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Mesoporous Thin-Films for Acoustic Devices in the Gigahertz Range

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ABSTRACT: *The coherent manipulation of acoustic waves on the nanoscale usually requires multilayers with thicknesses and interface roughness defined down to the atomic monolayer. This results in expensive devices with predetermined functionality. Nanoscale mesoporous materials present high surface-to-volume ratio and tailorable mesopores, which allow the incorporation of chemical functionalization to nanoacoustics. However, the presence of pores with sizes comparable to the acoustic wavelength is intuitively perceived as a major roadblock in nanoacoustics. Here we present multilayered nanoacoustic resonators based on mesoporous SiO₂ thin-films showing acoustic resonances in the 5-100 GHz range. We characterize the acoustic response of the system using coherent phonon generation experiments. Despite resonance wavelengths comparable to the pore size, we observe for the first time well-defined acoustic resonances. Our results open the path to a promising platform for nanoacoustic sensing and reconfigurable acoustic nanodevices based on soft, inexpensive fabrication methods.*

Keywords: mesoporous thin-films, nanomechanics, nanophononics, acoustic-phonons, nanocavities, picosecond ultrasonics

Introduction

Nanophononics and nanomechanics deal with vibrations in solids where the typical frequencies are in the range spanning from few GHz up to THz.¹⁻¹² These frequencies have associated wavelengths in the 1-100 nm range, making them interesting for high-resolution acoustic imaging and sensing applications. Ultrasound imaging in the kHz-MHz has revolutionized medical applications; a similar impact can be predicted for nanoacoustic waves for non-destructive testing at the nanoscale.¹³⁻¹⁵ The design and engineering of acoustic interference devices have been traditionally based on almost atomically-flat interfaces presenting roughness only well below the phonon wavelength. The individual nanometric layer thicknesses are usually very well defined.^{5,16} Naturally adapted to these requirements, the vast majority of the works on nanophononics are based on samples grown by molecular-beam epitaxy (semiconductor, oxides),^{3,16-21} and processed using electron beam lithography (plasmonic and micropillar structures).^{6,9,22-25} This results in expensive devices with predetermined functionality.

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3 Colloidal crystals or polymer and mesoporous multilayers seem equally promising for new developments
4 in phononic crystals or metamaterials.^{4,26} For example, hypersonic one-dimensional crystals were made
5 from alternating layers of poly(methyl methacrylate) and porous silica.²⁷ as well as multilayered porous
6 silicon.²⁸ More recently, a new class of tunable hypersonic phononic crystals has been developed, based
7 on economically viable polymer-tethered colloids that present a tunable hybridization gap.²⁹ These
8 systems opened the path towards the integration of soft matter-derived materials into nanoacoustic
9 devices.

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11 The fabrication of mesoporous thin films is an efficient, cheap, and reproducible technique. Mesoporous
12 materials present great versatility for optical sensing applications^{30,31} and feature the capability of hosting
13 fluids and particles in their pores. For instance, porous networks from a wide variety of metal-oxides in
14 crystalline and amorphous states can be designed, offering tailored electronic and optical properties, like
15 ultra-low dielectric constants and photocatalytic activity.³²⁻³⁵

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17 All these characteristics could be useful in the nanoacoustic domain to develop tunable nanoacoustic
18 devices and sensing applications.³⁶ Despite its potential, the development of high-frequency acoustic
19 devices based on mesoporous materials has received little attention from the scientific community.
20 Mesoporous materials are perceived as diffuse media since their pores have sizes comparable to the
21 acoustic wavelength. Intuitively, this should prevent the fabrication of interference-based nanoacoustic
22 devices.
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25 Here we demonstrate multilayered nanoacoustic resonators based on mesoporous SiO₂ thin-films showing
26 acoustic resonances in the 5-100 GHz range. We characterize the acoustic response of the system using
27 coherent phonon generation experiments. Despite resonance wavelengths comparable to the pore size, we
28 observe well-defined acoustic resonances with Q-factors ranging from 5.0 ± 0.5 to 17 ± 2 .

