1991 is the code year and benchmark year for this region. So, clearly the postbenchmark score modifier seems to push many buildings over the threshold of 2.0. All building types in the "Very High" seismicity region have a basic score, S_b , below 2.0 (excluding W1 buildings), so it is impossible for the final building score, S_{L1} , to surpass 2.0 unless a positive score modifier is present. The only positive score modifiers are the post-benchmark score modifier, S_{pb} , and some soil type score modifiers, S_{soil} . Since no buildings are located on a site with soil type A or B, the only applicable positive score modifier for the study region is S_{pb} . Figure 8 further shows the relationship between the year built and the building score, S_{L1} . The correlational coefficient between S_{L1} and the year built is 0.64, which indicates a moderate correlation between the two variables. It can be deduced that the year built is the single-most deciding factor of which buildings are most likely to have a score above the cut-off score for this study region.

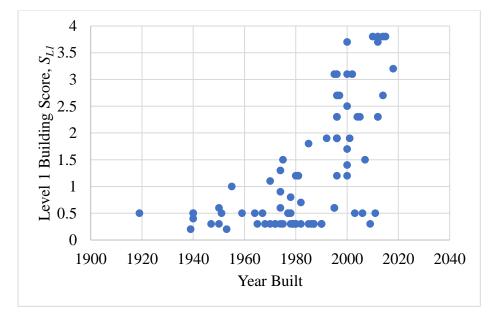


Figure 8. Building Score vs. Year Built

In addition to the year built, whether a building has irregularities has a significant impact on the score of the building. Table 7 shows the impact of the presence of irregularities on the overall score. From Table 7, approximately 45% of buildings surveyed had both a plan irregularity and a vertical irregularity. Of the 38 buildings, only one had a score above the cutoff. The one building that had both irregularities, but still had a score above the cutoff was a PC1 building in a "Moderately High" seismicity region designed post-benchmark with an S_{LI} of 2.5. If the same exact building were constructed in the "High" seismicity region, the score would have been reduced to 2.3, and in a "Very High" seismicity region 1.8. So, there are very few cases when a building with both irregularities could obtain a score above the cut-off score.

Table 7. Integularities of Dunulings		
		Percent of
Irregularity	Number of	Structures Above
Туре	Structures	Cut-off Score
Vertical only	12	16.67%
Plan only	16	56.25%
None	19	47.37%
Both	38	2.63%

Table 7. Irregularities of Buildings

The most common plan irregularity observed was a reentrant corner. A building with a reentrant corner is common even among modern buildings, so although strides have been made in earthquake engineering, buildings are still being designed with awkward plan dimensions. The most popular plan irregularity is a specific example of a reentrant corner, observed in the school buildings and some hospitals, it resembles a spider-like plan view of four or more separate hallways. Although this formation, shown in Figure 9, is convenient for hallway congestion, it is not safe seismically as it causes buildings to be subject to torsion.

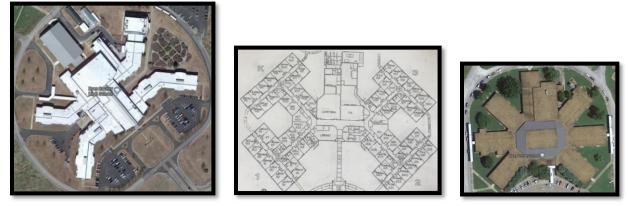


Figure 9. Examples of Buildings with a Reentrant Corner

Hazus-MH 4.2 Results

The Advanced Engineering Building Module (AEBM) within Hazus-MH 4.2 yields damage state probabilities, predicted casualties, as well as predicted economic losses. The damage state probabilities are calculated for three different components: structural components (STR), nonstructural components sensitive to acceleration (NSA), and nonstructural components sensitive to drift (NSD). Structural components of a building consist of materials and systems resisting expected forces, such as beams and columns. Non-structural components sensitive to drift include architectural elements that would be affected by inter-story drifts, such as sheetrock, ceiling tiles, or glass panes inside windows and doors. Non-structural components sensitive to acceleration are items or systems that could be ripped from the structure, including air conditioning units, shelving units anchored to the wall, and sinks. Appendix G contains the damage state probabilities determined for each structure for each case. Appendix H contains the predicted casualties and economic losses. Table 8 shows an example of a building's damage state probabilities for different components. One axiom in probability is that the probability of all possibilities will sum to 1.0 or 100%. For instance, a building is either damaged to a certain degree, completely damaged, or not damaged at all. So, if each different set of components will fall into one of the five damage states described, then each row of Table 8 (and all damage state probability tables) will sum to 1.0. Damage states have different descriptions for each structure type, but generally slight damage, moderate damage, extensive damage, and complete damage all have a clear connotation. If one is interested in knowing what damage states mean for different building types, the damage state definitions by building type are described in FEMA's Hazus-MH 2.1 Earthquake Technical Manual (2012).

Component	None	Slight	Moderate	Extensive	Complete
STR	0.012	0.084	0.527	0.359	0.018
NSA	0.068	0.299	0.426	0.183	0.024
NSD	0.022	0.148	0.585	0.207	0.038

 Table 8. Damage State Probabilities for TN002548

The Damage state probabilities for structural components (STR) are used to compute the Immediate Occupancy Factor, *IO*, and Major Damage Factor, *MD*, both developed by Boling (2009). *IO* is the summation of the "None" and "Slight" damage state probabilities, and it represents the probability that a building may be occupied after an earthquake event. *MD*, or the probability that a building will suffer major damage, is the summation of the "Extensive" and "Complete" damage state probabilities for structural components.

One parameter based solely on occupancy type in Hazus-MH 4.2 is the "Percent Loss" of a structure according to damage state and component type. Since all the structures in this study have the same occupancy type, EDU1, all structures have the same Percent Loss Parameters shown in Table 9. The percent loss parameters are percentages of the building's worth that would be required to replace or repair portions of the building if the building fell into that damage state. For example, if the building in Table 9 suffered moderate damage, 1.9% of the building's cost would be required to repair structural components, an additional 3.2% of the building's cost would be required to repair the non-structural components sensitive to acceleration, and another 4.9% of the building's cost would be required to repair the non-structural components sensitive to drift. It should be noted that the percent loss parameter for the "None" damage state is intuitively zero (0) for all building types, because if a building suffers no damage, then zero money (or zero percent of the building's worth) is required to fix and/or replace damaged materials. The percent loss parameters are used in conjunction with the corresponding damage

27

state probabilities to calculate the Building Replacement Cost Factor, *BRC*, developed by McKenzie Boling (2009). An example calculation of the IO factor, MD Factor, and BRC Factor are shown below for Structure 1, HazusID = TN002548.

	able 9. Perce	ent Loss Par	ameters: EDU	
EDU1 Repair	Slight	Mod	Extensive	Complete
Cost Ratios				
STR	0.4	1.9	9.5	18.9
NSA	0.7	3.2	9.7	32.4
NSD	0.9	4.9	24.3	48.7

Table 9. Percent Loss Parameters: EDU1

The IO Factor is calculated using equation 3:

$$IO = P(N)_{STR} + P(S)_{STR}$$

where $P(N)_{STR}$ is the probability that the building's structural components will suffer "None" damage, and $P(S)_{STR}$ is the probability that the building's structural components will suffer "Slight" Damage. For Structure 1, *IO* is calculated as:

(3)

$$IO = 0.012 + 0.084$$
 (3a)

$$IO = 0.096$$
 (3b)

Therefore, there is about a 9.6% chance that Structure 1 will be able to be occupied immediately after the described earthquake event in Hazus-MH 4.2. *MD* is calculated in a similar manner using Equation 4:

$$MD = P(E)_{STR} + P(C)_{STR}$$
⁽⁴⁾

where $P(E)_{STR}$ is the probability that the building's structural components will suffer "Extensive" damage, and $P(C)_{STR}$ is the probability that the building's structural components will suffer "Complete" Damage. Alternatively, *MD* can be calculated using *IO* as:

$$MD = 1 - P(M)_{STR} - I0 \tag{5}$$

where $P(M)_{STR}$ is the probability that a building's structural components will suffer "Moderate" damage.

$$MD = 0.359 + 0.018 \tag{4a}$$

$$MD = 0.377$$
 (4b)

Therefore, there is a 37.7% chance that Structure 1 will suffer major damage. Finally, *BRC* for Structure 1 is calculated as:

$$BRC = \sum_{i=1}^{3} BRC_i \tag{6}$$

where *i* represents the systems STR, NSA, and NSD, and BRC for each group, *i* is calculated as:

$$BRC_i = \sum_{j=1}^5 P(j)_i * PL_{ij} \tag{7}$$

where j represents the five damage states "None", "Slight"," Moderate"," Extensive", and "Complete", also known as N, S, M, E, and C. So, $P(j)_i$ is the probability of the j^{th} damage state in the i^{th} component group, and PL_{ij} is the percent loss parameter associated with the i^{th} component group and j^{th} damage state. So, BRC_1 , BRC_2 , and BRC_3 are calculated as follows:

$$BRC_{STR} = P(N)_{STR} * PL_{STR,N} + P(S)_{STR} * PL_{STR,S} + P(M)_{STR} * PL_{STR,M} + P(E)_{STR} * PL_{STR,E} + P(C)_{STR} * PL_{STR,C}$$

$$BRC_{STR} = (0.012)0 + (0.084)0.4 + (0.527)1.9 + (0.359)9.5 + (0.018)18.9$$

(7b)

(7a)

 $BRC_{STR} = 4.786$

(7c)

Similarly, $BRC_{NSA} = 4.125$ and $BRC_{NSD} = 9.880$, and BRC for structure one is:

$$BRC = BRC_{STR} + BRC_{NSA} + BRC_{NSD}$$
(6a)

$$BRC = 4.786 + 4.125 + 9.880$$
(6b)

$$BRC = 18.791$$
(6c)

So, based on the *BRC* calculated for Structure 1, after the earthquake event it was subjected to in Hazus-MH 4.2, it will cost an estimated 18.791% of the structure's cost to repair it.

The Pearson correlational coefficient, r, shows how closely two variables x and y are linearly related, and r is calculated using:

$$r = \frac{\sum_{i=1}^{n} (z_{x_i} z_{y_i})}{n-1}$$
(8)

where *n* is the number of (x,y) pairs. z_{xi} is the z-value for x_i and z_{yi} is the z-value for y_i from statistics, and the z-value is calculated using the formula:

$$z_a = \frac{a - \mu}{\sigma} \tag{9}$$

Where *a* is the x_i or y_i of interest, μ is the mean of all *a*, and σ is the standard deviation of all *a*. r ranges from -1 to +1. About 68% of all values of a dataset fall within one standard deviation of the mean, 95% fall within two standard deviations of the mean, and 99% fall within three standard deviations of the mean. A negative correlational coefficient indicates an inverse relationship between two variables, and a positive correlational coefficient indicates a positive correlation between to variables. If the magnitude (or absolute value) of r is between 0 and 0.3, then there is no significant correlation between the two variables. If the absolute value of r falls between 0.3 and 0.7, then there is a moderate correlation between the two variables. Then, it is

deduced that if r falls between 0.7 and 1, then there is a strong correlation between the two variables. The correlational coefficient is commutative, so it does not differentiate between the dependent and independent variables. The correlational coefficient will be used to help identify relationships, if any, between resultant variables.

The results from this study are divided into the three separate cases discussed earlier: All four counties with the coarse ground motion maps, Dyer County TN with the coarse ground motion maps, and Dyer County TN with the finer Dyer County TN ground motion maps. *IO*, *MD*, and *BRC* values will be presented and discussed for each case below. Then, the resultant variables are used to sort the structures from safest to least safe in Appendices F-H.

Dyer, Gibson, Lauderdale and Obion County: Coarse Map Results

Dyer, Gibson, Lauderdale, and Obion counties encompass the entire study region, so all 85 structures were analyzed in this case. The ground motion maps used for this case were the coarse maps developed on a 0.1° grid with PGA values ranging from 0.447g-1.600g. This dataset recorded many buildings with high Moderate, Extensive, and Complete damage state probabilities. Table 10 gives a summary of the variables calculated for this case.

	S_{L1}	BRC (%)	ΙΟ	MD
Average, μ	1.275	50.235	0.117	0.696
Standard Deviation, σ	1.124	31.228	0.238	0.351
Unique Values	24	45	22	38

Table 10. Case 1: Summary of Result Variables

From Table 10, The average *BRC* and *MD* are high, and the average *IO* and S_{LI} are low. This generally makes sense, because if there is more likely to be a lot of damage and almost half the cost of a structure is required to repair it, then it is likely that the structure will not be immediately occupied, thus a score below the cut-off score of 2.0 is also expected. While the averages make sense, the standard deviations are high. For instance, $\sigma = 31.228$ for *BRC*, meaning only 68% fall within 20% and 80%, indicating *BRC* is highly varied. The unique values are recorded to rank the structures later. Table 11 lists the correlational coefficient matrix which is used to analyze the relationships between the variables.

	S_{L1}	<i>BRC</i> (%)	ΙΟ	MD
S_{L1}	1	-0.287	-0.113	-0.124
BRC (%)	-0.287	1	-0.673	0.910
IO	-0.113	-0.673	1	-0.871
MD	-0.124	0.910	-0.871	1

Table 11. Case 1: Correlational Coefficient Matrix

From Table 11, there is a strong positive relationship between BRC and MD. There is also a strong negative relationship between MD and IO, which is guaranteed since each has a direct influence over the other in Equation 5. There is a moderate inverse relationship between BRC and IO. All relationships involving SL1 are considered insignificant. However, the relationship between S_{L1} and *BRC* is very close to the threshold of a moderate inverse correlation. These relationships described are shown graphically in Figures 10-12.

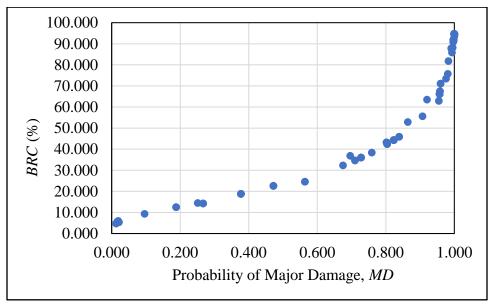


Figure 10. Case 1: BRC vs. MD

From Figure 10, as the probability of major damage increases, the estimated cost to repair the structure also increases. The strong correlation between BRC and MD is clearly visible in Figure 10. Intuitively, a BRC and IO should be inversely correlated.

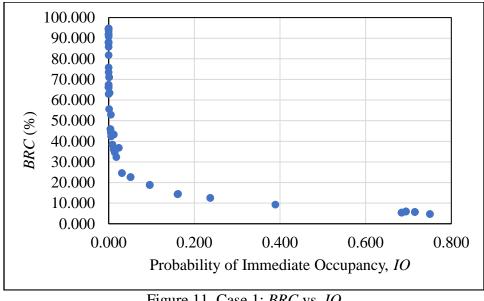


Figure 11. Case 1: BRC vs. IO

From Figure 11, as the probability of immediate occupancy increases, the cost to repair the building decreases. Though the graph above shows a seemingly strong inverse correlation exists, the correlational coefficient, r, is -0.673, indicating a moderate inverse correlation. The primary reason for this is the large variation in *BRC* when *IO* is zero. For an IO = 0, *BRC* ranges anywhere from 55%-95%.

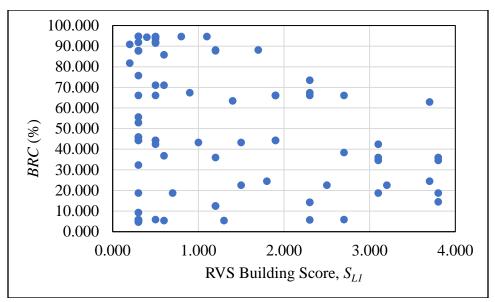


Figure 12. Case 1: BRC vs. SL1

Since S_{LI} represents the resistance to earthquakes, all scores above 2.0 should have a lower *BRC*, and scores below 2.0 should have a higher *BRC*. However, S_{LI} was determined using a different methodology (RVS) that is based on different, more basic assumptions related to the age of the building, the shape of the building, and general site conditions. So, it makes sense that there is not a strong correlation between two variables developed using different methods. However, it should be noted that the weaker correlation that does exist is negative, showing that generally a lower S_{LI} results in a higher *BRC*. Appendix I shows the structures sorted using the variable with the largest number of unique values first, which is *BRC*. Any ties are broken with the variable with the second-most unique values, *MD*, followed by S_{LI} and *IO*.

After the structures in this case were ranked, they were plotted over a map displaying the PGA values in Figure 13 to see if there is a relationship between the higher PGA values and the final rank of the structures.

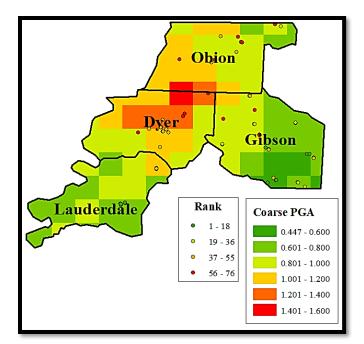


Figure 13. Rank and Coarse Map PGA Values

Clearly, from Figure 13, there is a correlation between the PGA values and the rank of the building, even though the PGA value for the structure was not directly a sorting mechanism. The PGA values correspond very well to the level of seismicity shown in Figure 7 that helps determine S_{Ll} , and the PGA values help directly calculated the probability that a building's various components will fall into a certain damage state.

Dyer County: Coarse Map Results

Dyer County encompasses 17 of the structures surveyed. The ground motion maps used for this case were the coarse maps developed on a 0.1° grid with PGA values ranging from 0.69g-1.69g. This dataset is a subset of case 1, and thus the results are a subset of case 1. All structures in this area recorded "Complete" as the highest damage state probability for all components. Compared to the other three counties, Dyer county was subjected to the highest ground motions (most of the county was subjected to 1g-1.6g PGA values). Table 12 gives a summary of the variables calculated for this case.

	S_{LI}	BRC (%)	IO	MD
Average, μ	1.235	78.432	0	0.976
Standard Deviation, σ	0.865	14.069	0	0.021
Unique Values	8	5	1	5

Table 12. Case 2: Summary of Result Variables

There is significantly less variation in BRC, IO, and MD than in case 1. One possible reason for that is the fact that all the buildings are subjected to significantly higher ground motions than the remaining three counties. Since IO = 0 for all the Dyer County results, it is impossible to calculate a correlational coefficient between it and any other variable. Since these results are a subset of case 1, it is hypothesized that the correlations will be weaker. The correlational coefficient matrix is shown in Table 13.

	S_{Ll}	<i>BRC</i> (%)		MD
S_{L1}	1	-0.636	-	-0.606
BRC (%)	-0.636	1	-	0.995
ΙΟ	-	-	1	-
MD	-0.606	0.995	-	1

Table 13. Case 2: Correlational Coefficient Matrix

Although *r* was unable to be calculated for *IO* and any other variable, the existing correlational coefficients for this subset are higher than for case 1. There is a strong positive correlation between *MD* and *BRC*. There is a moderate inverse correlation between S_{LI} and *BRC*. There is a moderate inverse correlation between *S*_{LI} and *BRC*. There is also a moderate inverse correlation between S_{LI} and *MD*. These results are shown in Figures 14-16.

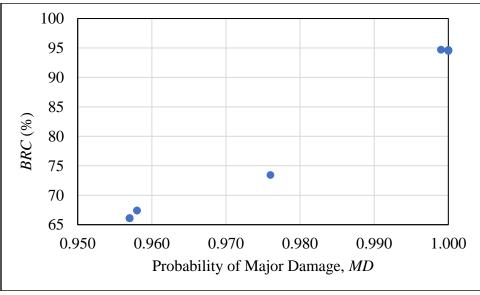


Figure 14. Case 2: BRC vs. MD

Although there is clearly a strong positive correlation between *BRC* and *MD*, as r = 0.995 for the pair, shown in Figure 14, recall that each variable only has 5 unique values.

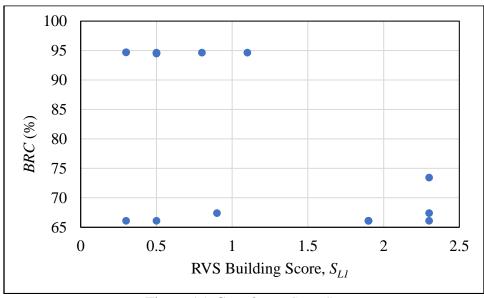


Figure 15. Case 2: BRC vs. SL1

While Figure 15 does not appear to display much of a correlation, it does show that the higher scoring buildings have relatively lower *BRC* values compared to the lower scoring buildings.

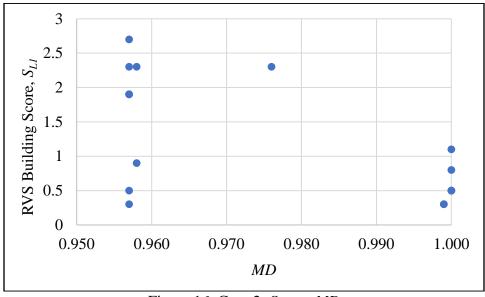


Figure 16. Case 2: SLI vs. MD

Again, although there does not seem to graphically be a significant relationship between S_{LI} and MD, the probability of major damage is generally lower for buildings with higher scores. The problematic part of the correlational coefficient for these specific pairs (S_{LI} , BRC, and S_{LI} ,MD) is that even the buildings scoring above the benchmark of 2.0 still record BRCs upwards of 60% and MDs higher than 95%. So, although there is a correlation, S_{LI} operates on different assumptions than the Hazus-MH software. Appendix J shows the structures sorted using the variable with the most unique values first, which is BRC. Any ties are broken with the variable with the second-most unique values, MD, followed by S_{LI} . Since all IO are zero for this case, it does not affect the ranking.

Dyer County: Finer Map Results

Dyer County encompasses 17 of the structures surveyed. The ground motion maps used for this case were the finer maps developed on a 0.005° grid with PGA values ranging from 0.690g-

38

1.800g. All structures in this area recorded "Complete" as the highest damage state probability for all components. This is likely due to the higher ground motions. Table 14 gives a summary of the variables calculated for this case.

	1 4010 1 11 04			
	S_{L1}	<i>BRC</i> (%)	ΙΟ	MD
Average, μ	1.235	81.434	0.000118	0.983
Standard Deviation, σ	0.865	11.921	0.000332	0.017
Unique Values	8	14	2	9

Table 14. Case 3: Summary of Result Variables

The *BRC* and *MD* values are slightly higher for this case than for case 2. This makes sense because the ground motion values are higher for the finer maps than the coarse maps. The *IO* value is still relatively zero. The average S_{LI} is the same for this case as case 2, because S_{LI} does not change according to earthquake event. So, if the buildings surveyed are the same sample, S_{LI} will not change due to what earthquake event is considered. The correlational coefficient matrix for this case is shown in Table 15:

	Tuele Iei euse	or contentional co	ernerent maann	
	S_{L1}	BRC (%)	IO	MD
S_{L1}	1	-0.579	-0.059	-0.443
BRC (%)	-0.579	1	-0.533	0.965
IO	-0.059	-0.533	1	-0.719
MD	-0.443	0.965	-0.719	1

Table 15. Case 3: Correlational Coefficient Matrix

From Table 15, there is a strong positive correlation between *BRC* and *MD*, and *MD* and *IO*. There is a moderate inverse correlation between S_{L1} and *BRC*, *BRC* and *IO*, and *MD* and S_{L1} . Since there is very little variation in *IO* and *BRC*, while S_{L1} is incredibly varied, a similar situation to case 2 occurs in which the structures with S_{L1} greater than 2 still have *BRC* greater than 60% and *MD* probabilities higher than 98%. So, while the correlations are in the right direction, there is clearly a disconnect between the RVS methodology and Hazus-MH 4.2 software. Appendix K shows the ranking structures according to the number of unique values. So, the structures are first ranked by *BRC*, then *MD*, S_{Ll} , and *IO*.

Discussion and Conclusions

This study was initially funded to locate the most seismically vulnerable buildings utilizing the RVS Method and the most up-to-date available local seismic data. After surveying each building, recording data, and running three Hazus-MH 4.2 advanced analyses, the buildings have been sorted from least seismically vulnerable to most seismically vulnerable. Appendix L gives the individual structure Level 1 Data Collection Forms for the 85 structures surveyed. Individual school building names have been removed. Table 16 gives results from Case 1 showing the distribution of structures that fall into the highest, upper, lower, and lowest quadrants of the total ranking from 1-76. Recall that although there are 85 structures, there are also ties that result in 76 ranks.

Rank	Dyer	Gibson	Lauderdale	Obion
1-18	0.00%	25.58%	57.14%	0.00%
19-36	0.00%	34.88%	0.00%	27.27%
37-55	58.82%	13.95%	42.86%	27.27%
56-76	41.18%	25.58%	0.00%	45.45%
Total	100.00%	100.00%	100.00%	100.00%

Table 16. Percent of Structures in Each County Ranking

Table 16 indicates that Obion County contains the highest percentage of seismically vulnerable schools, followed by Dyer County, Gibson County, and Lauderdale County. Hopefully, this table sheds some light on which counties need more immediate attention in terms of which school buildings to retro-fit first.

After utilizing both methods and calculating correlational coefficients between resultant variables from both methods, it has been determined that there is little correlation between the RVS method and Hazus-MH 4.2 software. Some reasons include that the underlying assumptions and required variables are different. Additionally, in the RVS method, there is no distinguishable difference between a structure with $S_{LI} = 0.2$ and a structure with $S_{LI} = 1.9$. According to RVS, both need "a more detailed structural evaluation," so the RVS method was not initially developed to rank structures. However, there is a slight correlation between SL1 and the final ranking of the structures in Case 1:

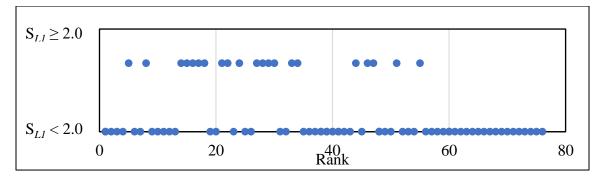


Figure 17. Case 1: *S*_{L1} Versus Rank

Although not a perfect correlation, the structures with a score of 2.0 or higher generally ranked better than structures with a score below 2.0.

After utilizing both methods, it is recommended that screeners use Hazus-MH 4.2 to rank structures from least seismically vulnerable to most seismically vulnerable, as RVS is not an extremely reliable indicator of seismic vulnerability for comparison of structures. The primary reason that RVS does not perform well for comparing structures is that it uses a "yes" or "no" approach for all parameters except for building type, soil type, and region of seismicity. In contrast, Hazus-MH 4.2 uses all categorical variables.

4. APPENDICES

Appendix A: Region of Seismicity's Effect on Level 1 Data Collection Form

Figures A1-A5 show the "Basic Score, Modifiers, and Final Level 1 Score, S_{L1} " section of the Level 1 Data Collection form for the Low, Moderate, Moderately High, High, and Very High seismicity regions, respectively. Figure A6 shows the entire Level 1 Data Collection form for the "Very High" region of seismicity.

The top row of each table indicates the FEMA Building Type that describes the materials and construction methods used in the building that result in a basic score for the building against a collapse in the event of an arbitrary earthquake. For instance, the first FEMA building type on the form in Figure A1 is "W1", which is a "light wood frame single- or multiple-family dwelling." For more information on what each building type is, see Appendix B. As shown in Figure A1, the basic score for W1 is 6.2. (For a reference point, the generally accepted cut-off score is 2.0). When looking at Figure A2, the score for the W1 building decreases to 5.1. In Figures A3-A5, the basic score for a W1 structure continues the downward trend with 4.1, 3.6, and 2.1, respectively. Upon closer inspection of the Very High seismicity region represented in Figure A5, W1 is the only FEMA building type with a basic score above the cut-off score. The reason for the basic score of each building decreasing with each higher seismicity region is that intuitively, a building built in the same manner in a place subjected to higher seismic forces is more likely to collapse.

FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score		6.2	5.9	5.7	3.8	3.9	4.4	4.1	4.5	3.3	4.2	3.5	3.8	3.3	3.7	3.7	3.2	4.6
Severe Vertical Irregularity, VL1		-1.5	-1.5	-1.5	-1.4	-1.3	-1.6	-1.2	-1.3	-1.3	-1.2	-1.1	-1.3	-1.1	-1.1	-1.1	-1.2	NA
Moderate Vertical Irregularity, VL1		-1.0	-0.9	-0.9	-0.9	-0.8	-1.0	-0.7	-0.7	-0.7	-0.7	-0.6	-0.8	-0.6	-0.6	-0.6	-0.7	NA
Plan Irregularity, PL1		-1.6	-1.4	-1.3	-1.2	-1.1	-1.4	-1.0	-1.1	-1.0	-1.0	-0.9	-1.2	-0.9	-0.9	-0.9	-1.0	NA
Pre-Code		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Post-Benchmark		2.2	2.4	2.5	2.0	1.6	1.4	2.1	NA	2.3	2.2	NA	1.9	2.6	2.3	2.3	NA	1.8
Soil Type A or B		0.9	1.1	1.3	1.0	1.2	0.8	1.3	1.4	0.9	1.2	1.2	1.3	1.3	1.4	1.4	1.3	0.9
Soil Type E (1-3 stories)		-1.2	-1.7	-2.3	-1.2	-1.4	-1.0	-1.7	-2.0	-1.4	-2.0	-1.6	-1.7	-1.6	-1.7	-1.7	-1.5	-2.1
Soil Type E (> 3 stories)		-1.7	-2.0	-2.2	-1.2	-1.4	NA	-1.7	-1.9	-1.3	-1.9	-1.6	NA	-1.6	-1.6	-1.7	-1.4	NA
Minimum Score, S _{MIN}		2.7	2.1	1.5	0.9	0.8	1.2	0.8	0.9	0.5	0.6	0.5	0.6	0.4	0.6	0.5	0.4	2.5

Figure A1. Basic Score and Modifiers for Low Seismicity Region

FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score		5.1	4.5	3.8	2.7	2.6	3.5	2.5	2.7	2.1	2.5	2.0	2.1	1.9	2.1	2.1	1.7	2.9
Severe Vertical Irregularity, VL1		-1.4	-1.4	-1.4	-1.2	-1.2	-1.4	-1.1	-1.2	-1.1	-1.2	-1.0	-1.1	-1.0	-1.1	-1.1	-1.0	NA
Moderate Vertical Irregularity, VL1		-0.9	-0.9	-0.9	-0.8	-0.7	-0.9	-0.7	-0.7	-0.7	-0.7	-0.6	-0.7	-0.6	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1		-1.4	-1.3	-1.2	-1.0	-0.9	-1.2	-0.9	-0.9	-0.8	-1.0	-0.8	-0.9	-0.8	-0.8	-0.8	-0.7	NA
Pre-Code		-0.3	-0.5	-0.6	-0.3	-0.2	-0.2	-0.3	-0.3	-0.3	-0.4	-0.3	-0.2	-0.2	-0.2	-0.2	-0.1	-0.5
Post-Benchmark		1.4	2.0	2.5	1.5	1.5	0.8	2.1	NA	2.0	2.3	NA	2.1	2.5	2.3	2.3	NA	1.2
Soil Type A or B		0.7	1.2	1.8	1.1	1.4	0.6	1.5	1.6	1.1	1.5	1.3	1.6	1.3	1.4	1.4	1.3	1.6
Soil Type E (1-3 stories)		-1.2	-1.3	-1.4	-0.9	-0.9	-1.0	-0.9	-0.9	-0.7	-1.0	-0.7	-0.8	-0.7	-0.8	-0.8	-0.6	-0.9
Soil Type E (> 3 stories)		-1.8	-1.6	-1.3	-0.9	-0.9	NA	-0.9	-1.0	-0.8	-1.0	-0.8	NA	-0.7	-0.7	-0.8	-0.6	NA
Minimum Score, S _{MIN}		1.6	1.2	0.9	0.6	0.6	0.8	0.6	0.6	0.3	0.3	0.3	0.3	0.2	0.3	0.3	0.2	1.5

Figure A2. Basic Score and Modifiers for Moderate Seismicity Region

FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score		4.1	3.7	3.2	2.3	2.2	2.9	2.2	2.0	1.7	2.1	1.4	1.8	1.5	1.8	1.8	1.2	2.2
Severe Vertical Irregularity, VL1		-1.3	-1.3	-1.3	-1.1	-1.0	-1.2	-1.0	-0.9	-1.0	-1.1	-0.8	-1.0	-0.9	-1.0	-1.0	-0.8	NA
Moderate Vertical Irregularity, VL1		-0.8	-0.8	-0.8	-0.7	-0.6	-0.8	-0.6	-0.6	-0.6	-0.6	-0.5	-0.6	-0.6	-0.6	-0.6	-0.5	NA
Plan Irregularity, PL1		-1.3	-1.2	-1.1	-0.9	-0.8	-1.0	-0.8	-0.7	-0.7	-0.9	-0.6	-0.8	-0.7	-0.7	-0.7	-0.5	NA
Pre-Code		-0.8	-0.9	-0.9	-0.5	-0.5	-0.7	-0.6	-0.2	-0.4	-0.7	-0.1	-0.4	-0.3	-0.5	-0.5	-0.1	-0.3
Post-Benchmark		1.5	1.9	2.3	1.4	1.4	1.0	1.9	NA	1.9	2.1	NA	2.1	2.4	2.1	2.1	NA	1.2
Soil Type A or B		0.3	0.6	0.9	0.6	0.9	0.3	0.9	0.9	0.6	0.8	0.7	0.9	0.7	0.8	0.8	0.6	0.9
Soil Type E (1-3 stories)		0.0	-0.1	-0.3	-0.4	-0.5	0.0	-0.4	-0.5	-0.2	-0.2	-0.4	-0.5	-0.3	-0.4	-0.4	-0.3	-0.5
Soil Type E (> 3 stories)		-0.5	-0.8	-1.2	-0.7	-0.7	NA	-0.7	-0.6	-0.6	-0.8	-0.4	NA	-0.5	-0.6	-0.7	-0.3	NA
Minimum Score, S _{MIN}		1.6	1.2	0.8	0.5	0.5	0.9	0.5	0.5	0.3	0.3	0.3	0.3	0.2	0.3	0.3	0.2	1.4

Figure A3. Basic Score and Modifiers for Moderately High Seismicity Region

FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1		-1.2	-1.2	-1.2	-1.0	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1		-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1		-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code		-1.1	-1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark		1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B		0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)		0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, S _{MIN}		1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0

Figure A4. Basic Score and Modifiers for High Seismicity Region

FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	\$4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score		2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Severe Vertical Irregularity, VL1		-0.9	-0.9	-0.9	-0.8	-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Moderate Vertical Irregularity, VL1		-0.6	-0.5	-0.5	-0.4	-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3	NA
Plan Irregularity, PL1		-0.7	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code		-0.3	-0.3	-0.3	-0.3	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark		1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type A or B		0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (1-3 stories)		0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories)		-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, S _{MIN}		0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0

Figure A5. Basic Score and Modifiers for Very High Seismicity Region

Figure A6 shows the entire Level 1 Data Collection form for the "Very High" region of

seismicity. How to fill out this form is described in the Methodologies section under "RVS."

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Level 1 VERY HIGH Seismicity

													Add	fress:										
														_						2	Sip:			
													Oth	er Identi	ifiers:									
													Bui	lding Na	me:									
													Lat	itude:					Lonaitu	de:				
						рнот	OGR	APH					Sc.						Sr:	_				
													Scr	eener(s)	:				D	ate/Time				
													No.	Stories	Abov	e Grade	5	Belo	w Grade	5	Yea	r Built	[EST
													Tot	al Floor	Агеа (зо	1, mt.):					Code	Year:		
														titions:										
													Oct	supancy		embly striel	Office		Erner, S School			istonic overnmen	□ Shelt #	er
															Util	y .	Wareho	use	Residen	tial, ≢Ur				
													Soi	І Туре:							JF D		-	-
															Hard Rock	Avg Rock	Den				oor /r. Ioil	DNK, ess	ите Туре	D.
													Geo	ologic Ha	azarda:	Liquefec	tion: Yes	No/DN	K Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/	No/DNK
													Adj	acency:			ounding		Falling H	azards fr	om Taller	Adjaceni	t Building	
													IПе	gularitie	G:	_	ertical (ty		ity)					
													_				an (type)							
											erior Fal ards:	ling		ibraced (propets				svy Clado sendages		eavy Ver	leer			
														arapets ther:										
											CC	MMENT	S:											
													_											
													_											
	_												_											
													_											
	+												_											
													_											
						SP	ETC	н						Addition	al sketch	es or cor	nments o	n separa	ste page					
								BA	ASIC	sco	RE, MO	DIFIE	RS, A	ND FIN	IAL LE	EVEL	1 SCO	RE, S	L1					
FEMA B	UILC	NNG	TYPE			Do Not Know		1	W1A	W2	81 (MRF)	92 (BR)	33 (JM)	84 (RC	S5 (UFM	C1 MRD	C2 (SW)	CS (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (PD)	URM	MH
Basic S							2	-	19	1.8	15	14	1.6	św) 1.4	INF)	1.0	1.2	INF)	1.1	10	1.1	1.1	0.9	1.1
Severe \	/ertic	al In					-0		-0.9	-0.9		-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Moderat				derity,	VLr		-0	6	-0.5 -0.7	-0.5		-0.4 -0.5	-0.5	-0.4	-0.3 -0.4	-0.4 -0.4	-0.4 -0.5	-0.3 -0.3	-0.4 -0.5	-0.4	-0.4	-0.4	-0.3 -0.3	NA NA
Plan Ine Pre-Cod		ny, r	14				-0		-0.3	-0.8		-0.5	-0.0	-0.4	-0.1	-0.4	-0.5	0.0	-0.5	-0.4	-0.4	-0.4	0.0	0.0
Post-Ber							1		1.9	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type Soil Type			-					5	0.5	0.4		0.3	-0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type								4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum								7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL	LEV	/EL	1 SC	ORE	, SLI	≥ S _{MIN}	¢.																	
EXTE	NT	OF	RE	VIE	W						OTHER	R HAZ	ARDS	6		ACT	ION R	EQUI	RED					
Exterior					Partial				Aer		Are Then	Hazan	ds That	Trigger /	4	Detail	ed Struc	tural Ev	aluation	Require	:d?			
Interior Drawing		evie	wed:		None Yes		No	e	Ent	erea	Detailed:						es, unkno es, score				r other b	uilding		
Soil Typ	pe S	ourc	e:	_							cut-o	ff, if kno	wn)			🗆 ¥e	es, other							
Geolog Contact				urce:	_					_	E Fallin	-	ds from t	aller adja	cent									
—										=	buildi Geok		ards or \$	Soil Type	F								eck one)	
LEVE							OR	NED			Signi the d			terioratio	n to							uld be ev vire mitig:	valuated ation, but	
Ves Nonstru					e, S⊔ □ \			_			ine si	according 1	system			de	tailed ev	eluction	is not ne	cessary				
Nonseu	CIUN	al nei			_		Cano	of he	_		ener shal	I note ti	ha follow	vina: E	T = Eaf	_				ls identifi DNK = D		_		
Legend:			"			manche				-	ener snall inforced cor			VING: ES					_	ctured Ho			ie diaphra	gm
						ed frem					cer well			TU = Tit u					= Light m				disphregm	

Figure A6. Level 1 Data Collection Form

Appendix B: FEMA Building Type Descriptions and Compatible Hazus-MH 4.2 Types FEMA over the years has continuously refined the number of recognized building types primarily from the original ATC-14 document (FEMA, 2015). Each of the 17 FEMA building types listed below also has a comparable Hazus-MH 4.2 building type, which is based on FEMA-178 (FEMA 2012). This is important in the screening process to ensure that each structure may be evaluated through both RVS and Hazus-MH 4.2. Otherwise, each site visit would require two separate on-site evaluations.

The only difference between Hazus-MH 4.2 and the Level 1 Data Collection form in terms of building type is that Hazus-MH 4.2 also distinguishes between low, medium, and high-rise buildings and the MH building type for Hazus does not include non-residential buildings, such as school portables. For instance, a 1-3 story S1 is an S1L in Hazus-MH 4.2. similarly, 4-7 story buildings are denoted by adding an "M," and any building over 7 stories is denoted with an "H" after the conventional FEMA building type designation. Some buildings that are only developed at certain heights (for instance, all W1 buildings are 1-3 stories in height), do not include any height designation. So, there is no W1L, W1M, or W1H, only W1. All buildings in this study were 3 stories or less, so they are all classified as low-rise buildings. There is one MH building that was initially screened and subsequently removed from the study due to the inconsistency between RVS and the Hazus-MH 4.2 software. The following list of FEMA building types is directly from FEMA P-154 and the Hazus-MH 4.2 model building types, and descriptions are from Earthquake Model Hazus-MH 2.1 User Manual, published in 2016 and 2012, respectively:

RVS: W1 buildings are Light wood frame single- or multiple-family dwellings of one or more stories in height.
 Hazus: W1 are typically single- or multiple-family dwellings. The essential structural feature of these buildings is repetitive framing by wood rafters or joists on wood stud walls. Loads

are light and spans are small. These buildings may have relatively heavy masonry chimneys and may be partially or fully covered with masonry veneer. Most of these buildings, especially the single-family residences, are not engineered but constructed in accordance with "conventional construction" provisions of building codes. Hence, they usually have the components of a lateral force-resisting system even though it may be incomplete. Lateral loads are transferred by diaphragms to shear walls. The diaphragms are roof panels and floors which may be sheathed with wood, plywood or fiberboard sheathing. Shear walls are exterior walls sheathed with boards, stucco, plaster, plywood, gypsum board, particle board, or fiberboard, or interior partition walls sheathed with plaster or gypsum board.

- RVS: W1A buildings are light wood frame multi-unit, multi-story residential buildings with plan areas on each floor of greater than 3,000 square feet.
 Hazus: Hazus does not recognize the difference between W1 and W1A buildings, so if the RVS screener/Hazus user encounters a W1A building in the field, consider it a W1 building in Hazus software.
- RVS: W2 buildings are wood frame commercial and industrial buildings with a floor area larger than 5,000 square feet.
 Hazus: These buildings usually are commercial or industrial buildings with a floor area of

5,000 square feet or more and with few, if any, interior walls. The essential structural character of these buildings is framing by beams or major horizontally spanning members over columns. These horizontal members may be glued-laminated wood, solid-sawn wood beams, or wood trusses, or steel beams, or trusses. Lateral loads usually are resisted by wood diaphragms and exterior walls sheathed with plywood, stucco, plaster, or other paneling. The walls may have diagonal rod bracing. Large openings for storefronts and garages often require post-and-beam framing. Lateral load resistance on those lines may be achieved with steel rigid frames (moment frames) or diagonal bracing.

- 4. **RVS:** S1 buildings are steel moment-resisting frame buildings.
 - **Hazus:** S1L, S1M, and S1H buildings have a frame of steel columns and beams. In some cases, the beam-column connections have very small moment resisting capacity but, in other cases, some of the beams and columns are fully developed as moment frames to resist lateral forces. Usually the structure is concealed on the outside by exterior walls, which can be of almost any material (curtain walls, brick masonry, or precast concrete panels), and on the inside by ceilings and column furring. Lateral loads are transferred by diaphragms to moment resisting frames. The diaphragms can be almost any material. The frames develop their stiffness by full or partial moment connections. The frames can be located almost anywhere in the building. Usually the columns have their strong directions oriented so that some columns act primarily in one direction while the others act in the other direction. Steel moment frame buildings are typically more flexible than shear wall buildings. This low stiffness can result in large inter-story drifts that may lead to relatively greater nonstructural damage.
- 5. **RVS:** S2 buildings are braced steel frame buildings.

Hazus: S2L, S2M, and S2H buildings are like steel moment frame buildings except that the vertical components of the lateral-force-resisting system are braced frames rather than moment frames.

6. **RVS:** S3 buildings are light metal buildings.

Hazus: S3 buildings are These buildings are pre-engineered and prefabricated with transverse rigid frames. The roof and walls consist of lightweight panels, usually corrugated metal. The frames are designed for maximum efficiency, often with tapered beam and column sections built up of light steel plates. The frames are built in segments and assembled in the field with bolted joints. Lateral loads in the transverse direction are resisted by the rigid frames with loads distributed to them by diaphragm elements, typically rod-braced steel roof framing bays. Loads in the longitudinal direction are resisted entirely by shear elements which can be either the roof and wall sheathing panels, an independent system of tension-only rod bracing, or a combination of panels and bracing.

- 7. RVS: S4 buildings are steel frame buildings with cast-in-place concrete shear walls. Hazus: S4L, S4M, and S4H buildings have shear walls that are cast-in-place concrete and may be bearing walls. The steel frame is designed for vertical loads only. Lateral loads are transferred by diaphragms of almost any material to the shear walls. The steel frame may provide a secondary lateral-force-resisting system depending on the stiffness of the frame and the moment capacity of the beam-column connections. In modern "dual" systems, the steel moment frames are designed to work together with the concrete shear walls in proportion to their relative rigidities.
- 8. **RVS:** S5 buildings are steel frame buildings with unreinforced masonry infill walls. **Hazus:** S5L, S5M, and S5H buildings are This is one of the older types of buildings. The infill walls usually are offset from the exterior frame members, wrap around them, and present a smooth masonry exterior with no indication of the frame. Solidly infilled masonry panels, when they fully engage the surrounding frame members (i.e. lie in the same plane), provide stiffness and lateral load resistance to the structure.
- 9. RVS: C1 buildings are concrete moment-resisting frame buildings. Hazus: C1L, C1M, and C1H buildings are like steel moment frame buildings except that the frames are reinforced concrete. There is a large variety of frame systems. Some older concrete frames may be proportioned and detailed such that brittle failure of the frame members can occur in earthquakes, leading to partial or full collapse of the buildings. Modern frames in zones of high seismicity are proportioned and detailed for ductile behavior and are likely to undergo large deformations during an earthquake without brittle failure of frame members and collapse.
- 10. RVS: C2 buildings are concrete shear-wall buildings.

Hazus: C2L, C2M, and C2H buildings have vertical components of the lateral-forceresisting system that are concrete shear walls that are usually bearing walls. In older buildings, the walls often are quite extensive, and the wall stresses are low, but reinforcing is light. In newer buildings, the shear walls often are limited in extent, thus generation concerns about boundary members and overturning forces.

- 11. **RVS:** C3 buildings are concrete frame buildings with unreinforced masonry infill walls. **Hazus:** C3L, C3M, and C3H buildings are like steel frame buildings with unreinforced masonry infill walls except that the frame is of reinforced concrete. In these buildings, the shear strength of the columns, after cracking of the infill, may limit the semi ductile behavior of the system.
- 12. RVS: PC1 buildings are tilt-up buildings

Hazus: PC1 buildings have a wood or metal deck roof diaphragm, which often is very large, that distributes lateral forces to precast concrete shear walls. The walls are thin but relatively heavy while the roofs are relatively light. Older buildings often have inadequate connections for anchorage of the walls to the roof for out-of-plane forces, and the panel connections often are brittle. Tilt-up buildings usually are one or two stories in height. Walls can have numerous openings for doors and windows of such size that the wall looks more like a frame than a shear wall.

13. RVS: PC2 buildings are precast concrete frame buildings

Hazus: PC2L, PC2M, and PC2H buildings contain floor and roof diaphragms typically composed of precast concrete elements with or without cast-in-place concrete topping slabs. The diaphragms are supported by precast concrete girders and columns. The girders often bear on column corbels. Closure strips between precast floor elements and beam-column joints usually are cast-in-place concrete. Welded steel inserts often are used to interconnect precast elements. Lateral loads are resisted by precast or cast-in-place concrete shear walls. For buildings with precast frames and concrete shear walls to perform well, the details used to connect the structural elements must have sufficient strength and displacement capacity; however, in some cases, the connection details between the precast elements have negligible ductility.

14. **RVS:** RM1 buildings are reinforced masonry buildings with flexible floor and roof diaphragms.

Hazus: RM1L and RM1M buildings have perimeter bearing walls of reinforced brick or concrete-block masonry. These walls are the vertical elements in the lateral-force-resisting system. The floors and roofs are framed either with wood joists and beams with plywood or straight or diagonal sheathing, or with steel beams with metal deck with or without a concrete fill. Wood floor framing is supported by interior wood posts or steel columns; steel beams are supported by steel columns.

- 15. **RVS:** RM2 buildings are reinforced masonry buildings with rigid floor and roof diaphragms. **Hazus:** RM2L, RM2M, and RM2H buildings have bearing walls similar to those of reinforced masonry bearing wall structures with wood or metal deck diaphragms, but the roof and floors are composed of precast concrete elements such as planks or tee-beams and the precast roof and floor elements are supported on interior beams and columns of steel or concrete (cast-in-place or precast). The precast horizontal elements often have a cast-in-place topping.
- 16. RVS: URM buildings are unreinforced masonry bearing-wall buildings

Hazus: URML and URMM buildings are These buildings include structural elements that vary depending on the building's age and, to a lesser extent, its geographic location. In buildings built before 1900, the majority of floor and roof construction consists of wood sheathing supported by wood sub-framing. In large multistory buildings, the floors are cast-in-place concrete supported by the unreinforced masonry walls and/or steel or concrete interior framing. In unreinforced masonry constructed after 1950 wood floors usually have plywood rather than board sheathing. In regions of lower seismicity, buildings of this type constructed more recently can include floor and roof framing that consists of metal deck and concrete fill supported by steel framing elements. The perimeter walls, and possibly some interior walls, are unreinforced masonry. The walls may or may not be anchored to the diaphragms. Ties between the walls and diaphragms are more common for the bearing walls than for walls that are parallel to the floor framing. Roof ties usually are less common and more erratically spaced than those at the floor levels. Interior partitions that interconnect the floors and roof can have the effect of reducing diaphragm displacements.

17. **RVS:** MH buildings are manufactured housing. FEMA also includes non-residential buildings, such as school portables.

Hazus: MH buildings are prefabricated housing units that are trucked to the site and then placed on isolated piers, jack stands, or masonry block foundations (usually without any positive anchorage). Floors and roofs of mobile homes usually are constructed with plywood and outside surfaces are covered with sheet metal. Hazus software does not include non-residential buildings, such as school portables.

Appendix C. Procedure for CDMS Data Entry

Data entry into CDMS is briefly described in the Methodologies Section of this document. However, below is a more thorough guide complete with screen captures and specific references. First, one needs to select the state to update or replace inventory. State databases are found on FEMA's website at https://msc.fema.gov/portal/resources/hazus. The state databases are shown alongside downloading different versions of Hazus, but it is acceptable to just download a state database by itself. Save a copy of the statewide dataset separately from the one being modified. Once the database is saved, Open CDMS. CDMS is downloaded with Hazus, however it has its own icon and is opened separately from Hazus. The CDMS home screen is shown in Figure C1.

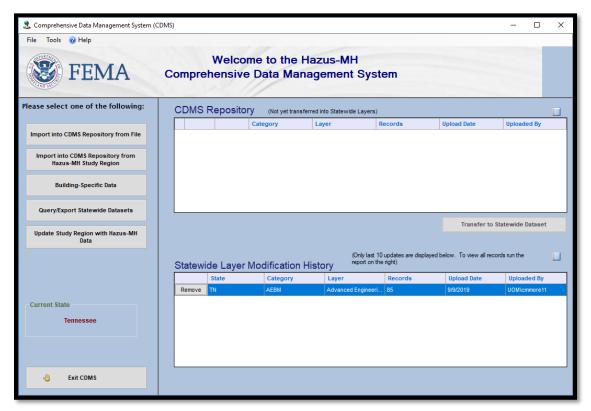


Figure C1. CDMS Home Screen

The home screen will have "Select a State" where "Tennessee" is shown in red in Figure C1. All of the following is useful for users seeking to run an AEBM module, and currently has a Microsoft Excel Spreadsheet to enter data into Hazus-MH 4.2. First, select the button that says "Import into CDMS Repository from File" as shown in Figure C1. Figure C2 will appear.

2 Comprehensive Data Management System	(CDMS)	- 🗆 X
File Tools 🕜 Help		
FEMA	Welcome to the Hazus-MH Comprehensive Data Management System	
Please select one of the following:	Import into CDMS Repository	
Import into CDMS Repository from File	Point O Line For Tsunami select both Earthquake and Flood Select a file for Import:	
Import into CDMS Repository from Hazus-MH Study Region	Specify hazards importing data for: Earthquake Flood Hurricane Wind Fields corresponding to the hazards selected will be displayed in the Field Matchi If importing an excel document. Jease make sure the first row contains field name	
Building-Specific Data	If importing a mdb file, please make sure file names have four (4) or more charact	
Query/Export Statewide Datasets Current State Tennessee	AEBM The following fields: The following fields are required for up information. Please make sure your dat required fields below: Select Hazus-MH Inventory Dataset (Layer): Area (Sq feet) Advanced Engineering Building Module Advanced Engineering Building Module Ccupany Type 	
Exit CDMS	Continue 💇	CDMS Home

Figure C2. Import into CDMS Repository from File Page

Choose the options shown in Figure C2. The required fields for the AEBM module will appear in the right pane. As shown in Figure C2, the required fields to run the AEBM module are the area of the structure in square feet, the earthquake building type (learn more in Appendix B), earthquake design level, and the Occupancy type. All of the required fields are discussed in detail in the Methodologies Section. Select the Microsoft Excel file that includes at least all four of the required fields, the latitiude of the structure, and the longitude of the structure. If one is

updating previous inventory, be sure to include the Hazus ID to avoid having duplicate

structures. Ensure only "Earthquake" is selected as the specified hazard. Figure C3 will appear.

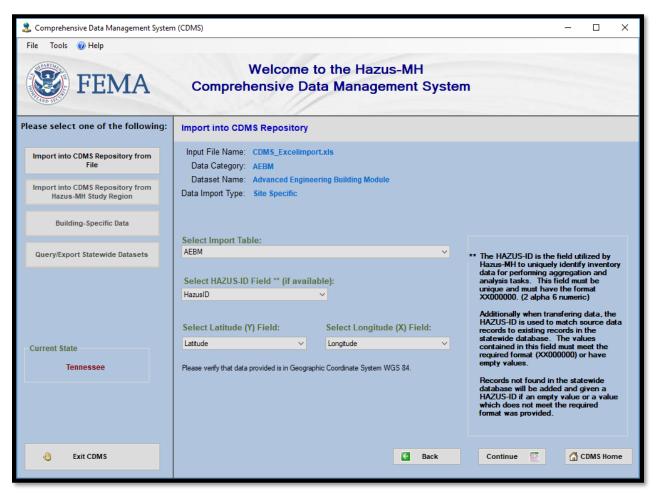


Figure C3. Import into CDMS Repository Screen

Choose the options shown in Figure C3. Then select "Continue". CDMS will then begin to validate the data. This process appears different for each file imported. However, there is a uniform process applied to each file. Refer to Figure C4 below.

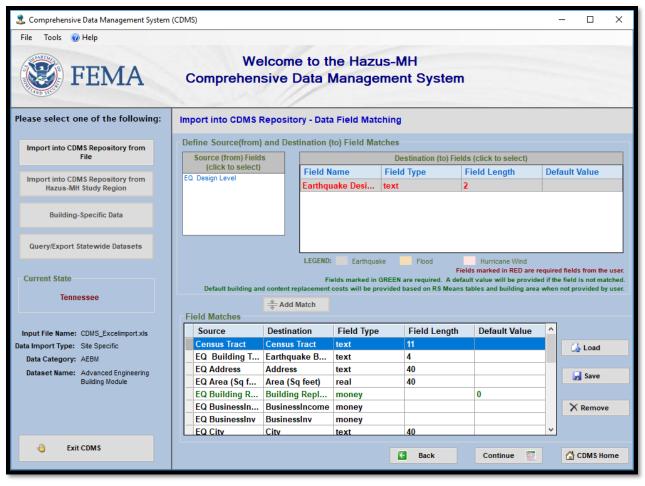


Figure C4. Data Field Matching Window

As Figure C4 shows, CDMS automatically matches as many fields as it can detect. The fields in black are not required but are recognized by CDMS and Hazus as useful fields for plotting or other purposes. The fields marked in green are required to be present, but the user may leave them all empty (such is the case for this study). Hazus uses RS Means to estimate the economic parameters. The fields marked in red are required, and default values will not be estimated by Hazus. As one can see in Figure C4, although the user has specified an "EQ Design Level", CDMS did not automatically detect the field as the "Earthquake Design Level" shown in red. So, the user must first click the source field in the left pane, the destination field in the right pane,

and finally click the "Add Match" button. Click "Continue." The "Category Value Matching" window will appear for applicable fields, as shown in Figure C5.

logory raido in	atching : Earthq	uake Buil	ding Type		
ource (click to :	select) [Destinatio	on (click to sel	lect)	Ź
Field Val		Value		Description	1
3		C1H		Concrete Mome	
3L	C. Constanting	C1L		Concrete Mome	
		C1M		Concrete Mome	
		C2H		Concrete Shear	
		C2L		Concrete Shear	
Marine and a second		C2M		Concrete Shear	
		C3H		Concrete Frame	. ~
latching Res	Add № Ilts Destinatio		escription		1
	C3L	Co		🔹 🚺 Load	
C3L	CJL		ncrete Fr	Lur coud	
C3L PC1	PC1		ncrete Fr ecast Con		
		Pr			
PC1	PC1	Pro Pro	ecast Con		
PC1 PC2L	PC1 PC2L	Pro Pro Re	ecast Con ecast Con		

Figure C5. Category Value Matching Window

The user is to match the source fields (specified in the excel spreadsheet) to the destination fields (CDMS Data Dictionary definitions). In the example above, "S3L" is not recognized, because according to Hazus all "S3" buildings are low-rise, so the official designation is "S3." If CDMS did not go through the process in Figure C5, the user would have to detect and re-type all the "S3L" buildings as "S3". However, using CDMS the user can match the "S3L" in the left pane to the S3 designation in the right pane, and CDMS will correct the designation for calculations in Hazus. This feature is what makes CDMS such a powerful tool for data entry. Continue for all fields. Finally, CDMS will notify the user that data has been imported into the CDMS repository. Select "OK." The user is then returned to the home screen, and the data will be displayed in the top pane. The user may view, edit, or remove the data in the top pane. To use the data in Hazus,

the data must be transferred to the statewide dataset by pushing the appropriate button on the home screen. The user will specify to either "update" or "replace" the statewide inventory. Once the data has been transferred to the statewide dataset, it can only be removed if it is replaced. For example, if the dataset given contains 10 buildings, the user adds 6, but only wanted to add 5. The only way to remove the 6th building is by replacing all 16 buildings with the 5 buildings by importing 5 buildings and specifying to "replace" the statewide database. However, the original 10 buildings the dataset started with will be lost unless the user keeps a copy of the dataset saved separately.

Appendix D: Procedure for Creating Ground Motion Maps from Text File Compatible with Hazus-MH 4.2

A procedure for converting ground motion point data into a Hazus compatible map was first developed in 2009 for ArcMap v. 9.2 and Hazus-MH MR3 (Boling, 2009). This procedure shown below is revised for ArcMap v. 10.5.1 and Hazus-MH 4.2.

The data supplied for this study was in a text file with a grid spacing of 500 meters. The text file contained longitude, latitude, and a parametric value such as the spectral acceleration (S_a) or peak ground acceleration (PGA). The procedure can be broken down into three sections: Importing points into ArcMap, creating a fishnet, joining the points with the fishnet to create a useable map.

Importing Points into ArcMap

- 1. Start Microsoft Excel, navigate to the "Data" tab, and select "from Text/CSV" button.
- When browsing for the file, select "All Files" (see Figure D1). Some text files, such as the one used in this example are 004 files, will not be found when searching for .txt files only.

🗧 🔿 🗠 🕇 📘 > Thi	is PC \rightarrow Local Disk (C:) \rightarrow HazusData	> HazardInput	√ Č	Search HazardInput	م
Organize 👻 New folde	r				
💱 critty Dropbox	Name	Date modified	Туре	Size	
	Isprob	7/19/2019 4:00 PM	00040 File	261 KB	
OneDrive - The Ur	1ssenario.det2	7/19/2019 4:01 PM	DET2 File	335 KB	
ArcGIS	03sprob	7/19/2019 4:00 PM	00040 File	261 KB	
Attachments	03sscenario.det2	7/19/2019 4:01 PM	DET2 File	310 KB	
Curtom Office T		0/16/2010 4.07 084	CDC 51-	1 1/0	
File na	me: 1sprob		~	All Files	~

Figure D1. Importing Data into Microsoft Excel

3. Once the file is selected, another window will come up asking how the data should be displayed and what sheet to use. After selecting appropriate options, the data will look

like Figure D2. Label the top row of data if not already done. The parametric value (spectral acceleration, PGA, PGV, etcetera) **must** be labeled "ParamValue" for Hazus-MH to accept the map. The data does not have to have an ID column, as shown in Figure D2.

1	ID 🔽	LONG 🗾	LAT 📮	ParamValue 🗸
2	1	-89.75	35.875	0.797
3	2	-89.75	35.88	0.803
4	3	-89.75	35.885	0.808

Figure D2. Imported Text Data in Microsoft Excel

- 4. Save a Microsoft Excel file.
- 5. Open ArcMap. Select the "Add Data" button.
- 6. Search for the file created in Step 4 and select it. Select the appropriate sheet to import.
- Right-click on the Layer added in step 2 in the Table of Contents in ArcMap. Select "Display XY Data."
- 8. The Display XY Data window will appear as shown in Figure D3. Ensure the "X Field" is the longitude, the "Y Field" is the Latitude, and the "Z Field" is the parametric value that must be called "ParamValue" in Excel, so that the field will be called "ParamValue" in ArcMap. Select "Edit" underneath the "Coordinate System of Input Coordinates" section. Select the appropriate coordinate system. For this project, all coordinates are in WGS 1984. Select "OK." There may be a warning that there is not an Object ID Field. Select "OK" anyways.

Display XY Data	I.	×
A table containir map as a layer	ng X and Y coordinate data can be added to the	
Choose a table f	from the map or browse for another table:	
ExternalDa	ta_1	<u> </u>
Specify the fie	lds for the X, Y and Z coordinates:	
X Field:	LONG	
Y Field:	LAT	
Z Field:	ParamValue ~	
Coordinate Sy Description:	stem of Input Coordinates	
	Coordinate System: _WGS_1984 ~	
Show Deta	ails <u>E</u> dit	
<u> W</u> arn me if t	ne resulting layer will have restricted functionalit	у
About adding XY	OK Cancel	

Figure D3. Display XY Data Window

9. Now, the XY data is visible, and an Object ID Field is to be assigned. Right-click on the "Event Theme" created in Step 8. Go to "Data" then "Export Data." The Export Data window will appear. Select the options shown in Figure D4. The Output shapefile or feature class location is not important if it can be located and used in a later step. Select "OK."

Export Da	ita ×
Export:	All features
Use the s	ame coordinate system as:
Ithis lay	yer's source data
🔿 the da	ita frame
	ature dataset you export the data into applies if you export to a feature dataset in a geodatabase)
Output fe	ature class:
C:\Users	s\cmmore11\Documents\Thesis\data_HazusArcmap\Earthqu
	OK Cancel

Figure C4. Export Data Window

10. Another window will appear, asking, "Do you want to add the exported data to the map as a layer?" select "Yes." Another layer automatically labeled "Export_Output_#" will show up in the Table of Contents. This shapefile will be the one that is eventually joined with the fishnet created in the next section.

Creating a Fishnet in ArcMap

- 1. Under "Data Management Tools" in ArcMap, find "Create Fishnet." Select it.
- 2. The Create Fishnet window will appear as shown in Figure D5. The location of the output feature class is not important if it may be located for a later step. Under Template Extent, choose the Export_Output_# file created in Step 10 under Importing Points into ArcMap. Then, to the Top and Bottom boxes, extend the point half of the grid spacing up and down, respectively. For instance, the top extent of the point data layer in this example is 36.245. the grid spacing is 500 meters (0.005° grid), and the extents in ArcMap go by the degree (or grid spacing). So, in order to create a map where the points from the point data fall in the middle of the box, half of 0.005 is added to the top extent location and subtracted from the bottom extent location. For example, 36.245 + (1/2)0.005 = 36.2475is the new location of the top extent. Repeat to extend the left extent further left, right extent further right, and bottom extent further down. The origin coordinate boxes will automatically populate when the extents are populated. The cell width and height are the same as the grid spacing. The number of rows is calculated by subtracting the bottom extent from the top extent and dividing it by the grid height (0.005 for this example). The number of columns is calculated in a similar manner using the left and right extents and the cell width. Under geometry type, select polygon. Select "OK."

🔨 Create Fishnet				- 0	×
Output Feature Class					
C:\Users\cmmore11\Documents\Thesis\data_Haz	usArcmap\Earthquake Loo	cation and Magnitude∖	PGADyer_Export_Output.shp	2	
Template Extent (optional)					
				~ 🖻	
	Тор				
		36.247500			
Left			Right		
-89.812500		l		-89.122500	
Γ	Botton	n 35.872500		Clear	
L		55.072500		Clear	
Fishnet Origin Coordinate					
X Coordinate	-89.8125	Y Coordinate		35.8725	
	-09.0125			33.6725	
Y-Axis Coordinate X Coordinate		Y Coordinate			
	-89.8125			45.8725	
Cell Size Width					
				0.005	
Cell Size Height					
				0.005	
Number of Rows					
				75	
Number of Columns					- 1
				138	
Opposite corner of Fishnet (optional)					
X Coordinate		Y Coordinate			
Create Label Points (optional)					
Geometry Type (optional)					
POLYGON				~	
					\sim
		ОК	Cancel Environme	ents << Hide Help	

Figure D5. Create Fishnet Window

3. The result of the previous step is shown in Figure D6. The newly created fishnet is a rectangular grid around the points that were imported. Now, right-click the file created in step 2. Go to data, then click export data. The familiar Export Data window will appear. Choose to export all features and use the same coordinate system as this layer's source data. The output feature class location does not matter. A question will appear asking, "Do you want to add the exported data to the map as a layer?" select "Yes." Export_output_##.shp" has now been created.

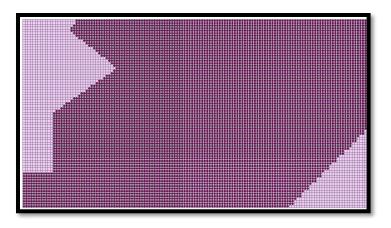


Figure D6. Fishnet Over Point Data

4. Finally, a projection must be added to the fishnet layer. Search for the "Define Projection" tool under Data Management Tools. Select it. Select the file created in step 3. The projection should be the same coordinate system used for the point data. There are now two files created from exporting the point layer and exporting the fishnet layer. Now, the point data and fishnet can be joined together.

Joining the Point Data with the Fishnet to Create a Useable Map

- Right-click on the fishnet layer created in Step 4 of Creating a Fishnet in ArcMap. Go to Joins and Relates and Join...
- 2. The Join Data window will appear as shown in Figure D7. Choose the exported point data layer entitled "Export_output_#." Under section 2, select the option "Each polygon will be given all the attributes of the point that is closest..." as shown in Figure D7. Select "OK." The file created is "Join_output.shp", and it will show up in the Table of Contents.

Join Data	×
Join lets you append additional data to this layer's attribute table so you can, for example, symbolize the layer's features using this data.	
What do you want to join to this layer?	
Join data from another layer based on spatial location	\sim
1. Choose the layer to join to this layer, or load spatial data from disk:	
🚸 Export_Output 💽 🖻	
2. You are joining: Points to Polygons	
Select a join feature class above. You will be given different options based on geometry types of the source feature class and the join feature class.	
Each polygon will be given a summary of the numeric attributes of the points that fall inside it, and a count field showing how many points fall inside it.	
How do you want the attributes to be summarized?	
Average <u>Minimum</u> Standard <u>D</u> eviation	
Sum Maximum Variance	
Each polygon will be given all the attributes of the point that is closest to its boundary, and a distance field showing how close the point is (in the units of the target layer).	
Note: A point falling inside a polygon is treated as being closest to the polygon, (i.e. a distance of 0).	
3. The result of the join will be saved into a new layer.	
Specify output shapefile or feature class for this new layer:	
C:\Users\cmmore11\Documents\Thesis\data_HazusArcmap\	
About joining data OK Cancel	

Figure D7. Join Data Window

3. Search for the "Dissolve" tool under Data Management Tools. This command aggregates polygons that are adjacent and have the same attributes (for this example, the same ground motion data value). The Dissolve window is shown in Figure D8. For this example, the dissolve field is ParamValue, since that is what the user is dissolving with respect to. Select "OK."

≪ Dissolve		-			×
Input Features					
Join_Output			-	6	
Output Feature Class					
C:\Users\cmmore11\Documents\ArcGIS\Default.gdb\Join_Output_Dissolve1				6	
Dissolve_Field(s) (optional)					
□ FID_2					
LAT					
Select All Unselect All		А	dd Field		
Statistics Field(s) (optional)					
				\sim	
Field	Statistic Type			+	
				×	
			_	1	
				Ŧ	
٢			>		
Create multipart features (optional)					
Unsplit lines (optional)					
					1
	OK Cancel Enviro	nments	<< Hide	e Help	
					_

Figure D8. Dissolve Window

- 4. Open ArcCatalog. Find the desired location for a geodatabase. Right-click the location and create a "Personal Geodatabase."
- 5. Find the dissolved file in ArcCatalog (NOT in the Table of Contents pane) created in step 3. Right-click, go to "Export," then "To Geodatabase (single)." The Feature Class to Feature Class window shown in Figure D9 will appear. The "Input Features" is the dissolved file created in step 3. Select the new personal geodatabase created in step 4 as the "Output Location." The "Output Feature Class" is the name of the new useable map being created.

≪ Feature Class to Feature Class	-			×
Input Features				~
C:\Users\cmmore11\Documents\ArcGIS\Default.gdb\Join_Output_03sdyer_Dissolve		-	1	
Output Location				
C:\HazusData\HazardInput\New Personal Geodatabase.mdb			eð	
Output Feature Class				
Join_Output_03sDyer_dissolve				
Expression (optional)				
			SQL	
Field Map (optional)				
PARAMVALUE (Double)			+	
Shape_Length (Double)			-	
⊡-Shape_Area (Double)			×	
			t	
			-	
			Ŧ	
			•	
		_		
ୡ Geodatabase Settings (optional)				
				-
OK Cancel Environments.		<< Hid	e Help	

Figure D9. Feature Class to Feature Class Window

Appendix E: Seismic Hazard Maps Used

This section includes seismic hazard maps used for this study. Each case used PGA, PGV, 0.3s spectral acceleration, and 1.0s spectral acceleration for a 2% in 50-year probability of exceedance. Figures E1-E4 show the maps used in case 1, which are the coarse ground motion maps. Figures E5-E8 show the ground motion maps used for case 2, which are the same maps used in case 1 but only considering structures within Dyer County. Figures E9-E12 show the ground motion maps used in case 3, which are the finer ground motion maps that were solely developed for Dyer County.

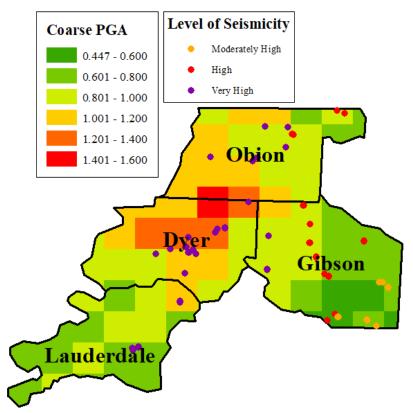


Figure E1. PGA Values (g), Coarse Ground Motion Maps, Entire Study Region

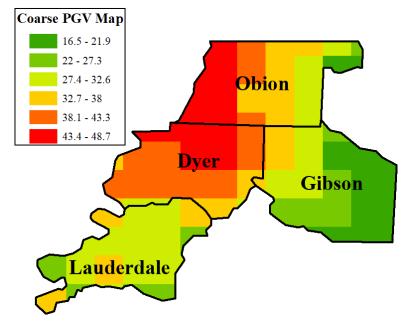


Figure E2. PGV Values (in/s), Coarse Ground Motion Maps, Entire Study Region

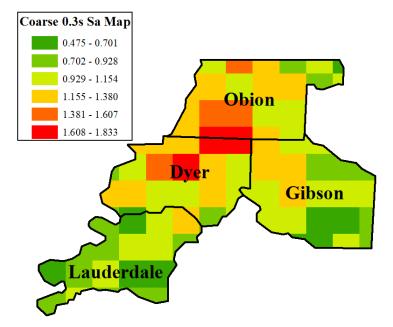


Figure E3. 0.3s Sa Values (g), Coarse Ground Motion Maps, Entire Study Region

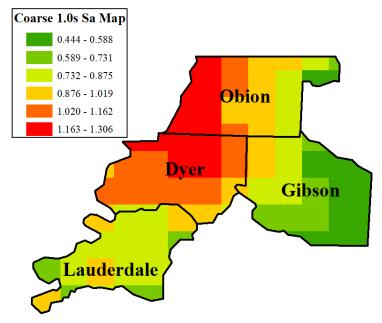


Figure E4. 1.0s Sa Values (g), Coarse Ground Motion Maps, Entire Study Region

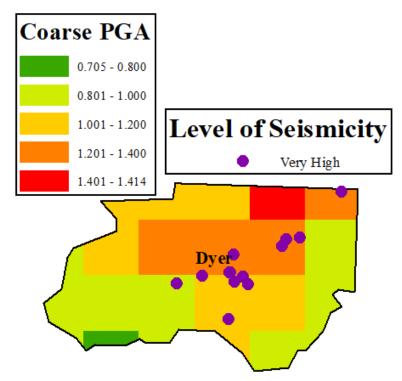


Figure E5. PGA Values (g), Coarse Ground Motion Maps, Dyer County

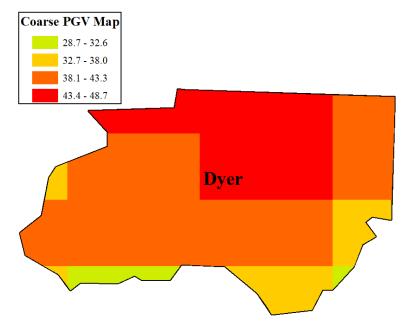


Figure E6. PGV Values (in/s), Coarse Ground Motion Maps, Dyer County

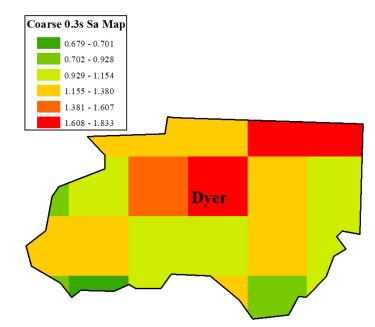


Figure E7. 0.3s Sa Values (g), Coarse Ground Motion Maps, Dyer County

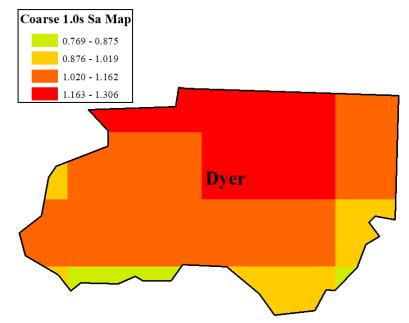


Figure E8. 1.0s Sa Values (g), Coarse Ground Motion Maps, Dyer County

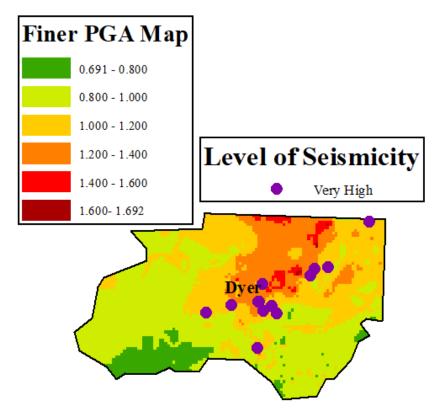


Figure E9. PGA Values (g), Fine Ground Motion Maps, Dyer County

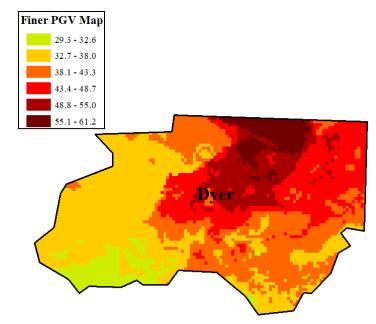


Figure E10. PGV Values (in/s), Fine Ground Motion Maps, Dyer County

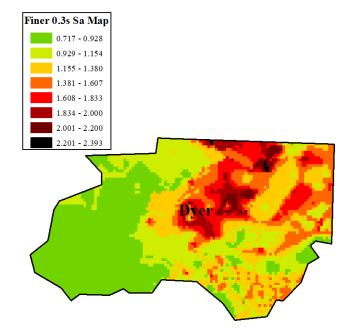


Figure E11. 0.3s Sa Values (g), Fine Ground Motion Maps, Dyer County

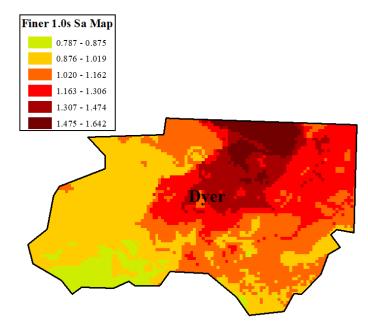


Figure E12. 1.0s Sa Values (g), Fine Ground Motion Maps, Dyer County

Appendix F: Ancillary Data from RVS

Similar data are used in both the development of SL1 and the Hazus-MH 4.2 output. Table F1 includes the two primary identifiers of each structure: the Hazus ID and the Structure Number. Table F1 also includes the location and other recorded aspects of each structure that are used in calculating a score for the building in RVS and for calculating damage losses in Hazus-MH 4.2.

Since this project is funded by the West Tennessee Seismic Safety Commission, in addition to the data collected to determine a score or damage state for each structure, additional information was also documented: the kitchen square footage and gymnasium square footage. Table F1 gives these ancillary data for each structure identified, and Table F2 gives these data for each school analyzed. It should be noted that some of the structures below are additions that, when added together, comprise one building. A result of that is that some buildings below have a "0" for the kitchen area or gym area. A "0" means that there is not a kitchen in that area of the building or no gym in that area of the building.

