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33	Andrew Gleadow
34	Tel: +61 3 8344 5700
35	Email Address: <u>gleadow@unimelb.edu.au</u>
36	ORCID ID: 0000-0003-0496-0028
37	
38	Barry Kohn
39	Tel: +61 3 8344 7217
40	Email Address: <u>b.kohn@unimelb.edu.au</u>
41	ORCID: 0000-0001-5064-5454
42	()
43	Steven Reddy
44	Tel: +61 8 9266 4371
45	Fax: +61 8 9266 3153
46	Email Address: <u>s.reddy@curtin.edu.au</u>
47	ORCID: 0000-0002-4726-5714
48	
49	
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52

53 Abstract

54 This study reports a range of etching and annealing experiments to establish the optimum 55 conditions for the etching of fission tracks in monazite. The previously reported concentrated (12M) HCl etchant at 90°C, was found to cause grain loss from epoxy mounts 56 57 and high degrees of grain corrosion, as did much longer etching times at lower temperatures. Using implanted ²⁵²Cf semi-tracks, a series of experiments were performed 58 on internal prismatic faces of monazite-(Ce) crystals from the Paleozoic Harcourt 59 60 Granodiorite (Victoria, Australia) using an alternative 6M HCl etchant, also at 90°C. Step-61 etch results show optimal etching at 60-90 minutes. Further, an isothermal annealing experiment, illustrated that the degree of annealing that can be expected during etching at 62 90°C under laboratory timescales is negligible. The etching rate between grains is not 63 64 uniform, with a correlation demonstrated between over-etched grains and high U and Th concentrations. 65

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67 1. Introduction

Monazite ((Ce, La, Nd, Sm)PO₄), a rare earth (RE) bearing phosphate, is commonly found as an accessory mineral in igneous, metamorphic and vein rocks. Resistance to weathering and abrasion also makes this mineral a common detrital phase in the heavy mineral fraction of clastic sedimentary rocks (e.g. Nesse, 2012).

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73 The common occurrence of monazite, containing significant uranium (U) and thorium (Th), 74 makes it a useful mineral for isotopic and chemical dating. While the U-Th-Pb and (U-Th)/He 75 dating systems (e.g. Cottle et al., 2009 and Peterman et al., 2014) have both been 76 developed, only limited investigations have been undertaken as to its potential for fission 77 track dating. A critical first-step towards developing monazite fission track 78 thermochronology is establishing the optimum fission-track etching conditions (e.g. 79 Gleadow et al., 2002). Shukoljukov and Komarov (1970) reported the first known etching 80 method for monazite using concentrated (37%, 12M) HCl at 90°C for 45 minutes. Since that work however, little progress has been made in further investigating monazite etching 81 82 properties. Fayon (2011) reported differences in fission-track etching efficiencies that could 83 possibly be attributed to U content (i.e. lower U content required longer etching times). 84 Weise et al., (2009) reported a monazite annealing study based on the implantation of Kr 85 heavy ion tracks, using concentrated HCl at 50°C for 18 hours. This lower temperature was 86 used due to the prediction that fission tracks in monazite are likely to anneal at lower 87 temperatures than in apatite (Gleadow et al., 2004, 2005; Shipley & Fayon, 2006).

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Although the original concentrated HCl protocol etches clear fission tracks, a significant problem is the highly corrosive nature of the etchant. After 45 minutes, grains may be corroded such that fission tracks are difficult to observe and grain loss from the epoxy mount becomes common (Figure 1). This study aims to explore alternative etchants under varying concentrations and temperatures, particularly to assess whether tracks can be etched effectively at lower temperatures or concentrations to minimise grain loss.

- 95
- 96 ------ Figure 1 hereabouts -----
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98 2. Experiments and Results

99 Euhedral monazite-(Ce) crystals (~100-250 μ m in length) from the late Devonian Harcourt 100 Granodiorite (Victoria, Australia) were used in this study. This is a high-K, calc-alkaline 101 granite dated by zircon U-Pb at ~370 Ma (Clemens, 2018). Grains were mounted in epoxy 102 and polished using standard procedures (e.g. Kohn et al, 2018). Different acid and alkali etchants were tested including: HF (40%), HF (40%) : HNO₃ (34.81%) : HCl (37%) : H₂O 103 (1:2:3:6 by volume), 98% H₂SO₄, H₂SO₄ (98%) : HCl (37%) : H₂O (1:1:1 by volume), HNO₃ 104 105 (34.81%) and NaOH (0.52% and 4%) (see Fleischer et al, 1975; Wagner & Van den Haute, 106 1992 for different etchant lists). Most of these experiments were conducted at room 107 temperature but none successfully etched tracks, even for up to 10 hours. After further 108 experiments with HCl at various concentrations and temperatures, it was concluded that a 109 6M HCl (HCl (37%) : H₂O (1:1 by volume)) solution at 90°C reduced both grain corrosion and 110 grain loss from the epoxy mount, while typically etching fission tracks within 1-2 hours.

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112 **2.1 Electron Backscatter Diffraction**

Electron Backscatter Diffraction (EBSD), a microstructural characterization technique used 113 114 to analyze the structure and crystal orientation of minerals (e.g. Prior et al., 1999), was carried out to determine the dominant orientation at which monazite crystals settle when 115 116 being prepared for fission-track etching using standard mounting techniques (see Kohn et 117 al., 2019). Analyses were carried out at the Microscopy and Microanalysis Facility, Curtin 118 University, as described by Erikson et al. (2015), on two different mounts of Harcourt monazite grains. The hypothesis tested was that euhedral grains would fall on their {100} 119 120 prismatic faces, which would ensure consistency in experiments and routine fission-track 121 dating. Analysis of grains of similar orientation is important as different crystallographic orientations in monazite could have varying etching characteristics. Individual crystal 122 123 orientation measurements are shown in Figure 2 and show strongly preferred orientations 124 with the {100} plane lying parallel to the mounting substrate in 26 of 33 monazite crystals 125 (across both mounts). These measurements strongly suggest that monazite grains retaining 126 their crystal morphology will predominantly be oriented on their {100} prismatic faces 127 during mounting.

