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**Production of polymeric carbon solids (PCS) and their application as adsorbents
for potentially toxic elements in water and wastewater**

By

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degree of

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DEDICATION

This dissertation is sincerely dedicated to my mother Mohubedu Dorcus Mabu for her encouragement and support towards my studies.



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“Be strong and take heart, all you who hope in the LORD”

Psalm 31:24 (NIV)

DECLARATION

I Dance Mabu hereby declare that this dissertation titled '**Production of polymeric carbon solids (PCS) and their application as adsorbents for potentially toxic elements in water and wastewater**' is my own work carried out as a Master's student at the University of Johannesburg. All the sources that I have used or quoted have been indicated and acknowledged by means of references and this work has not been submitted before for any other degree to any other institution.



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Date

ABSTRACT

Heavy metals are considered as some of the toxic substances that pollute water globally, as such, they tend to have negative effects on living organisms. Manganese and chromium metals exist in different oxidation states which some are dangerous at their low concentrations and they can cause dementia, anxiety, and ataxia, and nervous system problems. The main aim of this study was to produce PCS, hydrochar, and AC from wood chips and evaluate their potential as adsorbents for toxic inorganic ions from aqueous systems. The hydrochar was successfully produced by hydrothermal carbonization (HTC) of eucalyptus wood chips in the presence of a catalyst, water as a solvent, under the temperature of 240 °C and pressure of 4 bars. The activated carbon (AC) was generated by heating the hydrochar in a tube furnace, this process is called annealing. The hydrochar and AC were used as adsorbents for the removal of Mn(II) and Cr(VI) from aqueous solutions. The hydrochar and AC were characterized by sophisticated analytical instruments such as scanning electron microscopy (SEM), transmission electron microscopy (TEM), x-ray powder diffraction (XRD), thermogravimetric analyzer (TGA), energy dispersive x-ray (EDX), Dynamic Light Scattering (DLS), Fourier transform infrared spectroscopy (FTIR), and Brunauer–Emmett–Teller (BET). The parameters explored on the adsorption of Mn(II) and Cr(VI) include initial metal ion concentration, temperature, solution pH, contact time, and adsorbent dose. The filtrates of Mn(II) and Cr(VI) were analyzed by using the flame atomic absorption spectrometer (FAAS). Based on the results obtained from the characterization techniques, the surface area, average diameter, and pore volume of the hydrochar were found to be 29.16 m²/g, 305.7 Å, and 0.223 cm³/g while the surface area, average diameter, and pore volume of the AC were revealed to be 63.35 m²/g, 515.00 Å and 0.767 cm³/g. The surface parameters had increased after the hydrochar was activated by heating it in a tube furnace generating AC. Therefore, the surface parameters of the AC had been improved. The achieved average particle size values of hydrochar and AC were discovered to be 2084 and 3543 d.nm, respectively. When hydrochar was used as an adsorbent, the adsorption of Mn(II) resulted in the adsorption capacity of Mn(II) being 44.03 mg/g at pH 8, adsorbent dose=0.25 g/L, contact

time=180 mins, and temperature= 25°C. When AC was used as an adsorbent, the adsorption capacity of Mn(II) increased to 56.31 mg/g at pH 7, adsorbent dose=0.25 g/L, contact time=210 mins, and temperature=25°C. The results of the adsorption of Cr(VI) showed the maximum adsorption capacity of 43.81 mg/g at pH 5, adsorbent dose=0.25 g/L, contact time=150 mins, and temperature= 25°C when hydrochar was applied. The results obtained when AC was used as an adsorbent in the adsorption of Cr(VI) were: adsorption capacity=38.26 mg/g at pH 7, adsorbent dose=0.25 g/L, contact time=120 mins, and temperature=25°C. Adsorption kinetics were studied and the experimental data was modelled with Langmuir and Freundlich isotherms. The coefficient of determination of the Langmuir model for Mn(II) and Cr(VI) metal ions were higher than that of Freundlich model. The Langmuir coefficient of determination obtained were $R^2 = 0.9915$ for hydrochar and $R^2 = 0.9924$ for AC for Mn(II); $R^2 = 0.5326$ for hydrochar and $R^2 = 0.5082$ for AC for Cr(VI). Therefore, Langmuir isotherm model best fitted the experimental data. The produced Hydrochar and AC were applied in aqueous solutions as adsorbents, and they were efficient enough to obviate Mn(II) and Cr(VI) ions from aqueous solution. Hydrochar and AC could be applied in real samples for the removal of heavy metals.

LIST OF PUBLICATIONS AND CONFERENCES

Publications

- A paper titled 'The application of mesoporous hydrochars in the removal of Mn(II) in wastewater' has been submitted to the Journal of Physics and Chemistry of the Earth.

Presentations

- Dance Mabu, Caliphs Zvinowanda and Abayane Ambushe, The application of mesoporous hydrochars in the removal of Mn(II) in wastewater, 21st WaterNet/WARFSA/GWP-SA Symposium, October 2020, Victoria Falls, Zimbabwe.



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ABBREVIATIONS AND ACRONYMS

AC	Activated carbon
ACNPs	Activated carbon nanoparticles
AMD	Acid mine drainage
BET	Brunauer– Emmett–Teller
CBC	Carbonization bacterial cellulose
CCD	Charge-coupled device
DAF	Dissolved air flotation
DLS	Dynamic Light Scattering
EDLC	Electrical double layer capacitance
EDS	Energy dispersive spectrometer
EDTA	Ethylenediaminetetraacetic acid
EDX	Energy dispersive x-ray
FAAS	Flame atomic absorption spectroscopy
FTIR	Fourier transform infrared spectroscopy
GA	Glutaric acid
HTC	Hydrothermal carbonization
IAF	Induced air flotation
KOH	Potassium hydroxide
PCS	Polymeric carbon solids
SANS	South African national standards

SEM	Scanning electron microscopy
SSA	Sulfosuccinic acid
TEM	Transmission electron microscopy
TGA	Thermogravimetric analyzer
UF	Ultrafiltration
WHO	World health organization
WWTPs	Wastewater treatment plants
XRD	X-ray powder diffraction



1.1. BACKGROUND

Water pollution has raised a serious concern worldwide as clean water is essential for human activities such as agriculture, industrial, and domestic purposes [1, 2]. Water is polluted by pernicious substances like heavy metals, pathogens, and dyes which tend to have a calamitous effect on human and animal lives [3]. When heavy metals enter water bodies they bioaccumulate. Long time exposure to heavy metal ions can cause serious diseases. The health effects associated with chromium include asthma, perforated eardrums, respiratory irritation, kidney damage, liver damage, pulmonary congestion and edema, upper abdominal pain, nose irritation and damage, respiratory cancer, skin and eye irritation [4–6]. Chromium occurs in two oxidation states that are trivalent Cr(III) and hexavalent Cr(VI) [7, 8]. The solubility of Cr(VI) is higher and consequently, it is more toxic at lower concentrations than Cr(III) [9]. The Cr(VI) is carcinogenic, genotoxic, and hemotoxic [10]. When Cr(VI) enters the bloodstream, it harms blood cells because it causes oxidation reactions. The damage that may result from these oxidation reactions can lead to hemolysis and the patients might be treated with dialysis [11, 12]. Manganese is another heavy metal that negatively affects human biochemical processes too. The inhalation of manganese is perilous, the body normally transports the minerals straight into the brain without first being processed for their actual use. The exposure to manganese by inhalation for a long period can lead to a consequential condition called manganism [13]. Manganism is a disease that is similar to Parkinson's disease [14]. Manganese can also damage the central nervous system and this may result in permanent disability [15, 16]. Manganese displays oxidation states from +2 to +7, but the common oxidation states are +2, +4, and +7 [17]. The removal of heavy metal from water, wastewater, and acid mine drainage (AMD) has been reported [18]. Various conventional methods such as chemical precipitation, adsorption, coagulation and flocculation, flotation, ion exchange, membrane filtration, electrochemical treatment, and bioremediation have been employed in the removal of heavy metals from wastewater [19–22]. Urbanization and industrialization are the major sources of heavy metals for the contamination of water.

1.2. PROBLEM STATEMENT

Manganese and chromium metals affect the living organisms in a pessimistic way. These heavy metals exist in different oxidation states which some are hazardous at their low concentrations and extremely toxic at high concentrations. The Cr(VI) is toxic even at its lowest concentrations [23]. Industries are generally the common sources of different heavy metals, for instance, Cr(VI) is used in wood preservation, metal finishing, leather tanning, and steel fabrication [24]. South Africa's economic growth is attributed to the mining industry. In mining industries, the ore contains very high levels of chromium, and the wastes that come from the industries are deposited into the rivers via runoff [25]. Moreover, the sources of drinking water like boreholes in Mpumalanga province, South Africa, were indicated to be having chromium [26]. This is ascribed to the high concentration of chromium in shallow levels of groundwater and it results in chromium contamination of groundwater [27]. The wastewater is always having high concentrations of heavy metals [28], Mn(II) is one of the rich metal ions [29, 30]. Although manganese has a variety of applications in dry battery cells, ceramics, and electrical coils [31]; Mn(II) has neurotoxic consequences on the nervous system by giving rise to the following conditions: dementia, anxiety, and ataxia [32]. A solid waste from the production of electrolytic manganese contains a lot of soluble Mn(II) [33]. Leachate that contains Mn(II) would be released when it rains. Heavy metals need to be removed from industrial wastewater before the wastewater could be released into the streams and rivers.

1.3. RATIONALE OF THE STUDY

Heavy metals are among many other pollutants that pollute water in the world. The main source of heavy metals is the industrial activities that are taking place. The reports showed that there is an escalation of potentially toxic elements through fertilizers, treated woods, and aging water supply infrastructures that rise a worry of water and environmental pollution [34, 35]. Various researches have been conducted on the removal of heavy metals from water and wastewater. The adsorption is a developed method preferred in removing heavy metals from water and wastewater due to its operational simplicity, cheap to use, and the materials used as adsorbents are easily

obtainable [36]. The adsorbents such as agricultural wastes, sludges from wastewater treatment plants, and plant materials are used in the adsorption methods. Some of the plant materials that have been triumphantly utilized for this purpose are as follows: sea-buckthorn stones [37], wooden precursors [38], rice husk [39], coffee grounds [40], tomato processing solid waste [41], corncob [42], oil palm shell [43], hazelnut husks [44], apricot stones [45], cherry/sweet cherry kernels [46], pistachio nut shells [47], Brazilian pine-fruit shell [48], grape processing wastes [49], blue jacaranda and plum stones [50], pine cone [51], and forest biowaste [52]. Adsorption technique also reuses waste products to benefit humans. In this study, hydrochar produced from eucalyptus wood chips would be exploited for its efficacy to remove Mn(II) and Cr(VI) from aqueous solutions.

1.4. PURPOSE OF THE STUDY

1.4.1. Aim

The main aim of this study is to produce polymeric carbon solids (PCS), hydrochar and (AC, from wood chips and evaluate their potential as adsorbents for toxic inorganic ions from aqueous systems.

1.4.2. Objectives

The objectives of this study are to:

- investigate conditions for the production of PCS suitable for inorganic ion adsorption:
 - reactor pressure
 - reactor temperature
 - reaction time
- characterize PCS by using DLS, BET, XRD, EDX, FTIR, TGA, SEM, and TEM techniques
- investigate adsorption capacities of PCS from eucalyptus wood chips for the removal of Mn(II) and Cr(VI) using aqueous solutions.

- investigate the effect of initial metal ions concentration, pH, solution temperature, contact time and adsorbent dose on metal ion adsorption.
- study the kinetics and thermodynamic properties of the adsorbent to these ions.

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CHAPTER TWO: LITERATURE REVIEW

2.1. INTRODUCTION

Water is a principal natural resource, the life of humans and animals revolve around it. Studies show that water envelops about 71% of the earth's surface, solely 2.5% of this water is freshwater, with at most 98.8% of this being groundwater and then merely 0.3% being available for utilization from streams or rivers, atmosphere, and the lakes [1]. There is a lesser percentage of water obtainable for consumption; therefore, there has been a focus on how to sustain water resources, assuring that water of good quality is available [2, 3]. The little percentage of water available for consumption gets polluted which then results in water scarcity and leaves people with less amount of pure water for utilization [4]. There is chemical pollution that occurs when chemicals/metals get into rivers directly by effluent outfalls from industries, refineries, and waste treatment plants and also indirectly by the contaminants that enter the water sources from soils/groundwater systems and the atmosphere via rainwater [5].

The reactivity of elements differs, for example, chromium is a highly reactive element and exists in two oxidation states, Cr(III) and Cr(VI) [6]. Heavy metals affect the environment negatively, other heavy metals tend to kill the plants when their concentrations are extremely high. Some heavy metals are needed by a human body in small amounts, for instance, zinc is an essential element needed in the body of infants to grow and develop properly and it also heals wounds [7–9]. The high concentration of various heavy metals found in industrial wastewater could cause brain damage, kidney failure, and many other diseases [10]. Cadmium is another heavy metal that is very toxic at low exposure that can cause serious damage to the kidneys and bones [11]. Consequently, heavy metals need to be prevented from entering the environment and water bodies. Thus, the treatment of wastewater from industries should take place so that water quality is achieved. Numerous methods have been employed for the removal of heavy metals from wastewater. In the adsorption method, different adsorbents have been reported in the removal of heavy metals from wastewater [12].

2.2. WATER POLLUTION

Water pollution is the presence of chemical, physical, biological components or factors producing a condition or impairment of a given water body for some beneficial use [13]. Naturally, there are different types of waters which include groundwater that is found beneath the earth and surface water, the water on the earth, for instance, rivers, lakes, oceans, etc. There are a lot of things like constructions that tend to pollute surface water and it is known that water pollution in construction sites influences the environment of the affected community and its natural surroundings [14]. The pollutants involved in water pollution depend on different sources. The pollutants that come from wastewater and agriculture are mainly chemicals, sediments, and nitrates [15]. The chemical salts like nitrates that are found in the surface water can also be found in underground water due to farming resulting from manures or human excrement or urine. Fertilizers are the major sources of nitrate in surface and underground water [16]. Water is polluted daily, more especially the surface water since the pollutants have to first travel all the way down the Earth's surface to reach the underground water. The other sources of water pollution may either be natural or artificial, that is human activities [17, 18]. One example of natural water pollution includes deforestation [19].

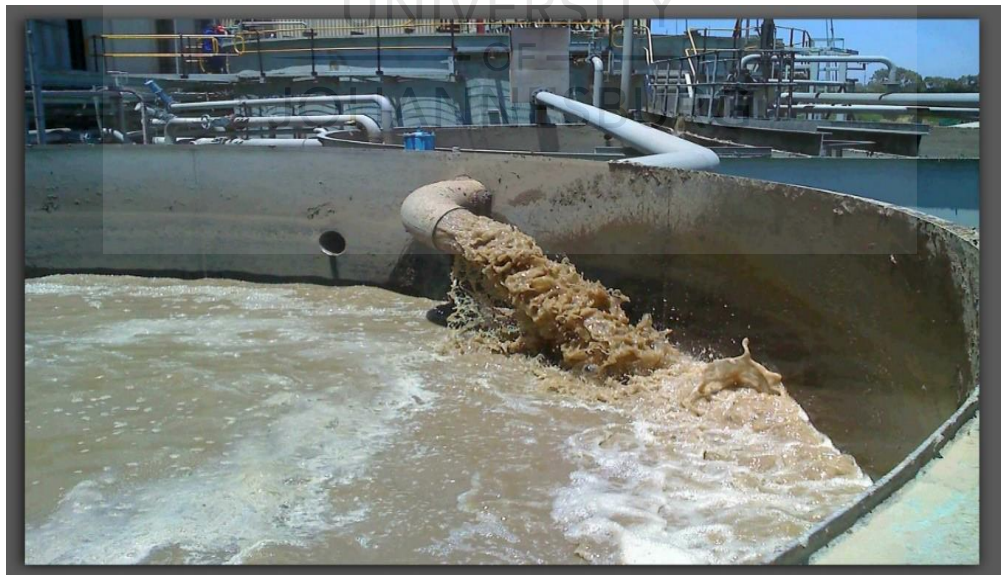


Figure 2.1: Photograph depicting the effluent discharged from metal industry source [20].

2.3. POLLUTION OF WATER BY POTENTIALLY TOXIC ELEMENTS

Industries release a variety of chemicals as wastes that are the source of potentially toxic elements into water bodies. A list of potentially toxic metals that are likely to be found in polluted water is as follows Hg, As, Pb, Sb, Ni, Sr, and Cd. These potentially toxic metals mostly occur at their lower concentrations in water [21, 22]. During the rainfall and other natural processes, these metals sink deep into the ground then in the later stages they enter rivers, lakes, and dam systems. The potentially toxic metals are absorbed by sediments and their residuals act as an organic and inorganic nutrients reservoir [23]. There is a large number of mineral resources distributed in which some toxic elements could leach [24]. It was reported that most of the potentially toxic metals cause problems to aquatic organisms [25]. The potentially toxic metals also occur naturally in the soil, but they occur at a low concentration and keep on increasing due to different human activities performed daily [26, 27].

