

Volatile Liquid Detection by Terahertz Technologies

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12 **Abstract**

13 The prospect of being able to move through security without the inconvenience of separating liquids
14 from bags is an exciting one for passengers, and there are important operational benefits for airports as
15 well. Here, two terahertz (THz) systems, 100 GHz sub-THz line scanner and attenuation total
16 reflection-based THz time domain spectroscopy (TDS), have been used to demonstrate the capability
17 of identifying different liquid samples. Liquid samples' THz complex permittivities are measured and
18 their differences have contributed to the variation of 100 GHz 2D images of volatile liquids with
19 different volumes inside of canister bottles. The acquired attenuation images at 100 GHz can easily
20 be used to distinguish highly absorbed liquids (Water, Ethanol, Fuel Treatment Chemicals) and low
21 loss liquids (Petrol, Diesel, Kerosene and Universal Bottle Cleaner). The results give a promising
22 feasibility for mm-wave imager and THz spectroscopy to efficiently identify different volatile liquids.

23 **1 Introduction**

24 In 2019, security restrictions at airports for carry-on luggage have eased significantly since the
25 turbulent response to the 2006 liquid explosives plot. However, one major regulation has endured at
26 most international airports around the world – the requirement that liquids be kept in 100ml bottles and
27 transferred from baggage into clear plastic bags before being scanned through security [1]. X-ray
28 imaging-based apparatus provides a major tool in checked baggage inspection, as it can detect the form
29 and density of items within luggage as well as other material dependent parameters. Recently,
30 conventional medical computed tomography (CT) scans have been developed and introduced to some
31 European airports, where 3D images of items are computing-processed to combine hundreds of
32 individual X-ray measurements from different angles [2-3]. The technology offers more detailed and
33 comprehensive image quality; however, it was not able to highlight whether a substance was a solid or
34 a liquid. This limited its ability to flag potentially explosive substances and required much more
35 intervention and analysis from members of staff, which made potentially dangerous substances prone
36 to oversight and human error. The reason this happens is because normal liquids we drink all have
37 densities in the range of around 1.0 g/cc and the average atomic number is similar to the ranges of those

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38 major explosives. This is why the airport security system does not allow passengers to carry liquids
39 into an airport checkpoint because they could generate false alarms and slow down the lines.

40
41 Because of the limitations of the original x-ray CT, x-ray diffraction, specifically, energy dispersive x-
42 ray diffraction (EDXRD) [4-5] has now been implemented for performing security checks on luggage
43 and cargo. It is an incredibly powerful non-invasive technique that reports various information
44 regarding the crystalline structure of samples being scanned. This allows it to detect specific materials,
45 as well as identify between solid and liquid substances. It works by incident x-ray beams that interact
46 with the photon matter of the sample materials. Where the beam hits the sample, an electron in an inner
47 shell becomes excited, resulting in its ejection, creating an electron-hole in the electronic structure of
48 the element. This hole is then filled by an electron from a higher energy shell, which expels the
49 difference of energy between the two shells as x-rays which then is picked up the detector. The amount
50 of energy released as x-rays, is unique for different elements, allowing the method to provide
51 information on the elements and substances present within the sample being scanned. Elements and
52 compounds used in explosives can be effectively detected automatically, with minimal need for human
53 intervention. Additionally, the technique can easily detect liquids due to the specific spectra produced
54 by materials in their different forms. Despite this important capability, EDXRD can only cover small,
55 thin areas, making it inefficient as a primary large area screening mechanism. By adding more detectors
56 into the spiral setup, the detection depth could be increased to cover the average luggage size [6].

57
58 Making use of X-ray diffraction measurements, however, is a tricky technical problem. To begin with,
59 the diffracted signal is several orders of magnitude weaker than the transmitted signal. So, it's harder
60 to measure them at all. It's also much harder to interpret. As a result, even though fingerprinting (more
61 properly called X-ray diffraction tomography) would be pretty promising in identifying threats, the
62 complexity of items in practice has required a more robust and straightforward method to achieve
63 aviation security, precise screening and an acceptable passenger experience. The bulk size and cost of
64 EDXRD are another concern and impediment to widely use the technology.

