ISSN 0794-5698



Available online at http://www.ajol.info/index.php/njbas/index Nigerian Journal of Basic and Applied Science (September, 2013), 21(3): 197-206

DOI: http://dx.doi.org/10.4314/njbas.v21i3.5

Reliability Analysis of a Two Dissimilar Unit Cold Standby System with Three Modes Using

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Kolmogorov Forward Equation Method

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ABSTRACT: Reliability is an important area that is receiving attention globally. This paper studies reliability analysis of a two-dissimilar-unit cold standby system with three modes using Kolmogorov forward equation's method, in which its reliability and availability analysis are evaluated. This proposed system has been investigated under three modes: normal, partial failure, total failure. The failure and the repair time are assumed to have exponential distribution. The effect of failure rate on meantime to system failure (MTSF), steady state availability ($A_T(\infty)$) and the profit function $PF(\infty)$ of the system are compared. It was found that MTSF, $A_T(\infty)$, and $PF(\infty)$ are decreasing with the increase of the failure rate.

Keywords: Cost analysis, Meantime to System Failure, Steady State Availability and Kolmogorov forward equation.

INTRODUCTION

Reliability is a vital for proper utilization and maintenance of any system. It involves technique for increasing system effectiveness through reducing frequency maintenance and minimization. Studies on two unit redundant system with repair can be obtained in Arora(1976), Emara and El-said (1992), Goel et al. (1986). Damcese and Temraz (2010), Goel and Gupta (1984) have studied the analysis of two unit parallel system. El-said (2008), El-said and El-sherbeny (2005), Gopalan and Nagawalia (1985), and Rander (1994) have the cost analysis with preventive maintenance of different system. El-said and Elsherbeny (2005) by using linear first order differential equation evaluated the reliability and availability characteristics of two different systems. Gupta and Mittal (2006) studied the stochastic behavior of a two unit warm standby system with two types of repairmen and patience time. Mokaddis et al. (2009) using linear first order differential equation evaluated the reliability and availability characteristics of two-dissimilar-unit cold standby system with three mode for which no cost benefit analysis was considered. El-said (1994) contributed on stochastic analysis of a two-dissimilar-unit standby redundant system. This research work deals with the reliability analysis of a two-dissimilarunit cold standby system with three modes using

Kolmogorov forward equation method. Initially one unit is operative and the other unit is kept as a cold standby, i.e. it does not fail while standing by. Each unit works with three modes; normal, partial failure and total failure. The system fails when both units fail totally. The failure and the repair rate are assumed to have exponential distribution. The effect of failure rate on meantime to system failure, steady state availability and profit function are determined based on the assumed numerical values given to the system parameters and reliability measures.

METHODOLOGY Assumption and Notations Assumptions

The following assumptions were adopted:

- The system works with one unit that is operative and the other is kept as a cold standby, i.e. it does not fail while standing by unless it goes into operation.
- ii. The standby is switched to operative state in negligible time.
- The operative units have three modes of iii. operation: these are normal, O-mode, which means the functioning of the units with full capacity, partial failure, p-mode which means the functioning of the units with reduced capacity at specified level and the

- total failure, T-mode which means the capacity goes below a specified level.
- iv. A unit, which is replaced or repaired in total failure mode. This assumed to go directly to the normal without passing through the partial failure mode.
- v. A unit in the normal mode must pass through the partial failure mode to get in to the total failure mode. In the partial failure mode, a unit is working as good as being repaired.
- vi. The system is down when all units are nonoperative.
- vii. For constructing the probabilistic structure of the system, it is assumed that the failure and repair times have exponential distributions.

- λ_1 ; the failure rate of the ith unit from O_i mode to P_i -mode, i=1,2.
- α_i ; the failure rate of the ith unit from P_i mode to T_i -mode, i=1,2.
- μ_i ; the repair rate of the ith unit from T_i -mode to O_i -mode, i=1,2.
- β_i ; the repair rate of the ith unit from P_i -mode to O_i -mode, i=1,2.
- O_i ; the ith unit is operative, i=1, 2
- S_i ; the ith unit is in a cold standby mode, I = 1, 2.
- P_i ; the ith unit is partial failure, i=1, 2.
- T_i ; the ith unit is in a total failure mode, i=1, 2.
- S_i ; denotes the state of the systems i=0 to 8.

