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# THERMAL, ELECTROCHEMICAL AND MECHANICAL PROPERTIES OF SHAPE MEMORY ALLOY DEVELOPED BY A CONVENTIONAL PROCESSING ROUTE

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# ABSTRACT

A Cu based shape memory alloy (Cu-Al-Ni) having a composition 83% Cu, 14% Al, 3% Ni, was developed and studied to determine the shape memory effect. Powder of Cu, Al and Ni was melted in a pit furnace at about 1550<sup>o</sup>C, and casted alloy was heat treated at 850<sup>o</sup>C for a period of 50 minutes followed by water quenching. Microstructure characterization of alloy (Cu-Al-Ni) was carried out to determine the pre-quenched (cast structure) and quenched martensitic structure. The microstructure analysis of developed samples showed needle like structure of quenched martensite after heat treatment. It has a very good resemblance with structure of casted shape memory alloy obtained from the vacuum induction process. The Vickers hardness test was also performed. Quenched microstructure with improved hardness than pre-quenched structure was observed.

Keywords: Shape Memory Alloy, Microstructure, Mechanical Properties.

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## **1. INTRODUCTION**

The term Shape Memory Alloys (SMA) are put in application to a specific class of metallic materials that manifest the ability to return to a formerly defined size or shape when put into a suitable thermal methodology. Usually, these type of materials may be plastically deshaped at a relatively small temperature and upon exposure to some specific elevated temperature will come back to their shape attained before the deformation [1]. A lot of research has been carried out on shape memory alloys recently. Among them, Wongweerayoot et al. [2] prepared a NiTi-Cu shape memory alloy bimorph actuator and studied the effect of annealing conditions on nitinol (NiTi) at various temperatures i.e., 500, 600, and 650°C for 30 min. The annealing temperatures of 600 and 650°C produced appropriate crystalline structure of NiTi. The actuator prepared at annealing temperature of 650°C for 30 min with two pre-stressing conditions of straight and curved mold. It showed that deflection of the actuator is more affected by annealing temperature. Todorovic et al. [3] used melt spinning technique to produce thin Cu-Al-Ni ribbons. The results showed that Cu-Al-Ni base alloys almost completely reduced metabolic activity of peripheral blood mononuclear cells (PBC) during MTT (3-(4, 5-Dimethylthiazol-2-Yl)-2, 5-Diphenyltetrazolium Bromide) test while none of Cu-Al-Ni ribbon types showed a statistically significant effect on the metabolic activity of cells. Alana et al. [4] prepared different solutions for evaluation of TiNi polished surfaces and noticed their electrochemical behavior: Ringer solution, Hanks' balanced salt (HBSS) solution, Hanks solution and in Saline body fluid solution. All simulated body fluids revealed almost the same corrosion phenomenon. It was also found that Ringer solution proved itself to be most corrosive followed by SBF and HBSS. The corrosion potential also changes in a similar fashion. Francois et al. [5] had prepared SMA wire of nitinol mesh into technical fabric for examining it weaving properties as compared to stainless steel wire. These fabrics were investigated to use inside composites structure. It was found that nitinol wire showed better properties of weaving as compared to stainless steel. Ming et al. [6] discussed the industrial applications of shape memory alloys like eye glass having frames for super-elasticity and super elastic wire of cellular phone antennas. He also discussed the uses of superelastic NiTi powder for the resistance of SnPdAg solder against failure due to thermal stresses. European has been recently using NiTiNb plug for sealing high-pressure fuel passages in diesel engine injectors made of SMA actuators. This research is aimed to develop shape

memory alloy (Cu-Al-Ni) produced by a conventional processing route and study its mechanical properties and electrochemical behavior.

### 2. EXPERIMENTAL WORK

High purity of about 99.99% Cu-Al-Ni powder was purchased from local market. In this research the wt. % ratio of Cu 83%, Al 14%, and Ni 3% was taken and mixed using a ball mill for one hour. The melting of Cu, Al and Ni alloy was done in Pit furnace. Metal powder of Cu, Al and Ni (150g calculated composition) was put in graphite crucible and placed in pit furnace. The furnace was operated at 1550°C for 1 hour. The molten alloy was poured into Graphite Mold to get a rectangular shape test specimen. The cast specimen of the alloy in the rectangular form was cut into difference samples with the help of electric hacksaw for hardness, SEM, DSC and electrochemical behavior studies. Phase transformation temperature was determined by DSC at a cooling rate of 20°C/min by using an inert atmosphere.

