# Accelerated Weathering of Overhead Loadbreak Switch Interrupters NEETRAC

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High Voltage Switch Subcommittee
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#### NEETRAC Members 2008 - 2009

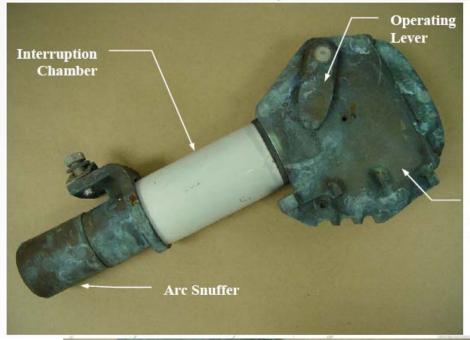
- 1. 3M
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#### Introduction

- NEETRAC completed a scoping study to identify field problems with distribution loadbreak switch interrupters in 2005.
- Utilities reported problems with "stuck" interrupters or failures when opening.
- 17 loadbreak interrupters were removed from field service and returned to NEETRAC for evaluation.
- Many of the problems with these units appeared to be caused by UV deterioration and corrosion.

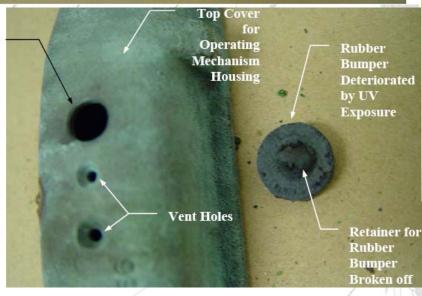
#### **Field Evaluation**



# Returned from Field Service: Alabama Power Company

Operating Mechanism Housing

Mounting Hole for Rubber Bumper

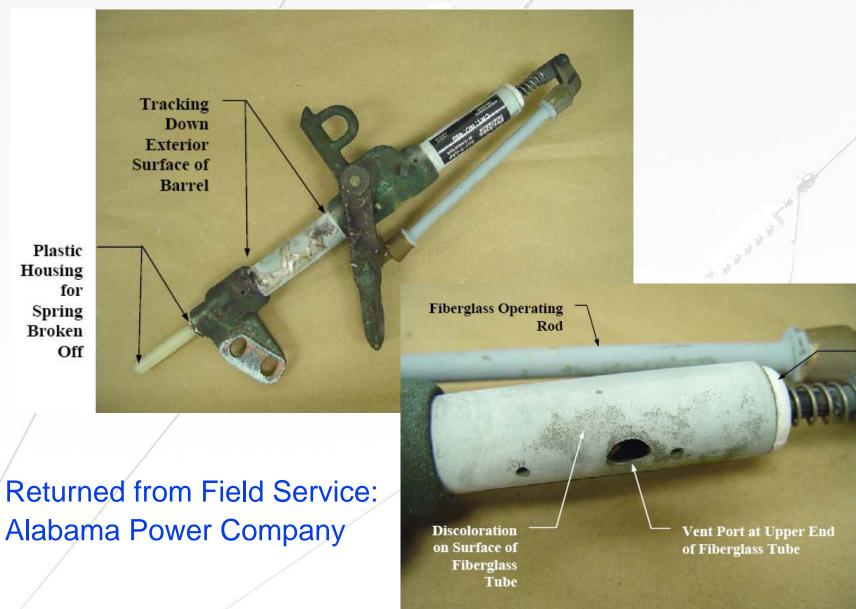




Cover for Operating Mechanism Casing

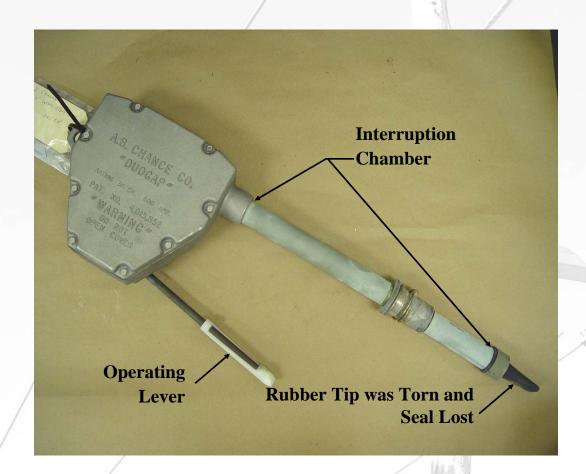
Rubber Bumper Deteriorated by UV Exposure

#### **Field Evaluation**



Nylon or Polyethylene Plug Serves as Guide Bushing for Bronze Push Rod

# **Field Evaluation**



Returned from Field Service: Dominion

# Accelerated Weathering of OH Loadbreak Interrupters

- Based upon a review of the units returned from the field, a project was initiated to investigate the affects of both UV deterioration and corrosion on new interrupters.
- Six different loadbreak interrupters from five manufacturers were exposed to both UV / condensation and salt-fog accelerated weathering at NEETRAC.
- Benchmark tests were performed during the aging process to measure dc contact resistance and mechanical force required for operation.