Hazus ID	Struc. No.	Latitude	Longitude	Design Level	Hazus Building	Day Occ.	Night Occ.	Total Area	Kitchen Area	Gym Area	RVS Score
					Туре			(sf)	(sf)	(sf)	
TN002548	1	35.969973	-88.940351	MC	RM1L	77	2	12250	-	-	0.7
TN002549	2	35.969550	-88.940584	MC	RM1L	314	8	49797	-	-	0.3
TN002550	3	35.969889	-88.941194	MC	RM1L	67	2	10700	-	-	3.1
TN002551	4	35.970259	-88.940874	MC	RM1L	81	3	12800	-	-	3.8
TN002552	5	35.963381	-88.926478	MC	S5L	413	21	81905	-	-	0.6
TN002553	6	35.961408	-88.927692	MC	S5L	424	22	84104	-	-	0.5
TN002554	7	35.971109	-89.388834	MC	RM1L	214	6	41782	1,250	2,400	0.3
TN002555	8	36.034741	-89.481789	PC	S5L	302	8	51170	375	4,800	0.5

Table F1. Ancillary Building Data

Hazus ID	Struc. No.	Latitude	Longitude	Design Level	Hazus Building Type	Day Occ.	Night Occ.	Total Area (sf)	Kitchen Area (sf)	Gym Area (sf)	RVS Score
TN002556	9	36.049700	-89.434919	MC	RM1L	498	25	119080	2,800	6,400	1.9
TN002557	10	36.087096	-89.379055	MC	RM1L	565	15	71175	1,600	3,200	2.3
TN002558	11	36.103397	-89.292079	MC	S5L	1273	64	194800	4,800	14,400	0.5
TN002559	12	36.114491	-89.284392	MC	C3L	469	24	99614	600	3,000	0.3
TN002560	13	36.200490	-89.184100	MC	S5L	154	4	27969	875	2,000	0.5
TN002561	14	36.117453	-89.259485	MC	RM1L	361	10	40000	0	0	2.3
TN002562	15	36.11721	-89.260402	MC	S5L	143	4	15800	1750	0	0.8
TN002563	16	36.117892	-89.25993	MC	S5L	113	3	12530	0	4,000	1.1
TN002564	17	36.074899	-88.813244	MC	URML	83	3	13420	0	0	0.6
TN002565	18	36.075303	-88.813324	MC	S5L	48	2	7800	600	0	1
TN002566	19	36.074980	-88.813344	MC	S5L	48	2	7800	0	0	1.5
TN002567	20	36.075038	-88.813780	MC	RM2L	84	3	13600	0	0	3.8
TN002568	21	36.075200	-88.813335	MC	S3L	27	1	4500	0	4,500	1.8
TN002569	22	36.075435	-88.813311	MC	RM1L	176	9	27200	0	6,400	1.2
TN002570	23	36.075907	-88.814487	MC	RM1L	64	4	9775	0	0	1.2
TN002571	24	36.076203	-88.814458	MC	S3L	28	2	4200	0	0	3.7
TN002572	25	36.415586	-89.039859	MC	RM1L	865	22	101000	800	4,800	3.1
TN002573	26	36.418647	-89.044852	MC	RM1L	385	10	53800	700	4,200	0.5
TN002574	27	36.417909	-89.043467	MC	C3L	486	25	107000	1,584	-	0.3
TN002575	28	35.824070	-88.804151	MC	PC1L	1229	62	105850	1,500	4,500	2.5
TN002576	29	35.803856	-88.775062	MC	PC1L	566	15	113350	1,350	10,000	3.2
TN002577	30	35.820230	-88.803833	MC	PC1L	805	41	160800	2,000	8,000	1.5
TN002578	31	35.983928	-89.124160	PC	RM1L	70	2	17225	800	3,600	0.5
TN002579	32	35.984219	-89.123791	MC	RM1L	59	2	14400	0	0	2.7
TN002580	33	36.092742	-89.119842	PC	S5L	137	4	32550	400	-	0.4
TN002581	34	36.129099	-88.986899	PC	RM1L	116	3	21400	0	0	0.5
TN002582	35	36.128848	-88.987620	MC	RM1L	78	2	14400	400	0	1.2
TN002583	36	36.12915	-88.987566	MC	S5L			1500	0	0	1.7
TN002584	37	36.129346	-88.987883	MC	S5L	70	2	12800	0	7,200	1.2

Hazus ID	Struc. No.	Latitude	Longitude	Design Level	Hazus Building Type	Day Occ.	Night Occ.	Total Area (sf)	Kitchen Area (sf)	Gym Area (sf)	RVS Score
TN002585	38	36.069692	-88.988583	PC	URML	128	4	22850	0	5,000	0.2
TN002586	39	36.069408	-88.988728	MC	RM1L	154	4	27300	0	0	3.1
TN002587	40	36.068942	-88.988267	MC	URML	134	4	23900	832	0	0.2
TN002588	41	36.068762	-88.988134	MC	RM1L	17	1	3000	0	0	3.8
TN002589	42	36.024991	-88.966588	MC	C3L	275	14	86500	4,914	17,400	0.3
TN002590	43	36.025544	-88.966840	MC	C3L	11	1	3536	0	0	1.2
TN002591	44	36.024101	-88.966583	MC	C3L	90	5	28300	0	0	0.3
TN002592	45	36.023394	-88.966441	MC	C3L	145	8	45600	0	0	0.3
TN002593	46	36.189252	-89.008097	MC	RM1L	56	2	17700	800	0	3.1
TN002594	47	36.189552	-89.008474	MC	RM1L	15	1	4875	0	0	3.8
TN002595	48	36.189498	-89.007514	MC	S3L	13	1	4000	0	4,000	3.7
TN002596	49	36.038613	-89.376964	MC	RM1L	132	4	21700	0	0	2.3
TN002597	50	36.038177	-89.377060	MC	RM1L	378	10	62125	1,250	4,900	0.5
TN002598	51	36.037744	-89.376773	MC	RM1L	136	4	22400	0	0	2.7
TN002599	52	36.033128	-89.353330	MC	RM1L	626	32	180000	3,840	14,400	1.9
TN002600	53	36.046834	-89.361546	MC	RM1L	668	17	74800	2,888	5,400	1.9
TN002601	54	36.055558	-89.384794	MC	C3L	719	36	225000	2,800	13,000	0.3
TN002602	55	36.055205	-89.385937	MC	RM1L	64	4	20000	0	0	0.9
TN002603	56	35.724526	-89.556411	MC	RM1L	647	17	98374	2,640	7,200	0.3
TN002604	57	35.731775	-89.557356	MC	RM1L	675	17	108948	3,264	7,140	2.3
TN002605	58	35.735006	-89.538585	MC	RM1L	352	18	79400	2,688	0	0.3
TN002606	59	35.734807	-89.537884	MC	PC2L	162	9	36400	0	0	2.3
TN002607	60	35.735626	-89.537495	MC	RM1L	58	3	13000	0	0	2.7
TN002608	61	35.736034	-89.537530	MC	RM1L	151	8	34000	0	0	0.5
TN002609	62	35.736074	-89.538663	MC	PC2L	177	9	39975	0	25,600	2.3
TN002610	63	35.728695	-89.555585	MC	RM1L	677	34	106426	2288	7,000	0.3
TN002611	64	35.882508	-89.404275	MC	RM1L	494	13	61949	1,300	0	0.3
TN002612	65	35.882721	-89.405093	MC	RM1L	216	6	27125	0	4,116	1.9
TN002613	66	35.879895	-89.403827	MC	RM1L	197	10	39900	0	8,640	0.30

Hazus ID	Struc. No.	Latitude	Longitude	Design Level	Hazus Building Type	Day Occ.	Night Occ.	Total Area (sf)	Kitchen Area (sf)	Gym Area (sf)	RVS Score
TN002614	67	35.879962	-89.404695	MC	RM1L	425	22	46598	2,880	0	0.5
TN002615	68	35.879373	-89.405175	MC	RM1L	358	18	39247	0	13,200	1.9
TN002616	69	35.880824	-89.404591	MC	RM1L	117	6	12915	0	0	0.5
TN002617	70	36.343188	-89.155814	MC	S5L	932	47	188000	5,600	11,200	0.5
TN002618	71	36.441321	-89.058616	MC	S5L	260	13	37638	0	0	0.5
TN002619	72	36.376722	-89.065628	MC	RM1L	373	10	57081	1,200	9,000	0.3
TN002620	73	36.494358	-88.899980	MC	S5L	399	20	112000	1,500	22,000	0.6
TN002621	74	36.485660	-88.876498	MC	RM1L	335	9	56000	1,200	8,000	0.3
TN002622	75	36.442604	-89.130471	MC	RM1L	573	15	72000	2,600	12,960	0.3
TN002623	76	36.344829	-89.307989	MC	RM1L	298	8	56000	1,500	8,000	0.3
TN002624	77	36.331675	-89.171331	MC	RM1L	573	15	70847	2,600	9,000	0.3
TN002625	78	35.840583	-88.906732	MC	C3L	1213	61	76100	1,944	16,800	0.3
TN002626	79	35.831765	-88.897299	MC	RM1L	133	4	20300	0	0	1.3
TN002627	80	35.831838	-88.896639	MC	RM1L	369	10	56200	1,800	9,775	0.6
TN002628	81	35.821615	-88.932404	MC	RM1L	248	7	54875	2,600	11,250	0.3
TN002629	82	35.941951	-88.764254	MC	RM1L	748	19	108500	3,200	8,292	0.3
TN002630	83	35.942686	-88.753493	MC	RM1L	655	33	92375	2,200	10,000	0.3
TN002631	84	35.926588	-88.736201	MC	RM1L	641	33	84800	1,440	18,225	0.3
TN002631	85	35.925469	-88.737142	MC	C3L	60	3	8000	0	0	1.4

Table F2. Ancillary School Data

School Number	Kitchen Area (sf)	Gym Area (sf)	Score of Building with Most Facilities
1	-	-	3.8
2	-	-	0.6
3	-	-	0.5
4	1250	2400	0.3

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	5	375	4800	0.5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		2800	6400	1.9
9 600 3000 0.3 10 875 2000 0.5 11 1750 4000 1.1 12 600 4500 1.8 130 16175 1.2 14 800 4800 3.1 15 700 4200 0.5 16 1584 1 0.3 17 1500 4500 2.5 18 1350 10000 3.2 19 2000 8000 1.5 20 800 3600 0.5 21 400 1 0.4 22 400 7200 1.2 23 832 5000 0.2 24 4914 17400 0.3 25 800 4000 3.7 26 1250 4900 0.5 27 3840 14400 1.9 29 2800 13000 0.3 30 2640 7200 0.3 31 3264 7140 2.3 32 2688 25600 2.3 33 2288 7000 0.3 34 1300 4116 1.9 35 $ 8640$ 0.30	7	1600	3200	2.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8	4800	14400	0.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9	600	3000	0.3
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	10	875	2000	0.5
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	11	1750	4000	1.1
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	12	600	4500	1.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	13	0	16175	1.2
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	14	800	4800	3.1
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	15	700	4200	0.5
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	16	1584	1	0.3
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	17	1500	4500	2.5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	18	1350	10000	3.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	19	2000	8000	1.5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	20	800	3600	0.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	21	400	1	0.4
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	22	400	7200	1.2
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	23	832	5000	0.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	24	4914	17400	0.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	25	800	4000	3.7
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	26	1250	4900	0.5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	27	3840	14400	1.9
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	28	2888	5400	1.9
31 3264 7140 2.3 32 2688 25600 2.3 33 2288 7000 0.3 34 1300 4116 1.9 35 - 8640 0.30	29	2800	13000	0.3
32 2688 25600 2.3 33 2288 7000 0.3 34 1300 4116 1.9 35 - 8640 0.30	30	2640	7200	0.3
33 2288 7000 0.3 34 1300 4116 1.9 35 - 8640 0.30	31	3264	7140	2.3
34 1300 4116 1.9 35 - 8640 0.30	32	2688	25600	2.3
35 - 8640 0.30	33	2288	7000	0.3
	34	1300	4116	1.9
36 2880 13200 1.9	35	-	8640	0.30
	36	2880	13200	1.9

			1
37	5600	11200	0.5
38	0	0	0.5
39	1200	9000	0.3
40	1500	22000	0.6
41	1200	8000	0.3
42	2600	12960	0.3
43	1500	8000	0.3
44	2600	9000	0.3
45	1944	16800	0.3
46	1800	9775	0.6
47	2600	11250	0.3
48	3200	8292	0.3
49	2200	10000	0.3
50	1440	18225	0.3

Appendix G. Hazus-MH 4.2 Results: Damage State Probabilities

This appendix contains the damage state probabilities of each structure under each case. The damage state probabilities are used to calculated *BRC*, *IO*, and *MD*.

Table G1. Damage State Probabilities: Case 1									
Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)			
	STR	0.012	0.084	0.527	0.359	0.018			
1	NSA	0.068	0.299	0.426	0.183	0.024			
	NSD	0.022	0.148	0.585	0.207	0.038			
	STR	0.012	0.084	0.527	0.359	0.018			
2	NSA	0.068	0.299	0.426	0.183	0.024			
	NSD	0.022	0.148	0.585	0.207	0.038			
	STR	0.012	0.084	0.527	0.359	0.018			
3	NSA	0.068	0.299	0.426	0.183	0.024			
	NSD	0.022	0.148	0.585	0.207	0.038			
	STR	0.012	0.084	0.527	0.359	0.018			
4	NSA	0.068	0.299	0.426	0.183	0.024			
	NSD	0.022	0.148	0.585	0.207	0.038			
	STR	0.000	0.001	0.039	0.320	0.640			
5	NSA	0.032	0.121	0.150	0.212	0.485			
	NSD	0.000	0.004	0.119	0.236	0.640			
	STR	0.000	0.001	0.039	0.320	0.640			
6	NSA	0.032	0.121	0.150	0.212	0.485			
	NSD	0.000	0.004	0.119	0.236	0.640			
	STR	0.000	0.000	0.043	0.426	0.531			
7	NSA	0.014	0.099	0.215	0.259	0.413			
	NSD	0.000	0.002	0.129	0.312	0.556			
	STR	0.000	0.000	0.000	0.001	0.999			
8	NSA	0.000	0.000	0.000	0.240	0.759			
	NSD	0.000	0.000	0.000	0.001	0.999			
	STR	0.000	0.000	0.043	0.426	0.531			
9	NSA	0.014	0.099	0.215	0.259	0.413			
	NSD	0.000	0.002	0.129	0.312	0.556			
	STR	0.000	0.000	0.041	0.416	0.542			
10	NSA	0.007	0.070	0.203	0.288	0.432			
	NSD	0.000	0.002	0.124	0.307	0.566			
	STR	0.000	0.000	0.000	0.003	0.997			
11	NSA	0.000	0.000	0.001	0.229	0.769			
	NSD	0.000	0.000	0.000	0.003	0.997			
12	STR	0.000	0.000	0.000	0.001	0.998			

Table G1. Damage State Probabilities: Case 1

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
12	NSA	0.000	0.000	0.001	0.228	0.771
	NSD	0.000	0.000	0.000	0.001	0.998
	STR	0.000	0.000	0.000	0.007	0.993
13	NSA	0.000	0.001	0.003	0.224	0.772
	NSD	0.000	0.000	0.000	0.007	0.993
	STR	0.000	0.000	0.024	0.332	0.644
14	NSA	0.007	0.062	0.161	0.266	0.504
	NSD	0.000	0.001	0.086	0.258	0.655
	STR	0.000	0.000	0.000	0.003	0.997
15	NSA	0.000	0.000	0.001	0.229	0.769
	NSD	0.000	0.000	0.000	0.003	0.997
	STR	0.000	0.000	0.000	0.003	0.997
16	NSA	0.000	0.000	0.001	0.229	0.769
	NSD	0.000	0.000	0.000	0.003	0.997
	STR	0.001	0.023	0.280	0.485	0.211
17	NSA	0.047	0.228	0.350	0.208	0.166
	NSD	0.007	0.069	0.444	0.268	0.211
	STR	0.001	0.011	0.186	0.517	0.285
18	NSA	0.082	0.264	0.279	0.157	0.217
	NSD	0.004	0.034	0.380	0.296	0.285
	STR	0.001	0.011	0.186	0.517	0.285
19	NSA	0.082	0.264	0.279	0.157	0.217
	NSD	0.004	0.034	0.380	0.296	0.285
	STR	0.024	0.138	0.586	0.245	0.006
20	NSA	0.088	0.333	0.409	0.152	0.017
	NSD	0.040	0.216	0.585	0.141	0.017
	STR	0.002	0.029	0.404	0.516	0.048
21	NSA	0.114	0.357	0.367	0.123	0.039
	NSD	0.005	0.069	0.542	0.302	0.082
	STR	0.048	0.189	0.575	0.185	0.003
22	NSA	0.091	0.338	0.406	0.148	0.017
	NSD	0.069	0.265	0.551	0.105	0.010
	STR	0.048	0.189	0.575	0.185	0.003
23	NSA	0.091	0.338	0.406	0.148	0.017
	NSD	0.069	0.265	0.551	0.105	0.010
	STR	0.002	0.029	0.404	0.516	0.048
24	NSA	0.114	0.357	0.367	0.123	0.039
	NSD	0.005	0.069	0.542	0.302	0.082
	STR	0.000	0.006	0.189	0.604	0.200
25	NSA	0.028	0.180	0.366	0.262	0.163
	NSD	0.001	0.020	0.340	0.386	0.253
26	STR	0.000	0.006	0.189	0.604	0.200
_0	NSA	0.028	0.180	0.366	0.262	0.163

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
26	NSD	0.001	0.020	0.340	0.386	0.253
	STR	0.000	0.000	0.002	0.043	0.954
27	NSA	0.002	0.010	0.021	0.239	0.728
	NSD	0.000	0.000	0.005	0.040	0.954
	STR	0.004	0.047	0.477	0.429	0.043
28	NSA	0.065	0.291	0.419	0.187	0.038
	NSD	0.010	0.101	0.579	0.242	0.069
	STR	0.004	0.047	0.477	0.429	0.043
29	NSA	0.065	0.291	0.419	0.187	0.038
	NSD	0.010	0.101	0.579	0.242	0.069
	STR	0.004	0.047	0.477	0.429	0.043
30	NSA	0.065	0.291	0.419	0.187	0.038
	NSD	0.010	0.101	0.579	0.242	0.069
	STR	0.000	0.000	0.002	0.041	0.957
31	NSA	0.002	0.010	0.020	0.239	0.730
	NSD	0.000	0.000	0.006	0.037	0.957
	STR	0.000	0.009	0.232	0.602	0.157
32	NSA	0.034	0.204	0.385	0.248	0.129
	NSD	0.002	0.028	0.384	0.378	0.209
	STR	0.000	0.000	0.000	0.005	0.995
33	NSA	0.000	0.001	0.003	0.238	0.758
	NSD	0.000	0.000	0.000	0.005	0.995
	STR	0.000	0.000	0.002	0.051	0.947
34	NSA	0.002	0.013	0.024	0.239	0.722
	NSD	0.000	0.000	0.008	0.045	0.947
	STR	0.001	0.011	0.260	0.595	0.133
35	NSA	0.036	0.212	0.396	0.246	0.111
	NSD	0.002	0.034	0.412	0.369	0.183
	STR	0.000	0.000	0.004	0.101	0.894
36	NSA	0.005	0.028	0.048	0.239	0.680
	NSD	0.000	0.000	0.019	0.087	0.894
	STR	0.000	0.000	0.004	0.101	0.894
37	NSA	0.005	0.028	0.048	0.239	0.680
	NSD	0.000	0.000	0.019	0.087	0.894
	STR	0.000	0.000	0.003	0.060	0.937
38	NSA	0.002	0.012	0.029	0.238	0.719
	NSD	0.000	0.000	0.015	0.047	0.937
	STR	0.001	0.011	0.260	0.595	0.133
39	NSA	0.036	0.212	0.396	0.246	0.133
	NSD	0.002	0.034	0.412	0.369	0.111
	STR	0.002	0.000	0.017	0.191	0.792
40	NSA	0.005	0.000	0.095	0.248	0.611
10	NSD	0.000	0.041	0.055	0.146	0.792

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
	STR	0.001	0.011	0.260	0.595	0.133
41	NSA	0.036	0.212	0.396	0.246	0.111
	NSD	0.002	0.034	0.412	0.369	0.183
	STR	0.000	0.000	0.008	0.104	0.887
42	NSA	0.005	0.027	0.051	0.240	0.677
	NSD	0.000	0.000	0.020	0.093	0.887
	STR	0.000	0.000	0.008	0.104	0.887
43	NSA	0.005	0.027	0.051	0.240	0.677
	NSD	0.000	0.000	0.020	0.093	0.887
	STR	0.000	0.000	0.008	0.104	0.887
44	NSA	0.005	0.027	0.051	0.240	0.677
	NSD	0.000	0.000	0.020	0.093	0.887
	STR	0.000	0.000	0.008	0.104	0.887
45	NSA	0.005	0.027	0.051	0.240	0.677
	NSD	0.000	0.000	0.020	0.093	0.887
	STR	0.001	0.013	0.276	0.589	0.121
46	NSA	0.040	0.226	0.399	0.234	0.101
	NSD	0.002	0.038	0.427	0.363	0.170
	STR	0.001	0.013	0.276	0.589	0.121
47	NSA	0.040	0.226	0.399	0.234	0.101
	NSD	0.002	0.038	0.427	0.363	0.170
	STR	0.000	0.000	0.044	0.470	0.485
48	NSA	0.033	0.153	0.227	0.217	0.371
	NSD	0.000	0.002	0.137	0.343	0.518
	STR	0.000	0.000	0.043	0.426	0.531
49	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
50	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
51	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
52	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.530
53	NSA	0.000	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.002	0.000	0.003	0.996
54	NSA	0.000	0.000	0.000	0.223	0.775
υт	NSD	0.000	0.000	0.002	0.003	0.996
55	STR	0.000	0.000	0.000	0.003	0.542

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
55	NSA	0.007	0.070	0.203	0.288	0.432
	NSD	0.000	0.002	0.124	0.307	0.566
	STR	0.364	0.351	0.268	0.017	0.000
56	NSA	0.108	0.359	0.391	0.129	0.013
	NSD	0.379	0.383	0.228	0.010	0.000
	STR	0.364	0.351	0.268	0.017	0.000
57	NSA	0.108	0.359	0.391	0.129	0.013
	NSD	0.379	0.383	0.228	0.010	0.000
	STR	0.341	0.353	0.286	0.019	0.000
58	NSA	0.106	0.357	0.393	0.131	0.013
	NSD	0.358	0.387	0.243	0.012	0.000
	STR	0.026	0.135	0.572	0.261	0.006
59	NSA	0.109	0.360	0.390	0.128	0.013
	NSD	0.041	0.210	0.588	0.147	0.015
	STR	0.341	0.353	0.286	0.019	0.000
60	NSA	0.106	0.357	0.393	0.131	0.013
	NSD	0.358	0.387	0.243	0.012	0.000
	STR	0.341	0.353	0.286	0.019	0.000
61	NSA	0.106	0.357	0.393	0.131	0.013
	NSD	0.358	0.387	0.243	0.012	0.000
	STR	0.026	0.135	0.572	0.261	0.006
62	NSA	0.109	0.360	0.390	0.128	0.013
	NSD	0.041	0.210	0.588	0.147	0.015
	STR	0.364	0.351	0.268	0.017	0.000
63	NSA	0.108	0.359	0.391	0.129	0.013
	NSD	0.379	0.383	0.228	0.010	0.000
	STR	0.000	0.005	0.173	0.602	0.221
64	NSA	0.024	0.167	0.357	0.272	0.180
	NSD	0.001	0.017	0.320	0.388	0.274
	STR	0.000	0.005	0.173	0.602	0.221
65	NSA	0.024	0.167	0.357	0.272	0.180
	NSD	0.001	0.017	0.320	0.388	0.274
	STR	0.000	0.005	0.173	0.602	0.221
66	NSA	0.024	0.167	0.357	0.272	0.180
00	NSD	0.001	0.017	0.320	0.388	0.274
	STR	0.000	0.005	0.173	0.602	0.221
67	NSA	0.000	0.167	0.357	0.002	0.180
57	NSD	0.001	0.017	0.320	0.388	0.274
	STR	0.000	0.005	0.173	0.602	0.221
68	NSA	0.000	0.167	0.357	0.002	0.180
00	NSD	0.024	0.017	0.320	0.388	0.130
69	STR	0.001	0.007	0.320	0.588	0.274
07	NSA	0.000	0.003	0.173	0.002	0.221

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
69	NSD	0.001	0.017	0.320	0.388	0.274
	STR	0.000	0.000	0.000	0.020	0.980
70	NSA	0.000	0.004	0.009	0.233	0.754
	NSD	0.000	0.000	0.002	0.018	0.980
	STR	0.000	0.000	0.001	0.045	0.953
71	NSA	0.002	0.011	0.021	0.239	0.727
	NSD	0.000	0.000	0.006	0.041	0.953
	STR	0.000	0.004	0.157	0.597	0.242
72	NSA	0.027	0.172	0.347	0.260	0.195
	NSD	0.001	0.015	0.302	0.388	0.295
	STR	0.000	0.000	0.007	0.135	0.858
73	NSA	0.009	0.042	0.063	0.236	0.650
	NSD	0.000	0.000	0.029	0.113	0.858
	STR	0.001	0.017	0.307	0.574	0.101
74	NSA	0.046	0.243	0.405	0.221	0.085
	NSD	0.003	0.045	0.453	0.351	0.148
	STR	0.000	0.004	0.157	0.597	0.242
75	NSA	0.027	0.172	0.347	0.260	0.195
	NSD	0.001	0.015	0.302	0.388	0.295
	STR	0.000	0.000	0.019	0.298	0.683
76	NSA	0.007	0.057	0.144	0.260	0.532
	NSD	0.000	0.001	0.073	0.238	0.689
	STR	0.000	0.001	0.092	0.540	0.367
77	NSA	0.015	0.117	0.288	0.287	0.294
	NSD	0.000	0.007	0.213	0.369	0.411
	STR	0.000	0.005	0.130	0.461	0.403
78	NSA	0.085	0.235	0.216	0.159	0.305
	NSD	0.002	0.019	0.272	0.304	0.403
	STR	0.330	0.354	0.295	0.021	0.000
79	NSA	0.146	0.394	0.356	0.097	0.008
	NSD	0.348	0.389	0.251	0.012	0.000
	STR	0.330	0.354	0.295	0.021	0.000
80	NSA	0.146	0.394	0.356	0.097	0.008
	NSD	0.348	0.389	0.251	0.012	0.000
	STR	0.330	0.354	0.295	0.021	0.000
81	NSA	0.146	0.394	0.356	0.097	0.008
-	NSD	0.348	0.389	0.251	0.012	0.000
	STR	0.406	0.344	0.237	0.012	0.000
82	NSA	0.155	0.401	0.346	0.090	0.007
-	NSD	0.417	0.374	0.201	0.008	0.000
	STR	0.406	0.344	0.237	0.013	0.000
83	NSA	0.155	0.401	0.346	0.090	0.007
	NSD	0.417	0.374	0.201	0.008	0.000

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
	STR	0.111	0.278	0.514	0.095	0.001
84	NSA	0.104	0.354	0.395	0.133	0.014
	NSD	0.139	0.344	0.459	0.054	0.003
	STR	0.000	0.002	0.078	0.382	0.538
85	NSA	0.052	0.170	0.182	0.190	0.406
	NSD	0.001	0.009	0.176	0.277	0.538

Table G2. Damage State Probabilities: Case 2

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
	STR	0.000	0.000	0.043	0.426	0.531
7	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.000	0.001	0.999
8	NSA	0.000	0.000	0.000	0.240	0.759
	NSD	0.000	0.000	0.000	0.001	0.999
	STR	0.000	0.000	0.043	0.426	0.531
9	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.041	0.416	0.542
10	NSA	0.007	0.070	0.203	0.288	0.432
	NSD	0.000	0.002	0.124	0.307	0.566
	STR	0.000	0.000	0.000	0.003	0.997
11	NSA	0.000	0.000	0.001	0.229	0.769
	NSD	0.000	0.000	0.000	0.003	0.997
	STR	0.000	0.000	0.000	0.001	0.998
12	NSA	0.000	0.000	0.001	0.228	0.771
	NSD	0.000	0.000	0.000	0.001	0.998
	STR	0.000	0.000	0.000	0.007	0.993
13	NSA	0.000	0.001	0.003	0.224	0.772
	NSD	0.000	0.000	0.000	0.007	0.993
	STR	0.000	0.000	0.024	0.332	0.644
14	NSA	0.007	0.062	0.161	0.266	0.504
	NSD	0.000	0.001	0.086	0.258	0.655
	STR	0.000	0.000	0.000	0.003	0.997
15	NSA	0.000	0.000	0.001	0.229	0.769
	NSD	0.000	0.000	0.000	0.003	0.997
	STR	0.000	0.000	0.000	0.003	0.997
16	NSA	0.000	0.000	0.001	0.229	0.769
	NSD	0.000	0.000	0.000	0.003	0.997
49	STR	0.000	0.000	0.043	0.426	0.531
	NSA	0.014	0.099	0.215	0.259	0.413

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
49	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
50	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
51	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
52	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.043	0.426	0.531
53	NSA	0.014	0.099	0.215	0.259	0.413
	NSD	0.000	0.002	0.129	0.312	0.556
	STR	0.000	0.000	0.000	0.003	0.996
54	NSA	0.000	0.000	0.002	0.223	0.775
	NSD	0.000	0.000	0.000	0.003	0.996
	STR	0.000	0.000	0.041	0.416	0.542
55	NSA	0.007	0.070	0.203	0.288	0.432
	NSD	0.000	0.002	0.124	0.307	0.566

Table G3. Damage State Probabilities: Case 3

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
	STR	0	0.001	0.048	0.441	0.511
7	NSA	0.015	0.104	0.224	0.259	0.398
	NSD	0	0.003	0.138	0.32	0.539
	STR	0	0	0	0	1
8	NSA	0	0	0	0.234	0.766
	NSD	0	0	0	0	1
	STR	0	0	0.021	0.313	0.666
9	NSA	0.008	0.061	0.151	0.262	0.519
	NSD	0	0.001	0.078	0.247	0.674
	STR	0	0	0.013	0.255	0.732
10	NSA	0.005	0.046	0.121	0.258	0.57
	NSD	0	0.001	0.058	0.21	0.732
	STR	0	0	0	0.004	0.996
11	NSA	0	0.001	0.002	0.235	0.762
	NSD	0	0	0	0.004	0.996
	STR	0	0	0	0.001	0.998
12	NSA	0	0	0.001	0.233	0.766
	NSD	0	0	0	0.001	0.998
13	STR	0	0	0	0.003	0.997

Structure No.	Component	P(N)	P(S)	P(M)	P(E)	P(C)
	NSA	0	0.001	0.001	0.234	0.764
	NSD	0	0	0	0.003	0.997
	STR	0	0	0.025	0.339	0.635
14	NSA	0.011	0.076	0.167	0.255	0.492
	NSD	0	0.001	0.089	0.263	0.647
	STR	0	0	0	0.003	0.997
15	NSA	0	0.001	0.001	0.236	0.762
	NSD	0	0	0	0.003	0.997
	STR	0	0	0	0.003	0.997
16	NSA	0	0.001	0.001	0.236	0.762
	NSD	0	0	0	0.003	0.997
49	STR	0	0	0.024	0.332	0.644
	NSA	0.008	0.064	0.161	0.264	0.503
49	NSD	0	0.001	0.086	0.258	0.655
	STR	0	0	0.024	0.332	0.644
50	NSA	0.008	0.064	0.161	0.264	0.503
	NSD	0	0.001	0.086	0.258	0.655
	STR	0	0	0.024	0.332	0.644
51	NSA	0.008	0.064	0.161	0.264	0.503
	NSD	0	0.001	0.086	0.258	0.655
	STR	0	0.001	0.049	0.446	0.504
52	NSA	0.018	0.113	0.227	0.251	0.391
	NSD	0	0.003	0.141	0.323	0.533
	STR	0	0	0.035	0.391	0.574
53	NSA	0.011	0.083	0.194	0.264	0.448
	NSD	0	0.002	0.111	0.293	0.594
	STR	0	0	0	0.001	0.999
54	NSA	0	0	0	0.222	0.778
	NSD	0	0	0	0.001	0.999
	STR	0	0	0.015	0.267	0.718
55	NSA	0.005	0.043	0.125	0.264	0.564
	NSD	0	0.001	0.062	0.218	0.719

			1: Predict	Day Ca		
Hazus ID	Struc.	Day		Day Ca	suarries	
	No.	Occ.	Level 1	Level 2	Level 3	Level 4
TN002548	1	77	0.49	0.09	0.01	0.02
TN002549	2	314	2.01	0.35	0.04	0.07
TN002550	3	67	0.43	0.07	0.01	0.02
TN002551	4	81	0.52	0.09	0.01	0.02
TN002552	5	413	21.98	6.8	1.08	2.14
TN002553	6	424	22.56	6.98	1.11	2.2
TN002554	7	214	11.77	4.03	0.75	1.49
TN002555	8	302	23.54	7.6	1.23	2.44
TN002556	9	498	27.4	9.39	1.74	3.46
TN002557	10	565	31.66	10.87	2.02	4.01
TN002558	11	1273	99.05	31.99	5.19	10.27
TN002559	12	469	48	18.03	3.55	7.06
TN002560	13	154	11.94	3.85	0.63	1.24
TN002561	14	361	23.42	8.19	1.53	3.04
TN002562	15	143	11.13	3.59	0.58	1.15
TN002563	16	113	8.79	2.84	0.46	0.91
TN002564	17	83	3.43	0.91	0.14	0.27
TN002565	18	48	1.33	0.37	0.06	0.11
TN002566	19	48	1.33	0.37	0.06	0.11
TN002567	20	84	0.36	0.05	0	0.01
TN002568	21	27	0.24	0.04	0	0
TN002569	22	176	0.6	0.08	0	0.01
TN002570	23	64	0.22	0.03	0	0
TN002571	24	28	0.25	0.04	0	0
TN002572	25	865	22.09	6.57	1.15	2.27
TN002573	26	385	9.83	2.92	0.51	1.01
TN002574	27	486	47.75	17.88	3.52	7
TN002575	28	1229	12.13	2.71	0.24	0.4
TN002576	29	566	5.58	1.25	0.11	0.18
TN002577	30	805	7.94	1.78	0.16	0.26
TN002578	31	70	6.43	2.33	0.44	0.88
TN002579	32	59	1.27	0.36	0.06	0.12
TN002580	33	137	10.63	3.43	0.56	1.1
TN002581	34	116	10.55	3.82	0.72	1.44
TN002582	35	78	1.5	0.41	0.07	0.14
TN002583	36		0.57	0.18	0.03	0.06
TN002584	37	70	4.95	1.58	0.26	0.51
TN002585	38	128	17.54	5.65	0.92	1.82
TN002586	39	154	2.95	0.81	0.14	0.27

Appendix H. Hazus-MH 4.2 Results: Ancillary Data

Table H1. Case 1: Predicted Casualties

TN1002507	40	124	15.0	5.04	0.01	1 (1
TN002587	40	134	15.9	5.04	0.81	1.61
TN002588	41	17	0.33	0.09	0.01	0.03
TN002589	42	275	25.3	9.42	1.85	3.68
TN002590	43	11	1.01	0.38	0.07	0.15
TN002591	44	90	8.28	3.08	0.61	1.2
TN002592	45	145	13.34	4.97	0.98	1.94
TN002593	46	56	1.01	0.27	0.04	0.09
TN002594	47	15	0.27	0.07	0.01	0.02
TN002595	48	13	0.44	0.11	0.01	0.01
TN002596	49	132	7.26	2.49	0.46	0.92
TN002597	50	378	20.8	7.12	1.32	2.63
TN002598	51	136	7.48	2.56	0.48	0.94
TN002599	52	626	34.44	11.8	2.19	4.35
TN002600	53	668	36.75	12.59	2.34	4.64
TN002601	54	719	73.46	27.58	5.43	10.81
TN002602	55	64	3.59	1.23	0.23	0.45
TN002603	56	647	0.57	0.05	0	0
TN002604	57	675	0.59	0.06	0	0
TN002605	58	352	0.33	0.03	0	0
TN002606	59	162	0.76	0.11	0.01	0.01
TN002607	60	58	0.06	0.01	0	0
TN002608	61	151	0.14	0.01	0	0
TN002609	62	177	0.83	0.12	0.01	0.02
TN002610	63	677	0.6	0.06	0	0
TN002611	64	494	13.56	4.11	0.72	1.43
TN002612	65	216	5.93	1.79	0.32	0.63
TN002613	66	197	5.41	1.64	0.29	0.57
TN002614	67	425	11.67	3.53	0.62	1.23
TN002615	68	358	9.83	2.97	0.52	1.04
TN002616	69	117	3.21	0.97	0.17	0.34
TN002617	70	932	71.41	23.03	3.74	7.39
TN002618	71	260	19.45	6.26	1.01	2.01
TN002619	72	373	10.98	3.37	0.6	1.19
TN002620	73	399	27.23	8.68	1.4	2.77
TN002621	74	335	5.37	1.39	0.23	0.45
TN002622	75	573	16.86	5.18	0.92	1.82
TN002623	76	298	20.34	7.15	1.34	2.67
TN002624	77	573	23.26	7.61	1.39	2.75
TN002625	78	1213	56.06	19.43	3.72	7.39
TN002626	79	133	0.13	0.01	0	0
TN002627	80	369	0.36	0.04	0	0
TN002628	81	248	0.24	0.02	0	0
TN002629	82	748	0.58	0.05	0	0
TN002630	83	655	0.51	0.05	0	0
TN002631	84	641	1.41	0.16	0	0.01

TN002631 85 60 355 127 024 049							
	TN002631	85	60	3.55	1.27	0.24	0.49

		1000 112. Cu	Econon	nic Losses (The		
Hazus ID	Struc. No.	STR	NSA	NSD	Contents	Total
TN002548	1	\$95,726	\$82,765	\$197,729	\$164,493	\$540,713
TN002549	2	\$389,134			\$668,676	\$2,198,033
TN002550	3	\$83,614	\$72,292	\$172,710	\$143,680	\$472,297
TN002551	4	\$100,024	\$86,481	\$206,607	\$171,879	\$564,990
TN002552	5	\$2,034,915	\$2,451,521	\$5,017,695	\$4,067,616	\$13,571,747
TN002553	6	\$2,034,515	\$2,517,340	\$5,152,411	\$4,176,823	\$13,936,123
TN002554	7	\$1,025,521	\$1,205,977	\$2,556,938	\$2,049,834	\$6,838,271
TN002555	8	\$1,676,073	\$2,388,463	\$4,318,756	\$3,899,866	\$12,283,158
TN002556	9	\$2,922,766	\$3,437,073	\$7,287,353	\$5,842,091	\$19,489,283
TN002557	10	\$1,762,876	\$2,156,761	\$4,399,272	\$3,685,728	\$12,004,637
TN002558	10	\$6,374,958	\$9,168,204	\$16,425,660	\$14,924,735	\$46,893,556
TN002559	11	\$3,261,751	\$4,697,522	\$8,404,489	\$7,643,965	\$24,007,726
TN002560	12	\$913,306	\$1,319,200	\$2,353,111	\$2,144,537	\$6,730,155
TN002561	13	\$1,066,293	\$1,349,467	\$2,675,837	\$2,268,061	\$7,359,659
TN002562	15	\$517,065	\$743,622	\$1,332,266	\$1,210,528	\$3,803,481
TN002563	16	\$410,052	\$589,721	\$1,056,538	\$959,995	\$3,016,305
TN002564	17	\$200,364	\$190,086	\$417,613	\$339,210	\$1,147,272
TN002565	18	\$135,843	\$122,789	\$292,769	\$209,551	\$760,951
TN002566	19	\$135,843	\$122,789	\$292,769	\$209,551	\$760,951
TN002567	20	\$80,359	\$79,536	\$162,518	\$156,574	\$478,987
TN002568	21	\$48,494	\$28,563	\$103,300	\$53,125	\$233,482
TN002569	22	\$132,703	\$155,607	\$265,887	\$305,813	\$860,010
TN002570	23	\$47,690	\$55,921	\$95,553	\$109,902	\$309,066
TN002571	24	\$45,261	\$26,659	\$96,413	\$49,584	\$217,917
TN002572	25	\$1,590,432	\$1,468,232	\$3,761,890	\$2,690,229	\$9,510,782
TN002573	26	\$847,180	\$782,088	\$2,003,858	\$1,433,013	\$5,066,139
TN002574	27	\$3,144,466	\$4,429,299	\$8,091,172	\$7,243,165	\$22,908,102
TN002575	28	\$1,003,927	\$794,378	\$2,102,396	\$1,550,425	\$5,451,127
TN002576	29	\$1,075,061	\$850,663	\$2,251,362	\$1,660,281	\$5,837,367
TN002577	30	\$1,525,097	\$1,206,763	\$3,193,815	\$2,355,299	\$8,280,974
TN002578	31	\$520,006	\$732,492	\$1,337,358	\$1,197,787	\$3,787,643
TN002579	32	\$214,690	\$187,008	\$499,579	\$347,224	\$1,248,500
TN002580	33	\$1,001,859	\$1,428,490	\$2,581,253	\$2,331,429	\$7,343,030
TN002581	34	\$642,404	\$901,337	\$1,650,876	\$1,474,794	\$4,669,412
TN002582	35	\$203,734	\$173,730	\$468,869	\$326,309	\$1,172,642
TN002583	36	\$43,773	\$60,084	\$112,062	\$98,605	\$314,524
TN002584	37	\$373,533	\$512,717	\$956,262	\$841,426	\$2,683,938
TN002585	38	\$682,210	\$959,617	\$1,748,366	\$1,569,863	\$4,960,056

Table H2. Case 1: Predicted Economic Losses

TN1002596	20	\$296.246	\$220.262	¢000 007	¢(10(0)	¢0 002 122
TN002586	39	\$386,246	\$329,363	\$888,897	\$618,628	\$2,223,133
TN002587	40	\$656,184	\$879,139 \$26,104	\$1,655,465	\$1,453,820	\$4,644,608
TN002588	41	\$42,445	\$36,194	\$97,681	\$67,981	\$244,300
TN002589	42	\$2,511,422	\$3,452,072	\$6,435,868	\$5,667,369	\$18,066,731
TN002590	43	\$102,663	\$141,116	\$263,089	\$231,674	\$738,543
TN002591	44	\$821,656	\$1,129,406	\$2,105,608	\$1,854,180	\$5,910,849
TN002592	45	\$1,323,940	\$1,819,820	\$3,392,781	\$2,987,653	\$9,524,195
TN002593	46	\$243,052	\$201,180	\$555,881	\$378,445	\$1,378,558
TN002594	47	\$66,942	\$55,410	\$153,103	\$104,233	\$379,688
TN002595	48	\$89,650	\$97,650	\$223,529	\$164,899	\$575,728
TN002596	49	\$532,617	\$626,339	\$1,327,977	\$1,064,607	\$3,551,540
TN002597	50	\$1,524,831	\$1,793,149	\$3,801,871	\$3,047,866	\$10,167,717
TN002598	51	\$549,798	\$646,544	\$1,370,816	\$1,098,949	\$3,666,107
TN002599	52	\$4,418,020	\$5,195,441	\$11,015,481	\$8,830,840	\$29,459,783
TN002600	53	\$1,835,933	\$2,158,994	\$4,577,545	\$3,669,705	\$12,242,177
TN002601	54	\$7,359,671	\$10,644,593	\$18,963,580	\$17,297,637	\$54,265,481
TN002602	55	\$495,364	\$606,044	\$1,236,185	\$1,035,680	\$3,373,273
TN002603	56	\$138,003	\$541,157	\$293,414	\$1,054,540	\$2,027,113
TN002604	57	\$152,836	\$599,325	\$324,952	\$1,167,890	\$2,245,003
TN002605	58	\$119,641	\$441,213	\$252,645	\$860,644	\$1,674,142
TN002606	59	\$235,453	\$199,067	\$465,635	\$387,748	\$1,287,903
TN002607	60	\$19,589	\$72,239	\$41,365	\$140,912	\$274,104
TN002608	61	\$51,232	\$188,932	\$108,185	\$368,538	\$716,887
TN002609	62	\$258,578	\$218,618	\$511,367	\$425,831	\$1,414,394
TN002610	63	\$149,298	\$585,451	\$317,430	\$1,140,855	\$2,193,034
TN002611	64	\$1,097,716	\$1,045,192	\$2,613,659	\$1,906,749	\$6,663,317
TN002612	65	\$480,646	\$457,648	\$1,144,417	\$834,890	\$2,917,601
TN002613	66	\$707,015	\$673,186	\$1,683,401	\$1,228,096	\$4,291,697
TN002614	67	\$825,701	\$786,193	\$1,965,993	\$1,434,256	\$5,012,143
TN002615	68	\$695,444	\$662,168	\$1,655,851	\$1,207,997	\$4,221,460
TN002616	69	\$228,850	\$217,900	\$544,890	\$397,515	\$1,389,155
TN002617	70	\$5,601,473	\$7,997,845	\$14,423,503	\$13,042,030	\$41,064,852
TN002618	71	\$1,106,082	\$1,554,743	\$2,844,344	\$2,543,050	\$8,048,220
TN002619	72	\$959,015	\$914,019	\$2,296,756	\$1,647,889	\$5,817,679
TN002620	73	\$3,122,738	\$4,206,703	\$7,966,087	\$6,914,246	\$22,209,774
TN002621	74	\$709,658	\$565,972	\$1,603,693	\$1,071,377	\$3,950,700
TN002622	75	\$1,209,668	\$1,152,912	\$2,897,049	\$2,078,590	\$7,338,219
TN002623	76	\$1,407,390	\$1,806,346	\$3,537,993	\$3,020,769	\$9,772,497
TN002624	77	\$1,380,839	\$1,500,554	\$3,387,340	\$2,641,267	\$8,910,001
TN002625	78	\$1,523,009	\$1,524,023	\$3,525,888	\$2,548,798	\$9,121,718
TN002626	79	\$29,832	\$86,581	\$62,939	\$165,485	\$344,838
TN002627	80	\$82,589	\$239,698	\$174,246	\$458,141	\$954,674
TN002628	81	\$80,642	\$234,047	\$170,138	\$447,339	\$932,166
TN002629	82	\$125,732	\$442,464	\$270,232	\$841,234	\$1,679,662
TN002630	83	\$107,046	\$376,706	\$230,071	\$716,212	\$1,430,035
		+,0.0	+ 5,, 66	+,0,1	+·, 	+ -, 0,000

TN002631	84	\$277,711	\$449,467	\$558,927	\$877,827	\$2,163,932
TN002631	85	\$182,162	\$205,265	\$441,318	\$341,637	\$1,170,383

Llagua ID	Struc.	Day	Day Casualties					
Hazus ID	No.	Occ.	Level 1	Level 2	Level 3	Level 4		
TN002554	7	214	11.77	4.03	0.75	1.49		
TN002555	8	302	23.54	7.6	1.23	2.44		
TN002556	9	498	27.4	9.39	1.74	3.46		
TN002557	10	565	31.66	10.87	2.02	4.01		
TN002558	11	1273	99.05	31.99	5.19	10.27		
TN002559	12	469	48	18.03	3.55	7.06		
TN002560	13	154	11.94	3.85	0.63	1.24		
TN002561	14	361	23.42	8.19	1.53	3.04		
TN002562	15	143	11.13	3.59	0.58	1.15		
TN002563	16	113	8.79	2.84	0.46	0.91		
TN002596	49	132	7.26	2.49	0.46	0.92		
TN002597	50	378	20.8	7.12	1.32	2.63		
TN002598	51	136	7.48	2.56	0.48	0.94		
TN002599	52	626	34.44	11.8	2.19	4.35		
TN002600	53	668	36.75	12.59	2.34	4.64		
TN002601	54	719	73.46	27.58	5.43	10.81		
TN002602	55	64	3.59	1.23	0.23	0.45		

Table H3. Case 2: Predicted Casualties

Table H4. Case 2: Predicted Economic Losses

Hazus ID	Struc.	Economic Losses (Thousands)						
	No.	STR	NSA	NSD	Contents	Total		
TN002554	7	\$1,025,521	\$1,205,977	\$2,556,938	\$2,049,834	\$6,838,271		
TN002555	8	\$1,676,073	\$2,388,463	\$4,318,756	\$3,899,866	\$12,283,158		
TN002556	9	\$2,922,766	\$3,437,073	\$7,287,353	\$5,842,091	\$19,489,283		
TN002557	10	\$1,762,876	\$2,156,761	\$4,399,272	\$3,685,728	\$12,004,637		
TN002558	11	\$6,374,958	\$9,168,204	\$16,425,660	\$14,924,735	\$46,893,556		
TN002559	12	\$3,261,751	\$4,697,522	\$8,404,489	\$7,643,965	\$24,007,726		
TN002560	13	\$913,306	\$1,319,200	\$2,353,111	\$2,144,537	\$6,730,155		
TN002561	14	\$1,066,293	\$1,349,467	\$2,675,837	\$2,268,061	\$7,359,659		
TN002562	15	\$517,065	\$743,622	\$1,332,266	\$1,210,528	\$3,803,481		
TN002563	16	\$410,052	\$589,721	\$1,056,538	\$959,995	\$3,016,305		
TN002596	49	\$532,617	\$626,339	\$1,327,977	\$1,064,607	\$3,551,540		
TN002597	50	\$1,524,831	\$1,793,149	\$3,801,871	\$3,047,866	\$10,167,717		
TN002598	51	\$549,798	\$646,544	\$1,370,816	\$1,098,949	\$3,666,107		

TN002599	52	\$4,418,020	\$5,195,441	\$11,015,481	\$8,830,840	\$29,459,783
TN002600	53	\$1,835,933	\$2,158,994	\$4,577,545	\$3,669,705	\$12,242,177
TN002601	54	\$7,359,671	\$10,644,593	\$18,963,580	\$17,297,637	\$54,265,481
TN002602	55	\$495,364	\$606,044	\$1,236,185	\$1,035,680	\$3,373,273

Harna ID	Struc.	Day	Day Casualties					
Hazus ID	No.	Occ.	Level 1	Level 2	Level 3	Level 4		
TN002554	7	214	11.4	3.89	0.72	1.43		
TN002555	8	302	23.55	7.61	1.24	2.44		
TN002556	9	498	33.26	11.67	2.19	4.34		
TN002557	10	565	40.94	14.49	2.72	5.41		
TN002558	11	1273	98.91	31.94	5.19	10.26		
TN002559	12	469	48	18.03	3.55	7.06		
TN002560	13	154	11.98	3.87	0.63	1.24		
TN002561	14	361	23.15	8.08	1.51	3		
TN002562	15	143	11.12	3.59	0.58	1.15		
TN002563	16	113	8.79	2.84	0.46	0.91		
TN002596	49	132	8.57	3	0.56	1.11		
TN002597	50	378	24.53	8.58	1.61	3.19		
TN002598	51	136	8.82	3.09	0.58	1.15		
TN002599	52	626	33	11.24	2.08	4.13		
TN002600	53	668	39.29	13.58	2.53	5.02		
TN002601	54	719	73.64	27.66	5.45	10.84		
TN002602	55	64	4.56	1.61	0.3	0.6		

Table H5. Case 3: Predicted Casualties

Table H6. Case 3: Predicted Economic Losses

	Struc.	Economic Losses (Thousands)						
	No.	STR NSA NSD		Contents	Total			
TN002554	7	\$1,009,534	\$1,172,835	\$2,513,795	\$1,998,626	\$6,694,790		
TN002555	8	\$1,676,573	\$2,402,608	\$4,320,055	\$3,915,908	\$12,315,144		
TN002556	9	\$3,221,600	\$4,104,228	\$8,092,827	\$6,876,446	\$22,295,101		
TN002557	10	\$2,008,644	\$2,639,169	\$5,062,106	\$4,392,411	\$14,102,330		
TN002558	11	\$6,369,300	\$9,108,405	\$16,410,996	\$14,853,462	\$46,742,163		
TN002559	12	\$3,261,587	\$4,679,093	\$8,404,489	\$7,623,669	\$23,968,837		
TN002560	13	\$915,349	\$1,311,072	\$2,358,482	\$2,137,049	\$6,721,952		
TN002561	14	\$1,059,871	\$1,317,280	\$2,658,810	\$2,210,339	\$7,246,300		
TN002562	15	\$516,988	\$739,326	\$1,331,999	\$1,205,684	\$3,793,997		
TN002563	16	\$409,991	\$586,314	\$1,056,326	\$956,153	\$3,008,784		
TN002596	49	\$578,464	\$730,439	\$1,451,642	\$1,227,198	\$3,987,743		

TN002597	50	\$1,656,087	\$2,091,177	\$4,155,910	\$3,513,350	\$11,416,524
TN002598	51	\$597,124	\$754,002	\$1,498,469	\$1,266,785	\$4,116,381
TN002599	52	\$4,326,284	\$4,963,768	\$10,766,398	\$8,447,834	\$28,504,283
TN002600	53	\$1,897,563	\$2,300,701	\$4,744,996	\$3,893,977	\$12,837,237
TN002601	54	\$7,370,241	\$10,669,438	\$18,990,040	\$17,333,219	\$54,362,938
TN002602	55	\$559,589	\$737,119	\$1,408,782	\$1,229,551	\$3,935,040

Appendix I: Case 1 Ranking

Hazus ID	ase 1 Struc Structure Number	BRC	MD		<i>IO</i>	Rank
TN002629	82	4.715	0.013	0.300	0.750	1
TN002630	83	4.715	0.013	0.300	0.750	1
TN002626	79	5.388	0.021	1.300	0.684	2
TN002627	80	5.388	0.021	0.600	0.684	3
TN002628	81	5.388	0.021	0.300	0.684	4
TN002604	57	5.691	0.017	2.300	0.715	5
TN002603	56	5.691	0.017	0.300	0.715	6
TN002610	63	5.691	0.017	0.300	0.715	7
TN002607	60	5.895	0.019	2.700	0.694	8
TN002608	61	5.895	0.019	0.500	0.694	9
TN002605	58	5.895	0.019	0.300	0.694	10
TN002631	84	9.282	0.096	0.300	0.389	11
TN002569	22	12.481	0.188	1.200	0.237	12
TN002570	23	12.481	0.188	1.200	0.237	13
TN002606	59	14.269	0.267	2.300	0.161	14
TN002609	62	14.269	0.267	2.300	0.161	15
TN002567	20	14.492	0.251	3.800	0.162	16
TN002551	4	18.791	0.377	3.800	0.096	17
TN002550	3	18.791	0.377	3.100	0.096	18
TN002548	1	18.791	0.377	0.700	0.096	19
TN002549	2	18.791	0.377	0.300	0.096	20
TN002576	29	22.572	0.472	3.200	0.051	21
TN002575	28	22.572	0.472	2.500	0.051	22
TN002577	30	22.572	0.472	1.500	0.051	23
TN002571	24	24.519	0.564	3.700	0.031	24
TN002568	21	24.519	0.564	1.800	0.031	25
TN002621	74	32.313	0.675	0.300	0.018	26
TN002594	47	34.616	0.710	3.800	0.014	27
TN002593	46	34.616	0.710	3.100	0.014	28
TN002588	41	35.991	0.728	3.800	0.012	29
TN002586	39	35.991	0.728	3.100	0.012	30
TN002582	35	35.991	0.728	1.200	0.012	31
TN002564	17	36.838	0.696	0.600	0.024	32
TN002579	32	38.361	0.759	2.700	0.009	33
TN002572	25	42.384	0.804	3.100	0.006	34
TN002573	26	42.384	0.804	0.500	0.006	35
TN002566	19	43.252	0.802	1.500	0.012	36

Table I1. Case 1 Structures Ranked by Predicted Performance

TN002565	18	43.252	0.802	1.000	0.012	37
TN002612	65	44.312	0.823	1.900	0.005	38
TN002615	68	44.312	0.823	1.900	0.005	38
TN002614	67	44.312	0.823	0.500	0.005	39
TN002616	69	44.312	0.823	0.500	0.005	39
TN002611	64	44.312	0.823	0.300	0.005	40
TN002613	66	44.312	0.823	0.300	0.005	40
TN002619	72	45.904	0.839	0.300	0.004	41
TN002622	75	45.904	0.839	0.300	0.004	41
TN002625	78	52.888	0.864	0.300	0.005	42
TN002624	77	55.587	0.907	0.300	0.001	43
TN002595	48	62.909	0.955	3.700	0.000	44
TN002632	85	63.447	0.920	1.400	0.002	45
TN002598	51	66.108	0.957	2.700	0.000	46
TN002596	49	66.108	0.957	2.300	0.000	47
TN002556	9	66.108	0.957	1.900	0.000	48
TN002599	52	66.108	0.957	1.900	0.000	48
TN002600	53	66.108	0.957	1.900	0.000	48
TN002597	50	66.108	0.957	0.500	0.000	49
TN002554	7	66.108	0.957	0.300	0.000	50
TN002557	10	67.396	0.958	2.300	0.000	51
TN002602	55	67.396	0.958	0.900	0.000	52
TN002552	5	71.035	0.960	0.600	0.001	53
TN002553	6	71.035	0.960	0.500	0.001	54
TN002561	14	73.430	0.976	2.300	0.000	55
TN002623	76	75.732	0.981	0.300	0.000	56
TN002587	40	81.768	0.983	0.200	0.000	57
TN002620	73	85.765	0.993	0.600	0.000	58
TN002590	43	87.767	0.991	1.200	0.000	59
TN002589	42	87.767	0.991	0.300	0.000	60
TN002591	44	87.767	0.991	0.300	0.000	60
TN002592	45	87.767	0.991	0.300	0.000	60
TN002583	36	88.132	0.995	1.700	0.000	61
TN002584	37	88.132	0.995	1.200	0.000	62
TN002585	38	90.838	0.997	0.200	0.000	63
TN002581	34	91.435	0.998	0.500	0.000	64
TN002618	71	91.826	0.998	0.500	0.000	65
TN002574	27	91.879	0.997	0.300	0.000	66
TN002578	31	92.056	0.998	0.500	0.000	67
TN002617	70	93.607	1.000	0.500	0.000	68
TN002580	33	94.309	1.000	0.400	0.000	69

TN002555	8	94.486	1.000	0.500	0.000	70
TN002560	13	94.559	1.000	0.500	0.000	71
TN002563	16	94.639	1.000	1.100	0.000	72
TN002562	15	94.639	1.000	0.800	0.000	73
TN002558	11	94.639	1.000	0.500	0.000	74
TN002559	12	94.694	0.999	0.300	0.000	75
TN002601	54	94.711	0.999	0.300	0.000	76

Appendix J:	Case 2	Ranking
--------------------	--------	---------

Hazus ID	Structure Number	S_{L1}	BRC	MD	ΙΟ	Rank
TN002598	51	2.7	66.108	0.957	0	1
TN002596	49	2.3	66.108	0.957	0	2
TN002557	10	2.3	67.396	0.958	0	3
TN002561	14	2.3	73.430	0.976	0	4
TN002556	9	1.9	66.108	0.957	0	5
TN002599	52	1.9	66.108	0.957	0	5
TN002600	53	1.9	66.108	0.957	0	5
TN002563	16	1.1	94.639	1.000	0	6
TN002602	55	0.9	67.396	0.958	0	7
TN002562	15	0.8	94.639	1.000	0	8
TN002597	50	0.5	66.108	0.957	0	9
TN002555	8	0.5	94.486	1.000	0	10
TN002560	13	0.5	94.559	1.000	0	11
TN002558	11	0.5	94.639	1.000	0	12
TN002554	7	0.3	66.108	0.957	0	13
TN002559	12	0.3	94.694	0.999	0	14
TN002601	54	0.3	94.711	0.999	0	15

 Table J1. Case 2 Structures Ranked by Predicted Performance

a <u>ble K1. Cas</u>	se 3 Struct	tures Ran	ked by	Predict	ted Per	forman
Hazus ID	Structure Number	BRC	MD	S_{L1}	ΙΟ	Rank
TN002599	52	64.264	0.95	1.9	0.001	1
TN002554	7	64.840	0.952	0.3	0.001	2
TN002600	53	68.978	0.965	1.9	0	3
TN002561	14	72.608	0.974	2.3	0	4
TN002598	51	73.379	0.976	2.7	0	5
TN002596	49	73.379	0.976	2.3	0	6
TN002597	50	73.379	0.976	0.5	0	7
TN002556	9	74.693	0.979	1.9	0	8
TN002602	55	78.017	0.985	0.9	0	9
TN002557	10	78.709	0.987	2.3	0	10
TN002558	11	94.440	1	0.5	0	11
TN002563	16	94.481	1	1.1	0	12
TN002562	15	94.481	1	0.8	0	13
TN002560	13	94.526	1	0.5	0	14
TN002559	12	94.580	0.999	0.3	0	15
TN002555	8	94.688	1	0.5	0	16
TN002601	54	94.927	1	0.3	0	17

Appendix K: Case 3 Ranking

 Table K1. Case 3 Structures Ranked by Predicted Performance

Appendix L. Level 1 Data Collection Form Results

Below are the Level 1 Data Collection forms for each structure studied and a few photographs of each structure studied in order of structure number. The Hazus ID and structure number are paired in Appendices F and H.

Level 1 HIGH Seismicity

	РНОТС	DGRAPI	н				Oth Bui Use Lati Ss: Scr No. Tot: Adc	e: E itude: 3 itude: 3 stories al Floor litions: cupancy	ifiers: Ime: Ie S 5 9 S 7 S 7 S 7 S 7 S 7 S 7 S 7 S 7	1 1 1 1 1 1 1 1 1 1 1 1 1 1	A Yes, Comme Office Wareho	Belo Belo 250 Year(s) E ercial	Longitu S1: O D W Grade Built: 1 Emer. S School Resider	ide: .413 ate/Tim e: 	e: 3/ _ Year Code ↓ 19 □ Hi □ G nits:	940 Built: Year: 95 istoric overnmer	351 510: 1982 2010 Shell	
	1 1	_		-			Soil	Type:	Hard	Avg	Den					NK DNK, ass	ите Туре	D.
XN,T.S.	F .						Gor		Rock	Rock	So	31	1.		Soil			~
T = this form								acency:			ounding				rom Taller			
	L	m-						gularitie		Ve Ve		pe/sever			level			
	-							erior Fa ards:	lling			, Chimney	/S		avy Clado pendages		eavy Ver	neer
					[]		CO	MMENT	S:	0.00	0	1			1.		4	
3	A	2 IIII Ling			0			Pol Pr	ren ¹ e 1	198°	for For	po esti	im	dinate	y 198	2.	3	
	SKE	ТСН						Addition	al sketch	es or cor	nments (on senar	ate nade					
		B.	ASIC	sco	RE, MC	DIFIE												
FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1		3.6 -1.2	3.2 -1.2	2.9		2.0 -1.0	2.6	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1		-0.7	-0.7	-0.7		-0.6	-0.7	-0.6	-0.5	-0.9	-1.0 -0.6	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7 -0.4	NA
Plan Irregularity, PL1		-1.1	-1.0	-1.0	1. States	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code		-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark Soil Type A or B		1.6 0.1	1.9	2.2	1996	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)		0.1	0.3 0.2	0.5	1	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9	in a second	-0.6	NA	-0.6	-0.4	0.0	0.0	-0.2	-0.3 NA	-0.1 -0.4	-0.1	-0.1	-0.2	-0.4
Minimum Score, SMIN		1.1	0.9	0.7		0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	-0.6 0.3	-0.2 0.2	1.0
FINAL LEVEL 1 SCORE, SL	≥ Smin:	0	7	20	1.3				and so the second							0.0		1.0
EXTENT OF REVIEW			and the second		OTHE	R HAZ	ARDS			ACT	ONR	EQUIF	RED					
Exterior: Partia Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Tor		All Sides Visible No	Aer Ent		Are Ther Detailed Pour cut-o	e Hazar Structu nding pol off, if kno ng hazar	ds That ' ral Evalu tential (ur	Trigger A ation? nless SL2	>	Detaile Ye X Ye No	ed Struc es, unkno es, score es, other	tural Even own FEM less that hazards	aluation A buildir n cut-off present	ng type o	or other bu	,		
				-	Geol	ogic haz	ards or S	oil Type	F						commend			
and the second	Yes			lo	Signi Signi the s	ficant da tructural	amage/de system	terioratio	n to	de de	o, nonstr tailed ev o, no nor	uctural had a luation a luation a structuration a la structuration a structuration a la structuration a la structuration a la structuration a structurati	azards e is not ne il hazard	xist that cessary s identifi		ire mitiga	aluated ation, but	а
Where info	mation c	annot b	e verifie	d, scr	eener sha	ll note ti	he follow	ing: ES	GT = Esti	mated o	r unrelia	ble data	OR	DNK = D			-	
Legend: MRF = M	oment-resi ced frame		e	RC = R	einforced co hear wall		1		Unreinfo	rced masc		MH	= Manufa = Light me	ctured Ho	_		e diaphrag diaphragm	gm

Structure 1, Building 1 Photographs



Joint between Structures 1 (Left) and 2 (Right)



Interior, Reinforced Masonry



Exterior

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Level 1 HIGH Seismicity

P	HOTOGR	арн			-6		Oth Buil Use Lati Ss:	er Ident ding Na : E tude: :	ifiers: ame: 1.evv 3.5.0 3.5.0 3.6	2 Lent	on inter	Sch	Longitu S1: C	de: -		940	584	
							No. Tota	Stories	: <u>C</u> : Abov Area (so	e Grade q. ft.):	49	Belov 79 (ear(s) B	v Grade	0	Year Code	Built: Year:	10:15	EST
							Occ	upancy		embly Istrial	Comme Office Wareho	rcial	Emer. S	ervices			Shelt	
KN.T.S.							Soil	Type:	Hard Rock	Avg Rock	Den: Soi		tiff S	oft P		N K DNK, ass	ume Type	D.
							Geo	logic H	azards:	Liquefac	tion: Yes	No/ON	Lands	lide: Yes	NODNK	Surf. R	upt.: Yes/I	NOUDNE
TI= this form				101				acency:			ounding						t Building	
	9	5		1			Irreg	gularitie	s:		ertical (ty an (type)	pe/sever	ity) Sf	tran	level t co	ner	od.	
	1						Haz	erior Fal ards:			arapets	Chimney	'S		avy Clado pendages		eavy Ven	neer
	1				\square		CO	MMENT	'S:			-			1 . 1	1		
	1111 1111 1111			(D			bi bi	shi ould it i	hpe ha t i	ve srit	pou	ndii n e	ng	pot lai	enf. Idin	als,	
							-					÷						
	SKETC	-							al sketch					-				
FEMA BUILDING TYPE Do	Not V		WIA	W2	RE, MO	DIFIE S2	-		-			24	1.50					
	lnow				(MRF)	(BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Severe Vertical Irregularity, VL1		200	3.2 -1.2	2.9 -1.2	2.1 -1.0	2.0 -1.0	-1.1	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6	1.4 -0.9	-0.9	1.7 -0.9	1.0 -0.7	1.5 NA
Moderate Vertical Irregularity, VL1		1000	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	0.5	-0.5	-0.4	NA
Plan Irregularity, PL1 Pre-Code	1.16	10.00	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	0.0	-0.7	-0.4	NA
Post-Benchmark		1.12	1.9	2.2	1.4	1.4	1.1	1.9	NA	-0.4 1.9	-0.7 2.1	-0.1 NA	-0.5 2.0	-0.3 2.4	-0.5	-0.5 2.1	0.0 NA	-0.1 1.2
Soil Type A or B			0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)		100	0.2	0.1 -0.9	-0.2	-0.4	0.2 NA	-0.1	-0.4 -0.4	0.0	0.0	-0.2 -0.3	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, SMIN			0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	NA 0.2	-0.4	-0.5 0.3	-0.6 0.3	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge$	Smin:	03	20)'5						101.0							U.L.	1.0
EXTENT OF REVIEW		-	-	-	OTHER	RHAZ	ARDS			ACT	ON R	EQUIF	RED			1		
Exterior: Partial Interior: None					Are Ther	e Hazar	ds That	Frigger A	4	Detaile	d Struc	tural Eva	aluation	Require	d?			
Interior: Interior: None Drawings Reviewed: Yes	Visib	ie D	Ente	red	Detailed	Sec. 1	1			TYe	s, unkno	wn FEM	A buildin	ng type o	r other bu	uilding		
Soil Type Source:					Poun cut-o	ding pot ff, if know		IIESS SL2	>			less than hazards						
Geologic Hazards Source: Contact Person:	H.c.	-1			Fallin	g hazard	ds from ta	aller adja	icent				Prosent					
1-1-1	Ka				build		ards or S	oil Type	F	Detaile	d Nons	tructural	Evaluat	tion Rec	ommend	led? (ch	eck one)	
LEVEL 2 SCREENING PE	RFOR	MED	?		🗌 Signi	ficant da	mage/de			🗆 Ye	s, nonst	ructural h	nazards i	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2			No 🕅			tructural				L No	, nonstru tailed ev	actural ha	azards e	xist that	may requ	ire mitig	ation, but	а
Nonstructural hazards? Ye			No No								, no non	structura	l hazard	s identifi		DNK		
Where informa												ble data	OR I	DNK = D	o Not Kr	ow		
Legend: MRF = Mome BR = Braced	ent-resisting frame	frame			inforced content	ncrete		JRM INF : TU = Tilt u	= Unreinfo	rced maso	nry infill		= Manufa = Light me	ctured Ho) = Flexib	le diaphrag diaphragm	gm

Structure 2, Building 1 Photographs



Joint between Structures 1 (Left) and 2 (Right)



Exterior

Level 1 HIGH Seismicity

Ρ	HOTOGRAP	н				Oth Buil Use Lati Ss: Scro No. Tota Add	er Ident ding Na : E tude: 1 . T eener(s) Stories	Tre ifiers: 	re Grade q. ft.): lone embly ustrial	1017 1017 1017 1017	Belov D 70 Year(s) B	v Grade	ide:	e: 3/ Year Code 198'	941 5 11 Suilt: Year: 7 2	194 2115 A 1995 1 010 010	EST
KN. to		11		-		Soil	Туре:	A Hard Rock	Avg Rock	Den	C St	D C	E Coft P		NK DNK, ass	ume Type	D.
A100113						Geo	logic H					22. J			Surf R	int · Yes/	NoON
= this form						17181181818181	acency:			ounding	and the second se	Comment of the second		om Taller			
	LAE					Irreg	gularitie	s:			pe/sever	ity)					
		1								an (type				int (
							erior Fa ards:	ling		arapets	Chimney	S		avy Clado pendages		eavy Ver	leer
3	awning SKETCH		SCO	RE, MO							on separa						
	o Not W1	W1A	W2	S1	S2	S3	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
	Know			(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score Severe Vertical Irregularity, VL1	3.6	3.2	2.9	-1.0	2.0 -1.0	2.6	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	1.7	1.7 -0.9	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.9	-0.7 -0.4	NA NA
Plan Irregularity, PL1 Pre-Code	-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark	1.6	1.9	-0.9	-0.6	-0.6 1.4	-0.8	-0.6	-0.2 NA	-0.4	-0.7	-0.1 NA	-0.5 2.0	-0.3	-0.5	-0.5 2.1	0.0	-0.1
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	NA 0.3	1.2
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	-0.3	-0.6	-0.9	-0.6	-0.6 0.5	NA 0.6	-0.6	-0.4	-0.5 0.3	-0.7	-0.3 0.3	NA 0.2	-0.4	-0.5 0.3	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1≥			0.		0.0	0.0	0.0	0.0	0.0	0.0	0.5	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW Exterior: Interior: Drawings Reviewed: Geologic Hazards Source: Contact Person: Contact Person: COMPUTE 2 SCREENING PU Section 2 Score, Size Nonstructural hazards? Yes	All Sides	Aeria Ente	al red	OTHEF Are There Detailed 3 Poun cut-of Fallin buildi Geolo Signif	e Hazaro Structur ding pot ff, if know g hazaro ng ogic haza	ds That T ral Evalu ential (ur wn) ds from ta ards or S mage/de	Trigger A ation? hless SL2 aller adja	> cent F	Detaile	ed Structes, unknown es, score es, other o ed Nons es, nonstr o, nonstructailed ev	tructural h	A buildir n cut-off present Evalua nazards i azards e s not ne	tion Rec identified xist that	commence I that show may requ	led? (ch	aluated	
Where inform Legend: MRF = Mom BR = Bracec	ent-resisting fran	ne R	C = Re	ener shall einforced cor near wall		1		= Unreinfo		r unrelia	ble data	OR	DNK = D ctured Ho	o Not Kn using FI	ow D = Flexib	le diaphrag	