Micro-Hardness-Tester was used to determine the hardness of the cast alloy. The cast samples mounted and ground with the help of emery papers of different sizes (60, 120 and 180 up to 1000). The cast alloy samples were also polished and etched with etching solution of Ammonium hydroxide (NH<sub>3</sub>OH) 5 parts, Hydrogen per Oxide (H<sub>2</sub>O<sub>2</sub>) 2-3 parts, Water H<sub>2</sub>O 5 parts. Casted alloy was also heat treated (homogenized) at  $850^{\circ}$ C for a period of 50 minutes followed by water quenching. Lieca Light Optical Microscope and SEM were used for microstructure analysis of developed shape memory alloy.

#### **3. RESULTS AND DISCUSSION**

### 3.1. DSC Analysis

The DSC analysis of as cast and quenced samples of Cu-14% Al- 3% Ni shape memory alloy is shown in fig.1. The cooling rate has been set 20°C/min for all samples. All samples were tested in an inert atmosphere. The obtained curve is shown in Fig.1.



**Fig.1.** DSC scan of samples A (Cast Sample) & B (Quenched Sample) Transformation temperatures of cast and quenched samples are inserted in Table 1.

Alloys	A <sub>s</sub> /°C	A <sub>p</sub> /°C	A <sub>f</sub> /°C	$M_s/^{\circ}C$	M <sub>p</sub> /°C	$M_{\rm f}/^{\circ}C$
As Cast	225	210	198	190	175	112
Quenched	215	208	205	202	138	90

Table1. Transformation temperatures of cast and quenched samples

The values of the transformation temperatures of Cu- Al- Ni shape memory alloy lies b/w 90 and 225°C which is in a close resemblance with the literature values [9-12]. The slight variation in the transformation temperatures is due to difference in alloying and operating conditions. It is quite obvious from the values that the transformation temperatures show a variation in as cast and quenched structure. The trend of transformation temperatures in the structures is  $A_p>A_f>M_p>M_f$ . The temperature scheme validates the transformation phenomenon that

it is in a right order. The values of heat flow from both the alloys start increasing as Martensitic transformation starts and get normalized as it finished. It gives an idea that during Martensitic transformation both alloys have dejected more heat from them and formation of needles of Martensite took place.

## **3.2. Optical Microstructural Analysis**

The microstructures of as cast samples are shown in Fig 2(a, b) and quenched closely martensite are shown in Fig 3 (a, b). The micrographs are shown at different magnification clearly showed the precipitate formation in Fig 2(a, b) and parallel martensite needles are shown in Figure 3 (a, b) due to quenching of the samples.



Fig2. (a, b) Optical micrographs of cast samples of Cu-Al-Ni shape memory alloy.



Fig.3. (a, b) Needle like structure showing the formation of martensite in shape memory alloy.

Optical micrographs of cast and heat treated alloys are shown in Figs. 2 &3. In the Fig. 2(a, b), microstructures of cast shape memory alloy at two dissimilar magnifications are shown. In Fig. 2a, fine grain microstructure can be distinctly seen. While in Fig. 2 b, the structure becomes much clear as the magnification increases. Dark and light grains shown in Fig. 3 a and b reveal martensite lamellar structure. Sharp needles of martensite can be clearly seen in Fig 3(b) as against in Fig 3 (a). Both microstructures give a proof of presence of some unseen needles or the ones which do not have a proper time for formation of martensitic structure. These may be due to the effect of slow cooling in that specific area or simply speaking a nonuniform cooling throughout the structure.

## 3.3. Electrochemical Analysis

Potentiodynamic polarization and open circuit potential (OCP) have been measured in a conventional three electrode electrochemical cell. A 0.9 % NaCl solution was prepared for analysis. The sample size was 1 cm<sup>2</sup>. For OCP total scan time was 1000 seconds and sample period was 0.5.



Fig.4. Measurement of OCP in 0.9% NaCl Solution

The maximum OCP value measured at 1000 sec was -217.5 mV which is the most active potential. This potential is achieved at a value of 1000 sec. Note that the curve shows an increasing trend but not in a smooth fashion, this might be due to contamination in the solution.



Fig.5. Measurement of OCP of Cu-14% Al- 3% Ni Shape Memory Alloy in Dextrose Solution

The maximum OCP value was noticed at -34.125 mV at an initial stage of the scan and it decreases gradually with time as shown in fig.5. This test has been performed in a dextrose solution with a sample period 0.5. The sample dimensions are 1cm\*1 cm. The corrosion potential for dextrose solution is higher for shape memory alloy as compared to brine solution.