30 31 **Methods**

32 33 **Sample Fabrication:**

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35 Mesoporous thin silica films were produced using the Evaporation-Induced Self-Assembly approach.³⁴
36 Silica dense and mesoporous layers were deposited onto glass substrates by dip-coating from absolute
37 ethanol-water solutions. Tetraethyl orthosilicate (Sigma-Aldrich) was used as the oxide precursor and
38 F127 block copolymer (EO)₁₀₆(PO)₇₀(EO)₁₀₆ (Sigma-Aldrich) as a mesopores template. A prehydrolysis
39 step is needed to optimize the chemical reactivity of the silica precursor. It consists of a 1-hour-reflux of
40 an initial solution of TEOS:EtOH:H₂O with a 1:5:1 molar ratio. After this step, the final solutions for
41 dense and mesoporous films are prepared by adding solvent, water and the template (when necessary) The
42 final mixture, with a molar relation of TEOS:H₂O:HCl:EtOH:F127 of 1:10:0.25:40:5x10⁻³ was aged at
43 room temperature for 48 h under agitation. A solution with the same composition but no added F127 was
44 also prepared in the same conditions, to deposit dense (*i.e.*, non-mesoporous) silica as an overlayer, or as
45 a control film.
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50 After dip-coating, the post-treatment for mesoporous layers involves an aging and thermal stabilization
51 process, that consisted of three 30-min steps, first in a chamber at room temperature and 50 % relative
52 humidity, and then thermal treatment at 60 and 130 °C, followed by a consolidation step of 2 h at 200 °C.
53 This stabilization treatment is essential to obtain ordered mesoporosity and to consolidate the mesoporous
54 film structure to keep its integrity when doing the dip-coating of the second layer.³⁷
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The thermal treatment for the dense layers consisted on a single step of 200 °C for 2 h, and for the samples with mesoporous silica, a final calcination step of 2 h at 350 °C with a 1 °C/min heating ramp is carried out, to eliminate the pores template.

The nickel cover layers were deposited by thermal evaporation using a home-made vacuum thermal evaporation system. The base pressure during evaporation was $8 \cdot 10^{-7}$ Torr. Nickel was evaporated by placing a piece of 99.95% Ni rod (Goodfellow) on a alumina covered Tungsten boat. Film thickness was measured during the deposition by monitoring the frequency change of a resonant quartz crystal.

TEM and SEM Characterization:

The TEM images were obtained in a JEOL JEM2010 FEG TEM operating at 200 kV. Samples were prepared by scratching off the films from the substrate and depositing them on FORMVAR and carbon-coated copper grids.

The SEM images were obtained in an FE-SEM Zeiss supra 40 equipped with a field emission gun. Samples were cleaved prior to imaging of the resulting vertical cross-section.

Coherent phonon generation and detection:

The coherent acoustic phonons were generated by an impulsive excitation with a pulsed laser (pump, $\lambda=758\text{nm}$, 200fs pulse duration, 80 MHz repetition rate, 275mW power). The detection was performed by implementing a Sagnac interferometer to recover the surface displacement induced by the coherent acoustic phonons. In the Sagnac interferometric detection, two counterpropagating pulses (probe, $\lambda=758\text{nm}$, 200fs pulse duration, 80 MHz repetition rate, typically 5mW power) impinge on the sample and are recombined in two photodetectors (PD1 and PD2 in Fig. 1c). The two pulses probe the optical reflectivity variation at different times and with cross polarization owing to the half-wave plate; the quarter-waveplate is rotated in order to maximize the sensitivity of the interferometer.^{38,39} Assuming there is only a surface displacement, each reflected pulse has encoded in the phase the instantaneous position of the surface. By making them interfere, we can measure this surface displacement. A careful analysis shows that the reflection and transmission through the beam splitters fixes the phase of the beams in such a way that the contributions measured by the detectors correspond to the two quadratures of the combined signal.