65
66 Millimeter(mm)-waves and Terahertz (THz) radiation, are defined to span frequencies of 30 to 10,000
67 GHz (10mm to 30 μ m in wavelength) [7], afford remarkable natural advantages of electromagnetic
68 waves, which are intrinsically safe, non-ionizing and non-destructive, transparent to majority of
69 packaging materials and clothes, and are also sensitive to materials' microstructural differences [8] and
70 surface properties [9]. The technology has recently been licensed to use for personal security screening
71 at many European and American airports. Whilst identifying contraband items in an airport, for
72 example weapons or firearms, is straightforward, there are many limitations in differentiating between
73 different types of liquids and fluids [10]. As liquids are indistinguishable under most THz and X-ray-
74 based imaging, virtually no airport facilities offer a commercially used THz based imaging system,
75 specifically for determining the identity of different liquids. Due to the nature of strong water
76 absorption to THz radiations, it is an ignored research area to detect volatile liquids by THz radiations.
77 However, THz has many penetration windows in the normal ambient air conditions and also it has
78 different absorption rate to different density of matters [11-12]. A THz electromagnetic signal can also
79 detect molecular vibrations uniquely, including molecular fingerprints; meanwhile, THz spectroscopy
80 such as Time Domain Spectroscopy (TDS), as a coherent detection system, offers not only absorption
81 information of samples, but also the dielectric permittivity values to uniquely identify different samples
82 [13]. These unique properties mean that THz technology can be used for liquid screening. This paper
83 aims to detect and identify different liquid samples via various THz methods. The first method is the

84 implementation of a 100 GHz (sub-terahertz) Line Scanner to produce high resolution 2D images of
85 sample liquids. This system slides a sample liquid between a THz source and detector in order to
86 produce a plot showing the varying levels of attenuation and penetration throughout a given volume of
87 a variety of liquids. The second method is a THz TDS system, where the attenuation total reflection
88 (ATR) module is applied to operate liquid characterization. The work here demonstrates THz
89 technology an advanced transforming technique for the liquid detection.

90

91 2 Sample Preparation

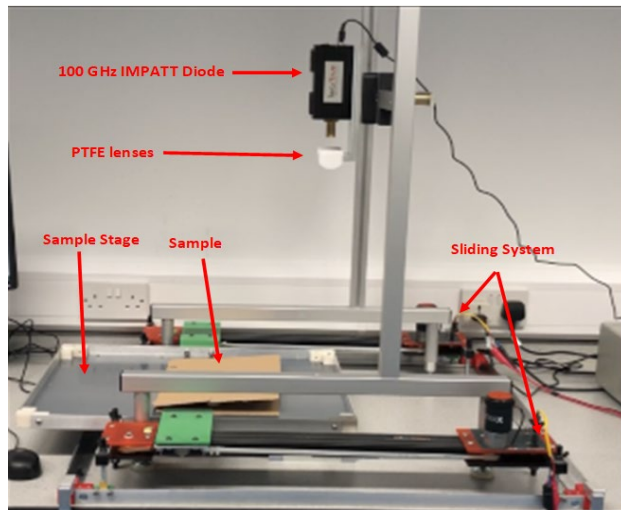
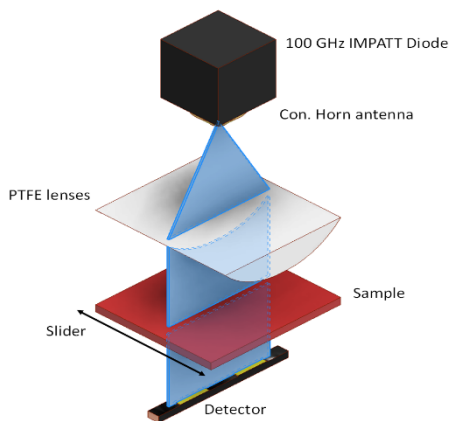
92 There were 9 liquid samples prepared for imaging and spectroscopy. The samples were Water(W),
93 Ethanol(E), Petrol 95 Ron Unleaded (P95), Petrol 98 Ron Super-Unleaded (P98), Diesel Oil (DO),
94 50/50 Petrol & Diesel (PD), Kerosene (KE), Fuel Treatment (FT) and Universal Bottle Cleaner (UC).
95 Each liquid was contained in a Polyvinyl Chloride (PVC) cannister and secured before imaging. All
96 sample liquids were provided by Motrac Ltd., England.

