


Unidirectional magnetoresistance and spin-orbit torque in NiMnSb

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Spin-dependent transport phenomena due to relativistic spin-orbit coupling and broken space-inversion symmetry are often difficult to interpret microscopically, in particular when occurring at surfaces or interfaces. Here we present a theoretical and experimental study of spin-orbit torque and unidirectional magnetoresistance in a model room-temperature ferromagnet NiMnSb with inversion asymmetry in the bulk of this half-Heusler crystal. Aside from the angular dependence on magnetization, the competition of Rashba- and Dresselhaus-type spin-orbit couplings results in the dependence of these effects on the crystal direction of the applied electric field. The phenomenology that we observe highlights potential inapplicability of commonly considered approaches for interpreting experiments. We point out that, in general, there is no direct link between the current-induced nonequilibrium spin polarization inferred from the measured spin-orbit torque and the unidirectional magnetoresistance. We also emphasize that the unidirectional magnetoresistance has not only longitudinal but also transverse components in the electric field: current indices which complicate its separation from the thermoelectric contributions to the detected signals in common experimental techniques. We use the theoretical results to analyze our measurements of the on-resonance and off-resonance mixing signals in microbar devices fabricated from an epitaxial NiMnSb film along different crystal directions. Based on the analysis we extract an experimental estimate of the unidirectional magnetoresistance in NiMnSb.

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I. INTRODUCTION

Anisotropic magnetoresistance (AMR) is an example of a relativistic transport phenomenon in ferromagnets with a long history. McGuire and Potter [1] provided a phenomenological model that fully explained the angular dependence of AMR. The model was based on a general argument that the magnetization-dependent conductivity tensor $\sigma_{ij}(\mathbf{m})$, like any other observable [2], reflects the symmetry of the ferromagnetic crystal. This means that if a symmetry operation belongs to the crystallographic point group, the conductivity tensor is left invariant under the same symmetry operation. As an example, when an electrical current flows in an isotropic (polycrystalline) ferromagnet, the magnetization direction defines the only axis of rotational symmetry, which results in a $\cos(2\theta)$ angular dependence of AMR, with θ being the angle between the magnetization and the current.

While AMR is allowed by symmetry in any magnetic system, ferromagnetic conductors with an inversion-asymmetric crystal structure have been more recently identified as a fruitful platform for discovering and utilizing a range of new relativistic spintronics phenomena [3–8]. Apart from the

exchange field \mathbf{B}_{ex} , which splits the electronic structure in majority- and minority-spin bands, the inversion-symmetry breaking in the lattice together with spin-orbit coupling introduces an additional splitting $\Delta H_{\text{SO}} = \mathbf{B}_{\text{SO}}(\mathbf{k}) \cdot \mathbf{s}$. Here $\mathbf{B}_{\text{SO}}(\mathbf{k})$ is an effective magnetic field that depends on the crystal momentum \mathbf{k} , while \mathbf{s} represents the spin polarization. The key property of $\mathbf{B}_{\text{SO}}(\mathbf{k})$ is that it is odd in \mathbf{k} and thus it results in opposite spin splitting for opposite \mathbf{k} . In inversion-asymmetric strained zinc-blende semiconductors like GaAs, $\mathbf{B}_{\text{SO}}(\mathbf{k})$ is a combination of Rashba and Dresselhaus symmetry terms, $\mathbf{B}_{\text{SO}}^{\text{R}}(\mathbf{k}) \propto (k_y, -k_x)$ and $\mathbf{B}_{\text{SO}}^{\text{D}}(\mathbf{k}) \propto (k_x, -k_y)$. A direct manifestation of this splitting is found in the spin-orbit torque (SOT) [9] in, e.g., (Ga,Mn)As, that emerges when an electrical current is applied to this inversion-asymmetric ferromagnetic semiconductor [3–6]. In metallic systems such as half-Heusler NiMnSb studied here, $\mathbf{B}_{\text{SO}}(\mathbf{k})$ is not described by the simple linear-in- \mathbf{k} Rashba and Dresselhaus form. SOT, nevertheless, contains Rashba- and Dresselhaus-type terms analogous to those observed in the zinc-blende semiconductors as those reflect the crystal symmetry which is the same in zinc-blende and half-Heusler crystals [8].

SOT in bulk noncentrosymmetric crystals is associated with a current-induced nonequilibrium spin polarization $\delta\mathbf{s}_{\text{SO}}$, an effect often referred to as the Edelstein effect or the inverse spin-galvanic effect (iSGE) [9–14]. When $\delta\mathbf{s}_{\text{SO}}$ is perpendicular to the magnetization, it will exert a torque on it via the

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exchange coupling. The component of $\delta\mathbf{s}_{\text{SO}}$ that is parallel to \mathbf{B}_{ex} does not lead to a magnetization torque and is, therefore, transparent to any experimental method that relies on driving the magnetization out of equilibrium by SOT [5,9,15].

Aside from SOT, $\mathbf{B}_{\text{SO}}(\mathbf{k})$ together with \mathbf{B}_{ex} can also lead to magnetotransport terms that are second order in the applied electric field and, unlike the first-order AMR, are odd under the magnetization. The unidirectional magnetoresistance (UMR) is an example of such a second-order magnetotransport effect that was previously reported in non-centrosymmetric ferromagnet/paramagnet bilayers or bulk ferromagnets [16,17]. The origin of UMR was considered to be closely connected to the phenomenology of the giant magnetoresistance (GMR) [17–20]. While in the GMR multilayer, the fixed reference ferromagnetic layer acts as an external source of spin $\delta\mathbf{s}$, in UMR this is replaced with $\delta\mathbf{s}_{\text{SO}}$ generated internally by the spin-orbit coupling. As for GMR, spin-dependent scattering within the ferromagnet results in this scenario in a different resistance depending on the orientation of $\delta\mathbf{s}_{\text{SO}}$ relative to the magnetization of the probed ferromagnet. Moreover, the accumulated spin can introduce a proportional change in the exchange splitting of the bands, further affecting the conductivity by influencing spin transmission of minority and majority spins. Another UMR mechanism considers that the magnons' population of the ferromagnet is increased or decreased depending on the orientation of $\delta\mathbf{s}_{\text{SO}}$ relative to the magnetization. This leads to a change in the average magnetization, which also results in a net change of the magnetoresistance. Although it is possible to experimentally distinguish these different contributions for their particular dependence on current density and magnetic field [20,21], they all share a common origin in the component of $\delta\mathbf{s}_{\text{SO}}$ collinear with the ferromagnet's magnetization.

In Sec. II we report our symmetry analysis and *ab initio* calculations of current-induced spin polarization and UMR in NiMnSb. We use this model system to highlight potential misconceptions when inferring these quantities from experiment. In Sec. III we then discuss our measurements in NiMnSb microbars patterned along different crystal directions, and in Sec. IV we summarize our main results.

II. THEORETICAL RESULTS AND GENERAL IMPLICATIONS FOR THE ANALYSIS OF EXPERIMENTS

A. Current-induced spin polarization and spin-orbit torque

The tetragonal distortion of the noncentrosymmetric cubic unit cell of NiMnSb, induced by the lattice mismatch with the substrate, lowers its symmetry to a $-42m$ symmetry point group and results in a Dresselhaus-type k -linear term of the spin-orbit coupling. Experiments in NiMnSb epilayers show an additional Rashba-type k -linear term of the spin-orbit coupling which we model by introducing a shear strain [8]. This lowers the symmetry further to a point group $mm2$. When an electrical current is passed in the plane perpendicular to the growth direction, carriers acquire a nonequilibrium spin polarization $\delta\mathbf{s}_{\text{SO}}$, which in general can be decomposed into a component that is parallel to the in-plane magnetization of the NiMnSb film $\delta\mathbf{s}_{\text{SO}}^{\parallel}$ and a component that is perpendicular to it $\delta\mathbf{s}_{\text{SO}}^{\perp}$. This includes both intrinsic and extrinsic contributions.

We use *ab initio* calculations to evaluate the current-induced nonequilibrium spin polarization as a function of the directions of magnetization and applied electric field (see Appendix C for the description of the numerical method). We consider here only the in-plane components of current-induced spin polarization since this is the component relevant for the UMR and the fieldlike torque. For these calculations we used the relaxation time τ chosen so that the theoretical conductivity matches the experimental value of $3.3 \times 10^4 \text{ S cm}^{-1}$. The tetragonal and shear strains are chosen to make the Rashba and Dresselhaus contributions of comparable strength [8], resulting in a nontrivial dependence of $\delta\mathbf{s}_{\text{SO}}$ on the crystal direction of the applied electric field. In Fig. 1 we plot the perpendicular ($\delta\mathbf{s}_{\text{SO}}^{\perp}$) and parallel ($\delta\mathbf{s}_{\text{SO}}^{\parallel}$) components of the current-induced nonequilibrium spin polarization. The dependence of $\delta\mathbf{s}_{\text{SO}}^{\perp} \sim \cos(\theta - \theta_{\text{SO}})$ on the magnetization angle θ corresponds to what we would expect to find for a fieldlike SOT generated by a magnetization-independent effective spin-orbit field $\mathbf{h}_{\text{SO}} \approx -J_{\text{ex}}\delta\mathbf{s}_{\text{SO}}/m$, where J_{ex} is the exchange constant between carrier spins and the in-plane magnetization \mathbf{m} . θ_{SO} would then correspond to the angle of $\delta\mathbf{s}_{\text{SO}}$ for the given crystal direction of the applied electric field. In our case, $\theta_{\text{SO}} = 0$ for the electric field along [110] or $[1\bar{1}0]$ axes since the Rashba- and Dresselhaus-type spin-orbit fields are (anti)parallel for these two crystal directions. For [100] or [010] axes, the two spin-orbit fields are orthogonal to each other and their vector sum results in $\theta_{\text{SO}} \neq 0$.