- 128
- 129 ------ Figure 2 hereabouts ------
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131 2.2 Monazite Step-Etching

132 Using the 6M HCl etchant at 90°C, a step-etch experiment was carried out to determine the optimal time needed to reveal fission tracks. Twenty monazite crystals were hand-picked 133 134 under a stereo microscope and annealed at 400°C for 18 hours in a block heater furnace to 135 remove all fossil fission tracks. Crystals were then mounted in cold-setting *Epofix* epoxy on their {100} faces, slightly ground and polished, then irradiated with collimated fission 136 fragments from a 252 Cf source for 7 hours to implant a density of ~5 x 10⁶ tracks/cm³. 137 Implanted ²⁵²Cf semi-tracks (Figure 3) were used throughout this study as the track density 138 could be easily controlled. ²⁵²Cf fission fragments have a similar mass distribution to those 139 140 of ²³⁸U and therefore serve as a useful proxy for the etching of fossil tracks (Wagner and Van 141 den haute, 1992). The implanted tracks were oriented at approximately 30° to the surface 142 and the mount was step-etched in 15-minute increments. Imagery of each monazite grain was captured in transmitted and reflected light using a 100x dry objective on a Zeiss Axio 143 Imager M1m motorised microscope fitted with a PI piezo-motor scanning stage and a 4 144 Megapixel IDS µEve USB 3 CMOS digital camera, interfaced to a control PC using *TrackWorks* 145 software (Gleadow et al., 2009). Each etching step was followed by image capture on the 146 147 same grains and this was repeated until the tracks were over-etched, after a total of 90 minutes. The track densities were then determined from the captured image stacks using 148 149 FastTracks software (Gleadow et al., 2009) as shown in Figure 4 suggesting an optimum etching time of ~75 min for this sample. 150

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156 **2.3 Isothermal Annealing Analysis**

Because monazite is thought to have a relatively low annealing temperature compared to apatite, it is important to determine whether any fission-track annealing occurs during etching at 90°C (Ure, 2010; Weise *et al.*, 2009). Therefore, an isothermal annealing experiment was carried out to evaluate the degree of annealing at 90°C under laboratory timescales. About 80 pre-annealed monazite grains were manually oriented on their {100}

----- Figure 4 hereabouts ------

162 face on double-sided tape in a control and each of five sample mounts. The samples were 163 then mounted in cold-setting *Epofix* epoxy, slightly ground and polished, and exposed to the ²⁵²Cf source as described in Section 2.2. After implantation, grains were removed from the 164 165 epoxy mount using a commercial paint-stripper. The loose grains were then annealed in 166 aluminium tubes in a *Ratek Digital* Dry Block Heater at 90°C for times of 1, 3, 7, 15 and 31 167 hours. Each aliquot was removed and quenched, then remounted by placing the grains 168 polished-face down on double-sided tape before re-embedding in epoxy. The original 169 polished surfaces were then etched in 6M HCl at 90°C for 1 hour. Although each sample 170 experienced an additional hour of exposure to this temperature during etching, it is argued below that the effective etching time is very much less. Image capture was performed as for 171 172 Section 2.2, and semi-track lengths determined on 500 tracks in each mount are presented 173 in Table 1 and Figure 5.

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------ Figure 5 hereabouts ------

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177 **2.4 Electron Microprobe Analysis**

Both the step-etch and isothermal annealing experiments showed that the etching rate between individual monazite grains was not constant, with clear variation in the degree of etching being evident within and between grains. Electron microprobe (EMP) analyses were carried out to characterise the Harcourt monazites and evaluate possible links between elemental composition and etching rate.

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Properly etched fission tracks were judged to be ~1-2 μ m in width, under-etched tracks noticeably fainter and thinner, and those over-etched noticeably wider. EMP results for all sample mounts are presented in Table 2, whereas analyses for monazite grains identified as under-etched, well-etched and over-etched, are presented in Tables 3-5, respectively.

188

189 **3. Discussion**

Using the 6M HCl etchant at 90°C, step-etching (Figure 4) shows that fission tracks on monazite {100} surfaces are progressively revealed in a similar way to that observed in other minerals. Up to about 15 minutes, no tracks are visible but by ~30 minutes the track density 193 increases rapidly, until a quasi-plateau is reached at ~60 minutes. We therefore conclude 194 that 60 minutes is a reasonable minimum time required to etch fission tracks in the 195 Harcourt monazite studied. Because of differences in etching-rate on {100} faces between 196 individual grains, however, it cannot be concluded that this etching time will be suitable for 197 every crystal. Rather, the etching required could vary between ~60-90 minutes for these 198 monazites. In cases of extreme variability, a multi-etch procedure may be needed, where 199 two or more monazite mounts are prepared and each etched for a different time between 200 60-90 minutes. This etching procedure would be important for obtaining a representative 201 distribution of ages where different intrasample grain populations occur, as is common 202 practice for zircon fission track dating (e.g. Naeser *et al.*, 1987).

203

204 Etching differences between grains can be attributed to a number of factors including 205 anisotropic etching in different crystallographic orientations, elemental composition (see 206 section 2.4) or accumulated radiation damage. It is well-known in minerals such as zircon and titanite (e.g. Gleadow, 1978; Gleadow et al., 1976) that accumulated alpha-recoil 207 208 damage causes fission tracks to etch more rapidly and more isotropically. Although 209 monazite must receive a large dose of radiation damage from U and Th alpha-decay, it has 210 never been reported in a metamict state, suggesting that it shares the same damage self-211 repair mechanism observed in apatite (e.g. Weise et al., 2009). It is also known in other 212 minerals (e.g. titanite) that accumulated alpha-recoil damage anneals at lower 213 temperatures than required for fission-track annealing (Gleadow, 1978). Assuming a similar 214 annealing relationship in monazite, with its postulated low thermal stability for fission tracks 215 (perhaps ~50°C, Weise *et al.,* 2009), suggests that alpha-recoil damage would not be stable 216 at ambient surface temperatures over geological time. As grains in this study have been pre-217 annealed to remove fossil tracks, at least some of this accumulated radiation damage is also 218 assumed to have been removed. However, the exceptionally high abundance of U and Th 219 (~0.40 - 7 wt. %) in monazite suggests that some radiation damage will still be present.