2.3.1. Manganese

Mn(II) is one of the most abundant elements in the Earth's crust and it is a major pollutant in drinking water [28]. Manganese is a vital element for humans and other animals and occurs naturally in various food sources. In drinking water, the consumption of a maximum concentration of 0.3 mg/L does not have any harmful effects on human health [29]. The World Health Organization (WHO) guideline value for manganese in drinking water is from 400 to 500 µg/L [30, 31] and the legal limit for manganese according to South African national standards (SANS) is ≤ 400 (chronic health), ≤100 (aesthetic) [32, 33], but above 500 µg/L it is undesirable and had caused health problems and also deteriorates the water quality [34]. The most essential manganese's oxidative states for the environment and biology are as follows: Mn(II), Mn(IV), and Mn(VII). When water is exposed to air, Mn(II) combines chemically with oxygen to form manganese(IV) oxide, MnO₂. Mn(IV) precipitate can discolor household utensils and clothes [35]. Some of the physical and chemical properties of manganese are given in Table 2.1.

Table 2.1: Physical and chemical properties of manganese [36, 37]

Property	Manganese	Mn(II) chloride	Manganese sulfate
Molecular weight	54.94	125.85	151.00
Color	Steel-gray	Pink	Pale rose-red
Physical state	Solid	Solid	Solid
Melting point	1244 °C	650 °C	700 °C
Boiling point	2095 °C	1412 °C	850 °C (decomposes)
Odor	No data	No data	Odorless
Density at 20 °C	7.26 g/cm ³ at 20 °C	2.325 g/cm ³ at 25 °C	3.25 g/cm ³

Manganese is useful in agriculture when it is combined with urea, nitrates, potassium, and phosphates [38]. Manganese is produced from mining, organic chemicals, pesticides, rubber and plastics, lumber and wood products, metal processing, pharmaceuticals, and tanneries and it is not corrosive in the presence of glass [39, 40]. Manganese is also used as an effective adsorbent, manganese oxide coated zeolite, for Mn removal in wastewater [41]. Manganese is soluble in both cold and hot water. In an aqueous solution, manganese is present mostly as Mn(II) ion depending on other parameters such as pH and temperature [42].

2.3.2. Chromium

Very small quantities of chromium are needed by the human body. Chromium exists in two oxidative states which are hexavalent chromium, Cr(VI), and trivalent chromium, Cr(III). Chromium is a common contaminant in the environment and aquatic systems. It has gained global attention, (Cr(VI) is known to be more mobile, a strong oxidizing agent, and more toxic than Cr(III) [43, 44]. Chromium causes health problems in humans when exceeding the permissible level [45]. It comes from natural sources such as rocks and also from effluents of industries such as metallurgy, electroplating, leather tanning, paints and pigments, textile, and steel fabrication [46]. Some of the physical and chemical properties of chromium are given in Table 2.2.

Table 2.2: Physical and chemical properties of chromium

Properties	Value
Atomic Number	24
Atomic Weight	52.00
Charge	3 ⁺ and 6 ⁺
Electron configuration	[Ar] 3d ⁵ 4s ¹
Electronegativity of atom	1.66
Ionic radius (Å)	2

2.4. TECHNIQUES USED FOR THE REMOVAL OF HEAVY METALS FROM CONTAMINATED WATER

For the security of humans, the environment, and other living organisms from the significant negative effect of toxic heavy metals including manganese and chromium, different methods have been advanced and used for the removal of heavy metals from water and wastewater. The following are the employed techniques: chemical precipitation, adsorption, coagulation and flocculation, flotation, ion exchange, membrane filtration, electrochemical treatment, and bioremediation [47–52]. These techniques have their advantages and disadvantages. Table 2.3 below shows some of the advantages and disadvantages of these techniques.

Table 2.3: Advantages and disadvantages of different techniques

Techniques	Advantage	Disadvantage	References
Chemical precipitation	<ul style="list-style-type: none"> •Permanent •Immediate results •Efficient •Easily implemented •Easy to monitor 	<ul style="list-style-type: none"> •High cost •Not applicable for all cases •Requires operation and maintenance (O&M) •Requires power •May generate a waste product 	[53, 54]
Adsorption	<ul style="list-style-type: none"> •Low energy and maintenance costs •Simple to operate •Reliable •Effectiveness(also at low contaminant concentrations) •Selectivity (tailored adsorbents) •Regenerability of used adsorbents •Cost-efficiency (low-cost adsorbents) 	<ul style="list-style-type: none"> •Waste product •Rapid saturation and clogging of the reactors 	[55–57]
Coagulation and flocculation	<ul style="list-style-type: none"> •Reduction of the time required to settle out suspended solids •Very effective in removing fine particles that are otherwise very difficult to remove •Effective in removing many protozoa, bacteria and viruses 	<ul style="list-style-type: none"> •Costly and the need for accurate dosing and frequent monitoring •Need accurate dosing equipment to function efficiently and the dose required depends on raw water quality that can vary rapidly 	[58–61]

Flotation	<ul style="list-style-type: none"> •Almost all minerals can be separated by this technique •Highly appreciate for the separation of sulfide minerals •Low cost 	<ul style="list-style-type: none"> •The method is quite complex and expensive •Long production cycle 	[62, 63]
Ion exchange	<ul style="list-style-type: none"> •Simple equipment •Easy operation •No or little use of organic solvents 	<ul style="list-style-type: none"> •Sometimes poor product quality •Large pH changes in the process 	[64–68]
Membrane filtration	<ul style="list-style-type: none"> •Flexible; can be used in the separation, concentration, and purification of a huge variety of materials across a wide range in industries. •Microfiltration and ultrafiltration processes can operate as highly efficient "sieves", capable of fractionating particle species according to size •The processes can function effectively at low temperatures •Energy requirements are low. •Processes are relatively simple to scale up. •Membranes can be manufactured in a uniform and highly precise manner 	<ul style="list-style-type: none"> •The processes are prone to membrane fouling effects which lead to a decrease in permeate flux •Expensive cleaning and regeneration schemes may be necessary •The high flow rates used in cross-flow feed can damage shear sensitive materials. •Equipment costs can be high 	[69–72]
Electrochemical treatment	<ul style="list-style-type: none"> •Environmental compatibility •Versatility •Energy efficiency •Selectivity •Amenability to automation and cost-effectiveness 	<ul style="list-style-type: none"> •High requirement of manual labor •Requires a high level of maintenance 	[73–75]

Bioremediation	•Lower costs and less disruption of the contaminated environment when compared to other cleanup methods	•If the process is not controlled there is a possibility that the organic contaminants may not be broken down fully resulting in toxic by-products that could be more mobile than the initial contamination	[76, 77]
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2.4.1. Chemical precipitation

Chemical precipitation is a widely used method for the removal of heavy metals from water and wastewater. By definition, chemical precipitation is the creation of a solid from the solution [78]. In chemical precipitation processes, the addition of reagents is involved then followed by the separation of formed solids [79], for instance, magnesium and phosphate are required for chemical precipitation [80]. This technique is usually used to treat AMD, neutral drainage, and pit lake water [81]. Chemical precipitation can also be used in combination with other technologies. The sequencing batch reactor (SBR) process is one of the technologies used in combination with chemical precipitation [82].

2.4.2. Coagulation and flocculation

Coagulation and flocculation are used in the removal of heavy metals, color, turbidity, algae, and other micro-organisms from wastewater and surface waters [83, 84]. The processes involved in this method are sedimentation, precipitation, and filtration. The floc forms when a chemical coagulant is added to aqueous solutions and wastewater. The commonly used coagulants are aluminum sulfate and ferric chloride [85]. Various coagulants such as aluminum potash, Polyaluminum Chloride (PAC), ferric sulfate, iron salts, etc., are used in coagulation and flocculation for removing heavy metals from wastewater [86, 87]. Those coagulants do not completely remove heavy metals from water and wastewaters, therefore, the other techniques are further employed for the completion of heavy metals removal [88].

2.4.2.1. Coagulation and flocculation mechanism

Coagulation is the destabilization of colloidal particles formed after the addition of coagulants. The flocculation happens when the destabilized colloidal particles come together, agglomeration, into fine lumps and bulky lumps settle down [89]. The mechanism of coagulation and flocculation is grounded on zeta potential (ζ) measurement which entails the electrostatic interaction between the pollutants and coagulants [90, 91]. The chelating ability of coagulant and flocculant (polyelectrolytes)

helps in the optimization of the removal of different types of pollutants [91]. Figure 2.2 below shows the coagulation and flocculation mechanism.

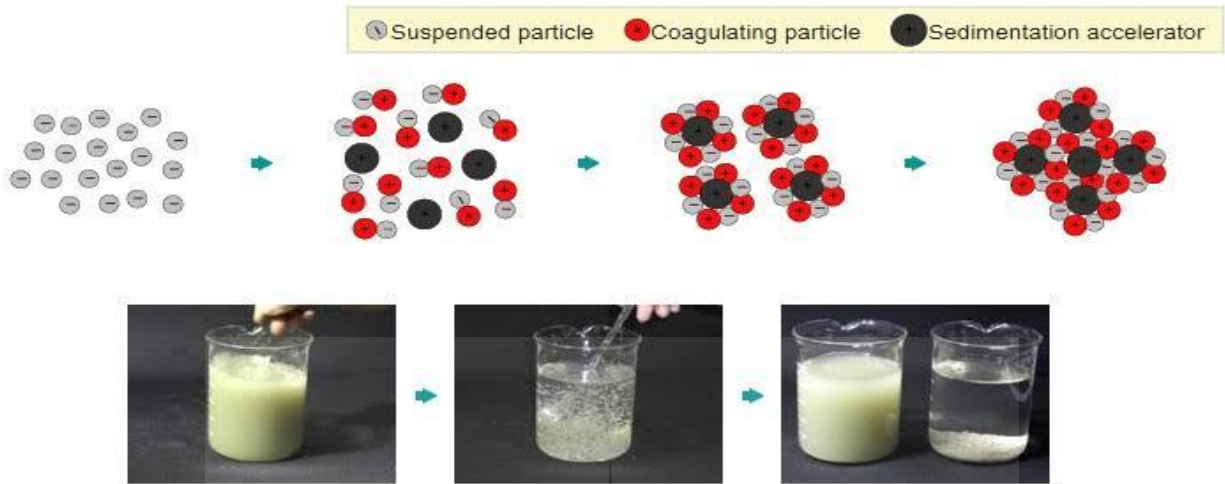


Figure 2.2: Coagulation and flocculation mechanism [92].

2.4.3. Flotation

The flotation technique is used for separating heavy metals from water and wastewater using bubble attachment [93]. The involved processes of this technique in the removal of heavy metals from wastewater are dissolved air flotation (DAF) [94], induced air flotation (IAF) [95], precipitation flotation [96], and ion flotation [97]. This method is mostly used to treat wastewater with a very low concentration of metals and it is normally employed in dams or simple treatment [98]. The flotation technique was found to be flexible by the researchers, the removal of Zn(II), Pb(II), and Cu(II) ions from simulated wastewater by (DAF) was reported [99, 100].

2.4.4. Ion-exchange

Ion exchange is another technology used for the removal of heavy metals. This technology involves the use of electrodes, synthetic and natural resins for the exchange of cations with heavy metals in water and wastewater [101, 102]. An example of the synthesized inorganic ion exchanger is sodium iron titanate (NaFeTiO) [103]. The reported fabricated electrodes used in ion exchange are ion-exchange polymer and modified carbonization bacterial cellulose (CBC) [104]. These electrodes are used by

varying amounts of cation-exchange polymers (glutaric acid (GA) and sulfosuccinic acid (SSA)) [105].

2.4.5. Membrane filtration

Membrane filtration is a conventional technique used for the removal of suspended solids, microorganisms, bacteria, particles, natural organic material and inorganic pollutants, heavy metals [106]. Generally, the membrane filtration technique makes use of a semi-permeable membrane that allows water to pass through obviating pollutants [107]. The membrane pores could be blocked and form lumps on the membrane surface causing membrane fouling which leads to a fast reduction of liquid flow in the early stage of the filtration process resulting in the reduction of membrane service life [108]. There are different types of membrane filtration processes divided into two general classes that are pressure-driven and electric-driven processes [109, 110]. The pressure-driven process comprises of ultrafiltration, nanofiltration, reverse osmosis and microfiltration, and the electric-driven process comprises of electrodialysis and electrodialysis reversal [111, 112]. The membrane used in microfiltration has the pore size ranging from 0.1 to 10.0 μm [113]. These pores allow water to pass while preventing the dissolved contaminants with bigger sizes. The membrane filtration technique has various applications, for instance, ultrafiltration (UF) is applied in oil emulsion waste treatment [114], production of ultra-pure water for electronics industry [109], reduction of high COD level in corn starch plants [115], wine or fruit juice clarification [116], treatment of whey in dairy industries and selective removal of dissolved toxic metals from groundwater consolidated with chemical treatment [117].

2.4.6. Electrochemical treatment

Electrochemical technology has been widely used for the extraction of metals such as Au, Mn Zn, Ni, Cu, etc., from water and wastewater, and to also recycle these metals [118, 119]. The mechanism of the electrochemical method for metal recovery is based on depositing a metal onto the cathode is shown in equation (1):



This technology has been applied in the mining industry for metal electrorefining [120]. The metals are removed from the water in the cathode chamber of the electrochemical cell, whereas water is getting oxidized in the anode chamber of the electrochemical cell [121, 122].

2.4.7. Bioremediation

Bioremediation is used for water purification by removing heavy metals from water and wastewater. Bioremediation utilizes living organisms to break down the inorganic materials into compounds that are not harmful to the environment and aquatic organisms [123]. The types of bioremediation are phytoremediation and mycoremediation [124]. The bacteria used in bioremediation include *pseudomonas putida*, *dechloromonas aromatica* [125], *deinococcus radiodurans* [126], *methylibium petroleiphilum* [127], *alcanivorax borkumensis* and *phanerochaete chrysosporium* [128].

2.5. ADSORPTION

The adsorption method is used to remove a variety of heavy metals from wastewater, manganese and chromium are among those heavy metals. The advantages of the adsorption method are mentioned in Table 2.3. This method purifies water by removing a broad range of compounds from wastewater coming from the industries [129]. Adsorption occurs when molecules or ions in a solution bind themselves to the surface of the adsorbent, while adsorbate is the constituent to be adsorbed. The two main types of adsorption are physisorption and chemisorption. The mechanism of physisorption is that the Van der Waals forces hold the adsorbate molecules and the adsorbent together, and the process is always exothermic [130, 131]. The mechanism of chemisorption is that the chemical forces binding the molecules are attached to the adsorbent, therefore it is hard for this process to be reversed [132].

2.5.1. Adsorption equilibrium

The adsorption equilibrium is established when the adsorption rate of the adsorbate ions or molecules on the surface of the adsorbent is equal to the rate of the desorption rate of the adsorbate ions or molecules on the surface of the adsorbent. The capacity of the adsorbent to take up the adsorbate depends on adsorbent dosage, temperature, and the concentration of the adsorbate [133]. The isotherm of adsorption capacity vs the equilibrium concentration could be plotted when the temperature is kept fixed [134]. The adsorption isotherms supply more details about adsorption mechanisms. The common isotherm models are Langmuir, Freundlich, Temkin and Dubinin-Radushkevich [135].

2.5.1.1. Langmuir isotherm model

In 1932, Irving Langmuir developed a Langmuir adsorption isotherm model, it is described by equation (2) below.

$$q_e = \frac{q_m K_L C_e}{1 + K_L C_e} \quad (2)$$

where: q_m is the maximum adsorption capacity (mg/g); q_e is the amount of adsorbate adsorbed per gram of adsorbent at equilibrium (mg/g) [136]; K_L is the Langmuir isotherm constant (L/mg) [137] and C_e is the equilibrium concentration of adsorbate (mg/L) [138]. The assumptions of the Langmuir model's derivation are:

- (1) Monolayer adsorption
- (2) Localized adsorption (occur on specific sites)
- (3) The heat of adsorption is constant (independent of the amount of material adsorbed)
- (4) Based on the kinetic model of the adsorption-desorption process

The linearization of equation (2) gives the equation below:

$$C_e / q_e = C_e / q_m + 1 / q_m K_L \quad (3)$$

Plotting C_e / q_e against C_e gives a straight line with slope $1 / q_m$ and intercept $1 / q_m K_L$ [139] if the adsorption data are described by the Langmuir model [140].

2.5.1.2. Freundlich isotherm model

The Freundlich isotherm model was developed in 1909 by Herbert Freundlich and it represents an empirical model [141]. The Freundlich isotherm can also be used for a mixture of compounds, no assumption is made for the Freundlich isotherm [142]. It is expressed by equation (4):

$$q_e = K_F (C_e)^{1/n} \quad (4)$$

where: K_F is the Freundlich indicative of relative adsorption capacity of adsorbent and n is the Freundlich indicative of the intensity of adsorption [143]. K_F and n are constants which can be determined experimentally. The unit of K_F depends on n . When taking the logarithms of equation (4), it becomes equation (5):

$$\log q_e = \log K_F + 1/n \log C_e \quad (5)$$

The plotting of $\log q_e$ versus $\log C_e$ gives a straight line with slope $1/n$ and intercept $\log K_F$ that means the data can be represented by the Freundlich model [144].