Structure 3, Building 1 Photographs



Exterior, Structure 3 (Right) and Structure 4 (Left), Connected Behind Tree

Level 1 HIGH Seismicity

PHOTOGRAPH Tright This Zip: 325322 PHOTOGRAPH User Section State Convertex Tright This PHOTOGRAPH Sic Ling Tright State Departments Sic Ling Tright State Sic Ling Tright State Distribution State Distribution State Distribution State Sic Ling Tright State Distribution State Distribution State Distribution State Distribution State Sic Ling Tright State Distribution State Distribution State Distribution State Distribution State Distribution State Sol Type Distribution State		-	Mar				12	Add	lress:				TAZ	: 51,		1in: 2	220	22	
PHOTOGRAPH Building Name: Latitude: Sc. (17.0.25) Longitude: 27.5 (1-0.5 GPU Latitude: Sc. (17.0.25) Longitude: 27.5 (1-0.5 GPU Screener(5): (1-0.7) Date: The St. (17.0.25) No. String: Control of								Oth	er Ident	ifiere	L	212	110			.ip: _3	025) C	
PHOTOGRAPH Use:: EL (wick rtor) School (SC) School (SC) School (SC) Streame(s): CM School (SC) DataTime: School (SC											-						-		
Hotograph Latitude: 55, 47, 20, 25, 40, 20, 54, 35 Conglude: 72, 53, 40, 05, 54, 40, 54, 44, 55 Hotograph Screener(s): C/N DataTime: 3, 115, 75, 10, 05, 54, 40, 54, 40, 54, 11, 52, 75, 10, 15, 50, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 52, 75, 10, 15, 54, 11, 12, 12, 11, 12, 15, 10, 15, 54, 11, 12, 12, 11, 12, 15, 10, 15, 54, 11, 12, 12, 11, 12, 12, 11, 12, 12, 11, 12, 12											low	ani	CIL	1			-		
Sr 1.13 22 0.411 1.15 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>Lati</th><th>tuda</th><th>LEC</th><th>630</th><th>220</th><th>SUP</th><th>1001</th><th>do:</th><th>28</th><th>alla</th><th>050</th><th></th></t<>								Lati	tuda	LEC	630	220	SUP	1001	do:	28	alla	050	
Screener(1): C_M Date:Time: 3/15 D D/15 D/15 AM No. Stories: Above Grade:		DUOTO	00040								110	103-1			.412	001	170	011	
No. Stories: Additional sketches or commercial on separate page. No. Stories: Additional sketches or commercial on separate page. No. This No. Stories: Additional sketches or commercial on separate page. Skitzer Dester Dester Dester Dester Skitzer Dester Dester Dester Dester Dester Skitzer Dester Dester Dester Dester Dester Dester Skitzer Dester Dester Dester Dester Dester Dester Dester Dester Skitzer Dester		PHOIC	GRAP	н							Λ	153.00					KA	101	c n.d.
Total Floor Area (pt, ft): 1:												-							111.0
Addition: None												_		w Grade	:0			2010	EST
Occupancy: Asarchy: Converted: Bigs: Bi																	Year:	-	
Industrial Office Image: Set Type: Image: Set Type														uilt:	198	6319	872	1995	
Soil Type: A B								Occ	upancy	Indu	ustrial	Office		School		G		A STATE OF STREET	ler
Roke Roke Bill Seil Seil Seil Seil Seil Seil Seil S								Soil	Type:]D [JE [ume Type	D
Adjacency: SP Pounding Falling Hozards from Taller Adjacent Building Imagularities: Vertical (type averity) Horizards from Taller Adjacent Building Imagularities: Vertical (type averity) Horizards from Taller Adjacent Building Imagularities: Vertical (type averity) Horizards from Taller Adjacent Building Imagularities: Vertical (type averity) Horizards from Taller Adjacent Building Imagularities: Vertical (type averity) Horizards from Taller Adjacent Building Imagularities: Vertical (type averity) Horizards from Taller Adjacent Building Imagularity Processor Additional sketches or comments on separate page EXETCH Additional sketches or comments on separate page Basic Soce Row Mithing Wild Wild Wild Big	*NIT.S.									Rock	Rock	So	il S	oil S	ioil S	Soil			
Image: line of the line		2 mil	Contain the	1				Geo	logic H	azards:	Liquefac	tion: Ye	s/No/DN	Lands	lide: Yes	NODNK	Surf. R	upt.: Yes/	No/QNK
Image: sector in the sector	1 = this form		2438																
Exterior Failing Unbraced Chimeys Heavy Cladding or Heavy Veneer Haards: Paragets Appendages Other: Comments on separate page SKETCH Additional sketches or comments on separate page Extender Type Additional sketches or comments on separate page Basic Score SKETCH Basic Score 35 32 24 21 20 24 20 17 15 20 12 16 14 17 10 15 Severe Vortical imgularity, V ₁ 12 12 12 20 24 20 17 15 20 12 16 14 17 10 15 Severe Vortical imgularity, V ₁ 12 12 10 15 15 20 12 16 14 10 15 Severe Vortical imgularity, V ₁ 12 12 10 15 15 20 17 15 20 12 16 14 17 10 15 Severe Vortical imgularity, V ₁ 12 12 14 10 03 05 <t< th=""><th>17</th><th></th><th>9-</th><th>1</th><th></th><th></th><th></th><th>Irreg</th><th>gularitie</th><th>IS:</th><th></th><th>ertical (ty an (type</th><th>pe/sever</th><th></th><th>in an an</th><th></th><th></th><th></th><th></th></t<>	17		9-	1				Irreg	gularitie	IS:		ertical (ty an (type	pe/sever		in an				
Comments on separate page SKETCH Comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 Moderatio Vertical Impguintly, Viz, -1, 2, 1, 2, 1, 2, 1, 2, 1, 0, 1, 0, -1, 1, 1, 1, 0, 0, 5, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,				24.14				100000		lling	D P	arapets	Chimney	/S				eavy Ver	neer
Additional sketches or comments on separate page SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.1 Tem Build SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.1 EMAID LIDING TYPE Do Not With With With With With With With With		16						CO	MMENT	S:				-	1.	-			
Additional sketches or comments on separate page SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FMA BULLDING TYPE Do Not With With With With With With With With		1		1	-			1	00	for	tip	1 6	1 VO	po.	shi	ng			
Additional sketches or comments on separate page SKETCH CASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S.r. EMAGE CONTROL 1000 (0000) (00000) (00000) (0000) (0000) (0000) (0000) (0000) (0000) (0000) (0000) (0000		1	a	1		0.	-1	-	0					1		7			
Additional sketches or comments on separate page SKETCH CASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S.r. EMAGE CONTROL 1000 (0000) (00000) (00000) (0000) (0000) (0000) (0000) (0000) (0000) (0000) (0000) (0000		1	G			U	1	_											
Additional sketches or comments on separate page SKETCH CASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, S.r. EMAGE CONTROL 1000 (0000) (00000) (00000) (0000) (0000) (0000) (0000) (0000) (0000) (0000) (0000) (0000	0	111	III	1	1		_												
SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not W1 W1A W2 St 2 St 2 St 3 St 4 St 5 Clock PC1 PC2 RM1 RM2 URM MM Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.0 0.0 0.9 0.9 0.9 0.9 0.9 0.9 0.7 NA Modarate Vertical Iregularity, V ₄ 0.7 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.3 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.6 0.4 0.5 0.4 0.5 0.4 0.5 <	(\mathbf{S})	+++	111			4													
SKETCH Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not W1 W1A W2 St 2 St 2 St 3 St 4 St 5 Clock PC1 PC2 RM1 RM2 URM MM Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.0 0.0 0.9 0.9 0.9 0.9 0.9 0.9 0.7 NA Modarate Vertical Iregularity, V ₄ 0.7 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.7 0.6 0.6 0.3 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.6 0.4 0.5 0.4 0.5 0.4 0.5 <						7.													
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not Know WI WI2 S1 S2 S3 S4 US C1 C2 C1 PC1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 (1)/// (1)// (1) 1.7 1.0 1.5 Severe Vertical Irregularity, VL, 1.2 1.2 1.2 1.2 1.0 1.0 1.1 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.0 NA Pian Irregularity, VL, 1.1 1.0 1.0 0.0 0.8 0.7 0.6		Qu	ning			L		-											
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not Know WI WI2 S1 S2 S3 S4 US C1 C2 C1 PC1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 (1)/// (1)// (1) 1.7 1.0 1.5 Severe Vertical Irregularity, VL, 1.2 1.2 1.2 1.2 1.0 1.0 1.1 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.0 NA Pian Irregularity, VL, 1.1 1.0 1.0 0.0 0.8 0.7 0.6		1	_	-				-											
FEMA BUILDING TYPE Do Not Know W1 W1A W2 S1 S2 S3 S4 S5 C1 C2 C3 PC1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 (1.7) 1.7 1.0 1.5 2.0 1.2 1.6 1.4 (1.7) 1.7 1.0 1.7 1.0 0.7 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.6 -0.5 -0.5 -0.6 -0.2 <td< th=""><th></th><th>SKE</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>-</th><th></th><th></th><th></th></td<>		SKE														-			
Know Min Min <th>FEMA BUILDING TYPE</th> <th>Do Not</th> <th></th> <th></th> <th>-</th> <th></th> <th></th> <th></th> <th>-</th> <th>-</th> <th>-</th> <th>-</th> <th>-</th> <th></th> <th>Dea</th> <th>Ditt</th> <th>Ditto</th> <th>11511</th> <th></th>	FEMA BUILDING TYPE	Do Not			-				-	-	-	-	-		Dea	Ditt	Ditto	11511	
Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.0 1.5 Severe Vertical Irregularity, V _{L1} -1.2 -1.2 -1.2 -1.0 -1.0 -0.7 -1.0 -0.7 -1.0 -0.7 -1.0 -0.7 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.4 NA 1.9 2.4 2.0 2.4 2.0 2.1 NA 1.2 1.0 1.0 1.0 1.0 1.0 1.0 -0.6		104212000000							(RC	(URM			(URM		PUZ			URM	MH
Severe Vertical Irregularity, V _{L1} -1.2 -1.2 -1.2 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -0.6 -0.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.6 -0.4 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.6 -0.4 NA Pian Irregularity, P _{L1} -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.5 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 <td></td> <td></td> <td>3.6</td> <td>3.2</td> <td>2.9</td> <td>2.1</td> <td>2.0</td> <td>2.6</td> <td></td> <td></td> <td>1.5</td> <td>2.0</td> <td></td> <td>16</td> <td>14</td> <td>(17)</td> <td>17</td> <td>10</td> <td>15</td>			3.6	3.2	2.9	2.1	2.0	2.6			1.5	2.0		16	14	(17)	17	10	15
Moderate Vertical Irregularity, V _{L1} -0.7 -0.7 -0.7 -0.7 -0.6 -	Severe Vertical Irregularity, VL1		1.		1.	1.000				1000		Charles -	100 C 100	1302507					
Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.5 -0.5 0.0 0.1 Post-Benchmark 1.6 1.9 2.2 1.4 1.4 1.1 1.9 NA 1.9 2.1 NA 2.0 2.4 0.5 0.5 0.0 0.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.4 0.5 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.5 0.4 0.5 0.5 0.4 0.5 0.5 0.3 0.4 0.5 0.5 0.3 0.4 0.5 0.5 0.3 0.4 0.5 0.5 0.3 0.3 0.3 0.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 <							1000	-0.7	-0.6	-0.5					1.	(10000	202		10020
Post-Benchmark 1.6 1.9 2.2 1.4 1.4 1.1 1.9 NA 1.9 2.1 NA 1.0.1 -0.1 -0.3 -0.3 -0.5 -0.5 0.0 -0.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.5 0.4 0.5 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.5 0.3 0.0 0.1 0.1 0.1 0.1 0.1 0.1 0.3			and the second	1	1 1 1 1 1 1 1 1 1				100000		20.00		6.02	1.1. OG	-0.6	-0.7	ALC: NOTE OF		
Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.4 0.5 0.4 0.5 0.4 0.5 0.5 0.4 0.5 0.5 0.5 0.6 0.4 0.5 0.4 0.5 0.5 0.5 0.6 0.4 0.5 0.5 0.5 0.6 0.6 0.4 0.5 0.5 0.5 0.6 0.6 0.4 0.5 0.5 0.5 0.6 0.4 0.5 0.5 0.5 0.6 0.6 0.4 0.5 0.5 0.5 0.6 <td></td> <td>1.1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1000</td> <td></td> <td>and the second</td> <td></td> <td>1</td> <td>10000</td> <td>-</td> <td>1.032.02</td> <td></td> <td>10.00</td>		1.1								1000		and the second		1	10000	-	1.032.02		10.00
Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.4 0.0 0.0 0.0 0.0 0.1 -0.				10.25782	10000	1.	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		11.3257		1 1 2 2 2 2	0.210202	200						1.2
Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, Sum 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.2 0.4 -0.5 -0.6 -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, Sum 1.1 0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.2 0.4 -0.6 -0.7 -0.8 -0.6 -0.2 NA -0.6									1000	1 1 1 1 1 1 1			00.81	100000	Sec.	2.4652	103.0	1000	10.015
Minimum Score, Sum 1.1 0.9 0.7 0.5 0.6 0.6 0.7 0.7 </td <td></td> <td>1000</td> <td>1.</td> <td>1 2533</td> <td>1.25</td> <td>100 T</td> <td></td> <td></td> <td>1</td> <td>1000</td> <td>1 12312</td> <td>1000</td> <td></td> <td>1.</td> <td></td> <td></td> <td></td> <td></td> <td>100.24</td>		1000	1.	1 2533	1.25	100 T			1	1000	1 12312	1000		1.					100.24
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: Image: Solution of the structural structur				-					-										
EXTENT OF REVIEW OTHER HAZARDS ACTION REQUIRED Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Detailed Structural Evaluation? Soil Type Source: Pounding potential (unless SL2> Ves, score less than cut-off Geologic Hazards Source: Pounding potential (unless SL2> Ves, other hazards present Contact Person: Ves, Final Level 2 Score, SL2 No Yes, Final Level 2 Score, SL2 No Significant damage/deterioration to the structural system No, nonstructural hazards identified that should be evaluated Where Information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MPF = Moment-resisting frame RC = Reinforced concrete URM MF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm	FINAL LEVEL 1 SCORE, SL	.1 ≥ Smin:		The second							0.0	0.0	0.0	0.2	0.2	0.0	0.0	0.2	1.0
Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless St2> cut-off, if known) Yes, score less than cut-off Geologic Hazards Source: Falling hazards from taller adjacent building No Contact Person: Tory Coss LEVEL 2 SCREENING PERFORMED? No Significant damage/deterioration to the structural system No Nonstructural hazards? Yes No No Detailed structural hazards identified Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MR = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm	EXTENT OF REVIEW						RHA7	ARDS			ACT		FOUR	DED		-	-	-	-
Interior: None Visible Visible Entered Drawings Reviewed: Yes No Detailed Structural Evaluation? Soil Type Source: Pounding potential (unless SL2 > cut-off, if known) Pounding potential (unless SL2 > cut-off, if known) Yes, score less than cut-off Contact Person: Torry LCASL Pounding potential (unless of cut-off, if known) Pounding potential (unless SL2 > cut-off, if known) Pounding potential (unless SL2 > cut-off, if known) LEVEL 2 SCREENING PERFORMED? Geologic hazards or Soil Type F Significant damage/deterioration to the structural system Pes, nonstructural hazards identified that should be evaluated Nonstructural hazards? Yes No No Detailed structural system Where Information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm		ial 🗖 4	All Sides	M Aer	ial			Contraction Press and		Δ					Decul	40			
Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless SL2 > cut-off, if known) Pes, score less than cut-off Geologic Hazards Source: Pounding potential (unless SL2 > cut-off, if known) Pes, score less than cut-off LEVEL 2 SCREENING PERFORMED? Geologic hazards or Soil Type F Significant damage/deterioration to the structural system No Ves, Final Level 2 Score, SL2 No No Detailed Nonstructural hazards identified that should be evaluated Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm										•									
Soil Type Source:	Drawings Reviewed: Yes		No							>	HY	es, unkno	own FEM	A buildir	ng type o	r other bi	uilding		
Contact Person: Tory kash LEVEL 2 SCREENING PERFORMED? Falling hazards from taller adjacent building Geologic hazards or Soil Type F Significant damage/deterioration to the structural system Yes, Final Level 2 Score, SL2 No Nonstructural hazards? Yes Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm									1000 012	-									
Contact Person: Dory ICash building LEVEL 2 SCREENING PERFORMED? building Geologic hazards or Soil Type F Yes, Final Level 2 Score, S _{L2} No Significant damage/deterioration to the structural system Pres, Final Level 2 Score, S _{L2} No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm	· · · · · · · · · · · · · · · · · · ·					🗌 Fallin	g hazard		aller adja	cent			nazarus	present					
LEVEL 2 SCREENING PERFORMED? Geologic hazards of Soli Type P Significant damage/deterioration to bignificant damage/deteriorati	Contact Person: Tor	YK	ash	-		buildi	ng						tructura	l Evalua	tion Rec	ommen	ded? (ch	eck onel	
□ Yes, Final Level 2 Score, SL2 □ Yes □ No the structural system □ No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Nonstructural hazards? □ Yes □ No No No No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm	LEVEL 2 SCREENING	PEREC	RME	D2							100								
Nonstructural hazards? Yes No Mode tailed evaluation is not necessary Nonstructural hazards? Yes No No No, no nonstructural hazards identified No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame PP = Record forme RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm			- NIVIE	-					elenoratio			o, nonstr	uctural h	azards e	xist that	may requ	lire mitia	ation, but	a
Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame PP = Brand frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm						010 31	- uoturai t	Jotom			de	tailed ev	aluation	is not ne	cessary				
Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry Infill MH = Manufactured Housing FD = Flexible diaphragm		10.0			_							o, no nor	structura	al hazard	s identifi				
Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry Infill MH = Manufactured Housing FD = Flexible diaphragm					d, scr	eener shal	I note th						ble data	OR	DNK = D	o Not Kr	wor		
			sting fram	ne	RC = Re	einforced cor	ncrete		URM INF	= Unreinfo	prced maso	onry infill	MH	= Manufa	ctured Ho		D = Flexib	le diaphra	gm

Structure 4, Building 1 Photographs



Exterior, Structure 3 (Right) and Structure 4 (Left), Connected Behind Tree



Exterior



Exterior

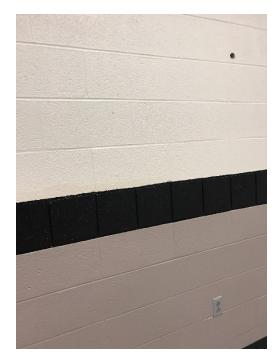
Level 1 **HIGH Seismicity**

	1111		-		,	201	(1	V L	11	115	0	AC			
				Add	ress: _	CUE TO	121	St	TWY	75		p.S		1	
				01		11	EVIT	no	112	-	Z	ip: <u>5</u>	838.	L	
					ding Na	ifiers: _	5			_					
							10 0	choo	1	-					
				Latit	ude: 3	45.0	633	21		ongitu	da	. 20.	671	UTX	,
PHOTOGRAPH				Set	1.1	6	6 -	101			ae:	2001	100	477	5
PHOTOGRAPH						: CV	M						< m	10:4	< AuA
				-	100				-						
							e Grade			v Grade	: 0			19950	EST
					itions:	Area (so		81-	905	2		Code	Year:		-
] Yes, Y							(1
				Occi	upancy		embly ustrial	Commer Office		Emer. S	ervices	HI		Shelte	er
						Utilit		Warehou			tial, #Un		overnmer	It	
				Soil	Type:		□В	580					NK		
		-		-	i jpc.	Hard	Avg	Dens	e St					ume Type	D.
¥12, T.S. == fl						Rock	Rock	Soil	in the second second	diversite and	Contraction of the local distance	oil			
	sped	100	ç	Geo	logic Ha	azards:	Liquefac	tion: Yes						upt.: Yes/N	
				Adja	cency:			ounding						t Building	
TATES				Irreg	ularitie	s:	N Ve	ertical (typ	e/sever	ity) Sf	plit	leve	1/10	od	
		/	1	-			PI PI	an (type)	r	e-er	ntra	nt u	orine	/	
	1	/	>		rior Fal	ling	U	hbraced (Chimney	S	Hea	avy Clado	ding or H	eavy Ven	eer
	/	-	/	Haza	ards:			arapets			App	endages	5		
		/		-			0	ther:	_	_	_				
	/	/	-		MMENT	5:		1	c.		01	11.1			
	<				spl	It	leve	1 (r	0051	ng	heig	hts)			
Land Land					-1		·			7	-	2			
		>													
		/		-											
	\bigvee			-											
		1		-											
SKETCH					Addition	al akatab		nments o							
BASIC S	COR		DIEIEE									-			
FEMA BUILDING TYPE Do Not W1 W1A	W2	S1	S2	\$3	S4	S5	C1	C2	C3	PC1	DCO	-	DHO		
Know		(MRF)	(BR)	(LM).	(RC	(URM	(MRF)	(SW)	(URM	(TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score 3.6 3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF)	1.5	2.0	INF) 1.2	1.6	1.4	1.7	1.7	1.0	15
Severe Vertical Irregularity, VL1 -1.2 -1.2	-1.2	-1.0	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	1.5 NA
Moderate Vertical Irregularity, VL1 -0.7 -0.7	-0.7	-0.6	-0.6	-0.7	-0.6	03	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1 -1.1 -1.0	-1.0	-0.8	-0.7	-0.9	-0.7	C-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code -1.1 -1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark 1.6 1.9 Soil Type A or B 0.1 0.3	2.2	1.4	1.4	1.1	1.9		1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B 0.1 0.3 Soil Type E (1-3 stories) 0.2 0.2	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories) -0.3 -0.6	-0.9	-0.2	-0.4	0.2 NA	-0.1 -0.6	-0.4	0.0	0.0	-0.2 -0.3	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
	0.0		0.5	0.6				0.3	0.3	NA 0.2	-0.4	-0.5 0.3	-0.6 0.3	-0.2	NA 1.0
Minimum Score, Smin 1.1 0.9	0.7	0.5			0.5	0.5	0.3				0.2			0.2	1.0
Minimum Score, S _{MIN} 1.1 0.9			0.0	0.0	0.5	0.5	0.3	0.3	0.0	UIL		0.0	0.0		and the second second
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$: $\bigcirc_{4} \bigcirc_{2} \ge$	0,5	S			0.5	0.5						0.0	0.0		
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: 0.6>> EXTENT OF REVIEW	0,5	S	R HAZ	ARDS			ACT	ON RE	QUIR	RED					
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: 0.6 2 EXTENT OF REVIEW Exterior: 2 Partial All Sides Aerial		S DTHEF re There	R HAZ	ARDS s That T	rigger /		ACT Detaile	ON RE	EQUIR ural Eva	RED aluation		d?			
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: 0.65 EXTENT OF REVIEW Exterior: 27 Partial All Sides Aerial	O S	S DTHER re There etailed \$	R HAZ/ Hazarda	ARDS s That T Il Evalua	rigger A ation?	A	ACT Detaile	ON RE	EQUIR ural Eva wn FEM	RED aluation A buildin	g type or	d?			
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O. 6 >> EXTENT OF REVIEW Exterior: D Partial All Sides Aerial Interior: None Visible D Enterd	O S	S THER re There etailed \$	R HAZ/ Hazard Structura	ARDS s That T Il Evalua ntial (un	rigger A ation?	A	ACT Detaile	ON RE ed Struct es, unkno es, score	EQUIR ural Eva wn FEM less thar	RED aluation A buildin	g type or	d?			
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O. 6 >> EXTENT OF REVIEW Exterior: D Partial All Sides Interior: None Visible Enterd Drawings Reviewed: Yes No Soil Type Source: Geologic Hazards Source:	O S	DTHER re There etailed \$ Pound cut-of	R HAZ/ Hazarda	ARDS s That T I Evalua ntial (un n)	rigger A ation? less SL2	A >	ACT Detaile	ON RE ed Struct es, unkno es, score es, other h	EQUIR ural Eva wn FEM less thar	RED aluation A buildin	g type or	d?			
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O.6 EXTENT OF REVIEW Exterior: Draving Partial Interior: None Drawings Reviewed: Yes Soil Type Source:		THER re There etailed \$ Pound cut-of Falling building	A HAZA Hazarda Structura ding pote f, if know g hazarda ng	ARDS s That T Il Evalua ntial (uni n) s from ta	rigger A ation? less SL2	A > cent	ACT Detaile Ye Ye No	ON RE ed Struct es, unkno es, score es, other h	EQUIR ural Eva wn FEM less thar nazards	RED aluation A buildin n cut-off present	ig type or	d? r other bu	uilding	eck opol	
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O.6 EXTENT OF REVIEW Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Geologic Hazards Source: Contact Person: Tory L05 H		THER re There etailed \$ Pound cut-of Falling buildin Geolo	R HAZ/ Hazards Structura ding pote f, if know g hazards ng ngic haza	ARDS s That T Il Evalua ntial (un n) s from ta rds or So	rigger A ation? less S _{L2} iller adja bil Type	A > cent F	ACT Detaile Pre Pre Detaile	ON RE ed Struct es, unkno es, score es, other h	EQUIR ural Eva wn FEM less thar nazards ructural	RED aluation A buildin o cut-off present Evaluat	ig type or tion Rec	d? r other bu	uilding		
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1≥ SMIN: O.652 EXTENT OF REVIEW Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Geologic Hazards Source: Contact Person: Toroy L055 LEVEL 2 SCREENING PERFORMED? Level 2 Screening Contact Person		THER re There etailed S Pound cut-of Falling buildin Geolo Signif	HAZ/A Hazard: Structura ding pote f, if know g hazard: ng ngic haza icant dan	ARDS s That T il Evalua ntial (un n) s from ta rds or So nage/det	rigger A ation? less S _{L2} iller adja bil Type	A > cent F	ACT Detaile Yee Yee No Detaile	ON RE ad Struct as, unknov as, score as, other h ad Nonst as, nonstru b, nonstru	EQUIF ural Eva wn FEM ess thar nazards ructural uctural ha	RED aluation A buildin n cut-off present Evaluat azards i azards e	tion Rec dentified	d? r other bu ommeno that sho	uilding ded? (ch uld be ev	aluated	a
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1≥ SMIN: O.65 EXTENT OF REVIEW Exterior: D Partial All Sides Aerial Interior: None Visible D Enterd Drawings Reviewed: Yes No No Soil Type Source: Geologic Hazards Source: Contact Person: Tony L05 b LEVEL 2 SCREENING PERFORMED? Yes, Final Level 2 Score, St2 D No		THER re There etailed S Pound cut-of Falling buildin Geolo Signif	R HAZ/ Hazards Structura ding pote f, if know g hazards ng ngic haza	ARDS s That T il Evalua ntial (un n) s from ta rds or So nage/det	rigger A ation? less S _{L2} iller adja bil Type	A > cent F	ACT Detaile Yee No Detaile	ON RE ed Struct es, unkno es, score es, other h ed Nonst es, nonstru tailed eva	EQUIF ural Eva wn FEM ess thar hazards ructural uctural ha uluation i	RED aluation A buildin cut-off present Evaluat azards i azards es s not ne	tion Rec dentified xist that r cessary	d? r other bu ommeno that sho nay requ	uilding ded? (ch uld be ev ire mitigi		a
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O. S EXTENT OF REVIEW Exterior: D Partial All Sides Interior: None Visible Enter Drawings Reviewed: Yes No Soil Type Source: Geologic Hazards Source: Contact Person: 1000000000000000000000000000000000000		THER re There etailed S Pound cut-of Fallin buildin Geolo Signif the st	R HAZ/ Hazards Structura ding pote f, if know g hazards ng gic haza icant dan ructural s	ARDS s That T Il Evalua ntial (un n) s from ta rds or So nage/det system	rigger A ation? less SL2 aller adja bil Type lerioratio	A cent F nn to	ACT Detaile Ye Ye No Detaile	ON RE ed Struct es, unknous, score es, other h ed Nonst es, nonstru tailed eva o, no nons	EQUIR ural Eva wn FEM ess than hazards ructural uctural ha uluation i structura	RED aluation A buildin cut-off present Evaluat azards i azards es s not ne I hazard	tion Rec dentified xist that r cessary s identifie	d? r other bu ommeno that sho nay requ	uilding ded? (ch uld be ev ire mitigi	aluated	a
Minimum Score, SMIN 1.1 0.9 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O. S EXTENT OF REVIEW Exterior: Partial All Sides Aerial Interior: None Visible Entere Drawings Reviewed: Yes No Soil Type Source: Geologic Hazards Source: Contact Person: Tory (205) LEVEL 2 SCREENING PERFORMED? Yes, Final Level 2 Score, SL2 No Nonstructural hazards? Yes No Where information cannot be verified, Where information cannot be verified,		THER re There etailed S Pound cut-of Fallin buildin Geolo Signif the st	R HAZ/ Hazard: Structura ding pote f, if know g hazard: ng gic haza icant dan ructural s	ARDS s That T I Evalua ntial (un n) s from ta nage/det system e follow	rigger A ation? less SL2 iller adja bil Type terioratio	A cent F n to ST = Esti	ACT Detaile Ye Ye No Detaile	CON RE ed Struct es, unknows, score es, other ho ed Nonst ed Nonstru b, nonstru tailed eva b, no nons r unrelial	EQUIR ural Eva wn FEM ess thar nazards ructural hactural ha iluation i structura ole data	RED aluation A buildin n cut-off present Evaluat azards i azards e s not ne I hazard: <u>OR</u>	tion Rec dentified xist that r cessary s identifie	d? r other bu that sho may requ ed	uilding ded? (ch uld be ev ire mitigi	aluated	a

Structure 5, Building 2 Photographs



Re-entrant Corner (1 Wing of Structure)



Interior of Structure



Exterior of Structure



Interior of Structure



Gymnasium, Exposed View of Roof

Level 1 HIGH Seismicity

рнотс	OGRAPI	H				Oth Buil Use Lati Ss: Scro No. Tota Add	ding Na : H tude: 2 L tude: 3 Stories	Tree (so	e Grade	80	Belov 104 ear(s) Bi	.ongitu Sr: O D v Grade	de: 403 ate/Time	881 881 9 9 Yea	3382 727 15 @ Built: 1 9 Year:		EST
							Type:		strial y B	Office Warehou	ise	Residen) ntial, # Un]E [G its:]F D	overnmen	it	
		TT				-		Hard Rock	Avg Rock	Dens	e St	iff S	Soft Po	oor <i>If</i>	DNK, assi	ите Туре	D.
						Geo	logic H	azards:			the strength of the	Contraction of the		Contraction of the second	Surf. Ru	upt.: Yes/	No/DNR
							acency:			ounding		alling H	lazards fro	om Tallei	Adiacen	t Building	
25 7	-					Irre	gularitie	es:	Ve Ve PI	ertical (typ an (type)	be/severi re	ity) Sf	olit 1 Ntra	Nt C	Im	od er	
<i>LS 4</i>	1						erior Fa ards:	lling		nbraced (arapets ther:				avy Clade	ding or H	eavy Ver	ieer
SKE	тсн						Addition	al sketch	es or cor	nments o	n senara	ate nace					
		ASIC	sco	RE, MO	DIFIEF			And in case of the local division of the loc	A REPORT OF THE OWNER.	A REPORT OF A PARTY OF	CONTRACTOR OF TAXABLE	STATISTICS. STATISTICS.					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INE)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	(1.7)	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2 -0.7	-1.2	-1.2	-1.0 -0.6	-1.0 -0.6	-1.1 -0.7	-1.0	-0.8	-0.9	-1.0	-0.7 -0.4	-1.0 -0.6	-0.9	-0.9	-0.9	-0.7 -0.4	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	00	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1	-1.0	-0.9	2000-0	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	1.6 0.1	1.9	2.2	1.4	1.4 0.6	1.1 0.1	1.9	NA 0.5	1.9	2.1	NA 0.3	2.0 0.6	2.4	2.1 0.5	2.1	NA 0.2	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.4	0.0	-0.2	-0.3	-0.1	-0.1	0.5	0.3	0.3 -0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, S _{MIN}	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW	(8		20.	OTHER					an and	ION RI							
Interior: None None None None Soil Type Source: Geologic Hazards Source:	All Sides /isible No			Are Then Detailed Poun cut-o	Structura	ntial (un ntial (un	nless SL2	>	Ye Ye	ed Struct es, unkno es, score es, other i o	wn FEM less thar	A buildir 1 cut-off	ng type o		uilding		
Contact Person: Tony KC	ish			buildi	ing				1000 C	ed Nonst	ructural	Evalua	tion Rec	ommen	ded? (ch	eck onel	
LEVEL 2 SCREENING PERFO	ORME		lo	Signi Signi the s	ogic haza ficant dan tructural s	nage/de system	eterioratio	on to		es, nonstru o, nonstru etailed eva o, no non	uctural h ictural ha aluation i structura	nazards azards e is not ne il hazard	identified exist that i ecessary ds identifie	that sho may requ ed	uld be ev uire mitig	aluated	
Where information of					and the second second second							1011111 I III			and the second		
Legend: MRF = Moment-res BR = Braced frame	sting fram			einforced co hear wall	ncrete		URM INF TU = Tilt (= Unreinfo up	rced mase	onry infill	MH LM =	= Manufa = Light m	actured Ho etal	using F R	D = Flexib D = Rigid	le diaphra diaphragn	gm 1

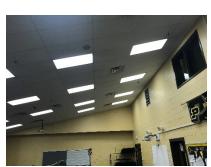
Structure 6, Building 3 Photographs



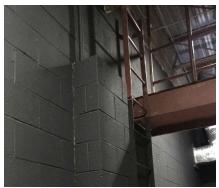
Exterior, Left of Foyer



Exterior, Right of Foyer



Vertical Irregularity



Masonry Covering Pipes



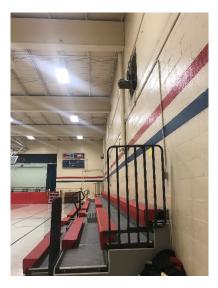
Exposed Roof

					1	Othe	er Ident	Dye	TN Visibi 7		IO TN)	2	Zip: <u>3</u>	8021	4	
РНОТС	GRAP	н				Use Latit Ss:	tude:	em 35,0 032	1711			ongitu	de:	89.3	888	34	
						Scre	ener(s)	: <u>C</u>	M			Da	ate/Tim	e: <u>51</u>	3.0	9 AN	1
						Tota		Area (so		41.	Below 78 (ear(s) B		:	-	Built: Year:	1950	EST
						Occ	upancy	: Ass	embly Istrial	Comme Office Wareho	rcial	Emer. S	ervices tial, #Ur		storic overnmer	□ Shelt nt	er
						Soil	Type:	Hard Rock	Avg Rock	Den	C C se St]D]E [oft P		NK DNK, ass	ите Туре	D.
		-				Geo	logic H	azards:		A DESCRIPTION OF TAXABLE PARTY.				NO/DNK	Surf. Ru	upt.: Yes/	No/IONR
					_	Adja	acency:		D Po	ounding	1	Falling H	azards fr	om Taller	Adjacen	t Building	
			F	-		Irreg	gularitie	IS:		ertical (ty an (type)	pe/sever	ity) S	plit ntra	level int ca)m	od r	
							erior Fal ards:	lling		arapets	Chimney	S	He	avy Clado pendages	ling or H		ieer
							MMENT										
							Ste	el.	col	im	151	ner	et	the	ve		
	ŀ.	-	1.											: ad		.1	,
					-	9										0.104	Uf-
		T				-	10	Jr	5 0	.20	ONC	bund	IN	indo)WS		
				_		-											
CKI	тсн						A	-1-1-1-1-1									
		ASIC	sco	RE, MO	DIFIEI				and the second se	the second s	RE S	COLOR DO NOT THE OWNER.		-	-	5.57 (7)	
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	SW)	INF) 1.2	1.0	1.2	INF) 0.9	1.1	1.0	(1.)	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9 -0.6	-0.9 -0.5	-0.9		-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.5	-0.5	1000	-0.4	-0.5 -0.6	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	8	-0.4	-0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3	53800	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	0.2	-0.2	0.0	0.0
Post-Benchmark Soil Type A or B	1.9 0.5	1.9 0.5	2.0	1 (C. 200) 1	1.1 0.3	1.1 0.4	1.5	NA 0.2	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	1000	-0.2	-0.2	-0.2	-0.1	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, Smin	0.7	0.7	0.7	-	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0	13	0	3							1						
EXTENT OF REVIEW				OTHER					ACT	ION R	EQUIF	RED					
Interior: INONE IN Drawings Reviewed: Yes I Soil Type Source:	Visible	Aer S Ent	rial tered		Structur ding pote ff, if know	al Evalu ential (ur vn)	nless SL2	>		es, unkni es, score	tural Evan own FEM less that hazards	A buildir n cut-off	ng type o	ed? or other bi	uilding		
Geologic Hazards Source: Contact Person: Miles Ho	llan	d	-	Fallin build	g hazard	is from ta	aller adja	acent	🗆 N	0		2					
			_	Geol	ogic haza									comment			
LEVEL 2 SCREENING PERFO Yes, Final Level 2 Score, SL2 Nonstructural hazards?			2001 - C		ficant da tructural		eterioratio	on to		o, nonstr tailed ev	ructural h uctural h aluation structura	azards e is not ne	exist that ecessary	d that sho may requ ied	uld be er uire mitig	valuated ation, but	ta
Where information of	annot b	e verifie	d, scr	eener sha	I note th	e follow	ing: E	ST = Est									
Legend: MRF = Moment-res BR = Braced frame		ne	RC = R	einforced co hear wall				= Unreinfo	orced mase		MH	= Manufa = Light me	ictured Ho	ousing Fl	D = Flexib	ole diaphra diaphragn	igm n

Structure 7, Building 3 Photographs



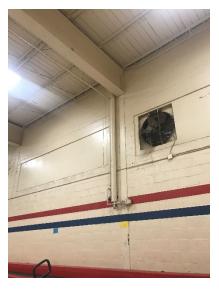
Added Reinforcement (1 of 2)



Gymnasium, Exposed Roof



Added Reinforcement (2 of 2)



Exposed Columns

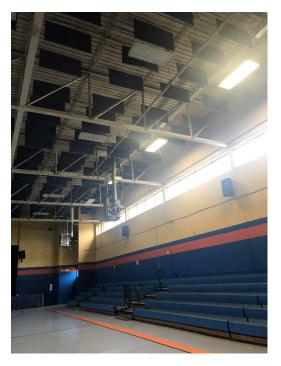
```
Level 1
VERY HIGH Seismicity
```

						Add	dress:	72 Fin	Po	plar	54.	1		Vin: 3	803	2	
						Oth	er Ident	tifiers:	8	1.1.	5			.ip:	003	-	
						1000	Iding Na		0								
						Use	E	lerv			Scr	loci	-				
								36.0	134	741		Longitu	de: 🔶	89,4	F181	89	
РНОТО	OGRAP	Н				Ss:	2:	49	~		-	S₁: Ŭ	,933	3			
): <u>C</u>				D	ate/Time	e: <u>51</u>	30	9:30	Am
								: Abov				w Grade	C is			19191	¥EST
								Area (s			170		the Li	1.100.000	e Year:	-	and t
T							ditions:				Year(s) B		unk:				
						Ucc	cupancy		embly ustrial ty	Comme Office Wareho		Emer. S Chool Resider		G	istoric overnme	☐ Sheil nt	ler
*N.T.S.						Soi	I Type:	Hard	□B Avg	Den	se St	liff S	oft P		NK DNK, ass	ume Type	D.
						Ger	ologic H	Rock	Rock	So So				lioil		upt.: Yes/	
							acency:			ounding						upt.: Yes/ It Building	
	F						gularitie		X V	ertical (ty	pe/sever	ity) SP	11+	teve	Im	ak	
			-			-					re		And the state of the second state	and the second second second second			
							erior Fa ards:	lling		arapets	Chimney	S	Hea	avy Clade	ding or H s	leavy Ver	neer
						CC	MMENT	S:	-	1.18.181 F					-		
							M	0.501	w	P	1 52	reel	n	nen	Ner	2	
							1.		1								
[]					1	1											
SYM																	
SKI	тсн							al sketch									
				RE, MO		RS, A	ND FI	NAL LI	EVEL	1 SCO	RE, S	1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	2.1	1.9	1.8	1.5	1.4	1.6	1.4	(1.2)	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9		-0.7 -0.4	-0.8	-0.7	-0.7	-0.7 -0.4	-0.8 -0.4	-0.6	-0.7 -0.4	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	1-1 12 12 12	-0.5	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark Soil Type A or B	1.9 0.5	1.9 0.5	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	552	0.3	-0.2	0.3	0.2	0.2	0.3 -0.2	0.1	0.3 -0.2	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.2	-0.1	NA	-0.1	-0.2	-0.2	0.0	-0.1 NA
Minimum Score, S _{MIN}	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	C).4	30	1.5)													
EXTENT OF REVIEW			T	OTHER					ACT	ION R	EQUIF	RED					
	All Sides /isible			Are Ther	e Hazard	Is That	Trigger /	4	Detaile	ed Struc	tural Eva	luation	Require	d?			
Drawings Reviewed: K Yes	No	PAL CIT	erea	Detailed					Ye Ye	es, unkno	wn FEM	A buildir	ig type or	other bu	uilding		
Soil Type Source:	202.	_		L Poun cut-o	ding pote ff, if know	vn) (ur	HESS SL2	>			less than hazards						
Geologic Hazards Source:	1.1			Fallin	g hazard	s from ta	aller adja	icent			nazalus	present					
Contact Person: Miles Har				buildi Geolo	ing ogic haza	rds or 9		F	Detaile	d Nons	tructural	Evalua	tion Rec	ommend	ded? (ch	eck one)	
LEVEL 2 SCREENING PERFO	RME	D?		Signi	ficant dar	mage/de	terioratio	on to	TY6	s, nonst	ructural h	azards i	dentified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2		X N	0	the s	tructural	system				o, nonstru	uctural ha aluation i	azards e	xist that r	may requ	ire mitig	ation, but	а
Nonstructural hazards? Yes			lo							o, no non	structura	l hazard	cessary s identifie	d b	DNK		
Where information of	annot b	e verifie	d, scre	ener shal	I note th	e follow	ing: ES	ST = Esti	mated o	r unrelia	ble data	OR	DNK = D	Not Kr	low		
Legend: MRF = Moment-resi BR = Braced frame	sting fram	le	RC = Re	einforced con near wall		1	JRM INF	= Unreinfo	rced masc	onry infill	MH :		ctured Hou			le diaphraç diaphragm	jm

Structure 8, Building 4 Photographs



Exterior views, Split Level



Steel Columns in Gym

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Level 1 VERY HIGH Seismicity

					1	Add	lress: _	32	00	Upp	ert	Finle		۵,			,
						Oth	er Ident	12y	ersbi	urg	TN		<u> </u>	Zip: <u>3</u>	302	4	_
							Iding Na	-	1		-						
									lle	sch	100	100		-			
							tude:	3610	347		1	ongitu	de: 🗂	-89,	434	919	
PHOTO	OGRAP	н				Ss:		453					,91	7			
							eener(s)	1					-	e: <u>51</u>		10A	
						Tota	al Floor			110	Belov Vear(s) B		: <u>U</u>		Built: Year:	1996	EST
							upancy		embly ustrial	Comme Office Wareho	ercial	Emer. S	ervices Itial, #U	and the second	storic overnmer	Shelt	er
	-		-			Soil	Type:	□A Hard	□B Avg	Den	C C	D C	E C	F Di Poor If	NK DNK, ass	ume Type	D.
						Geo	logic H	Rock	Rock	So So			and the second sec	Soil	Curf D	int · Voc	NICON
							acency:			ounding				rom Taller			-
	1						gularitie		Ve Ve		pe/sever	ity) Sy	1111	evel-	in	d	
	1						erior Fal ards:	ling		nbraced arapets	Chimney		He He	avy Clado pendages	ding or H		A STREET, STRE
				-			MMENT	· .	0	ther:							
		1				100		э.									
2																	
2	Ň			-													
		1			1	-											
				5	1												
	-			Г	1												
SK	ETCH	L	_								on separa	and the second se					
FEMA BUILDING TYPE Do Not			-	RE, MO			-							_			
Know	W1	W1A	W2	(MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8		1.4 -0.7	1.6 -0.8	1.4 -0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	1.0 -0.7	-0.7	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	-0.4	-0.4	-0.5	-0.4	-0.3	-0.4	-0.8	-0.3	-0.7	-0.7	0.1	-0.7	-0.6 -0.3	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7 -0.3	-0.6	201 H B 204	-0.5 -0.2	-0.6 -0.3	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	10 C C C C C C C C C C C C C C C C C C C	1.1	1.1	1.5	NA	-0.1 1.4	-0.2	0.0 NA	-0.2 1.5	-0.1	-0.2	-0.2	0.0 NA	0.0
Soil Type A or B	0.5	0.5	0.4		0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.2	-0.4		-0.2 -0.3	-0.2 NA	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7		0.5	0.5	0.5	0.5	-0.1	-0.3	-0.1	NA 0.2	-0.1	-0.2	-0.2	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	()	·9)=	20	3											0.0	VIL	1.0
EXTENT OF REVIEW				OTHE	R HAZ	ARDS	5		ACT	ION R	EQUIF	RED			100		
	All Sides			Are Ther				4	Detail	ed Struc	tural Eva	aluation	Require	ed?			
Drawings Reviewed: 🔀 Yes	Visible No	PAL EN	erea	Detailed					U Ye					or other bu	uilding		
Soil Type Source:				Pour cut-o	ff, if know		liess SL2	,			less that hazards						
Geologic Hazards Source: Contact Person: M:165 Hol	har A			🗌 Fallir	g hazard		aller adja	cent	Mar AND	9							
1 1100 101			-	build Geol	ing ogic haza	rds or S	Soil Type	F						comment			
LEVEL 2 SCREENING PERF	ORME	Contraction of the second		Signi	ficant dar	nage/de	eterioratio	on to		es, nonst	ructural h	nazards	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2		M N		the s	tructural	system				tailed ev	aluation	azards e is not ne	cessary	may requ	ure mitig	ation, but	a
Nonstructural hazards? Yes			250						No No	o, no nor	nstructura	I hazard	ls identifi	ed 🕅	DNK		
Where information of	cannot b	e verifie	d, scr	eener sha	I note th	e follow	ing: ES	GT = Esti	imated o	r unrelia	ble data	OR	DNK = D	o Not Kr	IOW		
Legend: MRF = Moment-res	isting fram		RC = R	einforced co hear wall	ncrete	I	URM INF : TU = Tilt u	= Unreinfo	orced maso	onry infill	MH	= Manufa = Light me	ctured Ho	using Fl	D = Flexib	le diaphrag	am

Structure 9, Building 5 Photographs



Exterior, 1 Wing Shown



Interior, Masonry



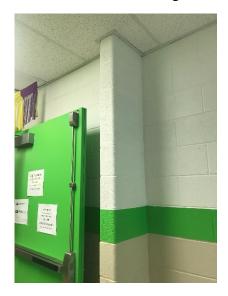
Interior, Masonry and Possibly Steel

	19722						1		rsb		field	d HV	JY	Zip: <u>3</u>	202	4		
						Buil	ding Na	me: _										
						Use	: <u>E</u>	lew	lent	ary	sur							
BUOT									1870	96				89,3	790	155	_	
PHOT	OGRAP	н						-174 1: CV	and the second se	-		S1: 0			2001	0201	AuA	
1 G														e: <u>51</u>				
						Tota		Area (s	· · · · · · · · · · · ·	7	Tear(s) B	1 100	:_0	-	' Built: ' Year:	20120	EST	
						Occ	upancy		embly ustrial ty	Comme Office Wareho	(Emer. S School Residen			storic overnmer	Shelt nt	er	
WALTE		-				Soil	Type:	A Hard	□B Avg	Den	C □ se St]E [NK DNK. ass	ume Type	D.	
*NT.S.	-					Rock Rock Soil Soil Soil Soil Geologic Hazards: Liquefaction: Yes/No/DNK Landslide: Yes/No/DNK Surf. Rupt.: Yes/No/DNK												
						************	logic H acency:			ction: Yes								
				~			gularitie				pe/sever		azards fr	om Taller	Adjacen	t Building		
NT				1/		Integ	Julainie		PI PI	an (type)) NOI	~113	SVS.	Re-	entr	enter	rmer	
					/		erior Fal ards:	lling			Chimney		He	avy Clado pendages	ling or H		and a balance of the local sectors in the	
1				1		CO	MMENT	S:					1	0				
	_			1			·A ·	ctu	$nl \leq$	stor	m s	Me	14 61	cre,				
							Li	ma	Sor	ry	ev	en	Whe	1921	colu	mns		
		_	_			1	-	500	inco	1		. 1						
Y	•				1	1		26.	. 30									
				-														
		_				_												
SK	ETCH	ARIC	800	DE MO	DIFIE						on separa							
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO	S2	S3	S4	S5	C1	C2	C3	.1 PC1	PC2	RM1	RM2	URM	МН	
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)	U.M.	mri	
Basic Score Severe Vertical Irregularity, VL1	2.1	1.9	1.8	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1	
Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9		-0.7 -0.4	-0.8	-0.7	-0.7	-0.7 -0.4	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7 -0.4	-0.7 -0.4	-0.6 -0.3	NA NA	
Plan Irregularity, PL1	-0.7	-0.7	-0.6	20 B B B B B B B B B B B B B B B B B B B	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA	
Pre-Code Post-Benchmark	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0	
Soil Type A or B	1.9 0.5	1.9 0.5	2.0	0.00	1.1	1.1	1.5	NA 0.2	1.4	1.7	NA	1.5	1.7	(1.6)	1.6	NA	0.5	
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	1987	-0.2	-0.2	-0.2	-0.1	0.2	0.3	0.1	0.3 -0.2	0.2	0.3	0.3	0.1	0.1	
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	-0.1 NA	
Minimum Score, S _{MIN}	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0	
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	(2	.33	20	1.3														
EXTENT OF REVIEW				OTHER					ACT	ION R	EQUIF	ED			-	-		
	All Sides			Are There				A	Detail	ed Struc	tural Eva	luation	Require	ed?				
	Visible No	Ent	ered	Detailed		100 TO 100	and the second second		Ye	es, unkno	wn FEM	A buildin	ig type o	r other bu	uilding			
Soil Type Source:				Poun			less SL2	>	🗌 🗌 Ye	es, score	less than	cut-off						
Geologic Hazards Source:				Fallin	ff, if know g hazard		aller adia	cent		es, other	hazards	present						
Contact Person: Miles H	ollan	4		buildi	ing		1200				tructural	Evaluat	tion Rev	ommend	led? (ch	ock onel		
LEVEL 2 SCREENING PERF	ORME	D2		Geolo	ogic haza	ards or S	oil Type	F						that sho				
Yes, Final Level 2 Score, SL2	ORIVIE	-			ficant da tructural		terioratio	on to		o, nonstr	uctural ha	azards e	xist that	may requ	ire mitia	ation, but	а	
Nonstructural hazards?						.,			de	tailed ev	aluation i	s not ne	cessarv					
		and the second	0.00								structura				DNK			
Where information																		
Legend: MRF = Moment-res BR = Braced frame	isting fram			einforced cor hear wall	ncrete		JRM INF : [U = Tilt u		rced maso	onry infill	MH	= Manufa Light me	ctured Ho	using Fl	D = Flexib D = Rigid	le diaphrag	m	

Structure 10, Building 6 Photographs



Left Front Exterior, 1 Wing Shown



Interior, Masonry

\bigcirc						Add	ress: _	1020	enil			157		(ip: 2	8020	2	
								ifiers:									
1 ¹							ding Na			1		de la composition				_	
						Use		1920- 36.14	222	97	-	ongitu	da: = 5	89.2	00 0	-10	
РНОТО	GRAP	4				Ss:		261				S1: C	182.6	9	910	14	
						Scre		: Cin	\wedge						60	9 AM	N
								: Above		2		w Grade	1	Year	Built:	20030	EST
							l Floor itions:	Area (sq		1.0	rear(s) B	805 Wilt		Code	Year:		
						Occ	upancy	: Asse Indu Utilit		Comme Office Wareho		Emer. S Chool Residen	ervices tial, #Ur		storic overnmen	☐ Shelt t	er
*N.T.S.	-	-	-			Soil	Туре:	Hard Book	B Avg	Dens	se S	tiff S	oft P	oor If	NK DNK, assi	ume Type	D.
	1	1		1		Geo	logic H	Rock	Rock Liquefac	Soi tion: Yes	A substitute and start			oil /No/DNK	Surf. Ri	ipt.: Yes/	No/DNK
			A	uditai	X		cency:		Pc							t Building	
< J grm	•	V		L	2		gularitie		Ve Ve	rtical (ty an (type)	pe/sever	ity) O	op si	etba	Alce	ever e	9
			1				erior Fal ards:	lling	Ur Pa	braced rapets	Chimney		Hea		ling or H	eavy Ver	
						0	MMENT	·C.	🗆 Ot		-	-					
							<10	s: e1 (cali	m	15	pre	2<80	1+1	hra	zah	at
			1				510									3	
				/		-											
$\langle \rangle$	\mathcal{L}			1													
SKE	TCH	1010)	<u> </u>				al sketche					-				
FEMA BUILDING TYPE Do Not	W1	W1A	SCO W2	RE, MO	S2	RS, AI					-			1			
Basic Score				(MRF)	(BR)	(LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8	-0.8	1.4 -0.7	1.6 -0.8	-0.7	(12) (0)	1.0 -0.7	1.2 -0.8	0.9 -0.6	-0.7	1.0 -0.7	1.1 -0.7	1.1 -0.7	0.9 -0.6	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	-0.4	-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.7	-0.7	-0.7	-0.6	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7 -0.3	-0.7 -0.3	-0.6		-0.5 -0.2	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	-0.3	2.0		-0.2	-0.3	-0.2	-0.1 NA	-0.1 1.4	-0.2 1.7	0.0 - NA	-0.2	-0.1 1.7	-0.2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	1.6	NA 0.1	0.5 0.1
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	10000000	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories) Minimum Score, S _{MIN}	-0.4	-0.4 0.7	-0.4		-0.3 0.5	NA 0.5	-0.3	-0.1 0.5	-0.1 0.3	-0.3	-0.1 0.3	NA 0.2	-0.1	-0.2 0.3	-0.2 0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	C)i13		,3)			0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW		13	Ì	OTHER	RHAZ	ARDS			ACT	ON R	EQUIF	RED		-		-	
Exterior: X Partial A	II Sides	Aer	ial	Are There Detailed				A					Require	d?			
Interior: None V Drawings Reviewed: Yes M	Interior: None Visible Stretere Drawings Reviewed: Yes No									ailed Structural Evaluation Required? Yes, unknown FEMA building type or other building							
Soil Type Source:	0			Poun	ding pote		less SL2	>	🔀 Ye	s, score	less tha	n cut-off			5		
Geologic Hazards Source:		_		Fallin	g hazard		aller adja	cent			hazards	present					
				buildi		an and and an	and the second s	- and a second second				Evolue					
Contact Person: Miles Hor	land	1							Detaile	a Nons	ructura	I EValua	tion Rec	ommend	led? (ch	eck onel	
			-	Geold	ogic haza	ards or S mage/de			🗆 Ye	s, nonst	ructural I	nazards i	dentified	that sho	led? (ch uld be ev	aluated	
LEVEL 2 SCREENING PERFO		D?	lo	Geolo	ogic haza	mage/de				s, nonsti , nonstru	ructural l	nazards i azards e	dentified xist that	that sho	uld be ev		
				Geolo	ogic haza ficant da	mage/de			Here Ye	s, nonstru , nonstru ailed ev	ructural l uctural h aluation	hazards i azards e is not ne	dentified xist that i cessary	that sho may requ	uld be ev ire mitiga	aluated	
LEVEL 2 SCREENING PERFO	RME		lo	Geolo Signi the si	ogic haza ficant da tructural	mage/de system	terioratio	on to	Ye No de No	s, nonstru , nonstru ailed ev , no non	ructural l uctural h aluation structura	hazards i azards e is not ne al hazard	dentified xist that i cessary s identifi	that sho may requ	uld be ev ire mitiga	aluated	

Structure 11, Building 7 Photographs



Exterior, 1 Wing Shown



Interior, Gymnasium, Arena-Style, Roof Exposed



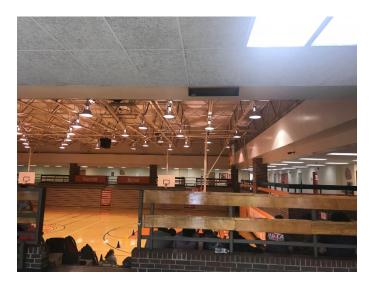
Interior Column (Steel Encased)

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

					1 45	Add	Iress:				0.ms			in: 2	805	n	
						Oth	er Identi	fiers:	12	XEN A	Sile	5		.ip: <u></u>	003	1	
							ding Na						_				-
						Use	1_:	Nid									
	924939						tude: 3		144	91	[ongitu	de: -	89.1	284	392	
PHOTO	OGRAP	н					2.		11.0	_			\$26	en	0.2		
						-	eener(s)			-				1000		DAM	
i ny produced						Tota	Stories: al Floor litions:		q. ft.):	9	Below G 61 Year(s) B		: _1	-	r Built: e Year:	1920	EST
						Occ	upancy		embly ustrial	Comme Office Wareho	ercial	Emer. S			istoric overnmer	Shelt Shelt	er
	-	T		-		Soil	Type:	□A Hard	B Avg	Der	C K	ĴD [JE C	F D	NK DNK, ass	ume Type	D.
						Geo	logic Ha	Rock	Rock Liquefac	So Stion: Ye	s/No/QNP				Surf. Ri	upt.: Yes/	NorDNK
1							acency:			ounding	the second s					t Building	
]					Irre	gularitie	s:		ertical (ty lan (type	/pe/sever)	ity) O	op se	ethan	14/5	avare	3
							erior Fal ards:	ling	U	nbraced arapets	Chimney	S		avy Clado endages		eavy Ver	ieer
						CO	MMENT	S:		-				1			
						\$	0	ne	.m	en	thr	51	pres	ent	Г		
												1	1	1			
-				1		p	WW	<i>NSO</i>	nr	Y -	thr	20,6	hoi	Л			
		-		1						•		-	2				
		_				_											
						-											
SK	ETCH										on separa						
FEMA BUILDING TYPE Do Not	W1	W1A	SCO W2	RE, MC	S2	S3	ND FIN	S5	EVEL		C3	PC1	DOG				
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8	1.5 -0.8	1.4 -0.7	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9	100 B 100	-0.7	-0.8 -0.5	-0.7	-0.7 -0.3	-0.7	-0.8	-0.0	-0.7 -0.4	-0.7	-0.7	-0.7	-0.6 -0.3	NA NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	10364	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code Post-Benchmark	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	1.9 0.5	1.9 0.5	2.0	1.0	1.1	1.1	1.5	NA 0.2	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	and the second	-0.2	-0.2	-0.2	-0.1	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	-0.1 NA
Minimum Score, S _{MIN}	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	(0)	13)	50	.3					_								
EXTENT OF REVIEW		_			RHAZ				a designed to be		EQUIF	ON THE OWNER					
Exterior: Partial Interior: None		ards That Trigger A Detailed Structural Evaluation Required?															
Drawings Reviewed: 🗌 Yes 🕅	No	Ent	ereu				analana .		Ye	es, unkn	own FEM	A buildir	ng type o	r other bi	uilding		
Soil Type Source:	and a				iding pote		IIESS SL2	,			hazards						
Geologic Hazards Source:		1		G Fallir	ng hazard		aller adja	cent		ó	nazalus	hiesent					
				build Geol		c hazards or Soil Type F Detailed Nonstructural Evaluation Recommended? (check one)											
LEVEL 2 SCREENING PERF	ORME	D?		Signi	ficant dan	nage/de				es, nons	tructural h	nazards	identified	that sho	uld be ev	valuated	
Yes, Final Level 2 Score, SL2	_		lo			ctural system No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary											
Nonstructural hazards? Yes			lo							o, no noi	nstructura	l hazard	s identifie	ed K	DNK		
Where information	cannot b	e verifie	d, scr	eener sha	Il note the	e follow	ing; ES	T = Esti									
Legend: MRF = Moment-res BR = Braced frame		10	RC = R	einforced co		1	URM INF =	Unreinfo			MH	= Manufa	ctured Ho	is secondarian	and the second	le diaphra diaphragm	gm
Drt = Draceu frame			OW = S	hear wall			TU = Tilt u	D			LM =	= Light me	atal	R	D = Rigid	dianhrann	

Structure 12, Building 8 Photographs



Interior, Gymnasium, Arena-Style



Interior, Exposed Concrete Column

					1	Oth	er Ident	ifiers:	rim	lege ble	St.	S	Z	ip: 3	8250		
							ding Na	ervi	ente	w <	cho	10			-		
								36,7					de:{	9.1	841	00	
PHOTO	GRAP	н				Ss:	1.9	92				S1: 0	:72				
						Scr	eener(s)	: Civ	1			Di	ate/Time	: 5	160	IOAW	\wedge
						Tota		Area (so	q. ft.):	27	Belov 96 (ear(s) B	v Grade 9 uilt:	: _	Yea Code	r Built:) e Year:	959	EST
						Occ	upancy		embly Istrial Iy	Comme Office Wareho	(Emer. S School Residen		State State	istoric overnmer	C Shelt nt	er
*NT,S.						Soil	Туре:	Hard Rock	Avg Rock	Den So	se St	iff S	oft P		NK DNK, ass	ume Type	D.
				_		Geo	logic H	azards:	Liquefac	tion: Yes	s/No/DNk	C Lands	lide: Yes	/No/DNK	Surf. R	upt.: Yes/I	No/DNK
			-			Adj	acency:			ounding			and all the last			t Building	
		-				Irre	gularitie	IS:		ertical (ty an (type)	pe/severi		off (
							erior Fa ards:	lling	D Pa	nbraced arapets ther:	Chimney		Hea	and a state of the	ding or H	eavy Ven	neer
						CO	MMENT	ipple	1 1-16	11 0	were	unt-	7501	45	tor	i	
					23		10	mr.	role	in in	1100	≤ 1	nt	ACO	Mark	t and	V
	L		_	T	1	•	Sta	s: ipple inc zel	bec	ms	on	gr.	bund	Als	SV		.1
SKI	тсн						Addition	al sketch	es or cor	nments o	on separa	ite page					
	В	ASIC	sco	RE, MO	DIFIEF												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	(12)	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9 -0.6	-0.9 -0.5	-0.9		-0.7	-0.8 -0.5	-0.7 -0.4	-0.7	-0.7 -0.4	-0.8 -0.4	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	0.4	-0.4	-0.4	-0.3 -0.3	-0.4 -0.5	-0.4	-0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3	12.36	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark Soil Type A or B	1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.5	0.5	0.4	0.3	0.3	0.4 -0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.2	-0.1	-0.1	-0.2	0.0	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, S _{MIN}	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.2	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0	36	2.3														
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIR	ED		1400	-		
		Aer		Are Ther				Ą	Detail	ed Struc	tural Eva	luation	Require	d?			
Interior: None	/isible	Ent	ered	Detailed				1.3.6			wn FEM				uilding		
Drawings Reviewed: Yes Soil Type Source:	Soil Type Source:							>	🔁 Ye	es, score	less than	n cut-off	3 9900		anding		- 3
	Cut-0									es, other	hazards	present					
Contact Person: Miles Fb	ilan	X		buildi			and a new particular	10000	Detail		tructure	Evelue	tion D-		1.10		
	Autorener		-	Geol	ogic haza	c hazards or Soil Type F											
LEVEL 2 SCREENING PERFO	JRME			Signi	ficant dan	nt damage/deterioration to Yes, nonstructural hazards identified that should be evaluated tural system											
Yes, Final Level 2 Score, SL2	-	N		the S	uucturals	ctural system No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary							d				
Nonstructural hazards? Yes								24		o, no nor	structura	I hazard	s identifi		DNK		
Where information of	annot b	e verifie	d, scr	eener shal	I note the	follow	ing: E	ST = Esti							wor		
Legend: MRF = Moment-resi																	

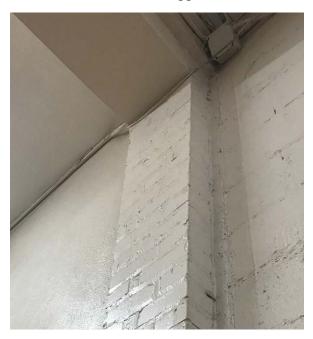
Structure 13, Building 9 Photographs



Exterior, Cripple Wall



Interior, Exposed Steel Column



Interior, Encased Steel Column



Encased Steel Members

PHOTO	Oth Buil Use Lati Ss: Scr No. Tota Addo Occ Soil Geo Adji	eener(s) Stories: al Floor litions: cupancy	ifiers: me: evvv Area (so Area (so))) Area (so Area (so)) Area (so Area (so)) Area (so)) Area (so)) Area (so) Area (so)) Area (so) Area (so)) Area (so) Area (so)) Area (so) Area (so)) Area (so) Area (so)) Area (so)) Ar	// Content of the second secon	Terrical (ty	Belov Belov Cear(s) B rcial use C X See St St NO/ON D I ppe/sever	ongitu Sr: 0 v Grade uilt: 1 Emer. S School Residen D C Sill S D Lands Falling H ity)	de: de:	e: <u>5</u> Year Code (CS1. Hi Ganits: F D	G 10 r Built: e Year:) storic overnmer NK DNK, ass Surf. Ru Adjacen	20120 Con20 Shelt ume Type	er					
						Haz	erior Fal ards:	-	Ο υ	nbraced arapets	Chimney		He	avy Clado pendages	ding or H	eavy Ven	eer
new District Hus	form	5	1			co E	at;	r	ted pour	10:50 1011 1011 1453	nv Nall gise	Kruce Sues	iy t :- :	0 "m 39.2	1 iddi 59 481	e" s	
SK	ETCH	ASIC	800	RE, MO	DIEIEI		Addition						-				
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3	-1 PC1 (TU)	PC2	RM1 (FD)	RM2	URM	МН
Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN}	2.1 -0.9 -0.6 -0.7 -0.3 1.9 0.5 0.0 -0.4 0.7	1.9 -0.9 -0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 -0.4	1.8 -0.9 -0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4	-0.8 -0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 -0.3	1.4 -0.7 -0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5	1.6 -0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5	SW) 1.4 -0.7 -0.4 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	INF) 1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	1.0 -0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3	1.2 -0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3	INF) 0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3	1.1 -0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2	1.0 -0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2	1.1 -0.7 -0.4 -0.2 -0.2 1.6 0.3 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2	(RD) 1.1 -0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0 0.0	1.1 NA NA 0.0 0.5 0.1 -0.1 NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	(2	3)	20	.3		-									0.0	0.2	1.0
EXTENT OF REVIEW Exterior: Partial Interior: None Interior: Yes Interior: Soll Type Source: Geologic Hazards Source: Contact Person: Mices	e Hazard Structur ding pote	zards from taller adjacent 🕅 No															
LEVEL 2 SCREENING PERFO	mage/de system	oil Type terioratio	n to		es, nonstru b, nonstru tailed ev b, no non	ructural h uctural ha aluation i structura	azards i azards e s not ne l hazard	identified xist that cessary s identifi		uld be ev ire mitiga	aluated	а					
Legend: MRF = Moment-res BR = Braced frame	isting fram	ie I	RC = R	einforced cor hear wall		1	JRM INF = TU = Tilt u	Unreinfo			MH :		ctured Ho	(Contraction of the second		le diaphrag diaphragm	Im

Structure 14, Building 10 Photographs



Front Right Exterior, 1 Wing Shown



Interior Connection to Older Building



Masonry Walls

							lress: _	NO	1 N 2 mbe	. Yo	TN	t.	Z	ip: 3	1208	9	
							er ident Iding Na	ifiers:	12	84.5	-		-	-			
									nen	terry	SU	1000		-			-
						Lati		about	197	920		ongitu	de: 🔁	SP.L	EXP	080	
PHOTO	DGRAPH	1				Ss:			10),79			0	
10.4	a he a h					and the second		:_01					_	-		sophin	
						Tota		Area (so	q. ft.): _	1580		v Grade	201	Code	Built: Year:	19780	EST
middle						Occ	upancy		embly istrial ty	Comme Office Wareho	(Emer. S School Residen	ervices tial, #Un		storic overnmen	□ Shelt nt	er
1000 C				F	-	Soil	Туре:	Hard Rock	Avg Rock	Den So	se St	iff S	oft Po		NK DNK, assi	ume Type	D.
	_			T		Geo	logic H	azards:	Liquefac	tion: Yes	No/DNK	**********			Surf. Ru	upt.: Yes/I	No/DNK
				10	6	Adj	acency:		and the second of	ounding						t Building	
				10		Irre	gularitie	s:		ertical (ty an (type)	pe/severi	ity)Sla	ping	517	elw	-ON	
							erior Fal ards:	ling		arapets	Chimney	S		avy Clado endages		eavy Ven	ieer
				1		CO	MMENT	S:	,	1 .	,			1 4			
(new)	-		-	/		-	160	nif	ecte	201 1:	y h ig is	ally	ray	p"	new		
			-			-	-1	no I	pau	rdir	ia is	KURS	S				
1 1		ن ــــــــــــــــــــــــــــــــــــ		-	1	-			1	1	1	11)			ent
CI=othe	a for sform	ws r			/	1	·Ste Lat	:36	me	721	2845 O	th	9.3	- 39	.26	040	2
SKI	ЕТСН						Addition	al sketch	es or cor	nments o	on separa	ite page	-				
			-	RE, MO			-	-		-							
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	\$3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8 -0.9	1.5 -0.8	1.4 -0.7	1.6 -0.8	-0.7	1.2	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	1.0 -0.7	-0.7	1.1 -0.7	0.9 -0.6	1.1 NA
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	100	-0.4	-0.5	-0.4	0.3	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3	NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7 -0.3	-0.6	S	-0.5 -0.2	-0.6 -0.3	-0.4	-0.4	-0.4 -0.1	-0.5	-0.3 0.0	-0.5 -0.2	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	-0.2 1.6	0.0 NA	0.0
Soil Type A or B Soil Type E (1-3 stories)	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	0.0	-0.2 -0.4	-0.4		-0.2 -0.3	-0.2 NA	-0.2	-0.1	-0.1	-0.2	0.0 -0.1	-0.2 NA	-0.1	-0.2	-0.2 -0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0	.8/2	0,	5													
EXTENT OF REVIEW		5		OTHER	RHAZ	ARDS	5		ACT	ION R	EQUIR	RED	-			1	
											tural Eva						
Drawings Reviewed: 🗌 Yes 🛛 🙀		ctural Evaluation? Yes, unknown FEMA building type or other building potential (unless SL2 > Yes, score less than cut-off															
Soil Type Source:	and the second	and the		cut-o	ff, if know	n)			1 Ye	es, other	hazards						
Geologic Hazards Source: Contact Person: Mikes Ho	Iland			Fallin buildi	g hazard	s from t	aller adja	cent		0							
tarbox 10			-	Geold	ogic haza	rds or S	Soil Type	F			tructural						
	DRMEI				ficant dar tructural s		eterioratio	on to		es, nonst	ructural h uctural ha	azards i	identified	that sho	uld be ev	aluated	•
Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes				ule S	aucturals	system			de	tailed ev	aluation i	s not ne	cessary			adon, Dul	a
	annett	_		anar-t 1	I made th						structura				DNK		
Where information of Legend: MRF = Moment-res				ener shall einforced con													
BR = Braced frame	ouny itam			near wall	ICI E (B		TU = Tilt u	= Unreinfo p	rced maso	onry Infill	MH =	Manufa Light me	ctured Hore	using FI	D = Flexib	le diaphrag diaphragm	gm

Structure 15, Building 11 Photographs



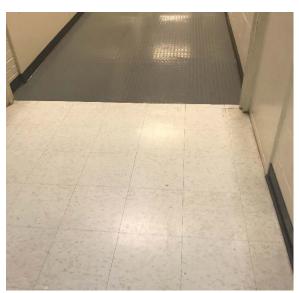
Exterior, Outside Cafeteria



Interior, Split Level, Exiting Cafeteria



Interior, Cafeteria



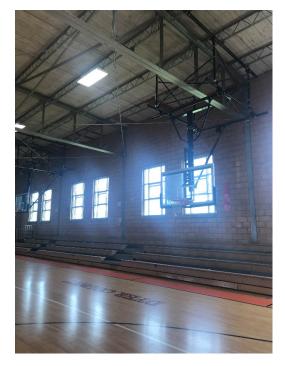
Connection to New Hallway to Newer Building

	1.00				Add	ress:	401	K	N. Y	NF	St	-				-
						-		when	m	TN	,	7	ip: 3	8050	1	
					Oth	er Identi	fiers:			110					1	
						ding Na										
					Use	EL	em	enta	NS	scho	p la	ymi	105 V	m		
					Lati		567		app			de:		a ros	300	
PHOTOGRA	н				Ss:	_	163					2,74			1	
					_		: <u>C</u> N				D	ate/Time	: 5	6 6	0/0/3	oam
							Abov Area (so	ą. ft.):	134	20	w Grade	:		r Built: Year:	19705	EST
					Add	itions:	Ø N	one 🗌	Yes, Y	(ear(s) B	uilt: _					
(middle)					Occ	upancy		embly Istrial	Comme Office Wareho		Emer. S School Residen	ervices tial, #Un		storic overnmer	C Shelt nt	er
			terret.	100	Soil	Type:	Hard	□B Avg	Den	se St	liff S	oft Po	oor If	NK DNK, ass	ume Type	D.
			1	T.M.S.	Geo	loaic H	Rock	Rock Liquefac	Soi tion: Yes					Surf P	upt.: Yes/	MODIE
			6			acency:			ounding				-		t Building	
			Pia)		gularitie	s:	Ve		pe/sever		02010311		Aujacen	Coulding	
						erior Fal ards:	ling	Ur 🗌	nbraced arapets	Chimney	S	Hea			eavy Ven	eer
			~		CO	MMENT	S:	_	2/DOMAN							
new			/		-	·St	eel	col	:5	W	N	iood ba	de	skiv	19	
				1												
[]=otherf	orms	1			×L	ati	36	111	189	21	ong	8	51.0	5993	0	
THUS P.	m		\searrow	/							•					
SKETCH							al sketch									
	BASIC S	sco	RE, MO	DIFIE	RS, AI	ND FIN	AL LE	EVEL	I SCO	RE, S	L1					
FEMA BUILDING TYPE Do Not W1 Know	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score 2.1 Severe Vertical Irregularity, VL1 -0.9	1.9 -0.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1 -0.6	-0.9	-0.9 -0.5		-0.7	-0.8 -0.5	-0.7	-0.7 -0.3	-0.7 -0.4	-0.8 -0.4	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6 -0.3	NA NA
Plan Irregularity, PL1 -0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code -0.3 Post-Benchmark 1.9	-0.3	-0.3	10 10 10 10 10 10 10 10 10 10 10 10 10 1	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark 1.9 Soil Type A or B 0.5	1.9 0.5	2.0 0.4	1.0	1.1	1.1	1.5	NA 0.2	1.4 0.2	1.7 0.3	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories) 0.0	-0.2	-0.4	16536	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories) -0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, SMIN 0,7 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: (1)	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW		T	OTHER					ACT		EQUIF	DED				-	-
	s 🔲 Aeri	al	Are There					1.1				Require	42			
Interior: None Visible		ral Evalu			- 765 Starting				ng type of		uilding					
Drawings Reviewed: 🗌 Yes 🛛 🛱 No Soil Type Source:		ential (ur	less SL2	>	Ye Ye	s, score	less that	n cut-off	ig type of	outer bi	uluing					
Geologic Hazards Source:	1	-		ff, if kno		allor adia	cont	Ye		hazards	present					
Contact Person: Miles Hollan	d		buildi		ds from ta	aller adja	cent	Dotail		tructure	Evelue	tion De-		1.10 ()		
LEVEL 2 SCREENING PERFORM		-	Geolo	ogic haz	ards or S	oil Type	F					tion Rec identified			eck one)	
Yes, Final Level 2 Score, SL2				ficant da tructural	mage/de system	terioratio	in to		o, nonstri	uctural ha	azards e	xist that I	nay real	uiu be ev ire mitia	aluated ation, but	а
			010 01		5)50011			1742 USA	Section 2010	and the second second	100000000000000000000000000000000000000					
Nonstructural hazards? Yes									tailed ev				. ~	d		
Nonstructural hazards? Yes Where information cannot		0	onor choi	I note ti	ha fallow	ing: Ef	T- F-"		, no non	structura	al hazard	ls identifie				

Structure 16, Building 12 Photographs



Exterior, Ceiling Heights Consistent



Interior, Masonry and Steel Exposed



Interior, Concrete Pillars in Half-Basement Level

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

			11			Add	dress: _		0 4			5				,	
						Oth	er Ident		adfi	JAN J	IN	-	Z	lip: <u>3</u>	831	6	
						10000000	Iding Na		11	-	10000						
									ner	Atar	V SC	has	1				
						Lati	itude:	361	079	899			ide: -	.88.	813	194	
РНОТ	OGRAP	н				Ss:		597					1379				
						Scr	eener(s)): _CI	M			D	ate/Time	: 5	1210	@ 9AI	M
						No.	Stories	: Abov	ve Grade	e:	Belov	w Grade	: ()	Yea	r Built:	1950 1	EST
							al Floor ditions:	Area (s		Yes,	5420 (ear(s) B		95	Code	e Year:	101	
						Occ	cupancy		embly ustrial	Comme Office Wareho	rcial	Emer. S		G	istoric overnme	Shelt Shelt	er
						Soi	l Type:	Hard Rock	□B Avg Rock	Den So	se S	tiff S	Soft P		NK DNK, ass	sume Type	D.
	1	m				Geo	ologic H	azards:	Liquefac	ction: Ye	s/No/DN	K Lands	lide: Yes	/No/DNK	Surf. R	upt.: Yes/	No/DNK
3 mye	1	0		6		Adj	acency:		P	ounding		Falling H	lazards fr	om Taller	r Adjacer	nt Building	
3			99			Irre	gularitie	s:		ertical (ty lan (type)			itrar	H CA	90106	<i>s</i>	_
						Ext	erior Fa	lling		nbraced						leavy Ver	eer
	-	-	ANDIA	11	11	Haz	ards:			arapets			App				
			-	11	51	CC	MMENT	'S:		. 1		11	M .		1	1	
			1	south (V	1	Ply	NO	sd	(ei	line	1 4	ilexi	ble	dia	phro	(qur)
			6-		-		100	10	mag	< 10	r i	SIC	· do	ntil	Cind	phro	U
						-	10	6	110	-2 U	YU	015	INE	1/11/	FICO	(
				31		-	"Li	Keli	y ur	cm		,		,			
						- '	pou	inau	ny	pot	ent	-ia)	W	by	ildir	y@	
SK	ETCH	4.010		DE NO	DIFIE				les or cor						-		
FEMA BUILDING TYPE Do Not	W1	WIA	W2	RE, MO	S2	S3	S4	S5	C1		RE, S		DC2	DIM	DHO		
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	INF) 1.2	1.6	1.4	1.7	1.7	(1.)	1.5
Severe Vertical Irregularity, VL1	-1.2	-1.2	-1.2	C	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.7	-0.7	-0.7		-0.6 -0.7	-0.7 -0.9	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.4	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA -0.1
Post-Benchmark	1.6	1.9	2.2	1	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B Soil Type E (1-3 stories)	0.1	0.3	0.5		0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (>3 stories)	-0.3	0.2	0.1	-0.2	-0.4	0.2 NA	-0.1	-0.4	0.0	0.0	-0.2	-0.3 NA	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, S _{MIN}	1.1	200	0.7		0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	: (0	·6)	20	.2													
EXTENT OF REVIEW				OTHER	RHAZ	ARDS	5		ACT	ION R	EQUIF	RED					
									Detailed Structural Evaluation Required?								
Drawings Reviewed: Yes	No	Ent	ered	Detailed					U Ye	es, unkno	wn FEM	IA buildir	ng type o	r other bi	uilding		
Soil Type Source:				Pounding potential (unless SL2 > cut-off, if known)						es, score							
Geologic Hazards Source:				Fallin	ig hazard		aller adja	cent	Ye Ye	o 0	r hazards present						
Contact Person: Larry	_			build	ing						tructura	l Evalua	tion Rec	ommen	ded? (c)	neck one)	
LEVEL 2 SCREENING PERF	ORME	D?					Soil Type eterioratio			es, nonst	ructural h	nazards i	identified	that sho	uld be e	valuated	
Yes, Final Level 2 Score, SL2		M N	。		tructural					o, nonstr	uctural ha	azards e	xist that r	may requ	ire mitig	ation, but	а
Nonstructural hazards? Ves										etailed ev			cessary Is identifie	d h	DNK		
Where information	cannot b	e verifie	d, scr	eener shal	I note th	e follow	ving: Es	ST = Est								-	
Legend: MRF = Moment-re:	sisting fram	ie l	RC = R	einforced co					orced maso				ctured Hou			ble diaphrag	m
BR = Braced frame)			hear wall			TU = Tilt u	p		.,	LM =	= Light me	etal		D = Rigid	diaphragm	4111

Structure 17, Building 13 Photographs



Exterior, Numerous Filled-In Windows Interior, Joint Between This and New Addition



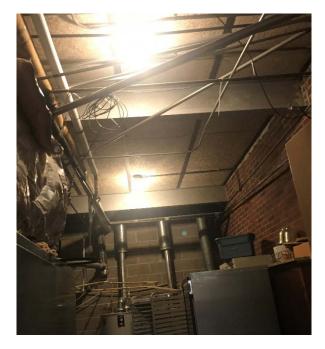
Interior, Openings Filled in with Bricks