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Figure 5 shows that significant laboratory annealing of fission-tracks in monazite occurs at 90°C with mean semi-track lengths reducing rapidly before reaching a plateau at about 80% of that of the control after 15 hours. Although at first sight this experiment suggests that track shortening of ~4% might result from etching for one hour at 90°C, the actual effect is 225 likely to be much less. The earliest track etching experiments (Price & Walker, 1962) 226 demonstrated that etchants penetrate almost instantaneously along the highly-reactive 227 core of the latent track. Their TEM observations showed that in various micas, a 20% HF 228 etchant produced well-defined hollow channels in <1 second. Subsequent enlargement of these initially ~10 nm diameter tracks to optically visible dimensions (~1 μ m) occurs by 229 230 dissolving the undamaged side walls of the tracks over their full etchable range, resulting in 231 the almost parallel-sided forms typical of etched tracks in minerals, including monazite. 232 These observations imply that the time for removing the damaged cores of the latent tracks 233 is about three orders of magnitude less than that required to enlarge them sufficiently for 234 optical microscopy. Assuming a similar relationship for monazite implies that the actual exposure of the annealable latent tracks to 90°C temperatures during etching is probably 235 236 negligible, and certainly very much less than the ~4% shortening that would result if the 237 tracks had been annealed over the entire duration of etching.

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Ideally it would be desirable to find an etchant for monazite that could be used at a lower temperature, but our experiments failed to identify any satisfactory alternative. Simply lowering the temperature for a particular etchant and compensating with longer etching times, may not make any significant difference, as noted by Weise *et al.*, 2009, because the rate laws governing fission-track etching and annealing are probably similar.

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Approximately half the major elements in Harcourt Granodiorite monazite-(Ce) were higher in Si, Y, Sm, Gd, Th and U content (particularly the last two elements) in the over-etched grains compared to under-etched and well-etched grains (see Tables 3 - 5). However, no significant chemical differences were observed between under-etched and well-etched grains. Taken at face value, we conclude, with Fayon (2011), that higher U and Th concentrations in monazite influence the etching-rate, probably due to residual radiation damage that was not removed by pre-annealing at 400°C.

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253 **4.** Conclusions

Etching experiments on polished {100} faces in a set of monazite-(Ce) grains showed optimal results for fission track revelation using a 6M HCl etchant at 90°C for 60-90 minutes. Fission tracks produced were of excellent shape and the weaker etchant relative to previous work

reduced grain corrosion and loss. Differences in etching-rate between individual grains, suggests the likely influence of composition and radiation damage. In extreme cases it may be necessary to prepare more than one mount, so that different etching times can be used to account for the range of possible fission-track age components.

261

Isothermal annealing experiments at 90°C showed clear evidence of fission-track annealing over times of 1 - 31 hours, confirming that monazite has a greater sensitivity to thermal annealing than apatite. Track length reductions of ~4% for one hour were observed, up to a maximum of ~20% for 15 hours or more. However, it is concluded that etching at this temperature is highly unlikely to have any measurable effect on track lengths due to the very short time (probably seconds) taken for the etchant to penetrate along the full etchable track range.

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There is evidence for some compositional control (principally by U and Th) on track-etching rate between different monazite grains, further suggesting some control by accumulated radiation damage. Needle-shaped track shapes in different directions suggest that etching is dominantly isotropic, although further investigation, including experiments to address the extent of possible anisotropic etching behaviour, are required to fully understand monazite fission-track etching properties.

276

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- 352

- 353 Figure Captions
- 354

Figure 1. a) Unetched monazite grain from the Harcourt Granodiorite. b) Corrosion of the same grain following a 60 min etch in 12 M HCl at 50°C. Arrows highlight areas where the grain has been completely lost along with the appearance of polishing scratches, together with a change in overall appearance with increased internal reflections. Both images in reflected light.

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Figure 2. a) Typical monazite crystal morphology illustrating common crystallographic planes and axes (after mindat.org) and showing that such grains are most likely to settle on their {100} faces. b) Equal area stereographic projections from EBSD analyses of 33 grains of Harcourt monazite that were not specifically oriented during the mounting process. Each point represents the average estimate for the pole to the {100} face for a particular grain. The strong clustering shows that 26 of the 33 grains have naturally settled onto their {100} faces during mounting in epoxy resin.

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367 Figure 3. a) Shows well-etched implanted ²⁵²Cf semi-tracks dipping at ~30° to the surface in a previously 368 annealed grain of monazite from the Harcourt Granodiorite. The tracks have been implanted under vacuum and are collimated by a distance of ~2 cm from the small-area ²⁵²Cf source. For comparison b) shows the 369 370 appearance of well-etched spontaneous fission-tracks from the Harcourt monazite etched in 6M HCl at 90°C 371 for 60 min. c) Diagram showing the experimental apparatus used for exposing polished mounts to the ²⁵²Cf 372 source. The mount carrier is enclosed within a small (10 cm diameter) acrylic chamber evacuated using a 373 rotary pump (external radiation shielding not shown). The mount is attached to a rotatable sample holder to 374 control the dip of the collimated semi-tracks to the surface (I_{t} = true semi-track length).

375

Figure 4. Step-etch results of 20 Harcourt Granodiorite monazite crystals, based on a total of 15,178 ²⁵²Cf semitracks counted after 15 minute increments up to a total 90 minutes of etching in 6M HCl at 90°C. Diagram shows the observed increase in track density with increasing etching time. Tracks first become visible by ~15 minutes after which the track density increases rapidly to a quasi-plateau at ~60 minutes after which there is little change other than a continued increase in size of the etch-pits.

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Figure 5. Semi-track lengths from the Harcourt monazite 90°C isothermal annealing experiment over annealing times from 1 to 31 hours. Five hundred semi-track lengths were measured over multiple grains for each annealing step, and results show the mean semi-track length corrected for dip and refractive index. The true semi-track length represents approximately half the length of an equivalent confined fission track (Ure, 2010). The average ²⁵²Cf semi-track length decreases from 4.96 µm for the unannealed control sample, to 3.99 µm after 31 hours annealing (left axis). The right axis shows the semi-track length reduction (%), normalized to the mean length of the unannealed control sample.

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Table 1. Isothermal laboratory annealing data for ²⁵²Cf semi-tracks in Harcourt Granodiorite monazite. The annealing time, average true semi-track length (±1σ error), track

392 length reduction normalized to the mean length in the unannealed control sample (±1σ error), and number of tracks measured is shown for each sample mount. The

annealing temperature for all samples was 90°C.

