

Scour from the interstitial spaces in cobble-bed rivers

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Abstract

The periodic removal of sand from the interstitial spaces between cobbles is extremely important for ecosystem functioning in cobble-bed rivers. In order to flush fine sediments from the interstitial spaces between cobbles in river reaches downstream of dams, specific dam releases known as flushing flows or sediment maintenance flows are utilised. This paper describes the development and calibration of a mathematical model to predict the equilibrium depth of scour of fine sands from between cobbles in terms of applied stream power principles. The model was developed with the aid of physical model experiments and is founded on a stream power model which defines the condition of dynamic equilibrium in a deformed sand-bed river. Calibration was done in the laboratory under clear water conditions and with uniform cobble sizes. The scouring of fine sands in cobble-bed rivers is associated with an increase in absolute bed roughness and an associated decrease in the unit stream power applied along the bed as the cobbles become exposed. When scour ceases, the sand particles on the bed are at the movement threshold and critical conditions exist. In order to establish the relationship between equilibrium scour depth and bed particle characteristics, the power which is required to suspend sand particles under laminar boundary conditions is equated with the turbulent power being applied along the bed.

Keywords: cobble-bed, interstitial spaces, flushing flows, stream power, scour depth, environmental flow requirements

Introduction

In cobble-bed rivers, many aquatic species are dependent on the interstitial spaces between the cobbles for their survival. Salmonids, for example, use these spaces for laying their eggs while the spaces also provide habitat and sheltering for various benthic insects (Gordon et al., 1992). The accumulation of fine sediments in cobble-bed rivers, which fill these interstitial spaces, can have a detrimental effect on the whole aquatic ecosystem and scouring of the interstitial sand from cobble beds is seen as the single most important substrate maintenance process for river biota (Hirschowitz et al., 2007). Natural phenomena such as catchment erosion may lead to sediment loads being introduced and deposited on cobble river beds, but natural floods ensure the periodic removal thereof. The construction of a dam, however, leads to a decrease in flood peaks, flood frequency and sediment transport capacity in the river channel downstream and fine sediments introduced into this part of the river system, either via the dam or from the downstream catchment, may accumulate on parts of the river bed.

In order to flush fine sediments from the interstitial spaces between cobbles downstream of dams, specific dam releases known as flushing flows or sediment maintenance flows are utilised. The range of effective flushing flows is relatively narrow. Whereas the rate and efficiency of fine sand removal increase with discharge, so does the cost if the released water is lost for storage, diversion or power generation. The transport rate of larger sized sediments also increases with discharge and may need to be kept within limits. The size of a flushing flow may be further constrained by the release capacity of the dam, financial

and legal liabilities associated with the creation of an artificial flood as well as the availability of water at the appropriate time (Wilcock et al., 1996). In addition, the quantification of flushing flows is subject to uncertainty due to the complexity of flow and sediment transport mechanisms in cobble-bed rivers. Although there is a clear need to specify flushing flows as accurately as possible, relatively crude methods are often used due to a lack of appropriate models. These include the specification of discharges with a certain return period or methods based on complicated estimates of critical shear stress in mixed size sediments (Reiser et al., 1989).

Ligon et al. (1995) and Kondolf and Wilcock (1996) noted that the goals of flushing flows need to be stated in terms of measurable changes to the physical habitat rather than the abundance of organisms. In line with this philosophy, this paper addresses flushing flows in terms of a sand scour model which is founded on the law of conservation of stream power and which defines the relationship between discharge and the absolute depth of scour of fine sands from between cobbles.

Sediment transport and the principle of least applied power

The law of conservation of power, which is defined in scalar terms and directly related to time, is a third derivative of Newton's second law together with the laws of conservation of energy and momentum. This law has been found to provide good insight into the sediment transport characteristics of rivers and is defined by Rooseboom (1974) under conditions of steady, turbulent uniform flow as:

$$\int_{y_0}^D \rho g s v dy = \int_{y_0}^D \tau \frac{dv}{dy} dy \quad (1)$$

where:

ρ = fluid density (kg/m³)

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- g = gravitational acceleration (m/s²)
 s = energy slope
 $v = \sqrt{2\pi g D s} \ln \frac{y}{y_0}$; velocity at distance y above the bed (m/s)
 D = flow depth (m)
 $y_0 \approx k/30$; ordinate where the velocity is mathematically equal to zero (m)
 k = absolute bed roughness (m)
 τ = shear stress at distance y above the bed (N/m²)

The term $\rho g s v$ in Eq. (1) represents the amount of unit power made available by a flowing river, whereas $\tau \frac{dv}{dy}$ represents the power applied per unit volume to maintain motion.