Remarkably, when we include $\delta\mathbf{s}_{\text{SO}}^{\parallel}$, total $\delta\mathbf{s}_{\text{SO}}$ becomes magnetization dependent (see Fig. 1). We emphasize that this dependence of $\delta\mathbf{s}_{\text{SO}}$ (\mathbf{h}_{SO}) on the magnetization angle would be invisible when measuring SOT, which only depends on $\delta\mathbf{s}_{\text{SO}}^{\perp}$. SOT can be reliably obtained from on-resonance mixing-signal measurements since the detected signal can be directly attributed to the precessing magnetization driven by the SOT. Our calculations in Fig. 1 demonstrate, however, that a simple harmonic dependence of $\delta\mathbf{s}_{\text{SO}}^{\perp}$ on the magnetization angle, when inferred from the SOT measurement, does not imply that the total $\delta\mathbf{s}_{\text{SO}}$ is constant and that its parallel component $\delta\mathbf{s}_{\text{SO}}^{\parallel}$ is a 90° phase shifted replica of the perpendicular component. Therefore, if considering $\delta\mathbf{s}_{\text{SO}}^{\perp}$ as the driving mechanism behind UMR, SOT measurements cannot be, in general, used to quantify experimentally $\delta\mathbf{s}_{\text{SO}}^{\parallel}$ in a given structure.

B. Unidirectional magnetoresistance

When writing the total current density j up to the second order in the applied electric field E as

$$j_i = j_i^{(1)} + j_i^{(2)} = \sigma_{ij}E_j + \xi_{ijk}E_jE_k, \quad (1)$$

UMR has been associated with the longitudinal component of the ξ_{ijk} transport coefficient [16,17]. Formally, ξ_{ijk} is described by the second-order quantum mechanical Kubo formula. However, finding accurate solutions of the formula is a major challenge, in particular in the presence of electron scattering. Here we analyze ξ_{ijk} using a semiclassical Boltzmann approximation, where

$$\xi_{ijk} = -\frac{e^3\tau^2}{2} \sum_n \int \frac{d\mathbf{k}}{(2\pi)^3} v_n^i v_n^j v_n^k \frac{\partial^2 f_0}{\partial \epsilon_n(\mathbf{k})^2}, \quad (2)$$

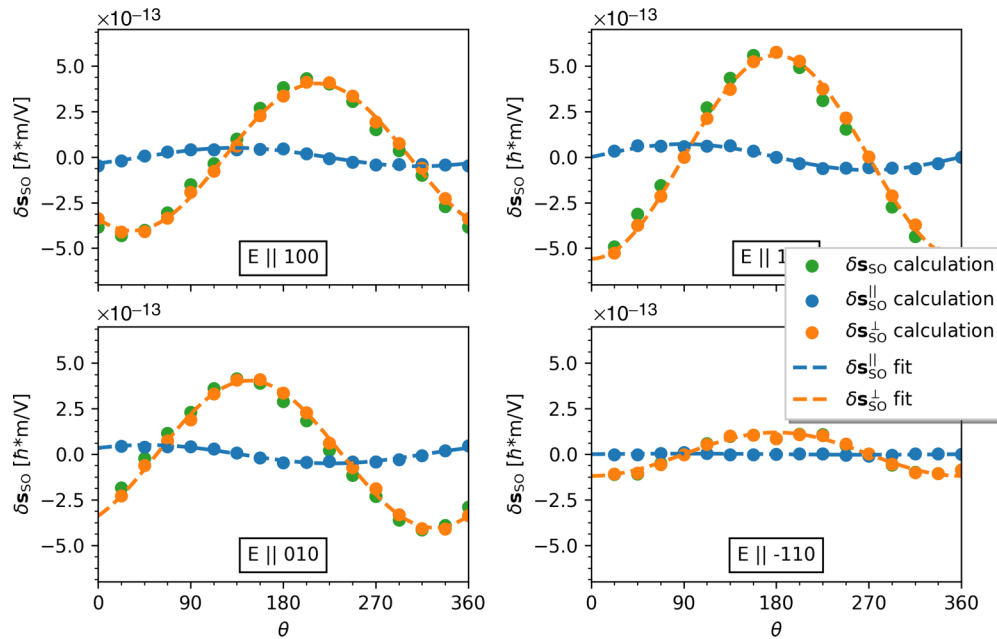


FIG. 1. Calculations of current-induced spin polarization for different directions of electric field. The plots show the total spin polarization, as well as its components that are longitudinal and transverse to the magnetization, as a function of the magnetization orientation within the (001) plane. In each plot, θ denotes the angle of the magnetization measured from the electric field. Dashed lines represent harmonic fits to the numerical points.

and $\mathbf{v}_n(\mathbf{k}) = \frac{1}{\hbar} \frac{\partial \epsilon_n}{\partial \mathbf{k}}$, f_0 is the Fermi-Dirac equilibrium distribution function, and $\epsilon_n(\mathbf{k})$ is the band energy (see Appendix A for the derivation of this formula).

Since the group velocity $\mathbf{v}(\mathbf{k})$ is odd under space inversion, the second-order term will vanish in crystals that have inversion symmetry. Moreover, it will also vanish in nonmagnetic crystals since $\mathbf{v}(\mathbf{k})$ is odd under time reversal. Furthermore, similarly to the anomalous Hall effect in coplanar magnetic systems, the second-order term will vanish in the absence of spin-orbit coupling, as the system will then be invariant under combined spin rotation and time-reversal symmetry [22]. ξ_{ijk} will thus be present in magnetic crystals with broken inversion symmetry as a consequence of the spin-orbit coupling. These are the same symmetry requirements as for the existence of SOT.

In Fig. 2 we plot the calculations of the longitudinal and transverse components of the second-order current obtained from the Boltzmann equation (2), normalized to the first-order current as a function of the magnetization angle for different directions of the electric field and for a current density of 10^{10} A m^{-2} . The relative amplitudes of the longitudinal component for different directions of the applied electric field are similar to the relative amplitudes of $\delta s_{\text{SO}}^{\parallel}$ (cf. Figs. 1 and 2). In both cases, the amplitudes are comparable for the electric field along [100] and [010] axes, while the largest (smallest) amplitude is obtained for fields along [110] ([$\bar{1}\bar{1}0$]) axes. From these results we can expect similar amplitude ratios also in the measured UMR and SOT. We point out, however, that this is not necessarily a consequence of a common proportionality of UMR and SOT to δs_{SO} . The Boltzmann approximation formula (2) gives an explicit example of a contribution to UMR with no direct relationship to δs_{SO} . The similar amplitude ratios in the two cases are merely a reflection of a common

Rashba-Dresselhaus-type symmetry of the underlying spin-orbit coupled electronic structure.

Our calculations in Fig. 2 also illustrate that the second-order current can have a sizable transverse component. Specifically in NiMnSb, the transverse component has a comparable amplitude to the longitudinal component for [100] and [010] crystal directions. Here we recall that in earlier experimental studies, the separation of UMR from competing thermoelectric contributions was based on the assumption that UMR had only a longitudinal component while the thermal effects contributed to both longitudinal and transverse signals [16,17]. Our results show that using the transverse signal for experimentally calibrating the magnitude of the thermal contribution is not, in general, reliable because the transverse component can also contain a contribution from UMR.