394

Sample	Annealing Time (Hours)	Average Semi-Track Length (µm)	I/I ₀	Number of Tracks
ETCH-21 (Control)	0	4.96 ± 0.03	1.00	500
ETCH-22	1	4.76 ± 0.04	0.96 ± 0.010	500
ETCH-23	3	4.55 ± 0.04	0.92 ± 0.010	500
ETCH-24	7	4.33 ± 0.04	0.87 ± 0.010	500
ETCH-25	15	4.00 ± 0.04	0.81 ± 0.009	500
ETCH-26	31	3.99 ± 0.04	0.80 ± 0.009	500

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Table 2. Average composition of Harcourt Granodiorite monazite, irrespective of etching category ($\pm 2\sigma$ error) from a total of 81 EPMA analyses (with 12 standards included in the run). Ce is the dominant REE, followed by La, Nd and Sm. ThO₂ and UO₂ show averages of 6.31 wt.% and 0.50 wt.%, respectively. Measurements made with a Cameca SX50 electron microprobe using a 10 µm beam width, 50 KeV beam current, 25 KV accelerating voltage and take off angle of 40°.

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	SiO ₂	P ₂ O ₅	CaO	Y ₂ O ₃	La ₂ O ₃	Ce ₂ O ₃	Pr ₂ O ₃	Nd ₂ O ₃	Sm ₂ O ₃	Gd ₂ O ₃	ThO ₂	UO ₂	Sum Ox%
Mean	1.63 ± 0.04	27.37 ± 0.15	0.45 ± 0.02	2.39 ± 0.05	14.13 ± 0.17	28.54 ± 0.26	4.45 ± 0.11	10.61 ± 0.13	1.80 ± 0.08	1.34 ± 0.08	6.31 ± 0.11	0.50 ± 0.04	99.52

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405 **Table 3.** Elemental compositions (±2σ) of under-etched monazite grains observed in ETCH-21, ETCH-23 and ETCH-24 sample mounts from Experiment 2. Run conditions are

- 406 identical to those listed in Table 2. The average across all 26 grains shows that Ce is the dominant REE, followed by Nd > La > Sm. ThO₂ content averages 5.74 wt.% and UO₂
- 407 content averages 0.49 wt.%.

ETCH-21													
Grain Number	SiO2	P ₂ O ₅	CaO	Y ₂ O ₃	La ₂ O ₃	Ce ₂ O ₃	Pr ₂ O ₃	Nd ₂ O ₃	Sm ₂ O ₃	Gd ₂ O ₃	ThO ₂	UO ₂	Sum
													Oxide%
Grain 01	1.19 ± 0.04	27.58 ± 0.15	0.42 ± 0.02	3.85 ± 0.06	13.38 ± 0.16	27.92 ± 0.26	4.37 ± 0.11	11.00 ± 0.13	2.02 ± 0.08	1.61 ± 0.08	4.67 ± 0.10	0.50 ± 0.04	98.51
Grain 15	1.02 ± 0.04	28.11 ± 0.15	0.38 ± 0.02	2.36 ± 0.05	15.33 ± 0.18	30.37 ± 0.27	4.66 ± 0.11	10.50 ± 0.13	1.76 ± 0.08	1.37 ± 0.07	3.45 ± 0.09	0.37 ± 0.04	99.68
Grain 29	0.70 ± 0.04	28.86 ± 0.16	0.40 ± 0.02	3.22 ± 0.06	14.40 ± 0.17	29.88 ± 0.27	4.65 ± 0.11	11.07 ± 0.13	1.97 ± 0.08	1.47 ± 0.08	2.39 ± 0.08	0.54 ± 0.04	99.56
Grain 31	1.73 ± 0.04	26.75 ± 0.15	0.42 ± 0.02	2.37 ± 0.05	14.10 ± 0.17	28.09 ± 0.26	4.48 ± 0.11	10.58 ± 0.13	1.89 ± 0.08	1.42 ± 0.08	6.10 ± 0.11	0.44 ± 0.04	98.38
Grain 32	1.38 ± 0.4	28.29 ± 0.15	0.39 ± 0.02	1.99 ± 0.05	15.26 ± 0.18	29.59 ± 0.27	4.49 ± 0.11	10.86 ± 0.13	1.74 ± 0.08	1.26 ± 0.07	4.71 ± 0.10	0.37 ± 0.04	100.35
Grain 36	1.36 ± 0.04	27.93 ± 0.15	0.35 ± 0.02	2.52 ± 0.05	15.59 ± 0.18	29.82 ± 0.27	4.51 ± 0.11	10.29 ± 0.13	1.62 ± 0.08	1.17 ± 0.07	4.42 ± 0.09	0.53 ± 0.04	100.12
Grain 43	1.13 ± 0.04	28.74 ± 0.16	0.43 ± 0.02	2.55 ± 0.05	14.78 ± 0.17	29.68 ± 0.27	4.54 ± 0.11	10.68 ± 0.13	1.89 ± 0.08	1.40 ± 0.08	4.21 ± 0.09	0.43 ± 0.04	100.45
Grain 56	1.24 ± 0.04	28.92 ± 0.16	0.38 ± 0.02	2.81 ± 0.06	14.92 ± 0.17	29.47 ± 0.27	4.40 ± 0.11	10.46 ± 0.13	1.79 ± 0.08	1.41 ± 0.08	4.17 ± 0.09	0.43 ± 0.04	100.40
Grain 59	1.03 ± 0.04	29.04 ± 0.16	0.42 ± 0.02	2.14 ± 0.05	15.72 ± 0.18	30.71 ± 0.28	4.47 ± 0.11	10.52 ± 0.13	1.62 ± 0.08	1.15 ± 0.07	3.43 ± 0.09	0.38 ± 0.04	100.63
Grain 70	2.01 ± 0.04	27.21 ± 0.15	0.46 ± 0.02	2.71 ± 0.05	14.07 ± 0.17	27.86 ± 0.26	4.23 ± 0.11	10.27 ± 0.13	1.76 ± 0.08	1.30 ± 0.08	6.37 ± 0.11	0.61 ± 0.04	98.88
ETCH-23	-												
Grain 09	1.25 ± 0.04	28.03 ± 0.15	0.40 ± 0.02	2.79 ± 0.06	13.55 ± 0.16	28.71 ± 0.26	4.57 ± 0.11	11.55 ± 0.14	2.06 ± 0.08	1.56 ± 0.08	4.50 ± 0.10	0.43 ± 0.04	99.39
Grain 12	1.86 ± 0.04	27.36 ± 0.15	0.43 ± 0.02	2.75 ± 0.06	13.72 ± 0.16	28.32 ± 0.26	4.38 ± 0.11	10.87 ± 0.13	1.96 ± 0.08	1.51 ± 0.08	6.47 ± 0.11	0.74 ± 0.04	100.38
Grain 30	1.08 ± 0.04	28.27 ± 0.15	0.42 ± 0.02	1.75 ± 0.05	15.59 ± 0.18	30.48 ± 0.28	4.70 ± 0.11	10.61 ± 0.13	1.69 ± 0.08	1.12 ± 0.07	4.08 ± 0.09	0.32 ± 0.04	100.11
Grain 42	2.04 ± 0.04	26.86 ± 0.15	0.47 ± 0.02	2.29 ± 0.05	13.19 ± 0.16	27.53 ± 0.25	4.40 ± 0.11	10.73 ± 0.13	1.86 ± 0.08	1.36 ± 0.08	8.88 ± 0.12	0.52 ± 0.04	100.14
Grain 54	0.83 ± 0.04	29.38 ± 0.`16	0.35 ± 0.02	1.53 ± 0.05	15.51 ± 0.18	31.36 ± 0.28	4.59 ± 0.11	10.76 ± 0.13	1.45 ± 0.08	0.96 ± 0.07	3.77 ± 0.09	0.28 ± 0.04	100.77
Grain 62	1.54 ± 0.04	28.23 ± 0.15	0.54 ± 0.02	1.58 ± 0.05	15.25 ± 0.18	29.68 ± 0.27	4.50 ± 0.11	10.47 ± 0.13	1.66 ± 0.08	1.18 ± 0.07	5.19 ± 0.10	0.53 ± 0.04	100.34
ETCH-24													
Grain 08	1.42 ± 0.04	27.39 ± 0.15	0.43 ± 0.02	2.66 ± 0.05	14.20 ± 0.17	28.56 ± 0.26	4.50 ± 0.11	10.50 ± 0.13	1.86 ± 0.08	1.39 ± 0.08	5.57 ± 0.10	0.56 ± 0.04	99.06
Grain 09	1.59 ± 0.04	27.13 ± 0.15	0.50 ± 0.02	1.39 ± 0.05	15.22 ± 0.18	29.18 ± 0.26	4.69 ± 0.11	10.13 ± 0.12	1.49 ± 0.08	0.98 ± 0.07	6.60 ± 0.11	0.35 ± 0.04	99.25
Grain 16	1.67 ± 0.04	26.52 ± 0.15	0.40 ± 0.02	2.51 ± 0.05	14.02 ± 0.17	28.20 ± 0.26	4.54 ± 0.11	10.32 ± 0.13	1.85 ± 0.08	1.40 ± 0.08	6.21 ± 0.11	0.59 ± 0.04	98.24