The threshold condition

Based on the hypothesis that where alternative modes of flow exist, that mode of flow which requires the least amount of unit power will be followed, it follows that fluid flowing over movable material would only transport the material, if it will result in a decrease in the amount of unit power being applied (Rooseboom, 1998). As the power applied along the bed of a river varies depending on whether laminar or turbulent flow conditions prevail at the bed, the critical condition for sediment movement also depends on whether the flow at the bed is laminar or turbulent. The applied power required per unit volume to suspend a particle with density ρ_s and settling velocity V_{ss} in a fluid with density ρ , equals (Rooseboom, 1992):

$$(\rho_s - \rho)g V_{ss} \quad (2)$$

Stokes's law (Graf, 1971) defines the settling velocity of a particle with diameter d under viscous conditions as:

$$d^2 g \frac{\rho_s - \rho}{18\rho\nu} \quad (3)$$

where:

$$\nu = \text{kinematic viscosity (m}^2/\text{s)}$$

Under conditions of turbulent flow, the settling velocity as expressed by Graf (1971) equals:

$$\sqrt{\frac{4(\rho_s - \rho)gd}{3\rho C_d}} \quad (4)$$

where:

$$C_d = \text{drag coefficient (assumed constant for larger diameters)}$$

Under conditions of laminar or smooth turbulent flow, Rooseboom (1974) showed that the unit stream power applied along the bed equals:

$$\frac{(\rho g s D)^2}{\rho\nu} \quad (5)$$

The critical condition for the movement of sediment particles is reached when the power applied along the bed exceeds the power required to suspend the sediment particles. From Eqs. (2), (3) and (5) a relationship defining the threshold for sediment transport under viscous conditions can be defined. This relationship, calibrated with data by Grass (1970) and Yang (1973), is found to be:

$$\frac{\sqrt{gDs}}{V_{ss}} = \frac{1.6 v}{\sqrt{gDs} d} \quad (6)$$

for values of $\frac{\sqrt{gDs} d}{\nu} < 13$, i.e. with smooth turbulent or completely laminar flow over a smooth bed (Rooseboom, 1992).

Under conditions of rough turbulent flow, Rooseboom (1992) showed that the unit applied power along a bed of particles with diameter d is:

$$\approx \frac{30\rho g s D \sqrt{2\pi g s D}}{d} \quad (7)$$

From Eqs. (2), (4) and (7) therefore, the critical condition for the movement of sediment along an even bed in rough turbulent flow is defined by:

$$\frac{\sqrt{gDs}}{V_{ss}} = \text{Constant} \quad (8)$$

This relationship was calibrated with measured data from Yang (1973) and the value of the constant was found to be 0.12 for values of $\frac{\sqrt{gDs} d}{\nu} > 13$ (Rooseboom, 1992).

Dynamic equilibrium and sand-bed deformation

Equation (7), which represents the amount of stream power applied along a bed under conditions of rough turbulent flow, can also be re-written as:

$$\left(\tau \frac{dv}{dy} \right)_0 = \frac{14.8 \rho g s D \sqrt{2\pi g s D}}{R_0} \quad (9)$$

where:

$$R_0 \approx d/2; \text{ the radius of a turbulent eddy next to the bed (m)}$$

From Eq. (9), and based on the concept of minimum applied power, it is evident that once the threshold condition for sediment movement is exceeded a further reduction in the amount of unit turbulent stream power applied along an alluvial bed is possible by means of various mechanisms (Rooseboom, 1974). One of these mechanisms entails the formation of bed forms, i.e. ripples, dunes, etc., which result in an increase in the value R_0 .

