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# Reliability-Based Optimization for Multiple Constraints with Evolutionary Algorithms

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**Abstract**—In this paper, we combine reliability-based optimization with a multi-objective evolutionary algorithm for handling uncertainty in decision variables and parameters. This work is an extension to a previous study by the second author and his research group to more accurately compute a multi-constraint reliability. This means that the overall reliability of a solution regarding all constraints is examined, instead of a reliability computation of only one critical constraint. First, we present a brief introduction into this so-called ‘structural reliability’ aspects. Thereafter, we introduce a method for identifying inactive constraints according to the reliability evaluation. With this method, we show that with less number of constraint evaluations, an identical solution can be achieved. Furthermore, we apply our approach to a number of problems including a real-world car side impact design problem to illustrate our method.

## I. INTRODUCTION

In handling real-world optimization problems, it is often the case that the underlying decision variables and parameters cannot be fixed exactly as specified. For example, if a deterministic consideration of an optimization problem results in an optimal dimension of a cylindrical member to have 50 mm diameter, there exists no manufacturing process which will guarantee producing a cylinder having exactly 50 mm diameter. Every manufacturing process has a finite machine precision and the dimensions are expected to vary around the specified value. Similarly, the strength of a material often labeled on it or on a handbook does not remain fixed on the entire length of the material and is expected to vary from point to point. When such variations in decision variables and parameters are expected in practice, an obvious question arises: ‘how reliable is the optimized design against failure when the suggested parameters cannot be adhered to?’ This question is important, as in most optimization problems the deterministic optimum lies on the intersection of a number of constraint boundaries. Thus, if no uncertainties in parameters and variables are expected, the optimized solution is the best choice, but if uncertainties are expected, in most occasions, the optimized solution will be found to be infeasible, violating one or more constraints. Assuming that the variables inherently follow a probability distribution of their possible variation in practice, reliability-based optimization methods find a *reliable* solution which is feasible with a pre-specified reliability, [11], [10].

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Different methods for evaluating the reliability of a solution exist. One straightforward method is to use Monte-Carlo simulation, however this gets computationally expensive when the desired reliability is very high. A more common and much faster approach is the evaluation of reliability with first- or second-order reliability methods (FORM/SORM), which are based on linear and quadratic approximation of the constraint functions [12], [13].

A previous study [10] used a stochastic optimization strategy along with an EMO procedure to handle such uncertainties in decision variables and parameters. The study has shown that by using the suggested procedures, a solution can be obtained to have an expected reliability against failure. However, the study made an assumption in its computation of the reliability. Even in the presence of a number of constraints, the study considered only the most critical constraint for failure and ignored the effect of other constraints. In other words, for each solution encountered in the optimization process the study computed the reliability against failure for each constraint at a time and the smallest reliability value is assigned to the solution. Obviously, such a consideration overestimates the reliability. Ideally the reliability of a solution must be computed by considering a cumulative effect of all constraints. In this paper, we borrow the idea of structural reliability and Ditlevson bounds [11], and extend the earlier study for a better computation of the reliability values.

## II. RELIABILITY-BASED OPTIMIZATION

Let us consider a typical reliability-based optimization problem:

$$\begin{aligned} & \text{Minimize} && \mu_f(\mu_{\mathbf{X}}, \mathbf{d}, \mathbf{P}), \\ & \text{Subject to} && P(g_i(\mathbf{X}, \mathbf{d}, \mathbf{P}) \geq 0) \geq R_i, \quad i = 1, 2, \dots, I, \\ & && h_k(d) \geq 0, \quad k = 1, 2, \dots, K, \\ & && X^{(L)} \leq \mu_X \leq X^{(U)}, \\ & && d^{(L)} \leq \mathbf{d} \leq d^{(U)}, \end{aligned} \quad (1)$$

where  $\mu_f$  is the objective function calculated at the mean of the random parameters,  $\mu_X$  is the vector of the mean values of the probabilistic design variables,  $d$  is the vector of deterministic design variables, and  $P$  stands for the mean values of the set of uncertain parameters. Bold letters are used for vectors, capital letters for random variables and lower case letters for deterministic variables.

We differentiate between the stochastic constraints  $g_i$ , which include at least one random variable, and the deterministic constraints  $h_k$ , which do not include random variables. The probability of constraint satisfaction  $g_i(\mathbf{X}, \mathbf{d}, \mathbf{P}) \geq 0$

should be equal to or larger than the desired reliability level  $R_i$ .

#### A. Concept of Structural Reliability

Assuming that

- an  $n$ -dimensional vector of variables in the solution space with the joint density function  $k_{XP}(\mathbf{x}, \mathbf{p})$  and
- a number of constraint functions which denote safe states if they are greater than zero and failure states if they are less than zero exists, where  $g_i(\mathbf{X}, \mathbf{d}, \mathbf{P}) = 0$  defines exactly the border between the feasible and the infeasible region,

then the failure probability is

$$P_F = P(g(\mathbf{X}, \mathbf{d}, \mathbf{P}) \leq 0) = \int_{g(\mathbf{X}, \mathbf{d}, \mathbf{P}) \leq 0} k_{XP}(\mathbf{x}, \mathbf{p}) dx. \quad (2)$$

Normally, it is very difficult to calculate the multi-dimensional integral for this equation. Monte-Carlo simulation can be used. This is based on creating a number of samples, evaluating them and approximating the failure probability with the ratio of feasible samples  $n$  and number of samples  $N$ . Then the failure probability can be approximated with:

$$P_F \approx \left(1 - \frac{n}{N}\right). \quad (3)$$

This simple approach works well for small reliability requirement, but if the desired reliability is large, the number of samples must also increase to find at least one infeasible solution. For example, for a failure probability of  $P_F = 10^{-6}$  the number of samples be at least  $N \approx 10^6$  to find one infeasible solution in a million samples. If the problem is high-dimensional or includes expensive finite element computations, the Monte-Carlo approach may not be feasible for practical use.

