

Continuous non-equilibrium transition driven by the heat flow

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We discovered an out-of-equilibrium transition in the ideal gas between two walls, divided by an inner, adiabatic, movable wall. The system is driven out-of-equilibrium by supplying energy directly into the volume of the gas. At critical heat flux, we have found a continuous transition to the state with a low-density, hot gas on one side of the movable wall and a dense, cold gas on the other side. Molecular dynamic simulations of the soft-sphere fluid confirm the existence of the transition in the interacting system. We introduce a stationary state Helmholtz-like function whose minimum determines the stable positions of the internal wall. This transition can be used as a paradigm of transitions in stationary states and the Helmholtz-like function as a paradigm of the thermodynamic description of these states.

Non-equilibrium thermodynamics [1–5] have never reached the same status as equilibrium thermodynamics [6]. Despite many decades of study, the question concerning the existence of universal extremal principles that determine behaviour of non-equilibrium systems is still open. The most prominent propositions are the maximum/minimum entropy production principles [7–9]. There are attempts to provide theoretical justifications of the maximum entropy production principle based on information theory [10, 11] or least action principle [12]. However, applicability of both principles is widely discussed [11, 13–16] and the lack of their predictive success is acknowledged.

Equilibrium thermodynamics provides a clear definition of a few macroscopic variables defining the equilibrium state and function, which has a minimum at this state. For example, the state of a one-component system interacting with the environment via isothermal walls is defined by three parameters T -temperature, V -volume, and N -number of particles. The state's function, the Helmholtz free energy, $F(T, V, N)$, is minimized in the equilibrium state. The minimization is over potential states obtained at constant T, V, N via internal constraints. The present paper introduces a methodology of non-equilibrium thermodynamics having a similar structure as the equilibrium counterpart. We use this methodology to analyze the continuous transition between two non-equilibrium stationary states that we discovered in a paradigmatic heat flow model.

In a series of our recent papers [17–19], we have analyzed one-component systems subjected to the constant heat flow. In the system's stationary state, its internal energy is a function of T, L, N , and the heat flux, J . Here T is the temperature at the boundary, where the heat flux leaves the system; L is the size of the system, and N is the number of particles. This observation suggests that

the thermodynamic parameters describing the stationary state of such a non-equilibrium steady state are similar to those describing its equilibrium counterpart. A new thermodynamic parameter characterizing the state is the heat flux, J .

Here, we study an ideal gas between two parallel walls at fixed temperature T separated by the distance L . The energy flows into the system's volume in the form of heat, and the energy supplied into the system per unit time and unit volume is $\lambda = J/V$. Such an energy supply can be realized by microwaves in an appropriate designed experimental setup. A schematic plot of the system is shown in Fig. 1. The internal energy in the steady state U has the following form:

$$U = U_{eq}f(\lambda L^2/kT), \quad (1)$$

where k is the thermal conductivity and U_{eq} is the energy of the same system in the absence of external energy supply. We introduce a movable adiabatic wall parallel to the bounding walls. At equilibrium, the wall is located precisely in the middle of the system. For small heat fluxes, the position of the wall is stable. Above a critical flux, the wall moves towards one of the bounding surfaces. We show that the minimum of the non-equilibrium Helmholtz-like free energy, defined in this paper, determines the stationary state's wall position. Unlike in the existing approaches, see e.g. Refs [20, 21], our construction of a non-equilibrium free-energy-like potential does not rely on the knowledge of entropy.

As shown in Fig. 1, the left and right boundaries are fixed at $x = \pm L$, with a large area $A \rightarrow \infty$, giving $V = 2AL$. A movable wall is adiabatic, i.e., does not allow heat to pass it, and constitutes the internal constraint. Thus the system is separated into two subsystems 1 and 2, each with a fixed number of particles N_1 and N_2 . In the following, we will denote variables of the subsystem $i = 1, 2$ with subscript $-i$, and the subsystem on the left(right) hand side is designated 1(2). The wall is assumed to move freely without friction. Therefore, the condition for the total system to reach steady state is that the pressures exerted by each subsystems

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are equal $P_1(x_w) = P_2(x_w)$, where x_w is the position of the wall. In equilibrium, according to the ideal gas law $P_{eq}V = Nk_B T$, where k_B is the Boltzmann constant, therefore the intended ratio of N_1/N_2 is achieved by placing wall such that N_1/N_2 is equal to the ratio of the volumes V_i . We make two assumptions about this

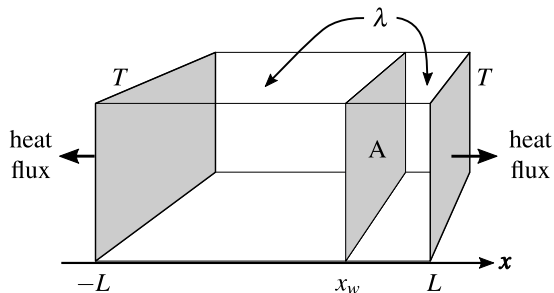


Figure 1. Schematic plot of a system with a movable wall. The vertical black lines represent the wall. The left and right boundaries have an area of A and are placed at $\pm L$. The heat flows through the boundaries. Energy is supplied through an homogeneous external energy input of density λ . The external walls are kept at temperature T .