III. MEASURED DATA AND DISCUSSION

In our experiments, we pattern all our bars from the same 34-nm-thick film of ferromagnetic NiMnSb epitaxially grown on a 200-nm-thick $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ buffer layer on an Fe:InP insulating substrate and capped with a 5-nm MgO layer. The vertical lattice constant of 5.97 Å indicates that the film is under compressive strain and is close to a stoichiometric composition [23]. Figure 3(a) illustrates our measurement setup. The NiMnSb film is patterned into $4 \times 40 \mu\text{m}^2$ bars along different crystal directions and mounted on the rotational stage of an electromagnet. See Appendix D for further details about the experimental setup. A microwave current $I_0 \cos(\omega t)$, where $\omega = 2\pi 13 \text{ GHz}$, is passed in the bars and the polarizing action of the spin-orbit coupling induces an oscillating nonequilibrium spin population $\delta s_{\text{SO}}(\omega)$ which scales linearly with the current. The transverse component $\delta s_{\text{SO}}^{\perp}$ is

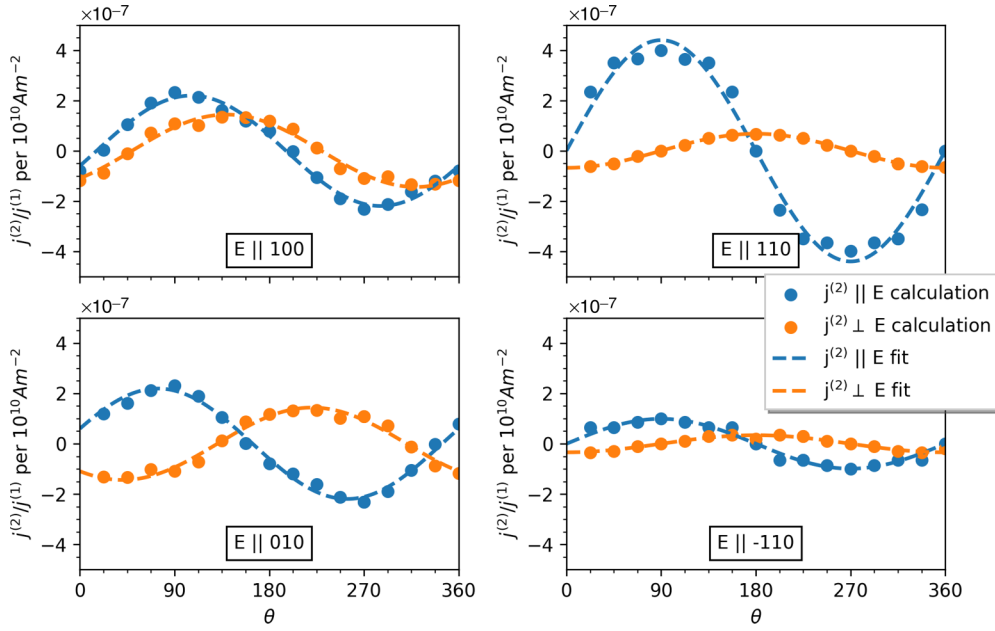


FIG. 2. Second-order current calculations for different directions of the electric field. The plots show the second-order current separated into parallel and perpendicular components to the electric field as a function of the magnetization orientation within the (001) plane. In each plot, θ denotes the angle of the magnetization measured from the electric field. The fits were done using the lowest-order expansion of the second-order conductivity tensor given in Eq. (B1). This tensor does not depend on \mathbf{E} and thus the fitting is done together for all directions of \mathbf{E} . The fitting is done for both the transverse and longitudinal components together. We plot the results as a ratio of the second-order current to the first-order longitudinal current. This ratio depends linearly on the electric field, and the values are given for an electric field that corresponds to a longitudinal current density of 10^{10} A m^{-2} .

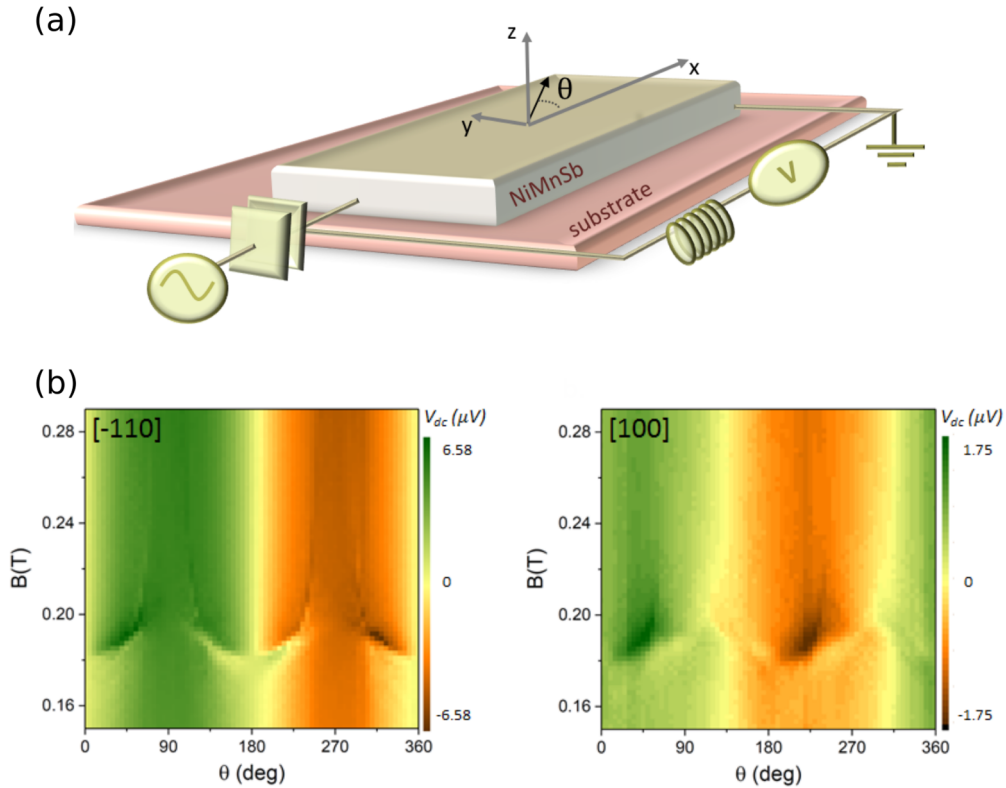


FIG. 3. Experimental setup and on- and off-resonance measurements of the mixing dc signal. (a) Design of the experimental layout. (b) Longitudinal dc voltage measured as a function of the external field \mathbf{B} and its direction θ with respect to the bar for a bar patterned along the $[\bar{1}10]$ and one patterned along the $[100]$ direction. A current density of $5.7 \times 10^{10} \text{ A m}^{-2}$ was used for the $[\bar{1}10]$ bar while a current density of $4.7 \times 10^{10} \text{ A m}^{-2}$ was used for the $[100]$ bar.

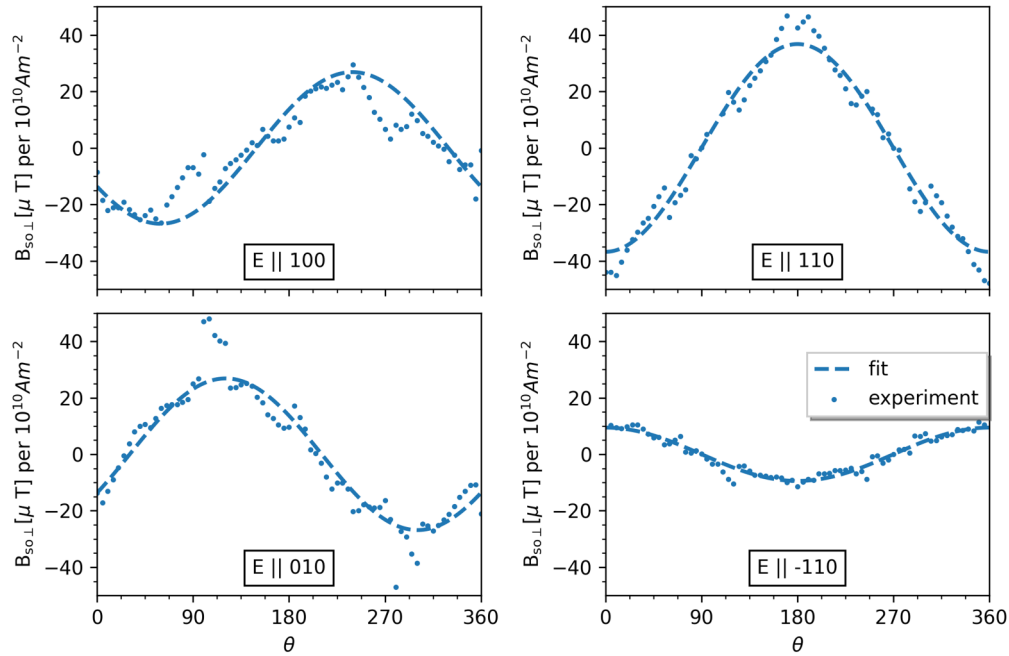


FIG. 4. Experimental SOT measurements for different bar orientations. The plots show the measured transverse components of the effective field \mathbf{B}_{so} , normalized to a unit current density of 10^{10} A m^{-2} , as a function of the magnetization orientation within the (001) plane. In each plot θ denotes the angle of the magnetization measured from the electric field, as illustrated in Fig. 3(a). Dashed lines are the harmonic fits.

responsible for generating torques on the magnetization via the effective field $\mathbf{h}_{\text{SO}}^{\perp} \approx -J_{\text{ex}} \delta \mathbf{s}_{\text{SO}}^{\perp} / m$. As described in the previous paragraph, the longitudinal component δS^{\parallel} is responsible for generating both longitudinal and transverse components of the unidirectional magnetoresistance. Here we focus on the longitudinal components only and measure the dc longitudinal voltage V_{dc} via a bias tee.