Numerical Simulation:

The simulations were performed using an implementation of the transfer matrix method,^{16,40} both for the electrical field and the acoustic displacements. Table 1 summarizes the material parameters used in the simulations of pump-probe spectra shown in Figure 2 (bottom row). These parameters were used in conjunction with the nominal layer thicknesses summarized in Table 2. The simulation was performed following the approach detailed in Ref. ^{16,40-42} We furthermore assumed that optical absorption and coherent phonon generation are entirely limited to the Nickel transducer layer.

	Refractive index	Speed of sound (m/s)	Mass density (g/cm ³)	Acoustic decay length (nm)
Air	1.00028	343	$1.275 \cdot 10^{-3}$	-
Nickel	2.218+4.893i	4970	8.908	-
Dense SiO ₂	1.538	5750	2.2	-
Mesoporous	1.323 (1.328 -	3156.7 (3479-3641)	2.2 (1.28-1.34)	90

	1.312)			
Glass	1.538	5750	2.2	-

Table 1: Optical and acoustic material parameters used for the simulation in Figure 2 of the main text. Ranges in brackets indicate parameters obtained by direct averaging of air and SiO₂ material properties.

Results and Discussion

Three samples were fabricated (named A, B, and C), each one consisting of three layers. A mesoporous SiO₂ thin film was first deposited on top of the substrate, and a capping layer of dense SiO₂ was deposited after a stabilization process. Subsequently, a thin film of Ni (~32 nm) was deposited by evaporation to act as a transducer in the nanoacoustic characterization experiments. The dense silica layer prevents the diffusion of the metal into the pores. We also fabricated a control sample without the mesoporous silica layer. The thickness and mesoporosity parameters of the layers, along with the withdrawal speeds, are presented in Table 2. The thickness and mesoporosity were deduced from ellipsometry measurements (SOPRA GES5E ellipsometer). All the sample preparation steps and characterization techniques are described in detail in the Methods section.

	Mesoporous layer			Dense layer	
	Thickness (nm)	Porosity (%)	Withdrawal speed (mm/s)	Thickness (nm)	Withdrawal speed (mm/s)
A	109	42	2	30	0.2
B	137	40	3	25	0.2
C	161	39	4	35	0.2
Control	-	-	-	50	1

Table 2: Samples properties and dip-coating withdrawal speeds. Errors are on the order of 5% for all the reported values.

Figure 1a shows a typical transmission electron microscopy (TEM) micrograph of mesoporous silica. In this image, the oxide walls are seen as darker areas while the lighter areas correspond to the pores. The observed pore array is compatible with the typical structure of F127-templated mesoporous oxides: a body-centered cubic array of pores, that in some cases, is slightly distorted, giving rise to regions in which the order is less evident. Figure 1b shows a typical scanning electron microscopy (SEM) image of the layer structure in sample A. A schematic sample cross-section is included as a guide to the eye. The image was taken before depositing the metallic transducer. The substrate, mesoporous, and dense layers can be clearly identified. By analyzing large cross sections, we observe that the thickness of the mesoporous layer is more uniform and better defined than the dense layer (see Supporting Information S1).