system. First, we assume that the heat conduction follows Fourier's law. Then, the temperature profile can be obtained from the local continuity equation of energy

$$-k\nabla^2 T(\vec{r}) = \lambda, \quad (2)$$

Second, assuming local equilibrium and the equation of state for monoatomic ideal gas can be extended to be valid locally so that in non-equilibrium steady states

$$P = n(\mathbf{r})k_B T(\mathbf{r}) \quad \epsilon = \frac{3}{2}n(\mathbf{r})k_B T(\mathbf{r}) = \frac{U}{V}, \quad (3)$$

where $n(\mathbf{r})$ is the local particle number density at position \mathbf{r} , with $\int_V n(\mathbf{r})d^3r = N$; $T(\mathbf{r})$ is the local temperature at \mathbf{r} ; ϵ is the energy density. In the above two relations, both P and ϵ are constant across the system. This is because the redistribution of mechanical energy occurs much faster than the redistribution of heat. From the above two assumptions, the steady state energy density of the system and of each subsystem can be obtained using

$$\epsilon = \frac{3}{2}Nk_B \frac{1}{\int_V \frac{d\vec{r}}{T(\vec{r})}} \quad \epsilon_i = \frac{3}{2}N_i k_B \frac{1}{\int_{V_i} \frac{d\vec{r}}{T_i(\vec{r})}}, \quad (4)$$

where the temperature profiles are obtained from Eq. (2) with the appropriate boundary conditions. As a result, the energy of the system prior to the constraint is given by Eq. (1) and the energy of the subsystem of N_i particles under the constraint is

$$U_i = U_{i,eq} f(\lambda L_i^2/kT) = \frac{3}{2}N_i k_B T f(\lambda L_i^2/kT) \quad (5)$$

with $N_1 + N_2 = N$, where $U_{eq} = (3/2)Nk_B T$ and $U_{i,eq}$ are the system and subsystem energy in equilibrium, L_i

is the length of the subsystem with $L_1 = L + x_w$ and $L_2 = L - x_w$, and the function f is given by

$$f(x) \equiv \frac{\sqrt{x(x+2)}}{2 \operatorname{Arctanh} \sqrt{x/(x+2)}}. \quad (6)$$

The derivations are shown in the Appendix A. We would like to make two remarks. First, the variables of f is separated to λ and L_i^2/kT , where λ is the control parameter, and the coefficient L^2/kT (or L_i^2/kT for the subsystems) are parameters that are either of the intrinsic properties of the system, or of the environment that is not changed (T). Second, this model is seemingly similar to the model considered in our previous paper [17] (named there as *case 1*). In *case 1*, however, the adiabatic wall is fixed in space, and the subsystems are independent. Whereas in the movable wall model, the constraint couples the two subsystems. This single difference results in an interesting second-order non-equilibrium phase transition which we will discuss next.

For our movable wall model, the condition of non-equilibrium steady states can be equivalently stated as $P_1(x_w) = P_2(x_w)$ or $\epsilon_1(x_w) = \epsilon_2(x_w)$. The solutions $x_w^{(i)}$ (where the superscript $-(i)$ indicates the i th solution) are obtained numerically. Graphically, the solutions and their corresponding stability can be observed at and around the zeros of $P_1(x_w) - P_2(x_w)$. We set $N_1 = N_2 = N/2$ and observe that as λ increases (at fixed T , V and N), the system undergoes a second-order non-equilibrium phase transition. The order parameter is the stable position of the wall x_w . For small λ , we find a stable steady state at $x_w = 0$. As this division gives identical subsystems, $P_1 = P_2$ trivially. An example is shown in Fig. 2(a) (dashed curve). One can see that the curve $P_1(x_w) - P_2(x_w)$ is monotonic and exhibit a single zero-crossing point at $x_w = 0$. To evaluate the stability, suppose now that the constraint is pushed away from the center towards $x_w > 0$. One observes that $P_1 - P_2 < 0$. Consequently, the pressure difference will push the wall back towards $x_w = 0$. Therefore, $x_w = 0$ is a stable solution in this phase. For large λ , interestingly, the system has three steady states. They correspond to the position of the wall at $x_w = 0$ and at $x_w = -x_w \neq 0$ due to symmetry. Qualitatively, one can imagine the asymmetric case where, according to Eq. (3), the smaller average number of particle density $\bar{n}_i \equiv N_i/V_i$ for the larger subsystem is compensated with a higher overall temperature, whereas larger \bar{n}_i in the smaller system is compensated with a lower overall temperature. This compensation can occur because the heat flux of the movable wall model is proportional to the volume V_i (inverse proportional to \bar{n}_i). An example of three solutions is shown in Fig. 2(a) (zeros of the red curve). Among these 3 solutions, further analysis show that $x_w^{(2)}$ (and $x_w^{(3)}$) are stable, whereas $x_w^{(1)}$ is unstable. As we can see from Fig. 2(a), the red curve is no longer monotonic and exhibits zero-crossing at 3 points. Suppose now that the constraint is pushed away from the steady state, in one case to the position