2.5.1.3. Temkin isotherm model

The Temkin isotherm was developed and grounded on the assumption that the heat of adsorption is decreasing linearly when the solid surface increases [145]. Temkin isotherm is expressed in equation (6):

$$q_e = (RT/b_T) \ln A_T C_e \quad (6)$$

The linearization of equation (6) makes it equation (7):

$$q_e = (RT/b_T) \ln A_T + (RT/b_T) \ln C_e \quad (7)$$

where: b_T is the Temkin isotherm constant; A_T is the Temkin isotherm equilibrium binding constant (L/g); T is the temperature (°K); R is the universal gas constant (8.314J/mol/K); C_e is the equilibrium concentration of adsorbate (mg/L) and q_e is the amount of adsorbate adsorbed at equilibrium (mg/g) [146].

2.5.1.4. Dubinin-Radushkevich isotherm model

The Dubinin-Radushkevich isotherm model is another model that is used to describe adsorption data, it has two parameters. The nonlinear equation of the Dubinin-Radushkevich isotherm model is shown in equation (8) :

$$q_e = q_s \exp [-K_{DR} \epsilon^2] \quad (8)$$

The linearization of equation (8) yields equation (9) below:

$$\ln q_e = \ln q_s - K_{DR} \epsilon^2 \quad (9)$$

$$\epsilon = RT \ln [1 + 1/C_e] \quad (10)$$

where: q_e is the amount of adsorbate in the adsorbent at equilibrium (mg/g); q_s is the theoretical isotherm saturation capacity (mg/g); K_{DR} is the Dubinin–Radushkevich isotherm constant (mol^2/kJ^2), R is the universal gas constant ($8.314 \text{ J/mol}\cdot\text{K}$); T is the absolute temperature ($^\circ\text{K}$) and C_e is the adsorbate equilibrium concentration (mg/L) [147, 148].

2.6. ADSORBENTS

There are various adsorbents found in different forms. The most known adsorbents that are in use are silica gel, activated alumina, molecular sieve zeolite, molecular sieve carbon, and AC [149, 150]. The synthesized adsorbents are AC and nanoparticles [151]. There are also biomass, by-products from industries, and agricultural waste adsorbents [152, 153]. These adsorbents have interesting properties and characteristics include high pore volume, large surface area, and regeneration of the adsorbent [154].

The AC is frequently used as an adsorbent in wastewater treatment facilities. The raw materials such as banana peels, orange peels, wood, and vegetable shells are calcined with a temperature ranging from $700\text{--}1000 \text{ }^\circ\text{C}$ to generate ACs with the desired pores [155,156]. The AC can also be generated by treating the raw materials with chemical reagents like sodium hydroxide, potassium hydroxide, zinc chloride, phosphoric acid or sulfuric acid [157]. The treated raw materials possess sufficient surface area and large pores enough to remove more heavy metals.

The AC is expensive and efficient, it makes the adsorption process costly. Consequently, low-cost and easily available materials are in need for application in

the removal of heavy metals from water and wastewater. The researchers have discovered various natural adsorbents that were applied to remove heavy metals from wastewater [158]. The natural adsorbents deployed are rice husk, pecan shells, and hazelnut shells [159–161]. The Fly ash and iron slags are industrial by-products that have been utilized as new adsorbents and they have similar properties as AC [162]. The generation of AC, the application of AC, and surface area modification will be explained in the following sections.

2.6.1. Generation of AC

AC is a carbonaceous material that is broadly used as an adsorbent and catalyst, it is also used as the catalyst support in industries [163]. Moreover, the functional groups, surface area, and micropore volume make the AC to be a suitable adsorbent for different environmental applications [164, 165]. The AC is mostly produced by chemical and thermal activation. A variety of raw and nonraw materials are used to synthesize AC, for example, AC nanoparticles (ACNPs) made from the biowaste [166]. The methods available to synthesize ACNPs are solution combustion, chemical vapor deposition, and hydrothermal synthesis [167]. In the hydrothermal process, the two steps involved are: (1) carbonization of carbon precursor material at high temperatures under inert conditions; (2) activated by using gas activating agents which are steam, air, and CO₂ [168, 169]. The chemical activation process involves only one step that is the chemical reaction on carbon precursor material with the addition of reagents such as salts, acids, and bases [170, 171]. The AC generated from the heating process has a large surface area compared to an AC produced from the chemical process [172]. The AC used for this study was generated by the heating method.

2.6.2. Application and modification of AC

The unique properties and characteristics of AC make it more deployed in various applications. Examples of AC applications are environmental, supercapacitors, and electronic applications [173, 174]. The materials used as electrodes in supercapacitors are mostly conductive polymers and metal compounds [175]. There is electrical double

layer capacitance (EDLC) and pseudocapacitance mechanism taking place in supercapacitors, in the EDLC mechanism the charges are accumulated and compensate lesser to the ions attached to the electrode interfaces through electrostatic interactions [176]. The pseudocapacitance mechanism is from the redox reactions on the pseudocapacitor surface that gives zero phase transitions due to fast ion insertion and extrusion [177, 178].

Although AC works efficiently, one of its difficulties is that it agglomerates in solutions due to chemical interactions, Van Der Waals forces, that occur [179]. This difficulty can be minimized by AC modification. Surface modification lessens the agglomeration on the AC and exposes the large surface area. This also increases adsorption capacity and the interactions of AC with pollutants [180]. Surface modification is mainly done chemically whereby the desired functional groups are permanently introduced to the AC [181]. The common reagents used in the surface modification process include potassium hydroxide (KOH) and Ethylenediaminetetraacetic acid (EDTA) [182]. Depending on the desired surface area, the other chemical reagents could be used. Scientific reports showed the biomass activation using KOH combined with K_2CO_3 and the AC obtained the greatest surface area of $2417 \text{ m}^2 \text{ g}^{-1}$ [183, 184]. The drawback of the chemical activation method is that a large number of chemicals are used and could cause a threat to the environment since some chemicals are not environmentally friendly [185]. The other influential method utilized is non-covalent whereby the functional groups are thermally leaped to the surface of the AC without demolishing the AC properties and structure [186]. The main advantages of the thermal activation process are low cost in the production of ACs, and AC shape is retained [187]. This process occurs under the air, CO_2 , and steam conditions [188].

2.7. THE APPLICATION OF AC IN THE REMOVAL OF HEAVY METALS FROM WATER AND WASTEWATER

The AC has been used for the removal of heavy metals from wastewater due to its attractive properties. AC has hydroxyl, lactone, and carboxylic functional groups that have a greater affinity for metal ions [189]. These functional groups and their effect on the adsorption behavior were studied. The effect of parameters such as pH,

adsorbent dose, temperature, initial metal ion concentration, and contact time were determined [190]. The reports showed the successful adsorption of Cu(II), Cr(III), Cd(II), and Pb(II) ions from wastewater at pH 5 when the marine macroalga *Ulva lactuca* and its AC were applied [191]. The AC collected from exhausted home filtration systems was also used to remove Cu(II) from aqueous solution at the optimal solution pH 5.5 [192]. The previous adsorption studies have revealed that the optimal solution pH ranges from 5 to 7 and the contact time ranges from 5 to 120 minutes [193, 194]. The by-products from the industries are also used to generate efficient adsorbents, sewage sludge from wastewater treatment plants (WWTPs) converted into AC through pyrolysis and activated with ZnCl₂ [195]. The metal removal efficiency was investigated using AC generated from sewage sludge and the results suggested 98.9%, 34.6%, and 42.6% removal of Cu, Al, and Zn from the simulated solutions [196]. An AC was found to be working excellently in removing various heavy metals. The greatest adsorption capacities of As(III), Pb(II), and Cd(II) were 151.5, 147.1, and 119.00 mg.g⁻¹ when the AC synthesized from pistachio shell was used to remove these metal ions from wastewater [197]. In this study, the hydrochar produced from eucalyptus wood chips would be used as an adsorbent. This material was chosen due to the interesting properties it possesses. The eucalyptus wood hydrochar is suitable for adsorption, it has a surface area ranging from 460 to 1,490 m²/g respectively [198]. The surface area of the hydrochar can further be increased when it is heated at high temperatures to generate the AC.

Table 2.4: Summary of studies on heavy metals removal using AC

Heavy Metal	Adsorption Capacity (mg/g) & Removal%	Contact time (min)	pH	References
Cr	99	90	5.5	[199]
Pb	96.1	60	2.0–5.5	[200]
Cd	93.8			
Cu	83.3			

Zn	69.6			
Ni	50.0			
Pb	95	60	2.6–8.7	[201]
Cd	86			

2.8. FACTORS AFFECTING THE ADSORPTION OF METAL IONS

In the adsorption process, AC removes heavy metals magnificently from water and wastewater. An AC is industrially utilized due to its versatility. The factors affecting the adsorption process are very important because they can impact the heavy metal ions binding to the adsorbent's surface [202, 203]. The factors are explained in detail in the following sections.

2.8.1. Effect of pH on adsorption efficiency

During the adsorption process, pH is one of the most important factors. It affects the active sites of the adsorbent that binds with heavy metal ions [204]. In general, pH affects the surface properties of the adsorbent. The adsorption of heavy metal ions is mainly successful at pH 6 and less, and the heavy metal ions begin to precipitate and form metallic hydroxides in the solution when the pH is above pH 8 [205, 206]. When the pH is low, hydronium ions compete with heavy metal ions for binding to the active sites of the adsorbent [207]. This results from the high concentration of protons which would decrease the heavy metal adsorption [208]. The hydronium ions get reduced when the pH is high and that reduces the competition with metal ions [209].

2.8.2. Effect of initial metal ion concentration on adsorption efficiency

Another crucial factor that influences the adsorption is the initial metal ion concentration. The increase in initial metal ion concentration contributes more to the adsorption capacity, the saturation point is reached since the driving forces in the solid-liquid bond get enhanced [210]. The available adsorption sites of the adsorbent become unfettered

by initial concentration at lower concentrations and there is a small number of free adsorption sites on the adsorbent at higher initial metal ion concentrations [211].

2.8.3. Effect of contact time on adsorption efficiency

The contact time is a vital parameter between the adsorbent and adsorbate in the adsorption. When contact time is investigated, the removal order of almost all metal ions sharply increases at initial points and then decreases slowly until the maximum equilibrium is achieved as the time is prolonged [212, 213]. The adsorption of Cr (VI) was reported and the maximum equilibrium occurred at 60 minutes, adsorption capacity increased as the time was increasing [214]. This is ascribed to the physicochemical properties of the adsorbent, countless available active sites are easily exposed and interact with metal ions through ion exchange and electrostatic interaction [215].

2.8.4. Effect of adsorbent dosage on adsorption efficiency

The adsorbent dosage also influences the adsorption process. An AC generated from cola nutshells showed a greater effect on the uptake of metal ions, the removal efficiency increased as the adsorbent dosage increased [216–218]. When the adsorbent dose increases results in excess in the solution and the surface area accessible for adsorption of metal ions gets reduced due to the aggregation of adsorption active sites [219].

2.8.5. Effect of temperature on adsorption efficiency

Apart from the factors mentioned above, temperature is also another parameter with a greater effect on the adsorption process. The adsorption capacity increases with increasing temperature as the reaction rate increases at higher temperatures [220]. When the temperatures get extremely higher, the adsorption capacity decreases [221, 222]. This is because when the temperature is increasing, the attractive forces involved between the adsorbent's surface and metal ions become weaker thus decreasing adsorption [223]. The adsorption process is endothermic at high temperatures, and the electrostatic interaction between adsorbent and metal ions becoming stronger [224].

2.9. REFERENCES

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CHAPTER THREE: EXPERIMENTAL PROCEDURES

The hydrochar and AC used as adsorbents in this study were prepared from eucalyptus wood chips. The characterization of these adsorbents using different analytical instruments is also described. The experimental procedures used in this study are well elaborated in this section with all the apparatus and instruments.

3.1. CHEMICAL REAGENTS USED IN PREPARATION OF STOCK SOLUTIONS

All the chemical reagents used in this work were received from Sigma-Aldrich, Germany. The stock solution of manganese was prepared by dissolving the mass of 7.205 g of manganese(II) chloride tetrahydrate ($\text{Cl}_2\text{Mn}\cdot 4\text{H}_2\text{O}$), which is 99.0% pure, in a 500 mL volumetric flask and filled to the mark with deionized water (Milli-Q® Direct 8/16 System, Merck, Germany) to get the stock solution of a concentration of 4000 mg/L Mn(II). The stock solution of chromium was prepared by dissolving the mass of 3.846 g of chromium trioxide (CrO_3), which is 99.0% pure, in a 500 mL volumetric flask and filled to the mark with deionized water to generate the stock solution of a concentration of 4000 mg/L Cr(VI). A 1 M of sodium hydroxide (NaOH) and 1% nitric acid (HNO_3) were used to adjust the pH ranging from 3 to 8.5 of aqueous solutions.

3.2. APPARATUS AND INSTRUMENTS

All the glassware used in this work were washed with deionized water (Milli-Q® Direct 8/16 System, Merck, Germany) and soap, wiped with jumbo tissue paper roll then dried in a 310-glassware drier (LABOTEC, South Africa) for 24 hours to remove the moisture. The hydrochar and AC were grinded using an agate mortar and pestle. The process of generating AC from the hydrochar was carried out by using a tube furnace (Carbolite, USA). The mass measurements of the adsorbents were performed by using a PA423C analytical balance. The thermal stability of the hydrochar was determined through thermogravimetric analysis by using DSC-TGA SDT Q600 (TA Instruments, France). The discovery of the functional groups that are present in the adsorbent materials was done by employing MIRacle-10 FTIR (Shimadzu, Japan). The average diameter, pore volume, and surface area of the hydrochar and AC were achieved by using BET (GAPP

Instruments, China). The particle sizes of the adsorbent materials were accomplished using the DLS (Malvern Panalytical, Germany). The internal structure of the hydrochar and AC was examined utilizing a Jeol JEM-2100F TEM (JEOL, Japan) equipped with a LaB6 source. The external morphology (texture) was analyzed using a TESCAN Vega 3 SEM (JSM-7800F, JEOL, Japan). The pH contents of Mn(II) and Cr(VI) were measured using the pH Meter (520A pH/mV/SE, Thermo Scientific Orion, USA). The analysis of the filtrates was carried out through the FAAS (AA-7000, Shimadzu, Japan). The crystallinity of the adsorbent materials was revealed by using XRD (D8 Advance, Bruker, Germany). The elements present in the hydrochar and AC were uncovered by employing the EDS (NORANTM System 7, Thermo Scientific, USA) coupled with an Oxford detector. The conductivity improvement of the samples was done by carbon-coating hydrochar and activated carbon using a coater (Q300T ES, Quorum, Japan). The samples were sonicated by using an ultrasonic bath.

3.3. PREPARATION OF HYDROCHAR AND AC FROM EUCALYPTUS WOOD CHIPS

The eucalyptus wood chips were collected from a timber processing company in North West Province, South Africa. Hydrochar was produced by hydrothermal carbonization (HTC) of eucalyptus wood chips in the presence of a catalyst, water as a solvent, under the temperature of 240 °C and pressure of 4 bars. The AC was generated by heating the hydrochar in a tube furnace under the temperature of 700 °C in an inert atmosphere supported by nitrogen gas. This process is called annealing. The process of hydrochar and its AC generation is summarized in Figure 3.1. The hydrochar and AC produced were pulverized by using an agate mortar and pestle supplied by Merck, South Africa.



Figure 3.1: The steps of hydrochar and AC generation from eucalyptus wood chips (a) Eucalyptus wood chips, (b) hydrochar, (c) AC

3.4. CHARACTERIZATION OF HYDROCHAR AND AC

3.4.1. TEM studies

TEM studies were performed at an acceleration voltage of 200 kV by using a Jeol JEM-2100F transmission electron microscope instrument equipped with a LaB6 source. Small sample masses of hydrochar and AC were mixed with methanol and sonicated for

5 minutes at room temperature using an ultrasonic bath. The TEM samples were prepared by dropping small amount of hydrochar and AC onto a TEM grid (200 mesh size Cu-grid) coated with a lacy carbon film. The images of the hydrochar and AC were captured using a digital charge-coupled device (CCD) camera connected to the transmission electron microscope.

3.4.2. SEM and EDS studies

The hydrochar and AC were carbon-coated to improve conductivity using a Q300 TT Plus triple sputter coater instrument for specimens up to 200 mm diameter. The analysis of the coated specimens was executed through SEM and EDS coupled with an oxford detector. The images were captured in different magnifications and the elements in the materials were confirmed.