97 3 Measurement System and Methodology

98 3.1 100 GHz Line Scanner

99 The first system used to digitally image the sample liquids is a 2D 100 GHz Line Scanner, shown in
100 Figure 1. The 100 GHz source is an IMPATT diode, and the detector is the GaAs HEMT (high electron
101 mobility) based line scanning array, supplied by Terasense Ltd. The samples are mounted on the 1D
102 sliding plate and the line scanner array is located spatially orthogonally underneath the plate in order
103 to achieve 2D images. The slider speed was 10 cm per second.

104



105 Figure 1: (Left) Schematic plot of 100 GHz line scanner, (Right) photograph of the Line scanner

106 Each liquid was carefully extracted from its source into a general-purpose medical syringe, and the
107 transferred into its corresponding sample plastic cannister. A different syringe was used per liquid and
108 each of the 4 volumes was measured with a high degree of accuracy. It is important to note that the
109 plastic cannisters were made of PVC in order to get minimum interference between the source and the
110 detector of the imaging system. This was to ensure that the PVC cannisters allowed the THz signal to
111 pass through to the liquids without blocking the signal and swaying the results. The canisters were
112 covered by cardboard to mimic a packaging scenario.

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113

114 Using the images harvested, it is possible to determine the percentage value of visually clear area taken
 115 by the THz line scanner. The clear area represents areas of high penetration, or where the sample liquids
 116 have less absorptivity. The clear area fraction was defined by the given equation:

117

$$F_{clear} = \frac{w \times l}{A} \%$$

118

119 Where w , represents the width of the clear area and l , represents the length of the clear area; and A is
 120 the cross-section area of the empty plastic cannister.

121

122 **3.2 THz-TDS ATR Spectroscopy**

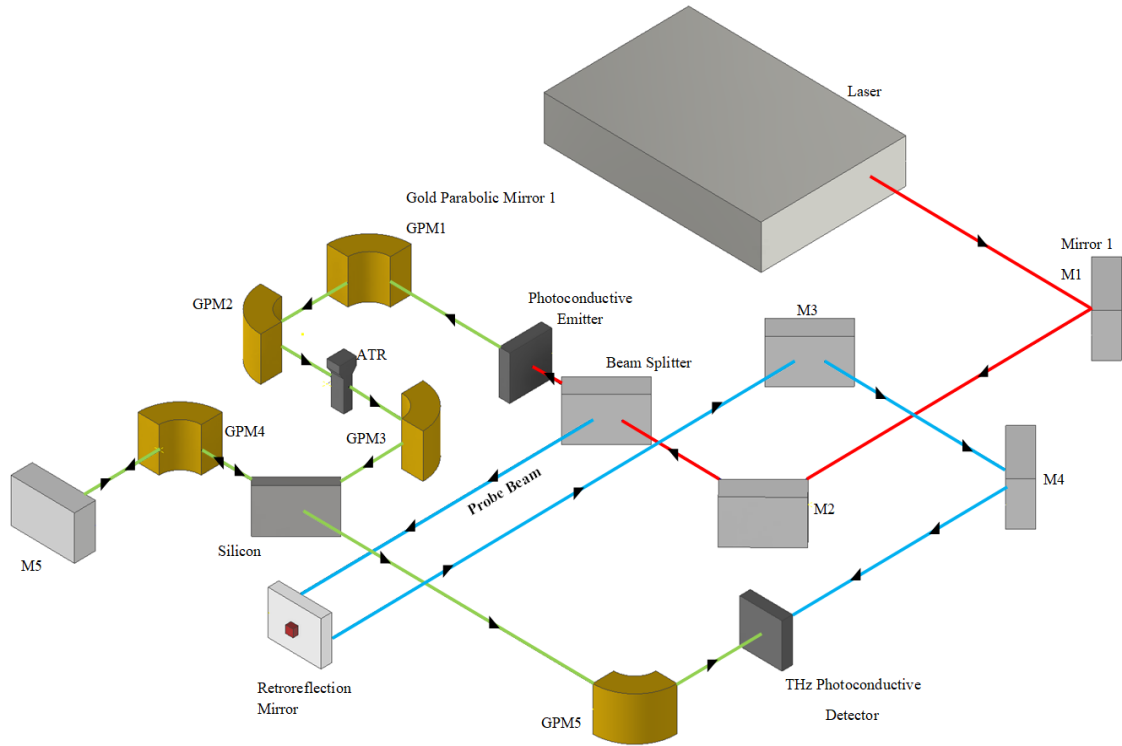
123 Per each sample of the ATR experiment, 1 ml of liquid was extracted from its source container into a
 124 general-purpose medical syringe. The volume of liquid should have no real impact on the results as the
 125 THz signal only passed through the liquid at the apex of the sample prism. The liquid was transferred
 126 from the syringe and injected into the top surface of the prism. Before the experiment could begin the
 127 test chamber was flooded with nitrogen gas, purging virtually all of the air within. This was done to
 128 push all of the air out of the chamber as air has a high humidity percentage, and the water would have
 129 high absorptivity of the inputted THz signal. Once each test was done, the liquid was removed via
 130 various clean methods, ensuring that no liquid remained in the prism surface, allowing for no
 131 contamination between test samples. A new sample liquid was then injected, and the chamber re-
 132 flooded with nitrogen. This process was repeated for all of the liquid samples.