РНОТС	DGRAP	н				Othe Build Use: Latif Ss: Scre No. Tota Add Occ	er Ident ding Na Eude:	ifiers: me: : Area (sq 	e Grade f. ft.): pone F strial	ary c 3	Belov Gear(s) Br rcial	ongitue Sr: O Da v Grade uilt: Emer. Sr School Residen	de: .379 ate/Time : ervices	881 Year Code 19 Hi Gaits:	Built: Year: 75 storic overnmen	324 94 955 □ 2014 0 Shelte t] EST
								Hard Rock	Avg Rock	Dens				oor <i>If I</i> oil	DNK, assi	ime Type	D.
	150			1		Geo	logic H	azards:	Liquefac	tion: Yes	/No/DNM	(Lands	lide: Yes/	No/DNK	Surf. Ru	pt.: Yes/N	No/DNK
Sym D TA	1		G		-	Adja	cency:		D Po	ounding			azards fro				
3 19							Jularitie	s:		ertical (typan (type)	pe/sever	ity) S	plit	leve	21-1	nod	
							erior Fa ards:	lling	🗆 Ur	nbraced arapets	Chimney	S		vy Clado endages	-	eavy Ven	eer
	Doper	d		1	_		MMENT			1				1			
	raft	reve		9		T	Ca	fete	nia	her	re						
	raithere 9						Ste	ele	5106	ed	Ceil	ing	ore	v Co	rfete	eri a	
1		Sfor					Ho	zel 1	se h	ms	PC0	153	m	ron	V V		
	2414	310				à	Na	old c	viki	der ny	pa	indi	ngi	but	Not	an	
SK	ETCH		1	1		-		al sketche		9							
		-	-	RE, MO	-	-		NAL LE	EVEL 1	I SCO	RE, S	L1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	3.6	3.2 -1.2	2.9 -1.2		2.0 -1.0	2.6 -1.1	2.0 -1.0	-0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	1.7	1.7 -0.9	1.0 -0.7	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA NA
Plan Irregularity, PL1 Pre-Code	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7 -0.6	-0.6	-0.6 -0.4	-0.8 -0.7	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark	1.6	1.9	2.2		1.4	1.1	1.9	NA	-0.4	-0.7	-0.1 NA	-0.5	-0.3	-0.5	-0.5	0.0 NA	-0.1 1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2 NA	-0.1	-0.4	0.0	0.0	-0.2	-0.3 NA	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	J.	.0)3	20).5													
EXTENT OF REVIEW				OTHE	RHAZ	ARDS	-		ACT	ION R	EQUIF	RED					
xterior: Partial All Sides Aerial Are There Haza								A	Detaile	ed Struc	tural Eva	aluation	Require	d?			
Drawings Reviewed: Ves No									Ye	es, unkno	wn FEM	IA buildir	ng type o	other bu	uilding		
Soil Type Source:	oil Type Source: cut-off, if kn										less that hazards						
Geologic Hazards Source:	eologic Hazards Source: Eralling haza							acent)							
Cont	ogic haza	ards or S	oil Type	F					tion Rec								
LEVEL 2 SCREENING PERF	ORME			Signi	ficant da	mage/de	terioratio	on to		s, nonst	ructural h	nazards i	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, S _{L2} Nonstructural hazards? Yes	_			the s	tructural	system			de	tailed ev	aluation	is not ne	cessary			adon, DUC	d
			10										s identifie		DNK		
Where information Legend: MRF = Moment-res				eener sha				ST = Estin = Unreinfor								a dl1	
BR = Braced frame	- g non			hear wall		-	U = Tilt u		oou mase	any num	IM-	= Manuta = Light me	ctured Ho	using Fl	D = Flexib	le diaphrag	Jm

Structure 18, Building 13 Photographs



Interior, Connection Between This Structure and Addition

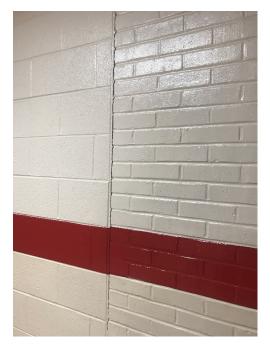


Interior, Mechanical Room, Exposed Ceiling

۱

РНОТ	PHOTOGRAPH								e Grade and the re Grade ft.): one strial ty	10/2 98	TN SU Below 66 Gear(s) Bi rcial	ongitu Sr: v Grade uilt: School-	de:	88↓ 9 Year Code 195	Built: Year: - 5 , 20	344 9 Ali 1975 c 514 514	EST
						Soil	Туре:	Hard Rock	Avg Rock	Den: Soi	se St	iff S	oft Po		N K DNK, assi	ume Type	D.
	1			1		Geo	logic H	azards:	Liquefac	tion: Yes	No/DNK				Surf. Ru	ipt.: Yes/I	NOIDNE
Sim	1		0		7		acency:			ounding		the second s	azards fro	and the second second second			and the second
3 2			0			Irre	gularitie	s:		ertical (ty an (type)	pe/severi	ity) _					
	1		_	1	1	Haz	erior Fal ards:			arapets	Chimney		🗆 App			eavy Ven	ieer
				s: ind													
51	ETCH	ASIC	sco	RE, MO	DIFIER			al sketch						-	-		
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	\$3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	SW) 2.0		1.5	2.0	INF) 1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1	-1.2	-1.2	-1.2	2 - 1 (Japper)	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.7	-0.7	-0.7		-0.6	-0.7 -0.9	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.6	-0.6 -0.4	-0.8 -0.7	-0.5 -0.1	-0.7	-0.6	-0.7	-0.7	-0.4 0.0	NA -0.1
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA NA	1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4 -0.6	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	1.1	0.9	-0.3		0.5	NA 0.6	-0.6	-0.4	-0.5 0.3	-0.7	-0.3 0.3	NA 0.2	-0.4	-0.5	-0.6 0.3	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	. 0	D	T.	SP	0,5	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.3	0.2	1.0
EXTENT OF REVIEW				OTHE		ARDS			ACT	ON R	EQUIR	RED	100		-		-
Exterior: Interior: Drawings Reviewed: Soil Type Source: Geologic Hazards Source:	e Hazard Structura ding pote ff, if know g hazard	al Evalu ential (ur vn)	nless SL2	>		es, unkno es, score es, other		A buildir n cut-off	Require ng type or		uilding						
Contact Person:				Fallir build		a num (and duja	UCIII	19.00 - 20.00		here a from the	Fuel					
LEVEL 2 SCREENING PERF Yes, Final Level 2 Score, SL2 Nonstructural hazards?			lo	Geole Signi the s	ogic haza ficant dar tructural s	mage/de system	eterioratio	on to		es, nonst o, nonstru tailed ev o, no non	ructural h uctural ha aluation i structura	hazards i azards e is not ne il hazard	s identifie	that sho may requ	uld be ev iire mitiga	aluated	
Where information	cannot k	e verifie	d, scr	eener sha	I note th	e follow	ing: E	ST = Esti	mated o	r unrelia	ble data	OR	DNK = D	o Not Kr	wor		122
Legend: MRF = Moment-re BR = Braced frame	sisting fran	10	RC = R	einforced co hear wall				= Unreinfo			MH :		ctured Hou	using Fl	D = Elexib	le diaphrag diaphragm	gm

Structure 19, Building 13 Photographs



Connection Between this Portion (Left) and Older Portion, Visible Cracking



Exterior, Connection to Older Portion

рнот	PHOTOGRAPH										Belov COO (ear(s) B rcial	S1: D D W Grade uilt: Emer. S School	de: .3] d ate/Time :: :: 	88 . Yea Cod 195	r Built: e Year: 5 2	180 20141 20141	EST
				-		Soil	Type:	Utili Hard	B Avg	Den	C C se Si]D [iff S	Boft P	JF D	NK DNK, ass	ume Type	D.
				7		Geo	logic H	Rock	Rock Liquefac	So So	-			Soil			
dym	1					- Contineering	acency:			ounding					r Adjacen		
32	Ì		0		1		gularitie			-	pe/sever		102010511		n Aujacen	it Building	
				1	1		erior Fal ards:	lling	U	nbraced arapets	Chimney	S		avy Clad bendage	lding or H s	eavy Ver	neer
=	ther this etch	form	~						nes or cor								
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO	S2	S3	S4	S5	EVEL ·		RE, S	PC1	PC2	RM1	RM2	URM	MH
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	1.02	(FD)	(RD)	UKM	WIT
Basic Score Severe Vertical Irregularity, VL1	3.6	3.2	2.9	2.1 -1.0	2.0 -1.0	2.6	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	1000	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-1.0 -0.6	-0.9	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1 Pre-Code	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark	-1.1	-1.0	-0.9	-0.6	-0.6 1.4	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	1.1 0.1	1.9	NA 0.5	1.9	2.1	NA 0.3	2.0	2.4	2.1	2.0	NA	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	0.5	0.5	0.3	0.3 -0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	3	.83	20.	13	_		_	_		-	1						
EXTENT OF REVIEW Exterior: A Partial Interior: None Drawings Reviewed: Yes Soil Type Source:		s That 1 al Evalu ntial (ur n) s from ta	Trigger A ation? nless SL2 aller adja	> cent	Detaile P Ye P Ye No	ed Struc es, unkno es, score es, other o		A buildir A buildir n cut-off present Evalua	ng type o	r other b ommen	ded? (ch						
	act Person:									es, nonst	ructural h	azards	identified	that sho	ould be ev uire mitiga	aluated	

Structure 20, Building 13 Photographs



Exterior



"Tornado Safe Room" Notice



Exterior of Addition

РНО	PHOTOGRAPH								ve Grade q. ft.):	tary I T	Belov SO S Year(s) B	S1:D w Grade uilt: Emer. S School	de: . 3 ate/Time : 0 Services	- 88 1 9 e: <u>S1</u> Yea Code	1817 210 r Built: 9 Year:	3335 9 9 Al	M EST
				1			Type:	Hard Rock	Avg Rock	Den	ise Si il Si	tiff S oil S	Soft P Soil S	oor <i>If</i> Soil		ume Type	
1 Aver	11.	n	Sch	0-1	1					an has seen in the second s						upt.: Yes/	\sim
	bu	ildiu	14	001	1	-	acency: gularitie			ounding	pe/sever		lazards fr	om Taller	Adjacen	t Building	
							gularitie			lan (type		(y) _				_	
		1		T	-		erior Fa ards:	lling		arapets	Chimney	'S		avy Clade bendages		eavy Ver	neer
			Г			CO	MMENT	S:									-
			1				·St	cel	n h	Ray	ns	60	ols	QX	pos	ed	
		1					M	650		1 10	nota	1	111		1		
	Herev	TOIV	ns			-	1	000	Yrin	A	at ou	1 m	17-1	beaw	1		
=	this	for	wa			-						posed	=79	iteel			
		1-1	80 0							-		T	-7				
		-							T		1	7	- 1	masar	VY		
SI	ETCH				_				nes or cor						'	-	
FEMA BUILDING TYPE Do Not	-	WIA	SCO W2	RE, MO	S2	S3	ND FII	S5	EVEL C1		C3	PC1	000				
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2 -1.2	2.9		2.0 -1.0	(2.6)	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	6 6 6 7 7 6 7	-0.6	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0 -0.6	-0.9	-0.9 -0.5	-0.9	-0.7 -0.4	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	5 S 3 8 5 1	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1	-1.0	-0.9		-0.6	(-0.8)	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	0.1	0.3	0.5	1 0.000	1.4	0.1	1.9	NA 0.5	1.9 0.4	2.1	NA 0.3	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.1		-0.4	0.2	-0.1	-0.4	0.4	0.0	-0.2	0.6	0.4	0.5	0.5	0.3 -0.2	0.3 -0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, Smin	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMI	r 1.	83	:0	16													
KTENT OF REVIEW OTHER HAZ/ terior: Partial All Sides Aerial erior: None Visible Entered awings Reviewed: Yes No Detailed Structura il Type Source: Pounding pote Cut-off, if know Falling hazards ologic Hazards Source:						Is That al Evalu ential (ur vn) Is from t ards or S	Trigger A lation? hless SL2 aller adja	> acent F	Detail	ed Struc es, unkno es, score es, other o ed Nons	EQUIF etural Eva own FEM less that hazards tructural ructural h	A buildir A buildir n cut-off present Evalua	ng type o	r other bi	ded? (ch	eck one)	
☐ Yes, Final Level 2 Score, S _{L2} Nonstructural hazards? ☐ Yes			lo	the s	tructural	system				o, nonstr tailed ev o, no nor	uctural ha aluation i structura	azards e is not ne il hazard	xist that i cessary s identifi	may requed	iire mitiga DNK	ation, but	а
Where information	cannot l	be verifie	d, scr	eener shal	I note th	e follow	ing: E	ST = Est								-	-
Legend: MRF = Moment-re BR = Braced fram	sisting fran	ne	RC = R	einforced co hear wall				= Unreinfo	orced mase		MH		ctured Ho	using FI	D = Flexib	le diaphrag diaphragm	gm

Structure 21, Building 14 Photographs



Exterior, Half Masonry Half Steel Wall



Interior, Exposed Wall



Interior Gym/Theater, Wall and Ceiling Exposed

PHOTOGRAPH							tude: 3	Bi ifiers: 	schi 751 ve Grade q. ft.):	2001 135	Belov	ongitu S1: O D v Grade	de:	Zip: 35 88+8 1 e: 5/ Year	144		
						Occ	upancy Type:	: Ass Indu Utili	embly ustrial ty B	Comme Office Wareho	ercial (ouse C	Emer. S School Residen	tial, # Ur]E [nits:]F DI	overnmer		
XN.tis =1	he	form		7-01	hor			Hard Rock	Avg Rock	Den So				oor If. Soil	DNK, ass	ume Type	D.
1.10,113	. 03	10348		-		Geo	logic H	azards:	Liquefac	tion: Ye	s/No/DNH	(Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/	No/DNK
1	_	-		101	ms	Adj	acency:		P	ounding		alling H	azards fr	om Taller	Adjacen	t Building	
						Irre	gularitie				pe/sever)	ity) _					
Shu			, awy	ing			erior Fal ards:	lling		arapets	Chimney	S		avy Clado pendages		eavy Ver	neer
		1/2					MMENT				1-1-1-	-					
	1441					1	RV	N									
									. di Hrani	aph t co	irag	M	l I Ca	nne	cled		
							be	ildi	ng			1					
SKI	ETCH								2	nmonte (on separa	te nade					
	В	ASIC	sco	RE, MO	DIFIE												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2	-1.2	-1.2	-1.0	-1.0	-1.1	-1.0	-0.8	-0.9 -0.5	-1.0 -0.6	-0.7 -0.4	-1.0 -0.6	-0.9	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.4	-0.0	-0.5	-0.5	-0.5 -0.7	-0.4	NA NA
Pre-Code	-1.1	-1.0	-0.9	37338	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	(-0.5)	-0.5	0.0	-0.1
Post-Benchmark Soil Type A or B	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.1	0.3	0.5	-0.2	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9		-0.4	NA	-0.1	-0.4	-0.5	0.0	-0.2	-0.3 NA	-0.1	-0.1	-0.1 -0.6	-0.2 -0.2	-0.4
Minimum Score, Smin	1.1	-0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	CI	5	>0).3									12.11				
EXTENT OF REVIEW				OTHER	R HAZ	ARDS			ACT		EQUIF	ED	-		-	100	
	All Sides	Aer	ial	Are Ther				4			tural Eva	Note and the	Require	242			
Interior: None	Visible	Ent	ered	Detailed	Structur	al Evalu	ation?							ea r or other bu	ilding		
Drawings Reviewed: Yes	No						less SL2	>	X Ye	es, unking	less that	n cut-off	ig type o	n other bl	unaing		
Soil Type Source: Geologic Hazards Source:	-			cut-o	ff, if know	vn)				es, other	hazards						
Contact Person:			_	Fallin build		is from t	aller adja	cent									
- Fatt &	2.0 1.0 M.M.		_	Geol	ogic haza	ards or S	oil Type	F						comment			
LEVEL 2 SCREENING PERFO	ORME	D?		Signi	ficant da	mage/de	terioratio	on to	P Ye	es, nonst	ructural h	azards	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2		N D	0	the s	tructural	system				o, nonstr	uctural ha	azards e	xist that	may requ	lire mitig	ation, but	a
Nonstructural hazards? Yes			lo							o, no nor	structura	hazard	s identifi	ed 🕅	S DNK		
Where information of	annot h	e verifie	d, scr	ener shal	I note th	e follow	ina: F	ST = Fet									-
Legend: MRF = Moment-res				einforced co					rced maso						Constraint -	1- d'	
BR = Braced frame	Jung hull		SW = S	hear wall			TU = Tilt u		nceu mast	лаў паш		= Manufa = Light me	ctured Ho etal			le diaphra diaphragm	



Structure 22, Building 16 Photographs

Exterior, Side of Building

Exterior, Canopy



Interior, Ceiling and Walls Exposed

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

		-			1.00	Add	ress:	36	Ola	HI	IV L	50	1	-			-
							_			id Tr	1	1 - (2 7	ip: 3	2216		
						Oth	er Ident	ifiers:	73	0111	7			.ip. <u> </u>	0310	7	
							ding Na										
						Use	: Hi	gh	Sel		(Ym	-					
									7590	70	3' Lo	ngitu		81.8	199	87	
РНОТС	GRAP	н				Contraction of the	1.0	-			S1		379			-	
						Scre	eener(s)	: _ CI	M		_	_ Da	ate/Time	: 51	00 15	430A	m
						No.	Stories	Abov	ve Grade	: 1	Below	Grade:	0	Year	Built:	19810	EST
							al Floor			97	75			Code	Year:		-
							litions:	<u>N</u>		Yes, Yea							
						Ucc	upancy		embly ustrial ty	Commerci Office Warehous	S	mer. Se chool esident	ervices tial, #Ur		storic overnmen	□ Shelt it	ər
	_					Soil	Type:	Hard	B	Dense	Stiff]E [NK DNK. assi	ume Type	D.
THE this for	m	D-	of	ner fo	IMS			Rock	Rock	Soil	Soil	S	oil S	Soil			_
								azards:		tion: Yes/N							NORDINK
IT THE LAST AND	Ge 10.100	1	*				acency:		D Po	ounding	🗆 Fa	lling Ha	azards fr	om Taller	Adjacent	t Building	
Arm			-			Irreg	gularitie	s:		ertical (type an (type)			Hra	ntc	erna	~	_
111	001 <u>0</u>		-	-			erior Fal	ling	U U	nbraced Ch	imneys		🗌 Hea	avy Clado	ling or He	eavy Ven	eer
the second second			101	PUINC	5	Haz	ards:			arapets ther:			🗆 App	bendages	0		
			1				MMENT										1.
						4	ne.	- 01	ntr	ant	Cor	ne	er 1	20	ther	a.	Iding
							1										2
																	. 13
*N.1.>.																	
SKI	тсн						Addition	al skotch	00 or con	nments on							. J
		ASIC	sco	RE, MO	DIFIE					1 SCOR				-	-		-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF)	1.5	2.0	INF) 1.2	1.6	1.4	(1.7)	1.7	1.0	1.5
Severe Vertical Irregularity, VL1	-1.2	-1.2	-1.2		-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.7 -1.1	-0.7	-0.7	0 0.00000	-0.6	-0.7	-0.6	-0.5	-0.5		-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9	1	-0.6	-0.9	-0.6	-0.0	-0.6 -0.4	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	-0.5	-0.7 -0.5	-0.6 -0.3	-0.7	-0.7 -0.5	-0.4	NA
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	-0.1 1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	-0.3	-0.6 0.9	-0.9	-0.6	-0.6 0.5	NA 0.6	-0.6	-0.4	-0.5 0.3	-0.7 0.3	-0.3	NA 0.2	-0.4 0.2	-0.5	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	(1.		0,3		0.0	0.0	0.0	0.0	0.5	0.5	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION RE		D				1	-
Exterior: 🗹 Partial 🔲 /	All Sides	Aeri	ial	Are There		10.00000				ed Structu			Require	42			
Interior: None	/isible	K Ente		Detailed	Structur	al Evalu	ation?			es, unknow					ilding		
Drawings Reviewed: Ves K N Soil Type Source:	No			Poun	ding pote	ential (un	less SL2	>	X Ye	es, score le	ss than o	cut-off	a type o	outer bl	nung		
Geologic Hazards Source:			_		ff, if knov		alles a l'		Ye	es, other ha							
Contact Person: Lorry		-	-	Fallin buildi	g hazard ng	s from ta	aller adja	cent									
	1000								Detaile	ed Nonstru	ctural E	valuat	ion Rec	amana			
I EVEL 2 CODEENING DEDE		DO	-	Geolo	ogic haza	ards or S	oil Type	F								eck one)	
LEVEL 2 SCREENING PERFO	ORME			Signit	ficant dar	mage/de	oil Type terioratio	F n to	Ye Ye	es, nonstruc	tural has	zards in	dentified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2	ORME			Signit	ogic haza ficant dar tructural s	mage/de	oil Type terioratio	F n to		es, nonstruct	tural haz	zards i ards ex	dentified	that sho	uld be ev	aluated	a
☐ Yes, Final Level 2 Score, S _{L2} Nonstructural hazards? ☐ Yes			0	Signit the st	ficant dar tructural :	mage/de system	terioratio	n to		es, nonstruct o, nonstruct tailed evalu o, no nonstr	tural haz ural haz ation is uctural h	zards in ards ex not neo nazards	dentified kist that i cessary s identifie	that sho may requ ed	uld be ev ire mitiga Ĵ DNK	aluated	а
Yes, Final Level 2 Score, SL2	annot b	No N	o d, scre	Signit the st	ficant dar tructural : I note th	mage/de system e follow	terioratio	n to ST = Esti		es, nonstruct o, nonstruct tailed evalu o, no nonstr r unreliable	tural haz ural haz ation is uctural h data	zards in ards ex not neo nazards OR D	dentified kist that i cessary s identifie	that sho may required ed to Not Kn	uld be ev ire mitiga Ĵ DNK	aluated	a

Structure 23, Building 15 Photographs



Interior Walls, Masonry



Interior, Mechanical Room, Exposed Ceiling and Walls



Interior, Connection to Addition

	Level 1
HIGH	Seismicity

РНОТ	PHOTOGRAPH Pavilion space								OI (uch for 24 24 24 24 24 24 24 26 26 26 26 26 26 26 26 26 26	: 1 Yes, N Office Wareho	Belov DO Year(s) B rcial use	Longitu Sr: O D w Grade tuilt: _ Emer S School	2 de:	881 	21 @ r Built: 2 e Year:	458 930β 2000 I	EST
		-	_			Soil	Type:	Hard	□ B Avg	Den					NK DNK. ass	ume Type	D.
								Rock	Rock	Soi	I S	oil S	Soil S	Soil			
Pavilions	sale	2					acency:	azards:		tion: Yes						upt.: Yes/ t Building	
		_	_			and the second second	gularitie	s:	Ve		pe/sever			om Tallel	Adjacen	t Building	
Outdoor iv	doc	yc				Haz	erior Fal ards:			nbraced arapets ther:	Chimney		App	bendages	5	eavy Ver	ieer
	ETOIL								fact					1190	irage		
Sr	ETCH	BASIC	sco	RE, MO	DIFIER				es or con					-	-		-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	\$3 (LM)	S4 (RC SW)	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMMV	3.6 -1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1	3.2 -1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	2.9 -1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2	2.0 -1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	2.6 -1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	INF) 1.7 -0.8 -0.5 -0.6 -0.2 NA 0.5 -0.4 -0.4 0.5	1.5 -0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5	2.0 -1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7	INF) 1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.2	1.6 -1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA	1.4 -0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5	1.7 -0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	1.0 -0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	1.5 NA NA -0.1 1.2 0.3 -0.4 NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN		3.7)	>1	2.6	0.0	0.0	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW Exterior: Partial Interior: None Source: Soil Type Source: Geologic Hazards Source: Contact Person: Lawy	al Evalu ential (un n) s from ta ards or S mage/de	Trigger A ation? alless SL2 aller adja oil Type	> cent F	Detaile Ye Ye Ye No Detaile Ye	ed Struc es, unkno es, score es, other o ed Nonsi es, nonst	own FEM less that hazards tructural ructural h	aluation IA buildir n cut-off present I Evalua hazards	tion Rec	r other be commended	ded? (ch	eck one) valuated						
Yes, Final Level 2 Score, SL2	Lacry building UEL 2 SCREENING PERFORMED? Geologic h									o, nonstru	aluation	azards e	xist that i	may requ	uire mitiga	ation, but	u



Structure 24, Building 15 Photographs

Interior, Gymnasium, Walls and Ceiling Exposed

				1313		Add	ress:	110	-	>, W	iles	Av	е.		0.00		
										cit	Y	TN	Z	ip: <u>3</u>	826	1	
								ifiers:	62	1.15	<u>'</u>			_	_		
							ding Na		ont	NY	211-	1	-				
								36.					de: -5	39.0	200	ra -	
PHOTO	GRAP	н				Ss:		184		00		S ₁ :		19	240	21	
						Scre	ener(s)		m				ate/Tim		249	DUA	M
						No.	Stories	: Abov	e Grade	: 1	Below	Grade	:0	Year	Built:	1000 0	
						Tota	I Floor	Area (so	q. ft.):	101	2000	2		Code	Year:		1 201
						*****	itions:		7	Yes, Y			e-p		100	the state of the second st	
						Occ	upancy		embly ustrial ty	Commer Office Warehou		Emer. S School Residen	ervices tial, #Ur		storic overnmer	Shelt It	er
XN.T.S. awings	I			-		Soil	Type:	Hard Rock	Avg Rock	Dens Soil	e St	iff S	oft P		NK DNK, assi	ume Type	D.
ama.2		K	ritie	5-		Geo	logic H					0.000		/No/DNK	Surf. Ri	int · Yes/I	No/DNK
		111				*********	acency:		CONTRACTOR OF THE OWNER	ounding				om Taller			
							gularitie			ertical (typ an (type)	e/severi	ty)	11	~ or			
- Ta, Ind Mandatin			-			Exte	erior Fa	lling		nbraced (avy Clado			eer
				_			ards:			arapets				pendages			
						CO	MMENT	S:									
						1	RI	M									
	-						1-1										
1 town	rory					-											
100	01.1	-															
=Original(1970's	7 6	7=L	e-1	wilt iv	200	0											
SKI	TCH	1010								nments o			-				
FEMA BUILDING TYPE Do Not	W1	-		RE, MO								0.0					
Know		W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2 -1.2	-1.2	-1.0	2.0 -1.0	2.6 -1.1	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.9	-0.6	-0.7	-1.0 -0.6	-0.9	-0.9 -0.5	-0.9 -0.5	-0.7 -0.4	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7)	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1 1.6	-1.0	-0.9	-0.6	-0.6 1.4	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	1.9	NA 0.5	1.9 0.4	2.1 0.5	NA 0.3	2.0 0.6	2.4	2.1	2.1 0.5	NA 0.3	1.2 0.3
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories) Minimum Score, SMIN	-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW	1-		-				6						-				
		Aeri		OTHER					100000000	ION RE			_				
Interior: 🗋 None 🔲 🕅		Ente	ered	Are There Detailed	Structur	al Evalu	ation?	A		ed Struct							
Drawings Reviewed: Yes X I Soil Type Source:	No			Poun	ding pote	ential (un	less SL2	>		es, unkno es, score	less than	A buildir	ig type o	r other bu	ilding		
Geologic Hazards Source:	-		-		ff, if know				Ye	es, other l							
								acent	No No						1.120000		. 8
			-	Geolo	ogic haza	ards or S	oil Type	F						ommend			
	JRME				icant dar		terioratio	on to		s, nonstru	uctural h	azards i	dentified	that sho may requ	uld be ev	aluated	2
Yes, Final Level 2 Score, SL2		N N		ule st	ructural	system			de	tailed eva	aluation i	s not ne	cessary			adon, DUC	d
Nonstructural hazards? Yes			1							o, no nons					DNK		
Where information of															ow		
Legend: MRF = Moment-resi BR = Braced frame	sting fram		RC = Re SW = Sh	nforced cor ear wall	ncrete	1	JRM INF	= Unreinfo	rced maso	onry infill	MH =	= Manufa Light me	ctured Ho) = Flexib	e diaphrag diaphragm	ym

Structure 25, Building 17 Photographs



Exterior, Courtyard



Interior, Masonry Walls



Interior, Gymnasium, Exposed Walls and Ceiling

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

			1			1.4		111	TU	61	CI	1.	Dic				
						Add	dress:	11	IT PI	"dh	SUL	100			22/1	_	
								UN	no	UT	4 21	N		Zip: 33	8661		COLLER W
							er Identi	-	16								_
							Iding Na			1	-						
						Use	: M	n dy	10.5	cho				00	1.1.0	6.0	
							itude: 3		1186	44				89,0	448	52	_
РНОТ	OGRAP	H	-1			Ss:	-	144					523		1.0	1 4 .41	
						Scr	eener(s)	: <u> </u>	W1			D	ate/Tim	e: <u>517</u>	2400	010A1	n
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1							Stories:				Belov	w Grade	: 1	Year	r Built:	1951 1	EST
							al Floor				53.8			Code	Year:		-
	7					Add	ditions:		lone 🏹	Yes,	rear(s) B	luilt: <u>(</u>	unk	now	>		
						Oco	cupancy	Indu	embly ustrial	Comme Office	rcial	Emer. S)		istoric overnmer	Shelt	er
								Utili	ty	Wareho	use	Residen	itial, #U	nits:			
	-		-	-		Soi	I Type:	Hard	□B Avg	Den	se S	tiff S	ioft P	oor If	NK DNK, ass	ume Type	D.
× .	-	X	-					Rock	Rock	So	Contraction of the second			Soil			~
		1.	1	-		COLUMN TWO IS NOT	ologic Ha										
						Adj	acency:		D Po	ounding		Falling H	azards fr	om Taller	Adjacen	t Building	
						Irre	gularitie	s:			pe/sever		Atro	mt (orne	V	-
						Ext	erior Fal	lina	and the second second second		Chimney	Sector States and States	and the state of the			eavy Ver	oor
		-	+			Haz	ards:			arapets				pendages	5		
	M					CC	NMENT Sto PV NC	S:						A			
	1			-			101	101	00	11:2	26	(Flo	N. V	lind	nna	m	
		-				-	" STO	zev.	06	12 () 1	17	1.1.	-331		3	1.)	
			-				NRV	M			0						
							0110	har	(p;	lin	Ci iv	n a	YCA	2			
							. NC	Noc	w.	1	7			5			
						-											
			_			-											
						-											
SK	ETCH						Additiona	al sketch	es or con	nments o	on separa	ate page					
	B	ASIC	sco	RE, MO	DIFIER									and the second			
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	SW)	INF)	15	20	INF)	10	11	2			
Severe Vertical Irregularity, VL1	-1.2	-1.2	-1.2		-1.0	-1.1	-1.0	-0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	-0.9	1.7 -0.9	1.0 -0.7	1.5 NA
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	(0.7)	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	1.6	1.9	2.2		1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.1	0.3	0.5	-0.2	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.2	-0.3 NA	-0.1	-0.1	-0.1	-0.2 -0.2	-0.4
Minimum Score, SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$: (0	1.51:	20	,3										0.0	0.0	0.2	1.0
EXTENT OF REVIEW				OTHER							EQUIF						
	All Sides			Are Ther				4	Detaile	ed Struc	tural Ev	aluation	Require	d?			
Drawings Reviewed: Yes	Visible	Ent Ent	ered	Detailed					U Ye	s, unkno	wn FEM	A buildir	ng type o	r other bu	uilding		
Soil Type Source:	NO			Poun			nless SL2	>	Ye Ye	s, score	less tha	n cut-off					
Geologic Hazards Source:			-	Fallin	ff, if know		aller adia	cent			hazards	present					
Contact Person: Chuck	reed	M		build	ing						tructure	Evolue	tion Dr.			a ali	
	0.000	DC	-	Geol	ogic haza	rds or S	Soil Type	F								eck one)	
LEVEL 2 SCREENING PERF	ORME			Signi	ficant dan	nage/de	eterioratio	on to		s, nonst	ructural h	azarde o	identified	I that sho	uld be ev	valuated ation, but	
Yes, Final Level 2 Score, SL2		N EQ		the s	tructural s	system			de	tailed ev	aluation	is not ne	cessarv	may requ	me mitig	auon, but	a
Nonstructural hazards? Yes									No No	, no non	structura	al hazard	s identifi		DNK		
Where information	cannot b	e verifie	d, scr	eener shal	I note the	e follow	ving: ES	ST = Esti	imated of	r unrelia	ble data	OR	DNK = D			-	
Legend: MRF = Moment-re:	sisting fram	10	RC = R	einforced co			URM INF =					and the second sec	ctured Ho			le diaphra	m
BR = Braced frame	3		SW = S	hear wall			TU = Tilt u	р		1	LM :	= Light me	etal		D = Rigid	dianhrann	

Structure 26, Building 18 Photographs



Front Left Exterior, Primary Hallway That Wings Come From, All Sides Similar



Front Right Exterior, Primary Hallway That Wings Come From, All Sides Similar

						Ada	Irocc:	30	SE	. 4:	ah C	-	117	~			
						Add	iless:	30		. 111	gh S	cho	01 17		07/1		
						0	er Ident	ifiere	7-7	-		-	2	.ip: <u>57</u>	8261		
							er ident Iding Na	and the lower start -	-	-		-			-		
с						Bui		ine:	Sci								
						Use	the index	2 Sr	419	000				00	0 (1)	11/2	7
21107									-111	409		ongitu	ide:	. 84	04:	546	t
РНОТО	OGRAP	Н					1.4		A A		8),52		2/10	100	14.1.4
):				D	ate/Time	Charles all		12	
									ve Grade		and the second se	v Grade	:	Yea	r Built:	19721	EST
								Area (s			0770			Code	e Year:		
							litions:	Ø N			Year(s) Bu	uilt: _					
						000	upancy		embly	Comme		Emer. S		Пн		Shelt	er
								Utili	ustrial	Office Wareho		School			overnme	nt	
						0.1	-			0000			ntial, #Ur				
			_	_		Sol	Type:	Hard	□B Avg	Der					NK acc	ume Type	
								Rock	Rock	Sc				ioil "	DIVN, ass	ume rype	D.
						Geo	logic H	azards:	Liquefac	ction: Ye	s/No/DNK	Lands	lide: Yes	/No/DNK	Surf R	unt · Yes/	
	1	1	-	~			acency:			ounding			lazards fr				
	-	V					gularitie		1000		ype/severi						
						Inte	guiaritte		N P	lan (type	ype/seven ⇒) <u>_C</u>	-01	tran	+ pro	WPV1	none	SUC
					1	Evt	erior Fa	lling			Chimney						
							ards:	ining		arapets						leavy Ver	ieer
														lenuaye:	5		
				1	1	CO	MMENT	S:	_					-			
		1	-	-		-	Alc	-0 <	5100	in	sit W(.el	Spri	ore	,		
		/					14	5	20-0-	. 7)	- /	~			٨	
	1		1.1			- 1		nc	. Co	151	WI	ma	Son	rv i	infil	1	
				-		-	0-			1	E IC	Vico		1			
						_	o He	en	12-	typ	e g	Ind					
		X	. 1	TO													
		×	N	111	2.												
						-											
SK	ETCH						Addition	al sketch	nes or cor	nments	on separa	te page	1				
	B	ASIC	sco	RE, MO	DIFIE	RS, A	ND FI	NAL LI	EVEL	1 SCC	DRE, SL	.1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1	RM2	URM	MH
					alway.	14001	ŚW)	INF)			INF)			(FD)	(RD)		
Basic Score Severe Vertical Irregularity, VL1	3.6	3.2 -1.2	-1.2	1 1 1 1 1 1 1 1 1	-1.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	and the second	-0.6	-1.1	-1.0	-0.8	-0.9	-1.0	-00	-1.0 -0.6	-0.9	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	1 1 1 1 1 1 1 1	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.5	-0.5	-0.4	NA NA
Pre-Code	-1.1	-1.0	-0.9	11.0	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark	1.6	1.9	2.2	223722	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B Soil Type E (1-3 stories)	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2 NA	-0.1	-0.4	-0.5	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	1.1	0.9	0.7		0.5	0.6	0.5	-0.4	-0.5	-0.7	-0.3	NA 0.2	-0.4	-0.5 0.3	-0.6 0.3	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	1	25	in	.3)			1	510	510	0.0	0.0	V.L	0.2	0.5	0.3	0.2	1.0
	(J -	2		-			-	-	_		_	-		_		
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIR	ED					-
	All Sides		2011 A	Are Ther				A	Detail	ed Struc	ctural Eva	luation	Require	d?			
Interior: Interi	Visible No	R Ente	ered	Detailed						es, unkn	own FEM	A buildir	na type o		uilding		
Soil Type Source:	110			Poun			nless SL2	>	K Y	es, score	e less than	cut-off					
Geologic Hazards Source:					ff, if kno g hazar	wn) ds from ta	aller adia	cent			hazards p	present					
Contact Person: Chuck	Reci	dy		build	ing				_	-	tructure	Evalua	tion De-		dad0 (-)	and and	
LEVEL 2 SCREENING PERF	ODAC	D2		Geol	ogic haz	ards or S	oil Type	F			structural h						
	URIVIEI			Signi the s	ficant da	amage/de system	terioratio	on to		o, nonstr	tructural h ructural ha	azards e	xist that	may requ	uid be e	valuated	a
Yes, Final Level 2 Score, SL2		N N	2.6	ule S	uuululal	system			de	etailed ev	valuation is	s not ne	cessary		and ming	auon, but	a
Nonstructural hazards? Yes										o, no noi	nstructural	I hazard	ls identifie		DNK		
Where information			d, scr	eener shal	I note th						able data	OR	DNK = D	o Not Kr	now		
Legend: MRF = Moment-res	isting fram	e f	RC = Re	einforced co		1	JRM INF	= Unreinfo	orced mase		MH =	Manufa	ctured Hor	40%	122.024	le diaphra	gm
BR = Braced frame			5W = S	hear wall			rU = Tilt u	ip			LM =	Light me	etal	R	D = Rigid	le diaphra diaphragm	ī

Structure 27, Building 19 Photographs



Out-of-Plane Setback



Out-of-Plane Setback



Concrete Columns Exposed



Split Level

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

		Level 1
DERATEL	Y HIGH	Seismicity

FEMA P-154 Data Collectio						M	DDE	RAT	ELY	HIGH	I Sei	ismic	ity				
	Oth	er Identi	Me	din	iddi T, p	N	scho		t. 2ip: <u>3</u>	8355	2						
							ding Na		10	Sch	Ico						
BUOT						Lati	tude: 2	5518	1240	70		Longitu	de: ~	88.2	804	ISI	
РНОТС	JGRAP	н					ener(s)		M			S1: 0	ate/Time	2 1: 5/	3000	9:30	MA
						No. Tota	Stories:	Abov	ve Grade q. ft.):	: <u> </u> 105 ·] Yes, Y	85	w Grade		Year		20000	
							upancy	Ass	embly Istrial	Commer Office Warehou	cial	Emer, Sechool		March 1997	storic overnmer	Shelt	er
				Т	_	Soil	Type:	Hard Rock	Avg Rock	Dens	e S	D C	JE [F D	NK DNK, assi	ume Type	D.
						Geo	logic Ha	azards:	Liquefac	tion: Yes	/No/DN	K Landsl	ide: Yes	/No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
						-	acency:			ounding		Falling Ha	azards fr	om Taller	Adjacen	t Building	
		-	-			Irreg	gularitie	s:	X Ve	ertical (typ an (type)	oe/sevel	rity) Sp -en	trav	level	mane	C	
		-					erior Fal ards:	ling		nbraced (arapets	Chimney	ys	Hea	in the second second	ding or H	eavy Ven	eer
	-					co	MMENT	S:	0	ther:	-	4	1				
						1	1.7	+	Wa	() (ar	istr	VCt	JQ/			
		Г	_			1	Re	inf	, 0	on	C,						
	_																
						-											
SKE	TCH	1010								nments o	and the second se	The lot of					
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO	S2	S3	ND FIN	S5	EVEL '	1 SCO	RE, S	L1 PC1	PC2	DHA	DHO	Unit	
Клож				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	PGZ	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	4.1 -1.3	3.7 -1.3	3.2 -1.3	707	2.2 -1.0	2.9 -1.2	2.2 -1.0	2.0 -0.9	1.7 -1.0	2.1 -1.1	1.4 -0.8	1.8	1.5 -0.9	1.8 -1.0	1.8 -1.0	1.2 -0.8	2.2 NA
Moderate Vertical Irregularity, VL1	-0.8	-0.8	-0.8	-0.7	-0.6	-0.8	-0.6	-0.6	-0.6	-0.6	-0.5	0.6	-0.6	-0.6	-0.6	-0.6	NA
Plan Irregularity, PL1 Pre-Code	-1.3 -0.8	-1.2	-1.1		-0.8	-1.0	-0.8	-0.7	-0.7	-0.9	-0.6	-0.8	-0.7	-0.7	-0.7	-0.5	NA
Post-Benchmark	1.5	1.9	2.3		1.4	1.0	1.9	NA	-0.4	-0.7	-0.1 NA	-0.4	-0.3 2.4	-0.5	-0.5	-0.1 NA	-0.3 1.2
Soil Type A or B	0.3	0.6	0.9	0.6	0.9	0.3	0.9	0.9	0.6	0.8	0.7	0.9	0.7	0.8	0.8	0.6	0.9
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0 -0.5	-0.1	-0.3		-0.5	0.0	-0.4	-0.5	-0.2	-0.2	-0.4	-0.5	-0.3	-0.4	-0.4	-0.3	-0.5
Minimum Score, Smin	1.6	1.2	-1.2		-0.7 0.5	0.9	-0.7	-0.6 0.5	-0.6 0.3	-0.8 0.3	-0.4	0.3	-0.5	-0.6	-0.7	-0.3	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	G		20		0.0	0.3	0.0	0.0	0.3	0.3	0.3	0.3	0.2	0.3	0.3	0.2	1.4
EXTENT OF REVIEW	-4	27	Ĭ	OTHER	RHAZ	ARDS			ACT			RED				titlest toto letter thank	
	All Sides	Aeri	al	Are Ther	e Hazard	Is That T	rigger A	1	1 - Contraction			aluation	Require	d?			
		Ente	ered	Detailed	Structur	al Evalu	ation?					A buildin			ulding		
Drawings Reviewed: Yes X I Soil Type Source:	No			D Pour			less SL2	>	Ye Ye	es, score	less tha	n cut-off	9.940.0				
Geologic Hazards Source:			-		ff, if knov ig hazard		aller adia	cent		es, other l	nazards	present					
	CES	an a	_	build	ing				Detaile		ructura	I Evaluat	tion Rec	ommen	led? /oh	eck anal	
LEVEL 2 SCREENING PERFO			-		ogic haza ficant dai				and the second			hazards i			and the second second	and the second second	1.0
Yes, Final Level 2 Score, SL2					tructural :		tenorado	11 10		o, nonstru	ictural h	azards ex	xist that	may requ	ire mitiga	ation, but	a
Nonstructural hazards?									de	tailed eva	aluation	is not nee	cessary				
	annot			oonor aba	Inoteth	o follow	ina Ef	T				al hazard			C DNK		
												= <u>OR</u> L = Manufac = Light me				e diaphrac	m

Structure 28, Building 20 Photographs



Exterior View



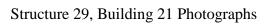
Tilt-Wall

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

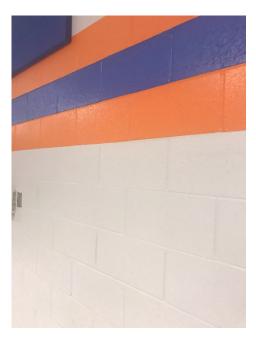
Level 1 MODERATELY HIGH Seismicity

						Oth	er Identi	Me.d	ina		₫ St.			Zip: 35	8355		
							ding Na		rent	tavy	Sch	1001	_				
						Lati	tude:	35.9	8038	56		Longitu	de: 🗌	88,7	.750	262	
РНО	TOGRAP	н				Ss:						S1: 0			1		
						-	eener(s)	17	CM			D	ate/Tim	e: <u>5</u>	130 1	NOAN	N
						Tota	Stories: al Floor litions:			11	Below 3,35 Year(s) B		. 0		Built: 7 Year:	2018 0	EST
						Occ	upancy		embly ustrial	Comme Office Wareho	ercial	Emer. S		01.000	storic overnmer	Shelt	ler
				-		Soil	Type:	A Hard	□B Avg	Den	C C]D	oft P	F D	NK DNK, ass	ume Type	D.
						Gan		Rock	Rock	So	damer molitik			Soil			
			-				acency:			ction: Yes				No/DNK			
							gularitie			ertical (ty	pe/sever	ity)					
		_	_	-		Evt	erior Fal	lina		lan (type)	Chimney			int Co			
							ards:	iiiig		arapets	Chinney	5		avy Clado pendages		eavy ven	ieer
							MMENT					-					
							-RE	sint	Force	ed M	Maso	nr	Y				
		-					-						1				
						_											
						_											
		_				1											
						-											
S	KETCH		_	1991 - 7591995							on separa		í	_			
FEMA BUILDING TYPE Do No		W1A	SCO W2	RE, MO			-			1	_			1			
Клоч		WIA	VV2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	4.1 -1.3	3.7 -1.3	3.2	2.3	2.2 -1.0	2.9 -1.2	2.2	2.0	1.7	2.1	1.4	1.8	1.5	1.8	1.8	1.2	2.2
Moderate Vertical Irregularity, VL1	-0.8	-0.8	-0.8	-0.7	-0.6	-1.2	-1.0 -0.6	-0.9 -0.6	-1.0 -0.6	-1.1	-0.8	-1.0 -0.6	-0.9	-1.0 -0.6	-1.0 -0.6	-0.8 -0.5	NA NA
Plan Irregularity, PL1	-1.3	-1.2	-1.1	-0.9	-0.8	-1.0	-0.8	-0.7	-0.7	-0.9	-0.6	-0.8	-0.7	-0.7	-0.7	-0.5	NA
Pre-Code Post-Benchmark	-0.8	-0.9	-0.9	-0.5	-0.5 1.4	-0.7 1.0	-0.6	-0.2	-0.4	-0.7	-0.1	-0.4	-0.3	-0.5	-0.5	-0.1	-0.3
Soil Type A or B	0.3	0.6	0.9	0.6	0.9	0.3	1.9	NA 0.9	1.9	2.1	NA 0.7	2.1	2.4	2.1	2.1	NA 0.6	1.2
Soil Type E (1-3 stories)	0.0	-0.1	-0.3		-0.5	0.0	-0.4	-0.5	-0.2	-0.2	-0.4	-0.5	-0.3	-0.4	-0.4	-0.3	0.9 -0.5
Soil Type E (> 3 stories)	-0.5	-0.8	-1.2		-0.7	NA	-0.7	-0.6	-0.6	-0.8	-0.4	NA	-0.5	-0.6	-0.7	-0.3	NA
Minimum Score, SMIN	1.6	1.2	0.8	0.5	0.5	0.9	0.5	0.5	0.3	0.3	0.3	0.3	0.2	0.3	0.3	0.2	1.4
FINAL LEVEL 1 SCORE, SL1 ≥ SM	N: (3	5.82	0,3	1.41	_			_	_						_		
EXTENT OF REVIEW Exterior: Partial Interior: None	All Sides Visible	Aer		OTHEN Are Ther Detailed	e Hazard	s That	Trigger A	4	Detail	ed Struc	EQUIF tural Eva	aluation	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
	No			Pour cut-o	ding pote ff, if know	ntial (ur n)	nless SL2			es, score es, other	own FEM less that hazards	n cut-off		or other bi	uilding		
	12K-SON	0		build			14		Detail		tructure	Evelue	tion Dr.		1.10 (-1	a also a s	
LEVEL 2 SCREENING PER				Geol	ogic haza ficant dan	rds or S	oil Type	F						comment that sho			
Yes, Final Level 2 Score, SL2	ORIVIE		10		tructural s		tenoratio	11 10		o, nonstr	uctural ha	azards e	xist that	may requ	ire mitig	ation, but	a
Nonstructural hazards? Yes			U	10000	CALCULATION OF THE OWNER				de	etailed ev	aluation	is not ne	cessary	and the second second			
			lo												DAILY		
Where informatio	annot l	and the second		ener cha	I note the	follow	ina: EC	T = Eet		o, no nor	nstructura	al hazard	ls identifi	ied Ď	DNK		
Where information Legend: MRF = Moment- BR = Braced fran	esisting fram	be verifie	ed, scre	ener shall einforced co						o, no nor or unrelia	nstructura able data	al hazard	ls identifi DNK = D	ied Do Not Kr	ow	le diaphrag	





Exterior View, Apparent Wall System



Interior, Reinforced Masonry

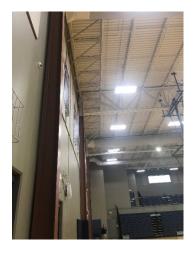
Level 1 MODERATELY HIGH Seismicity

				1		Add	ress:	100	Ho	orno.	- 17	r.					
								Me	dina	TI	1-		Z	ip: 39	8358	-	-
						Oth	er Ident	ifiers:	30								
~							ding Na										
						Use	: <u>Hi</u>	gh	Sch	100					10.0		
									2002	50					803	833	_
РНОТО	GRAP	н					0,0	: CN	٨			S1: C			12700	1 4 11 4	
No V		>						and a state of the second		~	-			7/211	3000		
	/								e Grade			w Grade	:0	-		ם דיכם	EST
	/		Г	T			itions:	Area (se			rear(s) B	Contraction of the second seco	cont		Year:		-
$\langle \rangle \langle \rangle$			1				upancy		embly	Comme		Emer. S				Shelt	or
$ \chi\rangle$							upancy		ustrial	Office Wareho		School	tial, #Un	G	overnmer		
$\wedge \wedge$	1			-		Soil	Type:	A Hard	B Avg	Den			1.000	-	NK DNK. ass	ume Type	D
		-				Goo	logic H	Rock	Rock	So	il S	oil S	oil S	Soil			
}				-		(111) 1110 Bloc	acency:			ction: Yes						upt.: Yes/I t Building	Contraction of the State of the
2							gularitie	And the second second	X V	ertical (ty	pe/sever	ity) SP	11-101	elfood	1,00S	Igaier	6
				-												m-par	
<		- 1		-			erior Fal ards:	lling	P	arapets	Chimney		Hea			eavy Ven	eer
						CO	MMENT	S:	0 []	tner:		-				-	
						A REAL PROPERTY.			WAL	(0)	actu	-1-	-		÷)		
	1		-		3	-	- 11	11	white	0	1211	U CE	gn				
						-											
						-											
			-														
SK	ETCU		-														
JN	ETCH	ASIC	800	RE, MO	DIFIER				es or cor				-	-	-		
FEMA BUILDING TYPE Do Not	W1	W1A	W2	S1	S2	\$3	S4	S5	C1	C2	C3	L1 PC1	PC2	RM1	RM2	URM	MU
Клож				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	FUZ	(FD)	(RD)	URM	мн
Basic Score	4.1	3.7	3.2	2.3	2.2	2.9	2.2	2.0	1.7	2.1	1.4	1.8	1.5	1.8	1.8	1.2	2.2
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.3	-1.3	-1.3	-1.1	-1.0 -0.6	-1.2 -0.8	-1.0	-0.9	-1.0	-1.1	-0.8	1	-0.9	-1.0	-1.0	-0.8	NA
Plan Irregularity, P_{L1}	-1.3	-1.2	-1.1	-0.9	-0.8	-1.0	-0.8	-0.7	-0.0	-0.6	-0.5	-0.8	-0.6	-0.6	-0.6	-0.5	NA NA
Pre-Code	-0.8	-0.9	-0.9	-0.5	-0.5	-0.7	-0.6	-0.2	-0.4	-0.7	-0.1	-0.4	-0.3	-0.5	-0.5	-0.1	-0.3
Post-Benchmark	1.5	1.9	2.3	1.4	1.4	1.0	1.9	NA	1.9	2.1	NA	2.1	2.4	2.1	2.1	NA	1.2
Soil Type A or B Soil Type E (1-3 stories)	0.3	0.6	0.9	0.6	0.9	0.3	0.9	0.9	0.6	0.8	0.7	0.9	0.7	0.8	0.8	0.6	0.9
Soil Type E (> 3 stories)	0.0	-0.1	-0.3	-0.4	-0.5 -0.7	0.0 NA	-0.4	-0.5	-0.2	-0.2	-0.4	-0.5 NA	-0.3	-0.4	-0.4	-0.3	-0.5
Minimum Score, SMIN	1.6	1.2	0.8	0.5	0.5	0.9	0.5	0.5	0.3	0.3	0.3	0.3	0.2	-0.6 0.3	-0.7 0.3	-0.3 0.2	NA 1.4
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	1.	520	2,3											0.0	0.0	0.2	1.4
EXTENT OF REVIEW				OTHE	RHAZ	ARDS			ACT	ION R	EQUIF	RED			-		
	All Sides			Are Ther				Ą	100000000		tural Ev	0.000000000	Require	d?			
Interior:	Visible	Ent Ent	ered	Detailed							own FEM				uildina		
Drawings Reviewed: Yes Soil Type Source:	NO			Pour			less SL2	>		es, score	less tha	n cut-off	0.0000				
Geologic Hazards Source:			-		ff, if know Ig hazard			ant	U Ye		hazards	present					
	KSOV	1		build		s nom t	aller adja	icent	Datal	Section 1	Amura A	I Evert					
			-	Geol	ogic haza										and the second second	eck one)	
	ORME	1227			ficant dar tructural s		terioratio	on to		o, nonstr	tructural l	azards e	vist that	may requ	uid be e	aluated // a	a
Yes, Final Level 2 Score, SL2		X.N	Contra de la contr	ule S	uuuunais	bystelli			de	tailed ev	aluation	is not ne	cessary	1	and mug	adon, Dul	a
Nonstructural hazards? Ves	-							_			nstructura				DNK		
Where information	cannot k	e verifie	d, scre	ener sha	I note th						ble data	OR	DNK = D	o Not Ki	now		
Legend: MRF = Moment-res BR = Braced frame	sisting fran	ne	RC = Re	einforced co near wall				= Unreinfo	orced mase		MH	= Manufa = Light me	ctured Ho	using F	D = Flexib	le diaphrag diaphragm	gm

Structure 30, Building 22 Photographs



Exterior View



Interior, Exposed Ceiling in Gymnasium



Exterior, Split Level, Out-of-Plane Setback

Level 1 VERY HIGH Seismicity

			Oth	er Ident	84 Then	noti				Z	(ip: <u>3</u>	8387						
								ding Na	eme:	nten	S.	hast				-		-
									5.9				ongitu	de	89,1	7411	D	
F	ното	GRAP	н				Ss:		11	0010	V			1,537		0116	20	
							1.5.7PM	eener(s)		M					e: 5/	S CE	11:30	AIN
							No.	Stories	Abov	e Grade	: 1	Belov	v Grade				940 0	115
							Tota		Area (so	q. ft.):	17	rear(s) B	5	996		Year:		
							Occ	upancy		embly istrial ty	Comme Office Wareho	(Emer. S School Residen	ervices		storic overnmer	☐ Shelt nt	er
	-				-		Soil	Туре:	A Hard	□B Avg	Den	se St	iff S	oft P	oor If	NK DNK, ass	ume Type	D.
			П	TRIA	thisto		Geo	logic H	Rock	Rock	So tion: Vo				Soil	0.40		
		3	L	State of the	1103 10	Anc	**************************************	acency:			ounding				/No/DNK om Taller			
		-	1		other	form		gularitie		Ve Ve		pe/sever			velow		t Building	
	5	1						erior Fal ards:	lling	U Ur	nbraced arapets	Chimney	S		avy Clado pendages		eavy Ver	neer
							CO	MMENT	S:									
	ad	dit	rior					Spl	it le	evel	6	gyw ise Iditi	~		1.			
								. 1.1	0.500	vr 43.	2001	se	MS	>> C	015			- 14
							4	pou	nosin	gn	y one	lditi	a					
	SKE	тсн						Addition	al sketch	es or con	nments o	on separa	ate page					
		В	ASIC	sco	RE, MC	DIFIE				and the second second second			The second s					an ganage
	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1		2.1 -0.9	1.9 -0.9	1.8	en se	1.4 -0.7	1.6 -0.8	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1		-0.6	-0.5	1		-0.7	-0.6	-0.7	-0.7	-0.7	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7	-0.7 -0.4	-0.6 -0.3	NA NA
Plan Irregularity, PL1		-0.7	-0.7	-0.6	and the second second	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code Post-Benchmark		-0.3 1.9	-0.3	-0.3	1000	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	0.2	-0.2	0.0	0.0
Soil Type A or B		0.5	0.5	2.0	1.	1.1 0.3	1.1 0.4	1.5	NA 0.2	1.4	1.7	0.1	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)		0.0	-0.2	-0.4		-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	0.3	0.1	0.1 -0.1
Soil Type E (> 3 stories)		-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 2	SMIN'	0.7	0.7	0.7	0.5 0,3	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW	- Omiti	(0.5		OTHE	R HAZ				ACT		EQUIF	ED			-		
Exterior: X Partial		II Sides	Aer	ial	Are Ther				Δ			tural Eva		Poquier	d2			
Interior: 🗌 None	terior: 🗌 None 🗌 Visible 🖬 Entere						al Evalu								r other bu	ulding		
Drawings Reviewed: Yes Soil Type Source:	Ø N	0			Pour			nless SL2	>	🛛 Ye	es, score	less that	n cut-off		outer bu	unuing		
Geologic Hazards Source:			-			off, if know		elles - P		🖾 Ye	es, other	hazards	present					=c }
Contact Person: Chad	Ta	des	no.		Fallir Duild	ng hazard ing	is from t	aller adja	icent				End					
	~			-	Geol	ogic haza									commend			
LEVEL 2 SCREENING P		RME				ficant dar		eterioratio	on to		es, nonst o, nonstr	ructural h	azards e	identified	that sho may requ	uld be ev	ation but	a
Yes, Final Level 2 Score, SL2 Nonstructural hazards?			N N		ule s	tructural	system			de	tailed ev	aluation	is not ne	cessary			auon, bul	a
					_	-		_				nstructura				DNK		
Where inform Legend: MRF = Mor																		
BR = Brace	d frame	sung iran			einforced co hear wall	ncrete		URM INF TU = Tilt u	= Unreinfo	rced maso	onry infill	MH I M =	= Manufa = Light me	etal	using FI	D = Flexib	le diaphra diaphragn	gm

Structure 31, Building 23 Photographs



Exterior, Joint between Structures 31 and 32



Gymnasium



Interior, Damage to Masonry

Rapid Visual Screening of Buildings for Potential Seismic Hazards

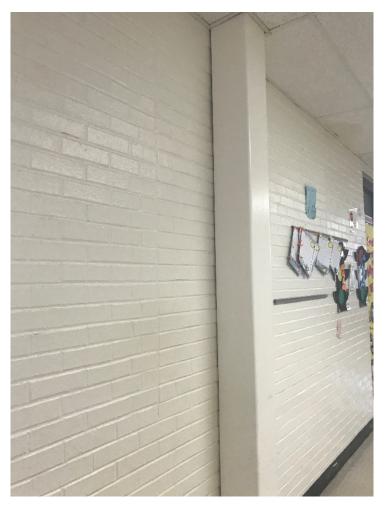
FEMA P-154 Data Collection Form

рнот	Othe Buil Use Latif Ss: Scre No. Tota Add Occ	er Ident ding Na : tude: <u>1,5</u> eener(s) Stories	Trendifiers: Trendifiers:	e Grade q. ft.): 1 one embly istrial ty B	TN WY SIA Yes, Y Comme Office Wareho	Below Cear(s) Bir rcial use	ongitu Sr: v Grade uilt: Emer, S Schoo Residen	de: <u>2</u> , <u>537</u> ate/Time : <u>0</u> ! <u>10</u> ! <u>0</u> ! <u>10</u> ! <u>10</u> ! <u></u>	•: <u>5/3</u> Year Code ☐ Hi ☐ Go lits:]F DI	23 7 Built: Year: storic overnmen	1130 A 199 b t □ Shelt t	I EST					
		mit	thi	sform		0	locic II	Hard Rock	Avg Rock	Dens Soi	I So	oil S	oil S	lioil		ume Type	
	-	0	in	5 10/17		**********	acency:	THE OWNER AND ADDRESS OF A	Liquefac	tion: Yes						upt.: Yes/l t Building	
	-1		oti	ner for	m		gularitie		U Ve		pe/severi						
Original	1						erior Fal ards:	lling	🔲 Ur	nbraced (arapets	Chimney	S		avy Clado endages		eavy Ver	ieer
	Ution ETCH						Addition	al sketch	es or com	nments c	on separa	ate page					
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO	S2	S3	S4	S5	C1		RE, S_L	PC1	PC2	RM1	RM2	URM	
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	FUZ	(FD)	(RD)	UKM	MH
Basic Score Severe Vertical Irregularity, VL1	-0.9	1.9 -0.9	1.8		1.4 -0.7	1.6 -0.8	1.4 -0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	1.0 -0.7	-0.7	1.1 -0.7	0.9 -0.6	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	-0.4	-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.7	-0.0	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6		-0.5 -0.2	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	3585	1.1	-0.3	-0.2	-0.1 NA	-0.1 1.4	-0.2 1.7	0.0 NA	-0.2 1.5	-0.1 1.7	-0.2	-0.2 1.6	0.0 NA	0.0
Soil Type A or B	0.5	0.5	0.4		0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.0
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.2 -0.4	-0.4	1002	-0.2	-0.2 NA	-0.2	-0.1	-0.1	-0.2 -0.3	0.0	-0.2 NA	-0.1 -0.1	-0.2	-0.2 -0.2	0.0	-0.1
Minimum Score, SMIN	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	-0.1	-0.2	-0.2	0.0	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	: 2	.Fr	0,3	,													
EXTENT OF REVIEW				OTHE	RHAZ	ARDS			ACT	ION R	EQUIR	RED					
Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Chad So	Are Ther Detailed Poun cut-o Fallir build	e Hazaro Structur ding pote ff, if know g hazaro ing	ds That T al Evalu ential (ur vn) ds from ta	Trigger / iation? hless S _{L2} aller adja	> acent	Detaile	ed Struc es, unkno es, score es, other o	tural Eva own FEM less than hazards	aluation A buildir n cut-off present	ng type o	r other bu	Ū	eck one)				
LEVEL 2 SCREENING PERF	ORME	D?			ogic haza ficant da						ructural h						
Yes, Final Level 2 Score, SL2	SILVE		0		tructural		Renoratio	JII (O		o, nonstru	uctural ha	azards e	xist that	may requ	ire mitig	ation, but	a
Nonstructural hazards? Yes											aluation i			ed b	DNK		
Where information	cannot k	e verifie	d, scr	eener sha	I note th	e follow	ing: E	ST = Esti								-	
Legend: MRF = Moment-re BR = Braced frame	sisting fran	10	RC = R	einforced co		1		= Unreinfo	rced masc		MH	ACCORD NO.	ctured Ho			le diaphra	gm

Structure 32, Building 23 Photographs



Exterior, Joint between Structures 31 and 32



Previous Exterior of Structure 31, Column Added to Support Addition of Structure 32

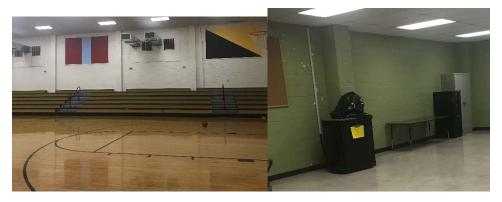
Level 1 VERY HIGH Seismicity

	Oth		ifiers: 3	KV:11	esth	York	cv; lle	<u>z</u> <u>p</u> d z	(ip: <u>3</u> {	338 0	1						
						Bui	ding Na	ime: Lew	Pup	1.01	Siles	-1			_		- Ten
						Lati	tude:	36.0	AJA	47	scho	Longitu	de:	89.	1199	47	
PHO.	OGRAP	Н				Ss:	1.7	706	16.	10		S1: O	,602	- 11	1110	10	
						Scr	eener(s):(CM			0.00	ate/Time		30	IIAN	\wedge
						Tota		Area (so		32	1550	w Grade	9.80	Code	r Built: Year:	19401	EST
							upancy	: Ass Indu	embly Istrial	Comme Office	ercial	Emer. S	ervices	Hi G	istoric overnmer	Shelt	ter
						Soil	Туре:	Utili Hard	B Avg	Wareho Den	C S	D D	oft P	F D	NK DNK, ass	ume Type	D.
	Г					Geo	logic H	Rock	Rock	So ction: Ye				oil No/DNK	Surf D	upt.: Yes/	
	H					CONTRACTOR OF THE OWNER	acency:									t Building	
L						Irre	gularitie		X Ve	ertical (ty	pe/sever	ity) S	rant	a si-	te lw		,
						Exte	erior Fa	llina			Chimney					eavy Ver	noor
		1					ards:			arapets						ouvy voi	
							MMENT										
	-		-		-		m	el (ry,	Mas	den	ceil	ing				
	r	1	-				40	01 1	du		C		J	1			
			-			-	- STE	er	0100	11	2						
		L				1	St	rige	ic S	ite							
			-			-			0								
		1		_		-											
SI	KETCH B	ASIC	sco	RE, MO	DIFIER			al sketch					-			-	
FEMA BUILDING TYPE Do No	W1	W1A	W2	S1	S2	S 3	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
Know	-			(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score Severe Vertical Irregularity, VL1	-0.9	1.9 -0.9	-0.9		1.4 -0.7	1.6 -0.8	-0.7	-0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	1.0 -0.7	1.1 -0.7	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5		-0.4	-0.5	-0.4	0.3	-0.4	-0.4	-0.0	-0.4	-0.7	-0.7	-0.7	-0.6	NA NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	673.6	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code Post-Benchmark	-0.3	-0.3	-0.3	2000	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	1.9 0.5	1.9	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	0.3 -0.2	0.4 -0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.2	-0.1	-0.1	-0.2	0.0	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.2	0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$	v:	0,4	之	5.5)													
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIF	RED				1	
	All Sides	Aeri	ial	Are There	e Hazard	s That	Trigger /	A	Detail	ed Struc	tural Ev	aluation	Require	d?			
Interior: None Drawings Reviewed: Yes Soil Type Source:	ered	Detailed Poun				>	A Ye	es, unkno es, score	own FEM less that	A buildir n cut-off	ng type oi		uilding				
Geologic Hazards Source:	-		-		f, if know		aller adia		Ye Ye	es, other	hazards	present	NA				
	acks	n		Fallin buildi	g hazard ng	s from ta	aller adja	icent	Detail		tructure	Evolue	tion Dee		1.10 (-)		
			-	Geolo	ogic haza											eck one)	
	ORME				icant dar ructural s		terioratio	on to		o, nonstr	uctural h	azards e	identified	that sho	uld be ev	aluated ation, but	ta
Yes, Final Level 2 Score, SL2		N N		ule SI	incural s	system			de	tailed ev	aluation	is not ne	cessary		ine mugi	adon, put	d
Nonstructural hazards? Yes					_					o, no nor	structura	I hazard	s identifie		DNK		
	cannot k	e verifie	d, scr	eener shal	note the			ST = Esti = Unreinfo			ble data	OR	DNK = D	o Not Kr	low	-	-
MDE - Mamont -	Where information cannot be verified, screener shall note to end: MRF = Moment-resisting frame RC = Reinforced concrete BR = Braced frame SW = Shear wall																

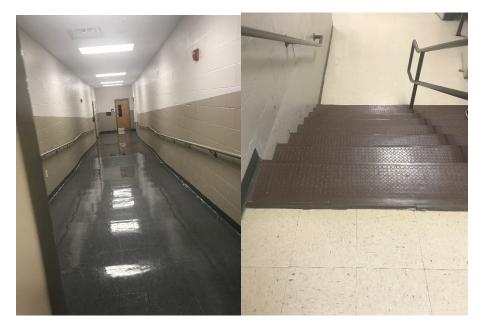
Structure 33, Building 24 Photographs



Exterior



Interior, Encased Steel Columns



Interior, Sloping Site

\cap								Iress: _	Ru	they	Kno	X St	i. J		Zip: 3	836	9	
							Buil Use	Iding Na	me:	ento	WY g	Scho	longitu	de:	881	926	899	
	РНОТО	GRAP	н				Ss:	1.4	01				S1: C),49	0			
								eener(s)	and the second second second		_				e: <u>51</u>		and the second second	
							Tota Add	Stories: al Floor litions:	Area (so	1. ft.): one	21] Yes, Y	(ear(s) B	uilt:		Year Code	Built: 1 Year:	940	EST
							Occ	upancy		embly strial y	Comme Office Wareho		Emer. S Chool Residen	ervices itial, #Ur		storic overnmer	☐ Shelt nt	er
							Soil	Туре:	Hard Rock	Avg Rock	Den: Soi	se S	tiff S	oft P		NK DNK, assi	ume Type	D.
			1				Geo	logic Ha	azards:	Liquefac	tion: Yes	/No/DNI	< Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/	No/DNK
				0			Adja	acency:		D. Po	ounding		Falling H	azards fr	om Taller	Adjacen	t Building	
							Irreg	gularitie	s:		ertical (ty an (type)	pe/sever		itrav	t Co	ner	,	
								erior Fal ards:	ling		arapets	Chimney	ſS		avy Clado pendages		eavy Ven	ieer
		4			-	-		MMENT					0					
	1.84			1			1	M	a sor	iry	'SY'6	sin	sorce	ed.				
4	addition			195														
1		C VIEWE	-	TIT	histo	1000	-											
			1		other.	and the second second second second												
	SKE	тсн						Addition	al sketch	es or con	nments o	n separa	ate page					
		В	ASIC	sco	RE, MC	DIFIE												
	FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
	Basic Score Severe Vertical Irregularity, VLr	3.6 -1.2	3.2 -1.2	2.9		2.0 -1.0	2.6	2.0	1.7 -0.8	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
	Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	82.0	-0.6	-0.7	-1.0 -0.6	-0.8	-0.9 -0.5	-1.0 -0.6	-0.7 -0.4	-1.0	-0.9 -0.5	-0.9 -0.5	-0.9 -0.5	-0.7 -0.4	NA NA
	Plan Irregularity, PL1 Pre-Code	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	0.0	-0.7	-0.4	NA
	Pre-Code Post-Benchmark	-1.1 1.6	-1.0 1.9	-0.9	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	-0.6	-0.8	-0.6 1.9	-0.2 NA	-0.4 1.9	-0.7 2.1	-0.1	-0.5	-0.3	95	-0.5	0.0	-0.1
	Soil Type A or B	0.1	0.3	0.5		0.6	0.1	0.6	0.5	0.4	0.5	NA 0.3	2.0	2.4 0.4	2.1	2.1 0.5	NA 0.3	1.2 0.3
	Soil Type E (1-3 stories)	0.2	0.2	0.1		-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
	Soil Type E (> 3 stories) Minimum Score, Smin	-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
	FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	6	5.2			0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
	EXTENT OF REVIEW	10	Aer		OTHE					-Wite Line W		EQUIF						
	Interior: None V Drawings Reviewed: Yes N Soil Type Source: Geologic Hazards Source:	tered	🗌 Fallir	Structur nding pote off, if know ng hazard	ral Evalu ential (ur wn)	ation?	>		es, unkno es, score es, other	own FEN less tha hazards	IA buildir n cut-off present		r other bu					
		KSO		_	build Geol		ards or S	Soil Type	F	11.11.11.11.11.11.11.11.11.11.11.11.11.					commend	200.00 m # 2000		
\cap	LEVEL 2 SCREENING PERFORM Yes, Final Level 2 Score, SL2 Nonstructural hazards?	RME	_	10 10	Signi		mage/de	eterioratio		D No de	o, nonstru tailed ev	uctural h aluation	azards e is not ne	xist that	I that sho may requ ed	uld be ev ire mitiga	valuated ation, but	a
	Where information c	annot b	e verifie	ed, scr	eener sha	ll note th	e follow	ing: ES	T = Esti		1.				-		-	
	Legend: MRF = Moment-resis BR = Braced frame		1e	RC = R	einforced co		1	URM INF = TU = Tilt u	Unreinfo			MH		ctured Ho	using FI	C SUCCESSION OF	le diaphra	gm

Structure 34, Building 25 Photographs



Exterior



Exterior

				-			Add	lress: _		N, herfo			ł,		Zip: 31	8360	1	
							Oth	er Ident				10				0.00		
								Iding Na					1				1	
							Use	E	lew	lent			10					
							Lati	tude:	361	158		}	Longitu	ide: - S	88,0	187	676	
	PHOTO	OGRAP	Н				Ss:		401				S1: 0	1,490)			
							Scr	eener(s)): <u>C</u>	M						30 (0 103	DAM
								Stories		ve Grade			w Grade			territe and the second	1980	
								al Floor litions:	Area (s		Yes,	140 (ear(s) E		1940	Code	Year:		-
							Occ	upancy		embly ustrial ity	Comme Office Wareho	(Emer. S Schoo Resider	Services ntial, #Ur		storic overnme	Shelt Shelt	er
							Soil	Type:	Hard Rock	Avg Rock	Den So	se S	tiff S	Soft P		NK DNK, ass	ume Type	D.
							Geo	logic H	azards:	Liquefa	ction: Yes	/No/DN	K Lands	lide: Yes	/No/DNK	Surf. R	upt.: Yes/	No/DNk
			-		-			acency:		****	ounding						t Building	
		-		-			- and	gularitie			ertical (ty lan (type)	pe/sever						
								erior Fal ards:	lling	Ο υ	nbraced arapets		/S		avy Clado bendages		eavy Ver	ieer
I		-		-			co	MMENT	S:		-uier	-			-	-		
	0			1	-	1	1	m	1501	nr 1	1							
	0	in ic	inc	41			-	1.0			1							
ALLE	T		5	-			-											
Addition			1				-											
			- 1	111	thisto	m	-											
	4		-		other f		-											
			1	-	once t	J.W.	-											
	SKI	ТСН						Addition	al skotch	ies or cor	nmente e	n conor	ato nace					
			ASIC	sco	RE, MO	DIFIE									-			-
FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score		3.6	3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF)	1.5	2.0	INF)		14	in		10	4.5
Severe Vertical Irregularity, VL1		-1.2	-1.2	-1.2		-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	1.6 -1.0	1.4 -0.9	-0.9	1.7 -0.9	1.0 -0.7	1.5 NA
Moderate Vertical Irregularity, V	L1	-0.7	-0.7	-0.7		-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1 Pre-Code		-1.1 -1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark		-1.1	-1.0	-0.9		-0.6 1.4	-0.8 1.1	-0.6 1.9	-0.2 NA	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B		0.1	0.3	0.5		0.6	0.1	0.6	0.5	0.4	0.5	NA 0.3	2.0	2.4	2.1 0.5	2.1 0.5	NA 0.3	1.2
Soil Type E (1-3 stories)		0.2	0.2	0.1		-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	0.3 -0.4
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMIN		14	0.9	0.7		0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE,		(1	·1.F	0,3	,													
EXTENT OF REVIEW	1				OTHER	RHAZ	ARDS			ACT	ION R	EQUIF	RED					
Exterior: A Pa Interior: A No Drawings Reviewed: A Ye	one 🗖 \	Visible	Aer		Are Ther Detailed	Structur	ai Evalu	ation?			ed Struc	tural Eva	aluation	na type o	d? r other bu	ildina		
Soil Type Source:	es 🔍 I	0			De Poun	ding pote	ential (ur	nless SL2	>	X Ye	es, score	less that	n cut-off	3 9 9 0 0				
Geologic Hazards Source:		-			cut-o	ff, if know g hazard	vn) s from to	aller adia	cent	Ye Ye	es, score es, other o	hazards	present					
Contact Person: Ch	ad Jac	ksor	1		buildi	ing												
LEVEL 2 SCREENING					Geolo	ogic haza	rds or S	oil Type	F								eck one)	
		JRIME			Signit	ficant dar tructural s	mage/de	terioratio	on to		es, nonstr o, nonstri	uctural h	azards e	xist that	that sho	ire mitic	aluated ation, but	a
Yes, Final Level 2 Score,			N		ule S	oucturals	system			de	tailed ev	aluation	is not ne	cessary		and a second	adon, but	a
	Yes				1		_				o, no non				ed 🎽	C DNK		
	nformation o											ble data	OR	DNK = D	o Not Kn	ow	-	
Legend: MRF = BR =	= Moment-resi Braced frame	sting fran			einforced cor hear wall	ncrete	l	JRM INF = TU = Tilt u	= Unreinfo	orced mase	onry infill			ctured Ho	using FL) = Flexib	le diaphrag	gm
DIVE					noai wali			10 - Tit U	h			LM :	= Light me	etal	RI	D = Rigid	diaphragm	

Structure 35, Building 25 Photographs

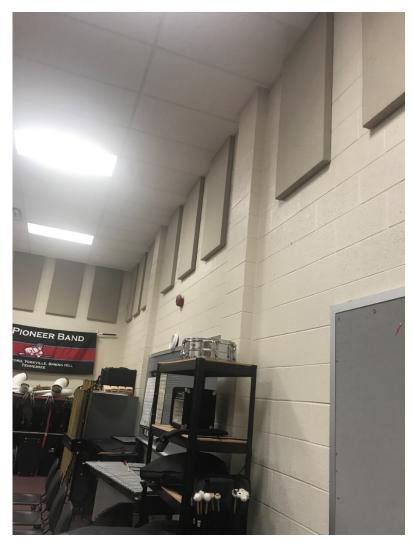


Masonry, Visibly Aged



Updated Section (Covered Older Large Window Opening)

			Othe	er Identi ding Na	fiers:		fordy	TN		Z	(ip: <u>3</u>	836	1				
						Use:	E	em	ento	WY S	schor	51	-	10			
DUCT						Latit	ude: 5	611	2915			Longitu	de:	88.0	18'4	>66	
PHOTO	OGRAP	н					ener(s)						ate/Time		00	10:30	nu
									ve Grade	. 1	Dala		: 0			and the second second	100000
						Tota	I Floor	Area (se	q. ft.): _	1,50				-	e Year:	20001	EST
						Occi	upancy		embly ustrial ity	Comme Office Wareho		Emer. S School Residen			istoric overnmer	Shelt Shelt	ter
						Soil	Туре:	Hard Rock	Avg Rock	Den So	se S]D	Be C	F D	NK DNK, ass	ume Type	D.
				1		Geo	logic Ha	zards:	Liquefac		3	96 L	1000		Surf. Ru	upt.: Yes/	No/DN
	1						cency:			ounding			azards fro				
							ularitie	s:		ertical (ty an (type)	pe/sever						
	L	-					rior Fal ards:	ling		arapets	Chimney	'S		avy Clade endages		eavy Ver	neer
							MMENT										-
		1					· m	as	onr cfo rs(f	v il	ns;c	le					
							. 0	. 1	2.	1	0						
	F						.P	rick	- +0	rcau	16						
		1	4	histo	sim	_	·P'	110	rs (F	rob	ably	, St	eer)			
		Ľ		other	form		1							/			
SK	ETCH								ies or con								
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO	S2	S3	S4	S5	EVEL '	C2	RE, S	L1 PC1	PC2	RM1	RM2	URM	
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INE)	(MRF)	(SW)	(URM INF)	(TU)	FUZ	(FD)	(RD)	URM	MH
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.2	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2	-1.2	-1.2	-1.0	-1.0 -0.6	-1.1 -0.7	-1.0 -0.6	-0.8 -0.5	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.0	-0.7	-0.0	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5 -0.6	-0.5	-0.5	-0.4	NA NA
Pre-Code	-1.1	-1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0,2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.7	0.0	-0.
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	-0.5	-0.6	-0.9	-0.6	-0.6 0.5	NA 0.6	-0.6 0.5	-0.4 0.5	-0.5	-0.7	-0.3 0.3	NA 0.2	-0.4	-0.5	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 2 SMIN			0,5		0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
the second s	(17	1,5	Contraction of the				-	-			-				_	
EXTENT OF REVIEW		CICEDON NO. 14		OTHER		1603600EC-TE			ACT	ION R	EQUIF	RED					
Exterior: 🛛 Partial	All Sides			Are Ther					Detaile	ed Struc	tural Ev	aluation	Require	d?			
	Visible No	Ente	ered	Detailed					Ye	es, unkno	own FEM	A buildir	ng type or	r other b	uilding		
Soil Type Source:				Poun			less SL2	>	Ye Ye	es, score	less that	n cut-off					
Geologic Hazards Source:					ff, if knov g hazard		iller adja	cent		es, other	hazards	present					
Contact Person:	acks	no		build	ing				Distantine State		tructura	I Evalua	tion Rec	ommen	ded? (ch	eck one)	
Contact Person: Unad St				Geol	ogic haza ficant dar	ards or So mage/det	oli iype	n to	Ye	es, nonst	ructural h	nazards	identified	that sho	uld be ev	aluated	
01 -00 13	ORME	D?											u				
LEVEL 2 SCREENING PERF	ORME			the s	tructural	system	onorabo			o, nonstr	uctural h	azards e	xist that r	may requ	ire mitig	ation, but	ta
LEVEL 2 SCREENING PERFO	ORME	N		the s	tructural	system			de	tailed ev	aluation	is not ne	cessary			ation, but	ta
LEVEL 2 SCREENING PERF			0	the s	tructural	system			de No	tailed ev o, no nor	aluation structura	is not ne al hazard	cessary Is identifie	ed 🔰		ation, but	ta