Furthermore, it can be shown (Rooseboom, 1992) that the sediment concentration at any level within a stream is directly proportional to (applied power)² and subsequently that the sediment-carrying capacity of a stream is directly proportional to (applied power along the bed)², with z defined as:

$$z = \frac{5\sqrt{2\pi} V_{ss}}{6\sqrt{gDs}} \quad (10)$$

It therefore follows that, as an alluvial river reduces the amount of unit stream power applied along its bed through deformation of the bed, the river is effectively decreasing its sediment-carrying capacity – a process which continues until a condition is reached where the sizes of the boundary eddies that fit in with the bed forms become so large that the average rate of deposition of particles is equal to their average rate of re-suspension. At this point, the river is in a state of steady sediment transport or dynamic equilibrium. Under these conditions, with particles on the bed being entrained and deposited at the same rate, it is obvious that critical hydraulic conditions must prevail at the bed where individual particles are continually crossing the movement threshold. However, it has been observed that it is not possible to have sand particles of less than about 2 mm in diameter at rest under turbulent boundary conditions on an even bed, as the absolute bed roughness is too small to induce a turbulent boundary layer (Rooseboom, 1974). It therefore follows that at the point of dynamic equilibrium along a deformed sand-bed river, critical conditions for sediment movement prevail at and below an interface between a thin laminar boundary layer along the bed and turbulent eddies above. This was confirmed by Rooseboom and Le Grange (1994) who, based on an analysis of recorded flood levels and scour depths, concluded that contrary to conventional wisdom, laminar boundary conditions come into play when equilibrium conditions are approached at the

flood peak. The applied turbulent unit stream power at the bed, expressed in terms of the absolute bed roughness, must therefore be proportional to the unit power which is required to bring particles into suspension under laminar conditions (Rooseboom and Le Grange, 1994). From Eqs. (2) and (3), the unit stream power required to suspend particles under laminar boundary conditions is directly proportional to:

$$\frac{(\rho_s - \rho)^2 g^2 d^2}{\rho v} \quad (11)$$

In similar fashion, from Eq. (7), the unit stream power applied in maintaining motion along a river bed under turbulent flow conditions is approximately equal to:

$$\frac{30 \rho g s D \sqrt{2 \pi g s D}}{k} \quad (12)$$

where:

k = absolute bed roughness

From Eqs. (11) and (12):

$$\frac{30 \rho g s D \sqrt{2 \pi g s D}}{k} \alpha \frac{(\rho_s - \rho)^2 g^2 d^2}{\rho v}$$

which simplifies to:

$$\frac{\sqrt{g D s}}{V_{ss}} = \left[\frac{\sqrt{g D s k}}{\sqrt{2 \pi v}} \right]^{1/2} \text{Constant} \left[\frac{v}{\sqrt{g D s d}} \right] \quad (13)$$

A comparison of Eq. (13), which represents the condition of dynamic equilibrium in a deformed sand-bed river and defines the relationship between absolute bed roughness, particle characteristics and bed deformation, and Eq. (6), which represents critical conditions for sediment movement in laminar flow, reveals that the two equations are similar, except for the additional term $\left[\frac{\sqrt{g D s k}}{\sqrt{2 \pi v}} \right]^{1/2}$ in Eq. (13). Rooseboom and Le Grange (2000) calibrated Eq. (13) with available data on sand-bed deformation under conditions of dynamic equilibrium. Their findings confirmed that, contrary to conventional wisdom, a laminar boundary layer comes into play at equilibrium conditions in a deformed sand-bed river. They also concluded that the term $\left[\frac{\sqrt{g D s k}}{\sqrt{2 \pi v}} \right]^{1/2}$, referred to as delta (Δ), represents the decrease in applied stream power due to deformation of the bed, with k , the absolute bed roughness, reflecting the size of the boundary eddies that fit in with the changing bed forms.

A sand scour model for cobble-bed rivers

The scouring of fine sediments from the interstitial spaces in a cobble river bed is associated with changes in absolute bed roughness as the cobbles become exposed during scouring. It is hypothesised that the process of fine sediment scouring in a cobble-bed river and the associated change in absolute bed roughness is similar to the process of bed deformation in a sand-bed river, except for the fact that the cobbles will limit the extent of bed deformation (see Fig. 1). Consequently, at a particular discharge, the relationship that exists between sand particle characteristics and the maximum depth of sand scour in a cobble-bed river would be similar to the relationship that exists between absolute bed roughness and particle characteristics under conditions of dynamic equilibrium on a deformed sand-bed river.

In order to evaluate the above hypothesis, laboratory studies were undertaken. During the laboratory experiments, various combinations of sand and cobble sizes were employed to develop relationships between applied power, particle characteristics and maximum scour depth.