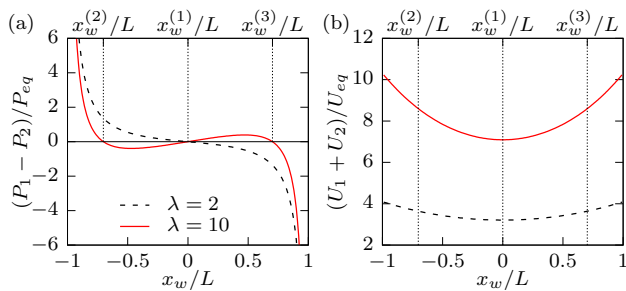


Figure 2. System's response as a function of x_w for two values of λ . (a) The difference between pressures in compartments normalized with equilibrium pressure $P_{eq} = Nk_bT/V$. (b) Total internal energy of the system normalized with U_{eq} . The vertical lines mark the position of the steady states $x_w^{(1)}$ for $\lambda = 2$ and $x_w^{(1)}, x_w^{(2)}$ and $x_w^{(3)}$ for $\lambda = 10$. λ is in units of kT/L^2

between $x_w^{(1)}$ and $x_w^{(2)}$, and in the other case beyond $x_w^{(2)}$. In both situations, the pressure difference will push the constraint towards $x_w^{(2)}$. Due to symmetry, the same argument holds for $x_w^{(3)}$ when the starting point of the constraint is $x_w > 0$. Note that the total energy of the system $U_1 + U_2$ has minimum always at $x_w = 0$ - see Fig. 2(b).

Diagram showing the position of stationary states in the parameter space $x_w - \lambda$ space (at fixed T, V, N) is presented in Fig. 3 (a). One can see that upon increasing λ the transition from one steady state to another is continuous. The transition point occurs at $\lambda_c L^2/kT \approx 4.55344$ (see Appendix B). The steady state energy of the total system $U = U_1 + U_2$ is plotted in Fig. 3(b). Interestingly, the energy of the stable steady states is higher than the unstable steady state. The same is valid for the total entropy production rate $\dot{S}_{tot} = A \int_{-L}^L \sigma_s(x) dx$, where $\sigma_s = k (\partial T(x)/\partial x)^2 / (T(x))^2$ - see Fig. 4. In Fig. 5 we demonstrate that the transition cannot be predicted from the extremum of the total entropy production rate as a function of x_w . \dot{S}_{tot} has a single minimum at $x_w = 0$ for the values of λ above the transition. The two minima occur at some λ^* , which is much larger than λ_c , but the positions of these minima do not correspond to the stable positions of a movable wall. Above λ_c , the temperature and number density profiles develop discontinuity at the movable wall as shown in Fig. 6.

This phase transition diagram is also retrieved, and the energy storage as a function of the mean rate of energy added per particle λ_p (see Fig.3(c) and (d)) is obtained using molecular dynamics simulations [22] of the soft-sphere fluid where no assumptions concerning local equilibrium or constancy of heat conductivity are made. Simulations are performed for fixed $N = 153600$ particles enclosed in the rectangular box of a size $L_x = L_y = 275.8\sigma, L_x \equiv 2L = 658.3\sigma$, where the molecular size unit σ is set to 1, with periodic boundary conditions applied along y and z axis. The energy flux is proportional to the density *i.e.*, the same amount of energy is added to