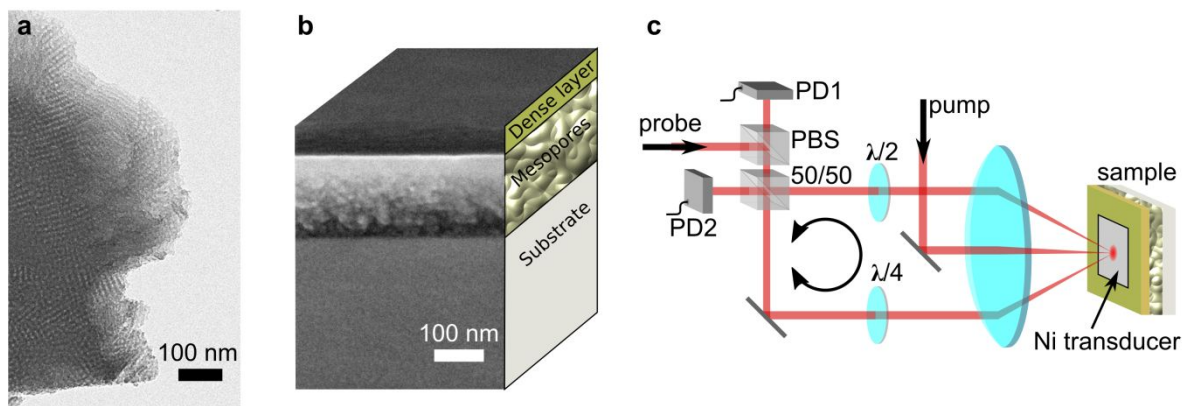


Figure 1: **a** TEM image of SiO₂ mesoporous film showing the mesopore array. **b** SEM micrograph of sample A showing the substrate, the mesoporous, and the dense layers. On the right, a schematic of the sample is presented as a guide to the eye. **c** Interferometric pump-probe setup. A strong pump pulse excites acoustic phonons through partial absorption in a Ni transducer layer. A probe pulse detects the time-resolved surface displacement using a Sagnac interferometer.^{38,39}

To acoustically characterize the samples, we performed coherent-acoustic-phonon generation experiments^{42,43} using the setup sketched in Figure 1c. This pump-probe technique allows the study of ultra-high frequency acoustic phonons traveling through a material. The time-resolved analysis of the optical reflectivity of the sample perturbed by the presence of coherent phonons enables the study of phonon dynamics on the picosecond time scale. In this technique, a short, intense laser pulse is absorbed by a transducer (Ni thin-film in our case), generating a broadband wavepacket of coherent acoustic phonons mainly by the thermoelastic effect. Usually, optically transparent materials such as SiO₂ are very inefficient optoacoustic transducers. The transducer material and thickness are crucial engineering parameters of the device. To permit the injection of phonons into the mesoporous layer, a material with an acoustic impedance sufficiently similar to that of SiO₂ is needed. Nickel meets this requirement reasonably well. Gold would represent a feasible alternative considering its acoustic impedance.

The propagation of phonons into the sample is governed by its frequency-dependent acoustic response. Upon propagation, the phonons modulate both the optical properties of the materials constituting the studied structure and the position of the interfaces. In our particular case, we implemented a Sagnac interferometric detection scheme that allowed us to recover mainly the contributions of the surface displacement to the change of optical reflectivity.^{38,39} A delayed, less intense pulse (probe) measures the instantaneous optical reflectivity as a function of the time delay between both pulses. Any resonance in the acoustic response of the sample thus induces a periodic modulation in the detected reflectivity time-trace. By performing a Fourier transform of this signal, the frequencies of the coherent acoustic phonons present in the sample can be determined. (For further details see the Methods section)