Hasofer and Lind [3] introduced a system called most probable point (MPP) to approximate the integral. To apply this system, we first have to transform the  $x$ -coordinate system (decision variables) with the Rosenblatt transformation [2] into the independent standard normal space  $U$ . The constraint function  $g(\mathbf{X}, \mathbf{d}, \mathbf{P})$  is subject to the same transformation into  $G(\mathbf{u})$ . The converted failure probability is

$$P_F = \int_{g(\mathbf{X}, \mathbf{d}, \mathbf{P}) \leq 0} k_{XP}(\mathbf{x}, \mathbf{p}) dx = \int_{G(\mathbf{u}) \leq 0} \varphi_U(\mathbf{u}) dx, \quad (4)$$

where  $\varphi_U(u)$  is the  $n$ -dimensional standard normal density with independent components. In this space, the MPP can be found for a particular constraint,

$$\mathbf{u}_i^* = \min \|\mathbf{u}_i\| \forall G(\mathbf{u}_i) \leq 0, \quad (5)$$

where  $\mathbf{u}_i^*$  are the points on the constraint functions with the shortest distance to the origin. For every constraint, a

separate MPP exists. Since the standard normal space is rotational symmetric we directly get the failure probability  $P_i$  of  $i$ -th constraint with

$$P_i = \Phi(\beta_i), \quad (6)$$

where  $\beta_i$  is  $\|\mathbf{u}_i^*\|$  and  $\Phi(\cdot)$  is the CDF (cumulated density function) of the standard normal distribution. The MPP corresponds directly to the required reliability index  $\beta$ . The described approach represents the FORM method which is based on a linear approximation of the constraint function (refer to Fig. [3]).

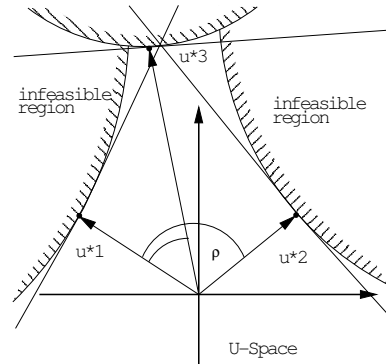


Fig. 1. FORM procedure with linear approximation at the MPP. The third constraint does not influence the feasible area.

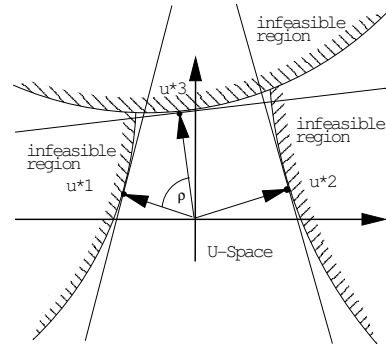


Fig. 2. The third constraint bounds the feasible area.

Importantly, the above procedure estimates the failure probability only for one constraint. In most optimization problems, the feasible area is bounded by more than one constraint and consists of constraint intersections. The fluctuation of the solution can be in any direction and so it is important to include all constraints in the reliability approximation. Simple bounds for the failure probability are given elsewhere [19],

$$\max_{i=1}^I P_i \leq P_F \leq \sum_{i=1}^I P_i. \quad (7)$$

Much closer bounds on the failure probability are given by Dietlevsen [1] which computes the joint failure probabilities of all constraints:

$$P_1 + \sum_{i=1}^k \max \left\{ P_i - \sum_{j=1}^{i-1} P_{ij}, 0 \right\} \leq P_F$$

$$\leq \sum_{i=1}^k P_i - \sum_{i=2}^k \max_{j \leq i} P_{ij}. \quad (8)$$

The formula depends on the sequence of the failure modes and a different order may cause different reliabilities. It is a practical experience that a good ordering is obtained by ordering the failure modes according to decreasing values  $P_i$  [14]. The joint probability  $P_{ij}$  is given by the CDF of the bivariate normal distribution with

$$P_{ij} = \Phi(-\beta_i, -\beta_j, \rho_{ij}) \quad (9)$$

and the correlation coefficient  $\rho_{ij}$  is given by

$$\rho_{ij} = \cos \left( \frac{\langle \mathbf{u}_i^*, \mathbf{u}_j^* \rangle}{\|\mathbf{u}_i^*\| \|\mathbf{u}_j^*\|} \right). \quad (10)$$

Here, the  $\cos(\cdot)$  of the angle between two  $\mathbf{u}^*$  vectors. By using higher-order intersections it is possible to improve the bounds but this involves much more numerical effort with a little gain in accuracy of the result [15]. Summing up the ideas, we can replace the stochastic constraint in (1) for a single constraint by the following expression:

$$P_i \geq R. \quad (11)$$

If we include all constraints and measure  $P_F$  with the Dietlevson bounds then we get

$$1 - \left( \sum_{i=1}^k P_i - \sum_{i=2}^k \max_{j \leq i} P_{ij} \right) \geq R. \quad (12)$$

### B. Methods For Finding the MPP

The search for the MPP point with a suitable algorithm is the computationally most expensive part of the FORM procedure. This is in itself an optimization problem [4]. Various methods have been proposed and an overview is given by Eldred [5]. For our following approach, we need the distance from the origin to the constraint in the  $U$  space. For this reason, we use the Reliability Index Approach (RIA) even if this procedure may be slower than others.