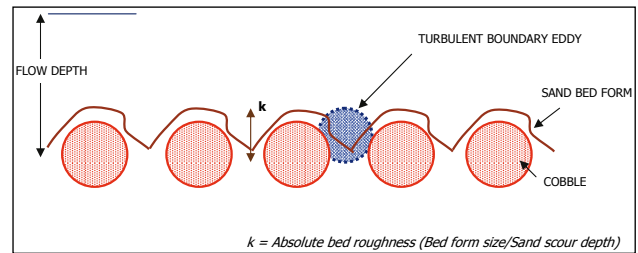


Figure 1
Schematic representation of similarities between cobble-bed sand scour and sand-bed deformation

Experimental procedure

Tests were performed in a horizontal flume of 1 m width and 40 m length in the hydraulics laboratory of the Department of Civil Engineering at the University of Stellenbosch. Cobbles were collected from rivers and sorted with a gravelometer. Two to three layers of uniform, spherical cobbles were arranged in a closely packed pattern in order to create an artificial cobble bed of approximately 2.4 m length. The cobbles were then completely covered with sand of a fairly uniform grading. At the upstream side of the cobble bed, a ramp of gravel and smaller cobbles was constructed to allow full development of the turbulent flow profile. Flow depths were controlled with an adjustable weir at the downstream end of the flume, which was also used for measuring discharge. Average velocities above the cobble bed were measured with an Ott-meter. The experiments focused on scour depths of up to one cobble diameter. In total, 50 experiments representing six different sand-cobble combinations were completed as shown in Table 1. The laboratory setup is shown diagrammatically in Fig. 2 (next page).

Experiment	Median sand diameter (mm)	Cobble diameter (mm)
I	0.22	60
II	0.22	71
III	0.22	130
IV	0.54	80
V	0.54	130
VI	0.83	60

After preparation of the sand-covered cobble bed, the following basic procedure was followed:

- With the adjustable downstream weir controlling the water level in the flume, water was allowed to fill the flume very slowly in such a way that no sand movement took place along the cobble bed
- The water supply to the flume was slowly increased until the desired discharge was obtained. The discharge was calculated from the water level at the downstream weir and was verified with velocity and depth measurements above the cobble bed. A large enough depth was maintained above the cobble bed to ensure that no sand movement took place.
- The adjustable weir was rapidly lowered until the desired water depth above the experimental cobble-bed area was reached. This represented the start of the experiment.
- At pre-determined positions along the bed, the level of the sand (depth of scour) was measured as the experiment pro-

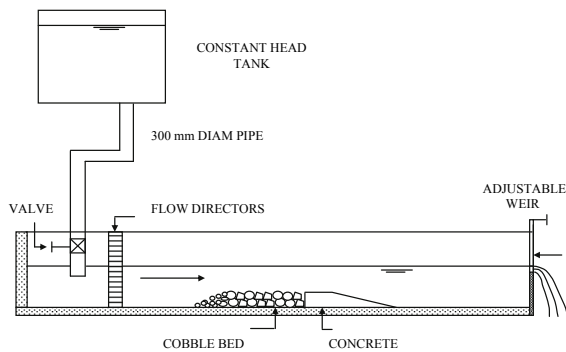


Figure 2
Laboratory set-up

gressed until no further change in the scour level could be observed.

Due to the relatively short length of the cobble bed within the flume, it was not possible to measure the difference in water levels between the upstream and downstream sections of the experimental cobble-bed reach accurately. As the flow depth above the cobble bed was controlled by the downstream weir, the flow in the flume was slightly non-uniform. Based on the procedure for calculating the energy slope under conditions of gradually varied flow, the Chézy formula was used to calculate the energy slope above the cobble-bed area based on the measured average flow velocity. Due to the large difference in resistance between the cobble bed of the flume and the glass sidewalls, it was assumed that flow resistance along the centreline would be affected only slightly by the sidewalls and the hydraulic radius in the Chézy equation was substituted with the flow depth above the cobble bed. The scour depth beneath the top of the cobbles was used to represent the absolute roughness (k) in the Chézy equation. In order to limit the uncertainty associated with large-scale roughness, the ratio of flow depth to absolute roughness was maintained at values above three throughout the experiments. Jonker (2002) provides a detailed description of the experimental procedure.

A summary of the experimental data is included as Table 2.