Notations

Stochastic Behaviour of the System

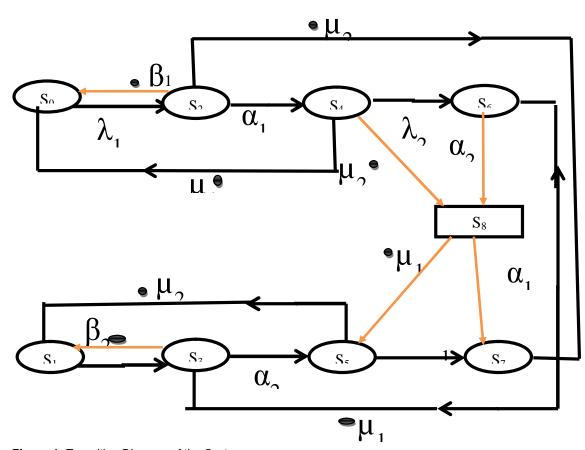


Figure 1: Transition Diagram of the System

Up State Down State Regeneration

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States of the System

state S_0 ; unit one is operative, unit two is in a cold standby. State S_1 ; unit two is operative, unit one is in a cold standby.

state S_2 ; one unit is in a partial failure, unit two is in a cold standby.

state S_3 ; unit one is in a cold standby, two unit is in a partial failure mode.

state S_4 ; unit one is in a total failure modes, unit two is operative. state S_5 ; unit one is operative, unit two is in a total failure mode. state S_6 ; unit one is operative, unit two is in a total failure mode.

state S_7 ; unit one is in a partial failure mode, unit two is in a total failure mode. state S_8 ; both units are in total failure mode. i.e. the system is down completely.

Mean Time to System Failure

By using the method of kolmogorov forward equations and the above mentioned set of assumptions, the mean time to system failure MTSF for the proposed system will be evaluated. From Figure 1, let $P_i(t)$ be the

probability that the system at time (t>=0) in state s_i . Let P(t) denote the probability row vector at time t, the initial conditions for this problem are

$$p(0) = [p_0(0), p_1(0), p_2(0), p_3(0), p_4(0), p_5(0), p_6(0), p_7(0), p_8(0)] = [1, 0, 0, 0, 0, 0, 0, 0, 0]$$
(1)

By employing the method of kolmogorov forward equations, El-Said and Elshebeny (2005), the following differential equations are obtained:

$$\frac{dp_0(t)}{dt} = -\lambda_1 p_0(t) + \beta_1 p_2(t) + \mu_1 p_4(t)$$

$$\frac{dp_1(t)}{dt} = -\lambda_2 p_1(t) + \beta_2 p_3(t) + \mu_2 p_5(t)$$

$$\frac{dp_2(t)}{dt} = -(\alpha_1 + \beta_1) p_2(t) + \mu_2 p_7(t) + \lambda_1 p_0(t)$$

$$\frac{dp_3(t)}{dt} = -(\alpha_2 + \beta_2) p_3(t) + \mu_1 p_6(t) + \lambda_2 p_1(t)$$

$$\frac{dp_4(t)}{dt} = -(\lambda_2 + \mu_1) p_4(t) + \alpha_1 p_2(t) + \mu_2 p_8(t)$$

$$\frac{dp_5(t)}{dt} = -(\lambda_1 + \mu_2) p_5(t) + \alpha_2 p_3(t) + \mu_1 p_8(t)$$

$$\frac{dp_6(t)}{dt} = -(\alpha_2 + \mu_1) p_6(t) + \lambda_2 p_4(t)$$

$$\frac{dp_7(t)}{dt} = -(\alpha_1 + \mu_2) p_7(t) + \lambda_1 p_5(t)$$

$$\frac{dp_8(t)}{dt} = -(\mu_1 + \mu_2) p_8(t) + \alpha_2 p_6(t) + \alpha_1 p_7(t)$$