Structure 36, Building 26 Photographs

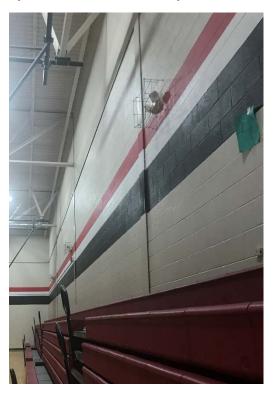
Interior, Steel Encased Columns (one-room building)

		1			100	Add	ress:	108	N.	Kn	ax	t				-	
							-	RU	the	rta	d't	N	7	ip: 2	836	q	
						Oth	er Ident	ifiers:	37	10	071	N			0.06	1	
							ding Na										
						Use	: E	len			Scho	10		- 11-22 - 22			
						Lati		36,17	293	46	1	ongitu	de: 🗂	88.	187	883	,
PHOT	OGRAP	Н				Ss:	17					S1: (1,490)			
						Scr	eener(s)	: <u>C</u>	M			D	ate/Tim	e: 51	30 1	0:304	IM
						No.	Stories	: Abov	e Grade		Below	v Grade	: 6	Yea	r Built: "	2000 1	EST
								Area (so			520				e Year:	4000	
						Add	litions:	N 12	one	Yes,	rear(s) B	uilt:		-			
						Occ	upancy		embly	Comme		Emer. S	ervices	Пн		Shelt	er
									ustrial	Office		School			overnmer	nt	
							_	Utili		Wareho			tial, #Ur				
					in the second	Soil	Type:	Hard	Avg	Den		1000			NK and	ume Type	
								Rock	Rock	So		100		Soil	DIVN, dss	ume rype	D.
						Geo	logic H	azards:	Liquefac	tion: Yes	s/No/DNH	(Lands	lide: Yes	/No/DNK	Surf. R	upt.: Yes/	No/DNK
							acency:			ounding						, t Building	
		1				-	gularitie			ertical (ty an (type)	pe/sever						
						- Fut	nian Eal						<u> </u>				
							erior Fal ards:	lling	P	arapets	Chimney	S		avy Clad bendages		eavy Ver	neer
						co	MMENT	S:	0	ther:		-				-	
						-	. 0.	~~~									
						-	.0	100									
						-	151	100	Fra	0.00	Stee	1 1.		ادم	10.01		
		1	-			-	- 04	-eci	114	milly	Stee	1 th	035	(611	11/101	1	
		-			-	****									6)	
		-	-	-		-											
						-											
SH	ETCH						Addition	al sketch	es or cor	nments o	on separa	ite page					
		-	-	RE, MO		RS, A											
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2	-1.2	-1.2		-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.7		-0.6	-0.7 -0.9	-0.6	-0.6	-0.5	-0.6	-0.4	-0.6 -0.7	-0.5	-0.5	-0.5	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.0	-0.0	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	-0.1
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	-0.3	-0.6	-0.9	-0.6	-0.6 0.5	NA 0.6	-0.6	-0.4	-0.5 0.3	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN		17.	20		0.0	0.0	0.0	0.0	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW		0		OTHER	RHAZ	ARDS	;		ACT	ION R	EQUIF	RED	1				
	All Sides	Aer	ial	Are Ther	e Hazard	s That	Trigger /	Ą			tural Eva		Require	d?			
	Visible	Ent	ered	Detailed	Structura	I Evalu	ation?		a second second		own FEM				uilding		
Drawings Reviewed: Yes Soil Type Source:	No				iding pote		nless SL2	>	🛛 🗹 Yı	es, score	less than	n cut-off	-9 -9 to 0		unung		
Geologic Hazards Source:					ff, if know ig hazard:		aller adia	cent			hazards	present					
Contact Person: Chad	Tay	.son	1	build	ing						tructural	Evalue	tion De-	ommer	dada (ch	ook	
LEVEL 2 SCREENING PERF	0			Geol	ogic haza	rds or S	oil Type	F			tructural ructural h						
Yes, Final Level 2 Score, SL2	ONNE			Signi the s	ficant dan tructural s	vstem	elerioratio	Dri to		o, nonstr	uctural ha	azards e	xist that	may real	uire mitia	ation. but	a
Nonstructural hazards?				010 0		Jotom			de	tailed ev	aluation	s not ne	cessary				
		The second	10-		ll made at						structura				DNK		
Where information							ALL	10/20/				and the second second					
Legend: MRF = Moment-re BR = Braced fram				einforced co hear wall	ncrete		URM INF TU = Tilt u	= Unreinfo Ip	rced mase	onry infill	MH LM =	= Manufa = Light me	ctured Ho etal	using F R	D = Flexib D = Rigid	le diaphrag diaphragm	gm 1

Structure 37, Building 27 Photographs



Gymnasium, Steel Truss System at Roof



Steel Columns Exposed

	Level 1
HIGH	Seismicity

						Add	ress:	327	ZE	Co.	llege	St					
						Product	_	Dv	er,7 38	N	2		Z	ip:	382	30	1
						Othe	er Ident	ifiers:	38'						~~~		
						Buil	ding Na	me:									
						Use			ile 5					20		- 05	
									696	-92		ongitu	de:	881	988	583	>
РНОТС	OGRAPI	н				Ss:	1.3	: CI					te/Time		10	10'20	mila
5-11 SIP						-		201 - B 1 - 10			P.I.		CONTRACTOR OF	-particular	-	10:30	10
						Tota		Area (so		A CONTRACTOR OF THE OWNER	850			-	Year:	939 0	EST
							upancy		embly	Commer		Emer. S	996	D Hi	etorio	Shelte	
							apanoy		ustrial	Office Warehou		\$chool	tial, #Un	G	overnmer		31
			_			Soil	Type:	Hard	□B Avg	Dens	se St	iff S	oft Po	oor If	NK DNK, ass	ume Type	D.
Partnerson		-	anterna .	1 0		1000	logio II	Rock	Rock	Soi		and the second second		oil			
	atte			thisf	orm		acency:			tion: Yes						upt.: Yes/N t Building	lo/DNK
JYM		11	I	Anoth	er form		gularitie		🖄 Ve		pe/severi	ity) SF	Alt k	arel-		d	
		-	-				erior Fal	lling	U	hbraced						eavy Ven	eer
			11				ards:			arapets ther:			App	endages	1		
							MMENT					•					
	Г	-				1	M	ison	ry.	,un	ve;	NFO	9)Y	ch			
Addition	H	- 1	-				1		,				~				1
(Foyer)			-			-											1.5
(Lader)				-													
		1		-		-											
						-											
SK	ETCH						Addition	al sketch	les or con	nments o	n separa	ate page					_
	в	ASIC	sco	RE, MO	DIFIER									-	1		
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9		2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2	-1.2	-1.2		-1.0 -0.6	-1.1 -0.7	-1.0	-0.8 -0.5	-0.9	-1.0 -0.6	-0.7 -0.4	-1.0 -0.6	-0.9 -0.5	-0.9 -0.5	-0.9 -0.5	-0.7	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	(-0.4)	NA
Pre-Code Post-Benchmark	-1.1	-1.0 1.9	-0.9	285-11	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	0.1	0.3	2.2	1.4	1.4	1.1 0.1	1.9	NA 0.5	1.9	2.1 0.5	NA 0.3	2.0	2.4	2.1	2.1 0.5	NA 0.3	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	0.3 -0.4
Soil Type E (> 3 stories) Minimum Score, SMIN	-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	1.1	20	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW	(1	2.6			RHAZA	RDS		-	ACT		FOLUE	ED		-		-	-
_					e Hazards			A					Require	d2			
	All Sides	Aeri	al	Are men				-					and reserves				
Interior: 🖸 None 🔲	Visible			Detailed		I Evalu	lation?		Ye	es, unkno	wn FEM	A buildin	ng type o	other h	uilding		
Interior: INone Drawings Reviewed: Yes				Detailed	Structura ding poter	ntial (ur	and the second second	>	Ye 🛛	es, unkno es, score	less than	n cut-off	ig type o	r other bi	uilding		
Interior: 🖸 None 🔲	Visible			Detailed Poun cut-o	Structura ding poter ff, if known	ntial (ur 1)	nless SL2		Ye Ye	es, score es, other	less than	n cut-off	ig type o	r other bi	uilding		
Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	Visible	Ente		Detailed Poun cut-o Fallin buildi	Structura ding poter ff, if known g hazards ing	ntial (ur 1) : from ta	nless S _{L2} aller adja	icent		es, score es, other	less than hazards	n cut-off present			5	eck onal	
Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Cho.d. Soc	Visible No			Detailed Poun cut-o Fallin buildi Geolo	Structura ding poter ff, if known ig hazards ing ogic hazar	ntial (ur 1) from ta ds or S	nless S _{L2} aller adja Soil Type	icent F	Ye Ye No Detaile	es, score es, other o ed Nonst	less than hazards tructural	n cut-off present I Evalua	tion Rec	ommene	ded? (ch	eck one) valuated	
Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Contact Perso	Visible No		ered	Detailed Poun cut-o Fallin buildi Geole Signi	Structura ding poter ff, if known g hazards ing	ntial (ur 1) from ta ds or S lage/de	nless S _{L2} aller adja Soil Type	icent F		es, score es, other o ed Nonst es, nonstr o, nonstru	less than hazards tructural ructural h uctural ha	n cut-off present I Evalua nazards i azards e	tion Rec	ommeno that sho	ded? (ch		а
Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Cho.d. Soc	Visible No		o	Detailed Poun cut-o Fallin buildi Geole Signi	Structura ding poter ff, if known g hazards ing ogic hazar ficant dam	ntial (ur 1) from ta ds or S lage/de	nless S _{L2} aller adja Soil Type	icent F		es, score es, other ed Nonsi es, nonstru o, nonstru tailed ev:	less than hazards tructural ructural ha uctural ha aluation i	n cut-off present I Evalua nazards i azards e is not ne	tion Rec identified xist that i cessary	ommeno that sho may requ	ded? (ch uld be ev lire mitig	valuated	а
Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Cho.d. Soc. LEVEL 2 SCREENING PERFORM Yes, Final Level 2 Score, SL2			o	Detailed Poun cut-o Fallin buildi Geole Signi the s	Structura ding poter ff, if knowi g hazards ing ogic hazar ficant dam tructural s	ntial (ur 1) from ta ds or S age/de ystem	nless S _{L2} aller adja coil Type eterioratio	F on to	Detaile	es, score es, other o ed Nonst es, nonstr o, nonstru tailed evi o, no non	less than hazards tructural ructural ha aluation i structura	n cut-off present I Evalua nazards i azards e is not ne il hazard	tion Rec identified xist that i cessary s identifie	ommeno that sho may requ	ded? (ch uld be ev lire mitig	valuated	а
Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Condact Perso	Visible No DRME cannot b	D? N N e verifie	o o d, scr	Detailed Poun cut-o Fallin buildi Geole Signi the s	Structura ding poter ff, if known g hazards ing ogic hazar ficant dam tructural s	ntial (ur 1) from ta ds or S age/de ystem	nless S _{L2} aller adja coil Type eterioration	F on to ST = Esti	Detaile	es, score es, other o ed Nonst es, nonstru tailed evi o, no non r unrelia	less than hazards tructural h uctural ha aluation i structura ble data	n cut-off present Evalua nazards i azards e is not ne il hazard	tion Rec identified xist that i cessary s identifie	ommeno that sho may requ ed O Not Kr	ded? (ch uld be ev ire mitig DNK	valuated	

Structure 38, Building 28 Photographs



Interior, Aged Masonry

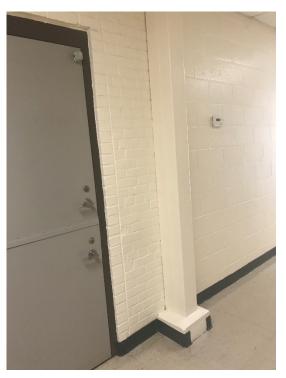


Exterior, Structure 38 Right and 39 Left

	Level 1
HIGH	Seismicity

												t	Z	ip: <u>3</u>	833	0	
						Use		Midd	bg i			ongitu	de: -	88,0	180	178	
РНОТ	OGRAP	н				Ss:		356		100			0,4'		100	140	
						Scre	eener(s)	:	CM	_		Da	ate/Time	:]/	240	10:3	MAG
						10000	Stories:		e Grade	_		w Grade	: 1	Year	Built:	19960	EST
1 - 2 약 - 2 PR 7 PA						100000	al Floor	Area (so		27	ear(s) B		00 0	-	Year:		_
							upancy	: Asse Indu	embly istrial	Comme Office	rcial	Emer. S		Hi Go	storic overnmen	Shelte	er
			_			Soil	Type:	Utilit DA Hard	B Avg	Wareho Dens	C C]D	oft P	JF Di	NK DNK, assi	ıme Type	D.
			T	1 0		Goo	logic U	Rock	Rock	Soi					0.45		
		14	100-	this fo	m	1	acency:			ounding				om Taller			
2 Sim			1	other	form		gularitie		🗆 Ve		pe/sever				nyacen		
			-	-			erior Fal ards:	lling		nbraced arapets	Chimney		Hea	avy Clado pendages	ling or H		neer
Origin	al					co	MMENT	S:									_
Addition (Foyer)	ILCI						re	into	rced	- MA	(rson	nry	(
SK	ETCH						Addition	al sketch	es or con	nments o	on separa	ate page					
	В	ASIC	sco	RE, MO	DIFIE							the second s	10.67	-			
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2 -1.2	2.9	1000	2.0 -1.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7		-0.6	-1.1 -0.7	-1.0 -0.6	-0.8	-0.9	-1.0 -0.6	-0.7	-1.0 -0.6	-0.9	-0.9	-0.9 -0.5	-0.7 -0.4	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	(-0.7)	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1 1.6	-1.0 1.9	-0.9		-0.6	-0.8 1.1	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	0.1	0.3	0.5	10.000	0.6	0.1	1.9	NA 0.5	1.9 0.4	2.1 0.5	NA 0.3	2.0	2.4	2.1	2.1 0.5	NA 0.3	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.1		-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	1.1	0.9	0.7	-	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW	. C	21/2	- 0 1		R HAZ			-	ACT		EQUIF	DED	-		_		
	All Sides		ial		re Hazard			4				aluation	Docuin	40			
Interior: Interi	Visible	Ent		Detailed Pour cut-o	Structur nding pote	al Evalu ential (ur vn)	nless SL2	>		es, unkno es, score	own FEM less tha		ng type o	r other bu	uilding		
Geologic Hazards Source: Contact Person:	Tack	-500		build					Datail		ter set	End	No. 5				
			-	Geo Geo	logic haza	rds or S	oil Type	F						ommend			
LEVEL 2 SCREENING PERF Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes	ORME			Sign Sign	ificant dar structural	mage/de system	eterioratio	on to	D No de	o, nonstru tailed ev	uctural h aluation	azards e is not ne	xist that cessary	I that sho may requ	ire mitiga	aluated ation, but	ta
												al hazard			DNK		
Where information	cannot b	be verifie	d, scr	eener sha	Il note th	e follow	ring: ES	ST = Esti	mated o	r unrelia	ble data	OR	DNK = D	Not Kr	IOW.		
Legend: MRF = Moment-re				einforced co					rced masc			= Manufa					

Structure 39, Building 28 Photographs



Interior, Joint between Structures 38 and 39



Exterior, Structure 38 Right and 39 Left

	Oth	er Ident	ifiers:	ELE, el J 10	N	ege	Sŧ.	Z	ip: <u>3</u>	833()						
РНОТ	OGRAP	H				Use Lati Ss:	tude: 13 eener(s)	1em	689	ory/f 42	L	.ongitu S1: 0	de:).47 ate/Time	5		267	MAG
						Tota		Area (so		5	5,90	v Grade	e <u>O</u>	Yea		9530	
							litions: upancy		embly Istrial	Yes, Y Comme Office Wareho	rcial (Emer. S School)		storic overnmer	Shelte	er
			-			Soil	Туре:	Hard Rock	B Avg Rock	Dens	c 🗖	D C	loft Po]F D	NK DNK, ass	ume Type	D.
						Geo	logic H					-			Surf. R	upt.: Yes/N	No/DNK
		1					acency:		D Po	ounding		alling H	azards fro	om Taller	Adjacen	t Building	
or.	Sir	191				Irreg	gularitie	s:		ertical (ty an (type)	pe/severi	ity) SI	plit 1 (trans	evel	Ino	d	
1 54-590	Ac	anop	1			10000	erior Fal ards:	lling		nbraced arapets ther:			Hea		ding or H	eavy Ven	ieer
				1050		U			rfar	Cel	人						
31	ETCH	ASIC	500	RE, MO	DIEIEI			al sketch							-		
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	.1 PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	(1.0)	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2	-1.2 -0.7	-1.2	1.2.2.2.4	-1.0 -0.6	-1.1	-1.0	-0.8 -0.5	-0.9	-1.0	-0.7 -0.4	-1.0 -0.6	-0.9 -0.5	-0.9 -0.5	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.0	-0.6	-0.5	-0.8	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA NA
Pre-Code Post-Benchmark	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	1.6	1.9 0.3	2.2	1.4	1.4 0.6	1.1	1.9	NA 0.5	1.9	2.1	NA 0.3	2.0 0.6	2.4	2.1 0.5	2.1 0.5	NA 0.3	1.2 0.3
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories) Minimum Score, SMIN	-0.3	-0.6 0.9	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	/	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
	(0.4	5-1-1				_		-	_	-			_		_	
Exterior: Partial Interior: None	terior: None Visible Entered Detailed Stru rawings Reviewed: Yes No									es, unkno es, score	tural Eva own FEM less thar	aluation A buildir n cut-off			uilding		
Geologic Hazards Source:										es, other	nazaros	present					
										ed Nonst	tructural	Evalua	tion Rec	ommen	ded? (ch	eck one)	
LEVEL 2 SCREENING PERFORM Yes, Final Level 2 Score, SL2 Nonstructural hazards?			0	Signii Signii the si	ficant da tructural	mage/de system	eterioratio	on to		es, nonstru o, nonstru tailed ev o, no non	ructural h uctural ha aluation i structura	azards azards e s not ne l hazard	identified exist that i ecessary Is identifie	that sho may requ ed	uld be er lire mitig		a
Where information											ble data	OR	DNK = D	o Not Ki	wor		
Legend: MRF = Moment-res BR = Braced frame	isting fram		RC = Re SW = S	einforced con hear wall	ncrete		URM INF TU = Tilt u	= Unreinfo	rced maso	onry infill	MH =	= Manufa = Light me	ictured Hoi			le diaphrag diaphragm	

Structure 40, Building 29 Photographs



Exterior, Gym @ Left End, Not Pictured



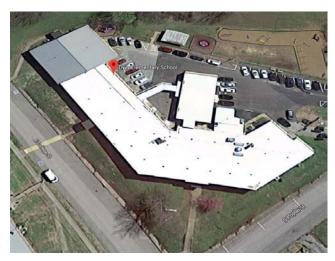
Exterior, Corner of Structure



Plan View, Structure 40 is L-shape and Green Roof Portion Structure 41 has a Hallway and Breezeway Connection to Main Building

		201				Add	dress:		LE,		ege ?	St.				0	
						Oth	er Ident		er,T	N	9		Z	ip: 3	835	0	
							er ident Iding Na	-	11								
						Use		-	Gaul	Elem	ont		Sela	1			
								36.0	68.7	67.	Erno	ongitu	de: -	88.	188	129	
PHOT	OGRAPI	н				Ss:		356	001	60		S1:	O.Y	JC.	00	01	
						Scr	eener(s)		CM				ate/Time	» Д	1241	@10.	SOAM
							Stories		e Grade		-	w Grade	: 0	Year	Built:	2015	EST
							al Floor ditions:			30			1 1 12	Code	Year:		
									one Ц embly	Yes, Y Commer			1953				
							upancy		istrial	Office Warehou		Emer. S School Residen			storic overnmer	Shelt	ter
						Soi	Type:		□в	D					NK		
				-	7			Hard Rock	Avg Rock	Dens Soil				oor <i>If I</i> ioil	DNK, ass	ите Туре	D.
7		-	-	1	-				Liquefac	tion: Yes							
Orig	ina	1					acency:		-	ounding			azards fro	om Taller	Adjacen	t Building	[
1)	-		1		Irre	gularitie	s:		ertical (typ an (type)	e/sever	ity) _					
shell ter							erior Fal ards:	ling		nbraced (arapets ther:	Chimney	rs		avy Clado pendages	-	eavy Ver	neer
1 1 cm	>					CC	MMENT	S:									
									an	NI							
	_						1	100	0111	Y							
		Ithi	is f	mo													
	-																
	L	701	her	form	2	-											
						-											
SK	ETCH	ASIC	800	RE, MC	DIEIE					nments o	and the second division of the second divisio	the second s		-		_	_
FEMA BUILDING TYPE Do Not	W1	W1A	W2	S1	S2	S3	S4	S 5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		-
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2 -1.2	2.9		2.0 -1.0	2.6	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	-0.9	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7		-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.9	-0.9	-0.7	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code Post-Benchmark	-1.1	-1.0	-0.9	2008	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	1.6	1.9 0.3	2.2		1.4	1.1	1.9	NA 0.5	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.1		-0.4	0.2	-0.1	-0.4	0.4	0.5	0.3 -0.2	0.6	0.4	0.5	0.5	0.3	-0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	1.	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMIN	1.1	0.9	0.7		0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:		(3,	OF	0,3				-					-	-		_	
EXTENT OF REVIEW	All Sides		ial	OTHE Are The						ION RI			Dent	40			
Interior: 🗋 None	terior: 🗋 None 🗌 Visible 🔀 Entered Detailed Stru									ed Struct es, unkno					ulding		
Drawings Reviewed: Yes X.	No						nless SL2	>		es, unkno				outer bl	unuing		
Soil Type Source:				cut-c	off, if know	wn)			1 Ye	es, other l							
Geologic Hazards Source: Contact Person:										0							
0.14.3			-	Geol	logic haza		Soil Type			ed Nonst							
LEVEL 2 SCREENING PERF	ORME	C. Callerin			ificant da structural		eterioratio	on to		es, nonstru o, nonstru	uctural h	azards e	xist that	may requ	uld be ev	aluated	ta
Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes			(CS)	ules	auotural	system			de	tailed eva	aluation i	is not ne	cessary			auon, pu	u
					II		da =	DT		o, no non					DNK		
Where information Legend: MRF = Moment-res	isting fram			einforced co			URM INF					A DESCRIPTION OF	DNK = D	Ment with the	and the second second	le dianhre	am
BR = Braced frame	y nan			shear wall	101010		TU = Tilt I	- Unidinit	nueu mas	vir A mum	MH	= Manuta = Light m	clured Ho	using Fl	U = Flexib	le diaphra	gm

Structure 41, Building 29 Photographs



Plan View, Structure 40 is L-shape and Green Roof Portion Structure 41 has a Hallway and Breezeway Connection to Main Building

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

and the second s										ti	- 1	1					100000000000000000000000000000000000000	-
											rent	on r	INI			222	^	
							0.1		VI	er, 7	112	-		Z	ip: <u>5</u>	833	0	
									ifiers:	76	-		-	-		-		
								ding Na		e . 1	- 1				_			
										SU			-		22	C	000	_
A. M.								tude: <	56:0	0249	91			de:	881	466	288	
	PHOTO	GRAP	Н				Ss:				_	5	i1:		-			
							Scre	eener(s)	i:		College		D	ate/Time	e:	_		
							No.	Stories	Abov	ve Grade	: 1	Below	Grade	: 1	Year	r Built:	19790	EST
1315 L. 1921									Area (se		86	502		-	Code	Year:		
							Add	litions:		lone	Yes,	Year(s) Bi	uilt: _	1996	20	Dg		
							Occ	upancy	: Ass	embly	Comme	ercial	Emer. S	ervices	H	istoric	Shelt	er
										ustrial	Office		School			overnmer	nt	
									Utili	ty	Wareho	use	Residen	itial, #Ur	its:			
							Soil	Type:		□в	Den	c 🗆	DC	E C		NK		
	1						-		Hard	Avg						DNK, ass	ume Type	D.
19961									Rock	Rock	So			2011	ioil			
	-	1		1	-		Chinese and					s/No/DNK						
				24			Adj	acency:			ounding						t Building	
		5		and a			Irreg	gularitie	s:	Ve R	ertical (ty	pe/severi	ty) Sf	rifle	1 level	mod	<i>.</i>	
	100	12	T				Ent	erior Fal	ling			Chimney					la au cult	analasi tab
the second se	them.		- Chang	1	His fo	100	10.200	ards:	ling		arapets	Chimney	5		endages		eavy Ven	leer
and a Reput state	an again	65 P	Same.	_ 12	This is	AWY									linuaye	,		
	The Prove		1	T	[Other	2	CO	MMENT	S:									
	the second		- Aritan	L	Tourd	1 GUY				~	1		11		1		1	
	1	-	T				-	°(/C	ma	. Ct	NUI	nns	th	NOL	Ah	-00	+	
	-		-				2	~	-			0			5			
	200	29					3											
	-	7	-	-														
			-															
		1	97	9			-											
						L	-											
	SKE	тсн						Addition	al sketch	nes or cor	nmonte	on separa	to nado					
		В	ASIC	sco	RE, MO	DIFIE												-
FEMA BUILDING TYPE	Do Not	W1	W1A	W2	S1	S2	S 3	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
	Know	1			(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score		3.6	3.2	2.9	- 21/042	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Severe Vertical Irregularity, VL1		-1.2	-1.2	-1.2		-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1		-0.7 -1.1	-0.7	-0.7		-0.6	-0.7 -0.9	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Pre-Code		-1.1	-1.0	-0.9	1.000	-0.6	-0.9	-0.7	-0.0	-0.6	-0.8	0.5	-0.7 -0.5	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark		1.6	1.9	2.2		1.4	-0.0	1.9	NA	1.9	2.1	NA	-0.5	-0.3	-0.5	-0.5	0.0 NA	-0.1 1.2
Soil Type A or B		0.1	0.3	0.5		0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)		0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories)		-0.3	-0.6	-0.9		-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, Smin		1.1	0.9	0.7		0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL	1 ≥ Smin:	0	1.23	2Q.	3)													
EXTENT OF REVIEW					OTHE	R HAZ	ARDS			ACT	ION R	EQUIR	ED				- A - A - A - A - A - A - A - A - A - A	
Exterior: X Partia		All Sides	Aer	ial	Are Ther				A	Detail	ed Struc	tural Eva	luation	Require	d?			
Interior: None			Ent	ered	Detailed	Structur	al Evalu	ation?		- 16		own FEM				uilding		
Drawings Reviewed: Yes Soil Type Source:	Ø,	00			Pour			nless SL2	>	X	es, score	e less than	n cut-off			and and a		
Geologic Hazards Source:				-	cut-c	off, if know	vn) Is from t	allor edi-	cont			hazards	present					
									Cent				F	41 F				
			-	-	Geol	ogic haza	ards or S	oil Type	F			tructural						
LEVEL 2 SCREENING		DRME				ficant da		eterioratio	on to		es, nonst	tructural h	azards	identified	that sho	uld be ev	valuated	
Yes, Final Level 2 Score, SL			N 🖄	ю	the s	tructural	system			de	tailed ev	uctural ha	s not ne	cessary	may requ	ure mitig	ation, but	а
Nonstructural hazards?	Yes			lo								nstructura			ed D	DNK		
Where info	rmation c	annot b	e verifie	d, scr	eener sha	ll note th	e follow	ing: E	ST = Est	imated o	r unrelia	able data	OR	DNK = D				-
Legend: MRF = N	oment-resi		ne	RC = R	einforced co					prced mase				ictured Ho			le diaphra	am
	iced frame				hear wall	neo neo		TU = Tilt u	ip		and and		Light m			D = Rigid	diaphragm)

Structure 42, Building 30 Photographs



Interior, Ground-Level Entries at Both Gym Floor and at Top of Bleachers

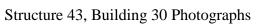


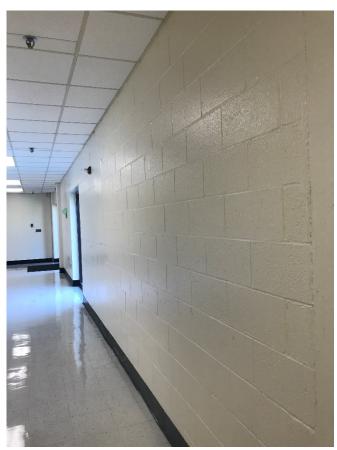
Joint Between Structure 42 (White Façade into Page) and Structure 44 (Stairs Out of Page)

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Address: 150 100 140 247 32 33 Building Name Use: Million Name Willion 100<		-					-	-	1.00	-		11	-				onne		
PHOTOGRAPH Building Name: Use: Use:							Add	Iress:				on H	WY			_		_	
Building Name: Building Name: Latitude: Chilling Name: Latitude: Chilling Name: Latitude: Chilling Name: Screener(b): Chilling Name: No. Stories: Abox Grade: Box Grade: Box Grade: Occupancy: Assertion: No. Stories: Non. Stories: Additions: Image: Name: Occupancy: Assertion: Soli Type: Image: Name: Occupancy: Assertion: Soli Type: Image: Name: Occupancy: Assertion: Soli Type: Image: Name: Image: Name: Image: Name:									121	101	TN			Z	ip: <u>3</u>	833	0		
PHOTOGRAPH Use: ILIANS SUMON Inorphited: S.S. Child, S.M. Streener(s): CAN Streener(s): CAN Data Time: Tide USE Streener(s): Streener(s): CAN Streener(s): CAN Data Time: Tide USE Streener(s): Streener(s): CAN Streener(s): CAN Data Time: Tide USE Streener(s): Cocupancy: Asserts/ Coreupancy: Asserts/ Cocupancy: Asserts/ Cocupancy: Streener(s): Constreener(s): Constreener(s): Constreener(s): Constreener(s): Cocupancy: Asserts/ Cocupancy: Asserts/ <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>45</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>-</td>										45						_		-	
PHOTOGRAPH Latitude::::::::::::::::::::::::::::::::::::										51	10.00	1							
PHOTOGRAPH Sr:							10000		ngh	2 SU	100				00	0110	100		
Screenrifs: CM Date/Time: T/2 CO Q SAM No. Stories: Above Grade: Book Crade: Deter Time: T/2 CO Q SAM No. Stories: Above Grade: Book Crade: Deter Time: T/2 CO Q SAM Common: Common: Deter Time: T/2 CO Q SAM Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: Common: <th colspan<="" td=""><td>BHOT</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>622</td><td>74</td><td></td><td></td><td></td><td>281</td><td>1668</td><td>10</td><td>_</td></th>	<td>BHOT</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>622</td> <td>74</td> <td></td> <td></td> <td></td> <td>281</td> <td>1668</td> <td>10</td> <td>_</td>	BHOT									622	74				281	1668	10	_
No. Stories: Above Grade: Var. Built: Utilt: Code Year: Total Floor Area (e, h): 35 3/L Code Year: Code Year: Code Year: Occupancy: Assentity Ornematic Earl: With: With: With: Occupancy: Assentity Ornematic Earl: With: With: With: Soli Type: Link: With:	PHOTO	JGRAP	н					_	210	c.m.			_	ate/Time	. 71	240	945 M	M	
Total Floor Area (cp, ft) Sol 1/gen Code Yar Code Yar Additions: None (VP, ft) Dit (TP) 2,004 Occupancy: Additions: None (VP, ft) Dit (TP) 2,004 Occupancy: Additions: None (VP, ft) Dit (TP) Dit Dit Dit <							_				. 1	Below			and all the second			_	
Addition: Invo: Every frag Bett: Every frag Bett: Invoid Invoid Every frag Bett: Invoid Invoid Every frag Bett: Invoid													Glaue	0			1946	L ESI	
Occupancy: Assertive Convention Estation Estation Utility Image: Solid State Provided in Convention Estate Provided in Convention Estate Provided in Convention Estate Provided in Convention Estate Provided in Convention Solid Type: Image: Convention Estate Provided in Convention Estate Provided in Convention Estate Provided in Convention Estate Provided in Convention Solid Type: Image: Convention Estate Provided in Convention Estate Provided in Convention Estate Provided in Convention Estate Provided in Convention Solid Type: Image: Convention Estate Provided in Convention Estate Provided in Convention Estate Provide in Convention Estate Provide in Convention Solid Type: Image: Convention Estate Provide in Convention Estate Provide in Convention Estate Provide in Convention Estate Provide in Convention Solid Type: Image: Convention Image: Convention Estate Provide in Convention Estate Provide in Convention Estate Provide in Convention Solid Type: Image: Convention Image: Convention Image: Convention Estate Provide in Convention Estate Provide in Convention <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Yes,</td><td>rear(s) B</td><td>uilt:</td><td>197</td><td>-</td><td></td><td></td><td></td></td<>											Yes,	rear(s) B	uilt:	197	-				
Induction Close of the second							Occ	upancy						ervices	1.6	Transidian lotton	Shelt	er	
Soil Type: B BC D E FM Box And Box									Indu			(School	7	G	overnmer	nt		
Hard Avg Örne Sitt Solt For II MAK assume Type D. Hard Avg Örne Sitt Solt Solt Solt Solt Solt Solt Solt For II MAK assume Type D. Gelogici Hazards: Upuefactor: VesNoDNK Landalde: VesNoDNK Surt. Rupt. YesNoDNK Adjacent Sult Hard Avg Örne Sitt Solt For II MAK assume Type D. Gelogici Hazards: Upuefactor: VesNoDNK Landalde: VesNoDNK Surt. Rupt. YesNoDNK Adjacency: Perunding Faller Massed Chinneys Heavy Cleding or Heavy Veneer Upuefactor: Other Other Other Appendages Other Other Other Other Appendages Additional alxetches or comments on segarate page Comments on segarate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, Sct FEMA BuilLoing TYPE Other Mith Vistor State Score State Score State Score State Score Additional alxetches or comments on segarate page Basic Score 3.5 3.2 2.9 2.1 2.0 2.6 2.6 1.1 1.5 2.0 1.5 1.6 1.4 1.7 1.7 1.5 1.5 1.5 2.0 1.5 1.6 1.4									Utili	ty			Residen	itial, #Un	its:				
Rode Rode <th< th=""><th></th><th></th><th></th><th></th><th>in the second second</th><th></th><th>Soil</th><th>Type:</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>une Tune</th><th></th></th<>					in the second		Soil	Type:									une Tune		
Geologic Hzards: Louedballow: YeshkolDVK Adjacency: Prounding Falling Hazards: Penunding Falling Hazards: United and the set of th	11001															DINK, assi	ume Type	D.	
Irregularities: Untrical (type/seventy) Irregularities: Vertical (type/seventy) Introduction Introduction Introduction Intretion Intretion	1430			1			Geo	logic H	azards:	Liquefac	tion: Ye	s/No/DNH	(Lands	lide: Yes	No/DNK	Surf. Ru	upt.: Yes/I	No/DNK	
Pinn (ppe) Pinn (ppe) Line and the state of th							Adj	acency:		D Po	ounding		alling H	azards fro	om Taller	Adjacen	t Building		
Exterior Failing Unbraced Chimneys Heavy Clading or Heavy Veneer Heaverds: Parapets Appendages Other: Other: Other: COMMENTS: Comments on separate page Sketcol Additional sketches or comments on separate page Basic Score Sketcol Sovere Ventral Imputanty, V.; 12 13 10 15 16 14 14 17 15 16 14 14 17 10 15 Severe Ventral Imegularity, V.; 12 12 10 1.0 1.1 10 65 05 05 06 07 09 03	Or Giv	la					Irre	gularitie	s:				ity) _	ne o ha e ana ana					
Image:	- Crepi	in	Ĩ				Ext	erior Fal	llina				s	□ Hea	vy Clade	ling or H	eavy Ven	eer	
COMMENTS: * Comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Ohne W1 Main Ministry Mi	19770	7		[1+1v	s form	Haz			D P	arapets						outy ten		
* C3 * C4 * C3 * C4 * C4 <t< th=""><th></th><th>-12</th><th></th><th>-</th><th>7.011</th><th>or fre</th><th>0</th><th></th><th>· C.</th><th></th><th>ther:</th><th></th><th></th><th></th><th></th><th></th><th>-</th><th>_</th></t<>		-12		-	7.011	or fre	0		· C.		ther:						-	_	
Additional sketches or comments on separate page Additional sketches or comments on separate page Basic Score Additional sketches or comments on separate page FMA BUILDING TYPE Do Not W1 W1 W2 Si		Dotter																	
Additional sketches or comments on separate page Additional sketches or comments on separate page Basic Score Additional sketches or comments on separate page FMA BUILDING TYPE Do Not W1 W1 W2 Si			T				-	" (S										
Additional sketches or comments on separate page Additional sketches or comments on separate page Basic Score Additional sketches or comments on separate page FMA BUILDING TYPE Do Not W1 W1 W2 Si		0		-			-												
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL: FEMA BUILDING TYPE Do Not WI WIA W2 NS S2 S3 S4 S5 C1 C2 C3 PC1 PC2 RM RMZ URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 8.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vortical Irregularity, V1, -1.2 -1.2 -1.0 -1.0 0.1 1.1 1.0 0.08 0.9 -1.0 0.7 0.6 0.6 0.4 0.6 0.5 0.5 0.4 NA Pre-Code -1.1 -1.0 0.9 0.6 0.6 0.6 0.6 0.7 0.6 0.6 0.6 0.7 0.6 0.6 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 <t< td=""><td>200</td><td>7</td><td>-</td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	200	7	-		-														
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL: FEMA BUILDING TYPE Do Not WI WIA W2 NS S2 S3 S4 S5 C1 C2 C3 PC1 PC2 RM RMZ URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 8.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vortical Irregularity, V1, -1.2 -1.2 -1.0 -1.0 0.1 1.1 1.0 0.08 0.9 -1.0 0.7 0.6 0.6 0.4 0.6 0.5 0.5 0.4 NA Pre-Code -1.1 -1.0 0.9 0.6 0.6 0.6 0.6 0.7 0.6 0.6 0.6 0.7 0.6 0.6 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 <t< th=""><th>Land Land</th><th>7-</th><th></th><th>-</th><th></th><th></th><th>_</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>	Land Land	7-		-			_												
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL: FEMA BUILDING TYPE Do Not WI WIA W2 NS S2 S3 S4 S5 C1 C2 C3 PC1 PC2 RM RMZ URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 8.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vortical Irregularity, V1, -1.2 -1.2 -1.0 -1.0 0.1 1.1 1.0 0.08 0.9 -1.0 0.7 0.6 0.6 0.4 0.6 0.5 0.5 0.4 NA Pre-Code -1.1 -1.0 0.9 0.6 0.6 0.6 0.6 0.7 0.6 0.6 0.6 0.7 0.6 0.6 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 <t< th=""><th></th><th></th><th>107</th><th>9</th><th></th><th></th><th>-</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>			107	9			-												
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not Know W1 W1 W2 S1 S2 R3 K4 (S5) C1 C2 C3 PC1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.0 1.6 1.4 1.7 1.7 1.0 0.9 -0.9 -0.9 -0.9 -0.9 -0.7 NA Moderate Vertical Irregularity, V _{L1} -0.7 -0.7 0.6 -0.6 -0.5 -0.6 -0.4 -0.6 -0.5 -0.5 -0.4 -0.7 -0.7 -0.6 -0.6 -0.8 -0.5 -0.7 -0.5 -0.5 -0.7 -0.6 -0.6 -0.7 -0.5 -0.7 -0.7 -0.6 -0.6 -0.6 -0.7 -0.7 -0.6 -0.6 -0.6 -0.7 -0.1 -0.5 -0.3 -0.7 -0.1			1			1	_												
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not Know W1 W1A W2 S1 S2 S3 S4 S5 C1 C2 C3 PC1 PC2 RM RMD URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 1.5 Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 1.5 Plan Inregularity, V _{Lr} -0.7 0.7 0.6	SKI	тсн						Addition	al sketch	es or cor	nments	on separa	ate page						
Know (NRF) (BR) (UN Processor (UN Processor <th></th> <th>В</th> <th>ASIC</th> <th>sco</th> <th>RE, MC</th> <th>DIFIE</th> <th></th> <th></th> <th></th> <th></th> <th>and the second se</th> <th>the second s</th> <th>the second s</th> <th></th> <th></th> <th></th> <th></th> <th></th>		В	ASIC	sco	RE, MC	DIFIE					and the second se	the second s	the second s						
Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.2 1.6 1.4 1.7 1.7 1.0 1.5 Severe Vertical Iregularity, V _{L1} -1.2 -1.2 -1.2 -1.0 -1.1 -1.0 -0.8 -0.9 -1.0 -0.7 -1.0 -0.7 -0.7 -0.6 -0.6 -0.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.7 -0.6 -0.5 -0.5 -0.5 -0.5 -0.5 0.5 0.0 -0.1 -0.5 -0.3 -0.5 0.5 0.3 <td< th=""><th></th><th>W1</th><th>W1A</th><th>W2</th><th></th><th></th><th></th><th>(RC</th><th>(URM</th><th></th><th></th><th>(URM</th><th></th><th>PC2</th><th></th><th></th><th>URM</th><th>MH</th></td<>		W1	W1A	W2				(RC	(URM			(URM		PC2			URM	MH	
Moderate Vertical Irregularity, V _{L1} -0.7 -0.6 -0.5 -0.5 -0.6 -0.4 -0.6 -0.5 -0.5 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.8 -0.2 -0.7 -0.7 -0.4 NA Post-Benchmark 1.6 1.9 2.2 1.4 1.4 1.1 1.9 NA 1.9 2.1 CM -0.6 0.6 0.6 0.4 0.5 0.3 0.6 0.5 0.3 0.3 0.6 0.6 0.6 0.6 0.6 0.6 0.		1000		0.000033			100000	100 C			1. W. 1988				1.7	1.7	1.0	1.5	
Plan Irregularity, PL1 -1.1 -1.0 -0.8 -0.7 -0.9 -0.7 -0.6 -0.8 -0.5 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.7 -0.4 NA Pre-Code -1.1 -1.0 -0.9 -0.6 -0.6 -0.6 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.2		1 2023	100000	1200	1.	1.	1.200-0	1000	1.					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0202	16 2		
Pre-Code -1.1 -1.0 -0.9 -0.6 -0.8 -0.6 -0.2 -0.4 -0.7 -0.1 -0.5 -0.3 -0.5 -0.5 0.0 -0.1 Post-Banchmark 1.6 1.9 2.2 1.4 1.4 1.1 1.9 NA 1.9 2.1 -0.7 -0.1 -0.5 -0.3 -0.5 0.0 -0.1 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.7 0.3 0.6 0.4 0.5 0.7 0.3 0.6 0.4 0.5 0.7 0.3 0.4 0.5 0.6		1	10000	1 39.55	1000	1000	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1000	10000	425550		1000			1 1000000		200		
Post-Benchmark 1.6 1.9 2.2 1.4 1.4 1.1 1.9 NA 1.9 2.1 No 2.0 2.4 2.1 2.1 NA 1.2 Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.5 0.3 0.3 Soil Type E (1-3 stories) 0.2 0.2 0.1 0.2 0.2 0.4 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.1 0.0 0.0 0.0 0.2 0.1 0.2 0.2 0.4 0.5 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.2 0.0 0.0 0.4 0.5 0.6 0.5 0.5 0.3 0.3 0.2 1.0 0.4 0.5 0.6 0.5 0.3 0.3 0.2 1.0 0.4 0.5 0.6 0.5 0.3 0.3 0.2 1.0 0.4 0.5 0.6		-1.1	-1.0	-0.9		Sinces.	10000			1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1			9 2000			8234	S. 20		
Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 -0.4 0.2 -0.1 -0.1 -0.1 -0.1 -0.1 -0.2 -0.4 Soil Type E (>3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 -0.3 0.1 -0.1 -0.2 -0.4 Minimum Score, Sumw 1.1 -0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.2 0.2 0.3 0.4 -0.6 -0.4 -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.6 -0.2 NA Minimum Score, Sumw 1.1 -0.9 0.7 0.5 0.5 0.6 0.5 0.3 0.3 0.3 0.3 0.3 0.2 0.0 -0.6 -0.2 NA FINAL LEVEL 1 SCORE, SL12 S MIN: Interior: Mone Visible Aerail Are There Hazards That Trigger A Detailed Structural Evaluation Required? Pauladian Structural Structural Structural Structural Structural St		and the second second	CHARLE -	1000		1846	1.1	1.9	NA	1.9	2.1		2.0	2.4	2.1	2.1	NA		
Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 NA -0.6 -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, Sumv 1.1 -0.9 0.7 0.5 0.5 0.6 0.5 0.5 0.3 0.3 0.2 0.2 0.3 0.2 0.2 0.3 0.2 1.0 FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: OTHER HAZARDS Are There HAZARDS Aret						200	5.02	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.000	10000	1200	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	6330	State of	0.5	0.5	0.3	0.3	
Minimum Score, Sunv 1.1 0.9 0.7 0.5 0.6 0.5 0.3 0.3 0.2 0.3 0.2 1.0 FINAL LEVEL 1 SCORE, SL1 > SMIN: CONTRECTION OF REVIEW EXTENT OF REVIEW OTHER HAZARDS ACTION REQUIRED Drawings Reviewed: Person: Visible Contact Person: Contact Pe		120038	2.2.2.2	100000	1000	22.000	1.000	10.00	A States							2011	1000		
FINAL LEVEL 1 SCORE, SL1 ≥ SMN: Image: Construct of the structural base of the structural b			-												-				
Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless St2> cut-off, if known) Yes, score less than cut-off Geologic Hazards Source: Falling hazards from taller adjacent building No Contact Person: Charker Sack Geologic hazards or Soil Type F Significant damage/deterioration to the structural system Geologic hazards exist that may require mitigation, but a detailed evaluation is not necessary Vest information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know	FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	(1.2)	20	3														
Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless SL2> cut-off, if known) Pounding potential (unless SL2> cut-off, if known) Geologic Hazards Source: Pounding potential (unless SL2> cut-off, if known) Pounding potential (unless SL2> cut-off, if known) LEVEL 2 SCREENING PERFORMED? Geologic hazards or Soil Type F Significant damage/deterioration to the structural system Ves, Final Level 2 Score, SL2 Mo No Nonstructural hazards? Yes No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know	and the second se				and a closer					ACT	ION R	EQUIF	RED					C	
Drawings Reviewed: Yes Yes No Soil Type Source:									A	Detail	ed Struc	tural Ev	aluation	Require	d?				
Soil Type Source:	Drawings Reviewed: Ves	wings Reviewed: Ves Via									es, unkn	own FEM	A buildir	ng type o	other b	uilding			
Geologic Hazards Source:		Type Source:																	
Contact Person: Chad GackSon building LEVEL 2 SCREENING PERFORMED? Beologic hazards or Soil Type F Beologic hazards or Soil Type F Yes, Final Level 2 Score, SL2 Value Value Nonstructural hazards? Yes No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR		ologic Hazards Source: Falling haz										nazalus	pieseill						
LEVEL 2 SCREENING PERFORMED? Geologic hazards of Soli Type P Yes, Final Level 2 Score, S _{L2} Significant damage/deterioration to the structural system Yes, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Nonstructural hazards? Yes No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know	Contact Person: Chad Sac	KS7	n		build	ling				_		tructura	Evalua	tion Rec	ommen	ded? (ch	eck one)		
□ Yes, Final Level 2 Score, SL2 □ No We structural system □ No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Nonstructural hazards? □ Yes □ No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know	LEVEL 2 SCREENING PERFO	ORME	D?								es, nonsi	tructural I	nazards	identified	that sho	uld be ev	valuated		
Nonstructural hazards? Yes No No No, no nonstructural hazards identified Mo Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know			and the second	0							o, nonstr	uctural h	azards e	exist that	may requ	uire mitig	ation, but	а	
Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know	the second s														ed r	DNK			
	Where information	cannot k	be verifie	d, scr	eener sha	ll note th	ne follov	ving: E	ST = Esti	100	1. C.				7				
BR = Braced frame SW = Shear wall TU = Tilt up LM = Light metal RD = Rigid diaphragm	And the second se	isting fram	ne	RC = R	einforced co				= Unreinfo			MH	= Manufa	actured Ho			le diaphra	gm	





Structure 43 is a One Hallway Addition to Structure 42 Concrete Column Exposed

Rapid Visual Screening of Buildings for Potential Seismic Hazards

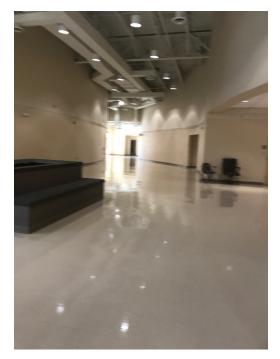
FEMA P-154 Data Collection Form

the second se						-		10	0	-		1.	_		han some server and	Version of the	-
						Add	ress:	13			nton	HW					
						1	-	17	yer.	TN	1	2	z	ip: 30	8330	5	
						Oth	er Ident	ifiers:	44								
							ding Na	me:			1						
						Use		Hig		scho							
						1.000000	tude:		241	01		ongitu	de:	.881	966	882	
PH	OTOGRAF	н				Ss:		271				S1: _(2,44				
						Scr	eener(s)	: <u>C</u>	M			D	ate/Time	e: <u>71</u>	240	9:45	Ah
						No.	Stories	: Abov	e Grade	:	Below	w Grade	: 0	Yea	r Built:	1 0005	EST
a first seattle seattle						Tota	al Floor	Area (se	q. ft.):	28	300	>		Code	Year:		
						Add	litions:		lone D		Year(s) B		1971	9.70	396		
						Occ	upancy	: Ass	embly	Comm	ercial	Emer. S	ervices	H	istoric	Shelt	er
									ustrial	Office		School		G	overnmer	nt	
						-		Utili	ty	Wareh	ouse	Residen	itial, #Un	nits:			
						Soil	Type:	A	□В	X	IC []E [-	NK		
LIGe I								Hard Rock	Avg Rock	Der					DNK, ass	ume Type	D.
[1996]			-			-	logia II			Concernance of the second	Service and State	States of the		Soil			
		-			-						s/No/DNF						
Origin	Val		-				acency:			ounding						t Building	
						Irre	gularitie	IS:	X V	ertical (t	ype/sever	ity) >p	lit le	vel/n	hod		1
195	19									an (type			1trong				
	11		1				erior Fal	lling			Chimney	s				leavy Ver	neer
				THUS	Ex.	Haz	ards:			arapets			App	pendages	5		
				1100	101W	0	MMENT	· .				-	-		-		_
		-		DOtte	S.	100	A D	5.	-		6-	and	1100	1			
	100	C		LUIR	TON	1,	US		Sar	ne	as	Our	710	11			
Free O	000	2 Parts											-				
L	009		and														
	T			_													
		1.0				-											
		, 19'	79			-											
				1		-											
	SHETCH			1			Addition	al skotch	00 01 001	nmonte	on separa	to none					
		ASIC	sco	RE, MO	DIFIER									-			-
FEMA BUILDING TYPE Do N	_	W1A	W2		S2	S3	S4	S5	C1	-	-		DOD				
Kn				(MRF)	(BR)	(LM)	(RC	(URM	(MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF)	1.5	2.0	(1.2)	1.6	1.4	1.7	1.7	10	4.5
Severe Vertical Irregularity, VL1	-1.2	-1.2	-1.2	1000000	-1.0	-1.1	-1.0	-0.8	-0.9	-1.0	-0.7	-1.0	-0.9	-0.9	-0.9	1.0 -0.7	1.5 NA
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark Soil Type A or B	1.6	1.9	2.2		1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.1	0.3	0.5	-0.2	0.6 -0.4	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.4	0.2 NA	-0.1	-0.4	0.0	0.0	-0.2	-0.3 NA	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	-0.6 0.3	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{R1}$	MIN:	03	1>0	0,3								012	0.2	0.0	0.0	0.2	1.0
		di	5-1	-			-	-	-	-	-	-	-				-
EXTENT OF REVIEW		-		OTHER					ACT	ION R	EQUIF	RED					
	All Sides			Are There				A	Detail	ed Stru	tural Eva	aluation	Require	d?			
	Visible	A Ent	ered	Detailed						es, unkn	own FEM	A buildir	ng type or	r other bi	uildina		
Soil Type Source:									Y DA	es, score	e less than	n cut-off					
Geologic Hazards Source:				□ Fallin	ff, if know g hazard	n) s from t	aller adia	cent			hazards	present					
Contact Person: Chad Jo	UKS ON			buildi	ng					-	structural	Evalue	tion De-	ommer	dada (-	and and	
LEVEL 2 SCREENING DEC	Geologic										tructural h						
	TORME			Signi Signi	ficant dan tructural s	nage/de	terioratio	on to		o, nonst	ructural h	azards e	xist that	may requ	uia de el	ation but	a
Yes, Final Level 2 Score, SL2		N		ule S	ucturals	ystem			de	tailed e	aluation i	is not ne	cessary	ind requ	and mug	auon, Dul	a
Nonstructural hazards? Yes										o, no no	nstructura	I hazard	ls identifie		DNK		
Where informati	on cannot i	be verifie	ed, scr	eener shal	I note the	e follow	ing: E	ST = Esti	imated o	r unreli	able data	OR	DNK = D	o Not Kr	now		Contraction of the local division of the loc
Legend: MRF = Momen	t-resisting fran	ne	RC = R	einforced cor		1	JRM INF	= Unreinfo	orced maso		MH	= Manufa	ctured Hou	using Fl	D = Flexib	le diaphra	gm
BR = Braced fr	ame		5W = S	hear wall			rU = Tilt u	p			LM =	= Light me	etal		D = Rigid	diaphragm	ĩ

Structure 44, Building 30 Photographs



Joint Between Structure 42 (White Façade into Page) and Structure 44 (Stairs Out of Page)



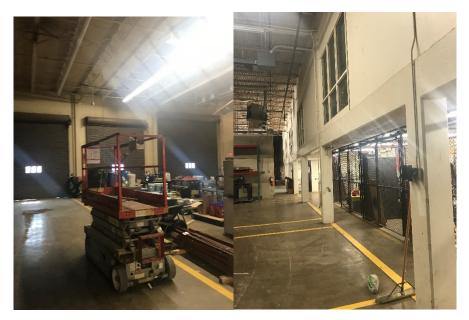
Interior, Split Level

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Address: 150 110 120 38330 PHOTOGRAPH Diversion of the second seco	1			-			-			-	-	-				_		-	
Bailding Name: Bailding Name: High School Latitude: School Latitude: School Latitude: School Steament(s: Latitude: Steament(s: CAS Steament(s: Date: Latitude: School Date: Drow Grade: Addition: Those Grade: Addition: Those Grade: Decorpancy: Asamity: Company: Asamity: Company: Asamity: Opticity: Part (Na) Decorpany:							Add	Iress: 1	50 -	Tre	non	HW	Y						
Building Name: Building Name: High School Latitude: Sci D12311 Latitude: Sci D12311 Scienter(science) Data/Time: Visc. Data/Direction: High School Data/Time: Visc. Data/Direction: High Science None Science Occupancy: Analysis Juit Jone: None Science Juit Jone None Science	and the second states							-	Dye	TT	7			Z	ip: <u>3</u>	8331	0		
PHOTOGRAPH Use: LV-S C/MON Complicate: St. Topologic St. Topo							Oth	er Identi	fiers:	45	Ser el a					-		_	
Hotoograph Latitude: 35 (7) 23 3 4 List on the formation region in the second of t							1000			CI					-	1.		_	
PHOTOGRAPH Sr. L_1_6 Sr. DutTime: T/2 / 1/								tudo: 2	High	1 20	1000			da. 7	00 00	111	ILII		
Screening: M Date: The: Date: The: The: <thdate: th="" the:<=""> <thdate: th="" the:<=""> <thd< td=""><td>BHOT</td><td></td><td></td><td></td><td></td><td></td><td></td><td>tude.</td><td>776</td><td>065</td><td>219</td><td></td><td></td><td>ae:</td><td>1</td><td>160</td><td>111</td><td></td></thd<></thdate:></thdate:>	BHOT							tude.	776	065	219			ae:	1	160	111		
No. Stories: Abore Balt Stories: Abore Balt Stories: Abore Balt Stories: Abore Balt Stories: Code Year: Code Year:	PHOTO	JGRAP	п					-	0		-	`				400	945	AM	
Total Floor Area (cr., h): Style Code Year Occupancy: Asserb Conversion Letters Development											. 7.	Below		-				and all a	
Additions: None BV eric Years (part) 1011: 1012: 100: Occupancy: Association Commonit Commonit Commonit Commonit Utility: Image: State in the s													v Glaue	. 0			1771	LESI	
Industrie Office Convertions Soil Type:													uilt: 1	970			1009		
Utility Wardbook Residence Utility Wardbook Residence Soil Type:							Occ	upancy	: Ass	embly	Comme	rcial	Emer. S	ervices	Hi	storic	Shelt	er	
Soil Type: Image: Image: <td></td> <td>~</td> <td></td> <td></td> <td>overnmer</td> <td>nt</td> <td></td>													~			overnmer	nt		
Hard way Dense Sell Soll Soll Soll Soll Soll Hard way Dense Sell Soll Soll Soll Soll Soll Geologic Hazards: Liquetecton: YesNODNK Landside: YesN										·									
Roke Roke Sel Sel Sol Sol Roke Roke Sel Sel Sol Sol Condectors Sel Sol Sol Sol Condectors Sel Sol Sol Sol Sol Sol Sol Sol Sol Sol So		_					Soil	Type:									umo Tuno	D	
Geologic Hazards: Lydeuctorin: YeshkoDKK and Kark Rupt. YeshkoDKK Geologic Hazards: Lydeuctorin: YeshkoDKK and Kark Rupt. YeshkoDKK Geologic Hazards: Lydeuctorin: YeshkoDKK and Kark Rupt. YeshkoDKK Geologic Hazards: Lydeuctorin: YeshkoDKK and Chrimeys Geologic Hazards: Lydeuctorin: YeshkoDKK and Yeshko An	[1996]															0111, 033	unio iypo	υ.	
Image: second							Geo	logic Ha	azards:	Liquefac	tion: Yes	s/No/DNK	(Lands	lide: Yes	No/DNK	Surf. Ru	upt.: Yes/I	No/DNK	
Bin (type) CC_CATE WAT CPINE(X) Exterior Falling Distraced Chimeys Heavy Cladding or Heavy Veneer Distraced Chimeys Distraced Chimeys Heavy Cladding or Heavy Veneer Distraced Chimeys Distraced Chimeys Heavy Cladding or Heavy Veneer Distraced Chimeys Distraced Chimeys Heavy Cladding or Heavy Veneer Distraced Chimeys Distraced Chimeys Heavy Cladding or Heavy Veneer Other Other Other Other Comments Other Other Other Other Stational Sketches or comments on separate page Other Other Other Other Basic Score Sone Ventral Informative, Vi 12 12 12 14 14 16 15 Moderale Ventral Informative, Vi 12 12 10 10 16 15 16 10 15							Adj	acency:											
Exterior Failing Unbraced Chimeys Heavy Cladding or Heavy Veneer Basic Score Basic Score COMMENTS: MGSDONY, CONC, Calls Hurd Ugent EXterior Failing Unbraced Chimeys Heavy Cladding or Heavy Veneer Basic Score Skietcel Comments on separate page Exterior Failing Unbraced Chimeys Heavy Cladding or Heavy Veneer Basic Score Basic Score Skietcel Comments on separate page Exterior Failing Unbraced Chimeys Heavy Cladding or Heavy Veneer PEM BUILDING TYPE Doket With WA V2 Skiet Score Sovee Veneal Insglathy, V1 12 12 20 24 20 15 14 11 10 13 30 90 10 13 10 13 30 90 10 11 10 14 14 17 17 10 15 Sovee Veneal Insglathy, V1 12 12 12 20 24 17 15 20 16 14 17 17 10 10 10 10 10 10 10 10 10 <	1979			-			Irre	gularitie	s:	Ve Ve	ertical (ty an (type)						1	_	
Hazards: Paragets Appendages Other: Other: Other: Other: Other: Other: Other: Other: Other: Other: Other: Other: Sketch Appendages Additional sketches or comments on separate page Bait Score Sketch Sketch NM Moderational sketches or comments on separate page Bait Score Status Bait Score Status Other 10 Imin Imputative, Vic. 38 11 10 10 11 10 11	Drinna	1-		-	mb.	0	Exte	erior Fal	ling							an and the second second	eavy Ven	leer	
COMMENTS: COMMENTS: MGSONYY, Conc., CMs fbro yghot MGSONY, Conc., CMs fbro yghot Comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.t FEM BUILDING TYPE Data BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.t Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.t Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.t Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.t Basic Score, MODIFIERS, AND FINAL LEVEL 1 SCORE, St.t Pascore Variatinguianty, Viz, 12, 12, 12, 12, 12, 10, 10, 10, 11, 11, 10, 40, 80, 07, 08, 05, 05, 05, 06, 06, 08, 02, 06, 06, 02, 06, 05, 05, 05, 00, 01, 10, 10, 01, 01, 01, 01, 01, 01	Un frim	1		-	1this	horm				D Pa	arapets	,					oury ron		
	1				TAU	F	-			0 0	ther:	_	_	_	_			-	
Additional sketches or comments on separate page EASIC SCORE, MODIFIERS, AND FINAL LEVEL SCORE, S.r. Fema Building TYPE Nonew With With With With Version 12 Pana Building TYPE Nonew With With With With Version 12 Pana Building TYPE Nonew Main Insplant 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 13 10 10 14 10 10 10 14 10					DO4M	er pan	CO	MMENT	S:			1	1	11		1	1		
Additional sketches or comments on separate page EASIC SCORE, MODIFIERS, AND FINAL LEVEL SCORE, S.r. Fema Building TYPE Nonew With With With With Version 12 Pana Building TYPE Nonew With With With With Version 12 Pana Building TYPE Nonew Main Insplant 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 13 10 10 14 10 10 10 14 10		1	TU		-		-	· W0	ison	NY1	Con	6,0	015	thr	000	hou	H		
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL FEMA BUILDING TYPE Do Not W1 W1 W2 St St St St St St C2 G2 N1 FOD FOD <td< td=""><td>2,009</td><td></td><td></td><td></td><td>1</td><td></td><td>-</td><td></td><td></td><td>• •</td><td></td><td></td><td></td><td></td><td>1</td><td>)</td><td></td><td></td></td<>	2,009				1		-			• •					1)			
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not VIII WIA WI MI WIA WIA <th co<="" td=""><td></td><td>-</td><td></td><td></td><td>1</td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th>	<td></td> <td>-</td> <td></td> <td></td> <td>1</td> <td></td> <td>_</td> <td></td>		-			1		_											
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SLr FEMA BUILDING TYPE Do Not VIII WIA W2 Afficience Secore Score			11	coulicipo															
Additional sketches or comments on separate page BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SLr FEMA BUILDING TYPE Do Not VIII WIA W2 Afficience Secore Score		-	1		100														
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not Know W1 W2 S1 S2 S3 S4 US C1 C2 C1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 0.5 0.5 0.6 0.5 0.5 0.6 0.5 0.5 0.6 0.7 0.6 0.6 0.6 0.5 0.5 0.6 0.7 0.6 0.6 0.6 0.6 0.5 0.5 0.6 0.6 0.7 0.6		120	19	79															
BASIC SCORE, MODIFIERS, AND FINAL LEVEL 1 SCORE, SL1 FEMA BUILDING TYPE Do Not Know W1 W2 S1 S2 S3 S4 US C1 C2 C1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.0 0.5 0.5 0.6 0.5 0.5 0.6 0.5 0.5 0.6 0.7 0.6 0.6 0.6 0.5 0.5 0.6 0.7 0.6 0.6 0.6 0.6 0.5 0.5 0.6 0.6 0.7 0.6	SKA	TCH			1.00			A .1.170											
FEMA BUILDING TYPE Do Not Know W1 W1 W1 W2 S1 S2 S3 S4 S5 C1 C2 C3 PC1 PC2 RM1 RM2 URM MH Basic Score 3.6 3.2 2.9 2.1 2.0 2.6 2.0 1.7 1.5 2.0 1.6 1.4 1.7 1.7 1.6 1.4 1.7 1.7 1.0 -0.7 -0.7 -0.7 -0.6 -0.6 -0.5 -0.5 -0.6 -0.5 -0.5 -0.6 -0.5 -0.5 -0.6 -0.5 -0.5 -0.6 -0.7 -0.7 -0.7 -0.7 -0.6 -0.6 -0.6 -0.6 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.3 -0.5 -0	014		ASIC	sco	RE MO	DIFIER										-	and the second		
Know (MRF) (BR) (MR) (BR) (MR) (BR) (MR) (BR) (MR) (BR) (MR) (MR) <t< th=""><th>FEMA BUILDING TYPE Do Not</th><th></th><th>-</th><th>-</th><th></th><th></th><th></th><th>-</th><th></th><th>-</th><th></th><th></th><th></th><th>PC2</th><th>DM1</th><th>DM2</th><th>UDM</th><th>MIL</th></t<>	FEMA BUILDING TYPE Do Not		-	-				-		-				PC2	DM1	DM2	UDM	MIL	
Severe Vertical Irregularity, V ₁₇ 1.2 1.2 1.2 1.0 1.0 1.0 1.0 1.4 1.7 1.0 0.0 Moderate Vertical Irregularity, V ₁₇ 0.7 0.7 0.6 0.6 0.7 0.6 0.0 0.0 0.7 1.0 0.7 0.5 0.5 0.6 0.05 0.5	and the second				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)		FUZ			URM	MH	
Moderate Vertical Irregularity, V ₁₇ -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.6 -0.7 -0.6 -0.5 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0.7 -0				200 100		27.5			10100000							0.000	2.20		
Plan inregularity, P ₁₁ -1.1 -1.0 -1.0 -0.8 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7 -0.7 -0.6 -0.7	Moderate Vertical Irregularity, VL1	0.02	1.01.52	200.000	1	100000		Contraction of the	100000	647273	1.000			226			1000		
Post-Benchmark 1.6 1.9 2.2 1.4 1.1 1.9 NA 2.0 2.4 2.1 2.1 NA 1.2 Soll Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.3 0.5 0.3 0.3 0.3 0.5 0.4 0.5 0.3 0.3 0.6 0.4 0.5 0.3 0.3 0.6 0.4 0.5 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.3 0.3 0.3 0.4 0.5 0.4 0.5 0.5 0.3 <		0.365		1.6.5%		10000		NG3325	10.000	1.	100	25	-0.7	-0.6	-0.7	10202	1.200		
Soil Type A or B 0.1 0.3 0.5 0.4 0.6 0.1 0.6 0.5 0.4 0.5 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.6 0.4 0.5 0.3 0.1 0.1 0.1 0.2 0.4 0.5 0.3 0.3 0.2 0.4 0.5 0.3 0.3 0.2 0.4 0.5 0.3 0.3 0.2 0.4 0.5 0.3 0.3 0.2 0.3 0.2 1.0 INAL LEVEL 1 SCORE, SL1 > SL1 SL1 <td></td> <td>1 2.1.52</td> <td>C. Lances</td> <td>1.</td> <td></td> <td></td> <td></td> <td>120102</td> <td>1000145</td> <td>1000</td> <td>2895</td> <td></td> <td></td> <td>1 - CONS</td> <td>100000</td> <td>1.000</td> <td>10,200</td> <td></td>		1 2.1.52	C. Lances	1.				120102	1000145	1000	2895			1 - CONS	100000	1.000	10,200		
Soil Type E (1-3 stories) 0.2 0.2 0.1 -0.2 0.4 0.2 0.1 -0.4 0.0 0.0 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.3 -0.1 -0.1 -0.1 -0.2 -0.3 NA -0.4 -0.5 -0.7 -0.3 NA -0.4 -0.5 -0.5 -0.5 -0.5 0	Soil Type A or B		15357	1.110.00	2505	and the second			1000					1 23523					
Soil Type E (> 3 stories) -0.3 -0.6 -0.9 -0.6 -0.6 NA -0.6 -0.7 -0.3 NA -0.4 -0.5 -0.6 -0.2 NA Minimum Score, Sum 1.1 0.9 0.7 0.5 0.5 0.5 0.3 0.3 0.3 0.2 0.2 0.3 0.2 0.4 -0.6 -0.6 -0.2 NA FINAL LEVEL 1 SCORE, SL1 > Smin: OT C 2.0 0.3 0.3 0.3 0.3 0.2 0.2 0.3 0.3 0.2 0.2 0.3 0.3 0.2 0.2 0.3 0.2 1.0 FINAL LEVEL 1 SCORE, SL1 > Smin: OTHER HAZARDS Aerial Are There Hazards That Trigger A Detailed Structural Evaluation Required? Detailed Structural Evaluation Required? Drawings Reviewed: Yes No Pounding potential (unless SL2 > cut-off, if known) Paling hazards from taller adjacent building Pes, sore less than cut-off Yes, other hazards present No Detailed Nonstructural Evaluation Required? Check one) Periadicate damage/deterioration to the structural system No Detailed Nonstructural hazards identified that should	Soil Type E (1-3 stories)	0.2	0.2	1000					10.23	1000	1000	0.000		A State of the second		103303	100000		
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: O O 0.0			100 M 100 M			-	-			-	1000			202022					
EXTENT OF REVIEW OTHER HAZARDS ACTION REQUIRED Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless St2> cut-off, if known) Pounding potential (unless St2> cut-off, if known) Yes, score less than cut-off Geologic Hazards Source: Pounding potential (unless St2> cut-off, if known) No Detailed Nonstructural Evaluation Recommended? (check one) LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to the structural system No Detailed valuation is not necessary Monstructural hazards? Yes No No Detailed valuation is not necessary Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm		-	0.9	0.7	The second se	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0	
Exterior: Partial All Sides Aerial Interior: None Visible Entered Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless SL2> Geologic Hazards Source: Pounding potential (unless SL2> Contact Person: Charled SourceSon EEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to Yes, Final Level 2 Score, SL2 No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know		(763	2Q			_		_	_									
Interior: None Visible Entered Detailed Structural Evaluation? Drawings Reviewed: Yes No Pounding potential (unless St2> Soil Type Source: Pounding potential (unless St2> Yes, score less than cut-off Geologic Hazards Source: Pounding potential (unless St2> Yes, other hazards present Contact Person: Charles Jack Sont Falling hazards from taller adjacent building No LEVEL 2 SCREENING PERFORMED? Geologic hazards or Soil Type F Significant damage/deterioration to the structural system Yes, nonstructural hazards identified that should be evaluated Yes, Final Level 2 Score, St2 No No No Detailed valuation is not necessary Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRR = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm			_																
Drawings Reviewed: Yes No Soil Type Source: Pounding potential (unless St2> cut-off, if known) Yes, score less than cut-off Geologic Hazards Source: Falling hazards from taller adjacent building Yes, other hazards present Contact Person: Check Son Falling hazards or Soil Type F LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to the structural system Ves, nonstructural hazards identified that should be evaluated to the structural system No No Detailed evaluation is not necessary Nonstructural hazards? Yes No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm					Are Then	e Hazard	S That	Trigger A	4										
Soil Type Source:	Drawings Reviewed: 🗌 Yes 🔥 I		YEA CITE	51CU						Ye	es, unkno	own FEM	A buildir	ng type or	other bu	uilding			
Geologic Hazards Source:	Soil Type Source:	-						11055 SL2	-										
LEVEL 2 SCREENING PERFORMED? Geologic hazards or Soil Type F Detailed Nonstructural Evaluation Recommended? (check one) Yes, Final Level 2 Score, St2 No Significant damage/deterioration to the structural system Person Structural hazards identified that should be evaluated Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm	-	ack /	~~~	-	Fallin	g hazards		aller adja	cent				- Soont						
LEVEL 2 SCREENING PERFORMED? Significant damage/deterioration to the structural system Yes, nonstructural hazards identified that should be evaluated Yes, Final Level 2 Score, SL2 No No Nonstructural system No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Nonstructural hazards? Yes No No No, no nonstructural hazards identified No Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm				-			rds or S	Soil Type	F										
□ Yes, Final Level 2 Score, SL2 Mo the structural system □ No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Nonstructural hazards? □ Yes □ No No No, no nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data <u>OR</u> DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm		ORME	D?		Signi	ficant dan	nage/de	eterioratio	n to	Ye	es, nonst	ructural h	nazards	identified	that sho	uld be ev	aluated		
Wonstructural hazards / Yes No No No No no nonstructural hazards identified Image: Constructural hazards identified Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm		-	N 🕅	0	the s	tructural s	ystem				o, nonstr	uctural ha	azards e	xist that I	may requ	lire mitig	ation, but	а	
Where information cannot be verified, screener shall note the following: EST = Estimated or unreliable data OR DNK = Do Not Know Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm											o, no nor	structura	l hazard	s identifie					
Legend: MRF = Moment-resisting frame RC = Reinforced concrete URM INF = Unreinforced masonry infill MH = Manufactured Housing FD = Flexible diaphragm		cannot b	e verifie	d, scr	eener shal	I note the	follow	ving: ES	ST = Esti	mated o	r unrelia	ble data	OR	DNK = D					
	Legend: MRF = Moment-res		ne l	RC = R	einforced co			URM INF :	= Unreinfo			MH	= Manufa	ctured Hor	using Fl	D = Flexib	le diaphrag	gm	

Structure 45, Building 30 Photographs



Interior, Split Level, Concrete Columns Exposed

РНОТ	Othe Buil Use Latii Ss: Scre No. Tota Add Occ	ding Na tude:	ifiers: L me: E C 36, 1 175 : : Abov Area (sc N : N : Indu Utilit	MeM 16 MeM 1897 Me Grade A. ft.): one Fembly istrial by B	LFavr 252 Yes, Y Comme Office Wareho	Belov Frear(s) B rcial use	os ongitu Sr: Di v Grade O Uuilt: Emer. S School Residen	de:	ip: <u>}</u> 89. • • • • • • • • • • • • • • • • • • •	DO 87 24 0 Year: storic overnmen	0 97 0 11 A 2002 c	I EST					
								Hard Rock	Avg Rock	Den So	il Se	oil S	ioil S	Soil		ume Type	
	_	TITA	the	S Port	~									/No/DNK		AN ANY WAY	
100			110	s form er for		-	acency: gularitie			ounding			azards fr	om Taller	Adjacent	t Building	
5105		0	074	er for	m	- Integ	Julanue	5.			pe/sever		ntra	nt ce	rner	,	-
						100000000000000000000000000000000000000	erior Fal ards:	lling		arapets	Chimney	S		avy Clado bendages		eavy Ven	ieer
SK	ETCH	ASIC	Zo	RE, MO	DIFIEF			al sketch									
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	SW) 2.0	INF) 1.7	1.5	2.0	INF) 1.2	1.6	1.4	(1.7)	1.7	1.0	1.5
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.2	-1.2 -0.7	-1.2	-1.0	-1.0 -0.6	-1.1 -0.7	-1.0 -0.6	-0.8 -0.5	-0.9 -0.5	-1.0 -0.6	-0.7 -0.4	-1.0 -0.6	-0.9 -0.5	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0		-0.7	-0.9	-0.0	-0.6	-0.5	-0.8	-0.4	-0.6	-0.5	-0.5	-0.5 -0.7	-0.4 -0.4	NA NA
Pre-Code Post Penchmark	-1.1	-1.0	-0.9		-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Post-Benchmark Soil Type A or B	1.6	1.9 0.3	2.2	1.4	1.4 0.6	1.1 0.1	1.9	NA 0.5	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.1	0.0	0.0	-0.2	-0.4	0.1	-0.1	-0.4	0.4	0.5	0.3	0.6	0.4	0.5	0.5 -0.1	0.3	0.3 -0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	(3,1	EO	.3													-
EXTENT OF REVIEW Exterior: Interior: Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Ves, Final Level 2 Score, SL2 Nonstructural hazards? Yes	R HAZ e Hazard Structura ding pote ff, if know ing hazard ing ogic haza ficant dar tructural s	s That T al Evalu ential (ur m) s from ta rds or S nage/de	Trigger / ation? Aless SL2 aller adja oil Type	> icent F	Detaile Ye Ye Detaile Detaile Ne de	ed Struc es, unkno es, score es, other o ed Nons es, nonst o, nonstr etailed ev	tructural h uctural h ructural h uctural h	aluation A buildir n cut-off present I Evalua nazards i azards e is not ne	tion Rec identified exist that	commend that sho may requ	led? (ch uld be ev ire mitiga	aluated					
Where information Legend: MRF = Moment-res BR = Braced frame	Il note the	1		= Unreinfo	mated o	r unrelia	MH	<u>OR</u>	DNK = D ctured Ho	o Not Kr) = Flexib	le diaphrag diaphragm	gm				