Laminar boundary conditions

In order to gain insight into the hydraulic conditions that existed at the experimental cobble bed when the maximum level of sand scour was reached, the laboratory data were analysed in terms of $\frac{\sqrt{gDs}}{V_{*c}}$ and $\frac{\sqrt{gDs}}{V_{*c}}$, which define the movement threshold for cohesionless sediment particles under both laminar and turbulent boundary conditions. The energy gradients in the above terms were calculated based on an absolute roughness equivalent to the maximum scour depth that was reached below the top of the cobble crests, while V_{*c} was calculated as the settling velocity of the sand particles (with diameter d) under laminar conditions, i.e. by means of Eq. (3).

Figure 3 shows the results of the experimental analysis superimposed on the modified Liu curve (Liu, 1957). It shows that cobble-bed scour data with

Setup	Median sand diam. (mm)	Cobble diam. (mm)	Flow depth (m)	Dis-charge (m ³ /s)	Veloc-ity (m/s)	Energy slope (-)	Scour depth (mm)
I	0.22	60	0.400	0.200	0.500	0.0002	8
	0.22	60	0.071	0.025	0.354	0.0018	15
	0.22	60	0.600	0.300	0.500	0.0002	15
	0.22	60	0.200	0.100	0.500	0.0011	30
	0.22	60	0.500	0.300	0.600	0.0004	30
	0.22	60	0.600	0.400	0.667	0.0004	40
	0.22	60	0.800	0.600	0.750	0.0004	40
	0.22	60	0.300	0.200	0.667	0.0013	45
	0.22	60	0.800	0.500	0.625	0.0003	45
	0.22	60	0.250	0.200	0.800	0.0027	60
II	0.22	60	0.400	0.300	0.750	0.0012	60
	0.22	60	0.500	0.400	0.800	0.0010	60
	0.22	60	0.600	0.500	0.833	0.0008	60
	0.22	71	0.201	0.099	0.494	0.0011	36
	0.22	71	0.400	0.200	0.500	0.0004	36
	0.22	71	0.804	0.502	0.624	0.0003	53
III	0.22	71	0.299	0.200	0.669	0.0016	71
	0.22	71	0.601	0.403	0.671	0.0006	71
	0.22	71	0.600	0.499	0.832	0.0009	71
	0.22	130	0.235	0.120	0.511	0.0010	36
	0.22	130	0.268	0.160	0.597	0.0013	53
IV	0.22	130	0.340	0.243	0.715	0.0014	64
	0.22	130	0.399	0.390	0.977	0.0029	121
	0.54	80	0.200	0.109	0.545	0.0012	29
	0.54	80	0.273	0.226	0.828	0.0023	49
	0.54	80	0.406	0.237	0.584	0.0005	28
	0.54	80	0.278	0.256	0.921	0.0031	59
	0.54	80	0.567	0.333	0.587	0.0004	36
	0.54	80	0.405	0.387	0.956	0.0017	46
	0.54	80	0.448	0.346	0.772	0.0009	45
V	0.54	80	0.698	0.525	0.752	0.0005	42
	0.54	80	0.374	0.465	1.243	0.0042	80
	0.54	130	0.289	0.162	0.561	0.0010	53
	0.54	130	0.308	0.236	0.766	0.0020	71
	0.54	130	0.339	0.332	0.979	0.0033	95
	0.54	130	0.321	0.186	0.579	0.0008	41
	0.54	130	0.320	0.228	0.713	0.0015	63
	0.54	130	0.399	0.530	1.328	0.0054	122
VI	0.83	60	0.305	0.200	0.656	0.0008	20
	0.83	60	0.499	0.295	0.592	0.0004	20
	0.83	60	0.703	0.505	0.718	0.0003	20
	0.83	60	0.400	0.295	0.738	0.0009	30
	0.83	60	0.599	0.394	0.658	0.0004	30
	0.83	60	0.601	0.505	0.841	0.0006	30
	0.83	60	0.501	0.394	0.786	0.0008	40
	0.83	60	0.709	0.600	0.846	0.0006	40
	0.83	60	0.397	0.394	0.992	0.0019	45
	0.83	60	0.502	0.505	1.006	0.0014	45
	0.83	60	0.303	0.295	0.973	0.0030	60
0.83	60	0.603	0.600	0.995	0.0012	60	

similar values of Δ , representing absolute bed roughness at the point of maximum scour, display the same pattern as that displayed by the curved section of the modified Liu Curve, which represents critical conditions for cohesionless sediment particles smaller than 2 mm on an even bed with laminar boundary layer conditions (Rooseboom, 1992). Figure 3 therefore suggests that similar to Rooseboom and Le Grange's (2000) findings related to dynamic equilibrium in a sand-bed river, the condition of maximum sand scour in a cobble bed goes hand in hand with critical conditions for sediment movement and the formation of a laminar sublayer below the turbulent eddies that fit in with the exposed cobbles.