(2)

This can be written in the matrix form as

$$\frac{dp(t)}{dt} = Q * p \tag{3}$$

Where,
$$Q = \begin{pmatrix} -\lambda_1 & 0 & \beta_1 & 0 & \mu_1 & 0 & 0 & 0 & 0 \\ 0 & -\lambda_2 & 0 & \beta_2 & 0 & \mu_2 & 0 & 0 & 0 \\ \lambda_1 & 0 & -(\alpha_1 + \beta_1) & 0 & 0 & 0 & 0 & \mu_2 & 0 \\ 0 & \lambda_2 & 0 & -(\alpha_2 + \beta_2) & 0 & 0 & \mu_1 & 0 & 0 \\ 0 & 0 & \alpha_1 & 0 & -(\lambda_2 + \mu_1) & 0 & 0 & 0 & \mu_2 \\ 0 & 0 & 0 & \alpha_2 & 0 & -(\lambda_1 + \mu_2) & 0 & 0 & \mu_1 \\ 0 & 0 & 0 & 0 & \lambda_2 & 0 & -(\alpha_2 + \mu_1) & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & \lambda_1 & 0 & -(\alpha_1 + \mu_2) & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \alpha_2 & \alpha_1 & -(\mu_1 + \mu_2) \end{pmatrix}$$

$$(4)$$

To calculate the MTSF, we took the transpose of the matrix Q and deleted the rows and columns for the absorbing state. The new matrix is called A

$$A = \begin{bmatrix} -\lambda_1 & 0 & \lambda_1 & 0 & 0 & 0 & 0 & 0 \\ 0 & -\lambda_2 & 0 & \lambda_2 & 0 & 0 & 0 & 0 \\ \beta_1 & 0 & -(\alpha_1 + \beta_1) & 0 & \alpha_1 & 0 & 0 & 0 \\ 0 & \beta_2 & 0 & -(\alpha_2 + \beta_2) & 0 & \alpha_2 & 0 & 0 \\ \mu_1 & 0 & 0 & 0 & -(\lambda_2 + \mu_1) & 0 & \lambda_2 & 0 \\ 0 & \mu_2 & 0 & 0 & 0 & -(\lambda_1 + \mu_2) & 0 & \lambda_1 \\ 0 & 0 & 0 & \mu_1 & 0 & 0 & -(\alpha_2 + \mu_1) & 0 \\ 0 & 0 & \mu_2 & 0 & 0 & 0 & 0 & -(\alpha_1 + \mu_2) \end{bmatrix}$$

$$(5)$$

Therefore, the expected time to reach an absorbing state was calculated from

$$MTSF = E[T_{p(0) \to p(absorbing)}] = p(0) * (-A^{-1}) * \begin{cases} 1\\1\\1\\1\\1\\1\\1 \end{cases}$$
(6)

$$\begin{split} MTSF &= [\mu_1^2\alpha_1^2 + \mu_1^2\alpha_1\mu_2 + \mu_1^2\alpha_1\beta_1 + \mu_1^2\beta_1\mu_2 + \mu_1^2\lambda_2\alpha_1^2 + \mu_1\lambda_1\alpha_1\beta_1 + \mu_1\lambda_2\beta_1\mu_2 + \mu_1\alpha_1^2\alpha_2 + \mu_1\alpha_1\alpha_2\mu_2 + \mu_1\alpha_1\alpha_2\beta_1 + \mu_1\beta_1\mu_2\alpha_2 + \alpha_1^2\alpha_2\lambda_2 + \alpha_2\mu_2\alpha_1\lambda_1 + \lambda_2\alpha_1\alpha_2\beta_1 + \lambda_2\beta_1\mu_2\alpha_2]/(\lambda_1\lambda_2\alpha_1)(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) \\ &+ \mu_1[\lambda_1\alpha_1\beta_2 + \lambda_1\beta_2\mu_2 + \alpha_2\mu_2\alpha_1 + \alpha_1\beta_2\mu_2 + \beta_2\mu_2^2 + \mu_2^2\alpha_2]/(\lambda_1\lambda_2\alpha_2)(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) + \\ [\alpha_1\mu_1^2 + \mu_1^2\mu_2 + \mu_1\lambda_2\alpha_1 + \mu_1\lambda_2\mu_2 + \alpha_2\mu_1\alpha_1 + \mu_1\mu_2\alpha_2 + \lambda_2\alpha_1\alpha_2 + \mu_2\alpha_2\lambda_2]/\lambda_2\alpha_1(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) + \\ \mu_1[\lambda_1\alpha_1 + \lambda_1\mu_2 + \mu_2\alpha_1 + \mu_2^2]/\lambda_1\alpha_2(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) + (\alpha_1\mu_1 + \mu_2\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2)/\lambda_2(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) \\ \mu_1[\lambda_1 + \mu_2]/\lambda_1(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) + (\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) + \mu_1/(\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2) \end{split}$$