When ferromagnetic resonance is excited, rectification between the microwave current and the oscillating AMR results in a resonance in V_{dc} [5]. The resonance is clearly visible in the two-dimensional (2D) plots in Fig. 3(b). It shows V_{dc} as a function of the external magnetic field and its direction θ with respect to the current direction, for bars parallel to the $[\bar{1}10]$ and $[100]$ axes. From the analysis of its line shape (see Ref. [6] for details) we are able to quantify $\mathbf{h}_{\text{SO}}^{\perp}$. In agreement with previous studies on different systems [5,6,15], we experimentally identify the θ dependence of $\mathbf{h}_{\text{SO}}^{\perp}$ for the different crystal directions in which the microbars are patterned, as shown in Fig. 4. As in the theoretical calculations of $\delta \mathbf{s}_{\text{SO}}^{\perp}$, the amplitudes of measured $\mathbf{h}_{\text{SO}}^{\perp}$ for bars along the $[100]$ and $[010]$ axes are similar, while the largest (smallest) amplitudes are obtained for the $[110]$ $[\bar{1}\bar{1}0]$ directions, consistent with the combined Rashba-Dresselhaus-type symmetry of the NiMnSb electronic structure. The theoretical magnitude of $|\mathbf{h}_{\text{SO}}^{\perp}| \approx |J_{\text{ex}} \delta \mathbf{s}_{\text{SO}}^{\perp} / m| \sim 10 \mu\text{T}$ at 10^{10} A m^{-2} current density was reported earlier in Ref. [8] and is of the same order of magnitude as in the experiment.

In Fig. 3(b) we notice that the resonance is sitting on a sinusoidally varying background, which we refer to as V_{BG} . This is also shown in Fig. 5, where the θ dependence of the background voltage at a saturating magnetic field is plotted for bars patterned along the four different crystal directions $[100]$, $[010]$, $[110]$, and $[\bar{1}\bar{1}0]$. The striking feature is that the magnitude of V_{BG} is again strongly dependent on the bar

direction, however, the directions corresponding to the largest and smallest V_{BG} switched place compared to \mathbf{h}_{SO} (or $\delta \mathbf{s}_{\text{SO}}$). We note that these amplitude ratios of V_{BG} , as well as the crystal-direction-dependent phase shifts, are reproducible in different physical sets of samples patterned along the four crystal directions and do not depend on applied power, as shown in Appendix E.

To interpret the measured V_{BG} we now consider UMR and the thermoelectric contribution, namely, the anomalous Nernst effect (ANE). When exciting the system by the applied ac current, an out-of-plane temperature gradient due to Joule heating can result in an electrical signal detected in the sample plane due to ANE. Since the heat deposited by the current scales with the square of the current density, ANE is a second-order effect in the electric field, just like the second-order term of the conductivity. Based on a recent experimental measurement [24] of ANE in NiMnSb and our numerical simulation of the heat gradient, we estimate that the contribution to V_{BG} due to ANE is $\sim 0.01\text{--}0.1 \mu\text{V}$ per current density of 10^{10} A m^{-2} (see Appendix F). While the magnitude is similar to that of the measured signals in Fig. 5, we do not expect a strong dependence of the ANE contribution to V_{BG} on the crystal direction of the applied current. This is because ANE requires only the time-reversal symmetry breaking by the magnetization while broken spatial symmetries of the crystal only lead to additional, higher-order corrections. Since we find that V_{BG} strongly depends on the direction of the current and even changes sign for the $[110]$ direction the ANE itself cannot explain the V_{BG} .

UMR, on the other hand, is generated by the inversion-symmetry breaking which is of the combined Rashba-Dresselhaus-type form in our NiMnSb samples. As discussed in the theory section, this leads to a strong crystal-direction dependence of the UMR. Since theory suggests that the

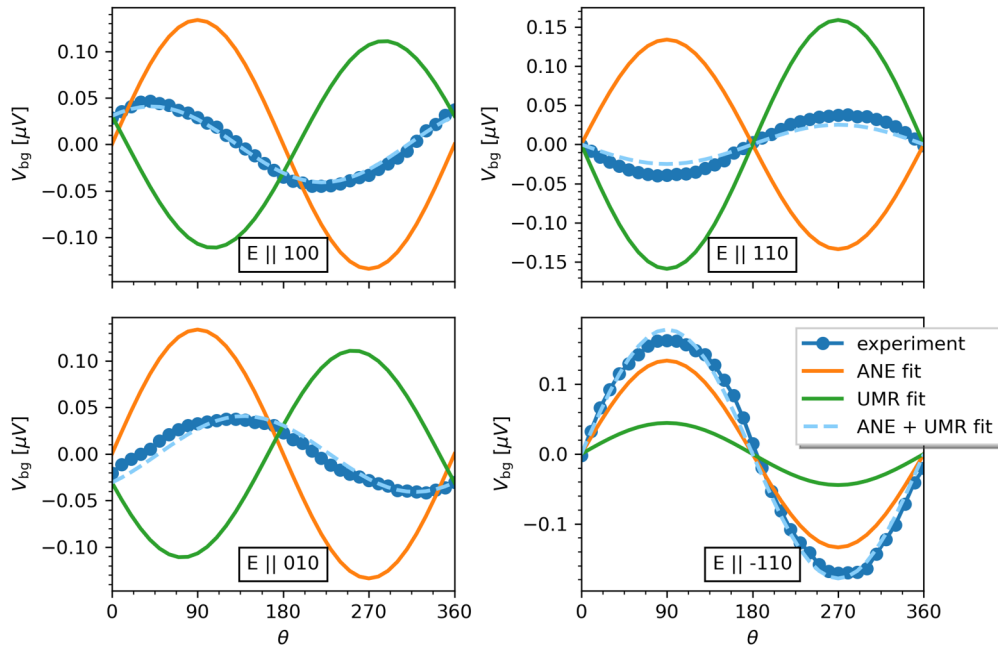


FIG. 5. Extraction of the UMR and ANE contributions from the measured background voltage. The plots show the measured background voltage for 10^{10} A m $^{-2}$ current density as a function of the magnetization orientation within the (001) plane. The UMR and ANE fits are done assuming that the ANE is isotropic and UMR is described by the lowest-order second-order conductivity tensor given in Eq. (B1) with the additional assumption that the relative amplitudes of the UMR for different bar directions are the same as the relative magnitudes of the SOT. This leaves three fitting parameters, which can be understood as the overall UMR magnitude, UMR phase shift for the [100] and [010] directions, and the ANE magnitude.

amplitude ratios for the different crystal directions of SOT and UMR are similar, we can use this as a constraint when fitting the measured V_{BG} data. The results of the fitting shown in Fig. 5 were obtained by assuming fixed amplitude ratios of the SOT fields \mathbf{h}_{SO}^{\perp} , plus an ANE contribution with an amplitude which is independent of the crystal direction. The extracted experimental ANE component is ~ 0.13 μV per current density of 10^{10} A m $^{-2}$, which is of the same order of magnitude as the above estimate. The fitted UMR contribution is ~ -0.16 μV per current density of 10^{10} A m $^{-2}$. This is an order of magnitude larger than our theoretical value which we attribute to the crude semiclassical Boltzmann approximation used in the UMR calculations. In the future, more elaborate Kubo formula calculations seem necessary to capture UMR in NiMnSb on the quantitative level. They will also allow for verifying the correspondence between the SOT and UMR amplitude ratios, and by this for more firmly establishing the fitting method we used to separate the UMR and thermoelectric contributions in the measured data.

IV. SUMMARY

Based on our study of ferromagnetic NiMnSb with non-centrosymmetric bulk crystal structure we make the following observations regarding the explored nonequilibrium spin-orbit coupling effects: (i) A harmonic dependence on the magnetization angle of the component of the current-induced spin polarization transverse to the magnetization does not imply, in general, that the in-plane component is its 90° phase shifted replica with the same amplitude. Despite the harmonic

dependence of the transverse component, the total spin-polarization vector, and the corresponding total current-induced spin-orbit field vector, are not necessarily independent of the magnetization angle. As a result, a measurement of SOT, driven by the transverse component of the current-induced spin-orbit field, should not be used, in general, for extracting the total nonequilibrium spin-orbit field (spin-polarization) vector. (ii) The approximate Boltzmann theory of UMR, together with the approximate assumption of SOT being proportional to the current-induced spin polarization, suggest that the amplitude ratios of UMR and SOT for electric fields applied along different crystal directions are similar. This can be used for separating experimental UMR and thermoelectric (e.g., ANE) contributions, by employing independently measured SOT. On the other hand, measurements of the diagonal and off-diagonal components in the electric field current indices is not, in general, a reliable tool for separating UMR and thermoelectric contributions because both can have sizable diagonal and off-diagonal components. (iii) Finally, the Boltzmann theory also illustrates that UMR can have microscopic contributions which are not directly related to the current-induced spin-polarization vector. Similar phenomenologies observed in UMR and SOT can be a mere reflection of the common underlying relativistic electronic structure with broken time and space-inversion symmetries.