The maximum depth of scour

As a further test of the hypothesis that the process of sand scouring in a cobble-bed river and the associated change in absolute bed roughness is

similar to the process of bed deformation in a sand-bed river, the results of the cobble-bed sand scour experiments were superimposed on a diagram which represents the full spectrum of bed conditions in a sand-bed river, from lower regime to upper regime, within a single system (Fig. 4). This diagram was developed by Rooseboom and Le Grange (1994) based on the theory of dynamic equilibrium. It displays the typical progression of equilibrium conditions in a sand-bed river for three sand particle diameters and shows that, for any particular sand particle diameter, as the value of $\frac{\sqrt{gDs}}{V}$ increases, equilibrium with lower regime bed forms goes hand in hand with increasing k or $\left[\frac{\sqrt{gDs} k}{\sqrt{2\pi} v}\right]^{1/2}$ values and laminar boundary conditions. This continues until a sharp turning point is reached when the boundary conditions below the turbulent eddies switch to being turbulent. The bed becomes unstable and while $\frac{\sqrt{gDs}}{V}$ values remain constant, k values decrease dramatically until a new turning point is reached, from where upper regime bed forms develop and laminar boundary conditions again dominate.

From Fig. 4 it is clear that for a particular sand particle diameter, as the value of $\frac{\sqrt{gDs}}{V}$ increases, the maximum sand scour depth that was reached in the cobble-bed scour experiments (as represented by Δ) increased in similar fashion to the progression of equilibrium conditions and the associated development of bed forms in a sand-bed river. Furthermore, as is evident in the case of the 0.22 mm and 0.54 mm diameter sand particles, Fig. 4 shows that no transition (represented by a sudden decrease in the value of Δ) occurred in the case of the cobble-bed river, as opposed to a sand-bed river where transition from lower to upper regime bed forms occurs at a critical value of $\frac{\sqrt{gDs}}{V}$. However, as the 'bed-forms' in a cobble bed are fixed by the exposed cobbles which cannot be washed away, this was expected. Figure 4 therefore confirms the hypothesis that the

hydraulic conditions at the point of maximum sand scour along a cobble-bed river are comparable to those that prevail under conditions of dynamic equilibrium in a sand-bed river.

As a final confirmation, the results of the cobble-bed scour experiments were superimposed on a diagram (Fig. 5) which provides a complete averaged picture of the relationship between absolute bed roughness and sand particle characteristics under different flow conditions in an alluvial sand-bed river (Rooseboom and Le Grange, 2000). Again it was found that similar relationships exist between the maximum scour depth in a cobble-bed, and dynamic equilibrium conditions in a sand-bed river, as represented by an increase in the magnitude of Δ . Furthermore, the results indicated that the order of magnitude of the cobble-bed and sand-bed Δ -values are similar up to the point of transition from lower to upper regime bed forms conditions for a sand-