133

134 The THz-TDS (TeTechS Ltd, Ontario, Canada) was used together with the ATR module and the
 135 spectra spans from 0.2 to 1 THz at room temperature, and the humidity in chamber was controlled <
 136 0.3% through continuous nitrogen purge. The 3D schematic THz-TDS set-up is presented in Figure 2
 137 (upper) and the beam propagation inside of the ATR module is graphically depicted in the lower part
 138 of Figure 2. The parameter extraction involves a transmitted Fourier transformed pulse waveform
 139 recording the temporal response of the THz reference pulse as a function of time delay [14]. The THz
 140 ATR technique is suitable for measuring liquid samples with high absorption, and also has excellent
 141 sample-to-sample reproducibility with minimal operator-induced variations. The core element of an
 142 ATR system is a silicon made prism, which is almost transparent and non-dispersive across the THz
 143 frequencies. In the ATR system, the THz beam from the emitter is directed into a silicon prism of
 144 relatively higher refractive index. The THz wave reflects from the prisms internal surface and produces
 145 an evanescent wave, which projects orthogonally into the liquid sample in close contact with the ATR
 146 prism. The sample absorbs some of the energy of the evanescent wave and the reflected radiation (some
 147 now absorbed by the liquid sample) is returned to the detector.

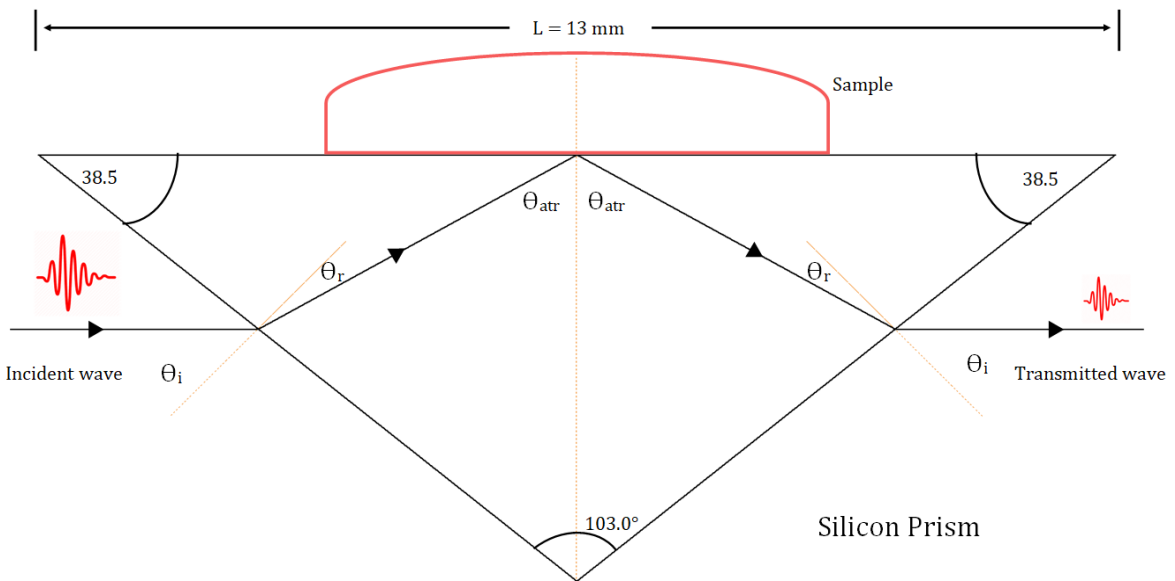
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151



152

Figure 2: Schematic plot of THz TDS (upper) and ATR module (lower).

153

154 After harvesting the experimental data, extraction of the sample's complex permittivity is implemented
 155 by the following procedures. At the interface between air and silicon, the THz beam follows the Snell's
 156 law:

157

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

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159 Here, n_1 is the refractive index of air, known to be 1; n_2 is the refractive index of silicon, known to be
 160 3.41; θ_1 represents the angle on incidence, which was determined by the ATR prism's structure, 51.5°
 161 and finally, θ_2 can be calculated, 13.27° . It is to be noted that the gas inside the TDS chamber is
