Using [2] we found the Nash's position optimal control

$$k^* = \frac{1}{2}x^4$$
,  $m^* = \frac{1}{2}x^3$ ,  $a^* = \frac{1}{2}x^2$ ,  $w^* = \frac{1}{2}x$ ,  $p^* = 0$ 

for our forest ecosystem model with  $\begin{aligned}
Q_1 &= \alpha x^6 + \frac{1}{2} \left( \frac{1}{2} x^8 + x^6 + x^4 + x^2 \right), Q_2 &= \alpha x^6 + \frac{1}{2} \left( x^8 + \frac{1}{2} x^6 + x^4 + x^2 \right), \\
Q_3 &= \alpha x^6 + \frac{1}{2} \left( x^8 + x^6 + \frac{1}{2} x^4 + x^2 \right), Q_4 &= \alpha x^6 + \frac{1}{2} \left( x^8 + x^6 + x^4 + \frac{1}{2} x^2 \right), \\
Q_5 &= \alpha x^6 + \frac{1}{2} \left( x^8 + x^6 + x^4 + x^2 \right).
\end{aligned}$ 

For this optimal control productivity x asymptotically tends to zero with  $t \to +\infty$ , i.e. to characteristic observed value of productivity in region, but dynamics of forest ecosystem is not asymptotically stable. Since  $u_i^* > 0$  for x > 0, then we have a slowly degrading forest.

## References

1. Guts A., Volodchenkova L. Mathematical model of interrelation "vegetation-soil" in forest ecosystem // Mathematical Structures and Modelling, 2015. No. 3 (35). 56-60.

2. Lewis F.L., Vrabie D.L., Syrmos V.L. Optimal control. John Wiley & Sons, Inc., 2012. 540 p.

## DIFFERENTIAL EQUATIONS OF MOTIONS OF MULTI-AXIS SYSTEMS

S. E. Karpovich (Minsk, Belarus), R. Szczebiot (Lomza, Poland), M. M. Forutan (Minsk, Belarus)

The problem of program motion synthesis is generally solved without uniqueness and control functions realizing the motion and minimizing a functional must be obtained.

Differential equations of motions of multi-axis systems based on linear spepping motors [1, 2] can be represented as

$$\dot{x}_i = p_i(\mathbf{x}) + u_i(\mathbf{x})b_i(\mathbf{x}), \quad i = 1, \dots, n.$$
(1)

where  $\mathbf{x} = (x_1, \ldots, x_n)$  are generalized device coordinates,  $\mathbf{u} = (u_1, \ldots, u_n)$  is the control vector.

The problem consists in forming controls  $u = (t, \mathbf{x})$  such that  $u \in \mathbf{R}^r$  and corresponding solution of the system (1) satisfies the additional conditions

$$\omega_k(t, \mathbf{x}) = 0, \quad k = 1, \dots, r.$$
<sup>(2)</sup>

However, if  $\mathbf{x} = \mathbf{x}(t)$  is a solution satisfied the program (2) then  $\omega_k(t, \mathbf{x}(t)) \equiv 0, \ k = 1, \dots, r$ . Whence

$$\frac{d}{dt}\omega_k(t,\mathbf{x}(t))\equiv 0,\quad k=1,\ldots,r$$

or

$$\sum_{i=1}^{n} \left( \frac{\partial \omega_k(t, \mathbf{x})}{\partial x_i} \left( p_i(\mathbf{x}) + u_i b_i(\mathbf{x}) \right) + \frac{\partial \omega_k(t, \mathbf{x})}{\partial t} \right) \equiv 0,$$

when  $\mathbf{x}$  satisfies (2).

The last expression is equivalent to the condition

$$\sum_{i=1}^{n} \left( \frac{\partial \omega_k(t, \mathbf{x})}{\partial x_i} \left( p_i(\mathbf{x}) + u_i b_i(\mathbf{x}) \right) + \frac{\partial \omega_k(t, \mathbf{x})}{\partial t} \right) = R_k(t, \mathbf{x}, \omega_k), \quad k = 1, \dots, r,$$
(3)

where  $R_k$  is the arbitrary functions such that  $R_k(t, \mathbf{x}, 0) \equiv 0$ .