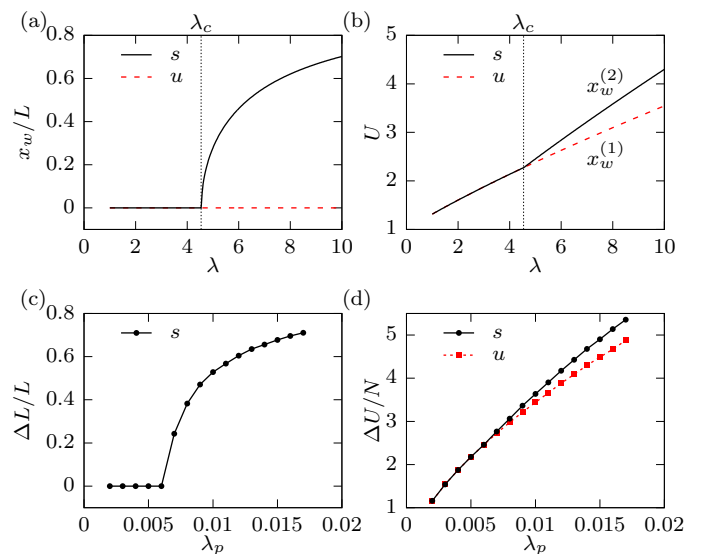


Figure 3. (a) Diagram showing the location of the stationary states in the parameter space (x_w, λ) . Stable (s) and unstable (u) stationary states are indicated in black (red); (b) Energy of the total system U (in units of U_{eq}) as a function of the flux per unit volume λ (in units of kT/L^2). (c) and (d) show molecular dynamic simulations results for the soft-sphere fluid: (c) the relative shift of the wall $\Delta L/L = |\langle x_w \rangle|$ as a function of λ_p - the mean rate of energy added per particle. $\langle x_w \rangle$ is the mean value of x_w at the end of the simulation run. (d) $\Delta U/N$ - the deviation of energy per particle (in units of the amplitude ε of the interaction potential) from its initial value established before the shift of the wall (black circles) and after the shift (red squares) as a function λ_p .

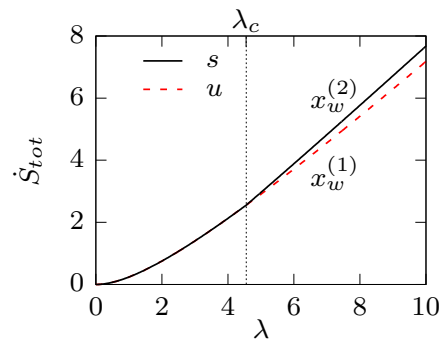


Figure 4. Total entropy production rate \dot{S}_{tot} (in units of kV/L^2) as a function of the flux per unit volume λ (in units of kT/L^2). Stable (s) and unstable (u) stationary states are indicated in black (red).

the same volume and equally shared between all particles in that volume (for more details of simulations see Appendix C).

For a system with a volume V and a fixed number of particles N in contact with a heat bath at temperature T and driven out-of-equilibrium by external control parameter λ , we propose a non-equilibrium state function B that is minimized for stable steady states, and pro-

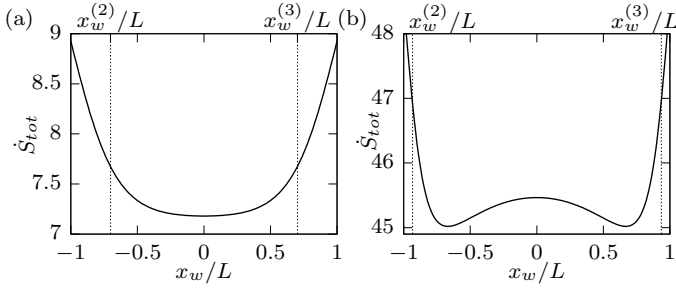


Figure 5. Total entropy production rate \dot{S}_{tot} (in units of kV/L^2) for (a) $\lambda = 10$ and (b) $\lambda = 50$. The vertical lines mark the position of the steady states, which differ from the positions of the extremes of \dot{S}_{tot} . λ is in units of kT/L^2

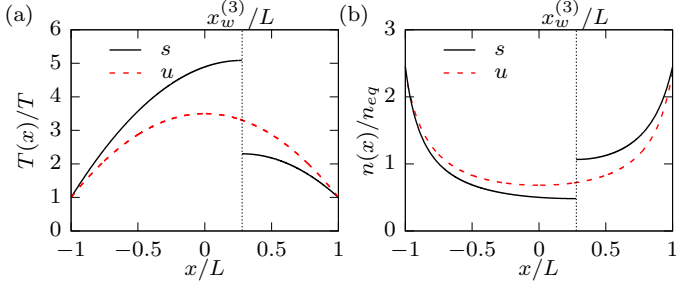


Figure 6. (a) Temperature $T(x)$ (in units of T) and (b) number density $n(x)$ (in units of $n_{eq} = N/V$) profiles for $\lambda = 5.0$, slightly above the transition point. The stable position of the wall $-x_w^{(2)} = x_w^{(3)} = 0.278564$ is marked by vertical lines. Stable (s) and unstable (u) stationary states are indicated in black (red).

vide its expression. We will demonstrate the use of this potential using the movable wall model, and show that it predicts the correct stable steady states. The development of the non-equilibrium state function is based on the assumption that the relevant parameters are the thermodynamic variables T, V, N , and the parameter λ that accounts for the non-equilibrium. In the limiting case $\lambda \rightarrow 0$, this state function should agree with the equilibrium free energy $\lim_{\lambda \rightarrow 0} B(T, V, N, \lambda) = F_{eq}(T, V, N)$, which is the correct state function of an equilibrium system. Moreover, in analogy to the equilibrium free energy, we postulate that B satisfies

$$dB = -SdT - PdV + \mu dN - Xd\lambda \quad (7)$$

where $P(T, V, N, \lambda)$, $S(T, V, N, \lambda)$, $\mu(T, V, N, \lambda)$ and $X(T, V, N, \lambda)$ are state functions conjugate to V, T, N and λ , respectively. Equation (7) defines the steady state pressure P , the steady state entropy S and the steady state chemical potential μ , which should retrieve its equilibrium values as $\lambda \rightarrow 0$; X is the new variable purely due to non-equilibrium, which has no equilibrium counterpart. Note that the first three terms are analogous to the differential form of the equilibrium free energy $dF_{eq} = -S_{eq}dT - P_{eq}dV + \mu_{eq}dN$. Finally, we postu-