Structure 46, Building 31 Photographs



Structure 46 Lower Roof, Structure 47 Higher Roof

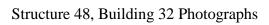
РНОТС	Oth Buil Use Lati Ss: Scru No. Tota Addo	er Identi Iding Na e: itude: <u>3</u>	fiers: me: E_\ew G Abov Area (so Indu Utiliti	A Grade A ft.): one e Grade a, ft.): one pembly ustrial by B	Yes, Y Commer Office Warehou	Below Below Crafs Ear(s) Bill Crail Use	ongitu ongitu Sı: O Grade uilt: _ Emer. S School Residen	b) (14) de:	ip: 3 89 Yea Code H G its:]F D	Built:	1774 2012 c K Shelt] EST					
								Hard Rock	Avg Rock	Dens Soi	So	oil S	oil S	oil		ume Type	
							ologic Ha										Contraction of the second
2017	37		-			_	acency: gularitie			ounding ertical (type)			azards fro	om Taller	Adjacen	t Building	
COIC	11						guiunite			an (type)						-	
							erior Fal ards:	ling		nbraced arapets ther:	Chimney	S	Hea			eavy Ven	eer
							MMENT				0						
Ori ginal 2002	-		Cy 20				·Ma	SON	x 2,	reiv	Hor	ced					
SKI	TCH						Addition	al sketch	es or con	nments o	n separa	ite page					
				RE, MO		RS, A	ND FIN	AL LE	EVEL	1 SCO	RE, S	.1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VLr	3.6 -1.2	3.2 -1.2	2.9	2.1 -1.0	2.0 -1.0	2.6 -1.1	2.0 -1.0	1.7 -0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	1.7 -0.9	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	-0.5	-0.9	-0.7 -0.4	NA NA
Plan Irregularity, PL1 Pre-Code	-1.1 -1.1	-1.0	-1.0	-0.8	-0.7	-0.9 -0.8	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark	1.6	1.9	2.2	-0.0	-0.0	-0.8	-0.6	-0.2 NA	-0.4	-0.7	-0.1 NA	-0.5 2.0	-0.3 2.4	-0.5	-0.5	0.0 NA	-0.1 1.2
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories) Minimum Score, Smin	-0.3	-0.6	-0.9	-0.6	-0.6 0.5	NA 0.6	-0.6	-0.4 0.5	-0.5 0.3	-0.7	-0.3 0.3	NA 0.2	-0.4	-0.5	-0.6 0.3	-0.2	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	(3,8			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.3	0.2	1.0
EXTENT OF REVIEW	,	9		OTHER	RHAZ	ARDS	3		ACT	ION R	EQUIF	RED	-				
Interior: None		Aeri			Structura ding pote ff, if know	al Evalu ntial (un n)	nless SL2	>		ed Structes, unknotes, score s, scores, other	tural Eva wn FEM less thar	Aluation A buildir n cut-off	ng type or		uilding		
Contact Person: Chad	Jack	Son		build					Dotail		ructure l	Evel	tion D				
LEVEL 2 SCREENING PERFORM Yes, Final Level 2 Score, SL2 Nonstructural hazards?	DRME	D? Ø N	0	Geole Signi the s	ogic haza ficant dar tructural s	nage/de system	eterioratio	on to		es, nonstr o, nonstru etailed eva o, no non	ructural h uctural ha aluation i structura	nazards i azards e is not ne il hazard	identified xist that r cessary s identifie	that sho may requ ed	uld be ev uire mitiga Z DNK	eck one) valuated ation, but	
Where information of	annot b	e verifie	d, scr	ener sha	I note the	e follow	ving: ES	ST = Esti	mated o	r unrelia	ble data	OR	DNK = D	o Not K	now		
Legend: MRF = Moment-res BR = Braced frame	sting fram			ainforced co near wall	ncrete		URM INF : TU = Tilt u		rced maso	onry infili		= Manufa = Light me	ctured Hoi etal	using F	D = Flexib D = Rigid	le diaphrag diaphragm	gm

Structure 47, Building 31 Photographs



Structure 46 Lower Roof, Structure 47 Higher Roof

	Othe Build Use: Latif Ss: Scre No. Tota Add Occ	er Identi ding Na sude: eener(s) Stories:	ifiers: ime: 36.1 36.1 175 : Area (so Area (so N : Ass	embly Istrial	ary 198	Belov Belov Crear(s) B rcial use	ongitu Sr:D w Grade S echool Residen JDS	de:	89.0 Yean Code Hi G its:	3823 24 00 75 24 00 75 20 75 75 20 75 75 75 75 75 75 75 75 75 75 75 75 75	2012 □ Shelt] EST er						
	201	2					Adja	cency:	azards:	Liquefac	tion: Yes		< Lands Falling H	lide: Yes	No/DNK	Surf. Ru Adjacent		
				141	isfor	m	Irreg	gularitie	S:		ertical (ty an (type)		ity) _	_				-
	200)?	E		1	brw		erior Fal ards:	lling	D P	nbraced arapets ther:	Chimney	/S	Hea		ding or He s	eavy Ven	eer
							co	MMENT	'S:									
	ekt	TCH			Cym		-		5					ding	5			
*	Ont		ASIC	sco	RE, MO	DIFIE				es or cor	_	the second s				-		
FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1		3.6 -1.2 -0.7	3.2 -1.2 -0.7	2.9 -1.2 -0.7	2.1 -1.0 -0.6	2.0 -1.0 -0.6	2.6 -1.1 -0.7	2.0 -1.0 -0.6	1.7 -0.8 -0.5	1.5 -0.9 -0.5	2.0 -1.0 -0.6	INF) 1.2 -0.7 -0.4	1.6 -1.0 -0.6	1.4 -0.9 -0.5	1.7 -0.9 -0.5	-0.9	1.0 -0.7 -0.4	1.5 NA NA
Plan Irregularity, PL1 Pre-Code		-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Post-Benchmark		-1.1 1.6	-1.0 1.9	-0.9	-0.6	-0.6 1.4	-0.8	-0.6	-0.2 NA	-0.4	-0.7	-0.1 NA	-0.5	-0.3	-0.5	-0.5	0.0 NA	-0.1 1.2
Soil Type A or B		0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories) Soil Type E (> 3 stories)		0.2	0.2	0.1	-0.2	-0.4	0.2 NA	-0.1	-0.4	0.0	0.0	-0.2 -0.3	-0.3 NA	-0.1 -0.4	-0.1 -0.5	-0.1	-0.2	-0.4
Minimum Score, SMIN		1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	-0.6	-0.2	NA 1.0
FINAL LEVEL 1 SCORE, SLI	≥ Smin:	C	De	000		3,	f≥6	0.6										
EXTENT OF REVIEW			-		OTHE	RHAZ	ARDS			ACT	ION R	EQUIF	RED					
Exterior: A Partia Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:		/isible	Aer		Are Ther Detailed Poun cut-o	Structu ding pot ff, if know	ral Evalu tential (un	ation? less SL2	>		es, unkno es, score es, other	wn FEM less tha	A buildir n cut-off			uilding		
Contact Person:	ing						tructura	I Evalua	tion Rec	ommen	ded? (ch	eck one)						
	Yes			lo	Signi Signi the s	ficant da tructural		terioratio	on to		es, nonst o, nonstri tailed ev o, no nor	ructural h uctural h aluation	hazards azards e is not ne al hazard	identified exist that i ecessary Is identifie	that sho may requ ed	uld be ev uire mitiga	aluated	
Where infor												ble data	OR	DNK = D	o Not Ki	now		
	oment-resi ced frame	sting fram			einforced co hear wall	ncrete	l	JRM INF [U = Tilt u	= Unreinfo	prced maso	onry infill	MH LM =	= Manufa = Light m	ctured Hore	using F	D = Flexib D = Rigid	le diaphrag diaphragm	gm

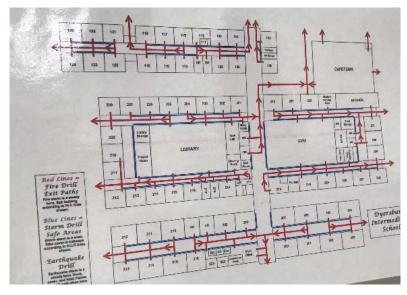




Exterior Views, Single Rectangular Manufactured Building

Level 1 VERY HIGH Seismicity

						Add	ress:	72	57	ibbs	St,			3	20-1		
						Oth	er Identi	fiere	Lia	Aure	JN,	1	Z	ip: <u>3</u>	2020	1	
							ding Na		19	0		1		1			
						Use	E	100	rent	arv	Soh	100		10.00	-		
						Lati	tude: 📑	3610	381	613		Longitu	de: 🛁	89.	376	964	
PHOTO	OGRAP	Ή				Ss:		275				S1: (0,83.	6			
							eener(s)			_	_	Da	ate/Time	: 61	D		
						Tota	Stories: al Floor litions:			21	705			Code	Year:	2005 1	EST
THUC N.							upancy		embly	Comme	Year(s) B	Emer. S	1964	191		Shelt	104
LITHIS TORM						000	upancy		ustrial	Office	illiai	School	el vices		vernmen		ter
I this form 01 Ler form								Utili	ity	Wareho	use	Residen	tial, #Un	its:			
					_	Soil	Type:	Hard Rock	Avg Rock	Den So	se St	tiff S	oft Po	JF DP por If L oil		ume Type	D.
1991	I					Geo	logic Ha	Conception of the local division of the loca	Liquefac						Surf. Ru	upt.: Yes/	No/DNK
199						***********	acency:		and a lot of the lot o	ounding				om Taller			
Lat.			T			Irre	gularitie	s:		ertical (ty an (type	pe/sever			evell			
7	-	-	1 -			Exte	erior Fal	ling			Chimney	S	Hea	vy Cladd	ina or H	eavv Ver	neer
			+			Haz	ards:			arapets				endages			
Library 196	4		G	ym		CO	MMENT	S:									
							Ma	san	vv.Y	ed-	Trav	~ m	nel	Mov	110	dial	Lv.)
							1	5011	ry,r	· ·			1 100	1100	bie	comp	ut agas)
	1					1	Sol	id (ion	cnet	e b	asen	heri	H			
E	1	1	Tues I			-											
Foyer	4		- Toronto														
	AT	a la free	17 A.	Series Person													
SK	тсн						Addition	al ekoteb	nes or cor	monto							
		ASIC	sco	RE, MO	DIFIE												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	sw)	INF)	1.0	1.2	INF) 0.9	1.1	1.0	50	1.1	0.9	1.1
Severe Vertical Irregularity, VL1	-0.9	-0.9	-0.9	-0.8	-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.6 -0.7	-0.5 -0.7	-0.5		-0.4 -0.5	-0.5 -0.6	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	0.4	-0.4	-0.3	NA
Pre-Code	-0.3	-0.3	-0.3		-0.5	-0.8	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5 -0.2	-0.4	-0.4	-0.4 -0.2	-0.3 0.0	NA 0.0
Post-Benchmark	1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0 -0.4	-0.2	-0.4		-0.2 -0.3	-0.2 NA	-0.2	-0.1	-0.1	-0.2	0.0	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, SMIN	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	-0.1	-0.2 0.3	-0.2	0.0	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	(2	1.3	≥0	3													
EXTENT OF REVIEW	-			OTHER	R HAZ	ARDS			ACT	ION R	EQUIF	RED					
		Aer		Are There				1	Detail	ed Struc	tural Eva	aluation	Require	d?			
Interior: Interi		Ent Ent	ered	Detailed						es, unkno	own FEM	A buildin	g type of	other bu	ilding		
Soil Type Source:		-		Poun cut-or	ding pote		less SL2	>			less than hazards						1
Geologic Hazards Source: Contact Person: Broad Broad	LAZ	-	_	🗌 Fallin	g hazard		aller adja	cent	NO NO)	11020103	present					
	NKEV			buildi		ards or S	oil Type	F						ommend			
LEVEL 2 SCREENING PERFO	ORME	D?		Signit	ficant dar	mage/de	terioratio	n to	Ye	es, nonst	ructural h	nazards i	dentified	that show	ld be ev	aluated	
Yes, Final Level 2 Score, SL2		N N			ructural				de	tailed ev	aluation i	is not ne	cessarv	may requ	re mitiga	ation, but	ta
Nonstructural hazards? Ves			1220							o, no nor	structura	I hazard	s identifie		J DNK		
Where information of Legend: MRF = Moment-res	annot b	e verifie	d, scr	eener shal	I note th	e follow	ing: ES	T = Esti	imated o	r unrelia	ble data	OR L	DNK = D	Not Kn	0₩		-
				einforced cor					orced maso				ctured Hor				



Structure 49, Building 33 Photographs

Plan View, Bottom Hallway is Structure 49



Exterior



Interior, Split Level

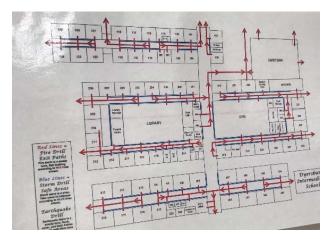


Connection from Structure 49 to 50

Level 1 VERY HIGH Seismicity

			1			Add	ress: _		ST								
						Oth	er Identi	Die	rsbui	Tep	IN		Z	Lip: 38	8024		
							ding Na	_	50								
						Use:	E	lew	ent	wv .	Scho	101	-				
							tude:	361	0381	77	L	ongitu		89,	377	060	
РНОТС	GRAP	H				Ss:	1.	Lt	5		5		1,831		10		
						-	ener(s)					_	ate/Time		10		
						10000000	Stories:		e Grade	17	Belov	v Grade	:0	-		19640	EST
							itions:			04	ear(s) B		009	199	Year:		
this form						Occ	upancy:	Asse	embly	Comme		Emer. S		Hi	storic	Shelt	er
									strial	Office		Schoot		7000	overnmen	ıt	
D other form						Soil	Tuno	Utilit	-	Warehou			tial, #Ur				
a		1	-			- 301	Type:	Hard	Avg	Dens	se St				NK DNK, assi	ume Type	D.
				1		Geo	logic Ha	Rock	Rock	Soi				Soil			
Add.							icency:	120105.		ounding		and the second diversion of the second se				ıpt.: Yes/I t Building	the second s
							gularitie	c.						iel / m		Building	
			1		Y	11109	Julainte	э.		an (type)	perseven		11100	ici j r	. 001.		
A PALITAR MARA		action			1		rior Fal	ling			Chimney	S	Hea	avy Clado	ding or H	eavy Ven	ieer
A		- Martin	No.	4	T	Haza	ards:		And a state of the	arapets her:			App	pendages	3		
[Library]			9	ymx	28	CO	MMENT	S:			-						
Land I	1.178	The has a			1	-	ASC	file	level	(m	ised	ceil	ina	1			
	行行的意	的制度	A MARINE	and the state	12		1		level nry	1100		with	h ?	,			
	1-	r L					s W	A 501	NYY	sre	7.Vt						
	-Oye																
	10																
SKI	TCH						Additiona	al sketch	es or con	nments o	n separa	ate page					
	В	ASIC	sco	RE, MO	DIFIEF												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	2.1	1.9 -0.9	1.8	1.5	1.4	1.6		I INFI									
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.0					1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
	-0.6		-0.9	10200	-0.7 -0.4	-0.8	1.4 -0.7	1.2 -0.7	-0.7	-0.8	0.9 -0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.6 -0.7	-0.5 -0.7	-0.5 -0.6	-0.4 -0.5	-0.7 -0.4 -0.5		1.4	1.2			0.9			-0.7 -0.4	1. 1. 1. 1. 1.	0.000	1000
Plan Irregularity, PL1 Pre-Code	-0.7 -0.3	-0.5 -0.7 -0.3	-0.5 -0.6 -0.3	-0.4 -0.5 -0.3	-0.4 -0.5 -0.2	-0.8 -0.5 -0.6 -0.3	1.4 -0.7 -0.4 -0.4 -0.2	1.2 -0.7 -0.3 -0.4 -0.1	-0.7 -0.4 -0.4 -0.1	-0.8 -0.4 -0.5 -0.2	0.9 -0.6 -0.3 -0.3 0.0	-0.7 -0.4 -0.5 -0.2	-0.7 -0.4 -0.4 -0.1	-0.7	-0.7 -0.4 -0.4 -0.2	-0.6 -0.3 -0.3 0.0	NA NA NA 0.0
Plan Irregularity, PL1	-0.7	-0.5 -0.7	-0.5 -0.6	-0.4 -0.5	-0.4 -0.5	-0.8 -0.5 -0.6	1.4 -0.7 -0.4 -0.4 -0.2 1.5	1.2 -0.7 -0.3 -0.4 -0.1 NA	-0.7 -0.4 -0.4 -0.1 1.4	-0.8 -0.4 -0.5 -0.2 1.7	0.9 -0.6 -0.3 -0.3 0.0 NA	-0.7 -0.4 -0.5 -0.2 1.5	-0.7 -0.4 -0.4 -0.1 1.7	-0.7 -0.4 -0.4 -0.2 1.6	-0.7 -0.4 -0.4 -0.2 1.6	-0.6 -0.3 -0.3 0.0 NA	NA NA 0.0 0.5
Plan Irregularity, <i>PL1</i> Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)	-0.7 -0.3 1.9 0.5 0.0	-0.5 -0.7 -0.3 1.9 0.5 -0.2	-0.5 -0.6 -0.3 2.0 0.4 -0.4	-0.4 -0.5 -0.3 1.0 0.3 -0.3	-0.4 -0.5 -0.2 1.1 0.3 -0.2	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2	1.4 -0.7 -0.4 -0.4 -0.2 1.5 0.3 -0.2	1.2 -0.7 -0.3 -0.4 -0.1	-0.7 -0.4 -0.4 -0.1	-0.8 -0.4 -0.5 -0.2	0.9 -0.6 -0.3 -0.3 0.0	-0.7 -0.4 -0.5 -0.2	-0.7 -0.4 -0.4 -0.1	-0.7	-0.7 -0.4 -0.4 -0.2	-0.6 -0.3 -0.3 0.0	NA NA NA 0.0
Plan Irregularity, <i>PL1</i> Pre-Code Post-Benchmark Soil Type A or B	-0.7 -0.3 1.9 0.5 0.0 -0.4	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.2	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2	-0.7 -0.4 -0.2 1.6 0.3 -0.2 -0.2	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	-0.7 -0.3 1.9 0.5 0.0	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 0.7	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5	-0.4 -0.5 -0.2 1.1 0.3 -0.2	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2	1.4 -0.7 -0.4 -0.4 -0.2 1.5 0.3 -0.2	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0	NA NA 0.0 0.5 0.1 -0.1
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (-3 stories) Minimum Score, SMIN	-0.7 -0.3 1.9 0.5 0.0 -0.4	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2	-0.7 -0.4 -0.2 1.6 0.3 -0.2 -0.2	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial □ /	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 0.7	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 -0.3 0.5 OTHEF Are There	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZA	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5	1.4 -0.7 -0.4 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.7 -0.4 -0.2 1.6 0.3 -0.2 -0.2	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$ EXTENT OF REVIEW Exterior: Partial Interior: None	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides /isible	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 0.7	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 -0.3 0.5 OTHEF Are There Detailed	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/ B HAZ/	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS s That T il Evalue	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Ves	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides /isible	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 0.7	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5 OTHEF Are There Detailed	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZA	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS s That T I Evaluential (un	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva wwn FEM less thar	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir n cut-off	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 -0.2 0.3	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides <i>V</i> isible No	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 0.7	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5 OTHEF Are There Detailed : Detailed : Poun cut-ol Fallin	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/ e Hazard: Structura ding pote ff, if know g hazard:	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 SThat T I Evaluential (un n)	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir n cut-off	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 -0.2 0.3	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (-3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Score	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides Visible No	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7 -0.4 0.7 -0.4 -0.4 -0.4 -0.4 -0.5 -0.2 -0.4 -0.4 -0.5 -0.2 -0.4 -0.5 -0.7 -0.3 -0.2 -0.4 -0.5 -0.7 -0.3 -0.5 -0.2 -0.4 -0.5 -0.2 -0.4 -0.4 -0.5 -0.2 -0.4 -0.5 -0.5 -0.2 -0.4 -0.5 -0.2 -0.4 -0.4 -0.5 -0.2 -0.4 -0.5 -0.5 -0.5 -0.2 -0.4 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 0.7	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5 OTHEF Are There Detailed 3 Detailed 3	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/ e Hazard: Structura ding pote ff, if know g hazard: ng	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS s That T il Evalu ntial (un n) s from ta	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile Ye Ye No Detaile	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3 ON RI ed Struct es, unkno es, score es, other	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva bwn FEM less thar hazards	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir present Evalua	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require ng type o	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 -0.2 0.3	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0 0.2	NA NA 0.0 0.5 0.1 -0.1 NA
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: Partial Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Scole Source: LEVEL 2 SCREENING PERFORMED	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides Visible No	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7 Aerit	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 -0.3 -0.3 -0.3 -0.3 -0.	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/ A HAZ/ B HAZ/ B HAZ/ C HAZ/ C	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS s That T I Evaluential (un n) s from ta	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile P Ye Not Detaile Detaile C Ye	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3 OON RI ed Struct es, unknows, score es, other of Nonst	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIF tural Eva bwn FEM less thar hazards tructural h	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir n cut-off present Evalua	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require ng type o	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 -0.2 -0.2 -0.3 -0.2 -0.3	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3 uilding	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0 0.2	NA NA 0.0 0.5 0.1 -0.1 NA 1.0
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Score, SL2	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides Visible No	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7 Q.7 Aeric Enter	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 -0.3 -0.3 -0.3 -0.3 -0.	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/ Structura ding pote ff, if know g hazards ng ogic haza	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS s That T I Evaluential (un n) s from ta	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile Ye Cont Ye Cont Detaile Detaile Detaile Detaile Detaile Detaile Detaile	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva swn FEM less thar hazards tructural h uctural hazards	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir present Evalua bazards i azards e s not ne	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require ng type o tion Rec identified xist that i cessary	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3 ed? r other but sommence that sho may requ	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3 uilding	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0 0.2	NA NA 0.0 0.5 0.1 -0.1 NA 1.0
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Brand Brand LEVEL 2 SCREENING PERFORMED Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides Visible No	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7 Q.7 Ente	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5 OTHEF Are There Detailed 3 Detailed 3	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/ B Hazard: Structura ding pote ff, if know g hazard: ng ogic haza icant dan ructural s	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS S That T I Evalu ntial (un n) s from ta rds or S nage/de ystem	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 -0.2 -0.3 0.5	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 -0.1 -0.5	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile Ye No Detaile C Ye C Ye C No de C No	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva bown FEM less thar hazards tructural hazards tructural hazards	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir n cut-off present Evalua azards i azards e s not ne I hazard	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require ng type o tion Rec identified xist that cessary is identified	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3 ed? r other but that sho may required	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 0.3	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0 0.2	NA NA 0.0 0.5 0.1 -0.1 NA 1.0
Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SMIN: EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Source LEVEL 2 SCREENING PERFORMED Yes, Final Level 2 Score, SL2	-0.7 -0.3 1.9 0.5 0.0 -0.4 0.7 All Sides Visible No	-0.5 -0.7 -0.3 1.9 0.5 -0.2 -0.4 0.7 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.2 -0.4 0.7 -0.3 -0.2 -0.2 -0.4 0.7 -0.2 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.2 -0.4 0.7 -0.5 -0.2 -0.4 0.7 -0.5 -0.2 -0.4 0.7 -0.5 -0.2 -0.4 0.7 -0.5 -0.2 -0.4 0 -0.5 -0.2 -0.4 0 -0.5 -0.2 -0.4 0 -0.5 -0.2 -0.4 -0.7 -0.5 -0.2 -0.4 -0.7 -0.5 -0.2 -0.4 -0.7 -0.5 -0.2 -0.4 -0.7 -0.5 -0.5 -0.2 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	-0.5 -0.6 -0.3 2.0 0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.4 -0.	-0.4 -0.5 -0.3 1.0 0.3 -0.3 -0.3 0.5 OTHEF Are There Detailed 3 Detailed 3	-0.4 -0.5 -0.2 1.1 0.3 -0.2 -0.3 0.5 R HAZ/A e Hazard Structural ding pote ff, if know g hazards ff, if know ff,	-0.8 -0.5 -0.6 -0.3 1.1 0.4 -0.2 NA 0.5 ARDS S That T I Evalu ntial (un n) s from ta rds or S nage/de ystem	1.4 -0.7 -0.4 -0.2 1.5 0.3 -0.2 -0.3 0.5 Frigger A ation? Iless SL2 aller adjac oil Type I terioratio	1.2 -0.7 -0.3 -0.4 -0.1 NA 0.2 -0.1 -0.1 0.5 Cent F n to	-0.7 -0.4 -0.4 -0.1 1.4 0.2 -0.1 -0.1 0.3 ACTI Detaile Ye No Detaile C Ye C Ye C No de C No	-0.8 -0.4 -0.5 -0.2 1.7 0.3 -0.2 -0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	0.9 -0.6 -0.3 -0.3 0.0 NA 0.1 0.0 -0.1 0.3 EQUIR tural Eva wm FEM less thar hazards tructural hazards tructural hazards tructural hazards tructural hazards	-0.7 -0.4 -0.5 -0.2 1.5 0.3 -0.2 NA 0.2 RED aluation A buildir present Evalua hazards is azards e is not ne l hazard	-0.7 -0.4 -0.4 -0.1 1.7 0.2 -0.1 -0.1 0.2 Require ng type o tion Rec identified xist that cessary is identified	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.3 -0.4 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.3 -0.4 -0.2 -0.3 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.2 -0.3 -0.2 -0	-0.7 -0.4 -0.4 -0.2 1.6 0.3 -0.2 -0.2 -0.2 -0.2 0.3 uilding	-0.6 -0.3 -0.3 0.0 NA 0.1 0.0 0.0 0.2	NA NA 0.0 0.5 0.1 -0.1 NA 1.0

Structure 50, Building 33 Photographs



Plan View, Middle Hallways are Structure 50



Previous Courtyards Filled-in to Build Library and Gym

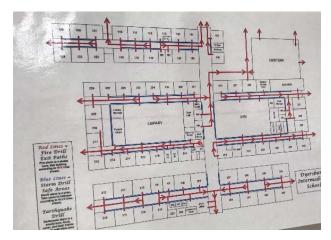


Connection from Structure 49 to 50

Level 1 VERY HIGH Seismicity

	A CONTRACTOR OF		1.00			Add	ress:	775	ST.	11 -	C1	(capture)					-
						Add	1622.		ST					1	1221)	
						Oth	er Identi	1AC	ersbi	ma)	IN			ip: 34	8064	1	
							ding Na		21		-	-	-				
						Use			mer	tur	50	lag					
The state of the second second								5104	237	Sur	304			00.3	MI	3M3	
PH	OTOGRA	ы				Ss:	27	175	051	444					540	773	2
	ion o ontra						ener(s)		μΛ	-	- '	1	083 ate/Time		17		-
						-				1				-04			
Sector States							Stories:		ve Grade			v Grade	: 0			19970	EST
							itions:			Yes, Y			964	70	Year:		
FIELD IN N							upancy:		embly	Comme		Emer. S	101		- 1).	Shelt	
Historm						000	apuncy.		ustrial	Office	1000	School	0111003		overnmen		er
TI Other form								Utili	ty	Wareho	use	Residen	tial, #Ur	10000			
D strict tarre						Soil	Type:		□в]E [NK		t::
			-					Hard	Avg	Dens	se St	iff S	oft P	oor If	DNK, assu	ıme Type	D.
14 41			No.		1	Geo	logic He	Rock	Rock	Soi					Quel D	ipt.: Yes/N	
add Add.		- marine				**********											NO/DNK
	Contraction in the		2000	-			acency:			ounding			azards fr	om Taller	Adjacen	Building	
			1		-	Irreg	gularitie	s:		ertical (ty an (type)	pe/sever	ity) –		10			
				1			erior Fal	ling		nbraced	Chimney	S	Hea	avy Clado	ling or H	eavy Ven	ieer
		1				Haz	ards:			arapets				bendages			
Library			4V	m		0	MMENT	c.	0	ther:	-						
		-	01														
					+	-	1 M	ASO	nn	1							
	1-1	5-1-				-	-	10.00	1								
	13				-	1	FIE	vil.	90	dia	ph	vali	ina				
		2					1 11	L J S K	nny	0.00		. not	VV C				
													,				
		1															
	SKETCH																
		ARIC	800		DIFIE				es or con				-				
FEMA BUILDING TYPE Do	Not W1	W1A	W2	RE, MO	_	-			-			100					
K	now	WIA	VVZ	(MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.9 -0.5	-0.9	100	-0.7 -0.4	-0.8 -0.5	-0.7 -0.4	-0.7 -0.3	-0.7	-0.8	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	0.000	-0.5	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3	-0.3	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark	1.9	1.9	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type A or B Soil Type E (1-3 stories)	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.2	-0.4		-0.2 -0.3	-0.2 NA	-0.2	-0.1 -0.1	-0.1	-0.2	0.0	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, SLI 2	SMIN: C	2.7	30),3													
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIF	RED					
Exterior: A Partial	All Side			Are Ther	e Hazaro	is That	Frigger A	4	Detail	ed Struc	tural Eva	aluation	Require	d?			
Interior: None		Ent Ent	ered	Detailed	Structur	al Evalu	ation?			es, unkno	wn FEM	A buildir	ng type o	r other bu	uildina		
Drawings Reviewed:				Poun			less SL2	>		es, score	less that	n cut-off					
Drawings Reviewed: Yes Soil Type Source:	Visible No				ff if Land	own) Yes, other hazards present											
Soil Type Source: Geologic Hazards Source:	No No		-	cut-o	ff, if knov g hazard		aller adia	cent			nazarus	present					
Soil Type Source: Geologic Hazards Source:				cut-o	g hazaro ng	ls from ta	aller adja		No No	D				ommon	had? (ab	ock cost	
Soil Type Source: Geologic Hazards Source: Contact Person: Brad	× No Baleer	:D?		cut-o	g hazaro ng ogic haza	ls from ta ards or S	oil Type	F	Detaile	o ed Nons	tructura	Evalua	tion Rec	comment			
Soil Type Source: Geologic Hazards Source: Contact Person: Brad for LEVEL 2 SCREENING PE	× No Baleer			cut-o	g hazaro ng ogic haza	ls from ta ards or S mage/de		F	Detaile	o ed Nons es, nonstr o, nonstru	tructural ructural h	l Evalua nazards azards e	tion Rec identified xist that	I that sho	uld be ev		
Soil Type Source: Geologic Hazards Source: Contact Person: Brad	RFORME			cut-o	g hazaro ng ogic haza ficant da	ls from ta ards or S mage/de	oil Type	F	Detaile	o ed Nons es, nonstr o, nonstru etailed ev	tructural ructural h uctural ha aluation	l Evalua nazards azards e is not ne	tion Rec identified xist that cessary	l that sho may requ	uld be ev ire mitiga	aluated	
Soil Type Source: Geologic Hazards Source: Contact Person: Brad for LEVEL 2 SCREENING PE Yes, Final Level 2 Score, S _{L2} Nonstructural hazards? Yes	RFORME		lo	cut-o Fallir build Geol Signi the s	g hazaro ng ogic haza ficant da tructural	ls from ta ards or S mage/de system	oil Type terioratio	F In to	Detaile	ed Nons es, nonstr o, nonstru etailed ev o, no non	tructural ructural h uctural ha aluation structura	l Evalua nazards azards e is not ne il hazard	tion Rec identified xist that cessary Is identifi	I that sho may requ ed	uld be ev lire mitiga	aluated	
Soil Type Source: Geologic Hazards Source: Contact Person: Brader LEVEL 2 SCREENING PE Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes Where information	RFORME	be verifie	lo ed, scro	cut-o Fallir build Geol Signi the s	g hazaro ng ogic haza ficant da tructural	ls from ta ards or S mage/de system ne follow	oil Type terioratio	F in to ST = Esti	Detaile	ed Nons es, nonstr o, nonstru tailed ev o, no non r unrelia	tructural h ructural h uctural ha aluation structura ble data	Evalua nazards azards e is not ne il hazard	tion Rec identified xist that cessary Is identifi	I that sho may requ ed E to Not Kr	uld be ev iire mitiga DNK	aluated	a

Structure 51, Building 33 Photographs



Plan View, Top Hallway is Structure 51



Interior, Reinforced Masonry

Level 1 **VERY HIGH Seismicity**

			-			Add	Iress:				, Mai			LVD	807	4	
						Oth	er Ident	ifiers:	52	9.0	1.12			p	0-2	1	
							Iding Na			_					and and		
									le S		1		and the second	00			
DUC	TOGRAF	ш							0331	85		Longitu	ide: ~	89.	35	3337	2
FIL	JIUGRAP	'n				Ss:	eener(s)	189	MA			1000	0.80	1.1.1	-		
						-		(a) 1998 (a)					ate/Tim	-			
						Tota	Stories al Floor litions:			18	Belov 0 0 0 C Year(s) E	00	ə: _O	Yea Code	r Built: e Year:	2001	EST
							upancy	: Ass	embly ustrial	Comme Office Wareho	ercial	Emer. S	Services ntial, #U		istoric overnmer	□ Shell nt	ter
						Soil	Туре:	Hard	B Avg	Der	ise S	D	E Soft F	F D	NK DNK, ass	ume Type	D.
1		1				Geo	logic H	Rock	Rock					Soil s/No/DNK	Curf D	unt : Vaci	
			1				acency:			ounding				rom Taller			
			1				gularitie		XV	ertical (t	pe/sever	ity) S	1 410	evel/	mad		
		-				Exte	erior Fa	ling			Chimney			avy Clade			
				-1			ards:			arapets	Chininey	5		pendages		eavy ver	neer
			Г			CO	MMENT	S:								-	
	_		L-	1		_	· Spl	if l	evel	0	dru	-101	hang	e in	1-00-	f Lei	ght)
						-	·Mo	Sor	ns	hein	nfor	ied	-				
				L			1.		.12			~~~					
F.		-					.110.	v-k	aval	let	syst	-em:	5				
	SKETCH	-				1	Addition	al sketch	les or cor	mments	on separa	ate nade					
	E	ASIC	sco	RE, MO	DIFIER												
FEMA BUILDING TYPE Do N Kno	ot W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	D	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 - Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9	-0.8	-0.7 -0.4	-0.8 -0.5	-0.7	-0.7 -0.3	-0.7	-0.8 -0.4	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3	NA NA
Pre-Code Post-Benchmark	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	1.9	1.9	2.0	1.0	1.1 0.3	1.1 0.4	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	-0.1 NA
Minimum Score, S _{MIN}	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_N$. DE (0.3		_												
EXTENT OF REVIEW				OTHER					ACT	ION R	EQUIF	RED	6		A COLOR		
Exterior: Partial Interior: None	All Sides			Are There Detailed	e Hazard	That T	Frigger A	1	Detail	ed Struc	tural Eva	aluation	Require	ed?			
Drawings Reviewed: Yes	No		cicu	Poun	ding pote	ntial (ur	0.0000000	>	Ye Ye	es, score	less that	n cut-off		r other bu	uilding		
Geologic Hazards Source: Contact Person: Brad B	aver	-			g hazards		aller adja	cent		0	hazards						
101000 10	Contraction New York	-	-	Geolo	ogic haza	ds or S	oil Type	F						comment			
LEVEL 2 SCREENING PER	FORME	<i>К</i> N			ficant dan tructural s		terioratio	n to		o, nonstr tailed ev	uctural ha	azards e is not ne	xist that cessary	I that sho may requ	uld be ev ire mitiga	aluated ation, but	а
Nonstructural hazards? Yes			and the second second			_				o, no nor	structura	I hazard	s identifi	ed ዾ	DNK		
Where information	n cannot k	e verifie	d, scre	ener shal	note the	follow	ing: ES	GT = Esti	mated o	r unrelia							
Legend: MRF = Moment- BR = Braced fra		ne (RC = Re SW = St	inforced cor near wall	ncrete	T	JRM INF = 'U = Tilt u	= Unreinfo p	rced maso	onry infill	MH =	= Manufa = Light me	ctured Ho etal	using FI Ri	D = Flexib D = Rigid	e diaphrag diaphragm	gm

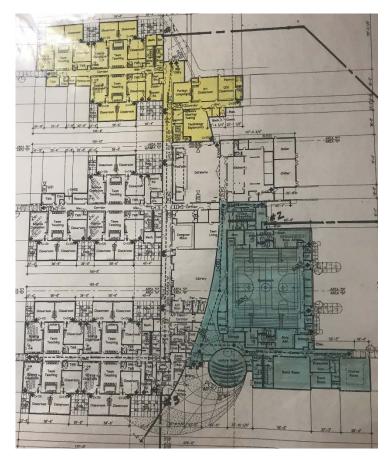
Structure 52, Building 34 Photographs



Reinf. Masonry, Non-parallel System



Gymnasium, Flexible Diaphragm Roof

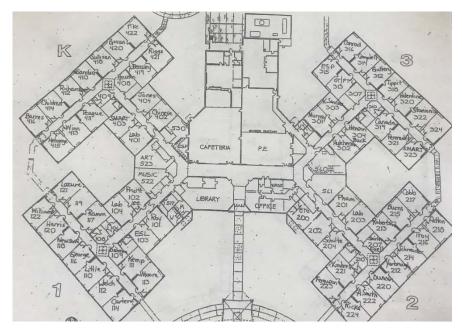


Plan View, Non-parallel Systems, Reentrant Corner

Level 1 VERY HIGH Seismicity

					10	Add	ress: _	1429 Dve	s Fr Susbu	ing, T	May	Nord	Dr	Zip: 38	3024		
						Oth	er Ident	ifiers:	53	0.				-			
						Buil	ding Na	me:									
						Use				Sch							
										831		ongitu	de:	89,3	5615	546	
РНОТО	OGRAP	н						267			•	A CONTRACTOR	1,834				
						_		: <u>C</u>	0	_	_	D	ate/Tim	e:			
						Tota	al Floor	Area (se	q. ft.):	74	2081		0	-	r Built: e Year:	9921	EST
							litions:	N		Yes, Y					- 101		
						Occ	upancy		embly ustrial ty	Comme Office Wareho	(Emer. S School Residen	ervices tial, #Ur	A PLATE AND A PLAT	istoric overnmer	Shelt nt	ter
		1				Soil	Type:	Hard Rock	Avg Rock	Den: Soi	se St	iff S	oft P		NK DNK, ass	ume Type	D.
		1	1			Geo	logic H	and the second state of th		ction: Yes					Surf. R	upt.: Yes/	No/DNK
		1		/			acency:			ounding						t Building	
		/			>	Irreg	gularitie	is:		ertical (ty lan (type)	pe/sever	ity) Sp		evel		1	
			\langle	× /			erior Fal ards:	lling		nbraced arapets ther:			Hea		ding or H	eavy Ver	neer
	-	1			>	co	MMENT	S:									
		1		,	/		M			reit	16.	ind					
	-		Y	/			1.10	son	rys.	101	101	Leo					
		1		/		.(otter	r plo	in m	rrear	Ilari	ty:	Non.	-paro	illel s	vstem	S
			V			-		V		1		1		1		1	
			-			-											
			1														
		-				-											
SK	ETCH	ASIC	500	RE, MO	DIFIE					mments o							
FEMA BUILDING TYPE Do Not	W1	W1A	W2	S1	S2	S3	S4	S5	C1	C2	C3	PC1	Dea	DHA	DHA	Unit	
Клож				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	(1.1)	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9	1000	-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, P_{L1}	-0.6 -0.7	-0.5	-0.5		-0.4	-0.5	-0.4	-0.3 -0.4	-0.4	-0.4	-0.3	-0.4	-0.4	2	-0.4	-0.3	NA
Pre-Code	-0.3	-0.3	-0.3	1000	-0.2	-0.3	-0.4	-0.4	-0.4	-0.5	-0.3 0.0	-0.5 -0.2	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	(1.0	-0.2	0.0 NA	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories) Minimum Score, Smin	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
and a second	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	0	.9)=	20,3	5				_	-								
EXTENT OF REVIEW		2		OTHER						ION R							
Exterior: A Partial	All Sides	Aer	ial	Are Ther				A	Detail	ed Struc	tural Eva	aluation	Require	d?			
	Visible No	Ent Ext	ered	Detailed						es, unkno	wn FEM	A buildin	iq type o		uildina		
Soil Type Source:	NU			Poun	ding pot	ential (ur	less SL2	>	X Y	es, score	less than	1 cut-off					
Geologic Hazards Source:	-	1		Cut-o	ff, if know	wn) ds from ta	aller adia	cent		es, other	hazards	present					
Contact Person: Brad Bak	ing				1000 AC		ruotural	Evelue	lion Dr.		de 40 /						
LEVEL 2 SCREENING PERF	ogic haza	ards or S	oil Type	F		ed Nonst											
		mage/de	terioratio	on to		es, nonsti o, nonstru	uctural h	azarde e	uentified	may room	uld be ev	aluated					
Yes, Final Level 2 Score, SL2		M N		the S	tructural	system			de	tailed ev	aluation	s not ne	cessarv	may requ	ine mug	auon, but	d
Nonstructural hazards? Yes			ю							o, no non	structura	I hazard	s identifi		DNK		
Where information	cannot b	e verifie	d, scre	ener shal	I note th	e follow	ing: ES	ST = Esti	mated o	r unrelia	ble data	OR I	DNK = D	o Not Ki	now		
Legend: MRF = Moment-res BR = Braced frame		le	RC = Re	einforced con		1	JRM INF :	= Unreinfo			MH	= Manufa	ctured Ho	using F	D = Elexib	le diaphra	gm
Dr - Diaceu liame			000 = 51	near wall		3	rU = Tilt u	p			LM =	Light me	tal	R	D = Rigid	diaphragm	1

Structure 53, Building 35 Photographs



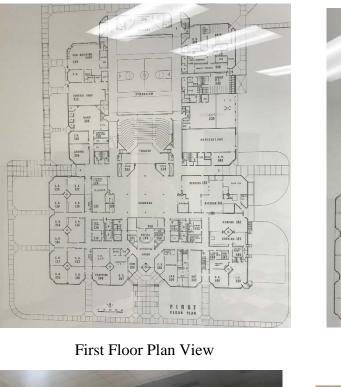
Plan View, Building Layout

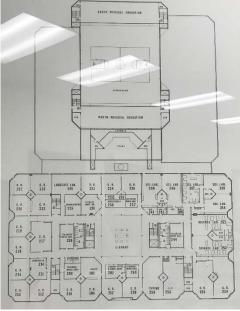


Exterior Aerial View

							Iroca	175	110	3-	(-					
						Add	Iress:	200	-VS		TAS	-	_	2	0001	1	
							1	yer	spr	41	10		Z	ip:)	8024	1	
								ifiers:	54	0	_	-		-			
							Iding Na										
									. se								
						Lati	tude:	36,	0559	58	1	ongitu	de: -	89	384	Fal	1
PH	OTOGRAP	н				Ss:		1.35					2.87				
						Scr	eener(s)		M				ate/Time				
										1			a second second		_	110.0	-
						NO.	Stories	: Abov	ve Grade	1	Belov	v Grade	: 1			19751	EST
											5,00		-		e Year:	-	
						Add	litions:	🗆 N	lone D	Yes,	Year(s) B	uilt: _	en	kna	n		
						Occ	upancy	: Ass	embly	Comme	ercial	Emer. S	ervices	Пн	istoric	Shelt	ter
								Indu	ustrial	Office		Schoo		G	overnmer	nt	
								Utili	ty	Wareho	ouse	Residen	itial, #Un	nits:			
			-			Soil	Type:		□в	X	c 🗆		E C]F D	NK	······	
5 ml h								Hard	Avg	Der	ise St	iff S	oft P			ume Type	D.
TASSFam		-						Rock	Rock	Sc	And the second sec			ioil			
	F	Concerned and	T	-		Geo	logic H	azards:	Liquefac	ction: Ye	s/No/DNF						
TJOther Form				-		Adj	acency:		D P	ounding		Falling H	azards fro	om Talle	r Adjacen	t Building	
	- NET TO THE		125	200 mart		Irre	gularitie		K V	ertical (h	/pe/sever						
	The pro-						Janantic		E PI	an (type)	-1- (i)	11 124	-/11-50	100	5121	06
	-			and a state of the		Ent	avian Fal										
	1000			D. Com			erior Fal ards:	lling			Chimney	S				eavy Ver	neer
	NG				-	naz	aius.			arapets ther:			Ц Арр	endages	5		
	sik hi	ayt	hrou	5h buij	ding	-				iner:		_			-		
Duilding		-		211	- 5	- 00	MMENT	5:	,								
	316.1		10 10	and the second s		1	» (x	ma.	COL	UMI	hs 1	thr	outh	out	8		
id ing	f	lint e	~	125					6				2				
125		Highe	5	-		-	1	Orl	CB)							
123	1	roof	1			-	~	-	-								
2	F.	heigh	1 1			_											
	1	ve gr	1 1	_													
-																	
	- d - a las					-											
	SKETCH	-					Addition	al sketch	es or cor	nments	on separa	te page					
	B	ASIC	sco	RE, MO	DIFIE												
FEMA BUILDING TYPE Do N		W1A	W2		S2	S3	S4	S5	-			-				1	
Kn			112	(MRF)	(BR)	(LM)	(RC	(URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	24	10	1.0	1.			SW)	INF)			INF)			(10)	(10)		
Severe Vertical Irregularity, VL1	-0.9	1.9 -0.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.5	-0.9	10000	-0.7 -0.4	-0.8 -0.5	-0.7	-0.7	-0.7 -0.4	-0.8	1.0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.4	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4 -0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.4	-0.2	0.0	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	-0.2	1.7	-0.2	-0.2	0.0 NA	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, S _{MIN}	0.7	0.7	0.T	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ S.	win:	0.	>1	1.31						in the second	-			HI			-
		U					-		-						_		-
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIR	RED					
	All Sides			Are There	e Hazard	Is That T	Trigger A	A	Detail	ed Struc	tural Eva	luation	Require	d?			
	Visible	A. Ent	ered	Detailed	Structur	al Evalu	ation?		100000		own FEM				uilding		
Drawings Reviewed: Ves Soil Type Source:	No No			Poun			less SL2	>	Ye Ye	es, score	less than	n cut-off	a abe of	Juner Di	unung		
Geologic Hazards Source:			-		ff, if know				1 🗋 Ye	es, other	hazards						
Contact Person: Brad	hak al	-	-			is from ta	aller adja	icent				Contraction of the					
JJAAN	JULCI	_		buildi		ards or O	oil Type	F	Detail	d Nons	tructural	Evalua	tion Rec	ommen	ded? (ch	eck one)	13
LEVEL 2 SCREENING PER	FORME	D?					terioratic		Ye	es, nons	tructural h	azards i	identified	that sho	uld be ev	aluated	1
Yes, Final Level 2 Score, SL2										o, nonstr	uctural ha	azards e	xist that r	may requ	ire mitig	ation, but	a
Nonstructural hazards?					de	tailed ev	aluation i	s not ne	cessary								
							nstructura				DNK						
Where informati						e follow	ing: ES	ST = Esti	imated o	r unrelia	ble data	OR I	DNK = D	o Not Kr	now		
Legend: MRF = Moment	-resisting fran	10	RC = Re	einforced cor		(JRM INF :	= Unreinfo	rced maso		MH	= Manufa	ctured Hou	using Fl	D = Flexib	le diaphrag	gm
BR = Braced fra	III III IIII		OW = S	hear wall			rU = Tilt u	p			IM=	Light me	atal		D - Digid	diaphragm	

Structure 54, Building 36 Photographs





Second Floor Plan View



Interior, Split Level



Interior, Exposed Concrete System



Exterior, Out-of-Plane Setback

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

			-			Add	ress:	175	()<		1						-
						Aud							-	1 7	707	4	
						044	or Idans	ifiers:	iburg	106	10		2	2ip: <u>3</u>	san c	-1	
								_	>>							-	
						Use	ding Na		~ 31	100	1						
									552			analtu	da	89,3	OFC	130	
PHOT	OGRAP	н				Ss:		370		.00		Longitu	.871	09,3	683	137	
11101	JOIN							: C1				and the second second	ate/Time				
							055							-341	-	IdMI	-
									e Grade			w Grade	:_0			1974	EST
								Area (se		70	Year(s) B	00		_ Code	Year:		
						Large Data			embly	Comme							
						000	upancy		istrial	Office	ircial	Emer. S	ervices	HI	storic overnmer	Shelt	ler
								Utili		Wareho	use		tial, #Ur	1000 20	over miner	n	
						Soil	Type:		□в	Ø	сг		JE D		NK		
FIN. C.			1			-	.,,	Hard	Avg	Den	se S	tiff S	oft P			ume Type	D.
Diris tam		1				-	1	Rock	Rock	So				Soil			
Dithis form DOther form	r	-	-									TITLET BUILDER COMPANY				upt.: Yes/	
Clothe rolling	- 1		-		-		acency:			ounding			azards fr	om Taller	Adjacen	t Building	
	MN	2				Irre	gularitie	S:		ertical (ty an (type	pe/sever	ity) _					
	Building										Chimney	S	Hea	avy Clado	ling or H	leavy Ver	neer
and the second s														pendages			
- k	Jalki	NOV Der				-			0	ther: _	- Sector			_			
	AA .	~		-		CO	MMENT	S:		in	inf	2000	nd				
	Mai	11				-	11/1	2001	h vy ble	216	7816	orce	en				
	Buil	dia	1				TI.	11:1	1.10	1:0	du	CA QU	~~				
	Dill	lari	9					exi	pic	Nu	pru	2	V				
			5			-											
la formation of the second sec		_				1											
sk	ETCH						Addition	al skotch	es or cor	monte		ato nono					
	a she make the set	ASIC	sco	RE, MO	DIFIE												-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	and the second s	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	SW)	INF)			INF)			2			
Severe Vertical Irregularity, VL1	-0.9	-0.9	-0.9	1000	-0.7	-0.8	-0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	-0.7	-0.7	-0.7	-0.7	0.9 -0.6	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5		-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.0	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	12.02	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code Post-Benchmark	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	1.9	1.9 0.5	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	1	-0.2	0.4	0.3	0.2	0.2	0.3 -0.2	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.2	NA	-0.2	-0.1	-0.1	-0.2	-0.1	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1 NA
Minimum Score, S _{MIN}	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	C	(P.C	20	5,0													
EXTENT OF REVIEW		-		OTHE	R HAZ	ARDS			ACT		EQUIF	RED					
	All Sides			Are Ther				4	1.1.1.1.1		tural Ev						
Interior: I None I None Drawings Reviewed: Yes	Visible No	Ent Ent	ered	Detailed					Ye	es, unkno	own FEM	IA buildir	ng type o	r other bu	uilding		
Soil Type Source:				Pour Cut-o			nless SL2	>	Ye Ye	es, score	less tha	n cut-off					
Geologic Hazards Source:	eologic Hazards Source:										hazards	present					
Contact Person: Brad Ba	ing		and the second		Detaile		tructura	I Evalua	tion Rec	ommen	led? (ch	eck one)					
LEVEL 2 SCREENING PERF	ogic haza ficant da	ards or S	terioratic	F						that sho							
The second s	LEVEL 2 SCREENING PERFORMED? Significant of the structural the st									o, nonstr	uctural h	azards e	xist that	may requ	ire mitig	ation, but	а
Nonstructural hazards?									de	tailed ev	aluation	is not ne	cessary				
	Where information cannot be verified, screener shall note th										structura				DNK		
Legend: MRF = Moment-res				eener snal					mated o								
BR = Braced frame	and indi			hear wall	101018	-	TU = Tilt u	- Unreinto	iceu maso	onry intill	MH	= Manufa	ctured Ho	using FI	J = Flexib	le diaphra	gm

Structure 55, Building 37 Photographs



Exterior



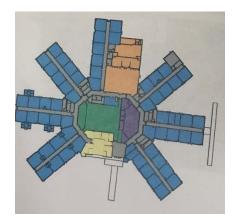
Interior, Reinforced Masonry, Flexible Roof System



Interior, Flexible Roof System

рнот	DGRAP	'n				Oth Buil Use Lati Ss: Scr No. Tota Ado	er Ident Iding Na : tude:	ifiers: 1 ime:	rawy 721 we Grade q. ft.):	501 4520 198	Belov Year(s) B	Longitu S1: D W Grade	de:	e: <u>6</u> Year Code	556 (1) Built: 1 Year:	980 (
							Type:		ustrial	Office Wareho	use C C se St	Residen	> tial, #Ui E [Soft P	TF DI	overnmen	Shelt	
		~		\wedge		Geo	logic H							No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
			1		>		acency:		D P	ounding		Falling H	azards fr	om Taller	Adjacen	t Building	
V		~		/		Irre	gularitie	s:	X Ve	ertical (ty	pe/sever	ity) Se	141	evel/	mod		
				4	_	Exte	erior Fal	lina			Chimney			avy Clado			loor
1		1					ards:		D Pa	arapets	orminoy			pendages		eavy ven	ieei
21	1	~]				CO	MMENT	S.		ther:		-					-
	1	1				-	SI	1 loc	dec	Kina	AW	· pro	ivel	rootems			
				/			01	line	00'1	lain	-DAC	allel	Sust	ms			
1 1		-		/			riar	1 761	ed.	1010	pm	with	100	chilo			
1Dar	red		1	1													
roz				\bigvee													
			_	_		-											
SK	TCH		-				Addition	al sketch	es or cor	nments c	on separa	ate page					
	_	1	-	RE, MO	-	-	ND FIN	NAL LI	EVEL	1 SCO	RE, S	L1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8	1.5 -0.8	1.4 -0.7	1.6 -0.8	1.4 -0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9	1.1	1.0	11	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5		-0.4	-0.5	-0.4	-0.7	-0.7	-0.0	-0.6 -0.3	-0.7 -0.4	-0.7 -0.4	-0.7	-0.7 -0.4	-0.6 -0.3	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	(-0.3	-0.4	-0.3	NA
Post-Benchmark	-0.3	-0.3	-0.3	-0.3	-0.2	-0.3	-0.2	-0.1 NA	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	1.4	1.7	NA 0.1	1.5 0.3	1.7	1.6	1.6 0.3	NA 0.1	0.5 0.1
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories) Minimum Score, Smin	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	Ċ	71	=(0,3)	-	-								-			
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIF	RED					
Interior: None Drawings Reviewed: Yes Soil Type Source:	/isible	Aer Aer			Structur ding pot ff, if know	al Evalu ential (ur wn)	ation? nless SL2	>		es, unkno es, score es, other	tural Eva own FEM less than hazards	A buildir n cut-off	ng type o	ed? r other bu	uilding		
	Geologic Hazards Source:									0							
101110														commend			
Ves, Final Level 2 Score, SL2 Nonstructural hazards?										o, nonstru tailed ev	ructural h uctural ha aluation i structura	azards e is not ne	xist that cessary	I that sho may requ ed	uld be ev ire mitiga DNK	aluated ation, but	а
Where information	Where information cannot be verified, screener shall note th																
Legend: MRF = Moment-res BR = Braced frame	sting fram	ne	RC = Re	einforced cor hear wall		1		= Unreinfo	rced masc		MH		ctured Ho	using FI) = Flexibl	e diaphrag diaphragm	gm

Structure 56, Building 38 Photographs



Plan View



Interior, Split Level in Library

						Add	ress:	101	TC	N-	19	1.					
								Rie	rev	1TC	J		Z	ip: 3	806	2	
						Othe	er Identi	ifiers:	57			1.000			0.00	0	
							ding Na	me:									
						Use	E	lerr	ren	tarv	Sur	1001					
and the second second						Latit		35.		77	SL	ongitu	de:	891	557	356	,
PHC	TOGRAP	н				Ss:	1.	555			5	S1: (0.54	14			
						Scre	ener(s)	: C	M			D	ate/Time	e: 6/	11		
						No.	Stories:	Abov	e Grade	: 1	Below	v Grade	:0	Yea	Built:	19960	EST
						Tota	I Floor	Area (so	q. ft.):	108	194				Year:		
						Add	itions:		one [Yes, Y	'ear(s) B	uilt:		-	a series and a		1
						Occ	upancy	: Ass	embly	Comme	rcial	Emer. S	ervices	н	storic	Shelt	er
									Istrial	Office		ChooD			overnmen	it	
								Utili		Wareho			tial, #Ur	nits:			
						Soil	Type:	Hard	Avg	Dens					NK and	uma Tuna	-
		-	-	-		_		Rock	Rock	Soi				oor <i>If</i> Soil	DINK, assi	ume Type	D.
						Geo	logic Ha	azards:	Liquefac	tion: Yes	No/DNK	(Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/N	No/DNK
						Adja	acency:		D P	ounding	F	alling H	azards fr	om Taller	Adjacen	t Building	
		1				Irreg	gularitie	s:			pe/severi		val	Corv	Orc.		
						Exte	erior Fal	ling			Chimney				the second s		
		Π	-	IT			ards:	iiriy	D Pa	arapets	Gnimney	5		oendages	aing or H S	eavy Ven	eer
			1	61	4	TCO	MMENT	S:		ther:						-	
	N					1	Mas	ioni	NO	reil	nfor ohro	ced					
			+-		-		1.10 .		1								
						(He	Xib	e d	UGA	phro	nar	n				
	- de	-	_	L		-			-	1		0					
	14			-													
						-											
	1.1.	1 1			-	-											
	KETCH	4010			DIFIE						on separa			_			_
FEMA BUILDING TYPE Do No			-	RE, MO		-	-		1				1				
Kno	Carlo Car	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score	2.1	1.9	1.8	0	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.9 -0.5	-0.9		-0.7	-0.8	-0.7	-0.7 -0.3	-0.7	-0.8	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3	555	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark Soil Type A or B	1.9	1.9	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.0	1.6	NA	0.5
Soil Type E (1-3 stories)	0.5	0.5	-0.4		0.3	-0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.2	-0.1	NA	-0.1	-0.2	-0.2	0.0	-0.1 NA
Minimum Score, S _{MIN}	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_N$	IIN: (2.3)2	0,3													
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION R	EQUIR	RED					
	All Sides			Are Ther				A	Detail	ed Struc	tural Eva	aluation	Require	ed?			
Interior: None Drawings Reviewed: Yes		K Ent	ered	Detailed										r other b	uilding		
Soil Type Source:	1 110			Poun cut-o	ding pote ff, if know		less SL2	>		es, score	less than	n cut-off					
Geologic Hazards Source:				Fallin	ig hazaro	ds from ta	aller adja	cent		s, outer D	hazards	present					
Contact Person: 120mn/C	Contact Person: 20001C VOCK building										tructural	Evalua	tion Rec	commen	ded? (ch	eck one)	
LEVEL 2 SCREENING PER	LEVEL 2 SCREENING PERFORMED?									es, nonst	ructural h	nazards	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2	tructural		ult			o, nonstru	uctural ha	azards e	xist that	may requ	ire mitig	ation, but	a				
Nonstructural hazards? Yes						alled ev	aluation i structura	Is not ne	cessary s identifi	ed D							
Where information	n cannot l	e verifie	d, scr	eener shal	I note th	e follow	ina: FS	ST = Esti									-
Legend: MRF = Moment- BR = Braced fra	resisting fran	ne l	RC = R	einforced co		l	JRM INF	= Unreinfo								le diaphrag	m
	ma			shear wall	a-0202556	-	rU = Tilt u							woning F	- 1 10/10	u u dullidu	401

Structure 57, Building 39 Photographs



Plan Views



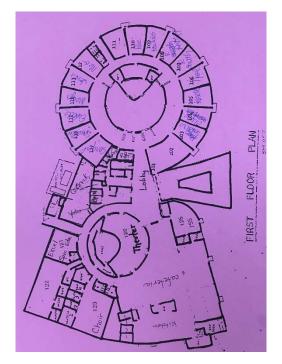
Exterior, Split Level



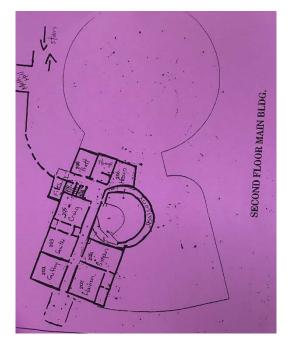
Interior, Split Level

РНОТ	OGRAP	н				Othe Buil Use Latin Ss: Scree No. Tota Add	er Identi ding Na	fiers: me: High SS, 34 Abov Area (so Area (so N : Asse	e Grade (, ft.): embly	206 1978, Y Comme	Belov Googlear(s) B rcial	ongitu Sr:Da v Grade uilt: 1 Emer. S	de: de: ate/Time : 996	e: 6/ Year Code	S38 1 Built: Year:	585 968 c	
						Soil	Type:	Utilit Utilit Hard Rock	strial y Avg Rock	Office Warehou Dens Soi	use	D	oft P	F Di	NK DNK, assi	ume Type	D.
1						Geo	logic Ha	azards:	Liquefac	tion: Yes	/No/DNk	(Lands		/No/DNK	Surf. Ru	upt.: Yes/i	No/DNK
						**********	acency:			ounding				om Taller			
$\langle \rangle \star$	X		-	-		Irreg	gularitie	s:	PI PI	an (type)	pe	m		lel a	1. 00 System		gran
1 LA	-	add	ïf;	on	7	and the second second	erior Fal ards:	ling		nbraced (arapets ther:	Chimney	S		avy Clado pendages		eavy Ven	eer
	/	-	/			CO	MMENT	S:			10.00						
Ly L	10B	V		~			TPZ	FI	exi	ble	100	f					
		1 DOM		is for									120	nir	Non	1	
migin	al 1								prin	ner c	SA 2 E	BWI	1 pin	4.14	icq.	.)	
(0)	131	FI	041	ner fo	m	1	PM	1									
Certification of the second se	/	4								1.							
						X	Vis	vble	: On	ACK	ng						
SK	ETCH	-	-			0.00	Additiona				2	ate page					
	В	ASIC	sco	RE, MO	DIFIER												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	91	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.9 -0.5	-0.9	22.22	-0.7 -0.4	-0.8 -0.5	-0.7	-0.7	-0.7	-0.8	-0.6 -0.3	-0.7 -0.4	-0.7 -0.4	-0.7	-0.7 -0.4	-0.6 -0.3	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA NA
Pre-Code Post-Benchmark	-0.3 1.9	-0.3 1.9	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	0.4	1.0	1.1 0.3	1.1 0.4	1.5	NA 0.2	1.4	1.7 0.3	NA 0.1	1.5 0.3	1.7 0.2	1.6	1.6	NA 0.1	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories) Minimum Score, SMN	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN		-0.1	1.	> (0,	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW		0	10	OTHE	-	ARDS		-	ACT	ION R	FOLIE	ED					
Exterior: 🕅 Partial 🔲	All Sides	Aer	ial	Are Ther					A CONTRACTOR OFFICE	ed Struc			Require	che			
	Visible	A Ent	ered	Detailed	Structura	al Evalu	ation?		1963					or other bu	uildina		
Drawings Reviewed: Yes X Soil Type Source:	INO				ding pote		nless SL2	>	2 Y	es, score	less that	n cut-off	• •				
Geologic Hazards Source:		ff, if know ig hazard		aller adja	cent	X Y	es, other	nazards	present					2			
Contact Person: Donnie	ing		and the second second		1.100	Second Second	ructural	Evalua	tion Red	comment	ded? (ch	eck one)					
LEVEL 2 SCREENING PERF	ogic haza ficant dar	ras or S nage/de	terioratio	r n to		es, nonst	ructural h	nazards i	identified	that sho	uld be ev	aluated					
Yes, Final Level 2 Score, SL2										o, nonstru	uctural ha	azards e	xist that	may requ	ire mitig	ation, but	а
Nonstructural hazards? Yes No										tailed ev	structura	Is not ne	cessary s identifi	ied 17	DNK		
Where information	cannot b	e verifie	d, scr	eener sha	I note the	e follow	ring: ES	T = Esti								No. of Street	
Legend: MRF = Moment-res BR = Braced frame	sisting fram	10	RC = Re	einforced co hear wall		(URM INF = TU = Tilt u	Unreinfo						ousing Fl		le diaphrag	jm

Structure 58, Building 40 Photographs



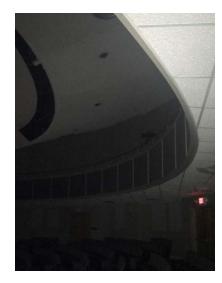
First Floor Plan View



Second Floor Plan View



Exterior, Out-of-Plane Setback



Interior, Split Level



Exterior, Split Level

						Add	ress: _	ZSL	1 5		Hers	ans					
								Rip	ley	TN			7	ip: 38	p63		
							er Identi		59		-						-
						Use	ding Na	Hia	6 5	scho	1		2.50	-	-		-
						100		35.	520	180	1	ongitu	de: -	-89.	<217	886	-
PHOT	OGRAP	н				Ss:		534	15	1.	-	S1: 0	153	7	22 1	00	1
						Scre	ener(s)		-M				ate/Tim		11		-
							Stories:		e Grade			v Grade	: 0			996	EST
							I Floor . itions:	Area (so		3 Yes, Y			196		Year:		
the indication							upancy		embly	Comme		Emer. S		U Hi	storic	Shelt	or
n network the									Istrial	Office	U.U.	School	0.11000	Contraction of the	overnmer		CI
								Utilii	ty	Wareho		Residen	tial, #Ui	nits:			
	-	1 1		-	-	Soil	Туре:	Hard	B Avg	Dens					NK and	ume Type	0
	4							Rock	Rock	Soi	I Se	oil S	ioil S	Soil			COALD
	1	140														upt.: Yes/I	and the second
/ HAL		1.					acency:		and the second second	ounding			azards fr	om Taller	Adjacen	t Building	
	1	Y	-	1		Irreg	gularitie	s:		ertical (ty an (type)	pe/sever <i>Ŷ C</i>	- Ch-	trant	Corr	cr		an analysis
	CIT	-	1.0	~ 1		Exte	erior Fal	ling		nbraced	ALLOWING CONTRACTOR	and the second se				eavy Ver	neer
1 74	1	040	(7)	/			ards:			arapets				pendages			
	/	210	/			CO	MMENT	S:						-	-	-	_
, ' L	-1	/					DIA	1									-
		1		this P	brm		FIV	17									1.38
(priAi	nal	1			0												÷.
1010	V	1	0	other	form												2.1
	X	30'															-184
	F	30															2.1
SK	ETCH						Addition	al sketch	es or cor	nments c	n senara	ate nade					
	-	-		RE, MO	DIFIE												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	11	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.9 -0.5	-0.9		-0.7 -0.4	-0.8	-0.7	-0.7 -0.3	-0.7 -0.4	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7 -0.4	-0.7 -0.4	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4	-0.4	(-0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code Post-Benchmark	-0.3 1.9	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0,2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	2.0	1.0	1.1	1.1	1.5	NA 0.2	1.4	1.7 0.3	NA 0.1	1.5	1.7	0.3	1.6 0.3	NA 0.1	0.5 0.1
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	1000	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories) Minimum Score, Smin	-0.4	-0.4	-0.4		-0.3	NA 0.5	-0.3 0.5	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	1	1,3)	20	3	0.0	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW		2.0).		OTHER	RHAZ	ARDS			ACT	ION R	FOLIE	PED			-		-
	All Sides			Are Ther	e Hazard	ds That	Trigger A	A		ed Struc			Require	d?			
	Visible No	A Ent	ered	Detailed	Structur	al Evalu	ation?							r other bi	uilding		
Soil Type Source:	NU			Poun cut-o	ding pot ff, if knov		nless SL2	>	Ye Ye	es, score es, other	less that	n cut-off			•		-
Geologic Hazards Source:	1-1-			Fallin	g hazard		aller adja	cent			11828105	present					
Contact Person: 1200020	ng Daic haz	ards or S	oil Type	F							ded? (ch	eck one)					
10111-20	1			1 1 1900													
LEVEL 2 SCREENING PERF	1	D?		🔀 Signi	ficant da	mage/de	terioratio	on to		es, nonst	ructural h	nazards	identified	that sho	uld be ev	valuated	
LEVEL 2 SCREENING PERF	1	D?		🔀 Signi	ficant da tructural	mage/de	terioratic	on to	D No de	o, nonstru tailed ev	aluation	azards e is not ne	xist that cessary	may requ	uld be ev ire mitig	valuated ation, but	
LEVEL 2 SCREENING PERF Yes, Final Level 2 Score, SL2 Nonstructural hazards?	ORME	D? ⊠ N	ю	X Signi the s	ficant da tructural	mage/de system	terioratio	on to	de de	o, nonstri tailed ev o, no non	uctural ha aluation structura	azards e is not ne Il hazard	xist that cessary Is identifi	may requ	ire mitig	valuated ation, but	
LEVEL 2 SCREENING PERF	ORME	D?	lo d, scr	X Signi the s	ficant da tructural I note th	mage/de system ne follow	terioratio	on to ST = Esti	de de	o, nonstru tailed ev o, no non r unrelia	aluation structura	azards e is not ne Il hazard <u>OR</u>	xist that cessary Is identifi	ed 0 Not Kr	ire mitig	valuated ation, but	

Structure 59, Building 40 Photographs



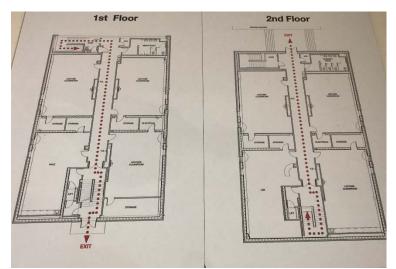
Joints Between Structure 58 and 59



Cracks in Structure, Evidence of Pounding and Deterioration/Settling

рнотс	OGRAPI	н	the second second second			Othe Buil Use Lati Ss: Scre No. Tota	er Identi ding Na : tude: eener(s) Stories: al Floor	Hiple fiers: igh igh 34 : Abov	S (L) S (L) 3556 A e Grade a, ft.):	1001/ 26	Shell Lor S1: Below G	2v ngitude 0.5 Date	: - 37 e/Time:	89.5 6/1 Year	The second s	495	EST
						Occ	itions: upancy:	Indu Utilit	embly istrial ty	Yes, Yea Commercia Office Warehouse	ial En Sc ie Re	her. Serv hool sidentia	I, #Uni	ts:	overnmen	Shelt	er
							Туре:	Hard Rock	Avg Rock	Dense Soil	Stiff Soil	Soft Soil	Po Sc	or <i>If L</i> iil		ıme Type	
				-	-			azards:		tion: Yes/N							
							acency: gularitie	s:	U Ve	ounding ertical (type			ards fro	m Taller	Adjacent	Building	
			-				erior Fal ards:	ling	Ur 🗌	an (type) hbraced Ch arapets	nimneys			vy Clado endages		eavy Ven	ieer
	-					_		_						3			
			+			CO	MMENT					1	. 1		1		
							·C	onl	-, ()	21.11	sck.) t	Col	Um	ins		
			-			-	150	fet	YK	sind he- ling	OW.	S					
							121	HLO	d +	ne-	-don	e.					
				1			N	0.1-	1.714	tin ()	1100	n's	2)				
SKI	тсн									nments on			5				
	and the second diversion of the second	ASIC	SCOR	RE, MO	DIFIER					1 SCOR		paye	-	-			
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2	C3 I (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	SW)	INF) 1.2	1.0	1.2	INF) 0.9	1.1	1.0	1.1	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9 -0.6	-0.9 -0.5	-0.9 -0.5	-0.8	-0.7 -0.4	-0.8 -0.5	-0.7 -0.4	-0.7 -0.3	-0.7 -0.4		2823282	0.7	-0.7	-0.7 -0.4	-0.7 -0.4	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.4	-0.4		2000	0.5	-0.4	-0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code Post-Benchmark	-0.3 1.9	-0.3	-0.3 2.0	-0.3	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2		0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	1.1 0.3	1.1 0.4	1.5	NA 0.2	1.4 0.2	1.7	1 2246	1.5 (0.3	1.7	1.6 0.3	1.6 0.3	NA 0.1	0.5 0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, S _{MIN}	-0.4	-0.4	-0.4	-0.3 0.5	-0.3 0.5	NA 0.5	-0.3	-0.1	-0.1 0.3	-0.3 0.3		NA 0.2	-0.1	-0.2	-0.2 0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	4	and a	≥ 0	-									UIL	0.0	0.0	0.2	1.0
EXTENT OF REVIEW	1	0		OTHER	RHAZ	ARDS			ACT	ION RE	QUIRE	D	*		-		
	/isible	Aeri	ial ered		Structura ding pote ff, if know	I Evalu ntial (ur n)	ation? nless SL2	>		ed Structures, unknownes, score le es, other ha	n FEMA tess than c	ation R building ut-off			uilding		
Contact Person: Donnie	VOCK		-	Fallin buildi	g hazard: ng	s from ta	aller adja	cent	No No								
	1		-	Geold	ogic haza	rds or S	oil Type	F		ed Nonstru							
LEVEL 2 SCREENING PERFORM Yes, Final Level 2 Score, SL2 Nonstructural hazards?	ficant dan tructural s	system			de de	es, nonstruct o, nonstruct tailed evalu o, no nonstr	tural haza uation is r ructural h	irds exis iot nece azards i	st that m ssary dentifie	nay requ	ire mitiga	aluated ation, but	a				
Where information of	annot b	e verifie	d, scre	ener shal	I note the	follow	ing: ES	GT = Esti								-	-
Legend: MRF = Moment-res BR = Braced frame		ne l		inforced cor		1		Unreinfo	rced masc		MH = M	anufactu ght meta	red Hou	sing FI) = Elexibi	e diaphrag diaphragm	gm 1

Structure 60, Building 41 Photographs



Plan View of Floors 1 and 2



12" Thick Concrete Walls and Exposed Concrete Columns, Safety Windows

Level 1 **VERY HIGH Seismicity**

							Add	iress:	250	J	ofta	RAL	\wedge	-+				
								-	b	1 J.	VI	N	-		Zip: 3	206	3	
							Oth	er Ident	tifiers:	Lipic	41	1 -			-ip	000	-	
								Iding Na		PI		117				-	N.C.	-
							Use			-sch	In							
1 S.							Lati	tude: 2	161	136	no li		Longitu	da: =	- 80	550	15:30	
A Contract of the second	РНОТО	GRAP	Н				Ss:	iuue.	534		057		S ₁ : C			122	1200	
	· ·····							eener(s		M			S. (16 1)		-	11		
							-					_		ate/Tim		11		
100 C										ve Grade			w Grade	: 0			19ng	EST
									Area (s			1001			_ Code	e Year:		
							Add	litions:		Ione L] Yes, \		wilt: _					
							Occ	upancy		embly	Comme		Emer. S	ervices	Пн		Shelt	er
										ustrial	Office	and the second s	Schoo			overnmer	nt	
									Utili		Wareho	p10	Station .	itial, #Ui				
			-	-			Soil	Type:	A Hard	B	M					NK	-	_
									Rock	Avg Rock	Den: Soi				oor <i>If</i> Soil	DNK, ass	ume Type	D.
							Geo	logic H	azards:	Liquefac	tion: Yes		in the second seco			Surf. R	int : Yes/	No/DNK
				7			************	acency:			ounding						t Building	
							-	gularitie							eve)			
			7				ine	guiaritit			an (type)	heisenei	ia) of	-111	000/	mol		
							Evt	erior Fa	Ilina		nbraced							
	_	_			_			ards:	ning		arapets	Chimney	S		oendages		eavy Ver	neer
															Jenuages	5		
							CO	MMENT	TS:									-
								, 0.	alm	for c	od	Mr.						
				-			-	R	311 ,	COLC	X	1.100	207	VYY		^		
							-	- []	1	11	10	.110	1	Pn'	rm	t,		
		_					2	1-10	1Ch	ple	Y	JAD	VI	0	100	1		
	SKI	TCH	_					Addition	al sketch	les or con	nments o	on separa	ate page					
		В	ASIC	sco	RE, MO	DIFIER	RS, A	ND FI	NAL L	EVEL	I SCO	RE, S	L1					
FEMA BUILDING TYPE	Do Not	W1	W1A	W2	S1	S2	S3	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
	Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score		2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	(1)	1.1	0.9	1.1
Severe Vertical Irregularity, VL1		-0.9	-0.9	-0.9		-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Moderate Vertical Irregularity, Vi Plan Irregularity, PL1	1	-0.6	-0.5	-0.5	1000	-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code		-0.7	-0.7	-0.6	-0.5	-0.5 -0.2	-0.6 -0.3	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark		1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	-0.1	-0.2 1.7	0.0 NA	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B		0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	1.6	NA 0.1	0.5
Soil Type E (1-3 stories)		0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.1	-0.1
Soil Type E (> 3 stories)	-	-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, S _{MIN}		0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE,	SL1 ≥ SMIN:	i	0,5	PC).3													
EXTENT OF REVIEW	1			T	100000000000000000000000000000000000000					1.0-		FOUNT					-	
				lai	OTHER					100 million and	ION R							
			Aer		Are Then Detailed	e Hazard	s That	i rigger /	A		ed Struc							
Drawings Reviewed: 🗌 Ye				5100	Poun					Ye	es, unkno	wn FEM	A buildir	ng type o	r other b	uilding		
Soil Type Source:					cut-o	ff, if know	nual (ur /n)	11855 OL2	-		es, score es, other							
Geologic Hazards Source:		-			Fallin	ng hazard	s from ta	aller adja	acent			nazarus	present					
Contact Person: Do	building									1000		tructura	I Evalua	tion Rec	ommen	ded? (ch	eck onel	
LEVEL 2 SCREENING	G PERFO	ORME	D?		Geol	ogic haza ficant dar	rds or S	ioil Type	F						I that sho			
Yes, Final Level 2 Score,			DI N			tructural s		nenoratio	511 (0		, nonstru	uctural h	azards e	xist that	may real	lire mitia	ation, but	а
	Yes						Joronn			de	tailed ev	aluation	is not ne	cessary			and a set	-
	and California			10.000							o, no non					DNK		
Where in	formation o	annot b	e verifie									ble data	OR	DNK = D	o Not Kr	wor	-	
Legend: MRF = BR = E	Moment-res Braced frame	sting fran	ne		einforced con near wall	ncrete	1	URM INF TU = Tilt u	= Unreinfo	orced masc	nry infill	MH	= Manufa	ctured Ho	using F	D = Flexib	le diaphrag diaphragm	gm
BIT	and in this				NGUI WOII			mil	ψ			LM :	= Light me	atal	R	U = Rigid	diaphragm	1