 162 nitrogen, but as nitrogen and air have a virtually identical refractive index with a negligible difference,
 163 n_1 will be noted as air. Inside of the prism and at the surface between the silicon and the top air surface,
 164 the incident angle θ_{atr} equals the sum of θ_2 and 38.5° .

165 The complex transmission coefficient is given as:

166

$$167 \quad \hat{T}(\omega) = \frac{E_{sample}(\omega)}{E_{ref}(\omega)} = \frac{r^p_{prism-sample}}{r^p_{prism-air}}$$

168

169 Where $E_{sample}(\omega)$ and $E_{ref}(\omega)$ are the electric field Fourier transforms of the sample and
 170 background measurements, respectively; and $r^p_{prism-sample}$ and $r^p_{prism-air}$ are reflection
 171 coefficients between two media, silicon prism to the liquid sample and silicon prism to the air,
 172 respectively.

173

174 The complex refractive index of the sample liquid can be extracted from [15-16]:

175

$$176 \quad \bar{n}_{sample} = \frac{1}{\phi} \sqrt{\frac{1}{2} (1 \pm \sqrt{1 - (2\phi n_{prism} \sin(\theta_{atr}))^2})}$$

177 where ϕ follows the equation:

178

$$179 \quad \phi = \frac{\cos(\theta_{atr})}{n_{prism}} \left(\frac{1 - \hat{T} \cdot r^p_{prism-air}}{1 + \hat{T} \cdot r^p_{prism-air}} \right)$$

180 The refractive index between the prism and the air, $r^p_{prism-air}$ must still be calculated, using the
 181 given equation:

182

$$183 \quad r^p_{prism-air}(\omega) = \frac{\bar{n}_{prism}(\omega) C_{prism,air}(\omega) - \bar{n}_{air}(\omega) \cos\theta_{prism}}{\bar{n}_{prism}(\omega) C_{prism,air}(\omega) + \bar{n}_{air}(\omega) \cos\theta_{prism}}$$

184

185 Where \bar{n}_{prism} is the complex refractive index of the silicon prism. It is a notable that in this form,
 186 $\theta_{prism} \equiv \theta_{atr}$. Yet, $C_{prism,air}$ remains unknown, however can be calculated using the given equation

187

$$188 \quad C_{prism,air} = \sqrt{1 - \frac{\bar{n}_{prism}^2(\omega)}{\bar{n}_{air}^2(\omega)} \sin^2\theta_{prism}}$$

189

190 From this equation, \bar{n}_{sample} can be determined. As \bar{n}_{sample} is a complex number in the standard form,
 191 the real and imaginary part of the sample's permittivity can be given in the following two equations,
 192 respectively.