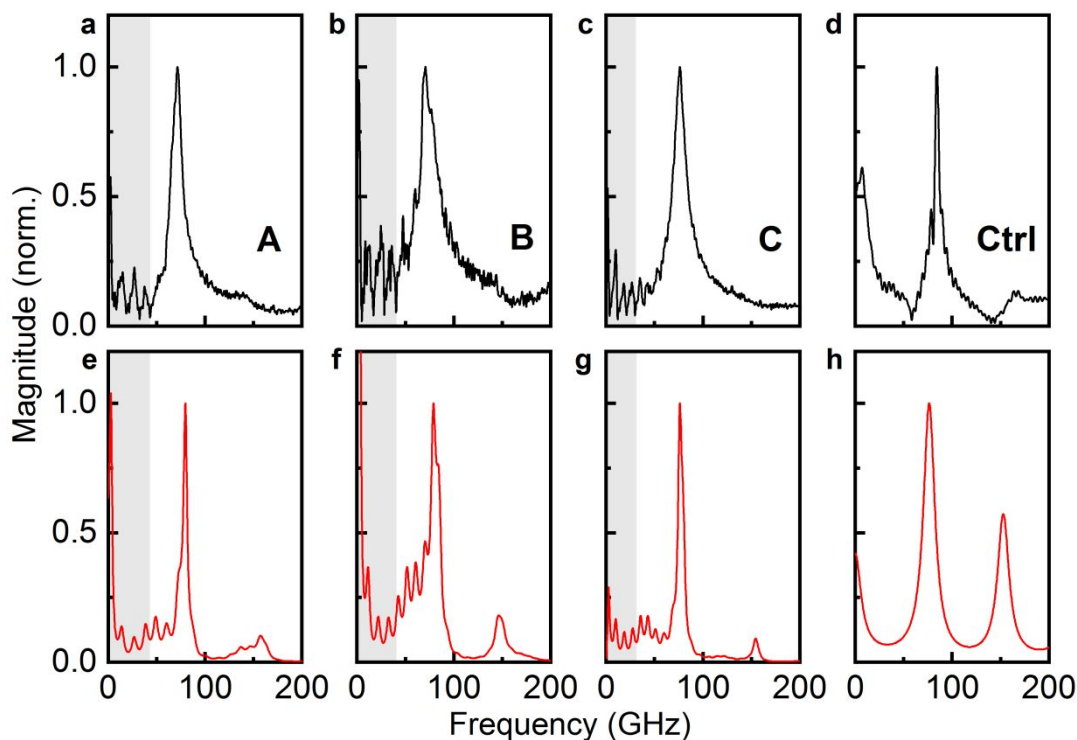


Figure 2: Coherent phonon generation spectra in mesoporous acoustic resonators. Panels a, b, c, and d correspond respectively to the samples A, B, C, and the control sample (Ctrl) without a mesoporous layer, respectively. The top row presents the measured spectra obtained from Fourier transforms of transient reflectivity traces. The bottom panels show the corresponding simulated spectra. The peaks in the low-frequency range correspond to the multiple resonances in the mesoporous thin film. The grey regions are guides to the eye, indicating the three first harmonics supported by the mesoporous layer. The intense peak appearing at 80 ± 5 GHz in all spectra corresponds to a joint acoustic resonance of the Ni transducer and the dense cap layers.

In Fig. 2, we show the results of the measured (top) and simulated (bottom) spectra of the time-resolved reflectivities in the studied mesoporous samples. In all spectra, an intense peak appears at 80 ± 5 GHz. As we will show later, this peak is associated with a joint acoustic resonance of the metal transducer and the dense cap layers. On the lower frequency side of this intense peak, we observe a series of clearly defined oscillations. They correspond to acoustic phonons confined in the mesoporous layer. The grey regions are guides to the eye, indicating the three first harmonic supported by the mesoporous film. For an isolated film, the mode spacing is purely determined by the mesoporous film thickness d_M and the speed of sound in the mesoporous material v_M via $\Delta f_M = v_M/2d_M$. As a rule of thumb, a thicker film thus results in more densely spaced resonances, *i.e.*, a larger number of visible peaks to the left of the main resonance at 80 ± 5 GHz.

For sample C (Fig. 2c), up to six harmonics of these modes can be distinguished in the experimental spectrum, at frequencies: 9.7, 18.2, 26.6, 35.0, 42.5, and 52.8 GHz with an associated error of 1%. For samples A and B, shown in Fig. 2a and 2b, respectively, the oscillations are still observable, yet less