Multiplying each term by the L.C.M. ($\alpha_1\mu_1 + \alpha_1\alpha_2 + \alpha_2\mu_2$) and simplifying the terms, the following equations were obtained:

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$$MTSF = (z_{1} + z_{2} + z_{3} + z_{4}) / z_{5}$$

$$z_{1} = \alpha_{2}(\alpha_{1} + \mu_{2})(\alpha_{2} + \mu_{1})(\alpha_{1} + \beta_{2})(\lambda_{2} + \mu_{1})$$

$$z_{2} = \alpha_{1}\mu_{2}(\alpha_{1} + \mu_{2})(\lambda_{1} + \mu_{2})(\lambda_{2} + \alpha_{2} + \beta_{2})$$

$$z_{3} = \lambda_{1}\alpha_{2}(\alpha_{1} + \mu_{2})[(\lambda_{2} + \mu_{1})(\alpha_{2} + \mu_{1}) + \alpha_{1}(\lambda_{2} + \alpha_{2})$$

$$z_{4} = \alpha_{1}\alpha_{2}\mu_{1}\lambda_{1}(\alpha_{1} + \lambda_{1})$$

$$z_{5} = \alpha_{1}\alpha_{2}\lambda_{1}\lambda_{2}(\alpha_{1}\mu_{1} + \alpha_{1}\alpha_{2} + \alpha_{2}\mu_{2})$$
(7)

Availability Analysis for the System

For the availability analysis of the states of the system represented in Figure 1, the initial conditions for this problem are the same as for the reliability case:

$$p(0) = [p_0(0), p_1(0), p_2(0), p_3(0), p_4(0), p_5(0), p_6(0), p_7(0), p_8(0)] = [1, 0, 0, 0, 0, 0, 0, 0, 0]$$

From the equation (3), the steady state availability could be obtained using the following procedure. In the steady state situation, the derivatives of the state probabilities become zero (El-Said and Elshebeny, 2005). That allowed to calculate the steady state availability for the system defined as:

$$A(\infty) = 1 - p_8(\infty) \tag{8}$$

we also have equation (9) been satisfied:

$$Q * p(\infty) = 0 \tag{9}$$

Thus, to obtain $P_8(\infty)$, equation (7) was solved under the following normalization condition

$$\sum_{i=1}^{8} p_i(\infty) = 1 \tag{10}$$

This was done by substituting equation (8) in any of the redundant rows in equation (3) to yield equation (11).