In the RIA approach, the MPP is found by searching for the point on the constraint boundary which has the minimal distance to the origin in the  $U$  space (see Fig. 3). This leads to the following minimization problem:

$$\begin{aligned} & \text{Minimize} && \|\mathbf{u}\| \\ & \text{Subject to} && G_i(\mathbf{u}) = 0. \end{aligned} \quad (13)$$

If we apply this optimization problem to every constraint, we get a vector  $\mathbf{u}^*$ , where  $\|\mathbf{u}_i^*\| = \beta_i$  is the shortest distance from the origin to the constraint  $i$ .

To solve the above problem, we use a fast gradient-based approximate approach proposed in [10], [4]. Fig. 4 illustrates the procedure and the steps are shown below.

- Step 1** compute the gradient  $\nabla \mathbf{g}_i^0$  of constraint  $i$  at the origin of the  $U$  space,
- Step 2** find the intersection (point A) of  $\nabla \mathbf{g}_i^0$  and a circle with radius  $\beta_i = 1$ ,
- Step 3** compute the new gradient  $\nabla \mathbf{g}_i^1$  at point A,
- Step 4** find the intersection of  $\nabla \mathbf{g}_i^1$  and the circle of radius  $\beta_i$  (point B),
- Step 5** repeat step 3 and 4 until  $\|\nabla \mathbf{g}_i^i\| - \|\nabla \mathbf{g}_i^{i+1}\| \leq 0,001$ . Then get  $\mathbf{u}^*$
- Step 6** perform a unidirectional search along  $\mathbf{u}^*$  with the Newton Raphson approach until tolerance level  $\epsilon = 0,001$  is met.

The convergence of this method is usually quick requiring only a derivate of the constraint in the  $U$  space. Since it is a gradient based procedure, there is no guarantee for convergence especially if highly non-linear constraints are involved. However, for most problems this approximation is sufficient and can be used.

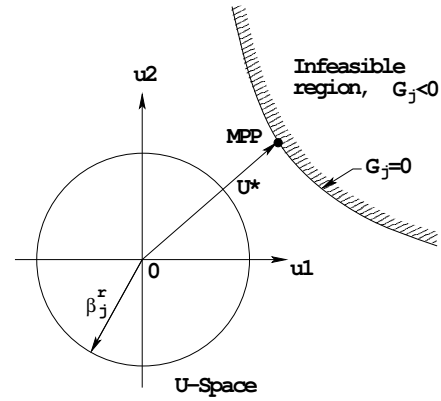


Fig. 3. RIA approach.

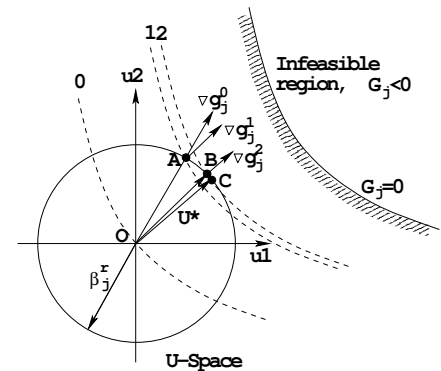


Fig. 4. Gradient based approximate method for solving the RIA problem.

### III. PROPOSED ACTIVE CONSTRAINT APPROACH

In the FORM analysis, the integral in (4) is bound by the set of tangent hyperplanes at the MPP for the different constraints (see Fig. 1). Normally, one calculates all the MPPs, then the correlation matrix and the probability matrix. The function for the reliability can be expressed as  $R(g_1, \dots, g_I)$  and depends on the distance from the constraints to the origin and the position of the different constraints relative to each other. Assume that there are three parallel constraints with different distances to the origin. Then only the closest constraint should be taken into account for  $P_F$  as the others do not increase  $P_F$ . Fig. 2 shows an example in which the feasible area is completely bound by three constraints. When the solution is moving away from constraint three, constraint three is no longer part of the bound and has no influence on the failure probability. If we know that constraint  $j$  does not bias  $P_F$ , we could reduce the reliability function to  $R(g_1, \dots, g_{j-1}, g_{j+1}, \dots, g_I)$ . This means the inner loop optimization for finding the MPP is not necessary and also the probability matrix can be reduced. Given the probability matrix

$$P_{ij} = \begin{pmatrix} P_{11} & & & & \\ P_{12} & P_{22} & & & \\ P_{13} & P_{23} & P_{33} & & \\ \vdots & & & \ddots & \\ P_{1j} & P_{2j} & P_{3j} & \dots & P_{ij} \end{pmatrix}$$

calculated using (9) and (6) the probability of violating constraint  $i$  is given by  $P_i$  and also the failure probability for the intersection of two constraints, given by  $P_{ij}$ . The upper bound of (8) is

$$\sum_{i=1}^k P_i - \sum_{i=2}^k \max_{j \leq i} P_{ij}. \quad (14)$$

If  $\max_{j \leq i} (P_{ji}) \geq P_i$ , then no additional failure probability is added. Given the above equation only a constraint parallel to another can get inactive. But also if they are not exactly parallel they are inactive because the intersection does only add irreducible failure probability. Therefore, we define the following:

**Definition 1:** Constraint  $i$  is called an inactive constraint, when the following criteria is fulfilled.

$$P_i \leq \max_{j < i} P_{ji} - \epsilon \quad \forall \quad j < i \in J, \quad (15)$$

where  $\epsilon$  describes the negligible failure probability.