3.4.3. Particle size studies of adsorbent materials

The Zetasizer samples were prepared by using water as a dispersant and the samples were placed into disposable sizing cuvettes. The particle sizes of the adsorbent materials were measured by using a DLS at 25 °C with a count rate of 140.5 kcps for a duration of 70s and the measurement position was 1.25 mm.

3.4.4. BET and FTIR studies

The sample masses of 0.094 g were used in BET instrument for the determination of the average diameter, pore volume, and surface area of the hydrochar and AC. The discovery of the functional groups present on the surface of adsorbent materials was done through the MIRacle-10 FTIR.

3.4.5. Thermal and XRD studies

The thermal stability of the hydrochar was carried out by TGA. The hydrochar and AC were placed in the steel sample holders then put in the XRD instrument for the determination of the crystallinity of the adsorbent materials.

3.5. ADSORPTION OF Mn(II) and Cr(VI)

The effect of pH, contact time, adsorbent dose, temperature, and initial metal ion concentration on the adsorption capacity of the hydrochar and AC was investigated. The volumes of 1.25, 3.75, 7.5, 10, 15, 20, 25, and 37.5 mL of 4000 mg/L manganese and 4000 mg/L chromium stock solutions were taken into 100 mL volumetric flasks and topped up with deionized water to get the solution of 50, 150, 300, 400, 600, 800, 1000, and 1500 mg/L of Mn(II) and 50, 150, 300, 400, 600, 800, 1000, and 1500 mg/L of Cr(VI). The contents were transferred into 250 mL Erlenmeyer flasks and the pH of each of these mixtures was recorded. A mass of 1.00 g of hydrochar was added to each Erlenmeyer flask. The mixtures were then placed into a water bath and continuously agitated with magnetic stirring bars to make particles move around more rapidly and collide with each other more often. The mixtures were removed from the water bath and filtered using the Buchner funnel set. Similar experiments were performed with a mass of 1.00 g of AC. All the parameter conditions used in these experiments are mentioned in Table 3.1 and 3.2. The standard solutions that were used for the analysis were prepared prior analysis. A volume of 1 mL of 1000 mg/L of manganese and chromium standard solutions were taken into two different 100 mL volumetric flask and topped up with deionized water to get the intermediate standard solutions of a concentration of 10 mg/L of manganese and chromium. The volumes of 2.5, 5, 7.5, 10, and 15 mL of the intermediate standard solutions of manganese and chromium were taken into 50 mL volumetric flasks and topped up with deionized water to get the standard solutions of 0.5, 1.0, 1.5, 2.0, and 3.0 mg/L. The filtrates were analyzed by utilizing the FAAS.

Table 3.1: Optimum parameter conditions for Mn(II) removal

Adsorbent	Initial metal ion concentration (mg/L)	Adsorbent mass (g)	Contact time (min)	pH	Temperature (°C)
Hydrochar	600	0.25	180	8	25
AC	800	0.25	210	7	25

Table 3.2: Optimum parameter conditions for Cr(VI) removal

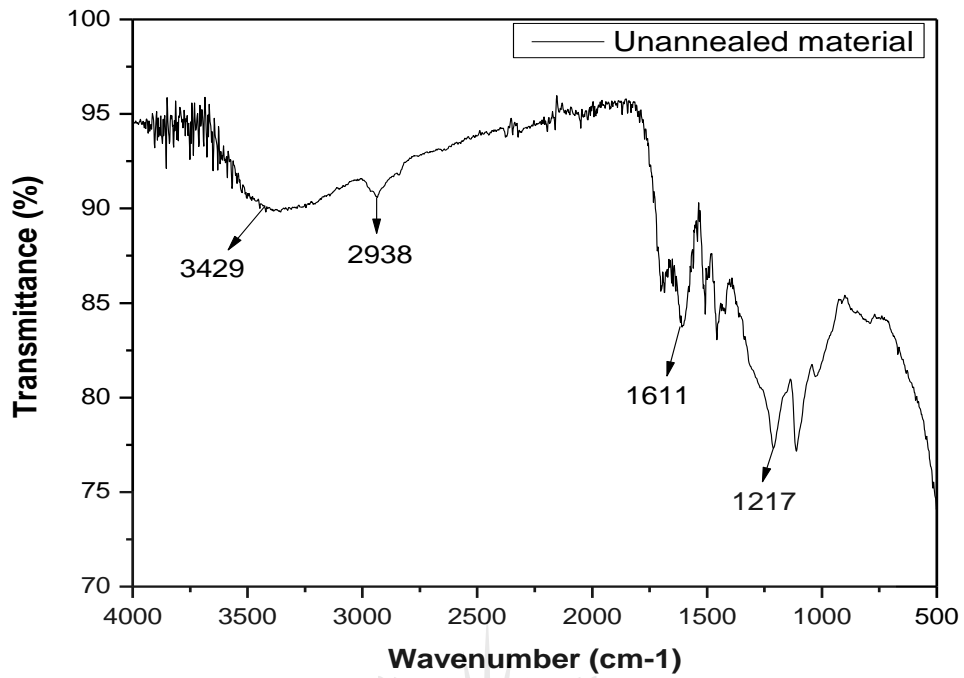
Adsorbent	Initial metal ion concentration (mg/L)	Adsorbent mass (g)	Contact time (min)	pH	Temperature (°C)
Hydrochar	600	0.25	150	5	25
AC	400	0.25	120	7	25



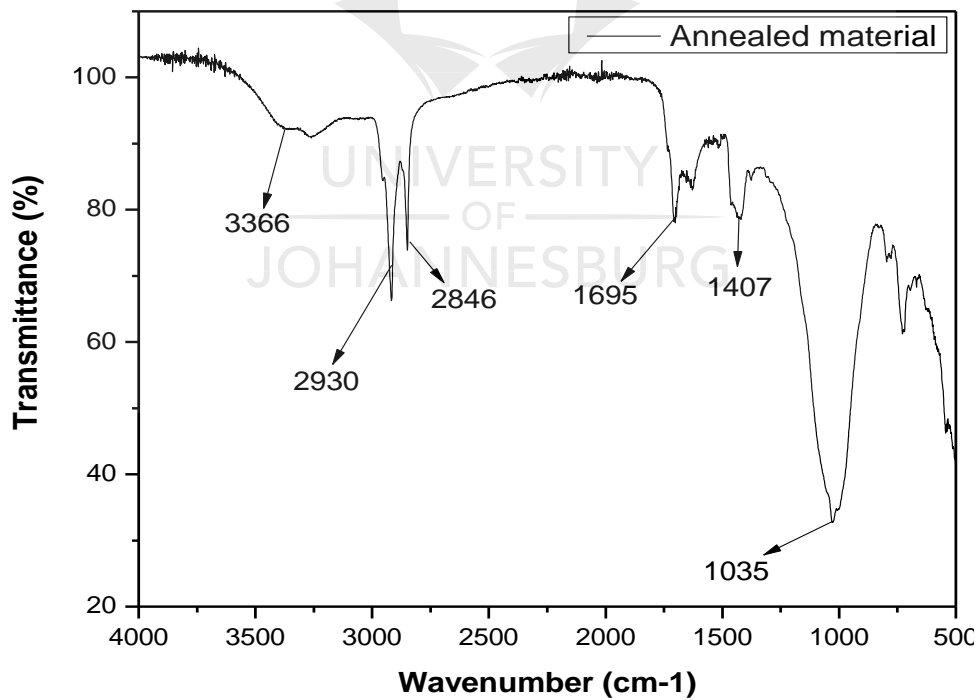
4.1. CHARACTERIZATION OF HYDROCHAR AND AC

4.1.1. FT-IR analysis

The FT-IR spectrum of the hydrochar is shown in Figure 4.1(a). It reveals a strong broad peak at 3429 cm^{-1} assigned to be O–H vibration [1], while the weak peak at 2938 cm^{-1} is the C–H stretching vibration. The sharp peak at 1611 cm^{-1} suggests being the carbonyl (C=O) functional group. The peak at 1217 cm^{-1} allotted to be C–O corresponding to syringol ring. The FT-IR spectrum of the AC shown in Figure 4.1(b) discloses the absorption band 3366 cm^{-1} assigned to be O–H vibration. The absorption bands at 2930 cm^{-1} and 2846 cm^{-1} suggest C–H stretching vibrations while the absorption band at 1695 cm^{-1} suggests carbonyl (C=O) functional group [2]. The peak at 1407 cm^{-1} is assigned to the aromatic ring [3], and the peak at 1035 cm^{-1} suggests the hydroxyl (O–H) functional group respectively. The carbonyl (C=O) and hydroxyl (O–H) functional groups are common to hydrochars derived from plant biomass [4]. The peak at 3366 cm^{-1} assigned to O–H, on the FT-IR spectrum of the AC in Figure 4.1(b), got reduced and that means water was reduced due to the heating process when the hydrochar was transformed into the AC. The peak at 1035 cm^{-1} has a transmittance of approximately 30% on the FT-IR spectrum of the AC in Figure 4.1(b), therefore, AC absorbed more radiation compared to hydrochar. The hydrochar started absorbing the radiation at approximately 77% as displayed on the FT-IR spectrum of the hydrochar in Figure 4.1(a).



(a)



(b)

Figure 4.1: FT-IR spectra of (a) hydrochar and (b) AC

4.1.2. SEM analysis

The results of the surface morphologies of the hydrochar and AC analyzed by SEM displayed the aggregate texture on the hydrochar as depicted in different magnifications in Figure 4.2. As shown in Figure 4.2(a) and (c), hydrochar particles are thin with a small surface area. In Figure 4.2(b) and (d), it was observed that the particles were roughly packed together and well-distributed. This could be due to the activation method like heating the hydrochar in a tube furnace, leading to the removal of impurities such as organic compounds [5]. The surface of the hydrochar was relatively rough, while that of AC was spongelike. The similar surface properties of other types of hydrochars produced by HTCs have been reported before [6, 7].

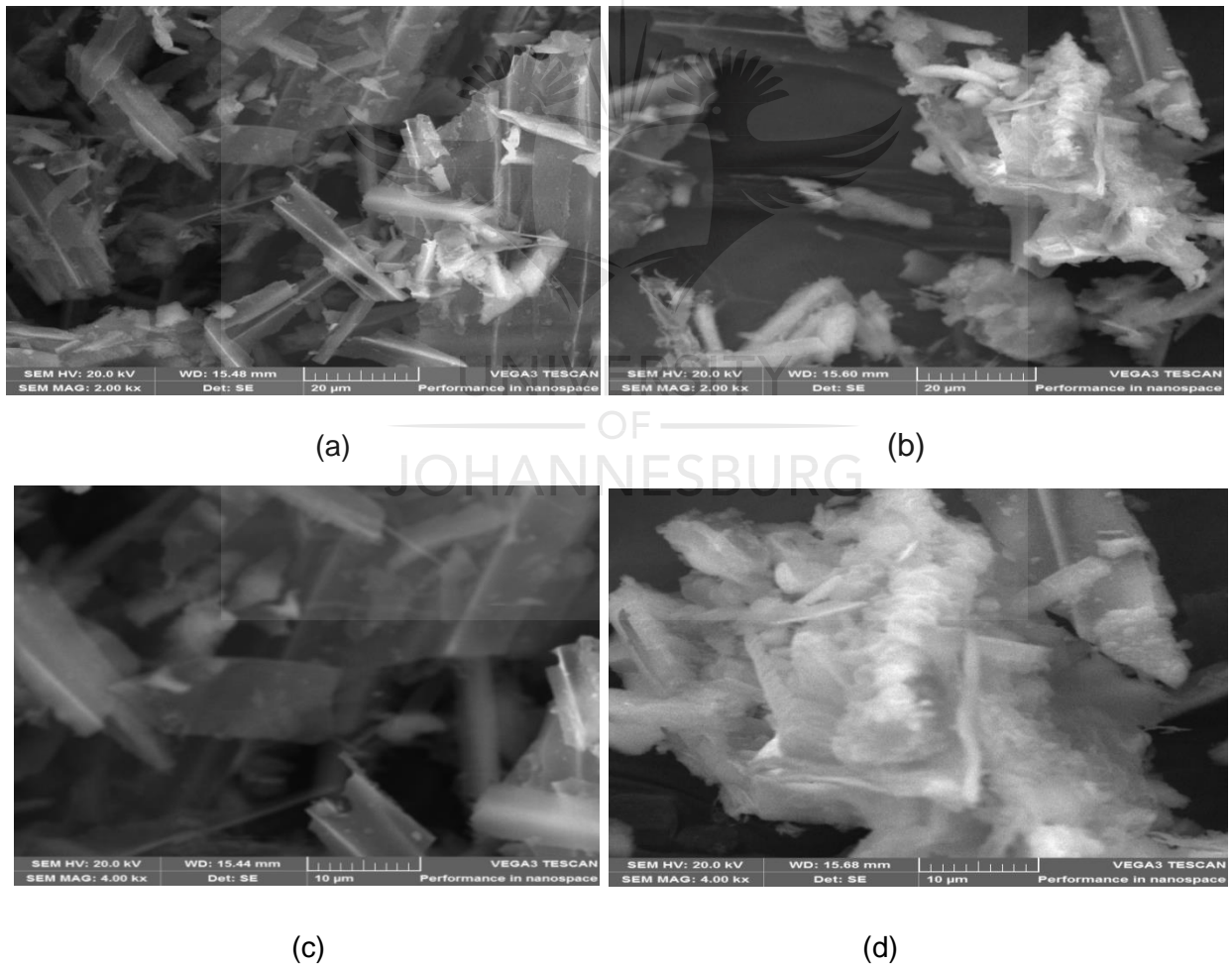


Figure 4.2: SEM images of hydrochar at (a) 2.00kx, (c) 4.00kx and AC at (b) 2.00kx (d) 4.00kx magnifications

4.1.3. TEM analysis

To identify the presence of nanopores, TEM analysis has been done. In Figure 4.3(a) and (c), the hydrochar had a small number of pores while the AC revealed a large number of pores as shown in Figure 4.3(b) and (d). In Figure 4.3(b), there are little dark spots that appear which are the small amounts of impurities representing traces of SiO_2 [8], and that is consistent with the particle distribution of the hydrochars and their AC [9].

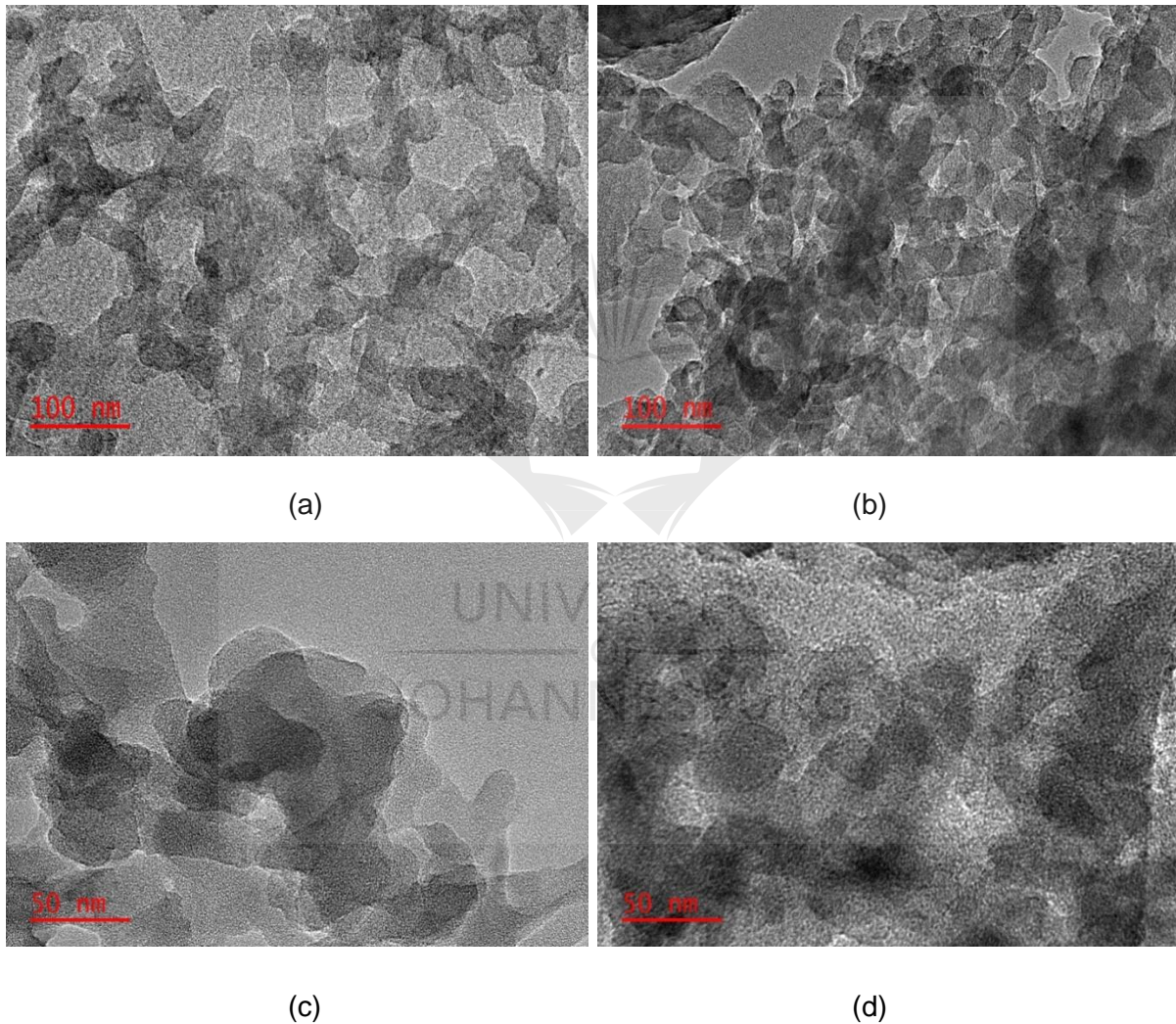


Figure 4.3: TEM images of hydrochar at 1.00kx (a) 5.00 kx (c) and AC at 1.00kx (b) 5.00kx (d) magnifications

4.1.4. EDX analysis

The EDX analysis was done to identify the elements present in the hydrochar and AC. The results of the hydrochar in Figure 4.4(a) are as follows (%): C, 38.9; O, 18.8; Si, 9.5; Al, 32.8 and the results of the AC shown in Figure 4.4(b) are as follows (%): C, 85.1; O, 13.1; P, 1.9. The high percentage of O element after activation in Figure 4.4(b) proved that the chemical properties of AC have been improved. The hydrochars that contain Al element have less porous structures [10], therefore, the AC has more porous structures since there is no Al element present in the AC as it is seen in Figure 4.4(a).