late that X is of the form of

$$X \propto \left(\frac{U - U_{eq}}{\lambda} \right). \quad (8)$$

This is inspired by our earlier observations [17–19] that for several seemingly different systems, a quantity $\mathcal{T} = (U - U_{eq})/J_U$ is minimized for steady states, where J_U is the total heat flow. The two quantities X and \mathcal{T} are similar since λ is quantitatively the total heat flow per unit volume. The proportionality constant is obtained through an argument of consistency that we describe below. Now, we proceed to demonstrate the use of B in the movable wall model. Taking the energy expression (1), we have used consistency relations analogous to the Maxwell relations of equilibrium thermodynamics in order to obtain the expression for the non-equilibrium potential and the steady state functions of the unconstrained system (see Appendix D); the proportionality constant in Eq. (8) equal to $1/3$ restores the pressure correctly. We found:

$$B(T, V, N, \lambda) = F_{eq}(T, V, N) - \int_0^\lambda X(T, V, N, \lambda') d\lambda'. \quad (9)$$

$$S = \frac{Nk_B}{2} \int_0^\lambda (f(\lambda' L^2/kT) - 1) \frac{d\lambda'}{\lambda'} - \frac{Nk_B}{2} (f(\lambda L^2/kT) - 1) + S_{eq} \quad (10)$$

$$P = \frac{Nk_B T f(\lambda(L^2/kT))}{V} = \frac{3U}{2V} \quad (11)$$

$$\mu = \frac{k_B T}{2} \int_0^\lambda (f(\lambda'(L^2/kT)) - 1) \frac{d\lambda'}{\lambda'} + \mu_{eq} \quad (12)$$

Note that as $\lambda \rightarrow 0$, $f \rightarrow 1$. It is then obvious that from these four expressions we retrieve the correct corresponding equilibrium potentials in the limit of $\lambda \rightarrow 0$. From Eqs. (10), (11) and (12), we also obtain the integral form of B of the unconstrained system as

$$B = U - TS - 4X\lambda, \quad (13)$$

in consistency with Eq. (9). This form is again analogous to the equilibrium free energy expression $F_{eq} = U_{eq} - TS_{eq}$. The additional term is the conjugate pair due to non-equilibrium $X\lambda$ with a coefficient 4.

For the constrained system, the non-equilibrium potential of movable wall system is given by

$$B(T, V, N_1, N_2, x_w, \lambda) = F_{eq}(T, V, N_1, N_2, x_w) - \int_0^\lambda X(T, V, N_1, N_2, x_w, \lambda') d\lambda', \quad (14)$$

where

$$X(T, V, N_1, N_2, x_w, \lambda) = \frac{1}{3} \frac{U_1 + U_2 - U_{eq}}{\lambda}. \quad (16)$$

The extremum condition at fixed T, V, N_1, N_2 and λ reduces to the condition of matching pressure:

$$\left. \frac{\partial B}{\partial x_w} \right|_{x_w^*} = 0 \Leftrightarrow -A(P_1 - P_2) = 0, \quad (17)$$

where

$$P_1 = \frac{N_1 k_B T}{V_1} f\left(\lambda \frac{(L + x_w)^2}{kT}\right), \quad (18)$$

$$P_2 = \frac{N_2 k_B T}{V_2} f\left(\lambda \frac{(L - x_w)^2}{kT}\right). \quad (19)$$

Thus, we have demonstrated that the extremum points correctly predict the steady states in the movable wall model. Further, analysis shows that $x_w^* = 0$ corresponds to a local maximum and $x_w^* \neq 0$ local minimum (see Appendix E).

In conclusion, for the movable wall case, we have retrieved the 3 steady states as the extremum of B , and the minimum of B predict correctly the stable steady state. In a general case of $N_1 \neq N_2$ the system still exhibits a second order phase transition under certain circumstances. The behaviour is more complex as it involves an additional variable and needs further study. The mov-

able wall model studied here analytically exhibits second-order non-equilibrium phase transition. The transitions in out-of-equilibrium states that can be fully characterized by analytical calculations are extremely rare. Therefore the transition that we have found can be used as a paradigm of such transitions. We have provided a full thermodynamic description of the transition introducing the Helmholtz-like function for stationary states. We think that such a description analogous to ordinary thermodynamics has great potential in the description of stationary states and could push forward non-equilibrium thermodynamics.

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A. Derivation of the Energy Expression

Here, we provide a derivation of the energy of the system Eq. (1) and of subsystems Eq. (5).