$$B = \begin{bmatrix} \lambda_1 & 0 & \beta_1 & 0 & \mu_1 & 0 & 0 & 0 & 0 \\ 0 & -\lambda_2 & 0 & \beta_2 & 0 & \mu_2 & 0 & 0 & 0 \\ \lambda_1 & 0 & (\alpha_1 + \beta_1) & 0 & 0 & 0 & 0 & \mu_2 & 0 \\ 0 & \lambda_2 & 0 & -(\alpha_2 + \beta_2) & 0 & 0 & \mu_1 & 0 & 0 \\ 0 & 0 & \alpha_1 & 0 & -(\lambda_2 + \mu_1) & 0 & 0 & 0 & \mu_2 \\ 0 & 0 & 0 & \alpha_2 & 0 & -(\lambda_1 + \mu_2) & 0 & 0 & \mu_1 \\ 0 & 0 & 0 & 0 & \lambda_2 & 0 & -(\alpha_2 + \mu_1) & 0 & 0 \\ 0 & 0 & 0 & 0 & \lambda_1 & 0 & -(\alpha_1 + \mu_2) & 0 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix}$$

For Figure 1, the steady state availability of the proposed system $A_T(\infty)$ is given by:

Where $N = \lambda_1 \lambda_2 h_5$

$$\begin{split} & D = \lambda_1 \lambda_2 \alpha_1 \mu_1 (h_1 + \mu_2 h_2) + \lambda_1 \lambda_2 \mu_1 (h_4 + \alpha_1 \mu_1 h_3) + \lambda_1^2 \lambda_2^2 \alpha_1 \alpha_2 h \\ & h_1 = (\alpha_1 + \mu_2) [\mu_1^2 (\lambda_2 + \beta_2) + \alpha_2^2 (\lambda_1 + 2\mu_1) + \lambda_2 \mu_1 (\lambda_1 + 2\alpha_2)] \\ & h_2 = (\alpha_2 + \beta_2) (\lambda_1 \alpha_1 + \lambda_1 \mu_2 + \alpha_1 \mu_2) + (\lambda_1 \mu_1 + \mu_2^2) + \alpha_2 (\alpha_2 \beta_1 + \mu_2 \beta_2 + \alpha_2 \beta_2) + 2\mu_1 \alpha_2 (\alpha_2 + \beta_1) \\ & h_3 = (\alpha_2 + \mu_2) (\lambda_1 \mu_1 + \lambda_1 \lambda_2 + 2\mu_1 \alpha_2) + \mu_1 (\mu_1 + \lambda_2) + (\lambda_1 + \alpha_1 + \beta_1) + \mu_2 (\alpha_1 \mu_2 + \alpha_2 \beta_1 + \lambda_1 \alpha_2) \\ & h_4 = \alpha_1 \alpha_2 (\mu_1 + \alpha_2) (2\lambda_1 \mu_2 + \lambda_2 \alpha_1) + \lambda_2 \mu_1 [\mu_2 (\alpha_1^2 + \alpha_2 \beta_1) + \alpha_2^2 (\alpha_1 + \beta_1)] \\ & h_5 = (\mu_1 + \mu_2) (\alpha_1 + \alpha_2 + \mu_1 + \mu_2) \end{split}$$

The solution of equation (12) above produced the steady state probabilities of the availability analysis.

2.5 Busy Period Analysis $BP(\infty)$

The initial conditions for this problem are the same as for the reliability case:

$$p(0) = [p_0(0), p_1(0), p_2(0), p_3(0), p_4(0), p_5(0), p_6(0), p_7(0), p_8(0)]$$

= [1,0,0,0,0,0,0,0]

The differential equation form can be expressed as shown in equation (13).

$$D = \begin{bmatrix} \lambda_1 & 0 & \beta_1 & 0 & \mu_1 & 0 & 0 & 0 & 0 \\ 0 & -\lambda_2 & 0 & \beta_2 & 0 & \mu_2 & 0 & 0 & 0 \\ \lambda_1 & 0 & (\alpha_1 + \beta_1) & 0 & 0 & 0 & 0 & \mu_2 & 0 \\ 0 & \lambda_2 & 0 & -(\alpha_2 + \beta_2) & 0 & 0 & \mu_1 & 0 & 0 \\ 0 & 0 & \alpha_1 & 0 & -(\lambda_2 + \mu_1) & 0 & 0 & 0 & \mu_2 \\ 0 & 0 & 0 & \alpha_2 & 0 & -(\lambda_1 + \mu_2) & 0 & 0 & \mu_1 \\ 0 & 0 & 0 & 0 & \lambda_2 & 0 & -(\alpha_2 + \mu_1) & 0 & 0 \\ 0 & 0 & 0 & 0 & \lambda_1 & 0 & -(\alpha_1 + \mu_2) & 0 \\ 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix}$$