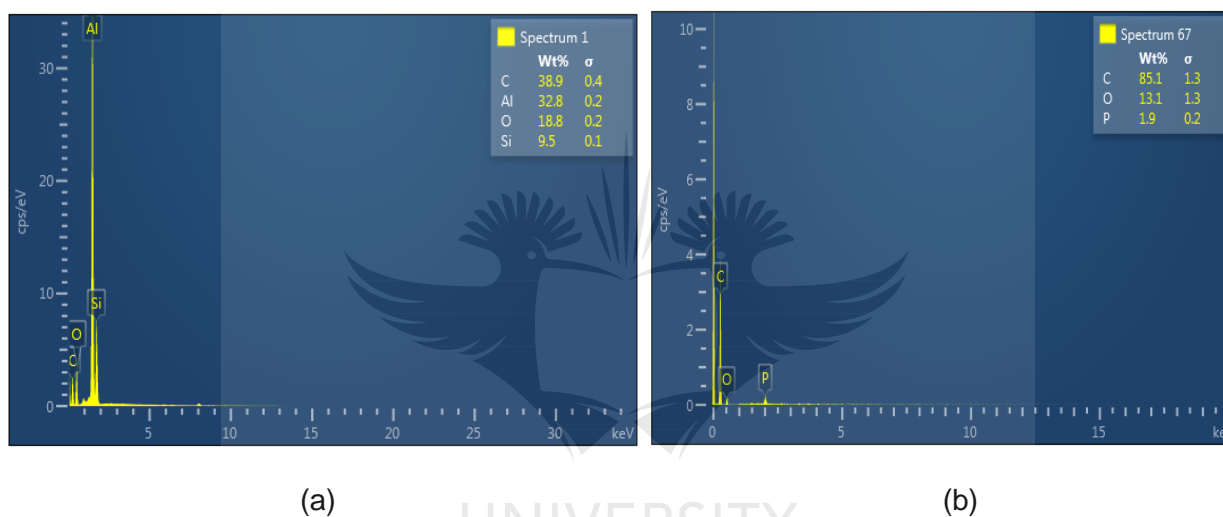
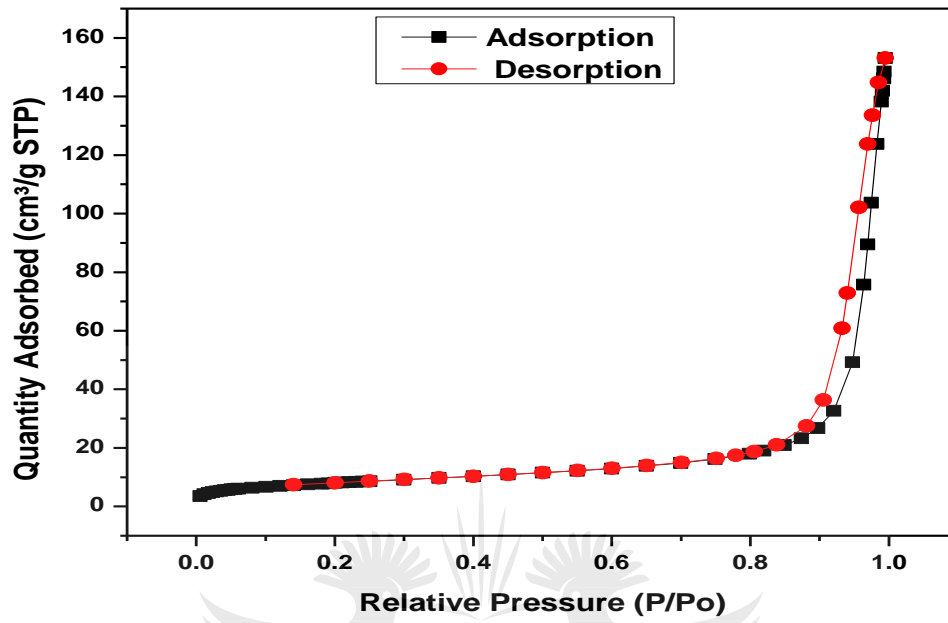


Figure 4.4: EDX spectra of (a) hydrochar and (b) AC

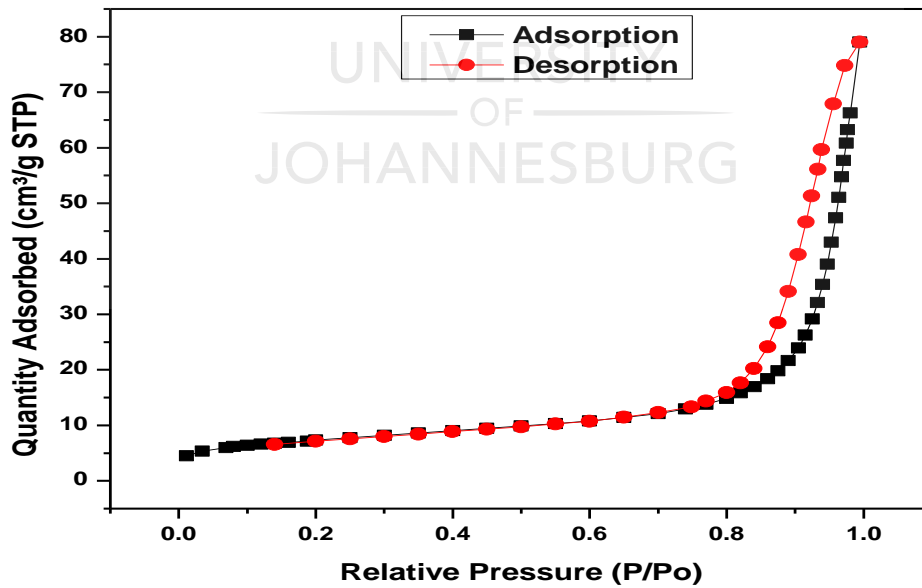
4.1.5. BET analysis

The N_2 adsorption-desorption studies were carried out to measure the average diameter, pore volume, surface area, and isotherm of the hydrochar and AC. Figure 4.5(a) and 4.5(b) show type-IV isotherm, producing an easy capillary condensation step at P/P0 of 0.6–0.1, which was due to the mesoporosity present [11]. The average diameter, pore volume, and surface area of the hydrochar shown in Figure 4.5(a) were found to be 305.7 Å, 0.223 cm³/g, and 29.16 m²/g. The average diameter, pore volume, and surface area of the AC depicted in Figure 4.5(b) were found to be 515.00 Å, 0.767 cm³/g, and 63.35 m²/g. It was revealed that the surface parameters like average diameter, pore volume, and surface area had increased after the hydrochar was

activated by heating it in a tube furnace to generate AC, therefore, the surface parameters of AC had been improved.



(a)

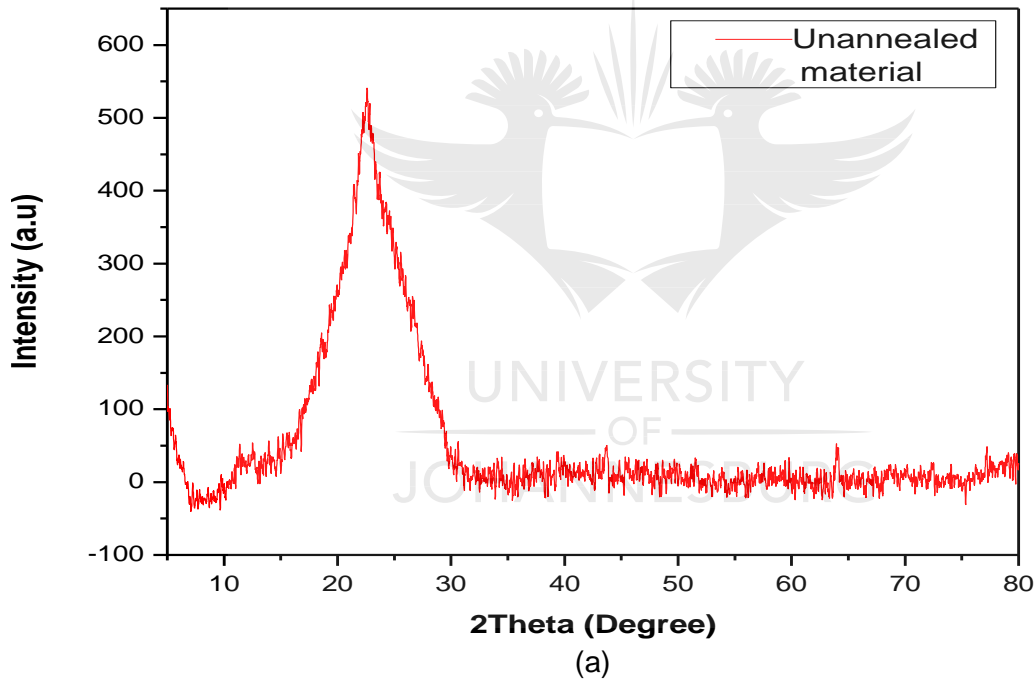


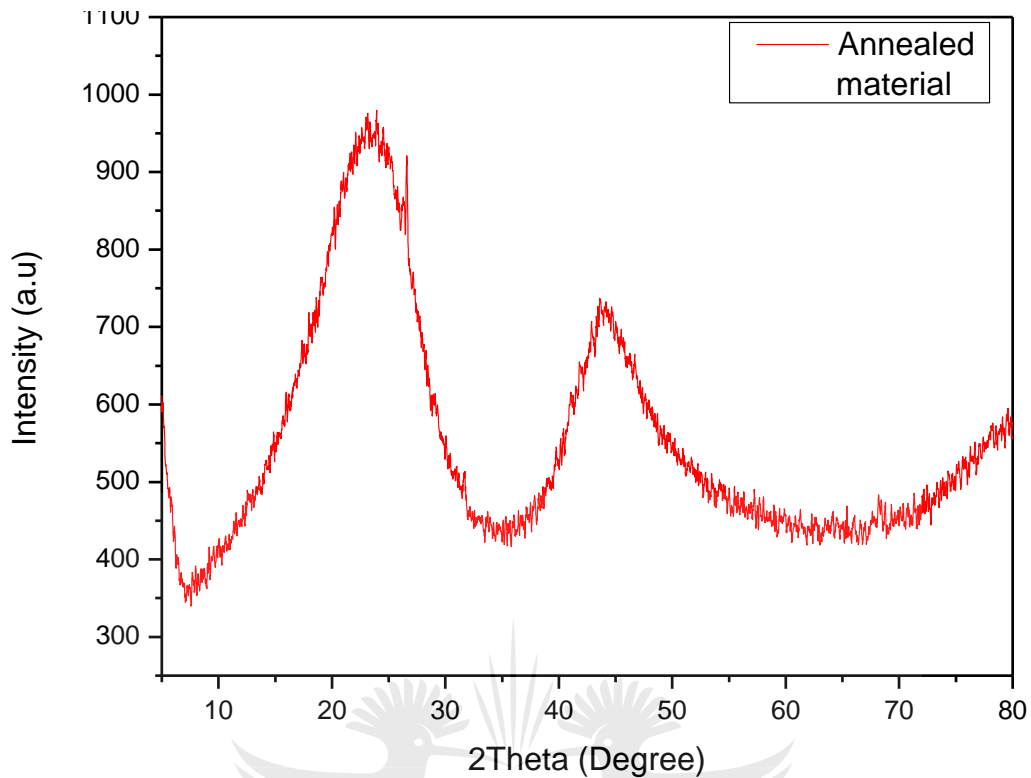
(b)

Figure 4.5: N₂ adsorption-desorption isotherm for (a) hydrochar and (b) AC

4.1.6. XRD analysis

The diffraction patterns of the hydrochar and AC are depicted in Figure 4.6(a) and 4.6(b), respectively. The peaks at around $2\theta=23^\circ$ of both hydrochar and AC in Figure 4.6(a) and 4.6(b) corresponding to the position of (002) and (100) crystal plane [12]. It suggested that the hydrochar prepared by hydrothermal carbonization (HTC) and the AC appear as porous and crystalline. The Si element was present in both the hydrochar and AC, it was confirmed in Figure 4.4(a) and 4.4(b). Consequently, the characteristic peak appearing in the 2θ angle at 45° in Figure 4.6(b) is the result of the SiO_2 impurities in the AC [13], and that peak originates from (111) plane of silicon and due to broad and medium-intensity signal [14].





(b)

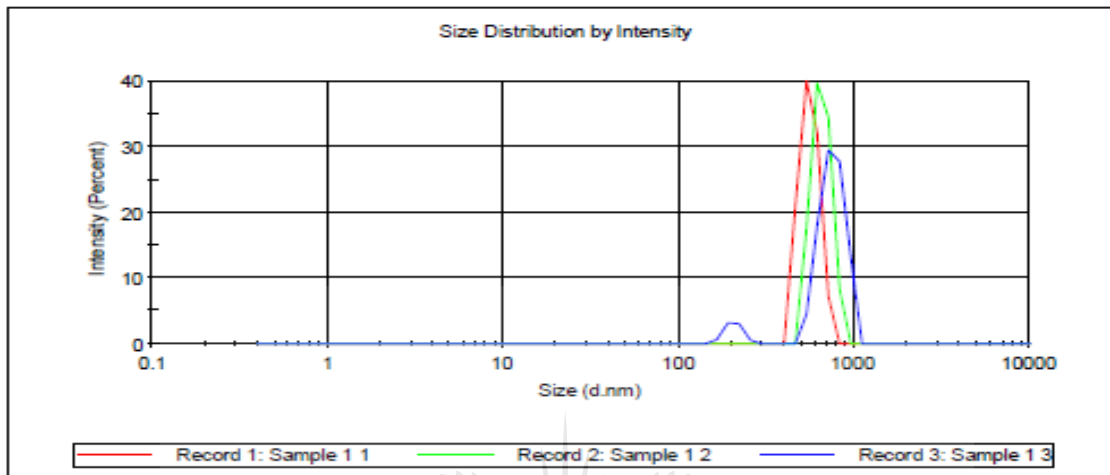
Figure 4.6: XRD patterns of (a) hydrochar and (b) AC

4.1.7. Particle size analysis

The Particle size studies were carried out to measure the particle size of the hydrochar and AC. As shown in Figure 4.7(a) and 4.7(b), the achieved average particle size values hydrochar and AC were 2084 and 3543 d.nm, respectively. The particle size of the AC was bigger than that of hydrochar, AC's chemical properties have been enhanced [15]. The particles of the AC were well dispersed in Figure 4.7(b), the annealing process removed the impurities and made AC particles to move freely without any disturbance [16]. Consequently, the AC particles increased in size.