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APPENDIX A: SECOND-ORDER BOLTZMANN FORMULA DERIVATION

Here we derive the second-order Boltzmann formula (2). The general form of the Boltzmann formula for a distribution function $g(t, \mathbf{r}, \mathbf{k})$ under the assumptions of a stationary and spatially homogeneous g and no magnetic field [25] can be expressed as

$$-\frac{e}{\hbar} \mathbf{E} \cdot \nabla_{\mathbf{k}} g = \left(\frac{dg}{dt} \right)_{\text{col}}, \quad (\text{A1})$$

where e is the (positive) elementary charge, \mathbf{E} is the electric field, and $\left(\frac{dg}{dt} \right)_{\text{col}}$ is the change of the distribution function due to scattering.

We will assume the constant relaxation-time approximation

$$\left(\frac{dg}{dt} \right)_{\text{col}} = -\frac{g - g_0}{\tau}, \quad (\text{A2})$$

where τ is the relaxation time and g_0 is the equilibrium distribution function, which for electrons is the Fermi-Dirac distribution function

$$g_0(\mathbf{r}, \mathbf{k}) = f_{\text{FD}}(\epsilon(\mathbf{k})) = \frac{1}{e^{\frac{\epsilon(\mathbf{k}) - \mu}{k_B T}} + 1}. \quad (\text{A3})$$

Within the constant relaxation-time approximation the Boltzmann formula has the following form:

$$-\frac{e}{\hbar} \mathbf{E} \cdot \nabla_{\mathbf{k}} g = -\frac{g - f_{\text{FD}}}{\tau}. \quad (\text{A4})$$

To find a solution for g up to second order in E we expand g in powers of E :

$$g = g_0 + g_1^i E_i + g_2^{ij} E_i E_j, \quad (\text{A5})$$

and insert it into the Boltzmann formula (A4). Keeping only the terms up to E^2 we find

$$-\frac{e}{\hbar} E_i \left(\frac{\partial g_0}{\partial k_i} + \frac{\partial}{\partial k_i} (g_1^j E_j) \right) = -\frac{g_1^i E_i + g_2^{ij} E_i E_j}{\tau}. \quad (\text{A6})$$

Since this equation must hold for all E , the coefficients for the E and E^2 terms on both sides of the equation must be the same. Therefore,

$$g_1^i = \frac{e\tau}{\hbar} \frac{\partial g_0}{\partial k_i}, \quad (\text{A7})$$

$$g_2^{ij} = \frac{e\tau}{\hbar} \frac{\partial g_1^j}{\partial k_i} = \frac{e^2 \tau^2}{\hbar^2} \frac{\partial^2 g_0}{\partial k_i \partial k_j}. \quad (\text{A8})$$

Considering that the dependence of g_0 on \mathbf{k} is only through ϵ we find

$$g_1^i = \frac{e\tau}{\hbar} \frac{\partial g_0}{\partial \epsilon} \frac{\partial \epsilon}{\partial k_i}, \quad (\text{A9})$$

$$g_2^{ij} = \frac{e^2 \tau^2}{\hbar^2} \left(\frac{\partial^2 g_0}{\partial \epsilon^2} \frac{\partial \epsilon}{\partial k_i} \frac{\partial \epsilon}{\partial k_j} + \frac{\partial g_0}{\partial \epsilon} \frac{\partial^2 \epsilon}{\partial k_i \partial k_j} \right). \quad (\text{A10})$$

Taking into account the relation

$$\mathbf{v}(\mathbf{k}) = \frac{1}{\hbar} \frac{\partial \epsilon}{\partial \mathbf{k}} \quad (\text{A11})$$

we have

$$g_1^i = e\tau v^i \frac{\partial g_0}{\partial \epsilon}, \quad (\text{A12})$$

$$g_2^{ij} = e^2 \tau^2 \left(\frac{\partial^2 g_0}{\partial \epsilon^2} v^i v^j + \frac{\partial g_0}{\partial \epsilon} \frac{1}{\hbar} \frac{\partial v^j}{\partial k_i} \right). \quad (\text{A13})$$

Electrical current is then given by

$$\mathbf{J} = -e \int \frac{d\mathbf{k}}{(2\pi)^3} \mathbf{v}(\mathbf{k}) g. \quad (\text{A14})$$

We note that this integral is done over the first Brillouin zone or any other unit cell in the reciprocal space. The first-order contribution to the current is given by

$$\mathbf{J}_1 = -e^2 \tau E_i \int \frac{d\mathbf{k}}{(2\pi)^3} \mathbf{v} v^i \frac{\partial g_0}{\partial \epsilon}, \quad (\text{A15})$$

and the second-order contribution

$$\mathbf{J}_2 = -e^3 \tau^2 E_i E_j \int \frac{d\mathbf{k}}{(2\pi)^3} \mathbf{v} \left(v^i v^j \frac{\partial^2 g_0}{\partial \epsilon^2} + \frac{1}{\hbar} \frac{\partial v^j}{\partial k_i} \frac{\partial g_0}{\partial \epsilon} \right). \quad (\text{A16})$$

Note that in a multiband system, these expressions give a contribution from each individual band and the total current will be a sum over all bands.

The expression for the second-order current can be further simplified. We first define a second-order conductivity tensor ξ_{ijl} :

$$J_2^i = \xi_{ijl} E_j E_l. \quad (\text{A17})$$

From Eq. (A18) we have

$$\xi_{ijl} = \xi_{ijl}^a + \xi_{ijl}^b, \quad (\text{A18})$$

where

$$\xi_{ijl}^a = -e^3 \tau^2 \int \frac{d\mathbf{k}}{(2\pi)^3} v^i v^j v^l \frac{\partial^2 g_0}{\partial \epsilon^2}, \quad (\text{A19})$$

$$\xi_{ijl}^b = -e^3 \tau^2 \int \frac{d\mathbf{k}}{(2\pi)^3} v^i \frac{1}{\hbar} \frac{\partial v^l}{\partial k_j} \frac{\partial g_0}{\partial \epsilon}. \quad (\text{A20})$$

Alternatively, using Eqs. (A7) and (A8), ξ can be written in the form

$$\xi_{ijl} = -\frac{e^3 \tau^2}{\hbar} \int \frac{d\mathbf{k}}{(2\pi)^3} v^i \frac{\partial}{\partial k_j} \left(v^l \frac{\partial g_0}{\partial \epsilon} \right). \quad (\text{A21})$$

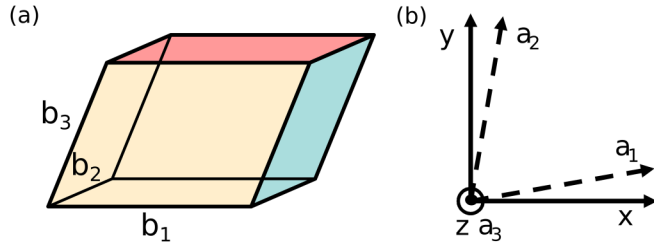


FIG. 6. (a) Unit cell of the reciprocal space defined by the reciprocal lattice vectors $\mathbf{b}_1, \mathbf{b}_2, \mathbf{b}_3$. (b) Coordinate system used for the symmetry analysis. The vectors $\mathbf{x}, \mathbf{y}, \mathbf{z}$ define the Cartesian coordinate system used for the symmetry analysis. $\mathbf{a}_1, \mathbf{a}_2, \mathbf{a}_3$ are the lattice vectors of the NiMnSb in presence of shear strain. Without the strain, the lattice vectors would correspond to the conventional lattice of the cubic NiMnSb lattice and would be oriented along the Cartesian coordinate system.

Using integration by parts

$$\xi_{ijl} = -\frac{e^3 \tau^2}{\hbar} \int_{\Gamma} \frac{d\mathbf{k}}{(2\pi)^3} v^i v^l v^j \frac{\partial g_0}{\partial \epsilon} + \frac{e^3 \tau^2}{\hbar} \int \frac{d\mathbf{k}}{(2\pi)^3} \frac{\partial v^i}{\partial k_j} v^l \frac{\partial g_0}{\partial \epsilon}, \quad (\text{A22})$$

here Γ signifies integral over the unit-cell boundary and v is the outward unit normal vector to the boundary. The first term in this relation in fact vanishes. To see that this is the case, it is useful to use for the integration a unit cell of the reciprocal space spanned by the reciprocal lattice vectors $\mathbf{b}_1, \mathbf{b}_2, \mathbf{b}_3$ (see Fig. 6¹), instead of the first Brillouin zone. The first term in (A22) is then given by sum over six surfaces. Since g_0 is a periodic function of \mathbf{k} , also $\frac{\partial g_0}{\partial \epsilon}$ must be periodic. This means that at the opposite boundaries of the reciprocal unit cell $\frac{\partial g_0}{\partial \epsilon}$ is the same. However, since the outward unit normal vector v is opposite for the opposite boundaries, the whole term vanishes.