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The steady state busy period was obtained using the following procedure. In the steady state, the derivatives of the state probabilities become zero (El-Said and Elshebeny, 2005). That allows us to calculate the steady state probabilities with

$$B(\infty) = 1 - [p(\infty) + p_1(\infty)]$$

$$\varrho * p(\infty) = 0$$
(14)

The matrix form of equation (15) is given in equation (16)

$$Q = \begin{bmatrix} \lambda_1 & 0 & \beta_1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -\lambda_2 & 0 & \beta_2 & 0 & \mu_2 & 0 & 0 & 0 \\ \lambda_1 & 0 & (\alpha_1 + \beta_1) & 0 & 0 & 0 & 0 & \mu_2 & 0 \\ 0 & \lambda_2 & 0 & -(\alpha_2 + \beta_2) & 0 & 0 & \mu_1 & 0 & 0 \\ 0 & 0 & \alpha_1 & 0 & -(\lambda_2 + \mu_1) & 0 & 0 & 0 & \mu_2 \\ 0 & 0 & 0 & \alpha_2 & 0 & -(\lambda_1 + \mu_2) & 0 & 0 & \mu_1 \\ 0 & 0 & 0 & 0 & \lambda_2 & 0 & -(\alpha_2 + \mu_1) & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & \lambda_1 & 0 & -(\alpha_1 + \mu_2) & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & -(\mu_1 + \mu_2) \end{bmatrix}$$

$$Q \times \begin{bmatrix} p_0(\infty) \\ p_1(\infty) \\ p_2(\infty) \\ p_3(\infty) \\ p_3(\infty) \\ p_4(\infty) \\ p_5(\infty) \\ p_5(\infty) \\ p_6(\infty) \\ p_7(\infty) \\ p_8(\infty) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$(16)$$

To obtain $P_0(\infty)$, $P_1(\infty)$, equation (16) was solved and the following normalization condition. Equation (16) was substituted in any one of the redundant rows in equation (15) to yield equation (17):

$$D \times \begin{bmatrix} p_0(\infty) \\ p_1(\infty) \\ p_2(\infty) \\ p_3(\infty) \\ p_4(\infty) \\ p_5(\infty) \\ p_6(\infty) \\ p_6(\infty) \\ p_7(\infty) \\ p_8(\infty) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