As stated in the main text, the energy density satisfies Eq. (3). By moving the temperature profile to the left hand side (as $T(\vec{r}) > 0$) and integrate over the whole volume, the dependence over the particle density profile $n(\vec{r})$ is eliminated,

$$\epsilon \int_V \frac{d^3\vec{r}}{T(\vec{r})} = \frac{3}{2}k_B \int_V d^3\vec{r}n(\vec{r}) = \frac{3}{2}Nk_B. \quad (\text{A1})$$

From this relation, an expression of the energy density can be obtained,

$$\epsilon = \frac{3}{2}Nk_B \frac{1}{\int_V \frac{d^3\vec{r}}{T(\vec{r})}}. \quad (\text{A2})$$

Analogously, the energy density of the subsystem is

$$\epsilon_i = \frac{3}{2}N_i k_B \frac{1}{\int_{V_i} \frac{d^3\vec{r}}{T_i(\vec{r})}}. \quad (\text{A3})$$

The temperature profile is obtained from Eq. (2) with the appropriate boundary conditions. Since the movable wall model is assumed to be infinite in y and z directions, it is sufficient to consider the dependence in x direction, so one has

$$-k \frac{\partial^2}{\partial x^2} T(x) = \lambda. \quad (\text{A4})$$

The boundary conditions prior to the constraint are $T(\pm L) = T_0$, giving

$$T(x) = -\frac{\lambda}{2k}x^2 + \frac{\lambda}{2k}L^2 + T_0, \quad (\text{A5})$$

The additional boundary conditions under the constraint is $\partial_x T_i(x_i) = 0$, giving

$$T_i(x) = -\frac{\lambda}{2k}(x - x_w)^2 + \frac{\lambda}{2k}(L - x_w)^2 + T_0. \quad (\text{A6})$$

Inserting Eq. (A5) into Eq. (A2), and Eq. (A6) into Eq. (A3), the final expressions of energy are obtained,

$$U = U_{eq} f\left(\lambda \cdot \frac{L^2}{kT}\right) = \frac{3}{2}Nk_B T f\left(\lambda \cdot \frac{L^2}{kT}\right), \quad (\text{A7})$$

$$U_i = U_{i,eq} f\left(\lambda \cdot \frac{L_i^2}{kT}\right) = \frac{3}{2}N_i k_B T f\left(\lambda \cdot \frac{L_i^2}{kT}\right). \quad (\text{A8})$$

where $L_1 = L + x_w$, $L_2 = L - x_w$ and $f(x) \equiv \sqrt{x(x+2)}/(2 \text{Arctanh} \sqrt{x/(x+2)})$, as in Eqs. (1) and Eq. (5).

B. Derivation of the phase transition point $\lambda_c L^2/kT$

Here we provide a derivation of the transition point $\lambda_c L^2/kT$ of the movable wall model with $N_1 = N_2 = N/2$, where it is stated that $\lambda_c L^2/kT \approx 4.55344$.

We start by rewriting Eq. (A8) using the normalised variables $\tilde{\lambda} \equiv \lambda L^2/kT$ and $x_w = x_w/L$, and let $N_i = N/2$. Next, a new function is defined as the negative difference between energy densities,

$$G(x_w) \equiv -(\epsilon_1 - \epsilon_2) \equiv -\frac{3Nk_B T}{2V}(g(x_w) - g(-x_w)), \quad (\text{B1})$$

$$g(x_w) = \frac{f\left(\tilde{\lambda}(1+x_w)^2\right)}{1+x_w}. \quad (\text{B2})$$

The negativity of $G(x_w)$ is not necessary, but it is chosen here so that it would simplify the explanation in a later section. Since the function is odd with respect to x_w , it is sufficient to look at half of the axis, say $x_w \in [0, 1]$.

Consider the range $x_w \geq 0$. For this movable wall model with equal subsystem particles, the phase transition occurs when the number of solutions transit from 1 to 2. Equivalently, this means that the number of times $\epsilon_1(x_w)$ crosses with $\epsilon_2(x_w)$ in $x_w \geq 0$ transit from 1 to 2, which is then equivalently the crossings of $G(x)$ with the x -axis.

More precisely, in the range $x_w \geq [0, 1]$, $G(0) = 0$ is fixed and $\lim_{x \rightarrow 1} G(x) \rightarrow \infty$. Therefore, when $G'(0) > 0$, $G(x)$ is monotonic and have only one crossing point at $x = 0$; when $G'(0) < 0$, $G(x)$ will have 2 crossing points; the transition point is $G'(0) = 0 = -2g'(0)$. Explicitly,

$$\left. \frac{dg}{dx} \right|_{x=0} = \frac{1}{2+\tilde{\lambda}} - \frac{\tilde{\lambda}^2 \text{Arctanh}(\sqrt{\tilde{\lambda}/(\tilde{\lambda}+2)})}{(\tilde{\lambda}(\tilde{\lambda}+2))^{3/2}} = 0. \quad (\text{B3})$$

Solving this implicit equation numerically, the solution is $\tilde{\lambda}_c = \lambda_c L^2/kT \approx 4.55344$.