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Grain 23	1.09 ± 0.04	27.43 ± 0.15	0.40 ± 0.02	2.39 ± 0.05	15.67 ± 0.18	30.97 ± 0.28	4.73 ± 0.11	10.16 ± 0.12	1.33 ± 0.08	0.84 ± 0.07	2.84 ± 0.08	0.89 ± 0.04	98.74
Grain 25	0.92 ± 0.04	27.44 ± 0.15	0.41 ± 0.02	2.50 ± 0.05	14.80 ± 0.17	30.02 ± 0.27	4.74 ± 0.11	10.51 ± 0.13	1.77 ± 0.08	1.46 ± 0.08	3.18 ± 0.09	0.38 ± 0.04	98.13
Grain 32	1.43 ± 0.04	27.38 ± 0.15	0.38 ± 0.02	1.96 ± 0.05	14.88 ± 0.17	29.74 ± 0.27	4.64 ± 0.11	10.53 ± 0.13	1.71 ± 0.08	1.22 ± 0.07	5.53 ± 0.10	0.41 ± 0.04	99.80
Grain 44	1.16 ± 0.04	28.26 ± 0.15	0.42 ± 0.02	2.16 ± 0.05	14.57 ± 0.17	30.27 ± 0.27	4.69 ± 0.11	11.03 ± 0.13	1.82 ± 0.08	1.35 ± 0.07	3.89 ± 0.09	0.40 ± 0.04	100.01
Grain 50	0.51 ± 0.03	29.05 ± 0.16	0.95 ± 0.02	2.25 ± 0.05	13.49 ± 0.16	28.23 ± 0.26	4.44 ± 0.11	11.46 ± 0.13	2.15 ± 0.08	1.62 ± 0.08	5.23 ± 0.10	0.22 ± 0.04	99.59
Grain 80	4.81 ± 0.06	22.62 ± 0.13	0.47 ± 0.02	1.83 ± 0.05	10.33 ± 0.14	22.92 ± 0.22	3.73 ± 0.10	10.40 ± 0.13	1.85 ± 0.08	1.35 ± 0.08	19.27 ± 0.18	0.80 ± 0.04	100.37
Grain 83	3.06 ± 0.05	24.9 ± 0.14	0.58 ± 0.02	2.76 ± 0.05	10.38 ± 0.14	24.09 ± 0.23	3.94 ± 0.10	11.29 ± 0.13	2.18 ± 0.08	1.63 ± 0.08	14.09 ± 0.15	0.65 ± 0.04	99.54
Mean	1.50 ± 0.04	27.60 ± 0.15	0.45 ± 0.02	2.37 ± 0.05	10.38 ± 0.17	28.91 ± 0.26	4.48 ± 0.11	10.68 ± 0.13	1.80 ± 0.08	1.33 ± 0.08	5.74 ± 0.10	0.49 ± 0.04	99.65

408 409

- 410 **Table 4.** Elemental compositions (±2σ) of well-etched monazite grains observed in ETCH-21, ETCH-23 and ETCH-24 sample mounts from Experiment 2. Run conditions are
- 411 identical to those listed in Table 2. As for the under-etched set of crystals, this set also indicates Ce as the dominant REE, followed by La, Nd and Sm (29 analyses). ThO₂ and
- 412 UO₂ average 5.60 wt.% and 0.46 wt.%, respectively.