193

$$\epsilon' = n^2 - k^2$$

194

$$\epsilon'' = -2nk$$

195

196 Where 'n' is the real part of refractive index and the term 'k' represents the imaginary part of the
 197 complex refractive index.

198

199 4 Results and Discussion

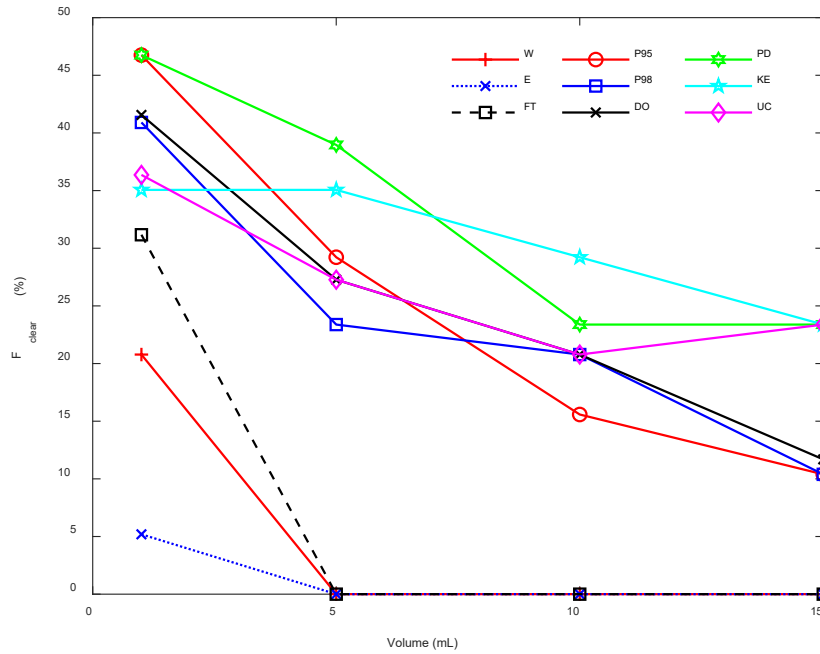
200 The relationship between the percentage of THz penetration area F_{clear} and the volume of volatile
 201 liquid samples is presented in Figure 3. The 2D images acquired from the line scanner and the detailed
 202 F_{clear} are presented in the supplementary materials SM.Table 1-5. The results have distinguished all
 203 liquid samples into two categories: highly absorbed samples and less absorbed liquids. The former is
 204 generally water-based, and includes Water, Ethanol and Fuel Treatment. For this group of samples,
 205 THz signal has less ability to penetrate the liquids, which is reflected by dark blue colours in the images.
 206 From Figure 3, 5ml, 10ml and 15ml samples all demonstrated 0 percentage of penetration area. For
 207 1ml samples, part of THz signals can pass through and this is due to the fact that there physically is
 208 less liquid in the sample cannisters, and so some signal passed through the substance and registered on
 209 the detector. This idea is supported by the fact that throughout all of the tests done: as the volume
 210 increases, the general fraction area of penetration decreases. In contrast, the low loss liquids are
 211 generally oil-based samples, with the exception of the water-based sample: Universal Bottle Cleaner.
 212 This category of liquids showed good penetration fraction areas and the general trend remains that they
 213 had a lower absorptivity than the water-based liquids.