Structure 61, Building 42 Photographs



Exterior



Interior, Split Level

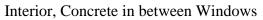
					1	Add	ress	250	T	effer	Sala	<4					
						1		Ric	62	TN	July 1	51		in: 😤	8063		
						Oth	er Identi	fiers:	62	1113				. <u>0</u>	0.00	5	
						Buil	ding Na	me:									1000
Sec. 1 (Use	:	H) ql	nsu	hool							
						1.000	tude:	35	,731	04	Lo	ongitu	de:	1,08	5386	63	
РНОТ	OGRAP	н				Ss:	-	34		_	S1	: <u>C</u>	1.23	1			
							eener(s)						ate/Time	-1			
									e Grade		Below		: 0	· · · · · · · · · · · · · · · · · · ·		20040	I EST
							al Floor . litions:	Area (so		39] Yes, Yes				Code	Year:		
							upancy		embly	Commerci			ervices	Пні	atoria	Shelte	
							upuncy.		ustrial	Office Warehous	S	choot		G	overnmen		81
			-			Soil	Type:	A Hard	B Avg	Dense		f S	E Coft Po	or If	NK DNK, assi	ıme Type	D.
		1				Geo		Rock	Rock	Soil tion: Yes/N	Soil		Soil So		0.40	1. 1. 0	-
			-				acency:	azaius.		ounding			lazards fro				NO/DNK
				7			gularitie	s:	Ve	ertical (type an (type)				and the second second second	1/m		
							erior Fal	ling	🗌 Ur	hbraced Ch	himneys					eavy Ven	eer
							ards:			arapets her:			🗆 Арри	endages	•		
			-			co	MMENT	S:	0								
		-				-	. 0	anc	, tr	rome JANS	5 JN	NAS	son	Y	n+0	NOV	
						-	1 /	200	c.h	JANS	>			/			
						-		1.1 1		0			1 1	11			1.1
			-	_		_	"Sp	141	6261	(0)	dan	10	10-1	040	V		
		_				_	4				0.				1		CL.
SK	ETCH						Additiona	al sketch	es or con	nments on	separate	e page					
	B	ASIC	sco	RE, MO	DIFIEF	11.00				SCOR	Contraction of the local division of the loc	The second s					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9	5.1	-0.7 -0.4	-0.8 -0.5	-0.7	-0.7	-0.7 -0.4	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6		-0.5	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4 -0.4	-0.4	-0.3 -0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark Soil Type A or B	1.9 0.5	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	0.5	0.4	0.3	0.3	0.4 -0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.2	-0.1	NA	-0.1	-0.2 -0.2	-0.2	0.0	-0.1 NA
Minimum Score, S _{MIN}	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	: 2	.3E	0.	2													
EXTENT OF REVIEW				OTHER	RHAZ	ARDS			ACT	ION RE	QUIRE	ED					
	All Sides			Are Ther				1	Detaile	ed Structu	ral Evalu	uation	Required	d?			
Interior: Interi	Visible	K Ent	ered	Detailed					1 Ye	es, unknow	n FEMA	buildir	ng type or	other bu	uilding		
Soil Type Source:					ding pote ff, if know		nless SL2	>	1 Ye	es, score le	ess than o	cut-off					1.1
Geologic Hazards Source:					ig hazard		aller adja	cent	Ve Ve No	es, other ha	azaros pr	resent					
Contact Person: Donnie	ontact Person: Vonnie Vork building									ed Nonstru	uctural E	Evalua	tion Reco	ommen	ded? (ch	eck onel	
LEVEL 2 SCREENING PERF	LEVEL 2 SCREENING PERFORMED?									es, nonstru	ctural ha	zards	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2			0	the s	tructural s	ystem			No.	o, nonstruc	tural haz	zards e	exist that n	nay requ	ire mitiga	ation, but	a
Nonstructural hazards? Yes			S							tailed evalu o, no nonst	uation is	not ne	cessary	d b	T DNK		
Where information	cannot b	e verifie	d, scr	eener sha	I note the	follow	ing: ES	T = Esti								-	
Legend: MRF = Moment-re BR = Braced frame	sisting fran	10	RC = Re	einforced co hear wall		l		= Unreinfo	rced maso		MH = 1	M. Comments	ctured Hou			e diaphrag	m

Structure 62, Building 43 Photographs



Exterior

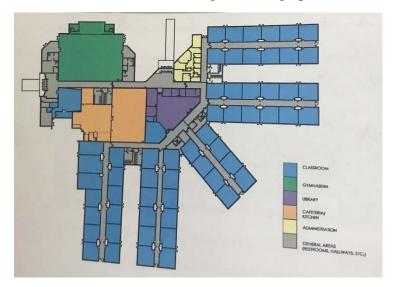






Interior, Cracks

							-	30 C Rip ifiers:	Kev.	nmile	's C	ig	45 0	st. Zip: 3	806	3	
						Buil	ding Na	me:		5.1	1	185					
						Use		Mide	110728	JUL				×a	eer	000	~
PHOT	OGRAP	н				Ss:			f L C	693		Longitu S₁: \	ide:	-89,	>23	2281	>
	ooru						ener(s)	A .	M				ate/Tim		-		
									e Grade	. 1	Rolov	w Grade		-	Duille	9870	7 507
						Tota	al Floor	Area (so	q. ft.): _	106		6			Year:	10 +1	_ ESI
						Occ	upancy		embly Istrial ty	Comme Office Wareho		Emer. S School Residen			storic overnmer	Shelt nt	er
						Soil	Туре:	Hard Rock	Avg Rock	Den	se St	D C	E		NK DNK, ass	ume Type	D.
	/					Geo	logic Ha	COLUMN TWO IS NOT THE OWNER.						/No/DNK	Surf. Ru	upt.: Yes/	No/DNK
						********	acency:			ounding				om Taller			
	E	-			_	Irreg	gularitie	s:	Ve Ve	ertical (ty an (type	pe/sever	ity) SP	title	vel/	mod		
							erior Fal ards:	ling	🗌 Pa	arapets	Chimney		Hea	avy Clado pendages	ding or H		neer
	1					CO	MMENT	S:	0	ther:		-	_	-			-
									cu Y	nin	C	in al					
	/					-	fle	.X.	ryst		101	n.v					
SK	ETCH	1 1					Addition	al sketch	es or con	nments o	on separa	ate page					
	B	ASIC	SCOR	RE, MO	DIFIER	RS, AI	ND FIN	AL LI	EVEL	1 SCO	RE, S	L1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1	-0.9	1.9 -0.9	1.8 -0.9	1.5 -0.8	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9	-0.8	-0.7 -0.4	-0.8 -0.5	-0.7	-0.7 -0.3	-0.7	-0.8 -0.4	-0.6 -0.3	-0.7	-0.7	-0.7	-0.7 -0.4	-0.6 -0.3	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	-0.3	-0.3	-0.3	-0.3	-0.2 1.1	-0.3 1.1	-0.2	-0.1 NA	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	1.7 0.3	NA 0.1	1.5 0.3	1.7	1.6	1.6	NA 0.1	0.5 0.1
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Soil Type E (> 3 stories) Minimum Score, Smin	-0.4	-0.4	-0.4	-0.3	-0.3 0.5	NA 0.5	-0.3	-0.1 0.5	-0.1 0.3	-0.3 0.3	-0.1 0.3	NA 0.2	-0.1	-0.2 0.3	-0.2	0.0	NA
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN		600			0.1	20,	3)	0.0	0.5	0.5	0.5	0.2	0.2	0.3	0.3	0.2	1.0
EXTENT OF REVIEW		\sim		OTHER	RHAZ	ARDS			ACT	ION R	EQUIF	RED					-
		Aer	ial	Are Ther	e Hazard	s That 1	Frigger A	١	Detaile	ed Struc	tural Eva	aluation	Require	ed?			1
Drawings Reviewed: X Yes Soil Type Source:	Visible No	🖾 Ent	ered		ding pote	ential (ur		>	🛛 Ye	es, score	less than	n cut-off		r other bu	uilding		
Geologic Hazards Source:	eologic Hazards Source:									es, other)	hazards	present					
2000 AL	contact Person: Donce York building									ed Nons	tructural	Evalua	tion Rec	ommend	ded? (ch	eck one)	
	LEVEL 2 SCREENING PERFORMED?									es, nonst	ructural h	nazards i	identified	that sho	uld be ev	aluated	411
Yes, Final Level 2 Score, SL2	tructural s					o, nonstr tailed ev	uctural ha	azards e is not ne	xist that	may requ	ire mitiga	ation, but	а				
Nonstructural hazards? Ves		_				o, no nor	structura	l hazard	s identifi		DNK						
Where information																	
Legend: MRF = Moment-res BR = Braced frame	isting fran		RC = Re SW = Sh	nforced cor ear wall	ncrete		JRM INF = TU = Tilt u		rced masc	onry infill	MH =	= Manufa = Light me	ctured Ho etal	using FI RI	D = Flexib D = Rigid	le diaphrag diaphragm	gm



Structure 63, Building 44 Photographs

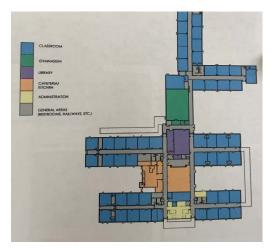
Plan View



Interior, Split Level

					1	Add	lress: _	601	115,7	mme	en s	St.	7	ip: 3	804	D	
						Oth	er Identi			19		100		.ip:	007	0	
							ding Na	me:			-						
24 T 4 A 1323						Use	: E	-Len	nen	tory	SCF			00		-	
DUCT						100000	tude:	\$5.8		508				89,	404	12:49	5
PHOTO	OGRAP	н				Ss:	1,	143			8		2.62			_	
							eener(s):			-			ate/Time		1000	075	
						Tota	Stories: al Floor / litions:			6 Yes, Y	T, qL	v Grade	1991	Code	Built: Year:	1978 0	EST
							upancy:		embly strial	Commer Office Warehou	rcial	Emer. S		His Go	storic overnmen	Shelte	er
	-	-				Soil	Туре:	A Hard	B Avg	Dens	se St	iff S	oft Pe	oor If L	NK DNK, assi	ume Type	D.
[] this form						Geo	logic Ha	Rock	Rock Liquefac	Soi tion: Yes				oil /No/DNK	Surf R	int: Yes/	No/DNK
	1	ddifi		1			acency:			ounding				om Taller			
Dother form	04	aditi	on	1			gularitie	s:	🗹 Ve	ertical (typan (type)	pe/severi	ity) S	plit	leve t cor	1/m		
	_			-			erior Fall ards:	ling	Ur	nbraced (arapets	-		Hea	avy Cladd bendages	ing or H	eavy Ven	ieer
		- AND	1			CO	MMENT	S:	-								
Origi	nai	•					•To	ir t	, gra	avel	100	,f					
		a la sul															
	10.1			30													
Carl and Carl Street	24-127		Sec.														
SK	ETCH						Additiona	al skotob		amonto a							
		ASIC	sco	RE, MO	DIFIER							the second s	-	-			-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	SW)	INF) 1.2	1.0	1.2	INF) 0.9	1.1	1.0	(1.1)	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9		-0.7 -0.4	-0.8 -0.5	-0.7	-0.7 -0.3	-0.7 -0.4	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.5	-0.5	6 N N N N N N N N N N N N N N N N N N N	-0.4	-0.5	-0.4	-0.3	-0.4	-0.4 -0.5	-0.3 -0.3	-0.4	-0.4	(0.4) (4)	-0.4 -0.4	-0.3 -0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3	201 - Control - 100	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	6.2	-0.4	0.0	0.0
Post-Benchmark	1.9	1.9	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type A or B Soil Type E (1-3 stories)	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	0.0	-0.2	-0.4	1000	-0.2 -0.3	-0.2 NA	-0.2	-0.1 -0.1	-0.1 -0.1	-0.2 -0.3	0.0	-0.2 NA	-0.1	-0.2	-0.2 -0.2	0.0	-0.1
Minimum Score, S _{MIN}	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0.	15	Q.3)													
EXTENT OF REVIEW				OTHE	RHAZ	ARDS	3		ACT	ION R	EQUIF	RED					
		Aer		Are Ther					Detaile	ed Struc	tural Eva	aluation	Require	ed?			
Interior: 🚺 None 🗌 Drawings Reviewed: 🔀 Yes		Enter Enter	ered	Detailed					Ye	es, unkno	own FEM	A buildir	ng type o	r other bu	uilding		
Soil Type Source:				Pour cut-o			nless SL2	>	Ye Ye	es, score	less that	n cut-off					
Geologic Hazards Source:	Geologic Hazards Source:									es, other	nazaros	present					
Contact Person: Donnie	Contact Person: Dannie, Vor K building										tructural	l Evalua	tion Rec	ommend	led? (ch	eck one)	
LEVEL 2 SCREENING PERF	ORME	D?		Geol	ogic haza	rds or S	Soil Type eterioratio	F n to	🗆 Ye	es, nonst	ructural h	hazards	identified	I that sho	uld be ev	valuated	
Yes, Final Level 2 Score, SL2										o, nonstru	uctural ha	azards e	exist that	may requ	ire mitig	ation, but	ta
Nonstructural hazards? Ves									de	tailed ev	aluation						
	cannot H		ю			e follor	vina. Ed	T = Eat	de No	tailed ev o, no non	aluation structura	al hazard	ls identifi	ed D	DNK		

Structure 64, Building 45 Photographs



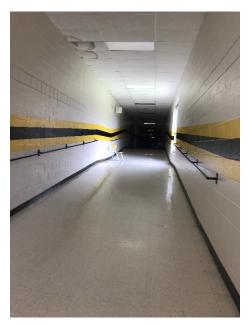
Plan View



Interior

		-	-		-	-			-	-							-
						Add	ress: _	601	Car	mer	1 St				2011	-	
								FIGI	SOT	N	-		Z	lip: 3	8041	5	
								fiers: (00					-	-		
						Use	ding Na		lenta	NI C	1.1.0	-1		1250 1128	-		
							tude:	25 4	882	771			10:	89,	LINE	700-	2
PHOT	OGRAP	н				Ss:	1.	793	200	161			0.67		10 .	501.	٢
						122	ener(s)					10.00	ate/Time		11		-
						No	Stories:	Abov	e Grade:	1	Below	Grade	Contractoria de la contractoria de		0.00	1996	T EST
							0.000	Area (so		27		oraue.	0	-	Year:	THOL	
							itions:	N		Yes, Y		uilt:	998	-			
						Occ	upancy	Asse	embly	Commer	cial	Emer. Se	ervices	🗆 Hi	storic	Shelt	er
									strial	Office		School		100	overnmen	t	
								Utilit		Warehou		Resident					
	No. In	-	-	-		Soil	Туре:	Hard	Avg	Dens			The fait		NK assi	ume Type	D
- Duc Como	10-1-1	10.1				-		Rock	Rock	Soil	Sc	oil S	oil S	Soil			
El this form		L		_		Geo	logic Ha	azards:	Liquefac	tion: Yes	No/DNK	Lands	ide: Yes	/No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
FIDD OV Arma	Add	ition				Adja	acency:		Po	unding	F F	alling Ha	azards fr	om Taller	Adjacent	t Building	
Lound iam			and I			Irreg	gularitie	s:		rtical (typ an (type)				nd s		modi	
	1			1		1.111	erior Fal ards:	ling		braced C rapets	chimney	S		avy Clado bendages		eavy Ven	neer
						CO	MMENT	S:				-					
origit	al				00:	nfa	red	m	San	()							
o.J.							pe.	1110	red	1.0	1 100	`γ					
						1	M	Aal	noo	f de	20K						
	-								evel				cal i	rrog	Vlor	(1)	
							SP	1171	eve	mo	00 (1	CIT	can	i. iej		rip	
SK	ETCH						Addition	al alcatab									
		ASIC	sco	RE, MO	DIFIE	and the second second	and and and and and		es or com					-	-	-	-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	\$3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2	C3	PC1	PC2	RM1	RM2	URM	MH
	24	40	4.0				ŚW)	INF)		(SW)	(URM INF)	(TU)		(FD)	(RD)		
Basic Score Severe Vertical Irregularity, VLt	2.1 -0.9	1.9 -0.9	-0.9	-0.8	1.4 -0.7	1.6 -0.8	-0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	-0.7	-0.7	-0.7	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.7	-0.7	-0.7	-0.6 -0.3	NA NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	14-11-14-14-14-14-14-14-14-14-14-14-14-1	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Post-Benchmark	1.9	1.9	2.0	2.24	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type A or B Soil Type E (1-3 stories)	0.5	0.5	0.4	-0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	10-17-10-1	-0.2	-0.2 NA	-0.2	-0.1 -0.1	-0.1	-0.2 -0.3	0.0 -0.1	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, SMIN	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	-0.2	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$	1.	qZ	0.3	5													
EXTENT OF REVIEW				OTHE	RHAZ	ARDS			ACT	ON R	EQUIF	RED					
	All Sides			Are Ther				A	Detaile	d Struct	ural Eva	aluation	Require	ed?			
	Visible No	Ent Ent	ered	Detailed										or other bi	uilding		
Soil Type Source:	140			Pour			nless SL2	>		s, score							
Geologic Hazards Source:	Cut-of									es, other l	hazards	present					
Contact Person: Donnie	ng hazard ing	is nom ti	aller adja	icent			nueture	Evelue	tion Dr.		4-40 (a al a a					
	ogic haza	ards or S	Soil Type	F						comment that sho							
	ficant dan tructural	mage/de	eterioratio	on to		o, nonstru	ictural h	azards e	xist that	may requ	uia de el	ation but	ta				
									de	tailed eva	aluation i	is not ne	cessary	1	1		
								-		o, no non					DNK		
Where information																	2162
Legend: MRF = Moment-res BR = Braced frame	asung fram	ne	KU = R	einforced co hear wall	ncrete		URM INF TU = Tilt u		prced maso	nry infill		= Manufa = Light me		ousing F	D = Flexib	le diaphra diaphragn	gm

Structure 65, Building 45 Photographs



Interior, Sloping Site



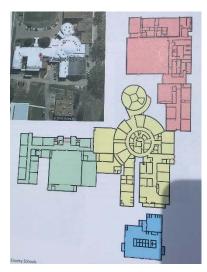
Interior, Gymnasium, Flexible Diaphragm Roof

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

						Add	ress: _	And in case of the local division of the loc	W. S.TN		gre tt	St	7	ip: 31	2040)	
						Oth	er Identi			the	D (.	6		.ip. <u>51</u>	0010	,	
							ding Na	me:	P		er o	0					
									e sc								
						198	tude:	55.8	79	895				89,4	038	327	
РНОТС	GRAP	4				Ss:	17		M	1.121	\$		161			-	
							eener(s)						ate/Time	e:			
									e Grade			Grade	: 0	-		9970	EST
								Area (so	-		190			Code	Year:	ar	
							litions:			Yes, Y		Service instances	967		10	~	
					•	Ucc	upancy		embly ustrial ty	Commen Office Warehou		School Residen	ervices tial, #Ur		storic overnmer	Shelt Shelt	er
			4			Soil	Type:	A Hard	B Avg	Dens	e St	iff S	oft P	oor If	NK DNK, assi	ume Type	D.
Dthis form						Geo	logic H	Rock	Rock	Soil tion: Yes			7	oil /No/DNK	Surf D		
	-	-	71			annon ment	acency:	the Residence of the Party of t		ounding						t Building	
[10ther form	$(\)$	ζŗ		7			gularitie		Ø Ve	ertical (typ an (type)	e/severi	ty) Sla	pesit	grad	split		
	1.	1	7			Exte	erior Fal	ling		nbraced C						eavy Ver	leer
	>	5	V				ards:		🗆 Pa	arapets ther:				pendages		cavy ver	ICCI
	_		-	Π		CO	MMENT	S:									
							00:	ofa	ro A	Mas	ionr	V					
and the state of the	Г	1											0				
					1		· TP	100	last	12.21	RXib	le r	004				
te de la																	
	U		_														
SK	тсн						Addition	al skotsh		nments o							
		ASIC	sco	RE, MO	DIFIE											-	-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	D	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9 -0.6	-0.9 -0.5	-0.9		-0.7 -0.4	-0.8	-0.7	-0.7 -0.3	-0.7 -0.4	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7 -0.4	-0.7	-0.7	-0.6	NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.4	-0.4	-0.4	-0.3	-0.4	-0.4	8	-0.4	-0.3	NA NA
Pre-Code	-0.3	-0.3	-0.3	-0.3	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	02	-0.2	0.0	0.0
Post-Benchmark Soil Type A or B	1.9 0.5	1.9 0.5	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	0.2	0.2	0.3	0.1	0.3 -0.2	0.2	0.3	0.3	0.1	0.1 -0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, Smin	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	0	131	Q.3)					-	-							
EXTENT OF REVIEW				OTHE	RHAZ	ARDS			ACT	ION RE	QUIR	ED					
	All Sides			Are Ther				4		ed Struct							
	/isible No	ELEN	ered	Detailed					Ye Ye	es, unkno	wn FEM	A buildin	ng type o	r other bu	uilding		
Soil Type Source:	ff, if know	vn)			A Ye	es, score l es, other h	less than hazards	i cut-off present									
Geologic Hazards Source: Contact Person: Dococe Wo	is from ta	aller adja	cent		0												
1200 Mile Vo	ards or S	oil Type	F		ed Nonst												
LEVEL 2 SCREENING PERFORMED?							terioratio	on to		es, nonstru	uctural h	azards i	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2		M N	2 C C C C C C C C C C C C C C C C C C C	the s	tructural	system			de	o, nonstru tailed eva	aluation i	s not ne	cessary		lire mitiga	ation, but	а
Nonstructural hazards? Yes										o, no nons	structura	I hazard	s identifi		DNK		
Where information of											ble data	OR I	DNK = D	o Not Kr	ow		
Legend: MRF = Moment-res	sting fram			einforced co hear wall	ncrete		JRM INF : TU = Tilt u		orced maso	onry infill		= Manufa = Light me	ctured Ho	using Fl	D = Flexib	le diaphrag	gm

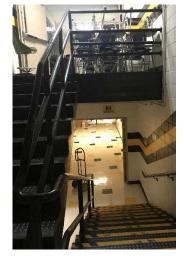
Structure 66, Building 46 Photographs



Structure 66 is Green Portion



Interior, Evidence of Split Level

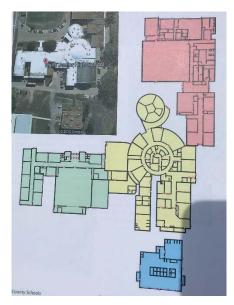




Exterior

						Othe	er Identi ding Na	fiers: _ me:			grett	St	2	Zip:	380	10	
PHOT	OGRAP	н				Use: Latit Ss:	tude: 3	35,8	icho 1799	167			de: - 0.67	7,08	P96	95	
						Scre	eener(s)	:(M			Da	ate/Tim	e: 61	11		
				I		Tota Add	Stories: Il Floor itions: upancy:	Area (so		G	ear(s) Br	uilt:	4605	Code	Year:	996	
						-		Utilii		Wareho	use	Residen	tial, #Ur				
							Туре:	Hard Rock	Avg Rock	Den: Soi	se St I Sc	iff S bil S	oft P oil S	oor If i Soil		ume Type	
this torm	4	-	- +			**********		azards:						/No/DNK			
I otherform	0	2		-			acency: jularitie	s:NA	Vel Ve		pe/severi	ty) 🤏	NG (1)	om Taller	200	8	
	1	2	5				erior Fal ards:	ling		nbraced arapets	Chimney:		He	×γ5 avy Clado pendages	ling or H		
	_		1			CO	MMENT	S:	0								
	AL.	20131					RI	10	Aspl . W	alt	fle	xibl	en	foc			
	and and		K				h		- T			,					
			Contraction of the second			,	ke	11/11	, w	uauson	(vr y						
SK	ЕТСН	1200					Addition	ol eksteb									
		ASIC	SCOP	RE, MO	DIFIEF				es or cor	and the second se	the same the share the same	Contract of the second second second					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8 -0.9	1.5 -0.8	1.4 -0.7	1.6 -0.8	1.4	1.2 -0.7	1.0	1.2	0.9	1.1	1.0	11	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	-0.4	-0.7	-0.8	-0.7 -0.4	-0.7	-0.7 -0.4	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7	-0.7 -0.4	-0.6	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.2	-0.4	-0.3	NA
Post-Benchmark	-0.3	-0.3 1.9	-0.3	-0.3	-0.2	-0.3 1.1	-0.2	-0.1 NA	-0.1	-0.2 1.7	0.0 NA	-0.2 1.5	-0.1	-0.2	-0.2 1.6	0.0 NA	0.0 0.5
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2 NA	-0.2	-0.1	-0.1	-0.2 -0.3	0.0 -0.1	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin					0.5	0.5		-0.1	-0.1			NA	-0.1	-0.2	-0.2	0.0	NA
	0.Z	Q.7	0.7	0.5	0.0	0.0	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.0	0.3		1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	1	.5 2		3	0.0	0.0	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.5	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$: EXTENT OF REVIEW	1		0	A DESCRIPTION OF THE OWNER.				0.5			0.3		0.2	0.5	0.3	0.2	1.0
EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source:	1	5) =	ial	CTHEF Are There Detailed	R HAZA Hazard Structura ding pote	ARDS s That 1 al Evalu ential (un n)	Trigger A ation? Iless SL2	4	ACT Detaile	ON R ed Struc es, unkno es, score es, other	EQUIF tural Eva	RED aluation A buildir n cut-off	Require			0.2	1.0
EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	All Sides Visible No	Aeri	ial	OTHEF Are There Detailed Poun cut-ol Fallin	R HAZ/ Hazard Structura ding pote ff, if know g hazard	ARDS s That 1 al Evalu ential (un n)	Trigger A ation? Iless SL2	4	ACT Detaile Ye Ye No	ON R ed Struc es, unkno es, score es, other	EQUIR tural Eva own FEM less thar hazards	RED aluation A buildin n cut-off present	Require	ed? or other bu	uilding		
EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Doc 0.2 LEVEL 2 SCREENING PERFORMED Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes	All Sides Visible No	□ Aeri Ø Ente D? N N	ial ered o	Are Therr Detailed Poun cut-oi Fallin buildi Geold Signit the st	R HAZ/ a Hazard Structura ding pote f, if know g hazard ng ogic haza iicant dan ructural s	ARDS s That T al Evalu ential (un m) s from ta rds or S mage/de system	Frigger A ation? aless SL2 aller adja oil Type terioratio	A cent F n to	ACT Detaile	ION R ed Struc es, unkno es, score es, other o ed Nons es, nonstru tailed ev o, no non	EQUIF tural Eva wm FEM less thar hazards tructural ructural h uctural ha aluation i structura	RED aluation A buildir present Evalua hazards i azards e s not ne I hazard	Require og type o tion Rec identifieo xist that cessary s identifi	ed? or other bu commence d that sho may requ ied 5	uilding ded? (ch uld be ev ire mitig:	eck one)	
EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: Donce LEVEL 2 SCREENING PERFO	All Sides Visible No Vor	D?	ial ered o o d, scre	Are Therr Detailed Poun cut-oi Fallin buildi Geold Signit the st	R HAZ/ e Hazard Structura ding pote ff, if know g hazard ng gic haza icant dan ructural s	ARDS s That T al Evaluential (un m) s from ta rds or S mage/de system e follow	Frigger A ation? alless SL2 aller adja oil Type terioratio	A cent F in to 67 = Esti	ACT Detaile	ION R ed Struc es, unkno es, score es, other es, nonstru- tailed ev o, no non r unrelia	EQUIR tural Eva own FEM less thar hazards tructural h actural ha aluation i structura ble data	RED aluation A buildir n cut-off present Evalua azards i azards e s not ne I hazard	Require og type o tion Rec identifieo xist that cessary s identifi	ed? or other bu d that sho may requ ied 5 Do Not Kr	uilding ded? (ch uld be ev ire mitig: Q DNK	eck one)	а

Structure 67, Building 46 Photographs



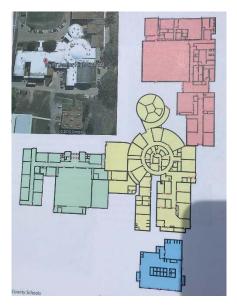
Structure 67 is Yellow Portion



Exterior

РНОТС	OGRAPI	Н				Othe Buil Use Latin Ss:	er Identi ding Na : tude:	ifiers: ime: igh 35,8 735	501			Longitu		89,u 7		10	
						No. Tota	ener(s) Stories: al Floor litions:	Abov	ve Grade q. ft.):	Yes,	524	w Grade	ate/Tim	Year	Built: Year:	1996 1] EST
				J			upancy	Indu Utili		Comme Office Wareho	use		tial, #Ur		storic overnmer	C Shelt It	er
			ないない				Type:	Hard Rock	Avg Rock	Den So	se Si I Si	tiff S oil S	oft P oil S	oor If i Soil		ume Type	
LITHS FORM	1.5		ALC: L											/No/DNK			
Dithis form	~	5		1			acency: gularitie		🖄 Ve	ounding ertical (ty	pe/sever	ity) S	pict	om Taller	Adjacen	t Building	
	(5	1							an (type)		-en			mer		
	>	4	F				erior Fal ards:	lling		nbraced arapets ther:	Chimney	S		avy Clado pendages		eavy Ver	ieer
	4			T		CO	MMENT	s:			onr	V			And a part of the second		
				-		(fler	(ib)	W le (5yn	^	U					
SKE	тсн								es or cor								
				RE, MO				1									
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8 -0.9	1.5 -0.8	1.4 -0.7	1.6 -0.8	-0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	1.0 -0.7	(1.1)	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	-0.4	-0.4	-0.5	-0.4	-0.3	-0.4	-0.8	-0.0	-0.7	-0.7	-0.7	-0.7	-0.6 -0.3	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6	-0.5	• -0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	-0.3 1.9	-0.3 1.9	-0.3 2.0	-0.3	-0.2 1.1	-0.3 1.1	-0.2	-0.1 NA	-0.1	-0.2	0.0 NA	-0.2 1.5	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	1.7	0.3	1.6 0.3	NA 0.1	0.5 0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0 -0.4	-0.2 -0.4	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, SMIN	0.4	0.7	-0.4	-0.3	-0.3 0.5	0.5	-0.3 0.5	-0.1 0.5	-0.1	-0.3	-0.1 0.3	NA 0.2	-0.1	-0.2	-0.2 0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	1	93	0	,3					1 0.0	0.0	0.0	0.2	0.2	0.0	0.5	0.2	1.0
Interior: None 🗌 \	All Sides /isible No	Aeri	ered		e Hazard Structura ding pote	s That T al Evalu ential (un m)	Trigger A ation? Iless SL2	>	Detaile Ve Ve Ve	es, score es, other	tural Eva own FEM less that	aluation A buildin n cut-off		ed? r other bu	uilding		
Contact Person: Donnie vo	rk		-	Fallin buildi	g hazard ng	s nom ta	aller adja	cent	Detail		land a state of the state of th						1.31
LEVEL 2 SCREENING PERFO Yes, Final Level 2 Score, SL2 Nonstructural hazards?	ORMEI		0	Geolo Signif the st	ogic haza ficant dar ructural s	ards or Soil Type F Detailed Nonstructural Evaluation Recommended? (check one) mage/deterioration to Yes, nonstructural hazards identified that should be evaluated No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary No, no nonstructural hazards identified No, no nonstructural hazards identified No, no nonstructural hazards identified No										0.100	
Where information c Legend: MRF = Moment-resi BR = Braced frame		ie F	RC = Re	ener shall inforced cor		l		= Unreinfo	imated o prced masc		MH	OR L = Manufac = Light me	ctured Ho	using FI) = Flexibl	e diaphrai diaphragm	gm

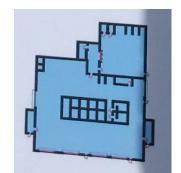
Structure 68, Building 46 Photographs



Structure 68 is Red Portion

						Add	lress: _	880 H (JK Ms,	TN	igre	H 5	5 7	Zip: 3	804	10	ity
						Oth	er Ident	ifiers:	69	-		_					
							ding Na		1 Sch	0001							
PHOTO	OGRAP	u				Lati	tude:	351	979		ا مۇ	Longitu S1: 0	de:	89.	405	175	-
FNOIC	JGRAP	n				Ss:	eener(s)		N		······ ·		ate/Tim		/11		
									ve Grade	2	Belov	w Grade			Built:	1977	T EST
						Tota	al Floor	Area (se		1	2-91	15			Year:	1177	2 231
						Occ	upancy		embly ustrial ty	Comme Office Wareho	(Emer. S School Residen	ervices itial, #Ur		storic overnmer	C Shelt	er
	-					Soil	Type:	Hard Rock	B Avg Rock	Den So	se St	tiff S	oft P		NK DNK, ass	ume Type	D.
						Geo	logic Ha	**********							Surf. Ru	upt.: Yes/I	No/DNK
		_				Adj	acency:		the second	ounding						t Building	-
Hiche	r	foc	_	-		Irre	gularitie	s:		ertical (ty an (type)	pe/sever	ity)Sp_	111	cvel,	mod	1	
Highe	eigr	4					erior Fal ards:	ling		arapets	Chimney	'S		avy Clado pendages		eavy Ven	ieer
Lover L						CO	MMENT	S:	000	0.1	11		- 81	9.40	45	91	
root			_			11	-at:	35	1880	200	TL	sud:	v	1115	13	11	
height		•					TPO	(f)*	arx;	le)r	`æf			9,40			
							tar	f dr	navel	3-	Ply !	rad					
						1.	ZM	1									
SKI	тсн								es or cor								
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO	S2	S3	ND FIN	S5	EVEL ·		RE, S	L1 PC1	000				
Клож				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8	1.5 -0.8	1.4 -0.7	1.6 -0.8	1.4 -0.7	1.2 -0.7	1.0 -0.7	1.2	0.9	1.1	1.0	0	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5	-0.4	-0.4	-0.5	-0.7	-0.7	-0.7	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7 -0.4	-0.7	-0.7 -0.4	-0.6 -0.3	NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6	10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.5 -0.2	-0.6 -0.3	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	1.0	-0.2	-0.5	-0.2	-0.1 NA	-0.1	-0.2	0.0 NA	-0.2	-0.1	-0.2	-0.2 1.6	0.0 NA	0.0 0.5
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.5
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0 -0.4	-0.2	-0.4	-0.3	-0.2 -0.3	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7	0.5	0.5	NA 0.5	-0.3 0.5	-0.1 0.5	-0.1	-0.3	-0.1	NA 0.2	-0.1	-0.2	-0.2 0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0	,5)3	0.	3			de recención de la compañía de la co		1					0.0	0.0	0.2	1.0
EXTENT OF REVIEW				OTHER	R HAZ	ARDS			ACT	ION R	EQUIF	RED					
		Aer		Are There				1	Detail	ed Struc	tural Eva	aluation	Require	ed?			
Interior: Interi								>	🚺 Ye	es, score	less that	n cut-off		r other bu	uilding		
Geologic Hazards Source: Contact Person:	ant	,		Fallin	g hazard		aller adja	cent			hazards	present					
1	Geologic haza							F						ommend			
LEVEL 2 SCREENING PERFO	DRME	/	-	Signit	ficant dar	nage/de	terioratio	n to		es, nonst	ructural h	nazards i	dentified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2 Nonstructural hazards? Yes			0		ructural s					tailed ev o, no nor	aluation i structura	is not ne Il hazard	cessary s identifi	ed 🖻	DNK	ation, but	а
Where information of	annot b	e verifie	d, scre	ener shal	note th	e follow	ing: ES	T = Esti									
Legend: MRF = Moment-resi			Sold States				and a short			, ann onu	Die uata	Un		O NOL AL	IOW		

Structure 69, Building 47 Photographs



Plan View



Exterior



Interior, Split Level

PHOTO		Oth Bui Use Lati Ss: Scr No. Tot: Add	eener(s Stories	Tr ifiers: ame: 3G 3C 3C 3C 3C 3C 3C 3C 3C 3C 3C	SUN 343 Ve Grade q. ft.): lone p embly istrial	188 881 1900	Belov Year(s) B ercial puse C	D w Grade built: Emer. S School Resider	de: ate/Time : : : : : tital, #Ur]E	2: <u>5</u> Yea Code □ H □ G wits:]F D	St St Year: storic overnmer	2006	ter				
Dother form						Geo	ologic H	Rock	Rock	So Stion: Ye	COLUMN TAXABLE PROPERTY OF	oil S		oil			
Dother form		1999		E	13921		acency:		D P	ounding		Falling H	azards fr	om Taller	Adjacen	t Building	1
					ister .	Irre	gularitie	S:	Ve X PI	ertical (ty an (type	pe/sever	ity) OC	ntrán	t co	mer	it Kne	1/mod
Firewal	1			J		Haz	erior Fa ards:			arapets	Chimney	S		avy Clado endages		eavy Ver	neer
Addition		ASIC	sco	RE, MO	DIFIE		Addition		es or con	nments	on separa						
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	SW)	(URM INE)	(MRF)	(SW)	(URM INF) 0.9	(TU) 1.1	1.0	(FD)	(RD)		
Severe Vertical Irregularity, VL1	-0.9	-0.9	-0.9		-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	1.1 -0.7	1.1 -0.7	0.9 -0.6	1.1 NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.6 -0.7	-0.5	-0.5		-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3 -0.3	-0.4 -0.5	-0.4	-0.4 -0.4	-0.4 -0.4	-0.3 -0.3	NA
Pre-Code	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.4	-0.4	-0.4	-0.3	NA 0.0
Post-Benchmark Soil Type A or B	1.9 0.5	1.9 0.5	2.0	1.0	1.1 0.3	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3 -0.2	0.3	0.1	0.1 -0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0.7	0.7	0.7	05	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
Contraction of the second s	-	0.1		0.5)												-	
EXTENT OF REVIEW Exterior: Interior: Drawings Reviewed: Yes Interior: Contact Person: EEVEL 2 SCREENING PERFO	Are Then Detailed Poun cut-o Fallin buildi Geole Signi	building Geologic hazards or Soil Type F Detailed Nonstructural Evaluation Recommended? (0)								led? (ch	aluated						
Nonstructural hazards? Yes Where information of	annot h	e verifie		ener shal	note th	e follow	ina: F	T = Feti	No No	o, no nor	structura	I hazard	s identifie		DNK		
Legend: MRF = Moment-resi				einforced cor		C IONOW	JRM INF	= Unreinfo	rced maso	unrella		A REAL PROPERTY AND	ctured Hou		Sector Control 11	e diaphra	

Structure 70, Building 48 Photographs



Exterior, Split Level

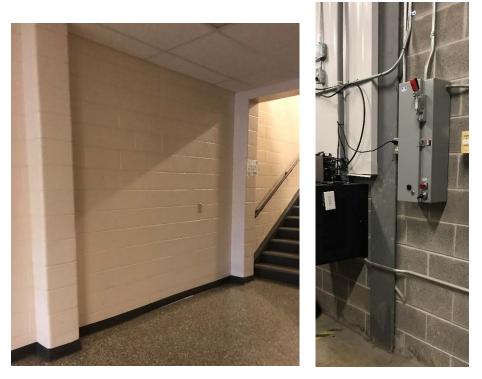


Interior, Steel Framing Exposed



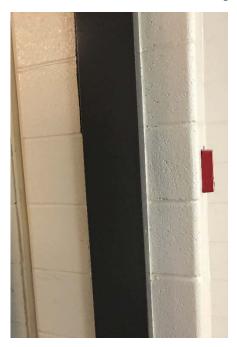
Firewall Between Structures 70 and 71

							er Identi	tr	20		IN.		Z	ip: <u>3</u>	826	0	
рно	TOGRAP	н				Use Lati Ss:	tude:	igh 36,2	141	hool 321).65	2	0580	616	
						-	eener(s)		M				ate/Time		131		
						Tota		Area (so	ı. ft.):			v Grade <u>638</u> uilt:	: <u>0</u> 19'7'	Code	Built: Year:	2011 1	EST
						Occ	upancy		embly strial y	Comme Office Wareho		Emer. S School Residen			storic overnmer	☐ Shelt nt	er
		1				Soil	Туре:	Hard Rock	Avg Rock	Den So	se St	iff S	oft Po		NK DNK, assi	ume Type	D.
This form						Geo	logic H	azards:	Liquefac	tion: Yes	s/No/DNł	< Lands	lide: Yes	No/DNK	Surf. Ru	upt.: Yes/	No/DNK
T-leb (lev		L	-	5			acency:			ounding						t Building	
Dother form Firewa	1		-		7	Irregularities: X Vertical (type/severity) 2005/ Severe 1501; Leve									level/	mod	
				Ţ			erior Fal ards:	lling		arapets	Chimney	S		avy Clado endages		eavy Ver	neer
						CO	MMENT	S:									
	КЕТСН	sina 1					Addition										
		ASIC	sco	RE, MO	DIFIER			AL LE				and the second second second					
FEMA BUILDING TYPE Do No Know	t W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	12	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9 -0.6	-0.9 -0.5	-0.9 -0.5	-0.8	-0.7 -0.4	-0.8 -0.5	-0.7 -0.4	-0.7	-0.7 -0.4	-0.8 -0.4	-0.6 -0.3	-0.7 -0.4	-0.7	-0.7 -0.4	-0.7	-0.6 -0.3	NA NA
Plan Irregularity, PL1 Pre-Code	-0.7 -0.3	-0.7	-0.6	0.2.5	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0,4	-0.4	-0.4	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	-0.3	-0.2 1.1	-0.3 1.1	-0.2 1.5	-0,1 NA	-0.1 1.4	-0.2	0.0 NA	-0.2 1.5	-0.1	-0.2 1.6	-0.2	0.0 NA	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.2	-0.4	-0.3	-0.2 -0.3	-0.2 NA	-0.2	-0.1 -0.1	-0.1 -0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, SMIN	0.7	0.7	0.Z	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	NA 0.2	-0.1	-0.2	-0.2	0.0	NA 1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$	»: (),7	51	2,5)													
EXTENT OF REVIEW				OTHER	RHAZ	ARDS	;		ACT	ION R	EQUIF	RED					
Exterior: Partial Interior: None Source: Yes Source:	e Hazard Structura ding pote ff, if know	al Evalu ential (ur vn)	nless SL2	>	Ye X Ye	es, unkno es, score	tural Even own FEM less that hazards	A buildir n cut-off	ng type or		uilding						
Geologic Hazards Source:							aller adja	icent		0							
Geologic haz							terioration to Yes, nonstructural hazards identified that should be evaluated No, nonstructural hazards exist that may require mitigation, but a detailed evaluation is not necessary										
		1000			-										DNK		
Where informatio		be verifie	d, scr	ener shal				ST = Estin = Unreinfor	mated o	r unrelia							



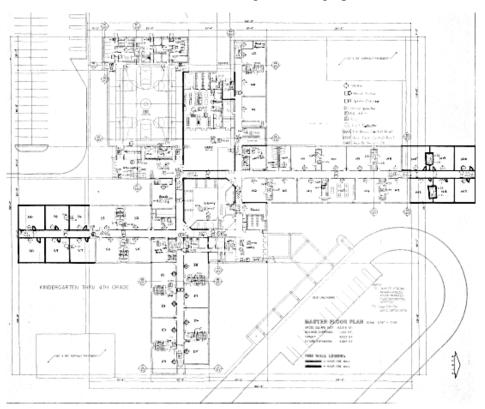
Structure 71, Building 48 Photographs

Interior, Steel Columns Encased (Left) and Exposed (Right)



Firewall Between Structures 70 and 71

						Ter		12	10	11	11.			The	0		
						Add	iress: _	12	-	121	H1 G	hn		45	Byp		
							-		ion	Cit	YT	N		Zip: _ 🗧	325		
							er Ident		ant.	L		12.10	200	an			
							Iding Na	me:	ANDER	10mg	CAN P	aron	NOU				
						Use		rew	1en	tarry	sch			.00	0/-	. 10	
BHOT	GRAP					1.000	tude:	3617	> + 0	+ CC		ongitu	de:	.89,	065	668	
PHOTO	JGRAPI	n				Ss:	1.3		M				2154				
						-	eener(s)						ate/Tim				
							Stories		e Grade			v Grade	: <u>0</u>		r Built:	1991 1	I EST
							al Floor litions:	Area (so			7,0		01.		e Year:	-0	
										Yes, Y			194.		6,19		
						000	upancy		embly Istrial	Comme Office	rcial	Emer. S	ervices		istoric overnmer	Shelt	er
								Utili		Wareho	use		ntial, #U		oveninei	n	
		5	1			Soil	Type:		□в						NK		
		1	an	~		-		Hard	Avg	Dens	se St	iff S	Soft P			ume Type	D.
1919			2.0	p)		1	1	Rock	Rock	Soi				Soil			
1994		1	/	1												upt.: Yes/	125 21 22 240 49
		/	/	'\'			acency:			ounding						t Building	
		11		1		Irre	gularitie	s:						evel			
P		1								an (type)			itrar	nt co	1 NOV		
	-						erior Fal ards:	ling		hbraced (Chimney	S				eavy Ver	ieer
Cafe Librar	V					naz	arus.			arapets				pendages	5		121
Cafe Librar	1				-		MMENT	S.		uner						and the second second	
										1	1.4						
P-XI I		T				-	·Re	inf	orce	AV	Vlas	NO	N				
Gym						-	1 -						0				
	-	-				-	'										
	-		-			-											
	19	96		_													
	tia	99-															
SKI	TCH	111					Addition	al akatab									
	and the second se	ASIC	000	DE MO	DIFIEI		Addition	and the second second second second		The party of the second se	ACCRET OF THE OWNER, NAME OF TAXABLE PARTY.	and the second second				-	
FEMA BUILDING TYPE Do Not	W1	W1A	W2	RE, MO			-						1				
Know	VVI	WIA	VV2	S1 (MRF)	S2 (BR)	\$3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	SW)	INF) 1.2	1.0	1.2	INF) 0.9	1.1	10	-			
Severe Vertical Irregularity, VL1	-0.9	-0.9	-0.9	0.00	-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	1.1 -0.7	0.9 -0.6	1.1 NA
Moderate Vertical Irregularity, VL1	-0.6	-0.5	-0.5		-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4		-0.4	-0.3	NA
Plan Irregularity, PL1 Pre-Code	-0.7	-0.7	-0.6		0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Post-Benchmark	-0.3 1.9	-0.3 1.9	-0.3		-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	(-0.2)	-0.2	0.0	0.0
Soil Type A or B	. 0.5	0.5	2.0	100	1.1	1.1 0.4	1.5	NA 0.2	1.4	1.7	NA	1.5	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	.0.0	-0.2	-0.4		-0.2	-0.2	-0.2	-0.1	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4		-0.3	NA	-0.3	-0.1	-0.1	-0.2	-0.1	-0.2 NA	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, S _{MIN}	0.7	0.7	0.7		0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	F	1.0	>	0.3	L.MORAN MON			Auto Automatica and and						department on some			
EXTENT OF REVIEW	-			OTHER		APDO			ACT		FOLUE						
	All Sides		ial	Are Ther		and a second second				ION RI			-				
	/isible			Detailed				`		ed Struct			approximation of				
Drawings Reviewed: 🔀 Yes 🗌 I	No			Pour				>		es, unkno es, score				r other bi	uilding		2
Soil Type Source:					ff, if know		1000 012			es, score							
Geologic Hazards Source:				Fallir	g hazard		aller adja	cent				- sount					
Contact Person: Phil Gr	ahan	^		build		rde en O	oil Turne	F	Detaile	ed Nonst	ructural	Evalua	tion Red	comment	ded? (ch	eck one)	
LEVEL 2 SCREENING PERFO	ORME	D?		Geol	ficant dar	nage/de	Soil Type eterioratio	r to	TYe	es, nonstr	uctural h	azards i	identified	that sho	uld be ev	aluated	2
Yes, Final Level 2 Score, SL2		TAN N	0		tructural		aud		No No	o, nonstru	ictural ha	azards e	xist that	may requ	uire mitig	ation, but	a
Nonstructural hazards?									de	tailed eva	aluation i	s not ne	cessary		-		
	annoth			eener cha	I note th	o follow	ling: Ef			o, no non					DNK		
Where information of Legend: MRF = Moment-res				eener snal											Contraction of the second		
BR = Braced frame	only hall			hear wall	ICIEIE		URM INF = TU = Tilt u	p onreinto	iceo maso	onry intili	MH =	= Manufa = Light me	ctured Ho etal		D = Flexib D = Rigid	le diaphrag diaphragm	gm

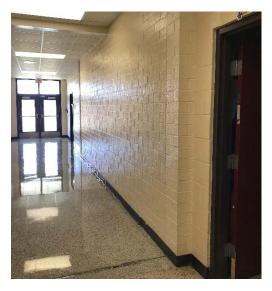


Structure 72, Building 49 Photographs

Plan View



Flexible Diaphragm Roof



Small Hallway Addition

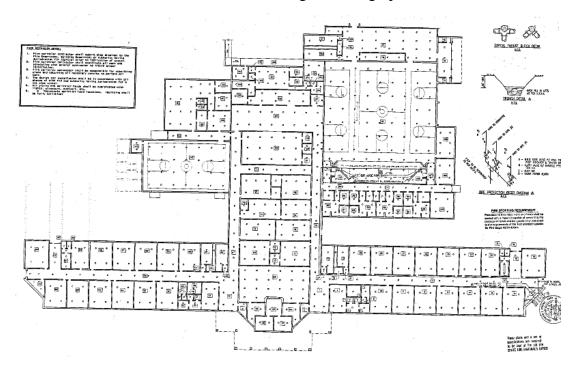
Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Level 1 HIGH Seismicity

								ress: _		th '	Fult			Z	ip: <u>3</u>	825'	7	
							Build Use:	ding Na	Contraction of the second s	10./1	tign 1358			de:	88.8	999	0	
	РНОТО	GRAPH					Ss:	1.2	25					1,419			, -	
							Scre	ener(s)	: <u>C</u>	M			Da	ate/Time	: <u>51</u>	31		
							Tota	Stories: I Floor itions:	Above Area (sq			1000		: 0		Built: Year:	19950	EST
							Occi	upancy	: Asse Indu Utilit		Commer Office Warehou	(Emer. S School Residen	ervices tial, #Un		storic overnmer	Shelt	er
	11			_			Soil	Туре:	A Hard Rock	Avg Rock	Dens Soil	e Sti	iff S	oft Po		NK DNK, assi	ume Type	D.
		Z	Slop	ed	roof		Geo	logic H	azards:	the fact and the second se						Surf. R	upt.: Yes/	No/DNH
								icency:			ounding			azards fro				
		Exti		-				gularitie			ertical (typ an (type)	e/severi	itySp		evell	mod	~	
		1.	F	4	-1		10 10 10 10 10 10 10 10 10 10 10 10 10 1	erior Fal ards:	ling	D Pa	nbraced (arapets ther:	Chimney	S		avy Clado endages		eavy Ven	eer
Flatr	toot						10000	MMENT	0.00									-
					5		,	Me	tal	dec	Kr	oof						
	R	Flat	m	P	1			Ste	tal cel usor	me	infi	ers 11						
	4	/	1	- [2				,									
Kanan ta and	SKE					_			al sketche									
					RE, MO								_1					
	Do Not	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
FEMA BUILDING TYPE	Know							SW)	INF)									
Basic Score Severe Vertical Irregularity, VLr	Know	3.6 -1.2	3.2 -1.2	2.9 -1.2	2.1 -1.0	2.0 -1.0	2.6 -1.1	SW) 2.0 -1.0	1.7	1.5 -0.9	2.0 -1.0	1.2	1.6 -1.0	1.4 -0.9	1.7 -0.9	1.7 -0.9	1.0	1.5 NA
Basic Score Severe Vertical Irregularity, VLr Moderate Vertical Irregularity, VLr	Know	-1.2 -0.7	-1.2 -0.7	-1.2 -0.7	-1.0 -0.6	-1.0 -0.6	-1.1 -0.7	2.0 -1.0 -0.6	1.28 (5)	-0.9 -0.5	2.0 -1.0 -0.6		1.6 -1.0 -0.6	1.4 -0.9 -0.5	1.7 -0.9 -0.5	1.7 -0.9 -0.5	1.0 -0.7 -0.4	NA NA
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	Know	-1.2 -0.7 -1.1	-1.2 -0.7 -1.0	-1.2 -0.7 -1.0	-1.0 -0.6 -0.8	-1.0 -0.6 -0.7	-1.1 -0.7 -0.9	2.0 -1.0 -0.6 -0.7	1.3056	-0.9 -0.5 -0.6	-1.0 -0.6 -0.8	1.2 -0.7 -0.4 -0.5	-1.0 -0.6 -0.7	-0.9 -0.5 -0.6	-0.9 -0.5 -0.7	-0.9 -0.5 -0.7	-0.7 -0.4 -0.4	NA NA NA
Basic Score Severe Vertical Irregularity, VLr Moderate Vertical Irregularity, VLr	Know	-1.2 -0.7	-1.2 -0.7	-1.2 -0.7	-1.0 -0.6 -0.8	-1.0 -0.6	-1.1 -0.7	2.0 -1.0 -0.6	1.28 (5)	-0.9 -0.5	-1.0 -0.6 -0.8 -0.7	1.2 -0.7 -0.4	-1.0 -0.6 -0.7 -0.5	-0.9 -0.5 -0.6 -0.3	-0.9 -0.5 -0.7 -0.5	-0.9 -0.5 -0.7 -0.5	-0.7 -0.4 -0.4 0.0	NA NA NA -0.1
Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B	Know	-1.2 -0.7 -1.1 -1.1 1.6 0.1	-1.2 -0.7 -1.0 -1.0 1.9 0.3	-1.2 -0.7 -1.0 -0.9 2.2 0.5	-1.0 -0.6 -0.8 -0.6 1.4 0.4	-1.0 -0.6 -0.7 -0.6 1.4 0.6	-1.1 -0.7 -0.9 -0.8 1.1 0.1	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6	1,000	-0.9 -0.5 -0.6 -0.4	-1.0 -0.6 -0.8	1.2 -0.7 -0.4 -0.5 -0.1	-1.0 -0.6 -0.7	-0.9 -0.5 -0.6	-0.9 -0.5 -0.7	-0.9 -0.5 -0.7	-0.7 -0.4 -0.4	NA NA NA
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)	Know	-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1	17 0 0 0 0 0 0 0 0 0 0 0 0 0	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2	NA NA -0.1 1.2 0.3 -0.4
Basic Score Severe Vertical Irregularity, V _{L1} Moderate Vertical Irregularity, V _{L1} Plan Irregularity, P _{L1} Pre-Code Post-Benchmark Soil Type A or B	Know	-1.2 -0.7 -1.1 -1.1 1.6 0.1	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6	17 00.6 0.2 NA 0.5 -0.4 -0.4	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	NA NA -0.1 1.2 0.3 -0.4 NA
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN		-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1	17 0 0 0 0 0 0 0 0 0 0 0 0 0	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2	NA NA -0.1 1.2 0.3 -0.4
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN		-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	17 00.6 0.2 NA 0.5 -0.4 -0.4	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	NA NA -0.1 1.2 0.3 -0.4 NA
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL: EXTENT OF REVIEW Exterior: Drawings Reviewed: Oray Reviewed: Soil Type Source:	1 ≥ Smin: al □ A	-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 -6 -6 -0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7 22 0.7	-1.0 -0.6 -0.8 -0.6 1.4 -0.2 -0.6 0.5 	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 R HAZ Structura ding pote ff, if know	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That T al Evalu ential (un vn)	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger J ation?	17 08 05 0.6 0.5 0.4 0.5 0.5	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIR tural Eva	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2	NA NA -0.1 1.2 0.3 -0.4 NA
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Exterior: Drawings Reviewed: Geologic Hazards Source:	1 ≥ Smin: al □ A ♀ □ Vi ☑ N	-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1	-1.2 -0.7 -1.0 1.9 0.3 0.2 -0.6 0.9 -0.6 0.9 -0.6 Aeri	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7 22 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are Then Detailed Detailed Detailed	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 R HAZ structure dding pote Structure dding pote	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That T al Evalu ential (un vn)	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger J ation?	17 08 05 0.6 0.5 0.4 0.5 0.5	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detail	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ION RI ed Struc: es, unkno es, score es, other o	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 0.3 EQUIF EQUIF Ever won FEM less than hazards	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation A buildir present	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMM FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Interior: Drawings Reviewed: Drawings Reviewed: Contact Person:	1≥ SMIN: al □ A ♀ □ VI ♀ N	-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 Il Sides isible 0	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7 22 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are Ther Detailed Poun cuto Etailio Detailed	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 R HAZ structure dding pote Structure dding pote	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS Is That T al Evalu ential (un vn) Is from ta	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5	1.7 -0.8 -0.2 NA 0.5 -0.4 -0.4 -0.4 0.5	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detail Detail VY VI Detail	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ION RI ed Struct es, unkno es, score es, other o ed Nonst	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIF cural Eva wn FEM less than hazards	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation A buildir n cut-off present	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Interior: Drawings Reviewed: Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING	1 ≥ SMIN: al □ A	-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 Il Sides isible 0	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 -0.6 0.9 -0.6 -0.9 -0.6 -0.9 -0.6 -0.7 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0 -1.0	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7 22 0.7	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are Ther Detailed Poun cut-o Fallin Builtin Geok	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.4 -0.6 0.5 R HAZ. e Hazard Structuration ding pote ff, if know ng hazard ing ogic haza ficant dar	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That T al Evalu ential (un vn) Is from ta ards or S mage/de	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger / ation? ation? aller adja oil Type	1.7 -0.8 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.4 -0.4 -0.5	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detail QY Y0 Detail	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ION RI ed Struct es, unkno es, score es, other o ed Nonst	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 0.3 EQUIF tural Eva who FEM less that hazards ructural h	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation A buildir n cut-off present Evalua	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require ng type o tion Rec identified	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 r other but that sho	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0
Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMM FINAL LEVEL 1 SCORE, SL1 EXTENT OF REVIEW Exterior: Drawings Reviewed: Drawings Reviewed: Contact Person: LEVEL 2 SCREENING Yes, Final Level 2 Score, SL1	1 ≥ SMIN: al □ A	-1.2 -0.7 -1.1 -1.1 1.6 0.1 0.2 -0.3 1.1 Il Sides isible 0	-1.2 -0.7 -1.0 -1.0 1.9 0.3 0.2 -0.6 0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9	-1.2 -0.7 -1.0 -0.9 2.2 0.5 0.1 -0.9 0.7 2 2 0 3 2 0 7 -0.9 0.7 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9 -0.9	-1.0 -0.6 -0.8 -0.6 1.4 0.4 -0.2 -0.6 0.5 OTHEF Are Ther Detailed Poun cut-o Fallin Builtin Geok	-1.0 -0.6 -0.7 -0.6 1.4 0.6 -0.4 -0.6 0.5 R HAZ. e Hazard Structura ding pote ff, if know ng hazard ing	-1.1 -0.7 -0.9 -0.8 1.1 0.1 0.2 NA 0.6 ARDS is That T al Evalu ential (un vn) Is from ta ards or S mage/de	2.0 -1.0 -0.6 -0.7 -0.6 1.9 0.6 -0.1 -0.6 0.5 Trigger / ation? ation? aller adja oil Type	1.7 -0.8 -0.2 NA 0.5 -0.4 -0.4 -0.4 -0.4 -0.4 -0.5	-0.9 -0.5 -0.6 -0.4 1.9 0.4 0.0 -0.5 0.3 ACT Detail ACT Detail ACT	-1.0 -0.6 -0.8 -0.7 2.1 0.5 0.0 -0.7 0.3 ION RI ed Struct es, unkno es, score es, other o ed Nonst	1.2 -0.7 -0.4 -0.5 -0.1 NA 0.3 -0.2 -0.3 0.3 EQUIR EQUIR Examples that hazards ructural h ructural h ructural h	-1.0 -0.6 -0.7 -0.5 2.0 0.6 -0.3 NA 0.2 RED aluation A buildin n cut-off present I Evalua hazards azards e is not ne	-0.9 -0.5 -0.6 -0.3 2.4 0.4 -0.1 -0.4 0.2 Require ng type o tion Rec identified exist that	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.5 0.3 ed? r other but sommend that sho may requ	-0.9 -0.5 -0.7 -0.5 2.1 0.5 -0.1 -0.6 0.3	-0.7 -0.4 -0.4 0.0 NA 0.3 -0.2 -0.2 0.2	NA NA -0.1 1.2 0.3 -0.4 NA 1.0

Structure 73, Building 50 Photographs



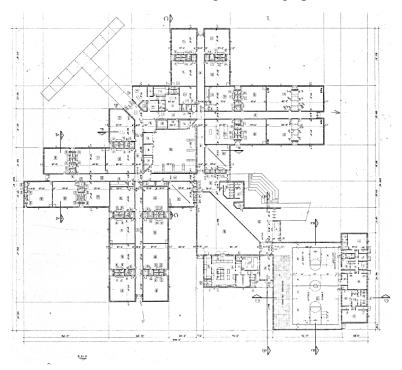
Plan View



Interior, Split Level

Level 1 HIGH Seismicity

								Sout	th t	shn Fulto	C,	Jor		lip: 3	3825	57	
						Oth	er Identi	ifiers:	74								
						Buil	ding Na				_						
						Use	: _	Eler	ment	ary !	Scha	10					
						Lati	tude: 3	36.4	8560	0	L	ongitu	de: 🦳	88.8	764	198	
PHOT	OGRAP	н				Ss:		199				S1:	0.41	0		10	
						Scre	eener(s)	: 0	M				ate/Time		-		
						No	Stories	: Abov	e Grade	. 1	Bolow	v Grade			Duilt	1980 0	7 cor
						Tota		Area (so	q. ft.): _		,00	С			Year:	14801	LESI
						Occ	upancy	: Ass	embly Istrial	Comme Office Wareho	rcial	Emer. S School	ervices Itial, #Ur		storic overnmen	□ Sheit nt	er
		1	-			Soil	Туре:	A Hard Rock	Avg Rock	Dens	C 🗖	D C	E		NK DNK, assi	ume Type	D.
Canopy						Geo	logic H						1000	/No/DNK	Curf D	unt : Vaal	
						220000000000000000000000000000000000000	acency:		the state of the s	ounding		and an other states in the states					
	1	-								7.				om Taller		t Building	
		-				Irreg	gularitie	IS:	D PI	an (type)	re	,~en	trant	cor	nev		
P	ſ						erior Fal ards:	lling		nbraced arapets ther:	Chimney	S		avy Clado bendages		eavy Ven	ieer
						CO	MMENT	S:					-		-	-	
	-					10.20.27				1 MA		~ 1					
	7					- '	Ke.	INP	SICC	y W	lason	YY					
	-	-	-			-											
	L			-	-												
		-															
		-				-											
	-			_		-											
SK	ETCH		L		-		Addition	al akatab		nments c							
	and the second second	ASIC	sco	RE, MO	DIFIER												-
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	\$3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score	3.6	3.2	2.9	2.1	2.0	2.6	SW)	INF)	A CONTRACTOR	- Andersteiner	INF)						
Severe Vertical Irregularity, VL1	-1.2	-1.2	-1.2		-1.0	-1.1	-1.0	-0.8	1.5 -0.9	2.0 -1.0	1.2 -0.7	1.6 -1.0	1.4 -0.9	-0.9	1.7 -0.9	1.0 -0.7	1.5 NA
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-0.6	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.6	-0.5	0.5	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	-0.7	-0.7	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	(-0.5	-0.5	0.0	-0.1
Post-Benchmark Soil Type A or B	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.1	0.3	0.5	-0.2	0.6 -0.4	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.2	-0.4	0.2 NA	-0.1	-0.4	0.0	0.0	-0.2 -0.3	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Minimum Score, Smin	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	NA 0.2	-0.4	-0.5	-0.6 0.3	-0.2 0.2	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN		C	12	0.3			0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.5	0.5	0.2	1.0
EXTENT OF REVIEW	Tel.	0		OTHER		APDO			1007		FOUNT		-	-	-	-	-
	All Sides		ial	Are There					Comession of	ION R		1000 C					
		Ent		Detailed				Ą		ed Struc							
	No			Poun	ding pote	ential (ur		>	X Ye	es, score	less than	n cut-off		r other bi	uilding		
Geologic Hazards Source: Contact Person: Phil Grad				Fallin	ff, if know g hazard		aller adja	cent		es, other o	nazards	present					
Contact Person: Phil Grai	am	-		buildi Geolo	ng ogic haza	rds or S	oil Type	F						ommend			
LEVEL 2 SCREENING PERF	ORME	D?		Signi	ficant dan	nage/de	eterioratio	on to	U Ye	es, nonst	ructural h	nazards	identified	that sho	uld be ev	valuated	
Yes, Final Level 2 Score, SL2	_		0	the st	tructural s	system				o, nonstru	uctural ha	azards e	xist that	may requ	ire mitiga	ation, but	а
Nonstructural hazards? Yes	1		lo							tailed ev				Je ho	DNK		
Where information	cannot h		-	ener chal	I note the	a follow	ina: E	ST = Eet								-	
Legend: MRF = Moment-res				ener snar													
BR = Braced frame	i ang nan			near wall	101010	1	TU = Tilt u	= Unreinfo Ip	nceu mas	any mu		= Manufa = Light m	etal		D = Flexib D = Rigid	le diaphrag	gm



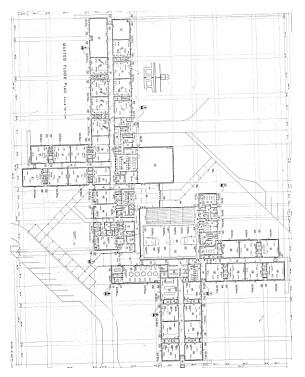
Structure 74, Building 51 Photographs

Plan View



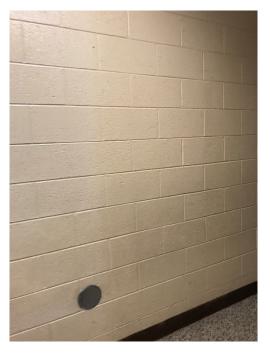
Exterior, Split Level

PHOTO	DGRAP	н				Oth Buil Use Lati Ss: Scre No. Tota	tude: <u>}</u> <u>1.68</u> eener(s)	fiers: me: ferv ferv ferv ferv ferv ferv ferv ferv	M re Grade q. ft.):	074	Scher Belov 72	Ongitur Sr: 0 Dr Dr V Grade OOO	de: 598 ate/Time	Year	Built: Year:] EST
						Occ	upancy	: Ass Indu Utili	embly ustrial ty	Comme Office Wareho	rcial - use	Emer. So School Residen	ervices) tial, #Un	His Go hits:	storic overnmen	Shelti	er
					-1	- 301	Type:	Hard	Avg	Den	se St	iff S	oft Po			ume Type	D.
		Ad	1:4	ion		Geo	logic Ha	Rock	Rock Liquefac	Soi tion: Yes				Soil /No/DNK	Surf Ru	int · Yes/	
		1	2012	-)		1010001000	acency:			ounding			and a state of the	om Taller			
						Irreg	gularitie	s:	🔀 Ve	ertical (ty an (type)	pe/sever	ity) S	plit	level	1m	od .	
		-	-	_			erior Fal ards:	ling	UI UI	nbraced (arapets			🗌 Hea	avy Cladd bendages	ing or He	eavy Ven	eer
	sym	1					MMENT				and a second second		And the second second				-
4						1	SBO										
	-		1				120	. 0	.(Ste	el	C.61.	s vi	nder	Gre	3 or	1y
1995	-		_				00		-								1
		-				-											
						-											
		-				-											
SK	ETCH						Additiona	al sketch	es or cor	nments c	n separa	ate page					
	B	ASIC	sco	RE, MO	DIFIER	RS, AI	ND FIN	AL LI	EVEL	1 SCO	RE, SI	L1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	2.1 -0.9	1.9 -0.9	1.8 -0.9	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	1.1	1.1	0.9	1.1
Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9	-0.8	-0.7 -0.4	-0.8 -0.5	-0.7	-0.7 -0.3	-0.7	-0.8	-0.6 -0.3	-0.7 -0.4	-0.7 -0.4	-0.7	-0.7 -0.4	-0.6 -0.3	NA NA
Plan Irregularity, PL1	-0.7	-0.7	-0.6	-0.5	-0.5	-0.6	-0.4	-0.4	-0.4	-0.5	-0.3	-0.5	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code Post-Benchmark	-0.3	-0.3	-0.3	-0.3	-0.2	-0.3	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	0.0
Soil Type A or B	1.9	1.9	2.0	1.0	1.1 0.3	1.1 0.4	1.5	NA 0.2	1.4	1.7	NA 0.1	1.5 0.3	1.7	1.6	1.6	NA	0.5
Soil Type E (1-3 stories)	0.0	-0.2	-0.4	-0.3	-0.2	-0.2	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	0.3	0.3 -0.2	0.1	0.1 -0.1
Soil Type E (> 3 stories)	-0.4	-0.4	-0.4	-0.3	-0.3	NA	-0.3	-0.1	-0.1	-0.3	-0.1	NA	-0.1	-0.2	-0.2	0.0	NA
Minimum Score, S _{MIN}	0.7	0.7	OZ	0.5	0.5	0.5	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	0	.13	(0.	3													
EXTENT OF REVIEW			T	OTHER	RHAZ	ARDS			ACT	ION R	EQUIR	RED					
		Aeri		Are Ther				1	A CONTRACTOR OF	ed Struc			Require	d?			
	Visible No	K Ente	ered	Detailed					T Ye	es, unkno	wn FEM	A buildin		r other bu	ilding		
Soil Type Source:					ding pote ff, if know		nless SL2	>	🔀 Ye	es, score	less than	n cut-off					
Geologic Hazards Source:				Fallin	ig hazard	s from ta	aller adja	cent		es, other o	nazaros	present					
Contact Person: Phil Gro	shan	1		buildi	ng						tructural	Evaluat	tion Rec	ommend	ed? (ch	eck one)	
LEVEL 2 SCREENING PERF	ORME	D?			ogic haza ficant dar				Ye	es, nonst	ructural h	nazards i	dentified	that shou	uld be ev	aluated	
Yes, Final Level 2 Score, SL2		N N	0		tructural					o, nonstru	uctural ha	azards e	xist that i	may requ	ire mitiga	ation, but	a
Nonstructural hazards? Yes		O N	22							tailed ev	aluation i structura	is not ne Il hazard	cessary s identifie	ed 🗖	DNK		
Where information of	cannot b	e verifie	d, scre	ener shal	I note th	e follow	ing; ES	T = Esti									
Legend: MRF = Moment-res	isting fram	ne F	RC = Re	einforced cor		1	JRM INF =	Unreinfo	rced maso				ctured Ho		and a start of the	e diaphrac	Im
BR = Braced frame		5	SW = SI	near wall		1	TU = Tilt u	p		1	LM =	= Light me	etal) = Rigid (diaphragm	



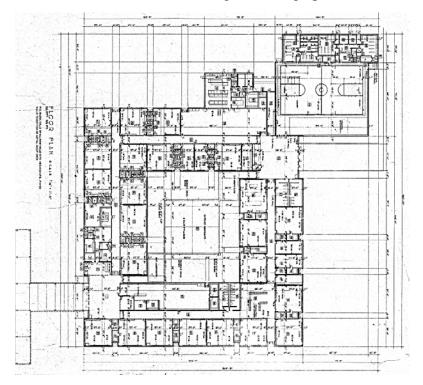
Structure 75, Building 52 Photographs

Plan View



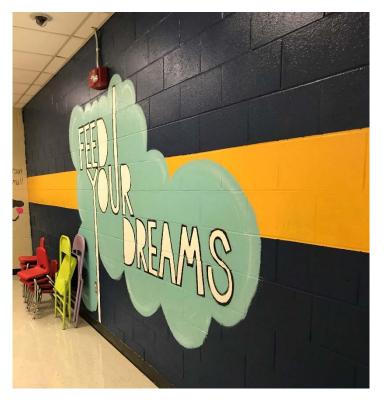
Interior, Reinforced Masonry

						Add	lress:	36	SN	Jr	Sha	sta	sn	Rd.			JILY
						0	ar Island	Hor	nbe Fil	aki	tN			Zip: 3	823	2	
								ifiers:	16	The second					(11.11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.		
						Bui	Iding Na	lan	ent	and	The	1					
						Use	tudo:	LUVI LL 2	<u>u</u> u	07a				00	2017	190	
РНОТО	GRAP	н				Ss:	2,	220	11	061).86	-89,	201	101	
						1.1	eener(s)		M		`		ate/Tim				
						No.	Stories	: Abov	e Grade	a:	Belov	w Grade	0	Yea	Ruitt-	985 1	7 EST
								Area (se			620				Year:	1.0	
						Add	litions:	🗆 N	one D		(ear(s) B		20		5000	झ	
· · · · · · · · · · · · · · · · · · ·						Occ	upancy		embly ustrial ty	Comme Office Wareho		Emer. S School Residen		1.	storic overnmer	Shelt nt	ler
						Soil	Type:		□В		c 🔀	D	JE [NK		
	-							Hard Rock	Avg Rock	Den So	il So	oil S	Soil S	Soil		ume Type	
	1	-	1	-		TTTDeterates	and a subscription of the subscription of							s/No/DNK			
			-			-	acency:			ounding		Falling H	lazards fr	om Taller	Adjacen	t Building	
						Irreg	gularitie	s:		ertical (ty lan (type)	pe/sever	ity) St	TARN	~ OP	mo	id Id	
0	on:	14					erior Fal ards:	lling		nbraced arapets	Chimney		He	avy Clado pendages	ding or H		ieer
0p (Cou	era	.1				0	MMENT	·c.	0	ther:							
(600	rtva	(h)				100		δ.									
		.05					12	N									-
		-		-		4											1999
		-				-											
	-	-	-			-											
		-				-											
SKI	ETCH						Addition	al sketch	es or cor	nments (n senara	ate nane					
	В	ASIC	sco	RE, MO	DIFIER												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	and the second sec	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score	2.1	1.9	1.8	1.5	1.4	1.6	1.4	1.2	1.0	1.2	0.9	1.1	1.0	(1.1)	1.1	0.9	1.1
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-0.9	-0.9	-0.9		-0.7	-0.8	-0.7	-0.7	-0.7	-0.8	-0.6	-0.7	-0.7	-0.7	-0.7	-0.6	NA
Plan Irregularity, P_{L1}	-0.6	-0.5	-0.5		-0.4	-0.5 -0.6	-0.4	-0.3	-0.4	-0.4	-0.3 -0.3	-0.4	-0.4	-0.4	-0.4	-0.3	NA
Pre-Code	-0.3	-0.3	-0.3		-0.2	-0.3	-0.2	-0.4	-0.4	-0.5	0.0	-0.5	-0.4	-0.4	-0.4	-0.3 0.0	NA 0.0
Post-Benchmark	1.9	1.9	2.0		1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	-0.2	1.6	NA NA	0.0
Soil Type A or B	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.2	-0.4		-0.2	-0.2 NA	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7		0.5	0.5	0.5	-0.1	-0.1	-0.3	-0.1 0.3	NA 0.2	-0.1	-0.2	-0.2 0.3	0.0	NA
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$:	C	51.(-0				-			0.0	0.0	VIL	0.2	1 0.0	0.5	0.2	1.0
EXTENT OF REVIEW				OTHER	HAZ	ARDS			ACT	ION R	EQUIR	RED					
		Aer		Are There	Hazard	s That 1	Trigger A	A	and the second		tural Eva		Require	ed?			1
	/isible No	Enter Enter	ered	Detailed	Structura	al Evalu	ation?		T Ye					or other bu	uildina		
Soil Type Source:	10		-	Poun			nless SL2	>	🔀 Ye	es, score	less than	n cut-off					
Geologic Hazards Source:					f, if know g hazard:		aller adia	cent			hazards	present					
Contact Person: PLI Gr	aho	im		buildi	ng						tructural	Evalua	tion Rec	comment	led? (ch	eck onel	
LEVEL 2 SCREENING PERFO	ORME	D?			ogic haza icant dan									that sho			
Yes, Final Level 2 Score, SL2	trella		0		ructural s		008101300	1110		o, nonstru	uctural ha	azards e	xist that	may requ	ire mitiga	ation, but	a
Nonstructural hazards?									de	tailed ev	aluation i	s not ne	cessary	1	1		
Where information of	annoth		Sec. 1	annor chal	note the	follow	ina E	T = [-+			structura				DNK		
Legend: MRF = Moment-resi				einforced cor				= Unreinfo							and the second second		
BR = Braced frame	a unit			hear wall	01010		U = Tilt u		iveu mas(vir A mum	MH :	= Manufa = Light me	ctured Ho	using Fl	J = Flexib	le diaphrag diaphragm	m