Therefore, the condition (3) is neccessary and sufficient for implementing the program (2) along solution  $\mathbf{x} = \mathbf{x}(t)$  of system (1). It can be used for calculating the neccessary controls  $u_i(t, \mathbf{x})$ , i = 1, ..., r.

As r < n, the system (3) defines the controls ambiguously, and the functional must be minimized on free controls additionally. E.g. the control optimization problem with constraints

 $u(t,\mathbf{x}) \in \tilde{U}, \quad \omega_k(t,\mathbf{x}) = 0, \quad k = 1, \dots, r$ 

can be considered for each time moment.

## References

1. Vorobiev E. I. The mechanic of industrial robots, Vol. 1, 2, 3, Moscow, Hihger School, 1988-1990 (in Russian).

2. Paul R. Modelling, trajectory, calculation and serving of computer controlled arm, Stanford, A.I.Metno 177, 1992.

## SOME GEOMETRICAL ASPECTS OF INFINITE-DIMENSIONAL DYNAMICAL SYSTEMS

V. M. Savchin (Moscow, Russia)

Denote  $U = C^2([t_0, t_1], U_1), V = C([t_0, t_1], V_1)$ , where  $U_1, V_1$  are normed linear spaces over the field of real numbers  $\mathbb{R}$ .

Let the position of infinite-dimensional dynamical system be described by the function  $u \in U$ , satisfying the conditions  $u|_{t=t_0} = u_0$ ,  $u|_{t=t_1} = u_1$ , where  $u_0, u_1$  are elements from  $U_1$ . In what it follows we will use the notations and the terminology of papers [1-3]. Let us consider the bilinear form  $\langle \cdot, \cdot \rangle : U_1 \times V_1 \to \mathbb{R}$  and the kinetic energy  $T[u, u_t] = \frac{1}{2} \langle u_t, A_u u_t \rangle$ , where  $A_u$  is a linear Gateaux differentiable operator, in general depending on u in a nonlinear way.

Let us denote  $A'_u(h;g) = \frac{d}{d\varepsilon}A_{u+\varepsilon g}h|_{\varepsilon=0}$ ,  $F[u] = \int_{t_0}^{t_1} T[u,u_t]dt$  and let  $f(t,u,u_t)$  be a density of acting proces

forces.

**Theorem 1.** There is an equality  $gradF[u] = \frac{1}{2}(A_u + A_u^*)u_{tt} + \frac{1}{2}[A'_u(u_t; u_t) + A''_u(u_t; u_t) - A''_u(u_t; \cdot)u_t],$ where  $(\cdots)^*$  is a conjugate operator.

**Theorem 2.** The operator  $k_{1u}$  of the kind

$$k_{1u}[u_t] = A'_u(u_t; u_t) + A^{*'}_u(u_t; u_t) - A'^*_u(u_t; \cdot)u_t$$

is an analog of the Christoffel symbols of the first kind.

Let us note that the equations of motion of the considered dynamical system can be presented in the form

$$\frac{1}{2}(A_u + A_u^*)u_{tt} + \frac{1}{2}k_{1u}[u_t] - f(t, u, u_t) = 0.$$
(1)

**Theorem 3.** If there exists the inverse operator  $(A_u + A_u^*)^{-1}$ , then the operator  $k_{2u}$  of the kind

$$k_{2u}[u_t] = (A_u + A_u^*)^{-1} k_{1u}[u_t]$$

defines an analog of the Christoffel symbols of the second kind.

**Theorem 4.** Operator  $\frac{D}{Dt}$  defined by

$$\frac{Du_t}{Dt} = u_{tt} + (A_u + A_u^*)^{-1} k_{1u}[u_t]$$

is an analog of the covariant derivative of  $u_t$  with respect to t.

**Consequence.** Evolutionary equation (1) can be written in the form

$$\frac{1}{2}(A_u + A_u^*)\frac{Du_t}{Dt} - f(t, u, u_t) = 0.$$

This form of equation has a special interest in connection with Riemannian geometry.

Aknowledgement. The work is supported by the Russian Foundation for Basic Research (project No. 16-01-00450a).