We have chosen  $\epsilon = 0,0000009$  for all our test cases. The impact of this approximation is much smaller than the influence of FORM and will not cause a loss in accuracy. The simulation results on test problems in this study also verify this. As an example, consider the following probability matrix:

$$\begin{pmatrix} 0.040 & & & \\ 0.005 & 0.020 & & \\ 0.005 & 0.010 & 0.010 & \end{pmatrix}$$

Then the upper bound of the failure probability is  $(0.040 - 0) + (0.020 - 0.005) + (0.010 - 0.010)$  or 0.055. The third

constraint does not add any failure probability to  $P_F$  because its intersection with the second constraint is too large. If we calculate the reliability of that specific point again without considering the third constraint the result would be exactly the same.

Based on the above active constraint strategy, we suggest solving two types of problems: (i) finding multiple reliability solutions for a single-objective optimization problem and (ii) finding multiple Pareto-optimal solutions for a specified reliability value.

### IV. FINDING MULTIPLE RELIABILITY SOLUTIONS

We suggest a reliability-based optimization procedure based on evolutionary algorithms for finding solutions with respect to different reliability values simultaneously [10]. It was shown in the previous study that by introducing an additional objective of maximizing reliability ( $R$  or  $\beta$ ) and treating the problem as a two-objective optimization problem (the other objective being the optimization of the original problem), the set of Pareto-optimal solutions consists of solutions corresponding to different reliability values. By analyzing these solutions, the user can also learn about how the solutions change with different reliability requirements and this knowledge may provide a plethora of important information about the problem. This changes our optimization problem to the following problem:

$$\begin{aligned} \text{Minimize} \quad & \mu_f(\mu_{\mathbf{X}}, \mathbf{d}, \mu_{\mathbf{P}}), \\ \text{Maximize} \quad & R(\mu_{\mathbf{X}}, \mathbf{d}, \mu_{\mathbf{P}}) = R = (1 - P_F), \\ \text{Subject to} \quad & h_k(d) \geq 0, \quad k = 1, 2, \dots, K, \\ & \beta^{(L)} \leq \beta \leq \beta^{(U)}, \\ & X^{(L)} \leq \mu_X \leq X^{(U)}, \\ & d^{(L)} \leq \mathbf{d} \leq d^{(U)}. \end{aligned} \quad (16)$$

To handle the reliability constraint, we use the RIA approach explained above as an inner-loop optimization. We then calculate  $P_F$  with the Ditlevsen bounds.

In real-world optimization problems there is often a large number of constraints. Since it is not known which constraints are active before finding the MPP, the above mentioned optimization problem has to be solved for every constraint. This becomes an expensive proposition. But in most situations, only a few constraints are active at the final solution. Thus, the active constraint strategy described above becomes an inexpensive procedure for computing failure probability.

It is also intuitive that for a solution in a specific neighborhood involving a particular constraint set are active. Here, we use a book-keeping strategy in which the hierarchy of active constraints for each solution is stored. For evaluating a subsequent solution, a stored solution is first searched. If found, only the corresponding active constraints are considered. If a subsequent solution happens to lie in a region deep inside the infeasible region, then only the most violated constraint of that area is evaluated. For solutions which do

not belong to a neighborhood, all constraints are evaluated. We present the complete constraint handling method in the following:

```

input x
find closest point  $m_i$  to x in the memory
if  $\|x - m_i\| \leq \epsilon$  then
  if the stored reliability  $P_F^{m_i}$  is smaller than parameter  $k$  then
    return  $P_F^{m_i}$ 
  else
    calculate the MPP for the active constraints of  $m_i$ 
    calculate  $P_F^x$  with active constraints
    return  $P_F^x$ 
  end if
else
  evaluate MPP for all constraints
  identify the active constraints
  calculate  $P_F^x$ 
  store x and  $P_F^x$ 
  return  $P_F^x$ 
end if

```

#### A. Simulation Results

To verify the suggested procedures, we apply them to two optimization problems: a two-variable test problem and a car side-impact problem.

Most classical reliability based methods start with searching for the deterministic solution. From this point the solution is shifted into the feasible area to satisfy the reliability constraint. With this method it is not secured that the obtained solution is the global optimum to the reliability based problem [10].