# Accelerated Weathering of OH Loadbreak Interrupters

- Both new and aged interrupters were then subjected to the full load current interruption tests according to Section 9.1 of IEEE C37.34 at a high power laboratory.
- Failures from the full load current interruption tests were examined to assess the impact of the weathering on performance.

# **Samples Tested**



S&C Electric Company Omni-Rupter 17 kV, 900 A 147442R1-Z3-S115



S&C Electric Company Alduti-Rupter 17 kV, 600 A 137512R7-S102

# **Samples Tested**



Bridges Vector 25 kV, 900A PN963XF-41AS



A. B. Chance Automation Ready 29 kV, 900 A AR114MSLP

# **Samples Tested**



Cooper Power Systems
M-Force
25.8 kV, 900 A
M2A41SC3AT



Inertia 25 kV, 600 A TRS26STSHX1125

# **UV / Condensation Aging**

UV / condensation aging according to ASTM D4329-05 and ASTM G154-06 using UVA-340 lamps.



# **UV / Condensation Aging**

- 2,000 hours total aging was required to produce results similar to those observed on field aged units (includes UV & condensation periods).
- The following aging cycle was used:
  - 8 hours of UV at  $60 \pm 3$  °C
  - 0.25 h water spray (no light), temperature not controlled
  - 3.75 h condensation at 50  $\pm$  3 °C
- Rotation of samples approximately every 333 hours, horizontally across the rack.
- Distilled water was used for the chamber.

# Salt-fog Aging

- Performed on one sample of each design after 2,000 hours of UV / condensation aging.
- 1,000 hour salt-fog aging test according to ASTM B117-07.
- A continuous fog of 5% salt solution was used.

#### **Benchmark Tests**

- dc contact resistance (closed position)
- Mechanical performance torque, force, etc. (both opening and closing)
- Performed on the samples four times:
  - -new
  - -after 1,000 hours of UV aging
  - -after 2,000 hours of UV aging
  - -after 1,000 hours of salt-fog aging
- Sample designations:
  - –UV is UV / Condensation aging only
  - -UVS is UV / Condensation and Salt-fog aging

# **Benchmark Test Results**

		dc Cor				
Sample Number	Initial	Post 1,000 hr UV Aging	Post 2,000 hr UV Aging	Post Salt- Fog Aging Before Operation	Post Salt- Fog Aging After Operation	Comments
A-UV-4	0.061	0.115	0.830			
A-UV-5	0.085	0.158	0.385			
A-UVS-6	0.067	0.339	0.218	0.068	0.134	
D-UV-4	0.003	0.006	0.005			Interrupter was rusted shut when
D-UV-5	0.009	0.007	0.032			removed from salt-fog. After interrupter was forced open,
D-UVS-6	0.004	0.014	0.003	0.018	12545	internal contacts never opened.
E-UV-4	0.297	0.379	0.182	2		
E-UVS-5	0.485	0.230	0.235	5.560	1.480	
E-UV-6	0.176	0.286	0.283		100	
F-UV-4	0.006	0.034	0.014			
F-UVS-5	0.063	0.015	0.078	0.012	0.098	
F-UV-6	0.004	0.028	0.006			X
G-UV-4	0.007	0.018	0.010			Could not close interrupter
G-UVS-5	0.009	0.020	0.011	0.206	open	internally after it was operated
G-UV-6	0.006	0.007	0.008			post salt-fog.
H-UV-4	0.054	0.081	0.018	N/		
H-UVS-5	0.068	0.019	0.029	1500	1398	
H-UV-6	0.039	0.031	0.060	16		16

#### **Benchmark Test Results**

	Force Measurements in Ibs									
	Initial		Post 1,000 hr UV Aging		Post 2,000 hr UV Aging		Post 1,000 hr Salt- Fog Aging			
Sample Number	Open to Closed Contacts	Closed to Open Contacts	Open to Closed Contacts	Closed to Open Contacts	Open to Closed Contacts	Closed to Open Contacts	Open to Closed Contacts	Closed to Open Contacts		
A-UV-4	9.8	8.2	10.0	9.8	11.0	10.5		5		
A-UV-5	11.4	9.9	12.4	10.2	10.5	10.7	3			
A-UVS-6	9.6	8.8	9.8	10.8	10.0	10.3	13.9	9.9		
D-UV-4	25.0	18.0	22.9	21.0	20.7	19.2		A.		
D-UV-5	23.7	20.0	23.0	19.0	21.9	21.8				
D-UVS-6	23.0	21.0	19.9	22.2	20.1	19.4	24+	26+		
E-UV-4	0.6	7.8	0.6	8.1	0.4	7.8				
E-UVS-5	0.9	7.6	0.4	7.5	0.9	7.9	2.0	8.2		
E-UV-6	0.9	8.4	0.6	8.2	1.0	7.8				

Sample D-UVS-6 had to be lubricated with rust buster and forced open in order to record the post salt-fog aging measurements.