	Size (d.n...	% Intensity:	St Dev (d.n...
Z-Average (d.nm): 2084	Peak 1: 753.0	92.8	118.2
Pdl: 0.869	Peak 2: 205.0	7.2	22.39
Intercept: 1.04	Peak 3: 0.000	0.0	0.000

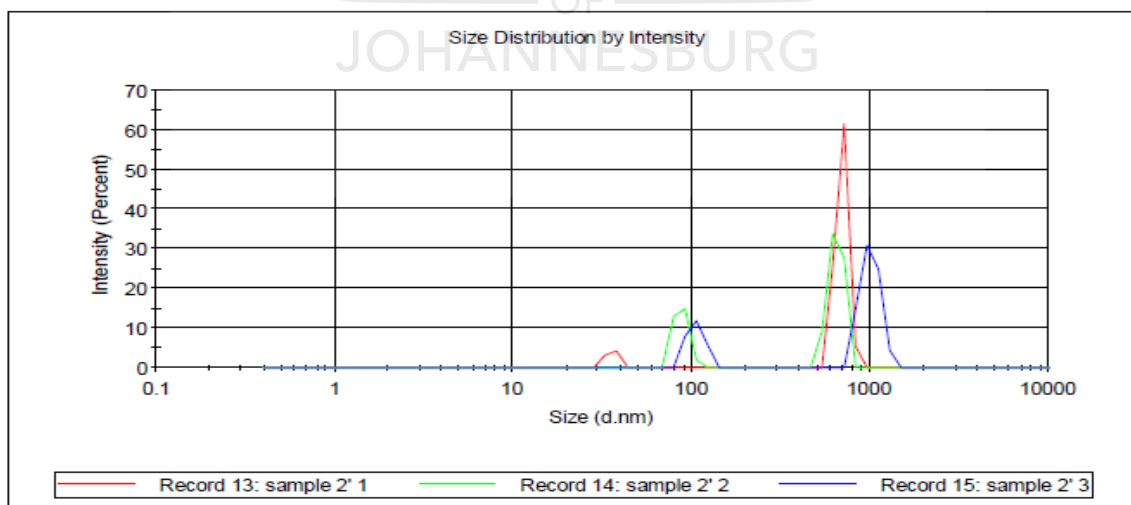
Result quality Refer to quality report



(a)

	Size (d.n...	% Intensity:	St Dev (d.n...
Z-Average (d.nm): 3543	Peak 1: 691.8	92.7	54.24
Pdl: 1.000	Peak 2: 35.64	7.3	2.553
Intercept: 1.05	Peak 3: 0.000	0.0	0.000

Result quality Refer to quality report

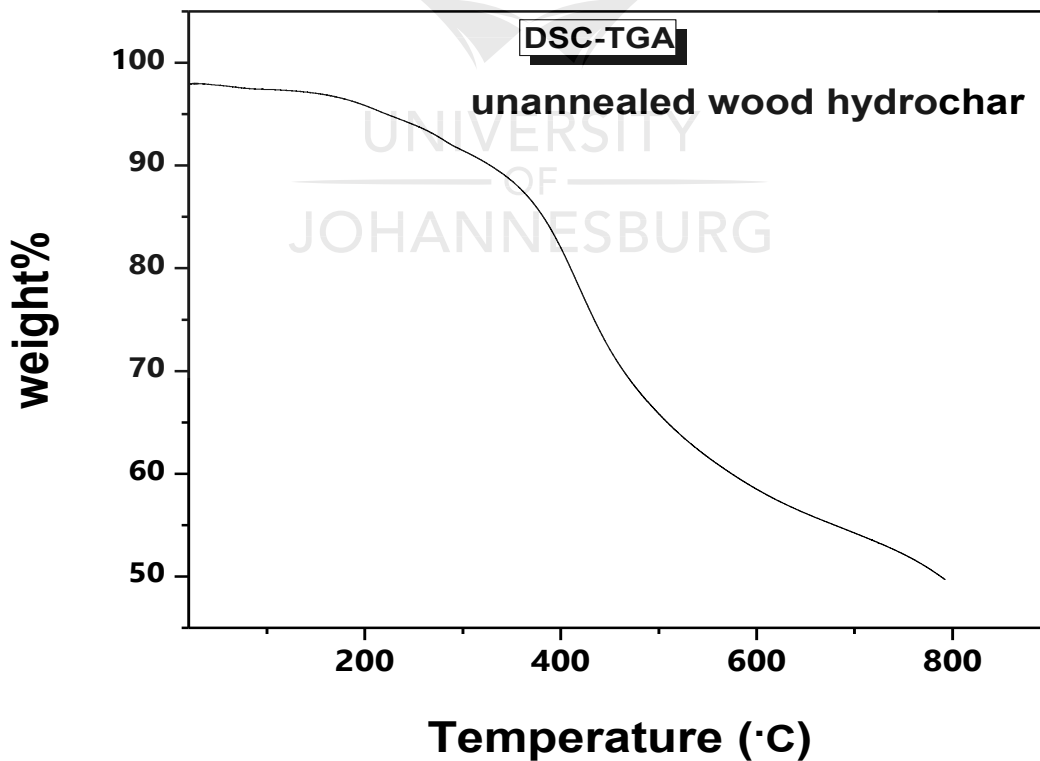


(b)

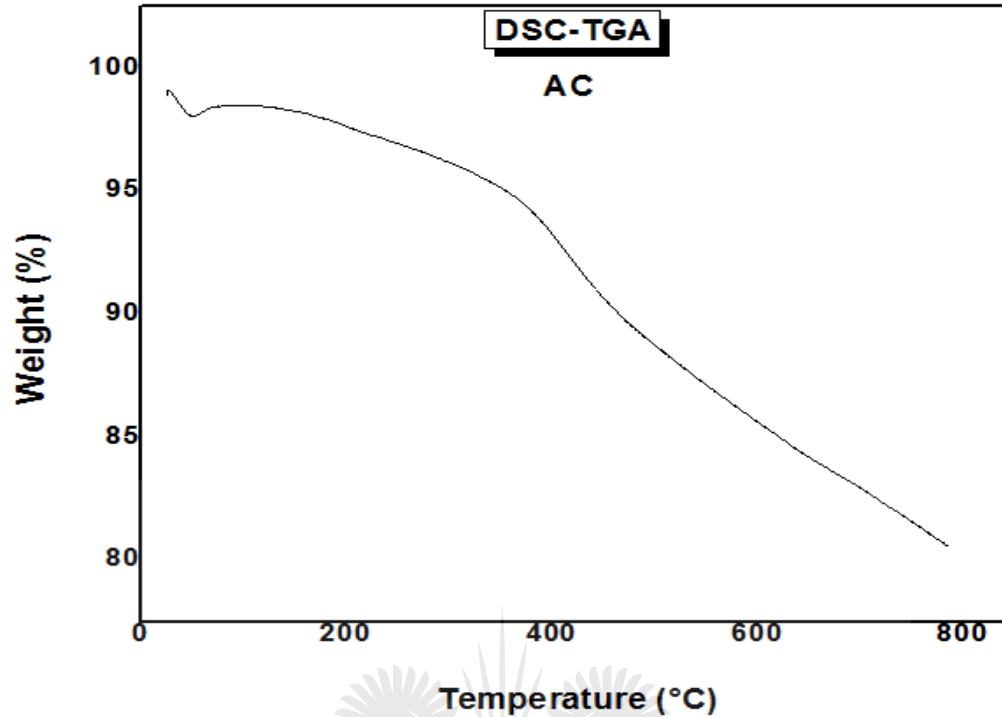
Figure 4.7: Particle size of (a) hydrochar and (b) AC

4.1.8. TGA analysis

The TGA thermograms of hydrochar and AC are shown in Figure 4.8(a) and 4.8(b). It showed that both the hydrochar and AC were not stable, they had decreased in mass with an increase in temperature. In Figure 4.8(a), there were three stages in the thermal decomposition of hydrochar during the pyrolysis: (1) the first stage occurred below 200 °C, including the removal of moisture; (2) the second stage occurred within the temperature range of 200–515 °C in which the decomposition of hemicelluloses and cellulose occurred [17]; and (3) the third stage occurred above 515 °C in which the decomposition reaction was starting to slow down. In Figure 4.8(b), there were two stages in the thermal decomposition of hydrochar during the pyrolysis: (1) the first stage occurred below 400 °C, moisture was also removed; and (2) the second stage occurred above 400 °C whereby decomposition reaction was occurring very slow. During the pyrolysis of hydrochars, the decomposition of lignin is possible within the temperature range of 455–1170 °C [18].



(a)



(b)

Figure 4.8: TGA thermogram of hydrochar and AC

4.2. ADSORPTION OF Mn(II)

4.2.1. Effect of initial metal ion concentration

The effect of initial metal ion concentration on the Mn(II) ions removal is shown in Tables 4.1 and 4.2. The results displayed that the adsorption capacity was increasing with the increase in initial metal ion concentration. That could be due to the utilization of more available active sites of the adsorbent [19]. The equilibrium was achieved and the increase in initial metal ion concentration did not bring about a positive change towards adsorption after the saturation point. This phenomenon appeared since there were no more available adsorption sites on the adsorbent materials [20]. It was evident from the listed data in Table 4.1 and 4.2 that the highest adsorption capacity was found to be 44.03 mg/g at an optimum initial metal ion concentration of 600 mg/L when hydrochar was applied while 56.31 mg/g adsorption capacity was obtained at an initial metal ion concentration of 800 mg/L when AC was used as an adsorbent.

Table 4.1: Effect of initial metal ion concentration using hydrochar in the removal of Mn(II)

Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Contact time (min)	pH
50.00	16.33	3.361	67.3	1.001	60	5.48
150.00	49.26	10.08	67.2	1.002	60	6.18
300.00	122.5	17.75	59.2	1.001	60	5.60
400.00	130.6	26.95	67.4	1.001	60	5.45
600.00	159.7	44.03	73.4	1.002	60	5.30
800.00	366.5	43.35	54.2	1.007	60	5.67
1000.00	561.5	43.85	43.9	1.002	60	5.10
1500.00	1060.00	44.00	29.3	1.002	60	5.81

Table 4.2: Effect of initial metal ion concentration using AC in the removal of Mn(II)

Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Contact time (min)	pH
50.00	3.213	4.679	93.5	1.001	60	7.01
150.00	4.235	14.58	97.2	1.007	60	7.03
300.00	5.999	29.40	98.0	1.008	60	7.02
400.00	5.000	39.50	98.7	1.008	60	7.04
600.00	229.00	37.10	61.8	1.007	60	7.01
800.00	8.879	56.31	98.9	1.001	60	6.98
1000.00	397.6	60.25	60.2	1.007	60	6.92
1500.00	1023.00	47.68	31.8	1.007	60	7.04

4.2.2. Effect of adsorbent dose

The effect of adsorbent dose on the Mn(II) ion removal was studied to attain the optimum value of adsorbent dose as shown in Table 4.3 and 4.4. It was perceived that the adsorption capacity of Mn(II) decreased as the adsorbent dose was increased when the hydrochar and AC were used as adsorbents. The highest Mn(II) adsorption capacities of 172.2 and 280.2 mg/g were achieved when hydrochar and AC were applied with the optimum adsorbent dosage of 0.25 g/L. Table 4.3 and 4.4 show the specific conditions at which the adsorption occurred. The decreasing of adsorption capacity when the adsorbent dose is increasing is attributed to the fact that the particles of the adsorbents are clustered [21, 22], as a result, the available active adsorption sites might get reduced [23]. Thus, the increasing of adsorbent dose did not improve the removal of Mn(II) ions. After the hydrochar was thermally activated, the higher removal percentage was improved from 63.2% to 88.7% as it appears in Table 4.3 and 4.4.

Table 4.3: Effect of adsorbent dose using hydrochar in the removal of Mn(II)

Adsorbent mass (g)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Contact time (min)	pH
0.251	600.00	169.6	172.2	71.7	60	5.31
0.502	600.00	180.5	83.92	69.9	60	5.31
0.750	600.00	189.3	54.80	68.5	60	5.28
1.002	600.00	191.3	40.87	68.1	60	5.26
1.251	600.00	191.8	32.66	68.0	60	5.25
1.502	600.00	184.3	27.71	69.3	60	5.22

Table 4.4: Effect of adsorbent dose using AC in the removal of Mn(II)

Adsorbent mass (g)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Contact time (min)	pH
0.2501	800.00	99.63	280.2	87.5	60	5.31

0.5013	800.00	112.2	137.6	85.9	60	5.31
0.7506	800.00	121.4	90.49	84.8	60	5.28
1.0021	800.00	129.9	67.01	83.8	60	5.26
1.2514	800.00	133.6	53.31	83.3	60	5.25
1.5013	800.00	156.4	42.91	80.5	60	5.22

4.2.3. Effect of contact time

The effect of contact time was studied as shown Table 4.5 and 4.6. In general, the adsorption process incorporates the rapid adsorption phase in the first few minutes then followed by a slower reaction to reach the equilibrium stage at a certain point in time [24, 25]. Therefore, it was seen that for the removal of Mn(II), when the hydrochar was applied the metal removal efficiency (%) increased fast when contact time was increasing up to 180 minutes and decreased as the contact time increased. The percentage removal was 66.2% with an adsorption capacity of 159.00 mg/g as listed in Table 4.5. When AC was used, the metal removal efficiency (%) increased fast when contact time was increasing up to 210 minutes and gradually decreased as the contact time increased, this could be ascribed to the available number of adsorption sites [26]. From the data in Table 4.6, it had shown that the percentage removal was 77.7% with an adsorption capacity of 248.6 mg/g.

Table 4.5: Effect of contact time using hydrochar in the removal of Mn(II)

Contact time (min)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	pH
5	600.00	299.3	120.3	50.1	0.251	5.28
10	600.00	297.5	121.00	50.4	0.251	5.08
30	600.00	279.1	128.4	53.5	0.251	5.12
60	600.00	277.4	129.1	53.8	0.252	5.37
90	600.00	250.7	139.7	58.2	0.251	5.09

120	600.00	218.3	152.7	63.6	0.251	5.24
150	600.00	208.00	156.9	65.3	0.250	5.80
180	600.00	202.6	159.00	66.2	0.250	4.68
210	600.00	249.3	140.3	58.5	0.251	4.41
240	600.00	248.00	140.9	58.7	0.251	5.53

Table 4.6: Effect of contact time using AC in the removal of Mn(II)

Contact time (min)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	pH
5	800.00	311.4	195.4	61.1	0.250	5.70
10	800.00	275.8	209.7	65.5	0.251	4.97
30	800.00	282.5	207.00	64.7	0.251	5.20
60	800.00	277.00	209.2	65.4	0.250	5.08
90	800.00	239.3	224.3	70.1	0.251	5.42
120	800.00	219.9	232.00	72.5	0.252	4.87
150	800.00	219.6	232.2	72.5	0.251	4.79
180	800.00	209.00	236.4	73.9	0.250	4.65
210	800.00	178.4	248.7	77.7	0.251	5.01
240	800.00	205.1	238.00	74.4	0.252	4.98

4.2.4. Effect of pH

One of the most important parameters studied is the effect of pH on the Mn(II) ions removal. Table 4.7 and 4.8 show the pH variation ranging from 3 to 8.5 on Mn(II) adsorption. A pH controls protons in the solution during the adsorption process [27]. When hydrochar was applied, the highest adsorption capacity of 28.32 mg/g was

obtained at pH 8, and there was a drastic drop of adsorption capacity to 9.876 mg/g at pH 8.5. When AC was applied, adsorption capacity increased as the pH was increasing. The adsorption capacity got to almost the same value from pH 4-6, the highest adsorption capacity of 254.4 mg/g was achieved at pH 7. A similar trend was reported, many metal ions precipitate in solution at pH>8 [28].

Table 4.7: Effect of pH using hydrochar in the removal of Mn(II)

pH	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Temperature (°C)	Contact time (min)
3.03	600	598.8	0.484	0.2	0.251	25	180
4.04	600	598.5	0.508	0.2	0.250	25	180
5.06	600	595.2	1.908	0.8	0.251	25	180
6.02	600	530.1	27.98	11.7	0.251	25	180
7.07	600	529.9	28.03	11.7	0.251	25	180
8.03	600	529.2	28.32	11.8	0.250	25	180
8.56	600	575.3	9.876	4.1	0.250	25	180

Table 4.8: Effect of pH using AC in the removal of Mn(II)

pH	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Temperature (°C)	Contact time (min)
3.00	800	194.4	242.2	75.7	0.250	25	210
4.02	800	179.9	248.1	77.5	0.250	25	210
5.04	800	178.3	248.7	77.7	0.250	25	210
6.03	800	181.4	247.5	77.3	0.251	25	150
7.04	800	164.1	254.4	79.5	0.250	25	150
8.02	800	191.4	243.5	76.1	0.250	25	150
8.51	800	180.4	247.8	77.5	0.252	25	210

4.2.5. Effect of temperature

The effect of temperature on the Mn(II) ions removal was assessed. The results showed that the adsorption capacity decreased with the increase in temperature as seen in Table 4.9 and 4.10. The data in Table 4.9 showed that when the hydrochar was used, the adsorption capacity decreased from 26.54 to 8.688 mg/g as the temperature was increasing from 25 to 45 °C while adsorption capacity decreased from 72.10 to 68.20 mg/g when AC was applied as it was stated in Table 4.10. The decrease in adsorption capacity with an increase in temperature showed a linear pattern that had started from the higher to the lower point of adsorption capacity [29]. When the temperature was increased the boundary layer at the adsorbate surface might have become thinner and this reduction in the boundary layer would have made the adsorbate easily to move back into the solution from the hydrochar and AC surfaces [30]. Both the hydrochar and AC removed more Mn(II) ions at the temperature of 25 °C.