1) *Two-Variable Multi-Modal Test Problem:* Here we consider the following problem, the constraints are taken from [8]:

$$\begin{aligned}
 &\text{Minimize} && \sin(3x^2) + \sin(3y^2) + x + y, \\
 &\text{Maximize} && R(g_i(x, y)) = (1 - P_F), \\
 &\text{Subject to} && g_1(x, y) \equiv \frac{1}{20}x^2y - 1 \geq 0, \\
 & && g_2(x, y) \equiv \frac{1}{30}(x + y - 5)^2 + \frac{1}{120} + \\
 & && \quad (x - y - 12)^2 - 1 \geq 0, \\
 & && g_3(x, y) \equiv \frac{80}{x^2 + 8y + 5} - 1 \geq 0, \\
 & && 0 \leq x, y \leq 10.
 \end{aligned} \tag{17}$$

To find the optimal solutions, we apply the NSGA-II with a population size of 100 for 200 generations. We restrict the reliability level to  $0.5 \leq \beta \leq 5.0$  causing a reliability between 69.14625% and 99.99997%. The standard deviation of both variables is assumed to be 0.03. The objective functions, shown in Fig. 5, includes many local optima. It is interesting to note that as the reliability requirement increase,

the solutions tend to move away further from the constraint boundaries, thereby causing the basin of attraction to change from one local optimum to another. Every gap represents a change towards an inferior local optimum to satisfy the reliability requirement.

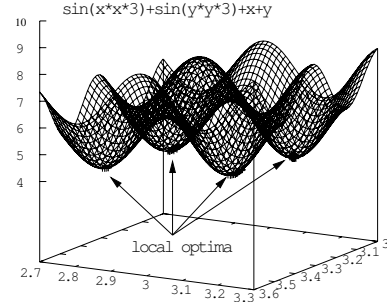


Fig. 5. Contour of the objective landscape of the test problem with four local optima.

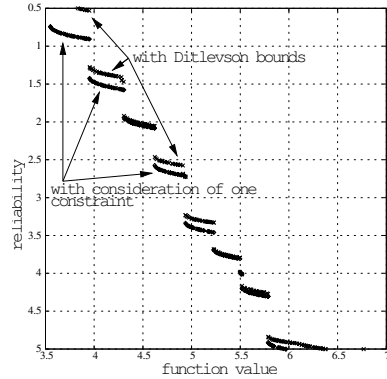


Fig. 6. Simulation results on the multi-modal test problem.

TABLE I  
COMPARISON OF THE NUMBER OF MPP EVALUATIONS.

Method	Car Side-Impact
Proposed method	329.825
Without memory	1000.000

2) *A Car Side-Impact Problem:* Next, we consider a car side-impact problem [8]. Cars have to pass tests to prove their safety for the passengers. This side-impact is based on European Enhanced Vehicle Safety Committee (EEVC) and measures the effect of a side-impact on a dummy according to several criteria. The impact on the dummy is directly related to the velocity of the front area and can be reduced by increasing the dimension of the car parameters. This, of course, will add weight to the car and will increase the material costs and the fuel consumption. Thus, we would like to minimize the weight and maximize the reliability in order to fulfill all test requirements. We apply NSGA-II with a population size of 200 for 500 generations. The problem

is defined as follows [10]:

$$\begin{aligned}
 & \text{Minimize}_{(x_1, \dots, x_7)} f(\mathbf{x}) = \text{Weight}, \\
 & \text{Subject to} \quad c_1(\mathbf{x}) \equiv \text{Abdomen load} \leq 1 \text{ kN}, \\
 & \quad c_2(\mathbf{x}) \equiv V * C_u \leq 0.32 \text{ m/s}, \\
 & \quad c_3(\mathbf{x}) \equiv V * C_m \leq 0.32 \text{ m/s}, \\
 & \quad c_4(\mathbf{x}) \equiv V * C_l \leq 0.32 \text{ m/s}, \\
 & \quad c_5(\mathbf{x}) \equiv D_{ur} \text{ upper rib deflection} \leq 32 \text{ mm}, \\
 & \quad c_6(\mathbf{x}) \equiv D_{mr} \text{ middle rib deflection} \leq 32 \text{ mm}, \\
 & \quad c_7(\mathbf{x}) \equiv D_{lr} \text{ lower rib deflection} \leq 32 \text{ mm}, \\
 & \quad c_8(\mathbf{x}) \equiv F \text{ Pubic force} \leq 4 \text{ kN}, \\
 & \quad c_9(\mathbf{x}) \equiv \text{Vel. of V-Pillar at mid. pt.} \leq 9.9 \text{ mm/ms}, \\
 & \quad c_{10}(\mathbf{x}) \equiv \text{Vel. of front door at V-Pillar} \leq 15.7 \text{ mm/ms}, \\
 & \quad 0.5 \leq x_1 \leq 1.5, \quad 0.45 \leq x_2 \leq 1.35, \\
 & \quad 0.5 \leq x_3 \leq 1.5, \quad 0.5 \leq x_4 \leq 1.5, \\
 & \quad 0.875 \leq x_5 \leq 2.625, \quad 0.4 \leq x_6 \leq 1.2, \\
 & \quad 0.4 \leq x_7 \leq 1.2.
 \end{aligned} \tag{18}$$

There are 11 design variables, all related to the dimensions of a specific area in a car. The set can be divided into  $x = (x_1, \dots, x_7)$  for design variables and  $p = (p_8, \dots, p_{11})$  for uncertain parameters.

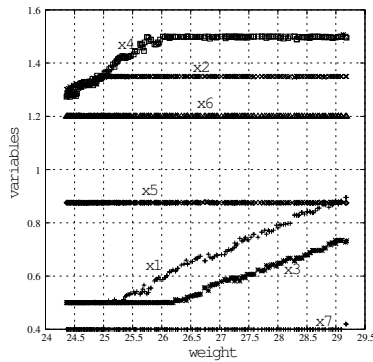


Fig. 7. Impact of the weight on the variables.