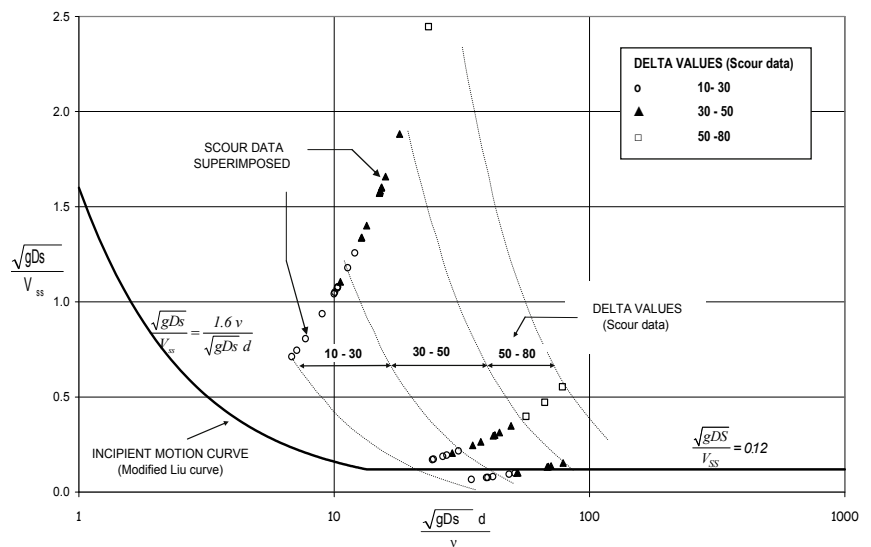


Figure 3
Cobble-bed scour data in relation to critical conditions for cohesionless sediment particles

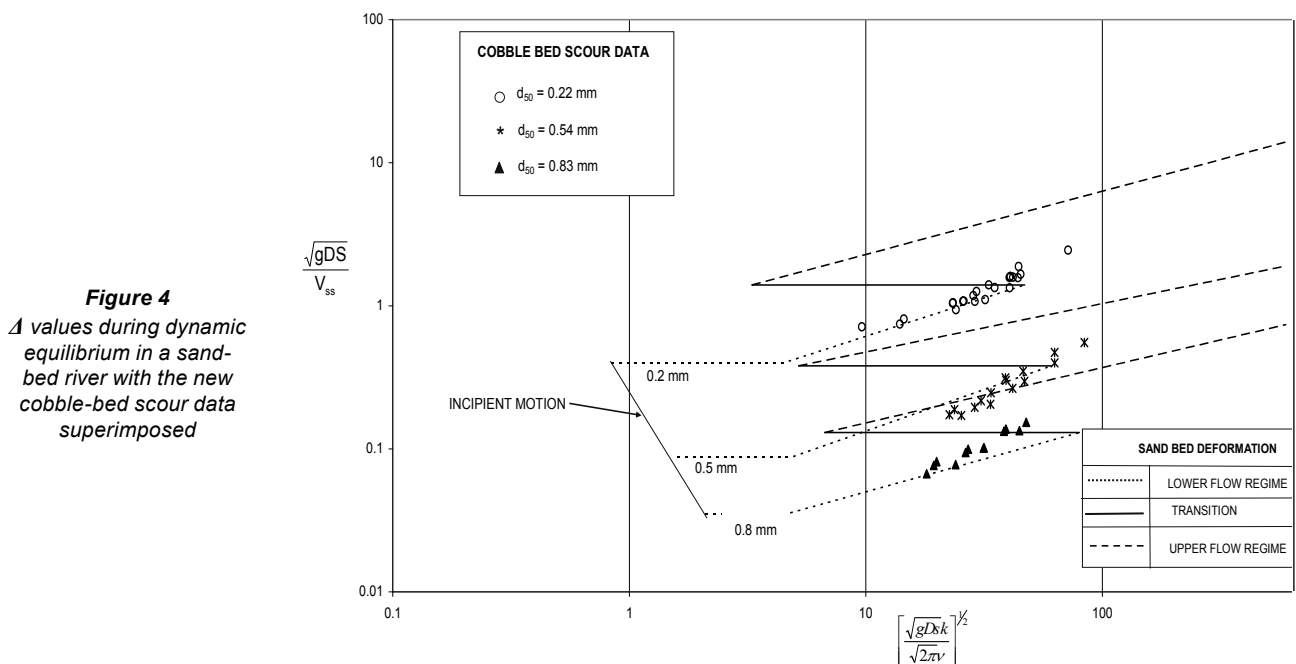


Figure 4
 Δ values during dynamic equilibrium in a sand-bed river with the new cobble-bed scour data superimposed