Combining Eqs. (A21) and (A22) we have

$$\xi_{ijl} = \xi_{ijl}^a + \xi_{ijl}^b = -\xi_{lji}^b. \quad (\text{A23})$$

To simplify this further we need to show that ξ_{ijl} is symmetric under interchanging any two indices. This is clearly satisfied for ξ_{ijl}^a , however, it is less obvious for ξ_{ijl}^b . From Eq. (A17), we see that $\xi_{ijl} = \xi_{ilj}$ must hold and thus also $\xi_{ijl}^b = \xi_{ilj}^{2,b}$

¹Image adapted from <https://commons.wikimedia.org/w/index.php?curid=29922624> under CC BY-SA 3.0..

TABLE I. Symmetry of second-order conductivity tensor in NiMnSb for different directions of the magnetization. Note that the ξ_{ijk} coefficients between different directions of \mathbf{M} are not in general related.

	ξ_{xjl}	ξ_{yjl}	ξ_{zjl}
$\mathbf{M} \perp [001]$	$\begin{pmatrix} \xi_{xxx} & \xi_{yxx} & 0 \\ \xi_{yxx} & \xi_{yyx} & 0 \\ 0 & 0 & \xi_{zxx} \end{pmatrix}$	$\begin{pmatrix} \xi_{yxx} & \xi_{yyx} & 0 \\ \xi_{yyx} & \xi_{yyy} & 0 \\ 0 & 0 & \xi_{zzy} \end{pmatrix}$	$\begin{pmatrix} 0 & 0 & \xi_{zxx} \\ 0 & 0 & \xi_{zzy} \\ \xi_{zxx} & \xi_{zzy} & 0 \end{pmatrix}$
$\mathbf{M} \parallel [110] \text{ or } [1-10]$	$\begin{pmatrix} \xi_{xxx} & \xi_{yxx} & 0 \\ \xi_{yxx} & -\xi_{yxx} & 0 \\ 0 & 0 & \xi_{zxx} \end{pmatrix}$	$\begin{pmatrix} \xi_{yxx} & -\xi_{yxx} & 0 \\ -\xi_{yxx} & -\xi_{xxx} & 0 \\ 0 & 0 & -\xi_{zxx} \end{pmatrix}$	$\begin{pmatrix} 0 & 0 & \xi_{zxx} \\ 0 & 0 & -\xi_{zxx} \\ \xi_{zxx} & -\xi_{zxx} & 0 \end{pmatrix}$

should be satisfied. This can be explicitly verified from $\frac{1}{\hbar} \frac{\partial v^l}{\partial k_j} = \frac{\partial^2 \epsilon}{\partial k_i \partial k_j}$, which is symmetric as long as ϵ is sufficiently smooth function. To show that the tensors are also symmetric under interchanging the other indices, we consider

$$\xi_{jil} - \xi_{ijl} = -\xi_{lji}^b + \xi_{lji}^b = 0. \quad (\text{A24})$$

Then it must also hold that the ξ_{ijl} and ξ_{ijl}^b tensors are symmetric under interchanging indices i and l :

$$\xi_{ijl} = \xi_{jil} = \xi_{jli} = \xi_{lji}. \quad (\text{A25})$$

We can thus rewrite Eq. (A23) as

$$\xi_{ijl} = \xi_{ijl}^a + \xi_{ijl}^b = -\xi_{ijl}^b. \quad (\text{A26})$$

Therefore, $\xi_{ijl}^b = -\xi_{ijl}^b/2$ and we finally find

$$\xi_{ijl} = \frac{\xi_{ijl}^a}{2} = -\frac{e^3 \tau^2}{2} \int \frac{d\mathbf{k}}{(2\pi)^3} v^i v^j v^l \frac{\partial^2 g_0}{\partial \epsilon^2}. \quad (\text{A27})$$

APPENDIX B: SYMMETRY OF SECOND-ORDER CURRENTS

Here we study the symmetry of the second-order currents. Similarly to other response phenomena, the second-order currents will in general contain both time-reversal even (\mathcal{T} -even) and time-reversal odd (\mathcal{T} -odd) components. Here we consider only the time-reversal odd component since this component corresponds to the UMR. In the following ξ_{ijk} will denote the \mathcal{T} -odd second-order conductivity tensor. Furthermore, we assume the ξ_{ijk} tensor is symmetric under interchanging any two indices. As shown in Appendix A, this holds for the Boltzmann formula that we use in our calculations. It is not clear whether this holds for the ξ_{ijk} in general, thus, the symmetry analysis here should be taken to refer specifically to the Boltzmann contribution. The method for the symmetry analysis is analogous to the one used in Ref. [26]. We have implemented the second-order symmetry analysis in the open source code SYMMETR [27]. All the results shown here are given in a Cartesian coordinate system described in Fig. 6(b). Since in the experiment the magnetization always lies in the [001] plane, we consider here only magnetization in this plane. In Table I we give the general shape of the ξ_{ijk} for general direction of magnetization within this plane as well as for the [110] and $[-110]$ directions where the symmetry is higher.

To describe the dependence of the second-order currents on magnetization, it is useful to expand the ξ_{ijk} tensor in

powers of the magnetization. We consider only the lowest-order term since it describes well both the calculations and the experiment:

$$\begin{aligned}\xi_{xjl} &= \begin{pmatrix} M_x x_1 - M_y x_2 & M_x x_3 - M_y x_4 & M_z x_5 \\ M_x x_3 - M_y x_4 & M_x x_4 - M_y x_3 & 0 \\ M_z x_5 & 0 & M_x x_6 - M_y x_7 \end{pmatrix}, \\ \xi_{yjl} &= \begin{pmatrix} M_x x_3 - M_y x_4 & M_x x_4 - M_y x_3 & 0 \\ M_x x_4 - M_y x_3 & M_x x_2 - M_y x_1 & -M_z x_5 \\ 0 & -M_z x_5 & M_x x_7 - M_y x_6 \end{pmatrix}, \\ \xi_{zjl} &= \begin{pmatrix} M_z x_5 & 0 & M_x x_6 - M_y x_7 \\ 0 & -M_z x_5 & M_x x_7 - M_y x_6 \\ M_x x_6 - M_y x_7 & M_x x_7 - M_y x_6 & 0 \end{pmatrix}.\end{aligned}\quad (\text{B1})$$

Here x_i denotes free parameters of the expansion.

APPENDIX C: CALCULATION DESCRIPTION

The calculations utilize the full-potential local-orbital (FPLO) density-functional theory (DFT) code [28,29] for description of the electronic structure. This DFT uses a local orbitals basis set for solving the Kohn-Sham equations. This makes it easy to transform the DFT Kohn-Sham Hamiltonian into a Wannier form, which is needed for the transport calculations. We use the full set of basis orbitals for this transformation, which makes the Wannier Hamiltonian very accurate. This is crucial for the second-order calculations since the second-order contributions are very small and very sensitive to small symmetry violations that often exist in Wannier Hamiltonians generated by the more conventional approach based on maximally localized Wannier functions. The transport calculations utilize Wannier interpolation to evaluate the response formula on a tight grid in the reciprocal space. We have implemented the second-order Boltzmann calculation in the freely accessible LINRES code [30]. We have also utilized this code for the calculations of the current-induced spin polarization.

The spin-polarization calculations use the following Kubo formula for the response tensor (i.e., tensor such that $\delta s_{\text{SO},i} = \chi_{ij} E_j$) [31]:

$$\chi_{ij} = -\frac{e\hbar}{V\pi} \text{Re} \sum_{\mathbf{k}, m, n} \frac{\langle u_n(\mathbf{k}) | \hat{S}_i | u_m(\mathbf{k}) \rangle \langle u_m(\mathbf{k}) | \hat{v}_j | u_n(\mathbf{k}) \rangle \Gamma^2}{\{[E_F - E_n(\mathbf{k})]^2 + \Gamma^2\} [E_F - E_m(\mathbf{k})]^2 + \Gamma^2}}.\quad (\text{C1})$$

Here, \hat{S} is the spin operator, $u_n(\mathbf{k})$ are the Bloch functions of a band n , \mathbf{k} is the Bloch wave vector, $\varepsilon_n(\mathbf{k})$ is the band energy, E_F is the Fermi energy, \hat{v} is the velocity operator, and Γ is a quasiparticle broadening parameter that describes the disorder strength. This formula becomes equivalent to the first-order constant relaxation time Boltzmann formula for small Γ (with $\tau = \hbar/2\Gamma$), but differs for finite values of Γ . For the Γ value that we consider the formula is close to the Boltzmann formula. We only consider the Boltzmann formula for the second-order calculations since the derivation and evaluation of the second-order Kubo formula is much more complex. We note that the Kubo formula (C1) describes only the \mathcal{T} -even part of the Kubo formula. We do not consider here

the \mathcal{T} -odd component since experimentally it is seen that the in-plane SOT has a fieldlike character and the corresponding current-induced spin polarization is thus \mathcal{T} even. Our test calculations of the \mathcal{T} -odd component also suggest that it is much smaller than the \mathcal{T} -even component for realistic values of Γ .