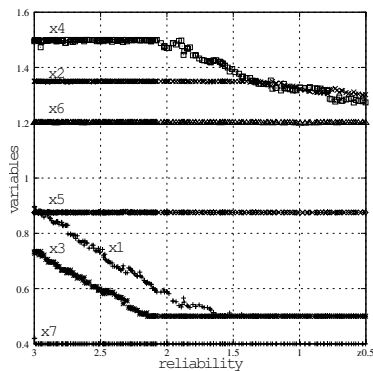


Fig. 8. Impact of the reliability on the variables.

Table II shows the angle between the constraints. The order of importance of the constraints depends on the chosen solutions and its distance to constraints. Every solution has its own order, although the order of constraints may be the

TABLE II  
CORRELATION MATRIX WITH ANGLE  $\rho$ .

	$c_8$	$c_2$	$c_3$	$c_7$	$c_9$	$c_{10}$	$c_4$	$c_5$	$c_1$	$c_6$
$c_8$	0	148	158	154	156	113	157	141	134	127
$c_2$	148	0	14	26	10	67	18	34	24	49
$c_3$	158	14	0	19	6	65	7	30	28	47
$c_7$	154	26	19	0	19	65	25	37	33	54
$c_9$	156	10	6	19	0	65	12	31	27	48
$c_{10}$	113	67	65	65	65	0	66	94	68	110
$c_4$	157	18	7	25	12	66	0	29	32	45
$c_5$	141	34	30	37	31	94	29	0	44	19
$c_1$	134	24	28	33	27	68	32	44	0	57
$c_6$	127	49	47	54	48	110	45	19	57	0

same for many solutions. In Fig. 9 we show the distance from the solution to the MPP. Constraint  $c_2$  and  $c_8$  are

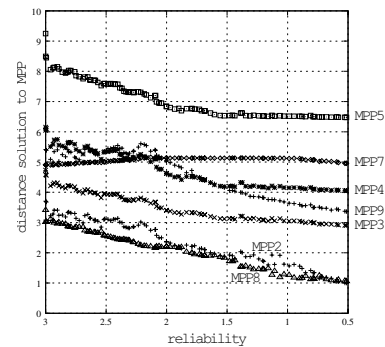


Fig. 9. Distance from the solution to the MPP.

close throughout the reliability spectrum. That means the solution gets centered between these two constraints and if one constraint gets closer to a solution than the others gets farther. This is to conform with the correlation matrix (shown in Table II) which shows an angle of 148 degrees between these two constraints. Thus, the displacement of the Pareto-optimal front into the feasible area gets comprehensible. For constraints  $c_2$  and  $c_9$ , it is another interplay. The angle between them is only 10 degrees, meaning that they are almost parallel and hence the one away from a solution does not have much effect on the reliability measure.

Fig. 10 shows the Pareto-optimal front obtained using three methodologies: (i) an earlier proposed one critical constraint approach which ignored all other constraints, (ii) our approach with Ditlevson bounds but all constraints are considered and (iii) our active constraint strategy in which only a few active constraints are considered. We restricted  $\beta$  to be between 0.5 (reliability of 69.14625%) and 3 (reliability of 99.865%). Like in the case of two-variable test problem shown earlier, the Pareto-optimal front using our approaches move deeper insider the search space due to a tighter computation of reliability. The earlier approach [10] used an optimistic reliability computation thereby resulting in an apparently better Pareto-optimal front. Interestingly, there is no

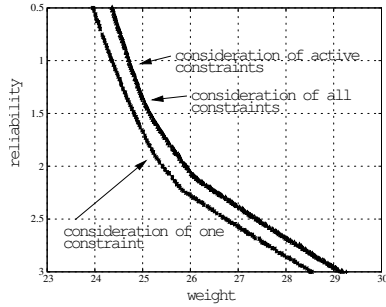


Fig. 10. Comparison between the proposed method where only active constraints are evaluated, where all constraints are evaluated, and where only one critical constraint is evaluated.

difference between the Pareto-optimal fronts obtained using both our approaches. However, our active constraint strategy requires only 32% of the total constraint calls compared to the all-constraint approach (refer to Table I). It is clear from Fig. 9 that only two constraints are critical in most reliable solutions. Thus, the active constraint strategy, in this problem, becomes very efficient in reducing the computational effort yet producing almost an identical accuracy in the result compared to the expensive all-constraint strategy.

#### V. MULTI-OBJECTIVE OPTIMIZATION FOR A SPECIFIED RELIABILITY

These problems are multi-objective in nature, but instead of finding the deterministic Pareto-optimal front, here our interest is to find a reliable front for a specified reliability. We use the active constraint strategy along with the RIA approach. If at a point, the computed reliability is smaller than the specified reliability, we declare the solution as an infeasible one. NSGA-II is employed for finding the reliable frontier. We illustrate the working of this procedure by solving a two-objective version of the car side-impact problem.