Table 4.9: Effect of temperature using hydrochar in the removal of Mn(II)

Temperature (°C)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	pH	Adsorbent mass (g)	Contact time (min)
25	600.00	533.6	26.54	11.1	8.06	0.251	180
35	600.00	552.8	18.89	07.9	8.04	0.251	180
45	600.00	578.3	8.688	03.6	8.02	0.251	180

Table 4.10: Effect of temperature using AC in the removal of Mn(II)

Temperature (°C)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	pH	Adsorbent mass (g)	Contact time (min)
25	800.00	223.6	230.2	72.1	7.03	0.250	210
35	800.00	146.6	219.5	69.2	7.06	0.252	210
45	800.00	254.4	217.1	68.2	7.01	0.251	210

4.3. ADSORPTION OF Cr(VI)

4.3.1. Effect of initial metal ion concentration

The results of the effect of the initial metal ion concentration are shown in Table 4.11 and 4.12. The adsorption of Cr(VI) was very rapid at the initial points as the initial metal ion concentration was increasing as seen in Table 4.11 and 4.12. Generally, the metal ions removal is decreased as the concentration increased with increasing adsorption capacity [31]. This may be due to the utilization of more available active sites of the adsorbent at the higher initial metal ion concentration. From the data in Table 4.11, the maximum percentage removal was found to be 73.0% at an optimal initial metal ion concentration of 600 mg/L with an adsorption capacity of 43.81 mg/g when the hydrochar was used as an adsorbent. It was shown in Table 4.12 that when the AC was used as an adsorbent, the maximum percentage removal was found to be 98.8% at an optimal initial metal ion concentration of 400 mg/L with an adsorption capacity of 38.26 mg/g. As the concentration increases, the movement of metal ions in solution becomes more intense, increasing the chances of contacting with adsorption sites. Consequently, the available sites are occupied and saturated very quickly [32, 33]. Due to the limited number of adsorption sites in adsorbents, the surplus of Cr(VI) ions would remain in the solution, resulting in the lower percentage removal.

Table 4.11: Effect of initial metal ion concentration using hydrochar in the removal of Cr(VI)

Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Contact time (min)	pH
50.00	15.99	3.401	68.0	1.003	60	6.68
150.00	50.41	9.959	66.4	1.005	60	6.55
300.00	120.1	17.99	60.0	1.004	60	6.39
400.00	128.1	27.19	68.0	1.005	60	6.30
600.00	162.00	43.81	73.0	1.001	60	6.29
800.00	365.6	43.79	54.3	1.007	60	6.29

1000.00	562.1	43.79	43.8	1.009	60	6.25
1500.00	1062.00	43.73	29.2	1.008	60	6.27

Table 4.12: Effect of initial metal ion concentration using AC in the removal of Cr(VI)

Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Contact time (min)	pH
50.00	3.333	4.667	93.3	1.001	60	6.39
150.00	4.840	14.52	96.8	1.007	60	6.04
300.00	6.336	29.37	97.9	1.008	60	6.11
400.00	4.800	38.26	98.8	1.008	60	6.10
600.00	229.7	37.04	61.7	1.007	60	5.97
800.00	443.3	35.67	44.6	1.004	60	5.94
1000.00	637.8	36.22	36.2	1.007	60	5.98
1500.00	1124.00	37.65	25.1	1.007	60	5.93

4.3.2. Effect of adsorbent dose

The effect of hydrochar and AC dose on the Cr(VI) ions removal was studied as shown in Table 4.13 and 4.14. Generally, the removal of contaminants increases as the adsorbent dose increases due to the increase of active adsorption sites [34, 35]. But from Table 4.13 and 4.14 it was revealed that the adsorption capacity was high at a smaller amount of 0.25 g of hydrochar and AC. The adsorption capacity decreased as the adsorbent dose was increasing. However, parts of the hydrochar and AC as adsorbents might have generated aggregates at high dose concentrations [36], which shielded the reactive sites and reduced the adsorption capacity [37]. As it was listed in Table 4.13 and 4.14, the optimal adsorbent dose, maximum percentage removal and

adsorption capacity of the hydrochar and AC are as follows: 0.25 g, 70.2%, and 168.6 mg/g; and 0.25 g, 80.3%, and 128.5 mg/g, respectively.

Table 4.13: Effect of adsorbent dose using hydrochar in the removal of Cr(VI)

Adsorbent mass (g)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Contact time (min)	pH
0.251	600.00	178.6	168.6	70.2	60	5.31
0.502	600.00	183.5	83.31	69.4	60	5.31
0.750	600.00	192.4	54.34	67.9	60	5.28
1.002	600.00	193.00	40.70	67.8	60	5.26
1.251	600.00	193.9	32.49	67.7	60	5.25
1.502	600.00	181.00	27.93	69.8	60	5.22

Table 4.14: Effect of adsorbent dose using AC in the removal of Cr(VI)

Adsorbent mass (g)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Contact time (min)	pH
0.250	400.00	78.83	128.5	80.3	60	5.31
0.501	400.00	85.21	62.96	78.7	60	5.31
0.751	400.00	102.5	39.67	74.4	60	5.28
1.002	400.00	115.2	28.48	71.2	60	5.26
1.251	400.00	122.9	22.17	69.3	60	5.25
1.501	400.00	131.3	17.92	67.2	60	5.22

4.3.3. Effect of contact time

The effect of contact time was evaluated. According to Table 4.15 and 16, when the hydrochar was used as an adsorbent, the process of Cr(VI) adsorption involved three distinct steps. In the first step (5–60 minutes), the adsorption process was rapid. In the

second step (60–150 minutes), the adsorption process increased and reached equilibrium at 150 minutes. Lastly, (150–240 minutes), the adsorption process decreased, and a similar trend was reported in Guerra et al. (2014). The decrease in the rate of adsorption could be attributed to the exchange of Cr(VI) ions with reactive adsorption sites [38]. The percentage removal was 65.0% with an adsorption capacity of 155.9 mg/g as presented in Table 4.15. When AC was applied, the process of Cr(VI) adsorption was very quick from the beginning of the experiment and reached equilibrium at 120 minutes. It was noticeable in Table 4.16 that the percentage removal was 76.7% with an adsorption capacity of 122.7 mg/g.

Table 4.15: Effect of contact time using hydrochar in the removal of Cr(VI)

Contact time (min)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	pH
5	600.00	300.6	119.8	49.9	0.252	5.38
10	600.00	295.4	121.8	50.8	0.251	4.97
30	600.00	280.5	127.8	53.3	0.252	5.22
60	600.00	280.00	128.00	53.3	0.252	5.32
90	600.00	245.2	141.9	59.1	0.250	5.01
120	600.00	220.3	151.9	63.3	0.252	5.34
150	600.00	210.3	155.9	65.0	0.252	4.80
180	600.00	219.4	152.2	63.4	0.250	4.78
210	600.00	248.2	140.7	58.6	0.251	4.79
240	600.00	251.8	139.3	58.0	0.252	5.04

Table 4.16: Effect of contact time using AC in the removal of Cr(VI)

Contact time (min)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	pH
5	400.00	191.7	83.32	52.1	0.250	5.38
10	400.00	176.00	89.60	56	0.252	4.97
30	400.00	146.9	101.3	63.3	0.251	5.22
60	400.00	124.5	110.2	68.9	0.251	5.32
90	400.00	101.6	119.3	74.6	0.251	5.01
120	400.00	93.30	122.7	76.7	0.251	5.34
150	400.00	101.6	119.4	74.6	0.251	4.80
180	400.00	98.44	120.6	75.4	0.250	4.78
210	400.00	95.21	121.9	76.2	0.251	4.79
240	400.00	96.49	121.4	75.9	0.251	5.04

4.3.4. Effect of pH

Another imperative parameter that was studied is the effect of pH on the Cr(VI) ions removal. The range of pH values evaluated in this work were from 3 to 8.5. The effect of pH on the Cr(VI) ions removal is shown in Table 4.17 and 4.18. The process of Cr(VI) adsorption included two steps when hydrochar was used as an adsorbent. In the first step, the adsorption rate was rapid from the beginning of the experiment up to pH 5. At lower pH, the electrostatic attraction between the hydroxyl (O–H) group of the hydrochar and Cr(VI) ions resulted in high adsorption capacity [39–41]. In the last step, pH (5–8.5), the rate of the adsorption process decreased. Table 4.17 showed that the highest adsorption capacity of 119.1 mg/g was reached at pH 5 with the percentage removal of 49.6% when hydrochar was used as an adsorbent. For AC, it was seen that the adsorption process was very fast from pH 3 and reached the equilibrium at pH 7, then at pH (7–8.5) the rate of adsorption decreased. From Table 4.18, it could be seen that

when AC was used, the highest adsorption capacity of 117.4 mg/g was reached at pH 7 with the percentage removal of 73.4%.

Table 4.17: Effect of pH using hydrochar in the removal of Cr(VI)

pH	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Temperature (°C)	Contact time (min)
3.03	600	495.4	41.83	17.4	0.251	25	150
4.02	600	421.00	71.59	29.8	0.251	25	150
5.05	600	302.1	119.1	49.6	0.252	25	150
6.01	600	322.2	111.1	46.3	0.250	25	150
7.06	600	365.9	93.64	39.0	0.250	25	150
8.04	600	355.7	97.73	40.7	0.251	25	150
8.53	600	480.00	48.40	20.2	0.251	25	150

Table 4.18: Effect of pH using AC in the removal of Cr(VI)

pH	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	Adsorbent mass (g)	Temperature (°C)	Contact time (min)
3.01	400	268.00	52.80	33	0.251	25	120
4.02	400	242.9	62.84	39.3	0.251	25	120
5.03	400	186.7	85.32	53.3	0.251	25	120
6.02	400	149.7	100.1	62.6	0.250	25	120
7.05	400	106.4	117.4	73.4	0.251	25	120
8.03	400	115.2	113.9	71.2	0.251	25	120
8.51	400	121.00	111.6	69.8	0.251	25	120

4.3.5. Effect of temperature

The effect of the temperature on the adsorption was evaluated at 25, 35, and 45 °C. The effect of temperature for the removal of Cr(VI) ions is shown in Figure 4.18. In most cases, the metal ions move very fast in solution at high temperatures and new reactive adsorption sites might be developed on the surface of the adsorbents, which would then result in higher adsorption capacity [42, 43]. According to Figure 4.18, when hydrochar was used as an adsorbent, the adsorption capacity decreased from 32.53 to 27.92 mg/g as the temperature was increased from 25 to 45 °C as it was noticeable in Table 4.19. When the AC was used as an adsorbent for the Cr(VI) ions removal, the adsorption capacity decreased from 109.00 to 90.06 mg/g as the temperature was increased from 25 to 45 °C. Table 4.20 presented all the adsorption conditions. The adsorption capacity decreased since high temperatures cause the desorption of Cr(VI) from the adsorbent surface [44].

Table 4.19: Effect of temperature using hydrochar in the removal of Cr(VI)

Temperature (°C)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	pH	Adsorbent mass (g)	Contact time (min)
25	600.00	274.8	32.53	54.2	5.26	1.009	60
35	600.00	291.4	30.86	51.4	5.24	1.001	60
45	600.00	320.8	27.92	46.5	5.21	1.007	60

Table 4.20: Effect of temperature using AC in the removal of Cr(VI)

Temperature (°C)	Initial conc. (mg/L)	Final conc. (mg/L)	Adsorption capacity (mg/g)	Metal removal efficiency (%)	pH	Adsorbent mass (g)	Contact time (min)
25	400.00	127.6	109.00	68.1	7.06	0.251	120
35	400.00	156.00	97.60	61.0	7.04	0.251	120
45	400.00	174.9	90.06	56.3	7.01	0.250	120

4.4. ADSORPTION ISOTHERM MODELS

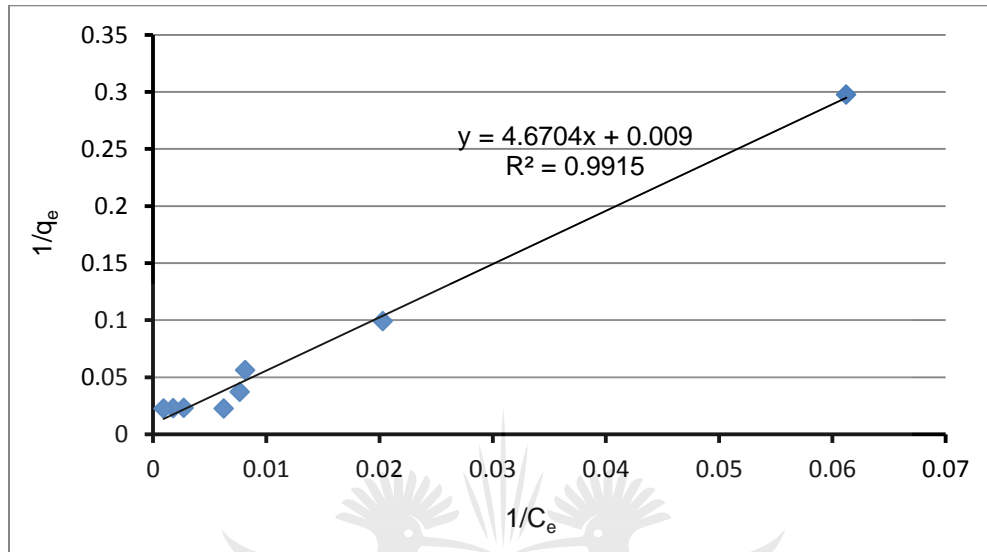
4.4.1 Langmuir and Freundlich isotherms

Adsorption isotherms play a very important role in adsorption processes. Langmuir and Freundlich isotherm [45, 46] were used for modeling the experimental data. These isotherms are grounded on the type of interaction and the nature of the adsorbent materials. Table 4.21 and 4.22 listed Langmuir isotherm model parameters for the adsorption of Mn(II) and Cr(VI) onto hydrochar and AC. The $1/C_e$ vs $1/q_e$ were plotted and the trend-line was used to determine the equations and the coefficients of determination, in Figure 4.19, the obtained coefficients of determination of the Langmuir model for Mn(II) metal ions were $R^2 = 0.9915$ for hydrochar and $R^2 = 0.9924$ for AC. Similar R^2 values were reported for the adsorption of Pb(II) by banana peel [47]. The obtained coefficients of determination of the Langmuir model for Cr(VI) metal ions were $R^2 = 0.5326$ for hydrochar and $R^2 = 0.5082$ for AC Cr(VI) metal ions as it is displayed in Figure 4.20. The data was fitted well with the Langmuir model [48]. Therefore, there was only a monolayer on the on hydrochar and AC surface as it was assumed by the Langmuir model. The high value of the coefficients of determination indicates a better adsorption process [49].