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ETCH-21													
Grain Number	SiO ₂	P ₂ O ₅	CaO	Y ₂ O ₃	La ₂ O ₃	Ce ₂ O ₃	Pr ₂ O ₃	Nd ₂ O ₃	Sm ₂ O ₃	Gd ₂ O ₃	ThO ₂	UO ₂	Sum Oxide %
Grain 02	1.72 ± 0.04	27.38 ± 0.15	0.42 ± 0.02	2.49 ± 0.05	14.66 ± 0.17	28.75 ± 0.26	4.38 ± 0.11	10.55 ± 0.13	1.87 ± 0.08	1.35 ± 0.08	5.32 ± 0.10	0.59 ± 0.04	99.46
Grain 03	1.65 ± 0.04	26.66 ± 0.15	0.47 ± 0.02	2.47 ± 0.05	14.63 ± 0.17	28.52 ± 0.26	4.53 ± 0.11	10.24 ± 0.13	1.76 ± 0.08	1.34 ± 0.08	6.05 ± 0.11	0.57 ± 0.04	98.90
Grain 04	1.59 ± 0.04	27.02 ± 0.15	0.43 ± 0.02	2.58 ± 0.05	14.76 ± 0.17	28.80 ± 0.26	4.48 ± 0.11	10.25 ± 0.12	1.77 ± 0.08	1.26 ± 0.07	5.36 ± 0.10	0.64 ± 0.04	98.94
Grain 08	1.66 ± 0.04	27.09 ± 0.15	0.40 ± 0.02	2.61 ± 0.05	14.57 ± 0.17	29.01 ± 0.26	4.47 ± 0.11	10.31 ± 0.13	1.81 ± 0.08	1.32 ± 0.08	5.64 ± 0.10	0.55 ± 0.04	99.43
Grain 10	2.36 ± 0.04	26.40 ± 0.15	0.45 ± 0.02	2.08 ± 0.05	13.71 ± 0.16	27.46 ± 0.25	4.29 ± 0.11	10.47 ± 0.13	1.83 ± 0.08	1.29 ± 0.08	9.02 ± 0.12	0.49 ± 0.04	99.85
Grain 17	1.17 ± 0.04	27.99 ± 0.15	0.42 ± 0.02	1.36 ± 0.05	16.42 ± 0.19	30.67 ± 0.28	4.81 ± 0.11	10.14 ± 0.12	1.49 ± 0.08	0.92 ± 0.07	4.24 ± 0.09	0.28 ± 0.04	99.90
Grain 20	1.37 ± 0.04	27.95 ± 0.15	0.36 ± 0.02	2.54 ± 0.05	14.55 ± 0.17	29.49 ± 0.27	4.56 ± 0.11	10.83 ± 0.13	1.81 ± 0.08	1.34 ± 0.08	4.15 ± 0.09	0.47 ± 0.04	99.41
Grain 27	1.24 ± 0.04	27.59 ± 0.15	0.41 ± 0.02	2.70 ± 0.05	14.95 ± 0.17	29.84 ± 0.27	4.54 ± 0.11	10.41 ± 0.13	1.76 ± 0.08	1.27 ± 0.07	3.92 ± 0.09	0.46 ± 0.04	99.09
Grain 28	1.13 ± 0.04	28.71 ± 0.15	0.43 ± 0.02	0.78 ± 0.05	16.59 ± 0.19	31.62 ± 0.28	4.87 ± 0.11	10.41 ± 0.13	1.41 ± 0.08	0.75 ± 0.07	3.96 ± 0.09	0.27 ± 0.04	100.92
Grain 30	1.21 ± 0.04	28.61 ± 0.15	0.64 ± 0.02	1.05 ± 0.05	15.97 ± 0.18	30.76 ± 0.28	4.79 ± 0.11	10.34 ± 0.13	1.33 ± 0.08	0.67 ± 0.07	5.16 ± 0.10	0.31 ± 0.04	100.85
ETCH-23													
Grain 26	1.77 ± 0.04	27.52 ± 0.15	0.42 ± 0.02	2.82 ± 0.06	13.88 ± 0.17	28.38 ± 0.26	4.41 ± 0.11	10.40 ± 0.13	1.89 ± 0.08	1.40 ± 0.08	6.33 ± 0.11	0.59 ± 0.04	99.81