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3 defined than in Fig. 2c. In contrast to samples A-C, the experimental spectrum of the control sample (Fig.
4 2d) does not show any of these oscillations featuring only the metal layer resonance.
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6 To account for the experimental results, we performed simulations of the pump-probe experiments using
7 a transfer matrix method.⁵ The resulting simulated spectra of surface displacement (*i.e.*, the same quantity
8 measured experimentally) are shown in Fig. 2e-h. We see a good agreement between experiments and
9 simulation in number, position, and relative height of the peaks. We also see good agreement in quality
10 factors for the low frequency resonances up to ~40GHz. For sample C the quality factors Q for the first
11 five resonances are: 5, 9, 10, 17 and 14 with an associated error of 15%. For the resonances around 80
12 GHz, the experimentally observed Q-factors are lower than in the simulations. As we show below, this is
13 likely a consequence of surface roughness.
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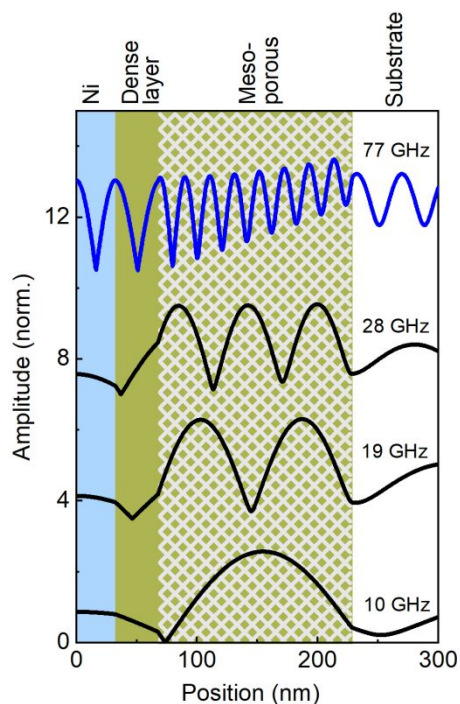
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17 The transient optical reflectivities are governed by the optical and acoustic response of the sample. That
18 is, the relevant parameters for the simulation are the geometric layer thicknesses in Table 2, together with
19 the corresponding refractive indices, speeds of sound, and mass densities. The speed of sound and the
20 mass density play different roles in the propagation of phonons in multilayer nanostructures. Essentially,
21 the speed of sound dictates the propagation phase acquired through each layer. Therefore, it determines
22 the resonance frequencies observed in Fig.2. In contrast, the acoustic impedance (product of speed of
23 sound and mass density) determines the acoustic reflectivity of each interface and hence the quality
24 factors of the acoustic resonances.
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27 For the substrate, the dense SiO₂, and the Ni layer, these parameters are well known and summarized in
28 Table 1 in the methods section. For the mesoporous layer, we derive the optical and elastic properties as
29 weighted averages of SiO₂ (dense matrix) and air (pores) with the porosity determining the relative
30 composition. These bare weighted averages are indicated between brackets in Table 1. For the multiple
31 resonances in the mesoporous films (grey regions in Fig. 2) we measure resonance frequencies which are
32 roughly consistent with the weighted average of SiO₂ and air. We find the closest agreement between
33 experiment and simulation for a refractive index of $n_{meso} = 1.32$ (at $\lambda=700\text{nm}-1000\text{nm}$) and speed of
34 sound of $v_{meso} = 3157 \text{ m/s}$. We furthermore consider the substantial acoustic losses in the mesoporous
35 material with an effective phonon decay length of $\delta_{meso} = 90 \text{ nm}$. Surprisingly, we find that the best
36 match between experiment and simulation is obtained for a mesoporous mass density of $\rho_{meso} = 2.2 \text{ g/c}$
37 m^3 , *i.e.*, the same density as the glass substrate and the dense SiO₂. That means the effective acoustic
38 impedance mismatch (determined by $Z = \rho \cdot v$) between the mesoporous material and the adjacent layers
39 is much lower than anticipated from a simple weighted impedance average. We hypothesize that this
40 effect may be a consequence of the *internal* impedance mismatch between the host material (SiO₂) and
41 the nanopores (air). Essentially, sound in the GHz-THz regime does not penetrate into air, hence
42 propagating only through the host material. This hypothesis still holds true if considering that the pores
43 are partially filled with water since the experiments were performed under ambient conditions.
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49 As a consequence, the much lower impedance mismatch between the host matrix and glass/SiO₂
50 determines the acoustic transmission from the mesoporous material into the adjacent layers. To test this
51 hypothesis, a systematic study of the variation of the mesoporous layer thickness while keeping all other
52 parameters constant should be performed. This study, however, goes beyond the scope of the present
53 manuscript.
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Figures 2d and 2h show the control sample experimental and simulated spectra, respectively. The lack of low-frequency modes is a contrasting result in comparison with the samples embedding a mesoporous layer (Fig. a-c and Fig. e-g). Additionally, we can see a slight red-shift of the simulated spectrum with respect to the experimental one. Since the metal layer was deposited during the same process for the four samples, we conclude that the difference is mainly due to the non-uniformity of the dense SiO_2 layer, and possible penetration of the metal into the oxide layer. This hypothesis is supported by SEM images, which show in general an increased roughness in the surface of the dense layer compared to the mesoporous film (Supporting Information S1). Similar results were obtained in a series of samples made out of mesoporous TiO_2 (F127) which are not shown in this work.