C. Molecular dynamics simulation

The simulations are performed using molecular dynamics method [22] for systems of $N = 153600$ particles of mass $m = 1$ enclosed in the rectangular box and interacting via the following potential:

$$V_{rep}(r) = \epsilon \left(\frac{\sigma}{r}\right)^{12} \quad (\text{C1})$$

where r is the interparticle distance and both the energy, ϵ , and the size, σ , parameter are set to one. The equations of motion are solved applying the Verlet method [22] for the time step $\delta t = 0.0025\sigma(m/\epsilon)^{1/2}$. The gas of particles is enclosed in the rectangular box of the edges: $L_z = L_y = 275.8$, $L_x \equiv 2L = 658.3$. The periodic boundary conditions were applied only along z and y

axis. The x -th direction was restricted by two walls that repulse the particles with the potentials: $V_{rep}(-L - x)$ and $V_{rep}(L - x)$, where $-L \leq x \leq L$. The movable wall of the mass $M = 32m$ is perpendicular to x -th axis and interacts with the surrounding particles with the potential:

$$V_w(x) = \begin{cases} V_{rep}(x_w + 1 - x), & \text{for } x \leq x_w - 1 \\ V_{rep}(x - x_w - 1), & \text{for } x \geq x_w + 1 \\ \infty, & \text{for } x_w - 1 \leq x \leq x_w + 1 \end{cases} \quad (\text{C2})$$

where x_w denotes the position of the wall. At the beginning of each simulation run $x_w = 0$ and the particles are equally distributed between the two parts.

Energy is added to the system once per time interval $0.1\sigma(m/\varepsilon)^{1/2}$ and removed from the system by keeping the boundary temperature T_0 constant ($= 0.5$) by applying Brownian simulations [22]. The Verlet scheme is completed with the stochastic term [23] for $x < -L + x_T$ and $x > L - x_T$ where $x_T = 3.0$. The system for $-L + x_T < x < L - x_T$ is imaginary divided into 20 equal size layers perpendicular to the x -th axis. The energy flux is proportional to the density [17] *i.e.*, the same amount of energy is added to the same volume (here, the layer) and equally shared between all particles in the layer. As the initial state for all simulation runs we adopted the system at the equilibrium state at the temperature $T = T_0 = 0.5$.

D. Derivation of the steady-state functions for the movable wall model

Using the movable wall model, in particular Eq. (1) and Eq. (5), we provide the derivation of the expressions for B , S , P and μ (Eqs. (9)-(12) , respectively). This is done by using consistency relations, which are analogs of Maxwell relations in equilibrium thermodynamics. Further, we derive the integration form of B (Eq. (13)).

In analogy to the Maxwell relations of equilibrium thermodynamics, in order for the proposed 3 postulates concerning state function B (described in the main text) to be valid, the following 6 relations of mixed derivatives must be satisfied,

$$\frac{\partial^2 B}{\partial T \partial \lambda} = \frac{\partial^2 B}{\partial \lambda \partial T} \Leftrightarrow \frac{\partial S}{\partial \lambda} = \frac{\partial X}{\partial T}, \quad (\text{D1})$$

$$\frac{\partial^2 B}{\partial V \partial \lambda} = \frac{\partial^2 B}{\partial \lambda \partial V} \Leftrightarrow \frac{\partial P}{\partial \lambda} = \frac{\partial X}{\partial V}, \quad (\text{D2})$$

$$\frac{\partial^2 B}{\partial N \partial \lambda} = \frac{\partial^2 B}{\partial \lambda \partial N} \Leftrightarrow -\frac{\partial \mu}{\partial \lambda} = \frac{\partial X}{\partial N}, \quad (\text{D3})$$

$$\frac{\partial^2 B}{\partial T \partial V} = \frac{\partial^2 B}{\partial V \partial T} \Leftrightarrow \frac{\partial S}{\partial V} = \frac{\partial P}{\partial T}, \quad (\text{D4})$$

$$\frac{\partial^2 B}{\partial T \partial N} = \frac{\partial^2 B}{\partial N \partial T} \Leftrightarrow -\frac{\partial S}{\partial N} = \frac{\partial \mu}{\partial T}, \quad (\text{D5})$$

$$\frac{\partial^2 B}{\partial V \partial N} = \frac{\partial^2 B}{\partial N \partial V} \Leftrightarrow -\frac{\partial P}{\partial N} = \frac{\partial \mu}{\partial V}. \quad (\text{D6})$$

From Eq. (D1), the steady state expression of entropy S can be obtained from

$$\begin{aligned} S(T, V, N, \lambda) &= \int_0^\lambda \frac{\partial X}{\partial T} d\lambda' + S_{eq}(T, V, N) \\ &= \frac{Nk_B}{2} \int_0^\lambda \frac{f(\lambda \frac{L^2}{kT}) - 1}{\lambda} d\lambda \\ &\quad - \frac{Nk_B}{2} (f(\lambda \frac{L^2}{kT}) - 1) + S_{eq}(T, V, N), \end{aligned} \quad (\text{D7})$$

which is Eq. (10). Further, from postulate Eq. (7) that $\partial B / \partial T \equiv -S$, B is given by

$$\begin{aligned} B(T, V, N, \lambda) - B(T_{ref}, V, N, \lambda) &= - \int_{T_{ref}}^T S dT' \\ &= - \int_{T_{ref}}^T dT' \left(\int_0^\lambda \frac{\partial X}{\partial T'} d\lambda' + S_{eq}(T', V, N) \right), \end{aligned} \quad (\text{D8})$$