Fig.6. Potentiodynamic polarization curve in 0.9% NaCl solution

Fig. 6 shows a potentiodynamic polarization behavior of shape memory alloy in a brine solution. The lower part shows a cathodic polarization upto -250mV and then there is an activation region b/w 10  $\mu$ A and 10 mA. After it passivation starts due to formation of a passive film of CuCl<sub>2</sub>. The activation region shows the dissociation of Cu into Cu<sup>+2</sup> ions and after it there is a formation of CuCl<sub>2</sub> passive layer which further inhibits the corrosion of Cu. Brine solution provides Cl<sup>-1</sup> ions for the formation of CuCl<sub>2</sub>.



Fig.7. Potentiodynamic polarization curve in Dextrose Solution

Potentiodynamic polarization curve for shape memory alloy in Dextrose solution has been shown in Fig 7. The alloy reveals a less activation region in this solution as compared to brine solution. It means that there is a low number of  $Cl^{-1}$  ions formations as compared to brine solution. The chances of corrosion of alloy in dextrose solution are less as compared to brine solution.



Fig.8. Formation of greenish colour of CuCl<sub>2</sub> on the sample

The greenish color of  $CuCl_2$  in fig8. further confirms the formation of  $CuCl_2$  in the passive region which prevents the sample from further corrosion. The formation of  $CuCl_2$  is due to the presence of  $Cl^{-1}$  ions in the brine solution.

# 3.4. SEM and EDX Analysis



Fig.9. SEM image of as quenched sample of shape memory alloy.

Coarse martensite plates of shape memory alloy were observed when sample was heat treated at  $850^{\circ}$ C for period of 50 mints followed by water quenching. Note that martensite lamellae are not found everywhere which represents a non uniform quenching. However the presence of plates reveals a quenched structure as revealed in fig.9.





Fig.10. EDX analysis of as cast sample of shape memory alloy.

EDX analysis further confirms the purity of alloy with a slight variation in composition from the parent alloy as shown in fig.10. This variation may be due to segregation or due to some oxidation of Al, as Al lose its weight as revealed by the analysis.



Fig.11. Horizontal scan representing the compositional analysis

Since the base metal is Cu and it is in higher amount as compared to Al and Ni the horizontal SEM scan further verifies the results. The red colour line scan confirms the presence of higher amount of Cu while Al and Ni in lower amounts sequentially across the sample. The ups and downs in the scan show segregation.

Table 2.	Vickers	micro	hardness	test	readings	of al	loys
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Samples Detail	1	2	3	Average value
As Cast	336 Hv	347 Hv	335 Hv	339 Hv
Quenched	370 Hv	374 Hv	369 Hv	371 Hv

Three successive Vickers hardness readings were noted from cast and quenched alloys and an average value was calculated from them. Both alloys show a different value at each measurement as the readings are from the surface. It is quite obvious that the microhardness values increases with quenching. The variations in the hardness values and SEM horizontal scan give an idea about structure and composition dissimilarity throughout the structure. Aydog du presented the hardness value 281 Hv of Cu-Al-Ni alloy when heat treatment has been done at 930°C for ashomogenized sample and for quenched sample he put up a value of 321 Hv [7]. Gojic et al. [8] put up a value of 275 Hv for shape memory alloy Cu-13.16% Al-4.11%Ni. Shokuhfar and Rezvani made two different compositions of alloys and they put up 220 Hv as a hardness values of their alloys.

## 4. CONCLUSIONS

After the analysis of shape memory alloy produced by pit furnace techniques following results are generated:

1. DSC experiment showed that there is no significant difference in transformation temperatures when compared the results with the literature values.

2. Optical microscopy results confirmed the formation of martensitic lamellae with a fine and coarse morphology with some unfinished lamellae in between the structure.

3. OCP and potentiodynamic curves show the activation, passivation and cathodic polarization regions which mention the corrosion properties of shape memory alloy.

4. The chances of corrosion of alloy are less in dextrose solution as compared to brine solution.

5. SEM/EDX analysis confirms the composition of alloy with a slight variation and revealed a segregated structure.

6. Hardness values are higher for quenched sample as compared to as cast sample and values for both the samples are higher when compared them with the literature values.

#### **5. ACKNOWLEDGEMENTS**

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