Grain 27	1	1.89 ± 0.04	27.56 ± 0.15	0.47 ± 0.02	2.31 ± 0.05	14.27 ± 0.17	28.62 ± 0.26	4.42 ± 0.11	10.28 ± 0.13	1.70 ± 0.08	1.28 ± 0.07	7.18 ± 0.11	0.57 ± 0.04	100.55
Grain 31	1	1.02 ± 0.04	29.02 ± 0.16	0.46 ± 0.02	2.56 ± 0.05	14.21 ± 0.17	29.69 ± 0.27	4.51 ± 0.11	10.87 ± 0.13	1.89 ± 0.08	1.46 ± 0.08	4.44 ± 0.10	0.47 ± 0.04	100.59
Grain 41	1	1.96 ± 0.04	27.34 ± 0.15	0.44 ± 0.02	2.09 ± 0.05	13.77 ± 0.16	28.25 ± 0.26	4.40 ± 0.11	10.79 ± 0.13	1.83 ± 0.08	1.29 ± 0.07	7.41 ± 0.12	0.47 ± 0.04	100.03
Grain 44		0.81 ± 0.04	28.99 ± 0.15	0.45 ± 0.02	1.12 ± 0.05	15.72 ± 0.18	31.56 ± 0.28	4.78 ± 0.11	10.47 ± 0.13	1.38 ± 0.08	0.86 ± 0.07	3.75 ± 0.09	0.47 ± 0.04	100.35
Grain 48		0.88 ± 0.04	28.58 ± 0.16	0.36 ± 0.02	3.37 ± 0.06	15.28 ± 0.18	30.31 ± 0.27	4.58 ± 0.11	10.30 ± 0.13	1.50 ± 0.08	1.18 ± 0.07	2.49 ± 0.08	0.58 ± 0.04	99.42
Grain 53	1	1.93 ± 0.04	27.69 ± 0.15	0.55 ± 0.02	2.85 ± 0.06	12.97 ± 0.17	26.91 ± 0.25	4.25 ± 0.11	10.84 ± 0.13	2.01 ± 0.08	1.53 ± 0.08	8.31 ± 0.12	0.64 ± 0.04	100.50
Grain 55		1.43 ± 0.04	28.31 ± 0.15	0.40 ± 0.02	2.53 ± 0.05	14.72 ± 0.16	29.24 ± 0.27	4.50 ± 0.11	10.44 ± 0.13	1.79 ± 0.08	1.39 ± 0.08	4.83 ± 0.10	0.45 ± 0.04	100.03
Grain 56	C	1.64 ± 0.04	28.28 ± 0.15	0.50 ± 0.02	1.41 ± 0.05	15.18 ± 0.18	29.63 ± 0.27	4.46 ± 0.11	10.30 ± 0.13	1.53 ± 0.08	1.08 ± 0.07	6.50 ± 0.11	0.32 ± 0.04	100.85
Grain 59		1.04 ± 0.04	28.9 ± 0.16	0.33 ± 0.01	2.10 ± 0.05	16.22 ± 0.18	30.67 ± 0.28	4.72 ± 0.11	11.64 ± 0.12	1.34 ± 0.08	0.83 ± 0.07	3.26 ± 0.09	0.50 ± 0.04	100.03
ETCH-24	U.													
Grain 02	(0.92 ± 0.04	28.12 ± 0.15	0.46 ± 0.02	1.00 ± 0.05	16.66 ± 0.19	30.98 ± 0.28	4.85 ± 0.11	9.98 ± 0.12	1.29 ± 0.07	0.75 ± 0.07	3.73 ± 0.09	0.25 ± 0.04	98.98
Grain 03	1	1.75 ± 0.04	27.01 ± 0.15	0.41 ± 0.02	2.25 ± 0.05	13.18 ± 0.16	27.26 ± 0.25	4.38 ± 0.11	11.23 ± 0.13	2.07 ± 0.08	1.52 ± 0.08	7.69 ± 0.12	0.38 ± 0.04	99.13
Grain 05	1	1.94 ± 0.04	26.29 ± 0.15	0.48 ± 0.02	1.82 ± 0.05	13.75 ± 0.16	27.80 ± 0.26	4.51 ± 0.11	10.65 ± 0.13	1.76 ± 0.08	1.30 ± 0.07	7.85 ± 0.12	0.45 ± 0.04	98.59
Grain 06	đ	1.31 ± 0.04	27.21 ± 0.15	0.46 ± 0.02	2.57 ± 0.05	14.40 ± 0.17	28.77 ± 0.26	4.50 ± 0.11	10.29 ± 0.12	1.79 ± 0.08	1.37 ± 0.08	5.56 ± 0.10	0.50 ± 0.04	98.73
Grain 11	L L	0.56 ± 0.04	28.51 ± 0.15	0.88 ± 0.02	1.54 ± 0.05	14.37 ± 0.17	28.38 ± 0.26	4.63 ± 0.11	11.66 ± 0.14	1.79 ± 0.08	1.30 ± 0.07	4.97 ± 0.10	0.20 ± 0.04	98.78
Grain 15		1.44 ± 0.04	26.99 ± 0.15	0.39 ± 0.02	2.81 ± 0.06	14.16 ± 0.17	28.46 ± 0.26	4.46 ± 0.11	10.51 ± 0.13	1.79 ± 0.08	1.47 ± 0.08	5.64 ± 0.10	0.57 ± 0.04	98.70
Grain 26		1.46 ± 0.04	27.39 ± 0.15	0.44 ± 0.02	2.21 ± 0.05	14.48 ± 0.17	29.44 ± 0.27	4.71 ± 0.11	10.61 ± 0.13	1.78 ± 0.08	1.36 ± 0.08	5.31 ± 0.10	0.43 ± 0.04	99.62
Grain 27	1	1.90 ± 0.04	26.05 ± 0.15	0.47 ± 0.02	2.24 ± 0.05	13.34 ± 0.16	27.58 ± 0.25	4.46 ± 0.11	10.51 ± 0.13	1.85 ± 0.08	1.45 ± 0.08	8.69 ± 0.12	0.48 ± 0.04	99.02
Mean	1	1.46 ± 0.04	27.68 ± 0.15	0.46 ± 0.02	2.15 ± 0.05	14.69 ± 0.17	29.17 ± 0.27	4.54 ± 0.11	10.51 ± 0.13	1.71 ± 0.08	1.23 ± 0.08	5.60 ± 0.10	0.46 ± 0.04	99.66

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415 **Table 5.** Elemental compositions (±2σ) of over-etched monazite grains observed in ETCH-21, ETCH-23 and ETCH-24 sample mounts from Experiment 2. Run conditions are

416 identical to those listed in Table 2. Based on these analyses from 27 grains, 6 elements in this category (including Si, Y, Sm, Gd, Th and U) show higher concentrations than

417 in the under-etched and well- etched categories. ThO₂ is noticeably higher by over 2 wt.%, averaging 7.81 wt.%. UO₂ with an average of 0.58 wt.%, is also noticeably

418 higher.

419

ETCH-21													
Grain Number	SiO2	P ₂ O ₅	CaO	Y ₂ O ₃	La ₂ O ₃	Ce ₂ O ₃	Pr ₂ O ₃	Nd ₂ O ₃	Sm ₂ O ₃	Gd ₂ O ₃	ThO ₂	UO ₂	Sum Oxide %
Grain 19	3.43 ± 0.05	25.38 ± 0.14	0.46 ± 0.02	2.76 ± 0.06	10.70 ± 0.14	24.13 ± 0.23	3.96 ± 0.10	11.56 ± 0.14	2.31 ± 0.09	1.66 ± 0.08	12.45 ± 0.15	0.67 ± 0.04	99.46