# Benchmark Test Results

					1					
	Force Measurements in Ibs									
	Initial		Post 1,000 hr UV Aging		Post 2,000 hr UV Aging		Post 1,000 hr Salt- Fog Aging			
Sample Number	Open to Closed Contacts	Closed to Open Contacts	Open to Closed Contacts	Closed to Open Contacts	Open to Closed Contacts	Closed to Open Contacts	Open to Closed Contacts	Closed to Open Contacts		
F-UV-4	13.9	9.8	14.5	10.0	15.2	11.0		1		
F-UVS-5	15.0	9.8	16.0	10.2	14.5	9.3	14.2	16.2		
F-UV-6	15.3	9.8	18.7	10.6	15.1	9.8	100			
G-UV-4	0.3	12.9	0.8	13.1	0.1	11.1				
G-UVS-5	0.4	12.0	0.9	12.6	0.6	12.3	2.0	10.2		
G-UV-6	0.4	11.9	0.5	11.4	0.4	12.0	2 ji	- /		
H-UV-4	3.8	15.0	0.9	15.0	0.4	16.1	i de la companya de	/		
H-UVS-5	5.7	17.0	0.9	15.1	0.5	14.9	4.0	12.6		
H-UV-6	2.7	19.0	1.2	16.1	0.2	15.4				

### **Load Current Interruption Tests**

- Performed at Powertech
   Labs October 2007
- IEEE Std 1247<sup>™</sup> 2005, Clause 8.3.2.1, Loadswitching tests



#### **Load Current Interruption Tests**

#### Test plan for each manufacturer's switch:

- Perform 10 load break switching operations at 100% load with new (un-aged) interrupters (as required by IEEE Std 1247™). A five minute "cool down" period was provided between each switching operation.
- 2. If the unit passed IEEE Std 1247<sup>TM</sup> requirements, replace interrupters with new (un-aged) interrupters and perform *three additional load break switching operations* under *wet conditions*. Prior to each operation, each interrupter was thoroughly wetted with water using a spray bottle with 100 ± 15 Ω-m water. A five minute "cool down" period was provided between each switching operation.

### **Load Current Interruption Tests**

- 3. Replace interrupters with the *aged units* (two UV aged only and one UV + salt-fog). During setup / calibration, locate the pole that opens first and install the UV + salt-fog interrupter at that location. Perform *10 load break switching operations* at 100% load. If an interrupter fails, substitute a new interrupter to try to complete the series to gain as much data as possible from the tests. A five minute "cool down" period was provided between each switching operation.
- 4. If the unit passed the requirements in (3), perform *three* additional load break switching operations under wet conditions. Prior to each operation, each interrupter was thoroughly wetted. A five minute "cool down" period was provided between each switching operation.

# Load Current Interruption Test Results

	Number of Successful Interruptions					
Manufacturer	New (10)	New Wet (3)	Aged (10)	Aged Wet (3)		
D	7 *1	*2	*2	*2		
F	8	3	3	3 *3		
I E E	10	3	2 *4	*4		
A Service A	10	3	10	3		
/ / H	10	3*5	10	3		
G	4	0	0	*6		

Notes: \*1 – Switch was removed from field service. Interrupters were not new.

- \*2 New and aged interrupters' mounting brackets were different. Aged units could not be tested.
- \*3 Only the aged F-UV-6 interrupter completed the three wet tests.
- \*4 Interrupters pickup hooks were not replaced after the tests on new interrupters. These worn hooks may have contributed to the failure of the aged interrupters.
- \*5 Wet tests were performed on the original new interrupters (13 total operations on same units).
- \*6 Wet tests were not performed on the aged interrupters due to previous failures.

#### **Benchmark Test Observations**

- dc contact resistance measurements did indicate problems with samples D-UVS-6, G-UVS-5, and H-UVS-5 after the salt-fog aging.
- Force measurements also indicated problems with D-UVS-6 after the salt-fog aging.

# **Interruption Test Observations**

- Wet tests did not affect results of the load current interruption tests.
- Three of the interrupters were definitely affected by the accelerated weathering tests.
  - -D-UVS-6 seized up due to corrosion.
  - F-UV-4 and F-UVS-5 failed after only three successful interruptions.
  - H-UVS-5 experienced corrosion of a riveted connection that vaporized during testing, but none-the-less passed as the connection arced over.

## **Interruption Test Observations**

- Two of the interrupters may have been affected by the accelerated weathering tests.
  - Manufacturer E interrupter tests terminated early due to pickup clip failure.
  - Manufacturer G failed interruption tests (new units also failed).
- One interrupter was *definitely not affected* by the accelerated weathering tests.
  - Manufacturer A interrupter passed all of the tests.

#### Recommendations for IEEE C37.34

- Add requirements for accelerated UV / Condensation aging prior to interrupting tests in Section 9 for usual service conditions.
- Add requirements for accelerated UV / Condensation aging and salt-fog aging prior to interrupting tests in Section 9 for unusual service conditions involving contaminated environments.





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