214

215 The high-loss liquids have shown fast decreasing gradients to become completely opaque to the THz
 216 signal once the volume is increased past 5ml. The Ethanol shows a relatively slow decreasing slope
 217 and the Fuel Treatment has the fastest falling rate. For low-loss samples, the fractions of the penetration
 218 area are slowly decreased; however, different samples have shown different gradients. For example,
 219 petrol and diesel-based samples (P95, P98 and DO) have shown relatively quicker decrease, while the
 220 mixed Petrol/Diesel, Kerosene and Universal Bottle Cleaner have shown a slow decreasing slope. In
 221 order to further interpret these results, ATR based THz-TDS are used to investigate the reasons. The
 222 calculated complex permittivities are presented in Figure 4 and 5. From Figure 4, the Ethanol has the
 223 highest permittivity and lowest loss, which explains why it has the lower degrading attenuation in the
 224 Figure 3. As the liquid sample is held inside of a cylinder-shaped cannister with a curved surface, the
 225 100 GHz mm-wave source illuminates the curved surface of the sample bottle creating an oblique
 226 incident angle into the liquid, causing higher refraction; due to the higher permittivity of the liquid,
 227 which results in strayed mm-wave beam into the detect. For the Fuel Treatment and Water samples,
 228 they have a relatively low permittivity, inducing less trouble for beam refraction, therefore, they will
 229 absorb the weak penetrated mm-wave signal only. Both Fuel Treatment and Water liquid have higher
 230 loss properties, to result in higher decreasing gradient. In Figure 5, all oil-based sample liquids and the
 231 Universal Bottle Cleaner have relative equal or higher permittivity than water, and most importantly,
 232 they all have relatively low loss properties. The higher permittivity and medium loss properties explain

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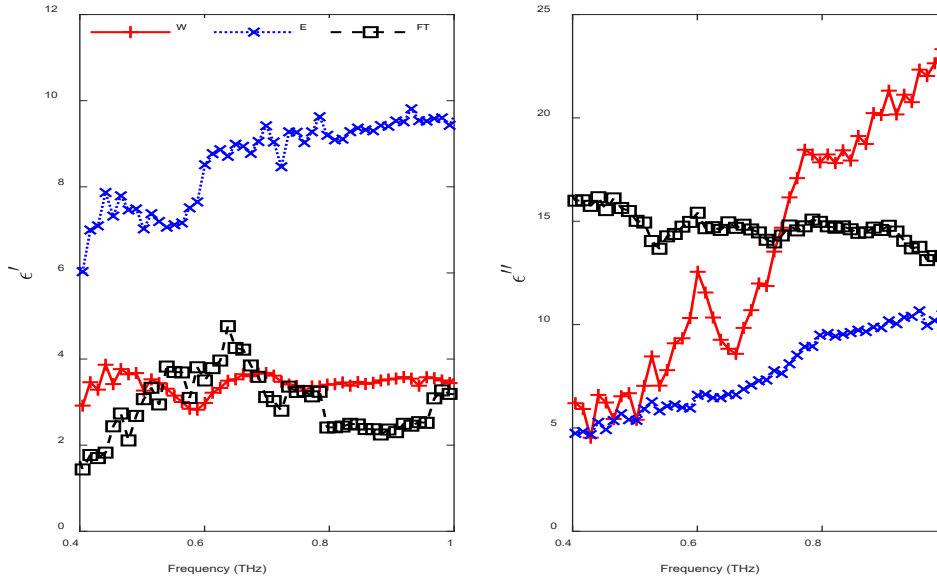
233 why they have better penetration results to the mm-wave, as it is easy to generate a strayed beam and
 234 less lost signals.



235
 236 Figure 3: Graph plot for clear area percentage against volume for each sample liquid.