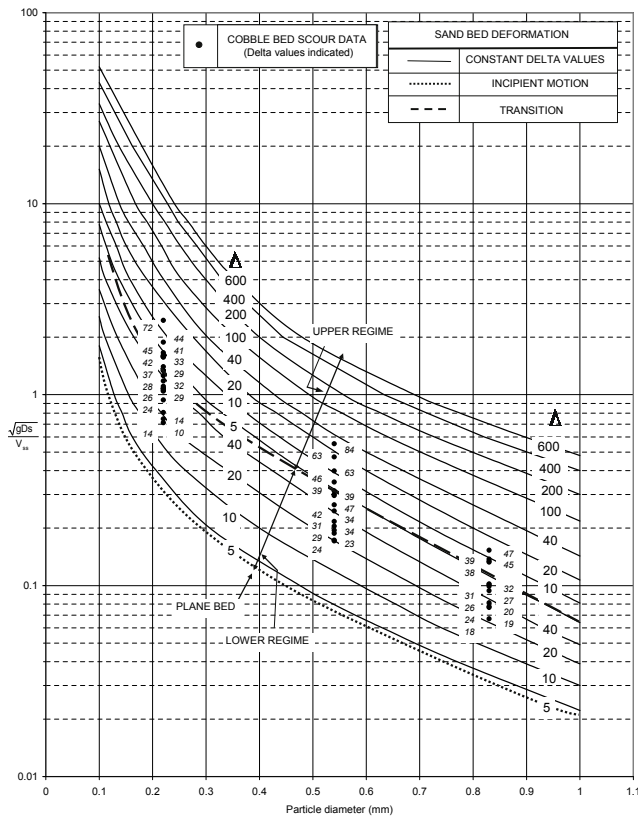


Figure 5
 Δ values and bed-forms in a sand-bed river with the new
 cobble-bed scour data superimposed

bed river. However, unlike in the case of a sand-bed river where there is a significant reduction in the magnitudes of the Δ -values at this point of transition, the cobble-bed Δ -values show a consistent increase above the 'sand-bed' transition line. This implies that the recorded Δ -values can be extrapolated according to the pattern for sand-bed rivers in order to calculate the discharges required to scour sand from cobble beds down to certain maximum depths.

Conclusions and recommendations

With the aid of physical model experiments and based on a stream power model which defines the condition of dynamic equilibrium in a deformed sand-bed river, a scour model has been developed to predict the maximum depth of scour of fine sands in a cobble-bed river. In essence, the model defines distinct relationships between absolute bed roughness or maximum scour depth, represented by $\left[\frac{\sqrt{gDs} k}{\sqrt{2\pi v}}\right]^2$ or Δ , sand particle characteristics and relative applied power $\left(\frac{\sqrt{gDs}}{V_{ss}}\right)$. The maximum scour depth is the level below the top of the cobbles at which no further scour is observed and is based on average conditions within a cobble-bed area.

The physical model experiments which were used to calibrate the cobble-bed sand scour model were conducted under clear water conditions as the artificial flushing of sediments in practice is likely to be with clear water releases from dams. However, the sand-bed deformation model on which the cobble-bed scour model is based, defines equilibrium under steady state sediment transport conditions. The fact that the relationship between Δ , sand particle characteristics and relative applied power $\left(\frac{\sqrt{gDs}}{V_{ss}}\right)$ for both of these models is similar, may be ascribed

to the fundamental principle on which both models is based. This principle, as described by Eq. (13), states that at the point of dynamic equilibrium in a deformed sand-bed river – or at the point of maximum sand scour in a cobble-bed river – critical conditions for sediment movement prevail at and below an interface between a thin laminar boundary layer along the bed and turbulent eddies above.

The experimental results suggest that, for a specific sand particle diameter, the size of the boundary eddies at critical sediment transport conditions, which reflects the power being applied at the bed and eventually determines maximum scour depth, is not affected by the cobble diameter. It rather seems that the size of the boundary eddies is primarily a function of the absolute scour depth or absolute roughness relative to the top of the exposed cobbles. This implies that the laboratory results may be extrapolated to represent larger scour depths associated with larger cobbles.

It was found that the Δ -values typically range from about 10 to 80 for the range of cobble and sand particle diameters that were tested. Larger cobbles would allow larger scour depths and higher Δ -values at higher values of $\frac{\sqrt{gDs}}{V_{ss}}$ as is confirmed by Fig. 4, which displays an almost linear increase in the value of delta with increasing values of $\frac{\sqrt{gDs}}{V_{ss}}$.

It is recommended that further research concentrate on the verification of the cobble-bed sand scour model under field conditions and specifically on how to accommodate the impact of non-uniform cobble sizes. Furthermore, the effect of steady state sediment transport on the calibrated Δ -values needs to be investigated. Finally, the relationship between discharge, sand particle characteristics and the rate of sand scour needs to be determined in order that not only the magnitude but also the duration of the flushing flow may be quantified, both of which are critical for developing the theoretical model into a practical applied methodology.

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