To further confirm that the nature of these peaks is related to the mesoporous layer, we simulated the acoustic mode profiles corresponding to the three first measured peaks in sample C. Figure 3 shows the profiles, from bottom to top, corresponding to 10, 19, 28 GHz and for the central peak at 77 GHz. The curves have been vertically shifted for clarity. We see that the modes at 10, 19, and 28 GHz indeed correspond to the first three harmonics of the confined standing wave modes in the mesoporous layer, showing 1, 2, and 3 maxima, respectively. These three modes are indicated with a grey guide to the eye in Fig. 2. For higher harmonic orders, the distribution of energy among all the layers prevents a precise localization in the mesoporous layer. For the mode at 77 GHz, there are 8 maxima within the mesoporous layer. However, most remarkably, this mode features a standing wave within the metal layer and the dense SiO_2 layer below, which together act as a resonator with an acoustic thickness of one wavelength. For this particular resonance, our simulations suggest higher quality factors than experimentally observed. We attribute this discrepancy to interface roughness and acoustic absorption in the metal. The joint mode of the transducer and SiO_2 cap layer is mostly confined at the sample surface. It is thus more susceptible to potential roughness and phonon absorption of the Nickel layer than the modes confined in the mesoporous layer.



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3 Figure 3: Numerical simulation of the mode-spatial profiles corresponding to the sample C. The curves
4 from bottom to top correspond to 10, 19, 28, and 77 GHz, respectively. The curves have been vertically
5 shifted for clarity. The three lowest-frequency modes show an evident standing wave character in the
6 mesoporous layer.
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11 For the past 20 years, there has been a growing interest in mesoporous materials due to their high surface
12 area -of the order of 1000 m²/g- the precise control in the pore size and shape, pore arrangement, and
13 tunable surface functionality.^{44,45} In particular, mesoporous thin films obtained from soft chemistry
14 methods present increasing interest as highly accessible materials with tunable structural, chemical
15 electronic and optical properties that open the path to applications in fields such as sensing, environment,
16 energy, and biomedicine.^{34,35} The optical properties of mesoporous films are easily tunable through
17 physical and chemical methods and are subject to change when exposed to the environment, which opens
18 the field of responsive thin-films acting as optical waveguides.⁴⁶ Besides, complex architectures such as
19 mesoporous multilayers can be processed as 1D photonic crystals or optical resonators with a selective
20 optical response to vapors with different chemical properties or molecular size.^{30,47,48} This application
21 exemplifies that molecular, supramolecular, or photonic information can be encoded into the structure of
22 a multilayer at several length scales⁶, or indeed combined with the plasmonic response.³⁷ The extension of
23 all these concepts into the nanoacoustic domain represents promising perspectives of this work.
24

25
26 In this work, we have shown that mesoporous materials with pore sizes of the order of 10 nm can support
27 stationary modes with frequencies in the 5-100 GHz range with Q-factors from 5 to 17 (with an
28 uncertainty of 15%). The chosen device geometry is the simplest one to demonstrate the feasibility of the
29 use of mesoporous materials in nanoacoustic applications.
30

31 We anticipate that the combination of a wall structure and pore size control with the possibility of
32 including molecular or nanosized species within the mesopores opens the gate for highly integrated
33 nanophononic devices responsive to external stimuli and to exploit confinement effects in mesopores.⁴⁹
34 This integration of physical and chemical phenomena at several length scales can be projected to
35 optoelectronics or optomechanical applications of responsive matter.⁵⁰
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40 Supporting information

41
42 **Supporting information available;** Additional sample surface characterization. This material is
43 available free of charge *via* the Internet at <http://pubs.acs.org>
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