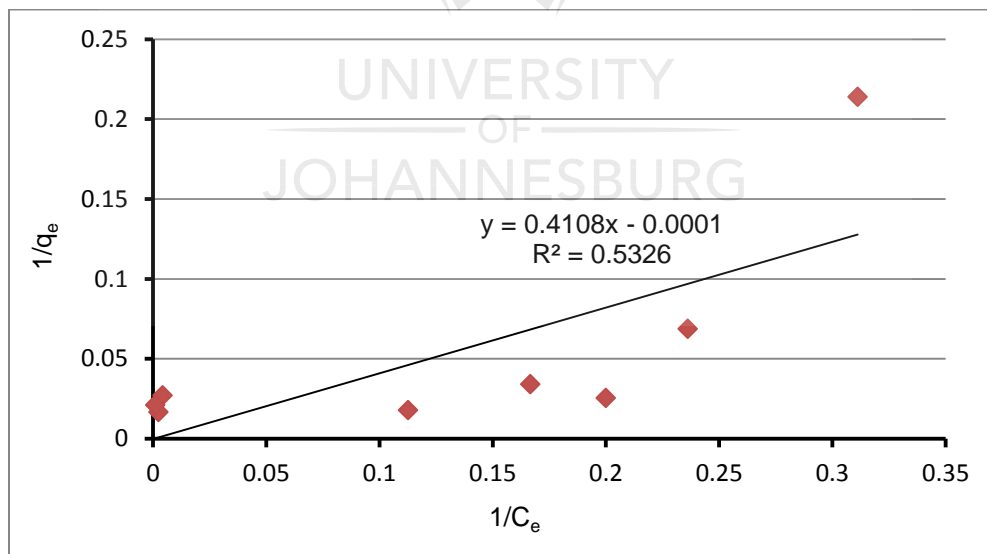
Table 4.21: Langmuir isotherm x and y axes values for the adsorption of Mn(II) onto hydrochar and AC

Hydrochar		AC	
$1/C_e$	$1/q_e$	$1/C_e$	$1/q_e$
0.061	0.298	0.312	0.214
0.020	0.099	0.236	0.069
0.008	0.056	0.167	0.034
0.008	0.037	0.200	0.025
0.007	0.023	0.004	0.027
0.003	0.023	0.113	0.018

0.002	0.023	0.003	0.017
0.001	0.023	0.001	0.021



(a)

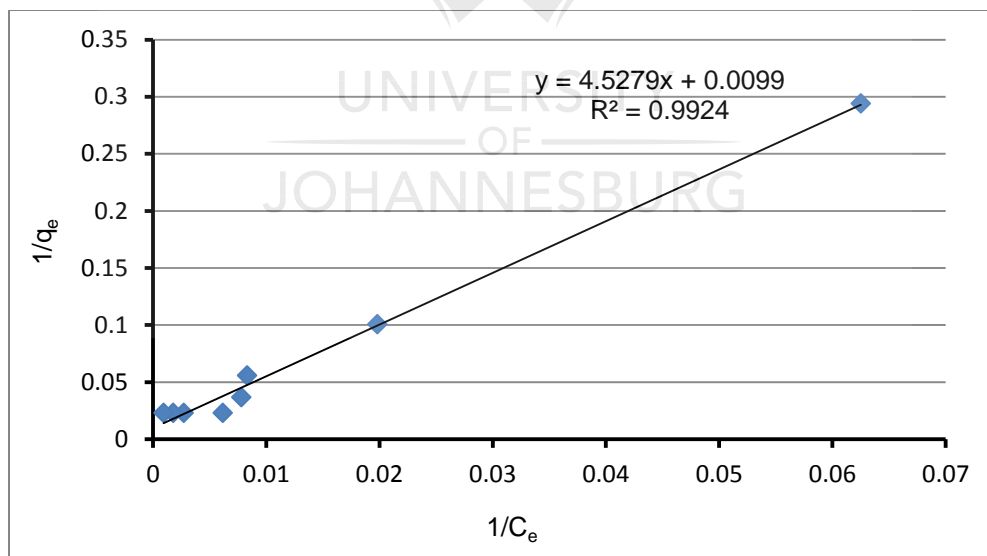


(b)

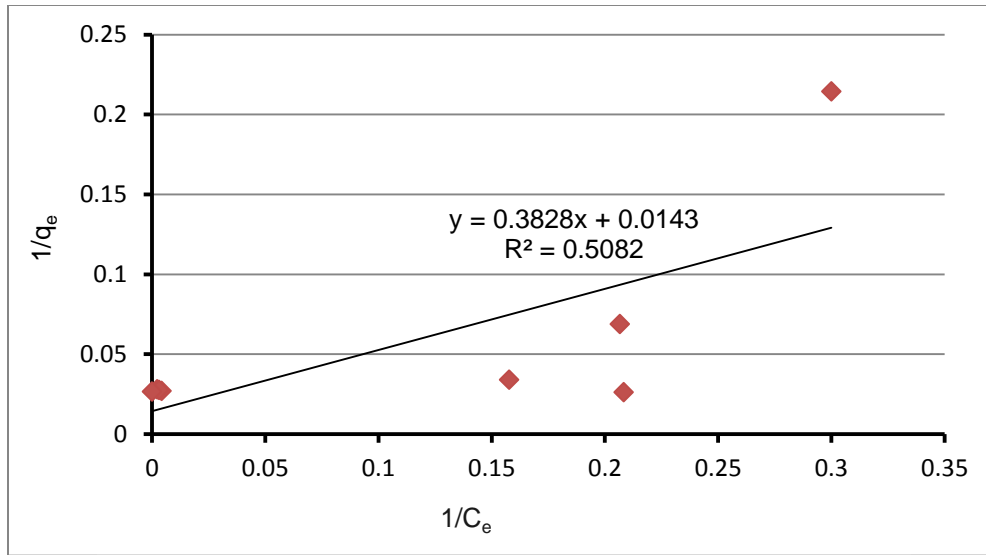
Figure 4.9: Plots of the for Langmuir isotherm for the adsorption of Mn(II) onto (a) Hydrochar, (b) AC

Table 4.22: Langmuir isotherm x and y axes values for the adsorption of Cr(VI) onto hydrochar and AC

Hydrochar		AC	
$1/C_e$	$1/q_e$	$1/C_e$	$1/q_e$
0.063	0.294	0.300	0.214
0.020	0.100	0.207	0.069
0.008	0.056	0.158	0.034
0.008	0.037	0.208	0.026
0.006	0.023	0.004	0.027
0.003	0.023	0.002	0.028
0.002	0.023	0.003	0.027
0.001	0.023	0.001	0.027



(a)



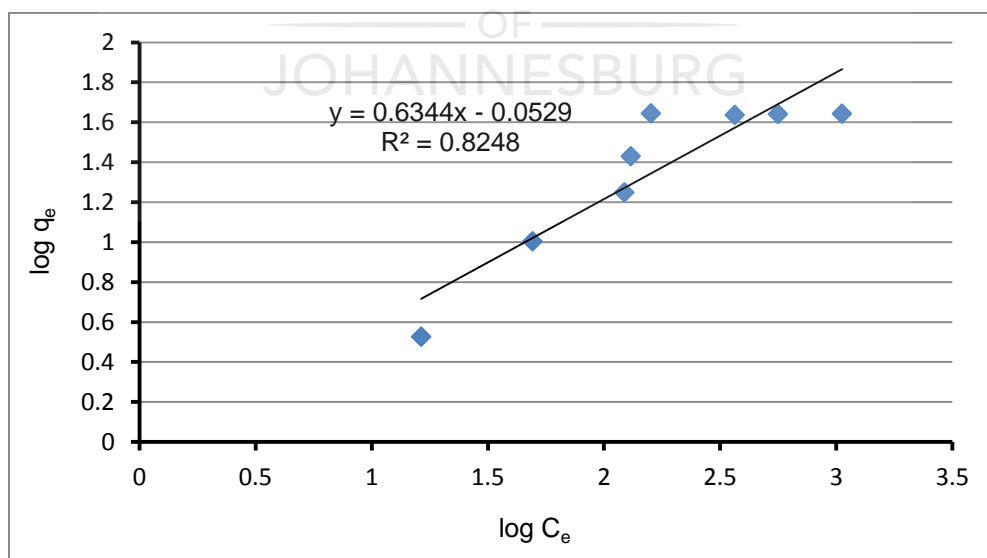
(b)

Figure 4.10: Langmuir isotherm plot for the adsorption of Cr(VI) onto (a) Hydrochar, (b) AC

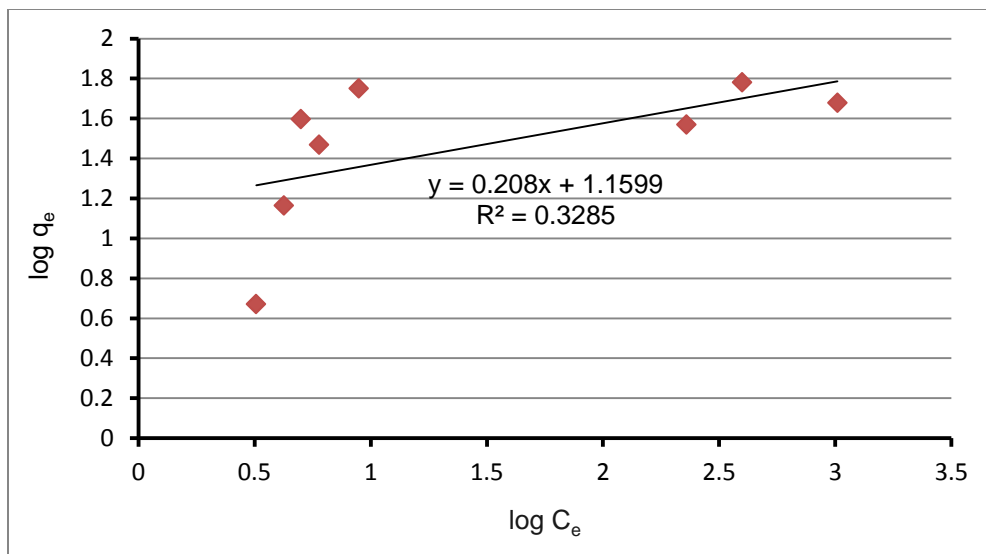
As for the Freundlich model, the logarithm of C_e (the amount of metal ion adsorbed in unit of adsorbent mass) was plotted against the logarithm of q_e (the equilibrium concentration of the metal ion) a straight line was obtained. Table 4.23 and 4.24 listed Freundlich isotherm model parameters for the adsorption of Mn(II) and Cr(VI) onto hydrochar and AC. Figure 4.21 and 4.22 showed the obtained coefficients of determination of the Freundlich model for Mn(II) metal ions to be $R^2 = 0.8248$ for hydrochars and $R^2 = 0.3285$ for AC while the obtained coefficients of determination to be $R^2 = 0.8261$ for hydrochars and $R^2 = 0.3648$ for AC of the Cr(VI) metal ions. Langmuir adsorption isotherm was the best model for the metal ions adsorption onto hydrochar and AC. The essential features of the Langmuir adsorption isotherm parameter can be used to predict the affinity between the sorbate and sorbent using a dimensionless constant called separation factor or equilibrium parameter, which is expressed by the following relationship [50–52].

Table 4.23: Freundlich isotherm x and y axes values for the adsorption of Mn(II) onto hydrochar and AC

Hydrochar		AC	
log C _e	log q _e	log C _e	log q _e
1.213	0.527	0.507	0.670
1.692	1.003	0.627	1.164
2.088	1.249	0.778	1.468
2.116	1.430	0.699	1.597
2.203	1.644	2.360	1.569
2.564	1.637	0.948	1.751
2.749	1.642	2.599	1.770
3.025	1.643	3.001	1.678



(a)

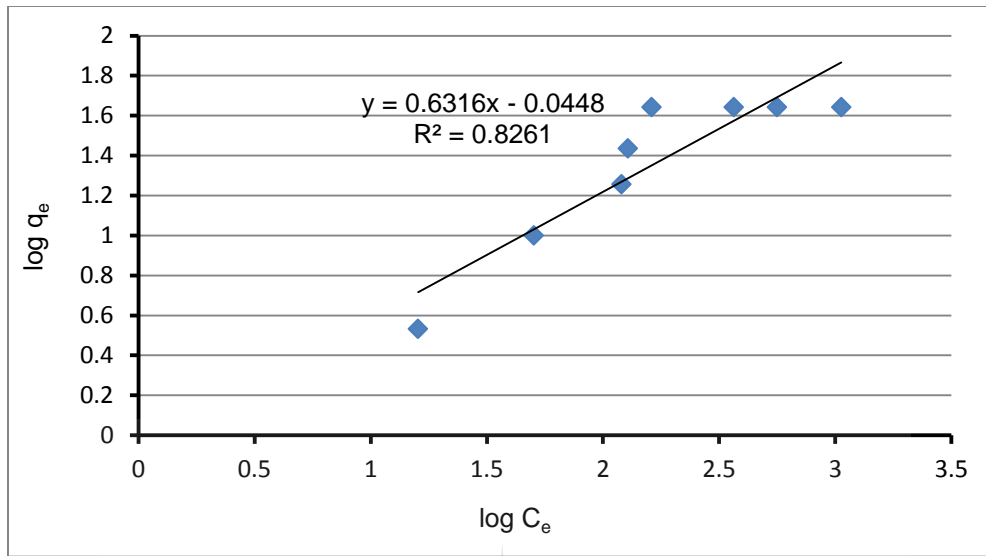


(b)

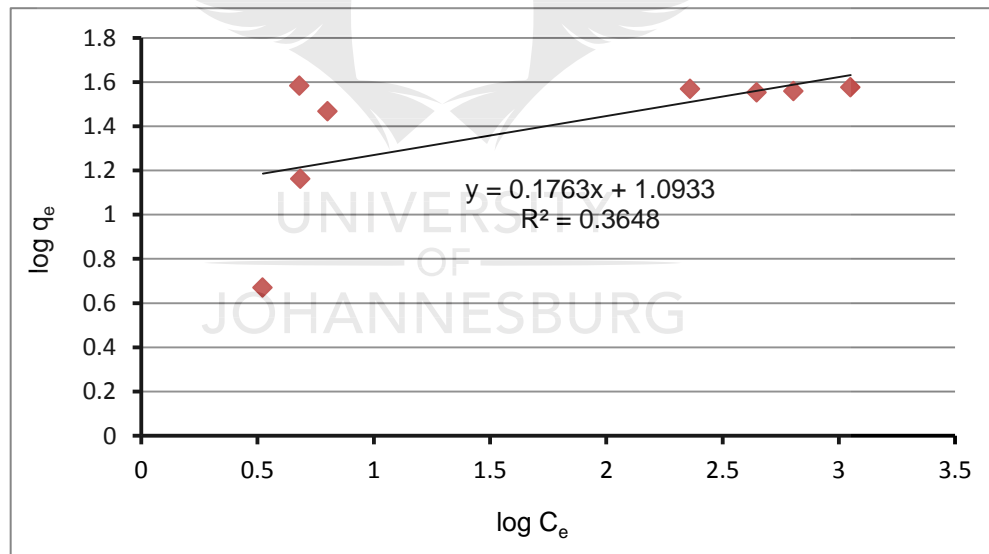
Figure 4.11: Plots of the Freundlich isotherm for the adsorption of Mn(II) onto (a) Hydrochar, (b) AC

Table 4.24: Freundlich isotherm x and y axes values for the adsorption of Cr(VI) onto hydrochar and AC

Hydrochar		AC	
log C _e	log q _e	log C _e	log q _e
1.204	0.532	0.523	0.669
1.703	0.998	0.685	1.162
2.080	1.255	0.802	1.468
2.107	1.434	0.681	1.583
2.209	1.642	2.361	1.569
2.563	1.641	2.647	1.552
2.750	1.641	2.805	1.559
3.026	1.641	3.051	1.576



(a)



(b)

Figure 4.12: Plots of the Freundlich isotherm for the adsorption of Cr(VI) onto (a) Hydrochar, (b) AC

4.5. REFERENCES

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5.1. CONCLUSIONS

The aim of this study was to produce PCS (hydrochar and AC) from the wood chips and evaluate their potential as adsorbents for toxic inorganic ions from aqueous systems. In the process of producing PCS, to ensure that the PCS would be suitable for inorganic ion adsorption, the reaction pressure, temperature, and time were successfully investigated. After the hydrochar was produced, then its AC was generated through annealing process shown (Figure 3.1) and explained in chapter 3. The hydrochar and AC were characterized by FTIR, XRD, BET, SEM, TGA, TEM, EDX, and DLS. The properties of AC were improved compared to hydrochar, the moisture was removed from the AC and that was confirmed by the first stage of TGA thermogram (Figure 4.8) that occurred below 200 °C and it was complemented by the reduced peak of a hydroxyl group from the FTIR (Figure 4.1(b)). The AC's surface area and particle sizes increased (Figure 4.5 and 4.7). Therefore, hydrochar and AC were used as adsorbents for the removal of Mn(II) and Cr(VI) from aqueous solutions. Based on the results of this study, the investigated adsorption capacity for Mn(II) was found to be 44.03 mg/g when hydrochar was applied while 56.31 mg/g adsorption capacity was obtained when AC was used. The investigated adsorption capacity for Cr(VI) was 43.81 mg/g when the hydrochar was applied and 38.26 mg/g was obtained when the AC was used as an adsorbent. The results showed that the AC removed more Mn(II) and less Cr(VI) ions than the hydrochar did, hydrochar removed 73.4% and AC 98.9% of Mn(II); and hydrochar removed 73.0% and AC removed 98.8% of Cr(VI). The optimum parameter conditions for the adsorption of Mn(II) were pH 8, adsorbent dose=0.25 g/L, contact time=180 mins, initial metal ions concentration=600 mg/g, and temperature= 25°C when the hydrochar was used as an adsorbent; and pH 7, adsorbent dose=0.25 g/L, contact time=210 mins, initial metal ions concentration=800 mg/g, and temperature=25°C when the AC was used as an adsorbent. Then the optimum parameter conditions for the adsorption of Cr(VI) were pH 5, adsorbent dose=0.25 g/L, contact time=150 mins, initial metal ions concentration=600 mg/g, and temperature= 25°C when the hydrochar was used as an adsorbent; and pH 7, adsorbent dose=0.25 g/L, contact time=120 mins,

initial metal ions concentration=400 mg/g, and temperature=25°C when the AC was used as an adsorbent. Langmuir and Freundlich isotherms were used to model the experimental data and the adsorption process favored the Langmuir model with coefficient of determination of $R^2 = 0.9915$ for hydrochar and $R^2 = 0.9924$ for AC for the removal of Mn(II) and $R^2 = 0.5326$ for hydrochar and $R^2 = 0.5082$ for AC for the removal of Cr(VI).

5.2. RECOMMENDATIONS

Although some works have already been done on the production of PCS through HTC and their application as adsorbents for potentially toxic elements in water and wastewater. For further studies, the following are recommended:

- Chemical activation of PCS and their application as adsorbents for potentially toxic elements in water and wastewater.
- The application of chemically and thermally activated PCS in environmental samples.