$$(17)$$

The steady state busy period $BP(\infty)$ is given

 μ_2 $\alpha_2 + (_2$ $BP(\infty) = (\mu_1^3)$ λ_1 μ_2 α_2 α_1 $\lambda_1 + \lambda_1$ μ_2 α_2^2 + μ_2 λ_2 μ_2 μ_2^2 μ_2^2 α1 $\lambda_2 + \alpha_1^2$ λ2 α_2 + α_2 + μ_2 λ_2 α_2 $\lambda_1 + \lambda_2$ α_2 μ_2 $\alpha_1 + \lambda_2$ α_2 λ₁) $\mu_1^2+(\lambda_1)$ $\mu_2^2 + 2$ μ_2 + λ_2 α_2^2 $\alpha_1^2 + \lambda_2$ α_2 α_1 λ_1 α_1 λ_2 α_2 α_1 + λ_1 $\mu_2^2 +$ μ_2^2 λ_1 $\alpha_1^2 +$ λ_1 λ_2 μ_2^2 λ_2 $\alpha_1^2 + \lambda_1$ λ_2 + λ_2 α_1^2 λ_1 λ_2 α_2 + α_2 μ_2 α_1 α_1^2 μ_2^2 $\alpha_2^2 + \lambda_1$ μ_2 +2 α_{1}^{2} μ_2 + λ_1 $\alpha_2^2 + \lambda_2$ $\mu_2^3 + 2$ α_2 λ_2 α_2 μ_2 λ_2 α_1 λ_2 α_1 $\alpha_1 + \lambda_2$ μ_2^2 λ_1 μ_2 α_2^2 λ_1 α_2^2 α_1 μ_1 + λ_1 α_1 μ_2^2 λ_2 $\alpha_2 + \lambda_1$ α_2^2 α_{2+2} μ_2 $\lambda_2 \\$ α_2 α_{1}^{2} + α_1 α_2^2 μ_2 + λ_1 λ_2 α_{1}^{2} λ_2 α_2^2 $\alpha_1^2 + \lambda_1$ μ_2^2 α_2^2)/((λ_1 μ_2 + λ_1 α_1 $\mu_1^3+(\alpha_1)$ λ_1 + α_1^2 α_2^2 β_2 + β_1 α_2 $\alpha_1 + \lambda_1$ μ_2 α_2 + μ_2 β_1 α_2 μ_2 + μ_2 α_1 λ_2 $\alpha_{2}^{2} +$ μ_2^2 μ_2^2 $\alpha_2^2 + \lambda_1$ λ_1 α_2 + λ_1 + λ_2+2 μ_2 μ_2 μ_2 α_1 β_2 λ_1 + λ_2 α_2 α_1 μ_2 λ_2 $\lambda_1 + 2$ $\alpha_2 + 2$ α_1^2 μ_2^2 β_2 + β_1 μ_2^2 μ_2 α_2 α_1 α_2 μ_2 + α_1 α_2 μ_2 $\alpha_1 + \alpha_1$ μ_2 α_1 α_1 λ_1 + λ_2 α_2 + λ_2 μ_2 α_{1}^{2} + μ_2^2 β_1 $\alpha_2 + \alpha_1^2$ λ_2 α_2 + λ_2 α_2 α_2 β_1 μ_2) $\mu_1^2 + (\alpha_1^2)^2$ $\alpha_1^2 +$ μ_2^2 μ_2^3 μ_2^3 μ_2^2 α_1^2 α_2+2 α_2^2 α_2^2 $\beta_1 + \alpha_1$ μ_2^2 $\beta_2 + \mu_2^2$ μ_2 β_2 + α_1 α_2+2 α_1 $\mu_2^3 +_2$ $\alpha_1^2 + \lambda_1$ $\alpha_2^2 + \lambda_1$ μ_2^2 $\alpha_2^2 + \lambda_2$ λ_2 μ_2 + λ_1 λ_2 α_1 λ_1 α_1 α_2 α_2 λ_2 $\mu_2{}^2$ $\alpha_2^2 + \lambda_2$ μ_2 α_2^2 $\alpha_1 + \lambda_1$ $\alpha_2 + \lambda_1$ λ_2 α_{1}^{2} + μ_2^2 α_1 $\lambda_2 + \lambda_1$ α_1^2 λ_2 λ_1 μ_2 μ_2 + λ_1 μ_2 α_2^2 $a_1 +_2$ α_{1}^{2} $\alpha_1 + 2$ α_1 $\mu_2^2 + 2$ λ_1 λ_2 α_2 λ_2 λ_1 α_2^2 λ_2 α_1 μ_2 + α_2 α_2^2 $\mu_2^2 +$ μ_2^2 $\alpha_1^2 + \lambda_2$ α_{1}^{2} μ_2^2 $\alpha_2 + \lambda_2$ λ_2 β_1 μ_2 $\alpha_2^2 + \lambda_2$ β_1 $\alpha_2 + \alpha_2^2$ μ_2 α_1 β_1+ μ_2^2 β_2 + α_1^2 μ_2^2 μ_2^2 α_{1}^{2} β_2 + λ_1 α_1 β_2 α_2 + α_1 α_2 $\mu_1 + \lambda_1$ μ_2 μ_2 $\alpha_{1}{}^{2}$ α_2^2 α_2^2 α_1^2 + λ_1 α_2^2 λ_2 μ_2 + λ_1 λ_1 $\alpha_1^2 + \lambda_1$ α_1 μ_2 + λ_1 λ_2 α_2 α_2 + α_1 α_2^2 (18) μ_2^2

RESULTS AND DISCUSSIONS Profit Analysis

The expected total profit per unit time incurred to the system in the state is given by

Profit = total revenue- total cost
$$PF(\infty) = C_0A(\infty) - C_1B(\infty)$$
 (19) Where, $PF(\infty)$: is the profit incurred to the system C_0 ; is the revenue per unit up-time of the system C_1 ; is the cost per unit time which the system is under repaired.