Structure 76, Building 53 Photographs

Plan View



Interior, Reinforced Masonry

PHOTO	DGRAP	H				Oth Buil Use Lati Ss: Scro No. Tota Add Occ	tude:	me: 	lone embly ustrial	itany 75	Belov D X Y Year(s) B rcial use	Longitu S1:Di w Grade 4 Emer. S School Residen	de: ate/Time : ervices tital, # Ur]E [e:	Built: Year: IBC Storic overnmen	33 986 Shelt	er
	1					Geo	logic Ha	Rock	Rock	So	il So	oil S	ioil S	Soli /No/DNK			
			1				acency:			oundina				om Taller			and the second se
			1	1			gularitie	s:			pe/sever	ity) 😽	114	level	mo	d	
		1	4	1		Exte	erior Fal	lina		an (type	Chimney	-ev		avy Clado	ting or H		loor
	1	-1	1				ards:			arapets				pendages		cavy von	1001
			1			CO	MMENT	S:	States and states and						0		
Entr	AN CC			addition		_								es es	00)		
31	Apple Contraction of the	ASIC	sco	RE, MO	DIFIE												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
Basic Score	2.1	1.9	1.8	1.5	1.4		(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)		
Severe Vertical Irregularity, VLr	-0.9	-0.9	-0.9	-0.8	-0.7	1.6 -0.8	1.4 -0.7	1.2 -0.7	1.0 -0.7	1.2 -0.8	0.9 -0.6	1.1 -0.7	-0.7	-0.7	1.1 -0.7	0.9 -0.6	1.1 NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.6 -0.7	-0.5 -0.7	-0.5		-0.4	-0.5	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.4	-0.3	-0.4	-0.3	NA
Pre-Code	-0.3	-0.3	-0.3	-0.5	-0.5 -0.2	-0.6 -0.3	-0.4 -0.2	-0.4	-0.4	-0.5	-0.3 0.0	-0.5 -0.2	-0.4	-0.4	-0.4 -0.2	-0.3	NA
Post-Benchmark	1.9	1.9	2.0	1.0	1.1	1.1	1.5	NA	1.4	1.7	NA	1.5	1.7	1.6	-0.2	0.0 NA	0.0
Soil Type A or B Soil Type E (1-3 stories)	0.5	0.5	0.4	0.3	0.3	0.4	0.3	0.2	0.2	0.3	0.1	0.3	0.2	0.3	0.3	0.1	0.1
Soli Type E (> 3 stories)	0.0	-0.2 -0.4	-0.4	-0.3	-0.2 -0.3	-0.2 NA	-0.2	-0.1	-0.1	-0.2	0.0	-0.2	-0.1	-0.2	-0.2	0.0	-0.1
Minimum Score, Smin	0.7	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.3	-0.3 0.3	-0.1 0.3	NA 0.2	-0.1	-0.2	-0.2 0.3	0.0	NA 1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	C	51.(05	E.				a and a second							0.0	0.2	1.0
Interior: None Drawings Reviewed: Yes Soil Type Source:	visible No	Aeri Ente	ial ered	cut-ol Fallin buildi Geolo Signif	e Hazard Structura ding pote if, if know g hazard ng ogic haza	Is That T al Evalu ential (ur vn) Is from ta urds or S mage/de	Frigger A	> cent F	Detaile	ed Struc es, unkno es, score es, other o ed Nons es, nonstr o, nonstr	less thar hazards tructural ructural h uctural ha	aluation A buildin n cut-off present I Evaluat nazards i azards e	tion Rec	ed? r other bu comment I that sho may requ	ied? (chi	aluated	a
Nonstructural hazards? Yes		D N	0						de No	tailed ev o, no nor	aluation i structura	is not ne Il hazard	cessary s identifi	ed 2	DNK		
Where information of	annot b														ow	and the Discourse	
Legend: MRF = Moment-res	sting fram	10	RC = Re	einforced cor	crete		IRM INF =	Unreinfo	rced masc	onry infill	MH	= Manufa	ctured Ho	uning Ef	PIC IN	e diaphrac	Contraction in the local division of the loc

Structure 77, Building 54 Photographs



Exterior, Two of 5 Wings



Interior, Reinforced Masonry

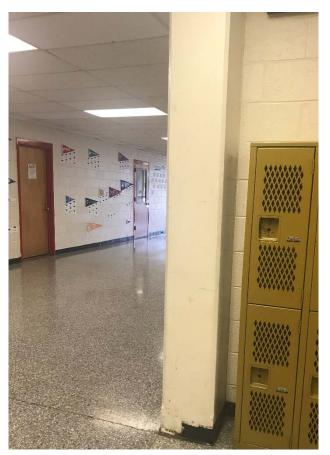
Level 1 HIGH Seismicity

				1	1	1				11.	-			-			-
						Add	ress:	Hum	V G	ikin th	3 P	<u>C.</u>	7	in: 3	834	3	
						Oth	er Ident	ifiers'	78	101	-			ip	051	2	
						Buil	ding Na	me:	10						1		
						Use	: +	tich	Sch	lac			-				
						Lati	tude: 3	5.8	405	83	1	ongitu	de:	88.	906	737	
PHOT	OGRAP	н				Ss:	1.0	14		-00		St: O	1352	001	100	100	
- India								: C1	M	-			ate/Time				
						12.44			e Grade	. 1	Polo		0		Duilt	1174)	
						Tota	al Floor	Area (so	q. ft.):	-7	6,100	V Grade	. 0		Year:	1/4)	EST
							litions:				Year(s) B			-			
						Occ	upancy	: Ass	embly	Comme	ercial	Emer. S	ervices	Н	storic	Shelt	er
								Indu Utili	ustrial ty	Office Wareho		School Residen	itial, #Un		overnmer	nt	
	_					Soil	Туре:	Hard	□B Avg	Den		D C	E	F Di	NK DNK, ass	ume Type	D.
								Rock	Rock	So				oil			
		-	-	1				and the second sec	Commission and the second second	CONTRACTOR OF A DESCRIPTION OF A DESCRIP	s/No/DNł		terms and the second seco	A CONTRACTOR OF			
		-			-	-	acency:			ounding			azards fro				
						Irreg	gularitie	s:	X Ve	ertical (ty an (type	/pe/sever) <u>r</u>	ity) St	olit k	avel A	mod ,		
		-				Exte	erior Fal	lina			Chimney					eavy Ver	oor
	7-	-					ards:	g		arapets	oninitio					cavy vei	
	1					CO	MMENT	S:									
						9	rais	ed	600	P 10	evs evs	m	t a	fete	evia		
						N	(0)	~	10.0	anl	0.0						
							00		PA4	ent	RND						
	gym	1				8	NG	hi	dial	Three	100						
	-					-	. 7)	100	-1.10	giv	5					
			-								0						
		-															
SK	ETCH	ASIC	500	RE, MO	DIEIEI						on separa			-			-
FEMA BUILDING TYPE Do Not	W1	W1A	W2	S1	S2	\$3	S4	S5	C1	C2	C3	PC1	PC2	RM1	RM2	URM	MH
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM INF)	(TU)		(FD)	(RD)	- Crum	
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2	2.9	2.1	2.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	1.7	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-1.2	-1.2	-1.2	-1.0	-1.0 -0.6	-1.1 -0.7	-1.0	-0.8 -0.5	-0.9	-1.0 -0.6	-0.7	-1.0	-0.9	-0.9	-0.9	-0.7	NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.0	-0.9	-0.7	-0.5	-0.5	-0.8	-0.4	-0.6	-0.5	-0.5	-0.5	-0.4	NA
Pre-Code	-1.1	-1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	(-0.1)	-0.5	-0.0	-0.7	-0.7	-0.4 0.0	NA -0.1
Post-Benchmark	1.6	1.9	2.2	1.4	1.4	1.1	1.9	NA	1.9	2.1	NA	2.0	2.4	2.1	2.1	NA	-0.1
Soil Type A or B	0.1	0.3	0.5	0.4	0.6	0.1	0.6	0.5	0.4	0.5	0.3	0.6	0.4	0.5	0.5	0.3	0.3
Soil Type E (1-3 stories)	0.2	0.2	0.1	-0.2	-0.4	0.2	-0.1	-0.4	0.0	0.0	-0.2	-0.3	-0.1	-0.1	-0.1	-0.2	-0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, S _{MIN}	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	(2,2	54	2.3					_								
EXTENT OF REVIEW	All 011			OTHER					1. 0-1. 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		EQUIF						
	All Sides Visible	Aer Ent	6759 A. 1997	Are Ther Detailed	e Hazard Structur	s That	rigger A	4			tural Eva						
Drawings Reviewed: 🗌 Yes 🛛 🕅	No		orou	Pour					Ye	es, unkn	own FEM	A buildir	ng type of	other bu	uilding		
Soil Type Source:					ff, if knov		iless SL2	-			e less that hazards						
Geologic Hazards Source:				Fallir	ng hazard		aller adja	cent				Probent					
Contact Person: Cherles/Ve	sie H	amlet	t	build	ing		ales de contra		Detaile	ed Nons	tructura	Evalua	tion Rec	ommend	ded? (ch	eck one)	
LEVEL 2 SCREENING PERF	ORME	D?		Geol	ogic haza ficant dar	nage/de	terioratic	r on to	1 Ye	es, nons	tructural h	nazards	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2			0	the s	tructural	system	all			o, nonstr	uctural h	azards e	xist that I	may requ	ire mitig	ation, but	а
Nonstructural hazards?						and a share			de	tailed ev	aluation	is not ne	cessary			5 - Es	
	cannot h			onoraka	Il note th	o follow	ing F		20102 - 202	and the second second	nstructura				DNK	and the second	
Where information Legend: MRF = Moment-res				ener sna								and the second se			Contraction		
BR = Braced frame	and in all		SW = SI	near wall	norete		TU = Tilt u	p onreinio	prced masc	niry mitiil		= Manufa = Light m	ctured Hor etal		D = Flexib D = Rigid	le diaphra diaphragm	gm 1

Structure 78, Building 55 Photographs



Interior, Cafeteria



Interior, Exposed Concrete Column

Level 1 MODERATELY HIGH Seismicity

							ress: _		lumk		30th	Ava		Zip: 3	834	3	
							er Ident ding Na		79		-		_				_
						Use			men	tar)	50	1000					
이 아님, 말한 아이들						Lati	tude: 🕺	35,6	3317	165		ongitu	de:	-38.8	97	299	
PHOT	OGRAP	Η					0,0			-			h34'	7			
							Contract Contract Contract	: <u>C</u> M		_			ate/Tim	e:	_		
						Tota		Area (so		2	Belov 0 30 (ear(s) B		: <u>0</u> : 97	Code	Built: Year:	19746	ST EST
						Occ	upancy		embly Istrial	Comme Office Wareho	rcial	Emer. S	ervices		storic overnmer	Sheltont	er
						Soil	Type:	Hard Rock	Avg Rock	Den]D [iff S	JE [oft F		NK DNK, ass	ume Type	D.
		-1				Geo	logic H						-	s/No/DNK	Surf R		
TELET							acency:			ounding				rom Taller			NOIDINK
		L					gularitie		U Ve		pe/sever						
							erior Fal ards:	lling			Chimney	S		avy Clado pendages		eavy Ven	eer
			-			co	MMENT	S:							-		
						•	RN	11									1
		1			1												
Ethisform Gy	\sim	10	ate	teria													A. 1
Elotherform																	
SK	ETCH								es or cor								
FEMA BUILDING TYPE Do Not	W1	W1A	SCO W2	RE, MO	S2	85, A	ND FIN	S5	C1	1 SCO	II mine a la com						
Know				(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score	4.1	3.7	3.2	2.3	2.2	2.9	2.2	2.0	1.7	2.1	1.4	1.8	1.5	1.8	1.8	1.2	2.2
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.3 -0.8	-1.3 -0.8	-1.3	2010	-1.0 -0.6	-1.2 -0.8	-1.0	-0.9 -0.6	-1.0 -0.6	-1.1	-0.8 -0.5	-1.0 -0.6	-0.9	-1.0 -0.6	-1.0 -0.6	-0.8 -0.5	NA NA
Plan Irregularity, PL1	-1.3	-1.2	-1.1		-0.8	-1.0	-0.8	-0.7	-0.7	-0.9	-0.6	-0.8	-0.7	-0.7	-0.7	-0.5	NA
Pre-Code Post-Benchmark	-0.8	-0.9	-0.9		-0.5	-0.7	-0.6	-0.2	-0.4	-0.7	-0.1	-0.4	-0.3	-0.5	-0.5	-0.1	-0.3
Soil Type A or B	1.5	1.9	2.3	1.4	1.4 0.9	1.0 0.3	1.9	NA	1.9	2.1	NA	2.1	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.0	-0.1	-0.3		-0.5	0.0	0.9	0.9	0.6	0.8	0.7	0.9	0.7	0.8	0.8 -0.4	0.6	0.9
Soil Type E (> 3 stories)	-0.5	-0.8	-1.2		-0.7	NA	-0.7	-0.6	-0.6	-0.2	-0.4	NA	-0.5	-0.4	-0.4	-0.3	-0.5 NA
Minimum Score, S _{MIN}	1.6	1.2	0.8	0.5	0.5	0.9	0.5	0.5	0.3	0.3	0.3	0.3	0.2	0.3	0.3	0.2	1.4
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN	: 1:	3)≥	0,3														
EXTENT OF REVIEW				OTHER	R HAZ	ARDS			ACT	ION R	EQUIF	RED					
Exterior: A Partial Interior: None	All Sides			Are Then				4	Detail	ed Struc	tural Eva	aluation	Requir	ed?			
Interior: X None Drawings Reviewed: Yes	Visible No	L Ent	ered	Detailed										or other bu	uilding		1
Soil Type Source:					ding pote ff, if know		liess SL2	,			less that hazards						
Geologic Hazards Source:				Fallin	g hazard		aller adja	cent			naturao	present					
Contact Person: 12/A				buildi	ng ogic haza	rds or S	oil Type	F						commend			
LEVEL 2 SCREENING PERF	ORME	D?		Signi	ficant dar	nage/de				es, nonst	ructural h	nazards i	identified	that sho	uld be ev	aluated	
Yes, Final Level 2 Score, SL2			lo		tructural					o, nonstr	uctural ha	azards e	xist that	may requ	ire mitig	ation, but	a
Nonstructural hazards? Yes											aluation structura				T DNK		
Where information	cannot l	be verifie	d. scr	eener shal	I note th	e follow	ina: F	ST = Esti									
Legend: MRF = Moment-re	sisting fran	ne	RC = R	einforced co					rced maso			= Manufa				le diaphrac	100
BR = Braced fram)			hear wall			TU = Tilt u				LM :	= Light me	etal	R	D = Rigid	diaphragm	4.11

Structure 79, Building 56 Photographs



Exterior



Left is Structure 79, Right is Structure 80, Connected by Hallway

			Level 1
MODER	ATELY H	IIGH Se	ismicity

							- ALANAN	dress:	ISU Avi	mbol	, 30°		reni	1 <u></u> 2	2ip: 32	334	3	
	рнотс	GRAP	н				Use Lati Ss:	itude: 🦉	E 10 29 35 9 9 9	men 333	tory 1866	, 1	Longitu S1: O	de:		396	624	
							_	Stories:	a state of the	/e Grade	. 1	Dela				B. 114	14/01	
							Tota	al Floor		q. ft.):		200	w Grade	97		Built: Year:	1979	EST
							Occ	upancy:		embly ustrial ty	Commen Office Warehou		Emer. S School Residen			storic overnmer	□ Shelt nt	er
							Soi	І Туре:	Hard Rock	Avg Rock	Dens Soi	se St	tiff S	oft P		NK DNK, ass	ume Type	D.
	TRUE I	Stat 1 ist	1919				Geo	ologic Ha	azards:	Liquefac	tion: Yes	/No/DNł	< Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/	No/DNK
								acency:		1.00	ounding				om Taller			
- 5		1. Frank	L	CROSS OF	11.12:30	CO. CALS	Irre	gularitie	s:	Ve Pla	ertical (typan (type)	pe/sever	ity) Sk	215+1 Noran	evel A co	Inor	A	
		7		FI				erior Fal ards:	ling	D Pa	nbraced arapets ther:	Chimney	S		avy Clado bendages		eavy Ver	neer
		100	1.8	1	No. of Concession, Name	and a state of	CO	MMENT	S:									
Llother fam	SKE	тсн						Addition	al skotch	es or com	mente o	n conar	to page					
			ASIC	sco	RE, MO	DIFIE									12.7			
FEMA BUILDING TYPE	Do Not Know	W1	W1A	W2		S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	МН
Basic Score Severe Vertical Irregularity, VL1		4.1	3.7	3.2		2.2	2.9	2.2	2.0	1.7	2.1	1.4	1.8	1.5	(1.8)	1.8	1.2	2.2
Moderate Vertical Irregularity, VL1		-1.3 -0.8	-1.3 -0.8	-1.3		-1.0 -0.6	-1.2 -0.8	-1.0 -0.6	-0.9	-1.0	-1.1 -0.6	-0.8 -0.5	-1.0 -0.6	-0.9	-1.0 -0.6	-1.0 -0.6	-0.8 -0.5	NA NA
Plan Irregularity, PL1		-1.3	-1.2	-1.1	En la constante de la constante	-0.8	-1.0	-0.8	-0.7	-0.7	-0.9	-0.6	-0.8	-0.7	0.2	-0.7	-0.5	NA
Pre-Code Post-Benchmark		-0.8 1.5	-0.9 1.9	-0.9	-0.5	-0.5 1.4	-0.7	-0.6	-0.2	-0.4	-0.7	-0.1	-0.4	-0.3	0.5	-0.5	-0.1	-0.3
Soil Type A or B		0.3	0.6	0.9	0.6	0.9	1.0	1.9	NA 0.9	1.9	2.1 0.8	NA 0.7	2.1 0.9	2.4	2.1	2.1 0.8	NA 0.6	1.2 0.9
Soil Type E (1-3 stories)		0.0	-0.1	-0.3	-0.4	-0.5	0.0	-0.4	-0.5	-0.2	-0.2	-0.4	-0.5	-0.3	-0.4	-0.4	-0.3	-0.5
Soil Type E (> 3 stories) Minimum Score, Smin		-0.5	-0.8	-1.2		-0.7	NA	-0.7	-0.6	-0.6	-0.8	-0.4	NA	-0.5	-0.6	-0.7	-0.3	NA
FINAL LEVEL 1 SCORE, SLI	≥ Smin:	1.6	1.2	0.8	0.5	0.5	0.9	0.5	0.5	0.3	0.3	0.3	0.3	0.2	0.3	0.3	0.2	1.4
EXTENT OF REVIEW			VII	b	OTHER	R HAT	ARDS			ACT	ON R	FOLUE	ED	-	-	-		-
Exterior: Partia		All Sides	Aer	ial	Are Ther				4	And the second				Require	d2			
Interior: 🛛 🖾 None		/isible	Ent	A DATA AND A DATA	Detailed	Structur	al Evalu	uation?							r other bu	ilding		
Drawings Reviewed: Yes Soil Type Source:	M N	lo			Pour			nless SL2	>	Ye Ye	s, score	less that	n cut-off			and and		
Geologic Hazards Source:			-			ff, if knov Ig hazard		aller adja	cent	Ye		hazards	present					
Contact Person: NA					build	ing						ructural	Evalua	tion Pee	ommend	lad2 /ab	ook one'	
LEVEL 2 SCREENING	PEREC	RME	D2					Soil Type							that sho			
Yes, Final Level 2 Score, SL2				0	_	tructural		sterioratio	1110	No No	, nonstru	uctural ha	azards e	xist that	may requ	ire mitig	ation, but	a
Nonstructural hazards?	50-42° -			610						de	tailed eva	aluation	is not ne	cessary	1			
Teach International Internationa International International Internation											0 000				ad is	DNIK		
where more	mation c	annot b	e verifie		eener shal	I note th	e follow	vina: ES	T = Feti		, no non r unrelia						_	

Structure 80, Building 56 Photographs



Left is Structure 79, Right is Structure 80, Connected by Hallway



Exterior

Level 1 **HIGH Seismicity**

РНОТ	OGRAP	Н				Oth Buil Use Lati Ss: Scru No. Tota Add	Iding Na tude: 1,0 eener(s) Stories:	ifiers:	Abol 81 8210 M ve Grade q. ft.):	5040 615	Belov 871 ear(s) B	Longitu S1:D w Grade	ide: 4 0.35 ate/Tim 2 2 n k	e: Year	Built:		EST
							Type:	Indu Utili DA Hard	ty Avg	Office Warehou	ise	Schoo Resider	ntial, #U]E [Goft F	Gonits:	overnmer		
	-					0.00	lorio II	Rock	Rock	Soil				Soil			
		-	-			111000011110000	acency:		of the second party of the same in the second	cuon: Yes ounding				s/No/DNK			
							gularitie		N Ve		e/sever	ity) S	plit	tom Taller tovel	Ino	d	
<u>gyn</u>	~	1					erior Fal ards:	lling	🗌 U	nbraced (arapets			🗌 He	avy Clado pendages	ling or H		neer
	-	1	-	~		co	MMENT	S:		iner:			-				
		1															
				-													
			1														
		1		-													
		-				-											
SK	ETCH				_					mments o							
	B	ASIC	scol	RE, MO	DIFIE	RS, AI	ND FIN	NAL LE	EVEL	1 SCO	RE, S	L1					
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
Basic Score Severe Vertical Irregularity, VL1	3.6 -1.2	3.2 -1.2	2.9 -1.2	-1.0	2.0 -1.0	2.6	2.0	1.7	1.5	2.0	1.2	1.6	1.4	0	1.7	1.0	1.5
Moderate Vertical Irregularity, VL1	-0.7	-0.7	-0.7	-0.6	-1.0	-1.1	-1.0 -0.6	-0.8	-0.9 -0.5	-1.0	-0.7 -0.4	-1.0 -0.6	-0.9	-0.9	-0.9 -0.5	-0.7 -0.4	NA NA
Plan Irregularity, PL1	-1.1	-1.0	-1.0	-0.8	-0.7	-0.9	-0.7	-0.6	-0.6	-0.8	-0.5	-0.7	-0.6	0.7	-0.5	-0.4	NA
Pre-Code Post-Benchmark	-1.1	-1.0	-0.9	-0.6	-0.6	-0.8	-0.6	-0.2	-0.4	-0.7	-0.1	-0.5	-0.3	-0.5	-0.5	0.0	-0.1
Soil Type A or B	1.6 0.1	1.9 0.3	2.2	1.4	1.4	1.1	1.9	NA 0.5	1.9	2.1	NA 0.3	2.0	2.4	2.1	2.1	NA	1.2
Soil Type E (1-3 stories)	0.2	0.2	0.0	-0.2	-0.4	0.1	-0.1	-0.4	0.4	0.5	-0.2	-0.3	0.4	0.5 -0.1	0.5 -0.1	0.3	0.3 -0.4
Soil Type E (> 3 stories)	-0.3	-0.6	-0.9	-0.6	-0.6	NA	-0.6	-0.4	-0.5	-0.7	-0.3	NA	-0.4	-0.5	-0.6	-0.2	NA
Minimum Score, SMIN	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.5	0.3	0.3	0.3	0.2	0.2	0.3	0.3	0.2	1.0
FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MIN}$		C) ≥	Q.3)	_												
EXTENT OF REVIEW				OTHER					ACT	ION RE	QUIF	RED					
Exterior: Partial	All Sides			Are Ther	e Hazard	s That	Trigger A	A	Detaile	ed Struct	ural Eva	aluation	Require	ed?			
Drawings Reviewed: 🗌 Yes 🛛	Visible No	Ente	ered	Detailed					Ye	es, unkno	wn FEM	IA buildir	ng type o	or other bu	ilding		
Soil Type Source:					ff, if know		nless SL2	,		es, score es, other h							
Geologic Hazards Source: Contact Person:				🗌 Fallin	g hazard		aller adja	cent		0		Prosent					
_19/15	-	_		buildi Geole		ards or 9	oil Type	F	Detaile	ed Nonst	ructura	l Evalua	tion Red	commend	led? (ch	eck one)	
LEVEL 2 SCREENING PERF		D?			ficant da	mage/de	terioratio		🗌 Ye	es, nonstr	uctural h	nazards	identified	d that show	uld be ev	aluated	
	ORME																120
Yes, Final Level 2 Score, SL2	ORME		0	the s	tructural	system				o, nonstru	ctural ha	azards e	xist that	may requ	ire mitiga	ation, but	а
			(***)	the s	tructural	system			de	o, nonstru etailed eva o, no nons	aluation	is not ne	cessary		ire mitiga	ation, but	а
Yes, Final Level 2 Score, SL2			0				ing: ES	ST = Esti	de No	etailed eva	aluation structura	is not ne al hazard	cessary Is identifi	ied ዾ	DNK	ation, but	a

Structure 81, Building 57 Photographs



Exterior



Exterior

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

Level 1 **MODERATELY HIGH Seismicity**

						Othe	er Identi	Mile fiers:	$\frac{1}{82}$: Kd		Z	Zip: <u>3</u> 1	835	8	
PHO	TOGRAP	и				Use: Latit Ss:	tude: <u>3</u>	10m 5,9 171	ent 419		I	ongitu S1: 0	337		7641	254	
							ener(s)						ate/Time				-
						Tota	Stories: Il Floor / itions:				875		. 0		Built: Year:	995)	S EST
						Occ	upancy:		embly Istrial ty	Commer Office Warehou	(Emer, So School Residen	ervices tial, #Ur		storic	□ Shelt t	er
			N			Soil	Туре:	Hard Rock	Avg Rock	Dens Soi	se St	ĴD ⊑ iff S]E [ıme Type	D.
			1	7		Geo	logic Ha						201 - C	/No/DNK	Surf. Ru	ipt.: Yes/	No/DN
		\checkmark		7			icency:		D Po	ounding		Falling H	azards fr	om Taller	Adjacent	Building	
					-	Irreg	gularitie	s:		ertical (typan (type)	pe/sever Y	ity) S Ve-e	plit	level	1/m	od	
				-			erior Fal ards:	ling		nbraced arapets			Hea	avy Cladd pendages	ling or He		neer
		1					MMENT										-
							PN	1 1						o di			
							FI				A		+7	a du	10		
						0	Cha	nge	in	Cili	ngl	neig	hru	o Th	vv c		
	-	14		5				2			4	U					
				JAK	n												
						-											
	KETCH				and the second se		Addition	al skotch	es or con	amonte e	0.00000	to none					
		BASIC	sco	RE, MO	DIFIER							the second se				1	
	ot W1	W1A	W2	S1 (MRF)	S2 (BR)	S3 (LM)	S4 (RC	S5 (URM	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	MH
FEMA BUILDING TYPE Do N Kno	W		0.0	2.3	2.2		SW)				INF)	1.8		0			
Kno Basic Score	w 4.1	3.7	3.2	2.0		2.9	2.2	INF) 2.0	1.7	2.1	1.4		1.5	1.8	1.8	1.2	2.2
Kno Basic Score Severe Vertical Irregularity, VL1	4.1 -1.3	-1.3	-1.3	-1.1	-1.0	-1.2	-1.0	2.0 -0.9	-1.0	-1.1	1.4 -0.8	-1.0	-0.9	-1.0	1.8 -1.0	1.2 -0.8	2.2 NA
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	4.1 -1.3 -0.8	-1.3 -0.8	-1.3 -0.8	-1.1 -0.7	-1.0 -0.6	-1.2 -0.8	-1.0 -0.6	2.0 -0.9 -0.6	-1.0 -0.6	-1.1 -0.6	-0.8 -0.5	-1.0 -0.6	-0.9 -0.6	-1.0	-1.0 -0.6	-0.8 -0.5	NA NA
Kno Basic Score Severe Vertical Irregularity, V_{Lf} Moderate Vertical Irregularity, V_{Lf} Plan Irregularity, P_{Lf}	4.1 -1.3 -0.8 -1.3	-1.3 -0.8 -1.2	-1.3 -0.8 -1.1	-1.1 -0.7 -0.9	-1.0 -0.6 -0.8	-1.2 -0.8 -1.0	-1.0 -0.6 -0.8	2.0 -0.9 -0.6 -0.7	-1.0 -0.6 -0.7	-1.1 -0.6 -0.9	-0.8 -0.5 -0.6	-1.0 -0.6 -0.8	-0.9 -0.6 -0.7	10	-1.0 -0.6 -0.7	-0.8 -0.5 -0.5	NA NA NA
Kno Basic Score Severe Vertical Irregularity, V_{Lf} Moderate Vertical Irregularity, V_{Lf} Plan Irregularity, P_{Lf}	4.1 -1.3 -0.8	-1.3 -0.8	-1.3 -0.8	-1.1 -0.7 -0.9	-1.0 -0.6	-1.2 -0.8 -1.0 -0.7	-1.0 -0.6 -0.8 -0.6	2.0 -0.9 -0.6 -0.7 -0.2	-1.0 -0.6 -0.7 -0.4	-1.1 -0.6 -0.9 -0.7	-0.8 -0.5 -0.6 -0.1	-1.0 -0.6 -0.8 -0.4	-0.9 -0.6 -0.7 -0.3	1999	-1.0 -0.6 -0.7 -0.5	-0.8 -0.5 -0.5 -0.1	NA NA NA -0.3
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code	4.1 -1.3 -0.8 -1.3 -0.8	-1.3 -0.8 -1.2 -0.9	-1.3 -0.8 -1.1 -0.9	-1.1 -0.7 -0.9 -0.5	-1.0 -0.6 -0.8 -0.5	-1.2 -0.8 -1.0	-1.0 -0.6 -0.8	2.0 -0.9 -0.6 -0.7	-1.0 -0.6 -0.7	-1.1 -0.6 -0.9	-0.8 -0.5 -0.6	-1.0 -0.6 -0.8	-0.9 -0.6 -0.7 -0.3 2.4	-10 -10 -10 -10 -10 -10 -10 -10 -10 -10	-1.0 -0.6 -0.7 -0.5 2.1	-0.8 -0.5 -0.5 -0.1 NA	NA NA -0.3 1.2
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4	-1.0 -0.6 -0.8 -0.5 1.4	-1.2 -0.8 -1.0 -0.7 1.0	-1.0 -0.6 -0.8 -0.6 1.9	2.0 -0.9 -0.6 -0.7 -0.2 NA	-1.0 -0.6 -0.7 -0.4 1.9	-1.1 -0.6 -0.9 -0.7 2.1	-0.8 -0.5 -0.6 -0.1 NA	-1.0 -0.6 -0.8 -0.4 2.1	-0.9 -0.6 -0.7 -0.3	1999	-1.0 -0.6 -0.7 -0.5	-0.8 -0.5 -0.5 -0.1	NA NA NA -0.3
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4	-1.0 -0.6 -0.8 -0.4 2.1 0.9	-0.9 -0.6 -0.7 -0.3 2.4 0.7	-1.0 -1.0 -1.0 -0.5 -1.0 -0.5 -2.1 0.8	-1.0 -0.6 -0.7 -0.5 2.1 0.8	-0.8 -0.5 -0.5 -0.1 NA 0.6	NA NA -0.3 1.2 0.9
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3	-10 -0.5 2.1 0.8 -0.4	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4	-0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3	NA NA -0.3 1.2 0.9 -0.5
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5	-1.0 -0.5 2.1 0.8 -0.4 -0.6	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7	-0.8 -0.5 -0.1 NA 0.6 -0.3 -0.3	NA NA -0.3 1.2 0.9 -0.5 NA
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ SA EXTENT OF REVIEW	4.1 -1.3 -0.8 -1.3 -0.5 1.5 0.3 0.0 -0.5 1.6	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2) > Q	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 0.3	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2	-1.0 -0.5 -0.5 2.1 0.8 -0.4 -0.6 0.3	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7	-0.8 -0.5 -0.1 NA 0.6 -0.3 -0.3	NA NA -0.3 1.2 0.9 -0.5 NA
Kno Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{I1}$ EXTENT OF REVIEW Exterior: Partial Interior: None	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2) > Q	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazarda Structura ding pote	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That T I Evalue ntial (un	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 0.3 EQUIF tural Eva wwn FEM less that	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require	-1.0 -0.5 -0.5 2.1 0.8 -0.4 -0.6 0.3	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3	-0.8 -0.5 -0.1 NA 0.6 -0.3 -0.3	NA NA -0.3 1.2 0.9 -0.5 NA
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SI EXTENT OF REVIEW Exterior: □ Partial Interior: □ Partial Interior: □ Yes	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6 UN:	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2) > Q	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Them Detailed Detailed Detailed Detailed	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/A B HAZA B HAZA C HAZA C HAZA C HAZA	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That T al Evalue ntial (un n)	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile □ Ye	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3 ION R ed Struc es, unkno es, score es, other	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 -0.4 0.3 EQUIF tural Eva wwn FEM less than hazards	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation NA buildin n cut-off present	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require	-1.0 0.0 0.1 2.1 0.8 -0.4 -0.6 0.3 ed? or other bu	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3	-0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 -0.3 0.2	NA NA -0.3 1.2 0.9 -0.5 NA 1.4
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, VL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SI EXTENT OF REVIEW Exterior: □ Partial Interior: □ Partial Drawings Reviewed: □ Yes Soil Type Source: □ Geologic Hazards Source: □ Contact Person: □/A	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6 -0.5 1.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 > Q S Aer Ent	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Ther Detailed Poun cut-0 F Fallin Build	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazards ng ogic haza	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That T Il Evaluential (un n) s from ta	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile Ye VYe Detaile	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3 ION RI ed Struct es, unknows, score es, other other states of the states of the stat	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 0.3 EQUIF tural Eva wwn FEM less that hazards	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation NA buildin n cut-off present	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require og type o	-1.0 0.0 2.1 0.8 -0.4 -0.6 0.3 ed? or other but commend	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3	-0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 0.2	NA NA -0.3 1.2 0.9 -0.5 NA 1.4
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SI EXTENT OF REVIEW Extreior: Partial Interior: Partial Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: NA LEVEL 2 SCREENING PER	4.1 -1.3 -0.8 -0.3 -0.8 1.5 0.3 0.0 -0.5 1.6 -0.5 1.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 > 0 2 2 2 Aer Ent	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8 -1.2 0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Ther Detailed Poun cut-0 Fallin Builtin Geok Signit	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazards Structura ding pote ff, if know g hazards ng ogic haza ficant dan	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That T I Evalu: ntial (un n) s from ta rds or S mage/del	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile Ye Detaile Detaile	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3 ION RI ed Struc es, unkno es, score es, other o d Nonst	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 -0.4 -0.4 -0.3 EQUIF tural Eva wwn FEM less that hazards	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation NA buildin n cut-off present I Evaluat	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require og type o	-1.0 0.0 2.1 0.8 -0.4 -0.6 0.3 ed? or other but commend that should that should that should that should be a should	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3	-0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 -0.3 0.2	NA NA -0.3 1.2 0.9 -0.5 NA 1.4
Kno Basic Score Severe Vertical Irregularity, V_{L1} Moderate Vertical Irregularity, V_{L1} Plan Irregularity, P_{L1} Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S_{MW} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_I$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Contact Person: Contact Person: NA LEVEL 2 SCREENING PER Yes, Final Level 2 Score, S_{L2}	4.1 -1.3 -0.8 -0.3 -0.8 1.5 0.3 0.0 -0.5 1.6 -0.5 1.6 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5 -0.5	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 -0.9 1.9 0.6 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.2 -0.9 1.9 0.6 -0.1 -0.8 -0.2 -0.9 1.9 0.6 -0.1 -0.8 -0.2 -0.9 -0.1 -0.8 -0.2 -0.9 -0.1 -0.8 -0.2 -0.9 -0.1 -0.8 -0.1 -0.8 -0.1 -0.9 -0.1 -0.8 -0.2 -0.9 -0.1 -0.8 -0.2 -0.9 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8 -1.2 0.8 -1.2 -0.8 -1.2 -0.8 -1.2 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Ther Detailed Poun cut-0 Fallin Builtin Geok Signit	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazards ng ogic haza	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That T I Evalu: ntial (un n) s from ta rds or S mage/del	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile V Ye Detaile Detaile Detaile	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3 ION RI ed Struc: es, unkno es, socre es, other o d Nonst es, nonstru tailed eva	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 -0.4 -0.3 EQUIF tural Eva tural Eva Eva Eva Eva Eva Eva Eva	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation NA buildin n cut-off present I Evaluat hazards ia azards e is not ne	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require og type o tion Rec identified xist that cessary	-1.0 0.5 2.1 0.8 -0.4 -0.6 0.3 ed? or other but commend that show may requ	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3 illding	-0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 -0.3 0.2	NA NA -0.3 1.2 0.9 -0.5 NA 1.4
Kno Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SI EXTENT OF REVIEW Extreior: Partial Interior: Partial Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: NA LEVEL 2 SCREENING PER	4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.0 -0.5 1.6 UN: Visible No	-1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 -0.9 1.9 0.6 -0.1 -0.8 -0.1 -0.8 -0.1 -0.8 -0.1 -0.9 1.9 0.6 -0.1 -0.9 -0.2 -0.9 -0.2 -0.9 -0.9 -0.9 -0.9 -0.2 -0.9 -0.9 -0.9 -0.9 -0.1 -0.9 -0.9 -0.9 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.9 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1	-1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8 -1.2 0.8 -1.2 -0.8 -1.2 -0.8 -1.2 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.8 -0.9 -0.3 -1.2 -0.8 -0.8 -0.8 -0.9 -0.9 -0.3 -1.2 -0.8 -0.8 -0.9 -0.3 -1.2 -0.8 -0.8 -0.8 -0.9 -0.3 -0.2 -0.9 -0.3 -0.2 -0.8 -0.9 -0.3 -0.2 -0.9 -0.3 -0.2 -0.9 -0.3 -0.2 -0.9 -0.3 -0.2 -0.9 -0.3 -0.9 -0.3 -0.2 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.3 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.9 -0.0 -0.0	-1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed Detailed Detailed Eallin buildi Geolo Signi the st	-1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/ B Hazard Structura ding pote ff, if know g hazards ng ogic hazards ng tructural s	-1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 S That T dl Evalue ntial (un n) s from ta rds or S nage/dei ystem	-1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	-1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile V Ye Detaile Detaile Detaile	-1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3 ION RI ed Struc: es, unkno es, score es, other o o d Nonst tailed ex, no nontru tailed ex, no non	-0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 -0.4 0.3 EQUIF tural Eva wm FEM less that hazards tructural h aluation i structural	-1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation NA buildin n cut-off present I Evaluat is not ne alazards ia azards e is not ne	-0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require og type o tion Rec identified xist that cessary s identifie	-1.0 -1.0	-1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3	-0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 -0.3 0.2	NA NA -0.3 1.2 0.9 -0.5 NA 1.4

Structure 82, Building 58 Photographs



Exterior

Rapid Visual Screening of Buildings for Potential Seismic Hazards

FEMA P-154 Data Collection Form

						Oth	ding Na	ifiers: <u>Σ</u> me:				rd.		Zip: <u>3</u>	8358		
РНОТС	Use: <u>Middle School</u> Latitude: <u>351992686</u> Longitude: <u>781753493</u> Ss: <u>01965</u> Sr: <u>01339</u> Screener(s): CM Date/Time:																
						No. Tota	Stories		ve Grade q. ft.):	10000	375	y Grade	1983 S.	Year	r Built: Year:	Z 2003 Q	EST
							upancy	: Ass	embly ustrial	Commerce Office Warehou	cial	Emer. S	ervices tial, #U	States - Course	storic overnmer	Shelt	er
						Soil	Type:	Hard Rock	Avg Rock	Dens Soil	X	D C]E [oft P		NK DNK, ass	ume Type	D.
	1					Geo	logic H	azards:	Liquefac	ction: Yes/	No/DNH	(Lands	lide: Yes	/No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
							acency:	*****		ounding				om Taller			The motion - south the
				L	1	Irreg	gularitie	s:		ertical (typ an (type)	e/sever	ity) S		level,			
							erior Fal ards:	ling	ŪU	nbraced (arapets			🗆 He	avy Clado pendages	ding or H		leer
				-	1	co	MMENT	S:			-						
	1		1			-	· cł	ame	je ;)	n le	ei la	ng t	reigi	t a	101	ъру	
SK	ЕТСН						Addition			nments or							
		ASIC	sco	RE, MO	DIFIER												
FEMA BUILDING TYPE Do Not Know	W1	W1A	W2		S2 (BR)	\$3 (LM)	S4 (RC SW)	S5 (URM INF)	C1 (MRF)	C2 (SW)	C3 (URM	PC1 (TU)	PC2	RM1 (FD)	RM2 (RD)	URM	мн
Basic Score Severe Vertical Irregularity, VL1	4.1 -1.3	3.7 -1.3	3.2 -1.3	1000	2.2 -1.0	2.9 -1.2	2.2 -1.0	2.0 -0.9	1.7 -1.0	2.1	INF) 1.4 -0.8	1.8 -1.0	1.5 -0.9	1.8	1.8 -1.0	1.2 -0.8	2.2 NA
Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	-0.8	-0.8	-0.8	at the second second	-0.6	-0.8	-0.6	-0.6	-0.6	-0.6	-0.5	-0.6	-0.6	0.8	-0.6	-0.5	NA
Pre-Code	-1.3 -0.8	-1.2	-1.1		-0.8 -0.5	-1.0	-0.8	-0.7	-0.7	-0.9	-0.6 -0.1	-0.8 -0.4	-0.7 -0.3	8	-0.7	-0.5	NA
Post-Benchmark	1.5	1.9	2.3	1.4	1.4	1.0	1.9	NA	1.9	2.1	NA	2.1	2.4	-0.5	-0.5	-0.1 NA	-0.3 1.2
Soil Type A or B	0.3	0.6	0.9	0.6	0.9	0.3	0.9	0.9	0.6	0.8	0.7	0.9	0.7	0.8	0.8	0.6	0.9
Soil Type E (1-3 stories) Soil Type E (> 3 stories)	0.0	-0.1 -0.8	-0.3		-0.5 -0.7	0.0	-0.4	-0.5	-0.2	-0.2	-0.4	-0.5	-0.3	-0.4	-0.4	-0.3	-0.5
Minimum Score, Smin	1.6	1.2	0.8	0.5	-0.7	NA 0.9	-0.7 0.5	-0.6	-0.6	-0.8 0.3	-0.4	NA 0.3	-0.5	-0.6	-0.7 0.3	-0.3 0.2	NA 1.4
FINAL LEVEL 1 SCORE, SL1 ≥ SMIN:	C)70	,3)							0.0	0.0	0.0	0.2	0.0	0.5	0.2	1.4
EXTENT OF REVIEW			1	OTHER	RHAZ	ARDS			ACT	ION RE	QUIF	RED			-		
Interior: Interi	All Sides Visible No	Aer Aer		cut-o	Structura ding pote ff, if know	al Evalu ntial (ur n)	nless SL2	>		ed Struct es, unknow es, score l es, other h	wn FEM ess thar	A buildir n cut-off	and a second		uilding		
Geologic Hazards Source: Contact Person:			_		g hazard	s from ta	aller adja	cent		0							
	AND ANT		_	buildi	ng ogic haza	rds or S	oil Type	F	Detail	ed Nonst	ructural	Evalua	tion Red	commend	ded? (ch	eck one)	
LEVEL 2 SCREENING PERFORM Yes, Final Level 2 Score, SL2 Nonstructural hazards?		N N	ю	Signi Signi the s	ficant dan tructural s	nage/de system	terioratio	on to		es, nonstru o, nonstru etailed eva o, no nons	ctural ha luation i structura	azards e is not ne I hazard	xist that cessary s identifi	may required	ire mitig	valuated ation, but	a
Where information of											ole data	<u>OR</u>	DNK = D	o Not Kr	wor		
Legend: MRF = Moment-res BR = Braced frame			RC = Re SW = S	einforced co hear wall	ncrete	ļ	URM INF TU = Tilt u	= Unreinfo p	orced mase	onry infill	MH =	= Manufa = Light me	ctured Ho		D = Flexib D = Rigid	le diaphrag diaphragm	gm

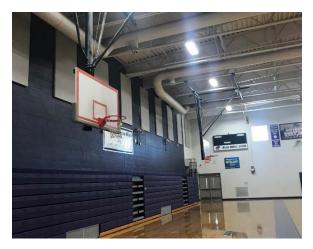
Structure 83, Building 59 Photographs



Exterior, Split Level



Interior, Split Level

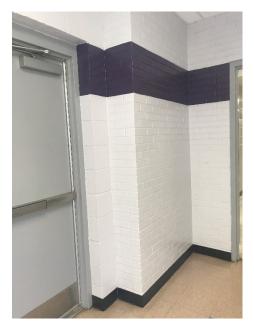


Interior, Exposed Flexible Diaphragm Roof

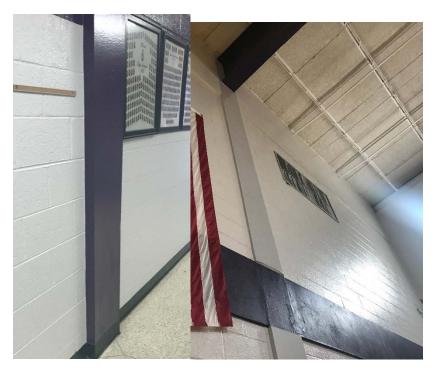
Level 1 MODERATELY HIGH Seismicity

P Voltingo Orig			Build Use: Latit Ss: Scre No. Tota Addi Occi Soil Geo Adja Irreg	er Identi ding Na : tude: eeener(s) Stories: al Floor itions: upancy: Type:	fiers: 4 me: 4 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	ye Grade q. ft.): lone embly ustrial ty B Avg Rock Liquefac ↓ Pc	: ↓ S S S S S Yes, Y Commer Office Warehou Dens Soil tion: Yes, bunding	Belov Belov Gear(s) B cial use Se St So No/DNI Do/sever	Longitu Sr: w Grade uilt: Emer, S Chool Residen JD tiff S oil S (Lands Falling H ity)	de: ate/Tim	e: Year Code I Hi Galanits: IF DI	736 Built: Year: storic overnmer NK DNK, ass Surf. Ru Adjacen Mod	201 I¶15c □ Shelt tt ume Type upt.: Yes/I t Building t,	er D. No/DNr			
This fam							ards: MMENT	s: 201	0	arapets ther:	vs	P		pendages 2WF		_	
Oldher form	SKETCH	BASIC	SCOR	RE. MO	DIFIEF					nments o		the second s	1				
FEMA BUILDING TYPE D	SKETCH E Do Not W1	BASIC W1A	SCOF W2	RE, MO	S2	RS, AN	ND FIN	S5	EVEL ·	1 SCO	RE, S	L1 PC1	PC2	RM1	RM2	URM	МН
FEMA BUILDING TYPE D	SKETCH E Do Not W1 Know	W1A	W2	S1 (MRF)	S2 (BR)	RS, AN S3 (LM)	ND FIN S4 (RC SW)	S5 (URM INF)	C1 (MRF)	1 SCO C2 (SW)	C3 (URM INF)	PC1 (TU)	PC2	(FD)	(RD)		
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1	SKETCH E Do Not Know 4.1 -1.3	W1A 3.7 -1.3	W2 3.2 -1.3	S1 (MRF) 2.3 -1.1	S2 (BR) 2.2 -1.0	RS, AN S3 (LM) 2.9 -1.2	S4 (RC SW) 2.2 -1.0	S5 (URM INF) 2.0 -0.9	EVEL ' (MRF) 1.7 -1.0	1 SCO	C3 (URM	L1 PC1				URM 1.2 -0.8	MH 2.2 NA
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	SKETCH E Do Not Know 4.1 -1.3 -0.8	W1A 3.7 -1.3 -0.8	W2 3.2 -1.3 -0.8	S1 (MRF) 2.3 -1.1 -0.7	S2 (BR) 2.2 -1.0 -0.6	RS, AN S3 (LM) 2.9 -1.2 -0.8	S4 (RC SW) 2.2 -1.0 -0.6	S5 (URM INF) 2.0 -0.9 -0.6	EVEL · C1 (MRF) 1.7 -1.0 -0.6	C2 (SW) 2.1 -1.1 -0.6	RE, S C3 (URM INF) 1.4 -0.8 -0.5	PC1 (TU) 1.8 -1.0 -0.6	PC2 1.5 -0.9 -0.6	(FD) -1.0 -0.0	(RD) 1.8 -1.0 -0.6	1.2 -0.8 -0.5	2.2 NA NA
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1	SKETCH E Do Not Know 4.1 -1.3 -0.8 -1.3	W1A 3.7 -1.3 -0.8 -1.2	W2 3.2 -1.3 -0.8 -1.1	S1 (MRF) 2.3 -1.1 -0.7 -0.9	S2 (BR) 2.2 -1.0 -0.6 -0.8	S3 (LM) 2.9 -1.2 -0.8 -1.0	ND FIN (RC SW) 2.2 -1.0 -0.6 -0.8	S5 (URM INF) 2.0 -0.9 -0.6 -0.7	EVEL · C1 (MRF) 1.7 -1.0 -0.6 -0.7	C2 (SW) 2.1 -1.1 -0.6 -0.9	RE, S (URM INF) 1.4 -0.8 -0.5 -0.6	PC1 (TU) 1.8 -1.0 -0.6 -0.8	PC2 1.5 -0.9 -0.6 -0.7	(FD) -1.0 -0.0 -0.1	(RD) 1.8 -1.0 -0.6 -0.7	1.2 -0.8 -0.5 -0.5	2.2 NA NA NA
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1	SKETCH E Do Not Know 4.1 -1.3 -0.8	W1A 3.7 -1.3 -0.8	W2 3.2 -1.3 -0.8	S1 (MRF) 2.3 -1.1 -0.7	S2 (BR) 2.2 -1.0 -0.6	RS, AN S3 (LM) 2.9 -1.2 -0.8	S4 (RC SW) 2.2 -1.0 -0.6	S5 (URM INF) 2.0 -0.9 -0.6	EVEL · C1 (MRF) 1.7 -1.0 -0.6	C2 (SW) 2.1 -1.1 -0.6	RE, S C3 (URM INF) 1.4 -0.8 -0.5	PC1 (TU) 1.8 -1.0 -0.6	PC2 1.5 -0.9 -0.6	(FD) 1.0 -1.0 -1.0 -0.7 -0.5	(RD) 1.8 -1.0 -0.6 -0.7 -0.5	1.2 -0.8 -0.5 -0.5 -0.1	2.2 NA NA NA -0.3
FEMA BUILDING TYPE D Basic Score Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B	SKETCH E Do Not Know W1 -1.3 -0.8 -1.3 -0.8 1.5 0.3	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6	W2 3.2 -1.3 -0.8 -1.1 -0.9 2.3 0.9	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9	RS, AN S3 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3	ND FIN S4 (RC SW) 2.2 -1.0 -0.6 -0.8 -0.6 1.9 0.9	S5 (URM INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9	EVEL · (MRF) 1.7 -1.0 -0.6 -0.7 -0.4	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7	RE, S (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1	PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4	PC2 1.5 -0.9 -0.6 -0.7 -0.3	(FD) -1.0 -0.0 -0.1	(RD) 1.8 -1.0 -0.6 -0.7	1.2 -0.8 -0.5 -0.5	2.2 NA NA NA
FEMA BUILDING TYPE D Basic Score Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (1-3 stories)	SKETCH E Do Not Know W1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1	W2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5	RS, AN 33 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0	ND FIN S4 (RC SW) 2.2 -1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4	JAL LI S5 (URM INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5	EVEL · (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2	RE, S/ C3 (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4	L1 PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3	(FD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3	2.2 NA NA -0.3 1.2 0.9 -0.5
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Voderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	SKETCH E Do Not Know W1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8	W2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7	RS, AN 33 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA	ND FIN S4 (RC SW) 2.2 -1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7	S5 (URM INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6	EVEL · (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8	RE, S/ C3 (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4	PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5	(FD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.6	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3	2.2 NA NA -0.3 1.2 0.9 -0.5 NA
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN Minimum Score, SMIN	SKETCH E Do Not Know W1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2	W2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 -0.8	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5	RS, AN 33 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0	ND FIN S4 (RC SW) 2.2 -1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4	JAL LI S5 (URM INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5	EVEL · (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2	RE, S/ C3 (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4	L1 PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3	(FD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3	2.2 NA NA -0.3 1.2 0.9 -0.5
FEMA BUILDING TYPE D Basic Score Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, VL1 Post-Benchmark Soil Type A or B Soil Type A or B Soil Type E (> 3 stories) Soil Type E (> 3 stories) Minimum Score, SMIN FINAL LEVEL 1 SCORE, SL1 ≥ Stories	SKETCH E Do Not Know W1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8	W2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5	RS, AN S3 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9	ND FIN S4 (RC SW) 2.2 -1.0 -0.6 -0.8 -0.6 1.9 0.9 -0.4 -0.7 0.5	S5 (URM INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6	EVEL - (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3	RE, S, (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 -0.4 -0.3	PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5	(FD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.6	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3	2.2 NA NA -0.3 1.2 0.9 -0.5 NA
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	SKETCH E Do Not Know W1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 ○≥ S □ Aer	W2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.0 0 -0.3	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 Are Ther Detailed □ Poun cut-o □ Fallin buildi	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZJ e Hazard Structura ding pote ff, if know g hazard ng	RS, AN S3 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That 1 al Evalue ential (un //n) s from ta	S4 (RC SW) 2.2 -1.0 -0.6 1.9 0.9 -0.4 -0.7 0.5	S5 CURM INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5 -0.6 0.5 -0.6 0.5 -0.6 0.5 -0.6 0.5 -0.6	EVEL - C1 (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaild ♀ Ye ♀ Ye ♀ Ye	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3	RE, S, C3 (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 0.3 EQUIF tural Eva wm FEM less that hazards	PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation A buildin n cut-off present	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require ng type of	(FD) 1.3 -1.0 -0.7 -	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3 uilding	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 0.2	2.2 NA NA -0.3 1.2 0.9 -0.5 NA 1.4
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ EXTENT OF REVIEW Exterior: Partial Interior: Interior: Partial Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING P Yes, Final Level 2 Score, SL2	SKETCH E Do Not Know 4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6 2 Smin: All Side Visible No ERFORME	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 ○≥ S □ Aer Ent	W2 3.2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.0 -0.3 -1.2 0.0 -0.3 -1.2 0.0 -0.3 -1.2 0.0 -0.3 -1.2 0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0 -0.3 -1.2 0.0 -0.0	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 Are Ther Detailed Poun cut-o □ Poun □ Geok □ Geok □ Signi	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ Structura ding pote ff, if know g hazard	RS, AN S3 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS Is That T al Evalue ential (un m) s from ta ards or S mage/de	S4 (RC SW) 2.2 -1.0 -0.6 1.9 0.9 -0.4 -0.7 0.5	S5 (URM) INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5	EVEL - C1 (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detail PY No Detail QY No Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail QY Actail Detail Actail Detail Actail Detail Actail Detail Actail Detail Actail Detail Actail Detail Actail Actail Detail Actai	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3	RE, S, C3 (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 0.3 EQUIF tural Eva wm FEM less that hazards tructural h aduation	PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 CED aluation A buildin n cut-off present I Evalua hazards azards e is not ne	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Rev identified exist that ccessary	(FD) (FD)	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3 uilding ded? (<i>ch</i> wuld be ev uire mitig	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 0.2	2.2 NA NA -0.3 1.2 0.9 -0.5 NA 1.4
FEMA BUILDING TYPE D Basic Score Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1 Plan Irregularity, PL1 Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ EXTENT OF REVIEW Exterior: Interior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING P	SKETCH E Do Not Know 4.1 -1.3 -0.8 -1.3 -0.8 1.5 0.3 0.0 -0.5 1.6 2 Smint ERFORME Former Fes	W1A 3.7 -1.3 -0.8 -1.2 -0.9 1.9 0.6 -0.1 -0.8 1.2 ○≥ S □ Aer Ent	W2 3.2 -1.3 -0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8 -1.2 0.8 -1.1 -0.9 2.3 0.9 -0.3 -1.2 0.8 -1.3 -0.9 -0.3 -1.2 0.8 -1.2 -1.2 0.8 -1.2 -	S1 (MRF) 2.3 -1.1 -0.7 -0.9 -0.5 1.4 0.6 -0.4 -0.7 0.5 Are Then Detailed □ Potailed □ Geold □ Signi the significance	S2 (BR) 2.2 -1.0 -0.6 -0.8 -0.5 1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazard ng ogic hazard ficant dar tructural s	RS, AN S3 (LM) 2.9 -1.2 -0.8 -1.0 -0.7 1.0 0.3 0.0 NA 0.9 ARDS s That T al Evalue ential (univ) s from ta ards or S mage/de system	S4 (RC SW) 2.2 -1.0 -0.6 -0.8 -0.6 1.9 -0.7 0.5	S5 (URM) INF) 2.0 -0.9 -0.6 -0.7 -0.2 NA 0.9 -0.5 -0.6 0.5 -0.6 0.5	EVEL - C1 (MRF) 1.7 -1.0 -0.6 -0.7 -0.4 1.9 0.6 -0.2 -0.6 0.3 0.3 ACT Detail P Ye No Detail Q Ye No Detail	C2 (SW) 2.1 -1.1 -0.6 -0.9 -0.7 2.1 0.8 -0.2 -0.8 0.3	RE, S, C3 (URM INF) 1.4 -0.8 -0.5 -0.6 -0.1 NA 0.7 -0.4 -0.4 0.3 EQUIF tural Eva wm FEM less that hazards tructural H cutural H cutural H cutural H cutural H cutural H	PC1 (TU) 1.8 -1.0 -0.6 -0.8 -0.4 2.1 0.9 -0.5 NA 0.3 RED aluation RED aluation A buildin n cut-off present I Evalua hazards azards e is not ne al hazard	PC2 1.5 -0.9 -0.6 -0.7 -0.3 2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Require identified exist that tracessary is identified	(FD) (FD)	(RD) 1.8 -1.0 -0.6 -0.7 -0.5 2.1 0.8 -0.4 -0.7 0.3 uilding ded? (ch vuld be ev uire mitig	1.2 -0.8 -0.5 -0.5 -0.1 NA 0.6 -0.3 -0.3 0.2	2.2 NA NA -0.3 1.2 0.9 -0.5 NA 1.4

Structure 84, Building 60 Photographs



Joint Between Structures 84 (Right) and 85 (Left)



Exposed Concrete Members

Level 1 MODERATELY HIGH Seismicity

						Add	ress: _	70		E, V	lan	1400	KS	¥.		2	
						Oth	er Identi	fiore	lan,	11	7			ip: 5	835	8	
이는 가슴을 잘 드셨는 것							ding Na		03								
							: Hi	And Address of the Ad	Sch	Ian							
									125		1	.ongitu	do. ~	XX.	73	714	7
PHO	TOGRAP	u				Ss:		941	10-	101			1,327	700	10	1.1	6
FIU	IUGRAP	n					ener(s)		M				ate/Time	and the second s			
						-	Stories		ve Grade	. [Bolow	/ Grade			Duilt.	0000	7.507
							al Floor				300 S	Grade	0		e Year:	9001	L EST
							litions:			Yes, Y			971	Cour	e i eai.		
						Occ	upancy	: Ass	embly ustrial	Commer Office Warehou	rcial	Emer. S		Children and a start of	istoric overnmer	Shelt	er
						Soil	Type:		В				itial, #Un		NK		
						1		Hard Rock	Avg Rock	Dens Soil	se St		oft P	oor <i>If</i> oll	DNK, ass	ume Type	D.
P		-				Geo	logic Ha	azards:	Liquefac	tion: Yes	/No/DNK	Lands	lide: Yes	No/DNK	Surf. Ru	upt.: Yes/I	No/DNK
		1				- Potentinini	acency:			ounding						t Building	
Addition Origin	21	1-	-			Irreg	gularitie	s:		ertical (typ an (type)	be/severi					5	
- 7		++		r			erior Fal	ling	U U	hbraced (s				eavy Ven	ieer
The second se	-					Haz	ards:			arapets ther:			App	endages	5		
						CO	MMENT	S:									Annual Protocold
							·Pa	2Sn	for	bo:	(0	20					
#Historm							1	- 1									
[] Other form			-														
S	KETCH	4010	0001		DIFIER				es or con								
FEMA BUILDING TYPE Do No		WIA	W2	RE, MO	S2	S3	S4	S5	C1	C2	RE, S_L	.1 PC1	PC2	RM1	RM2	URM	MILI
Know	'			(MRF)	(BR)	(LM)	(RC SW)	(URM INF)	(MRF)	(SW)	(URM	(TU)	102	(FD)	(RD)	URM	МН
Basic Score	4.1	3.7	3.2	2.3	2.2	2.9	2.2	2.0	1.7	2.1	(1.4)	1.8	1.5	1.8	1.8	1.2	2.2
Severe Vertical Irregularity, VL1 Moderate Vertical Irregularity, VL1	-1.3	-1.3	-1.3	-1.1	-1.0	-1.2	-1.0	-0.9	-1.0	-1.1	-0.8	-1.0	-0.9	-1.0	-1.0	-0.8	NA
woderate vertical inegularity, vLi	-0.8	-0.8	-0.8	-0.7	-0.6 -0.8	-0.8 -1.0	-0.6	-0.6	-0.6	-0.6	-0.5	-0.6	-0.6	-0.6	-0.6	-0.5	NA
Plan Irregularity Pre	-13	1 -1 2		-0.5		-1.0	-0.0			-0.9	-0.6	-0.8	-0.7	-0.7			
Plan Irregularity, PL1 Pre-Code	-1.3	-1.2	-0.9	-0.5	-05	-07	-0.6	-0.7	1993	1.	100000	04		0 E	-0.7	-0.5	NA
	-1.3 -0.8 1.5	-1.2 -0.9 1.9	-0.9 2.3	-0.5	-0.5 1.4	-0.7 1.0	-0.6 1.9	-0.2	-0.4	-0.7	100000	-0.4	-0.3	-0.5	-0.5	-0.1	-0.3
Pre-Code	-0.8	-0.9	1000	100000	1.120.000		1 2 2 2 2 2 2 2	10.52	-0.4 1.9	-0.7 2.1	AL A	2.1	2.4	2.1	-0.5 2.1	-0.1 NA	-0.3 1.2
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories)	-0.8 1.5	-0.9 1.9	2.3	1.4	1.4	1.0	1.9	-0.2 NA	-0.4	-0.7	100000				-0.5	-0.1	-0.3 1.2 0.9
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories)	-0.8 1.5 0.3 0.0 -0.5	-0.9 1.9 0.6 -0.1 -0.8	2.3 0.9 -0.3 -1.2	1.4 0.6 -0.4 -0.7	1.4 0.9 -0.5 -0.7	1.0 0.3 0.0 NA	1.9 0.9 -0.4 -0.7	-0.2 NA 0.9 -0.5 -0.6	-0.4 1.9 0.6 -0.2 -0.6	-0.7 2.1 0.8 -0.2 -0.8	-0.4 -0.4 -0.4	2.1 0.9	2.4 0.7	2.1 0.8	-0.5 2.1 0.8	-0.1 NA 0.6	-0.3 1.2
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN}	-0.8 1.5 0.3 0.0 -0.5 1.6	-0.9 1.9 0.6 -0.1	2.3 0.9 -0.3 -1.2 0.8	1.4 0.6 -0.4 -0.7 0.5	1.4 0.9 -0.5	1.0 0.3 0.0	1.9 0.9 -0.4	-0.2 NA 0.9 -0.5	-0.4 1.9 0.6 -0.2	-0.7 2.1 0.8 -0.2	0.7 -0.4	2.1 0.9 -0.5	2.4 0.7 -0.3	2.1 0.8 -0.4	-0.5 2.1 0.8 -0.4	-0.1 NA 0.6 -0.3	-0.3 1.2 0.9 -0.5
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, SL1 ≥ SM	-0.8 1.5 0.3 0.0 -0.5 1.6	-0.9 1.9 0.6 -0.1 -0.8	2.3 0.9 -0.3 -1.2 0.8	1.4 0.6 -0.4 -0.7 0.5	1.4 0.9 -0.5 -0.7 0.5	1.0 0.3 0.0 NA 0.9	1.9 0.9 -0.4 -0.7 0.5	-0.2 NA 0.9 -0.5 -0.6	-0.4 1.9 0.6 -0.2 -0.6 0.3	-0.7 2.1 0.8 -0.2 -0.8 0.3	-0.4 -0.4 -0.3	2.1 0.9 -0.5 NA 0.3	2.4 0.7 -0.3 -0.5	2.1 0.8 -0.4 -0.6	-0.5 2.1 0.8 -0.4 -0.7	-0.1 NA 0.6 -0.3 -0.3	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, S _{MIN} FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{MI}$ EXTENT OF REVIEW	-0.8 1.5 0.3 0.0 -0.5 1.6	-0.9 1.9 0.6 -0.1 -0.8 1.2	2.3 0.9 -0.3 -1.2 0.8 ≥ C	1.4 0.6 -0.4 -0.7 0.5 0.5 0.5	1.4 0.9 -0.5 -0.7 0.5	1.0 0.3 0.0 NA 0.9	1.9 0.9 -0.4 -0.7 0.5	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3	-0.7 2.1 0.8 -0.2 -0.8 0.3	-0.4 -0.4 -0.4 EQUIR	2.1 0.9 -0.5 NA 0.3	2.4 0.7 -0.3 -0.5 0.2	2.1 0.8 -0.4 -0.6 0.3	-0.5 2.1 0.8 -0.4 -0.7	-0.1 NA 0.6 -0.3 -0.3	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_{M}$ EXTENT OF REVIEW Exterior:	-0.8 1.5 0.3 0.0 -0.5 1.6 w:	-0.9 1.9 0.6 -0.1 -0.8 1.2	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 0 3 OTHEF Are There	1.4 0.9 -0.5 -0.7 0.5 R HAZ	1.0 0.3 0.0 NA 0.9	1.9 0.9 -0.4 -0.7 0.5	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3	-0.7 2.1 0.8 -0.2 -0.8 0.3	-0.1 0.7 -0.4 -0.4 0.3 EQUIR	2.1 0.9 -0.5 NA 0.3	2.4 0.7 -0.3 -0.5 0.2	2.1 0.8 -0.4 -0.6 0.3	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMN FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes	-0.8 1.5 0.3 0.0 -0.5 1.6 w:	-0.9 1.9 0.6 -0.1 -0.8 1.2	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 0.5 0.5 OTHEF Are There Detailed	1.4 0.9 -0.5 -0.7 0.5 R HAZZ	1.0 0.3 0.0 NA 0.9 ARDS s That T il Evalu	1.9 0.9 -0.4 -0.7 0.5 Trigger A ration?	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 ACTI Detaile	-0.7 2.1 0.8 -0.2 -0.8 0.3	0.7 -0.4 -0.4 -0.4 0.3 EQUIR tural Eva	2.1 0.9 -0.5 NA 0.3	2.4 0.7 -0.3 -0.5 0.2	2.1 0.8 -0.4 -0.6 0.3	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Yes	-0.8 1.5 0.3 0.0 -0.5 1.6 w:	-0.9 1.9 0.6 -0.1 -0.8 1.2	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed Poun cut-o	1.4 0.9 -0.5 -0.7 0.5 R HAZ e Hazard Structura ding pote ff, if know	1.0 0.3 0.0 NA 0.9 ARDS s That T al Evalu ntial (ur n)	1.9 0.9 -0.4 -0.7 0.5	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile	-0.7 2.1 0.8 -0.2 -0.8 0.3	0.7 -0.4 -0.4 0.3 EQUIR tural Eva wn FEM less thar	2.1 0.9 -0.5 NA 0.3 ED Iluation A buildir	2.4 0.7 -0.3 -0.5 0.2	2.1 0.8 -0.4 -0.6 0.3	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	-0.8 1.5 0.3 0.0 -0.5 1.6 w:	-0.9 1.9 0.6 -0.1 -0.8 1.2	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed Poun cut-o Fallin	1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazard:	1.0 0.3 0.0 NA 0.9 ARDS s That T al Evalu ntial (ur n)	1.9 0.9 -0.4 -0.7 0.5	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile	-0.7 2.1 0.8 -0.2 -0.8 0.3	0.7 -0.4 -0.4 0.3 EQUIR tural Eva wn FEM less thar	2.1 0.9 -0.5 NA 0.3 ED Iluation A buildir	2.4 0.7 -0.3 -0.5 0.2	2.1 0.8 -0.4 -0.6 0.3	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Yes	-0.8 1.5 0.3 0.0 -0.5 1.6 w:	-0.9 1.9 0.6 -0.1 -0.8 1.2	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Ther Detailed Poun cut-o Fallin buildi	1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazard: ng	1.0 0.3 0.0 NA 0.9 ARDS s That 1 al Evalu ntial (ur n) s from ta	1.9 0.9 -0.4 -0.7 0.5 Trigger A ation? hless S _{L2} aller adja	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile Detaile Y e Y e Y e No	-0.7 2.1 0.8 -0.2 -0.8 0.3	0.7 -0.4 -0.4 0.3 EQUIR tural Eva wn FEM less thar hazards	2.1 0.9 -0.5 NA 0.3 RED Iluation A buildin to cut-off present	2.4 0.7 -0.3 -0.5 0.2	2.1 0.8 -0.4 -0.6 0.3	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3 0.2	-0.3 1.2 0.9 -0.5 NA
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source:	-0.8 1.5 0.3 0.0 -0.5 1.6 w: Visible No	-0.9 1.9 0.6 -0.1 -0.8 1.2 Aer	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed Poun cut-o Fallin buildi Geolo	1.4 0.9 -0.5 -0.7 0.5 R HAZJ e Hazard Structura ding pote ff, if know ig hazard: ng ogic haza	1.0 0.3 0.0 NA 0.9 ARDS s That 1 al Evalu ntial (ur n) s from ta	1.9 0.9 -0.4 -0.7 0.5 Trigger <i>A</i> ation? nless <i>SL</i> 2 aller adja	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 ACT Detaile X Ye X Ye X Ye Detaile X Ye Detaile X Ye	-0.7 2.1 0.8 -0.2 -0.8 0.3 ION RE ad Struct as, unkno as, score as, other I o ad Nonst	-0.4 0.7 -0.4 -0.4 0.3 EQUIR tural Eva wm FEM less thar hazards in ructural h	2.1 0.9 -0.5 NA 0.3 EED Iluation A buildir o cut-off present Evalua azards	2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Rec	2.1 0.8 -0.4 -0.6 0.3 d? r other bit omment	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3 0.2	-0.3 1.2 0.9 -0.5 NA 1.4
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMIV FINAL LEVEL 1 SCORE, SL1 ≥ SM EXTENT OF REVIEW Exterior: Pravings Reviewed: Porawings Reviewed: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER	-0.8 1.5 0.3 0.0 -0.5 1.6 w: Visible No	-0.9 1.9 0.6 -0.1 -0.8 1.2 Aer Ent	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed Poun cut-o Fallin buildi Geolo Signi	1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazard: ng	1.0 0.3 0.0 NA 0.9 ARDS s That T al Evalu ntial (ur n) s from ta rds or S mage/de	1.9 0.9 -0.4 -0.7 0.5 Trigger <i>A</i> ation? nless <i>SL</i> 2 aller adja	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 Detaile Ye Not Detaile Ye Not Detaile Ye Not	-0.7 2.1 0.8 -0.2 -0.8 0.3 ION RE ad Struct as, unkno as, score as, other h	COLOR CO	2.1 0.9 -0.5 NA 0.3 EED Iluation A buildir ocut-off present Evalua azards e	2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Rec identified xist that i	2.1 0.8 -0.4 -0.6 0.3 d? r other bit omment	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3 0.2	-0.3 1.2 0.9 -0.5 NA 1.4
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, SL1 ≥ SM EXTENT OF REVIEW Exterior: Pravings Reviewed: Pres Soil Type Source: Geologic Hazards Source: Contact Person:	-0.8 1.5 0.3 0.0 -0.5 1.6 w: Visible No	-0.9 1.9 0.6 -0.1 -0.8 1.2 Aer	2.3 0.9 -0.3 -1.2 0.8 > C	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are There Detailed Poun cut-o Fallin buildi Geolo Signi	1.4 0.9 -0.5 -0.7 0.5 R HAZJ e Hazard Structura ding pote ff, if know ing ogic haza ficant dan	1.0 0.3 0.0 NA 0.9 ARDS s That T al Evalu ntial (ur n) s from ta rds or S mage/de	1.9 0.9 -0.4 -0.7 0.5 Trigger <i>A</i> ation? nless <i>SL</i> 2 aller adja	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 ACTI Detaile Y e X Ye C Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Detaile Deta	-0.7 2.1 0.8 -0.2 -0.8 0.3 ION RI ed Struct es, unkno es, score es, other lo o d Nonst es, nonstru o, nonstru o, nonstru	COLOR CO	2.1 0.9 -0.5 NA 0.3 RED Iluation A buildin o cut-off present Evalua azards e sa not ne	2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Rec identified xist that is	2.1 0.8 -0.4 -0.6 0.3 d? r other bin omment that sho may requ	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3 0.2	-0.3 1.2 0.9 -0.5 NA 1.4
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER Yes, Final Level 2 Score, S_{L2} Nonstructural hazards?	-0.8 1.5 0.3 0.0 -0.5 1.6 N: Visible No	-0.9 1.9 0.6 -0.1 -0.8 1.2 Aer Ent D? N N	2.3 0.9 -0.3 -1.2 0.8 2 0 8 ered	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Ther Detailed Poun cut-o Fallin buildi Geok Signii the st	1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazard: ing ogic haza ficant dan tructural s	1.0 0.3 0.0 NA 0.9 ARDS s That 1 al Evaluential (urn) s from ta rds or S mage/de system	1.9 0.9 -0.4 -0.7 0.5 0.5	-0.2 NA 0.9 -0.5 -0.6 0.5	-0.4 1.9 0.6 -0.2 -0.6 0.3 Detaile Yee X Yee X Yee X Yee X Yee X Yee X Yee X No Detaile X Yee No Detaile	-0.7 2.1 0.8 -0.2 -0.8 0.3 ION RI ed Struct es, unkno es, score es, other l o d Nonstruct es, nonstru tailed eva o, no nonstru	equip and a second sec	2.1 0.9 -0.5 NA 0.3 RED Iluation A buildir o cut-off present Evalua azards e s not ne I hazard	2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Rec identified xist that to cessary is identified	2.1 0.8 -0.4 -0.6 0.3 ed? r other but that sho may required	-0.5 2.1 0.8 -0.4 -0.7 0.3	-0.1 NA 0.6 -0.3 -0.3 0.2	-0.3 1.2 0.9 -0.5 NA 1.4
Pre-Code Post-Benchmark Soil Type A or B Soil Type E (1-3 stories) Soil Type E (> 3 stories) Minimum Score, SMW FINAL LEVEL 1 SCORE, $S_{L1} \ge S_M$ EXTENT OF REVIEW Exterior: Partial Interior: None Drawings Reviewed: Yes Soil Type Source: Geologic Hazards Source: Contact Person: LEVEL 2 SCREENING PER Yes, Final Level 2 Score, S_{L2}	-0.8 1.5 0.3 0.0 -0.5 1.6 w: 1 All Sides Visible No FORME	-0.9 1.9 0.6 -0.1 -0.8 1.2 Aer Ent D? N N De verifie	2.3 0.9 -0.3 -1.2 0.8 C ial ered 0 0 0 0 0	1.4 0.6 -0.4 -0.7 0.5 OTHEF Are Ther Detailed Poun cut-o Fallin buildi Geok Signii the st	1.4 0.9 -0.5 -0.7 0.5 R HAZ/ e Hazard Structura ding pote ff, if know g hazard: ing pogic haza ficant dan tructural s	1.0 0.3 0.0 NA 0.9 ARDS s That T I Evalu ntial (ur n) s from ta rds or S nage/de ystem s follow	1.9 0.9 -0.4 -0.7 0.5 0.5 Trigger A lation? allers SL2 aller adja terioratio terioratio	-0.2 NA 0.9 -0.5 -0.6 0.5 A > ccent F on to	-0.4 1.9 0.6 -0.2 -0.6 0.3 Detaile Yee X Yee X Yee X Yee X Yee X Yee X Yee X No Detaile X Yee No Detaile	-0.7 2.1 0.8 -0.2 -0.8 0.3 ION RE ed Struct es, unkno es, score es, other lo b d Nonstruct as, nonstruct tailed eva o, no nonstruct tailed eva o, no nonstruct	COLOR CO	2.1 0.9 -0.5 NA 0.3 ED Iluation A buildir ocut-off present Evalua azards e s not nee I hazard	2.4 0.7 -0.3 -0.5 0.2 Require ng type of tion Rec identified xist that to cessary is identified	2.1 0.8 -0.4 -0.6 0.3 r other br ommena that sho may requ ed to Not Kr	-0.5 2.1 0.8 -0.4 -0.7 0.3 uilding ded? (<i>ch</i> uild be ev uire mitig: b DNK	-0.1 NA 0.6 -0.3 -0.3 0.2	-0.3 1.2 0.9 -0.5 NA 1.4

Structure 85, Building 60 Photographs



Joint Between Structures 84 (Right) and 85 (Left)



Structure 85 is One Hallway Addition to Structure 84

REFERENCES

- Assadollahi, A. K. M. (2010). "Statistical Assessment of the Seismic Vulnerability of Mid-South Building Structures." M.S. Thesis, The University of Memphis, Memphis, TN.
- Boling, M. L. (2009). "Assessment of the Seismic Vulnerability of Shelby County Mass Emergency Shelters." M.S. Thesis, The University of Memphis, Memphis, TN.
- Chang, T.S., Pezeshk, S., Yiak, K. C., and Kung, H.T. (1995). "Seismic Vulnerability Evaluation of Essential Facilities in Memphis and Shelby County, Tennessee." *Earthquake Spectra*. 11(4), 527-544.
- Dhar, Mahesh Singh, and Cramer, Chris H. (2017). "Probabilistic Seismic and Liquefaction Hazard Analysis of the Mississippi Embayment Incorporating Nonlinear Effects." *Seismological Research Letters*. 89(1), 253-267.
- Mize, M. S. (2006). "Assessment of the Seismic Vulnerability of the University of Memphis Main Campus Buildings." M.S. Thesis, The University of Memphis, Memphis, TN.
- ESRI (2006). Quick Guide to Hazus-MH MR1. ESRI, Redlands, CA.
- FEMA (2012). Earthquake Model: Hazus-MH 2.1 User Manual. Department of Homeland Security and FEMA, Washington, D.C.
- FEMA (2012). Earthquake Model: Hazus-MH 2.1 Technical Manual. Department of Homeland Security and FEMA, Washington, D.C.
- FEMA (2019). "Hazus Analysis Levels." https://www.fema.gov/Hazus-MH-analysis-levels (September 10th, 2019).
- FEMA (2012). Hazus-MH 2.1 Advanced Engineering Building Module (AEBM) Technical and User's Manual. Department of Homeland Security and FEMA, Washington, D.C.
- FEMA P-154 (2016). "Rapid Visual Screening of Buildings for Potential Seismic Hazards: A Handbook, 3rd Edition." FEMA, Washington, D.C.
- FEMA P-155 (2015) "Rapid Visual Screening of Buildings for Potential Seismic Hazards: Supporting Documentation, 3rd Edition." FEMA, Washington, D.C.
- United States. Census Bureau. Washington: GPO, 2018. Web.

United States. Census Bureau. Washington: GPO, 2010. Web.