##### A. Two-Objective Car Side-Impact Problem

We use an additional objective of minimizing the average rib deflection, calculated by taking the average of three deflections  $g_5(x)$ ,  $g_6(x)$ ,  $g_7(x)$ . Figure 11 shows the reliable frontier for different reliability values using Ditlevson bounds (i) on all constraints and (ii) on active constraints only. Interestingly, for each specified reliability value, both all-constraint and active-constraint strategies have found an identical Pareto-optimal frontier. This usually happens when inactive constraints are far away from the optimal solutions. To investigate the distance of constraints from the optimal solution at different Pareto-optimal solutions, we plot the distance versus the weight objective at the solutions in Fig. 12. It is clear that only one constraint (the Pubic force constraint  $c_8$ ) is active and critical for all Pareto-optimal solutions in this problem. For better deflection solutions, the other constraints are more away from this constraint, thereby causing a negligible contribution in the computation of the

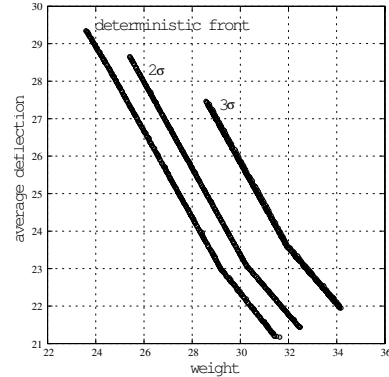


Fig. 11. Two-objective Pareto-optimal fronts for different specified reliabilities.

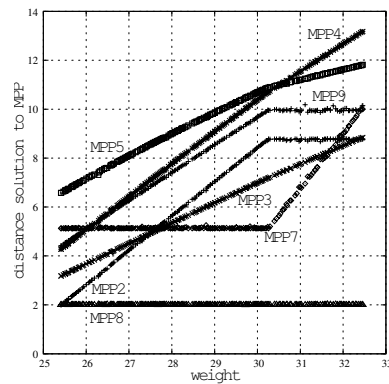


Fig. 12. Only one constraint affects the solution in a significant manner.

reliability of these solutions. Thus, both all-constraint and active-constraint strategies perform more or less the same. Also, identical reliable frontiers were obtained in the earlier study using the single critical constraint strategy [10] for the identical reason of having one critical constraint for each solution in this problem.

To investigate the properties of decision variables common to obtained Pareto-optimal solutions for a particular reliability (for  $\beta = 2$ ), we plot all seven variables against the weight objective in Fig. 13. Interestingly, six variables remains fixed in all solutions and for smaller weight solutions, a change in variable  $x_1$  changes one Pareto-optimal solution from another, while for smaller deflection solutions, a change in  $x_7$  changes one Pareto-optimal solution from another. Interestingly, with an increase in  $x_1$  the weight increases at the benefit of smaller deflection but when  $x_1$  reaches its upper limit, it cannot increase any further. To still make a trade-off between weight and deflection, the next thing to do is to increase  $x_7$  to obtain a better deflection solution. Such a knowledge deciphered from a problem is valuable to the designer or user and remains as an important by-product of evolutionary multi-objective optimization activities [18].



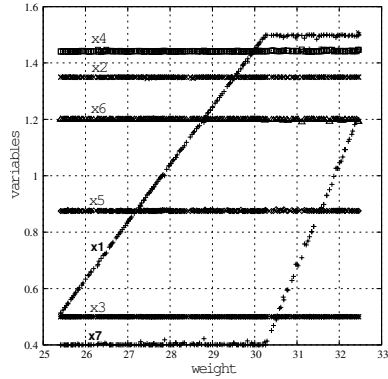


Fig. 13. Here the variables with  $\beta = 2$  are plotted against the weight (deflection problem).

## VI. CONCLUSIONS

In this paper, we have extended the one-critical constraint strategy adopted in an earlier study for finding reliable frontiers for handling uncertainties in decision variables and parameters. Based on Ditlevsen's probability computation, we have suggested two approaches: based on a composite success probability computation: (i) using all constraints and (ii) using only active constraints. On two types of multi-objective optimization problems involving test problems and a car side-impact design problem, we have shown that our proposed approaches produce a more accurate reliability estimate than the previous one-critical constraint strategy. Moreover, both of our approaches produce more or less identical frontiers, except that the active constraint strategy is computationally cheaper than the all-constraint strategy. Based on all these comparative studies, we recommend further and immediate use of active constraint strategy to more complex robust and reliability-based optimization problems.

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## REFERENCES

- [1] AO. Ditlevsen, *Narrow reliability bounds for structural system*, J. Struct. Mech. 4 (1) 431-439, 1979.
- [2] M. Rosenblatt, *Remarks on a multivariate transformation*, Ann Math.Stat., 23 470-472, 1952.
- [3] AM. Hasofer, NC. Lind, *An exact and invariant first order reliability format*, J Eng Mech Div ASCE, 100(EM1):111-121, 1974.
- [4] X. Du, W. Chen, *A Most Probable Point Based Method for Uncertainty Analysis*, Journal of Design and Manufacturing Automation, 1, pp. 47-66, 2001.
- [5] M. S. Eldred, B. J. Bichonz, B. M. Adams, *Overview of Reliability Analysis and Design Capabilities in DAKOTA*, Conference Paper, NSF Workshop on Reliable Engineering Computing (REC 2006), Savannah, GA, February 2006.
- [6] K. Deb, *Multi-objective optimization using evolutionary algorithms*, Chichester, UK: Wiley, 2001.
- [7] H. Agarwal, *Reliability based design optimization: Formulations and Methodologies*, PhD thesis, University of Notre Dame, 2004.
- [8] L. Gu, R. J. Yang, C. H. Tho, L. Makowski, O. Faruque, and Y. Li, *Optimization and robustness for crashworthiness of side impact*, International Journal of Vehicle Design, 26(4), 2001.