Table 1: Relation Between Failure Rate, MTSF, $A_T(\infty)$ and $PF(\infty)$ of the System.

λ_1	MTSF	SAV	Profit
0.10	49.6253	0.5175	431.8572
0.20	30.2215	0.4260	334.5789
0.30	23.7535	0.3873	293.3997
0.40	20.5196	0.3659	270.6531
0.50	18.5792	0.3523	256.2262
0.60	17.2856	0.3429	246.2603
0.70	16.3616	0.3361	238.9633
0.80	15.6686	0.3308	233.3898
0.90	15.1296	0.3267	228.9935
1.00	14.6984	0.3234	225.4372

The failure rate of the system, mean to system failure, system availability, and the profit incurred by the system are summarized in Table 1. Relationship between the system failure rate and the profit incurred is shown in Figure 2. System availability is plotted against its failure

in Figure 3 while mean time to system failure is plotted against the system failure rate as shown in Figure 4. In each of the three cases, it is found that as the system failure increases the dependent variable decreases exponentially.

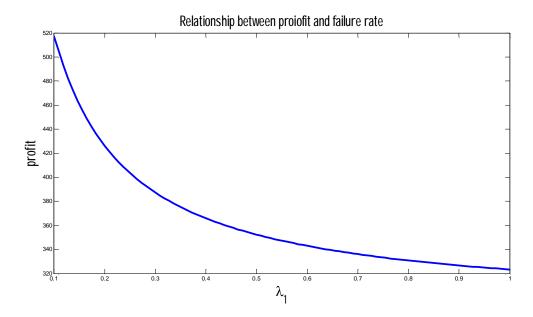


Figure 1: Relationship between $PF(\infty)$ and λ_1

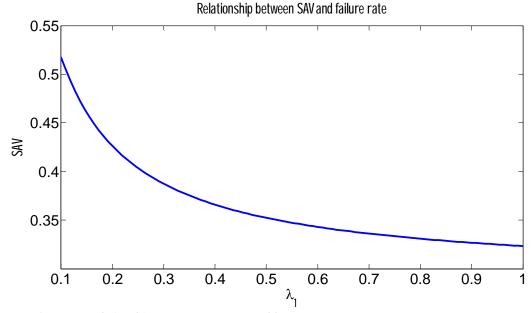


Figure 2: Relationship Between $A_T(\infty)$ and λ_1

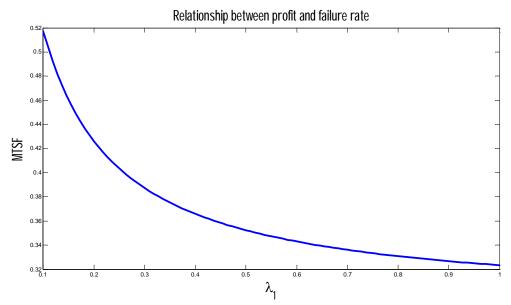


Figure 3: Relationship Between MTSF and λ_1

CONCLUSION

The characteristics, MTSF, $A_T(\infty)$ and $PF(\infty)$ were compared with respect to failure rate λ_1 for the system at fixed values of $\alpha_1, \alpha_2, \beta_1, \beta_2, \lambda_2, \mu_1, \mu_2$, R_1, R_2 . It was found that MTSF, $A_T(\infty)$ and $PF(\infty)$ are decreasing with the increase of the failure rate λ_1 . Periodic inspection, maintenance, and repairs of the units would fetch more profit to the system.

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