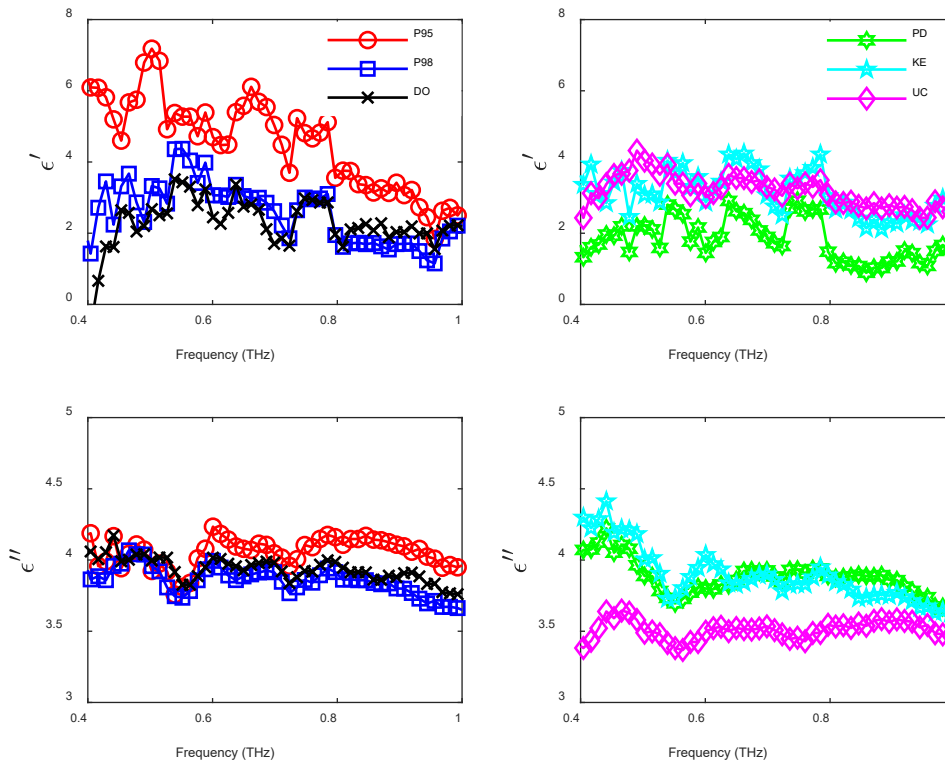
237
 238 The oil-based liquid samples, due to their organic chemicals that they are composed of, e.g. the
 239 hydrocarbons in petrol and diesel, generally contain less metallic elements and so therefore should
 240 have lower loss properties. The findings here suggest that mm-wave imaging can distinguish the
 241 difference of different kinds of liquids, as different liquids have demonstrated distinguishable
 242 attenuation rate and diffraction rate at the mm-wave and THz band. The mm-wave line scan imager is
 243 compact, poses no-radiation hazard, and could be an efficient method to distinguish different liquid
 244 samples.

245



246 Figure 4: the calculated complex permittivity of Water (W), Ethanol (E) and Fuel Treatment (FT).
 247 (Left) real part of permittivity, (Right) imaginary part of the permittivity.

248



249 Figure 5: the calculated complex permittivity of Petrol 95 (P95), Petrol 98 (P98), Diesel oil (DO),
 250 50/50 mixed Petrol/Diesel (PD), Kerosene (KE) and Universal Bottle Cleaner (UC). (Top) real part
 251 of permittivity, (Bottom) imaginary part of the permittivity.

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253 **5 Conclusion**

254 Combining 100 GHz 2D line scanner and THz ATR module-based TDS, 8 different volatile liquids
 255 and water have been imaged with high speed and characterized with their complex permittivities. The
 256 liquids' dielectric permittivities have contributed to the explanation of their mm-wave images. The
 257 higher permittivity of liquid can cause stray beams into the mm-wave detector, which can positively
 258 assist the detector to receive weak mm-wave beam and enhance the identification of the liquid samples.
 259 Through the mm-wave images, the volatile liquids can be subdivided into high loss samples (mainly
 260 water-based) and oil-based low loss samples (and the water-based Universal Bottle Cleaner), which
 261 also are proved by the THz spectroscopy analysis. The work here could give a positive, promising
 262 addition to a more precise baggage screening. Integrating these two systems could practically increase
 263 safety generally by requiring fewer additional manual bag checks to provide a clear security benefit.

264 **6 Supplementary Material**

265 See supplementary materials for the mm-wave line scanning images of all the liquids with different
 266 volume and also the calculated fraction of clear penetration area.

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