Changing the order of integration, the above expression becomes

$$\begin{aligned} B(T, V, N, \lambda) - B(T_{ref}, V, N, \lambda) &= F_{eq}(T, V, N) - F_{eq}(T_{ref}, V, N) \\ &\quad - \int_0^\lambda X(T, V, N, \lambda') d\lambda' + \int_0^\lambda X(T_{ref}, V, N, \lambda') d\lambda', \end{aligned} \quad (\text{D9})$$

Thus, we conclude:

$$B(T, V, N, \lambda) = F_{eq}(T, V, N) - \int_0^\lambda X d\lambda'. \quad (\text{D10})$$

Next, from Eq. (D2), we obtain P

$$P = \int_0^\lambda \frac{\partial X}{\partial V} d\lambda' + P_{eq}(T, V, N) = \frac{Nk_B T}{V} f(\lambda \frac{L^2}{kT}). \quad (\text{D11})$$

as given by Eq. (11). This expression is consistent with the ideal gas law where $P = 3U/2V$, and with the definition from $P \equiv -\partial B / \partial V$ where B is given by Eq. (D10).

Thirdly, from relation Eq. (D3), we obtain μ

$$\begin{aligned} \mu(T, V, N, \lambda) &= - \int_0^\lambda \frac{\partial X}{\partial N} d\lambda' + \mu_{eq}(T, V, N), \\ &= \frac{k_B T}{2} \int_0^\lambda \frac{f(\lambda \frac{L^2}{kT}) - 1}{\lambda} d\lambda + \mu_{eq}(T, V, N) \end{aligned} \quad (\text{D12})$$

as shown in Eq. (12). Similarly, this expression is consistent with the definition $\mu \equiv \partial B / \partial N$.

Now, we consider the rest of the relations, *i.e.*, Eqs. (D4, D5, D6). Using the above expressions of the

state functions, and obtain

$$\frac{\partial S}{\partial V} = \frac{\partial P}{\partial T} = \frac{Nk_B f}{V} - \frac{Nk_B \lambda L^2}{V} \frac{df}{kT dy}, \quad (\text{D13})$$

$$-\frac{\partial S}{\partial N} = \frac{\partial \mu}{\partial T} = -\frac{k_B}{2} \int_0^\lambda \frac{f-1}{\lambda'} d\lambda' + \frac{k_B}{2} (f-1) + \frac{\partial \mu_{eq}}{\partial T}, \quad (\text{D14})$$

$$-\frac{\partial P}{\partial N} = \frac{\partial \mu}{\partial V} = -\frac{k_B T}{V} f, \quad (\text{D15})$$

where $y = \lambda L^2/kT$, and we have used the equilibrium relation $\partial S_{eq}/\partial N = -\partial \mu_{eq}/\partial T$.

Finally, using postulate Eq. (8) and the above obtained Eqs. (D7, D11, D12), the integration form of B can be written as

$$B = U - TS - 4X\lambda, \quad (\text{D16})$$

which is Eq. (13), in order to be consistent with Eq. (D10).

E. Analysis of the extrema of B

Here we check the properties of the extrema of B of the movable wall model with $N_1 = N_2 = N/2$. Equivalently,

it is to check the second order derivative $\partial^2 B/\partial x_w^2$ at extrema x_w^* , which are solutions to $\partial B/\partial x_w = 0$. In other words, x_w^* are local maxima if $(\partial^2 B/\partial x_w^2)(x_w^*) < 0$, and local minima if $(\partial^2 B/\partial x_w^2)(x_w^*) > 0$.

Using $G(x_w)$ in Eq. (B1), the comparison between the second derivative of B and 0 simplifies to comparison between $-\frac{\partial}{\partial x_w} \left(\frac{f(\tilde{\lambda}(1+x_w)^2)}{1+x_w} - \frac{f(\tilde{\lambda}(1+x_w)^2)}{1-x_w} \right) \Big|_{x_w^*}$ and

0 or, equivalently, between $G'(x_w) \Big|_{x_w^*}$ and 0. As shown earlier, beyond the transition point we have $G'(0) < 0$, suggesting that $x_w^* = 0$ corresponds to a local maximum. Moreover, since $G(1) > G(0)$, the derivative at the crossing point $x_w^* > 0$ must be positive, $G(x_w^* > 0) > 0$, suggesting that this solution is a local minimum. Finally, since $G(x)$ is an odd function, $G'(-x_w) = G'(x_w)$ and the crossing point $x_w^* < 0$ is also a local minimum. The above discussion shows that $x_w^* = 0$ is the local maximum and $x_w^* \neq 0$ are local minima.