- [9] K. Deb, S. Agrawal, A. Pratap, and T. Meyarivan, *A fast and elitist multi-objective genetic algorithm: NSGA-II*, IEEE Transactions on Evolutionary Computation, 6(2):182-197, 2002.
- [10] K. Deb, D. Padmanabhan, S. Gupta, A. K. and Mall, *Handling Uncertainties Through Reliability-Based Optimization Using Evolutionary Algorithms*, Fourth International Conference on Evolutionary Multi-Criterion Optimization (EMO 2007) pp. 66-88 Lecture Notes on Computer Science 4403, 2007.
- [11] O. Ditlevsen, H. O. Madsen, *Structural Reliability Methods*, New York: Wiley, 1996.
- [12] HO. Madsen, S. Krenk, NC. Lind, *Methods of structural safety*, Englewood Cliffs (NJ): Prentice-Hall, Inc., 1986.
- [13] R. Rackwitz, *Reliability analysis: A review and some perspectives*, Structural Safety 23(4):365-395, 2001.
- [14] C.A. Cornell, *Bounds on the reliability of structural systems*, J. Struct. Div., ASCE, 93 (ST1) 171-200, 1967.
- [15] K. Ramachandran, M. Baker *New reliability bound for series systems*, In: Konishi I, Ang AH-S, Shinozuka M, editors. Proc. ICOSSAR '85, Kobe; p. 157-169 [Vol. 1], 1985
- [16] J. H. Holland, *Adaptation in Natural and Artificial Systems*, Ann Arbor, MI: MIT Press, 1975.
- [17] D. E. Goldberg, *Genetic Algorithms for Search, Optimization, and Machine Learning*, Reading, MA: Addison-Wesley, 1989.
- [18] K. Deb, A. Srinivasan *Innovation: Innovating design principles through optimization* Proc. of the Genetic and Evolutionary Computation Conference (GECCO-2006), New York: The ACM Press, p. 1629-1636, 2006
- [19] Henrik O. Madsen *First Order vs. Second Order Reliability Analysis of Series Structures* Structural Safety, 2 207-214, 1985

## APPENDIX

$$\begin{aligned}
 f(\mathbf{x}) &= 1.98 + 4.9x_1 + 6.67x_2 + 6.98x_3 + 4.01x_4 + 1.78x_5 \\
 &\quad + 0.00001x_6 + 2.73x_7, \\
 g_1(\mathbf{x}) &= 1.16 - 0.3717x_2x_4 - 0.00931x_2x_{10} - 0.484x_3x_9 \\
 &\quad + 0.01343x_6x_{10}, \\
 g_2(\mathbf{x}) &= 0.261 - 0.0159x_1x_2 - 0.188x_1x_8 - 0.019x_2x_7 \\
 &\quad + 0.0144x_3x_5 + 0.87570.001x_5x_{10} + 0.08045x_6x_9 \\
 &\quad + 0.00139x_8x_{11} + 1.575(10^{-6})x_{10}x_{11}, \\
 g_3(\mathbf{x}) &= 0.214 + 0.00817x_5 - 0.131x_1x_8 - 0.0704x_1x_9 \\
 &\quad + 0.03099x_2x_6 - 0.018x_2x_7 + 0.0208x_3x_8 + 0.121x_3x_9 \\
 &\quad - 0.00364x_5x_6 + 0.0007715x_5x_{10} - 0.0005354x_6x_{10} \\
 &\quad + 0.00121x_8x_{11} + 0.00184x_9x_{10} - 0.018x_2x_2, \\
 g_4(\mathbf{x}) &= 0.74 - 0.61x_2 - 0.163x_3x_8 + 0.001232x_3x_{10} \\
 &\quad - 0.166x_7x_9 + 0.227x_2x_2, \\
 g_5(\mathbf{x}) &= 28.98 + 3.818x_3 - 4.2x_1x_2 + 0.0207x_5x_{10} \\
 &\quad + 6.63x_6x_9 - 7.77x_7x_8 + 0.32x_9x_{10}, \\
 g_6(\mathbf{x}) &= 33.86 + 2.95x_3 + 0.1792x_{10} - 5.057x_1x_2 - 11x_2x_8 \\
 &\quad - 0.0215x_5x_{10} - 9.98x_7x_8 + 22x_8x_9, \\
 g_7(\mathbf{x}) &= 46.36 - 9.9x_2 - 12.9x_1x_8 + 0.1107x_3x_{10}, \\
 g_8(\mathbf{x}) &= 4.72 - 0.5x_4 - 0.19x_2x_3 - 0.0122x_4x_{10} \\
 &\quad + 0.009325x_6x_{10} + 0.000191x_{11}x_{11}, \\
 g_9(\mathbf{x}) &= 10.58 - 0.674x_1x_2 - 1.95x_2x_8 + 0.02054x_3x_{10} \\
 &\quad - 0.0198x_4x_{10} + 0.028x_6x_{10}, \\
 g_{10}(\mathbf{x}) &= 16.45 - 0.489x_3x_7 - 0.843x_5x_6 + 0.0432x_9x_{10} \\
 &\quad - 0.0556x_9x_{11} - 0.000786x_{11}x_{11}.
 \end{aligned}$$