The DFT calculations utilized $12 \times 12 \times 12$ k points and the GGA-PBE potential. The current-induced spin-polarization and the second-order conductivity response calculations use a $400 \times 400 \times 400$ k mesh, which we have confirmed to be sufficient for good convergence. To estimate the value of Γ we calculate the first-order conductivity using a conductivity formula analogous to Eq. (C1) and choose the Γ so that the conductivity matches the experimental conductivity. This corresponds to $\Gamma \approx 0.05$ eV or alternatively to $\tau \approx 6.6$ fs. In previous calculations of SOT in NiMnSb, a $\Gamma = 0.036$ eV was used [8] because the samples used in those experiments had somewhat larger conductivity. We note that our calculations of the current-induced spin polarization were done for the $\Gamma = 0.036$ eV value and have been afterwards rescaled to $\Gamma = 0.05$ eV, assuming $1/\Gamma$ scaling. This is quite accurate since for these values of Γ the formula is very close to the Boltzmann formula and thus has $1/\Gamma$ scaling.

APPENDIX D: EXPERIMENTAL DETAILS

All devices measured in these experiments are 2-terminal $4 \times 40 \mu\text{m}^2$ resistors obtained from the same wafer, patterned by e -beam lithography followed by ion milling. The bars are wedge bonded to the contact pads of a printed circuit board, which is mounted on the rotational stage of an electromagnet. All the experiments are carried at room temperature in air. The table below summarizes the resistance and AMR ratios measured for the four bars along the four crystal directions considered in the main paper.

Direction	Average resistance R_{av} (Ω)	AMR ratio $\Delta R/R_{\text{av}}$ ($\times 10^{-3}$)
[100]	105.4 ± 0.1	0.20 ± 0.01
[110]	97.4 ± 0.1	-1.30 ± 0.02
[010]	98.0 ± 0.1	0.21 ± 0.01
[-110]	104.2 ± 0.1	-1.16 ± 0.01

We point out that these are 2-terminal measurements which do not exclude contact resistance, estimated as $10 \Omega/\text{contact}$ from the comparison of bars with different aspect ratios. While the values of the resistance vary within 8% from bar to bar, the AMR ratio strongly depends on the crystal direction in which the bar is patterned. This is due to the partial compensation of noncrystalline and crystalline AMR terms in the NiMnSb film (please refer to the Supplemental Material of Ref. [6]).

Amplitude-modulated microwave power at a fixed frequency of 13 GHz is applied to the bars while the longitudinal dc voltage V_{dc} is extracted with a bias-tee and measured via a lock-in. To estimate the power that actually reaches the NiMnSb bar we use it as a resistance thermometer to quantify the Joule heating induced by the incident microwave signal. This procedure is discussed in detailed in the Supplemental Material of Ref. [6]. The values of the microwave current

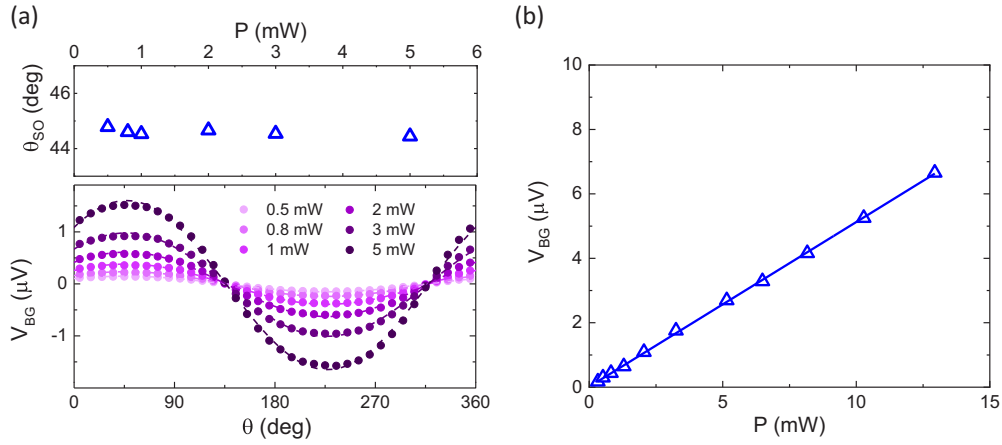


FIG. 7. (a) Top: phase shift θ_{SO} of V_{BG} , fitted by $V_{SO}^0 \sin(\theta + \theta_{SO})$, for a bar along [100] at different values of the microwave power. Bottom: angular dependence of V_{BG} for different microwave powers passed in the bar, showing no phase shift. (b) Power dependence of V_{BG}^0 for the same bar.

densities passed in each bar that we extract from this analysis are summarized in the following table.

Direction	Microwave current density ($A m^{-2}$)
[100]	4.7×10^{10}
[110]	1.3×10^{10}
[010]	5.1×10^{10}
[-110]	5.7×10^{10}

APPENDIX E: POWER DEPENDENCE AND REPRODUCIBILITY

In Fig. 7 we show that, as expected, the background voltage V_{BG} scales linearly with power and that the angular dependence of V_{BG} is independent of the power. In Fig. 8 we show that the results are reproducible between different bars patterned on the same chip.

APPENDIX F: MODELING TEMPERATURE GRADIENT USING FINITE ELEMENT METHOD

The system is excited by an ac current passing mainly through the NiMnSb layer which results in Joule heating. The heat scales with the square of the current density and dissipates into surrounding material giving rise to tempera-

ture gradients. The out-of-plane temperature gradient drives ANE which contributes to the electrical signal detected in the sample plane. We perform a simulation of heat transfer in the cross section of our device utilizing the finite element method (FEM) as implemented in COMSOL MULTIPHYSICS [32]. The software solves the heat equation numerically using an automatically generated triangular mesh with density adjusted to the size of individual domains of the device. The geometry is shown in Fig. 9 and consists of the NiMnSb wire (thickness = 37 nm, width = 1 μm) deposited on a (In,Ga)As mesa (thickness = 200 nm, width = 1 μm). There is also an InP substrate (thickness = 1 μm , width = 2 μm), a thin MgO capping layer (thickness = 5 nm, width = 1 μm), and a He atmosphere included in the simulation. We note that the experiments are done in air rather than in He, however, the choice of the atmosphere does not play an important role for the simulations. We find that replacing the He by air has a negligible effect on the thermal gradient. The simulations also consider much smaller thickness of the InP substrate since the full width of the experimental substrate would be difficult to simulate. This does not have any significant effect on the thermal gradient since the thickness we consider is sufficient to capture the substrate's cooling effect on the NiMnSb layer.

The reference temperature T_{ref} is set to 300 K (before the Joule heating takes place). The current density applied

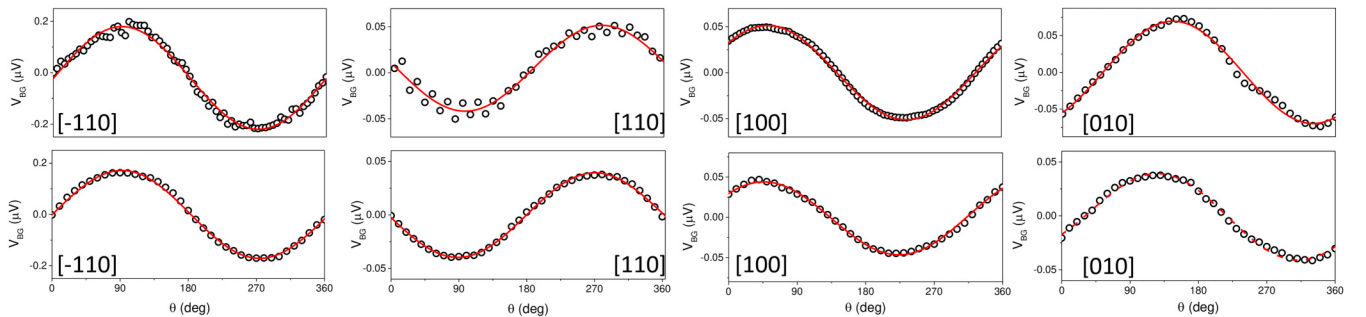


FIG. 8. Angular dependence of V_{BG} , normalized to a current density of $10^{10} A m^{-2}$, measured for two different bars patterned on the same chip along each of the four crystal directions. Top: measurements for the first set of bars. Bottom: measurement for the second set of bars.