Grain 24	1.35 ± 0.04	27.87 ± 0.15	0.48 ± 0.02	2.83 ± 0.06	13.26 ± 0.16	27.90 ± 0.26	4.37 ± 0.11	11.21 ± 0.13	2.08 ± 0.08	1.69 ± 0.08	5.84 ± 0.10	0.44 ± 0.04	99.32
Grain 38	1.83 ± 0.04	27.18 ± 0.15	0.84 ± 0.02	3.30 ± 0.06	11.57 ± 0.15	25.22 ± 0.24	4.20 ± 0.11	11.44 ± 0.13	2.20 ± 0.08	1.83 ± 0.08	9.09 ± 0.13	0.59 ± 0.04	99.29
Grain 39	2.24 ± 0.05	27.28 ± 0.15	0.24 ± 0.01	1.52 ± 0.05	15.71 ± 0.18	29.60 ± 0.27	4.35 ± 0.11	9.87 ± 0.12	1.36 ± 0.08	0.81 ± 0.07	7.44 ± 0.12	0.62 ± 0.04	101.05
Grain 44	2.43 ± 0.05	26.16 ± 0.15	0.33 ± 0.02	1.72 ± 0.05	14.89 ± 0.17	28.43 ± 0.26	4.39 ± 0.11	9.71 ± 0.12	1.41 ± 0.08	0.96 ± 0.07	8.40 ± 0.12	0.68 ± 0.04	99.51
ETCH-23													
Grain 11	1.53 ± 0.04	27.84 ± 0.15	0.39 ± 0.02	2.47 ± 0.05	13.27 ± 0.16	28.20 ± 0.26	4.45 ± 0.11	11.38 ± 0.13	2.02 ± 0.08	1.64 ± 0.08	6.32 ± 0.11	0.50 ± 0.04	100.01
Grain 28	2.24 ± 0.04	27.08 ± 0.15	0.53 ± 0.02	3.17 ± 0.06	12.18 ± 0.15	25.97 ± 0.24	4.16 ± 0.11	10.88 ± 0.13	2.08 ± 0.08	1.69 ± 0.08	9.45 ± 0.13	0.58 ± 0.04	100.02
Grain 34	2.93 ± 0.05	24.44 ± 0.14	0.35 ± 0.02	1.92 ± 0.05	13.96 ± 0.17	27.15 ± 0.25	4.24 ± 0.11	9.55 ± 0.12	1.48 ± 0.08	1.03 ± 0.07	10.40 ± 0.13	0.90 ± 0.04	98.35
Grain 51	1.91 ± 0.04	27.36 ± 0.15	0.45 ± 0.02	2.61 ± 0.05	14.04 ± 0.17	28.29 ± 0.26	4.34 ± 0.11	10.04 ± 0.12	1.81 ± 0.08	1.37 ± 0.08	7.32 ± 0.11	0.59 ± 0.04	100.14
Grain 57	2.78 ± 0.05	25.61 ± 0.14	0.46 ± 0.02	1.76 ± 0.05	12.61 ± 0.16	25.87 ± 0.24	4.06 ± 0.11	10.88 ± 0.13	1.85 ± 0.08	1.29 ± 0.07	11.71 ± 0.14	0.49 ± 0.04	99.39
Grain 67	1.48 ± 0.04	27.53 ± 0.15	0.51 ± 0.02	3.94 ± 0.06	12.66 ± 0.16	26.54 ± 0.25	4.23 ± 0.11	10.94 ± 0.13	2.15 ± 0.08	1.87 ± 0.08	6.44 ± 0.11	0.53 ± 0.04	98.82
Grain 77	1.99 ± 0.04	26.14 ± 0.15	0.51 ± 0.02	3.11 ± 0.06	12.48 ± 0.15	26.24 ± 0.25	4.21 ± 0.11	10.42 ± 0.13	2.04 ± 0.08	1.68 ± 0.08	8.66 ± 0.12	0.66 ± 0.04	98.13
Grain 78	2.17 ± 0.04	27.16 ± 0.15	0.45 ± 0.02	2.87 ± 0.06	12.90 ± 0.16	26.73 ± 0.25	4.21 ± 0.11	10.96 ± 0.13	2.19 ± 0.08	1.62 ± 0.08	7.45 ± 0.12	0.60 ± 0.04	99.29
ETCH-24	3												
Grain 04	3.17 ± 0.05	24.46 ± 0.14	0.53 ± 0.02	2.00 ± 0.05	11.47 ± 0.15	24.93 ± 0.24	4.08 ± 0.11	11.13 ± 0.13	2.03 ± 0.08	1.45 ± 0.08	13.13 ± 0.15	0.55 ± 0.04	98.94
Grain 12	1.36 ± 0.04	27.65 ± 0.15	0.48 ± 0.02	2.34 ± 0.05	13.82 ± 0.16	28.39 ± 0.26	4.46 ± 0.11	10.99 ± 0.13	1.86 ± 0.08	1.44 ± 0.08	5.75 ± 0.10	0.46 ± 0.04	98.99
Grain 19	2.34 ± 0.04	25.44 ± 0.14	0.37 ± 0.02	2.57 ± 0.05	12.52 ± 0.15	26.61 ± 0.25	4.18 ± 0.11	10.63 ± 0.13	1.92 ± 0.08	1.54 ± 0.08	10.07 ± 0.13	0.63 ± 0.04	98.83
Grain 20	0.86 ± 0.04	27.76 ± 0.15	0.41 ± 0.02	3.37 ± 0.06	14.47 ± 0.17	29.35 ± 0.27	4.63 ± 0.11	10.6 ± 0.13	1.82 ± 0.08	1.47 ± 0.08	3.35 ± 0.09	0.42 ± 0.04	98.53
Grain 22	0.77 ± 0.04	27.95 ± 0.15	0.43 ± 0.02	3.50 ± 0.06	14.08 ± 0.17	29.16 ± 0.26	4.52 ± 0.11	10.72 ± 0.13	1.90 ± 0.08	1.65 ± 0.08	3.04 ± 0.09	0.43 ± 0.04	98.15
Grain 42	1.83 ± 0.04	26.83 ± 0.15	0.46 ± 0.02	2.46 ± 0.05	14.51 ±0.17	28.73 ± 0.26	4.34 ± 0.11	9.86 ± 0.12	1.70 ± 0.08	1.29 ± 0.07	6.75 ± 0.11	0.58 ± 0.04	99.34
Grain 47	1.63 ± 0.04	27.00 ± 0.15	0.45 ± 0.02	2.86 ± 0.06	13.92 ± 0.16	28.78 ± 0.26	4.42 ± 0.11	10.37 ± 0.13	1.90 ± 0.08	1.48 ± 0.08	5.98 ± 0.11	0.53 ± 0.04	99.32
Grain 48	1.85 ± 0.04	26.88 ± 0.15	0.48 ± 0.02	2.72 ± 0.05	13.67 ± 0.16	28.20 ± 0.26	4.39 ± 0.11	10.60 ± 0.13	1.86 ± 0.08	1.34 ± 0.08	6.70 ± 0.11	0.62 ± 0.04	99.32
Grain 55	1.61 ± 0.04	27.36 ± 0.15	0.43 ± 0.02	2.25 ± 0.05	14.61 ± 0.17	28.75 ± 0.26	4.52 ± 0.11	10.54 ± 0.13	1.85 ± 0.08	1.41 ± 0.07	5.93 ± 0.10	0.49 ± 0.04	99.75
Grain 63	1.72 ± 0.04	26.47 ± 0.15	0.51 ± 0.02	4.37 ± 0.06	11.71 ± 0.15	25.64 ± 0.24	4.06 ± 0.11	10.82 ± 0.13	2.21 ± 0.08	1.94 ± 0.08	8.03 ± 0.12	0.68 ± 0.04	98.15
Mean	1.98 ± 0.04	26.73 ± 0.15	0.46 ± 0.02	2.71 ± 0.05	13.26 ± 0.16	27.34 ± 0.25	4.29 ± 0.11	10.66 ± 0.13	1.91 ± 0.08	1.48 ± 0.08	7.81 ± 0.12	0.58 ± 0.04	99.22



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Jones, S; Gleadow, A; Kohn, B; Reddy, SM

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