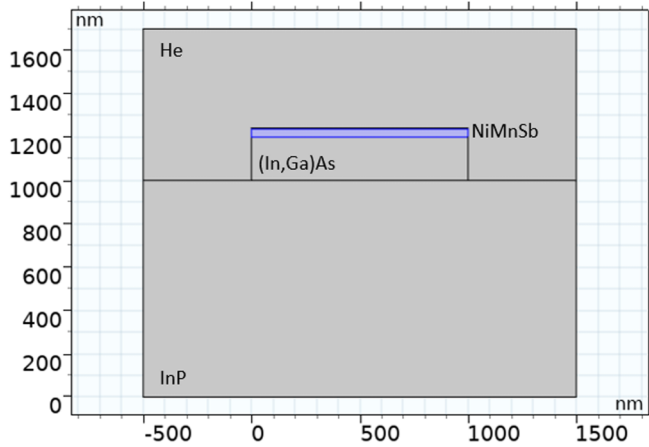


FIG. 9. Simulated geometry, cross section of the device, NiMnSb conducting the ac current is highlighted in blue, thin MgO capping layer (poorly visible in this plot) is included in the simulation.

to NiMnSb is 10^{10} or 10^{11} A m^{-2} . At the boundary of the simulated area the temperature is fixed to T_{ref} or a thermal insulation is assumed (except the bottom boundary again fixed to T_{ref}). These two types of boundary condition correspond to very efficient cooling (transfer of heat to the surroundings) or to extremely poor cooling, respectively. The real system would fall between these two limiting cases. Figures 10 and 11 show the simulated steady-state temperature distribution for the case with boundaries fixed to T_{ref} and with insulating boundaries, respectively.

The former case (Fig. 10) is simulated with applied current density of 10^{10} and 10^{11} A m^{-2} but we show the temperature profile only for 10^{10} A m^{-2} . The 10 times larger current density results visually in the same temperature profile but the maximum temperature increase $T - T_{\text{ref}}$ is 100 times larger.

The latter case (Fig. 11) is simulated only with applied current density of 10^{10} A m^{-2} and all the heat is dissipated only via the bottom boundary, through the substrate. The out-of-plane temperature gradient is evaluated along a vertical cut line (along the z coordinate) running through the middle of the mesa. Figure 12 shows the temperature increase $T - T_{\text{ref}}$ along

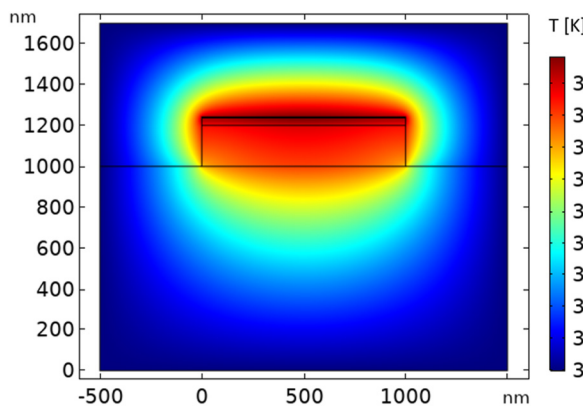


FIG. 10. Temperature distribution in case the applied current density is 10^{10} A m^{-2} and all boundaries are set to $T_{\text{ref}} = 300$ K, the most efficient cooling.

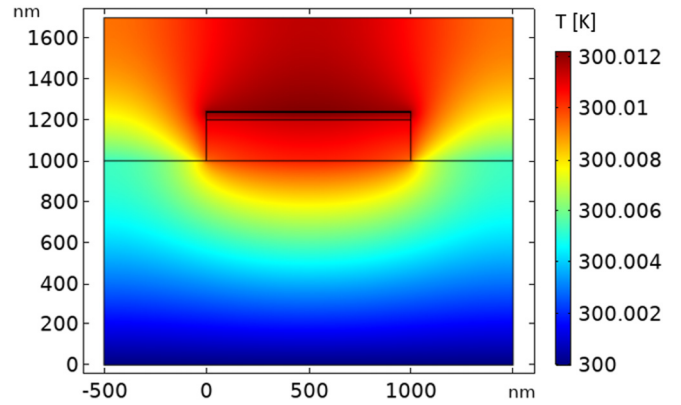


FIG. 11. Temperature distribution in case the applied current density is 10^{10} A m^{-2} and the top, left, and right boundaries of the simulated domain are insulating and the bottom boundary is set to $T_{\text{ref}} = 300$ K, the least efficient cooling.

the cut line within the NiMnSb layer (1200 to 1237 nm) for the three cases simulated.

As expected, the case with insulating boundaries shows a larger increase in temperature but the dependence on the z coordinate is the same. The case with 10 times larger applied current shows a 100 times larger increase of temperature which is due to the Joule heating scaling with the square of the applied current density.

Finally, Fig. 13 shows the out-of-plane temperature gradient generating ANE in the NiMnSb wire. It is evaluated simply as a numerical derivative of the temperature given in Fig. 12 for the three cases. Note that the gradient decreases linearly in the NiMnSb layer towards the top surface. The efficiency of the cooling (insulating boundaries or fixed temperature) does not affect the gradient so the approximation of the cooling mechanism assumed in our model should not significantly compromise the validity of our numerical results. Our model does not include heat convection in helium explicitly. To test whether a heat convection could be important, we have approximated this contribution to cooling by a constant heat flux through the top surface $q = 250 \frac{\text{W}}{\text{m}^2\text{K}}$.

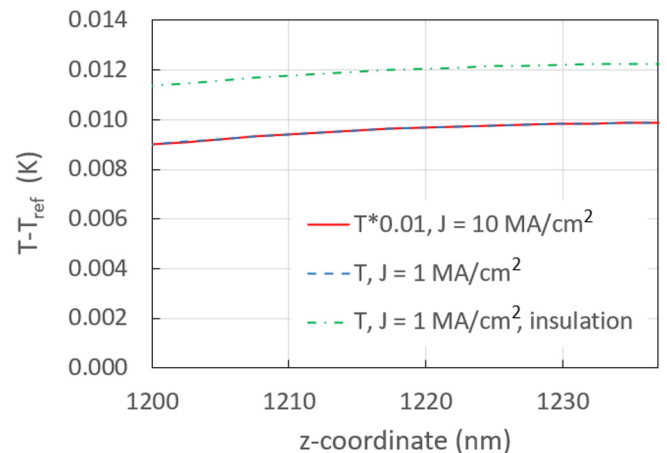


FIG. 12. Temperature increase $T - T_{\text{ref}}$ along vertical cut line within the NiMnSb layer.

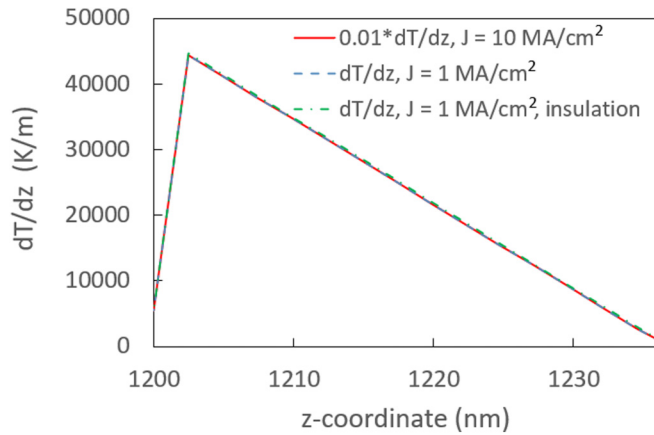


FIG. 13. Out-of-plane temperature gradient along vertical cut line within the NiMnSb layer.

This value corresponds to a forced air flow [33] so it overestimates the convection in our setup. The resulting temperature gradient shows only negligible difference to the case with fixed-temperature boundary condition described above. The main result of the FEM simulation relevant to the experimental device is that the average out-of-plane temperature gradient is of the order of 10^4 K m^{-1} for current density of 10^{10} A m^{-2} .

TABLE II. Material parameters used as input of FEM model: electrical conductivity σ_E , thermal conductivity σ_T , heat capacity c_p , and mass density ρ .

	σ_E (Sm^{-1})	σ_T ($\text{W m}^{-1} \text{K}^{-1}$)	c_p ($\text{J kg}^{-1} \text{K}^{-1}$)	ρ (kg m^{-3})
MgO	0	200 [34]	900 [35]	3600
NiMnSb	3.3×10^6	23 [36]	420 [37]	7600
InGaAs	1.43×10^4	200 [38]	300 [39]	5500
InP	0	68 [40]	310 [40]	4800
He	0	0.15 [41]	5200 [41]	145

Our FEM results depend on the material parameters used. We have measured the electrical conductivity of the individual layers at room temperature. The room-temperature thermal conductivity and heat-capacity parameters of our films are estimated based on literature as listed in Table II. In case of NiMnSb they are estimated based on related materials [36,37]. The thermal conductivity is underestimated, considering the metallic character of the film, so we report an upper estimate of the thermal gradient. The results are obtained for a steady state so there is no significant dependence on the heat capacity or mass density. (We estimate the mass density based on the molar masses and unit-cell volume.)

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