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# Thermal Protection System (TPS) Design and the Relationship to Atmospheric Entry Environments

By

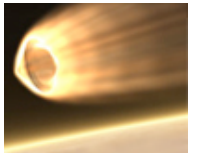
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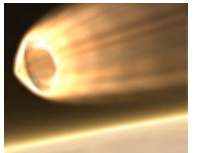
6<sup>th</sup> International Planetary Probe Workshop, Atlanta, Georgia  
Short Course on Extreme Environments Technologies

06/21-22  
2008

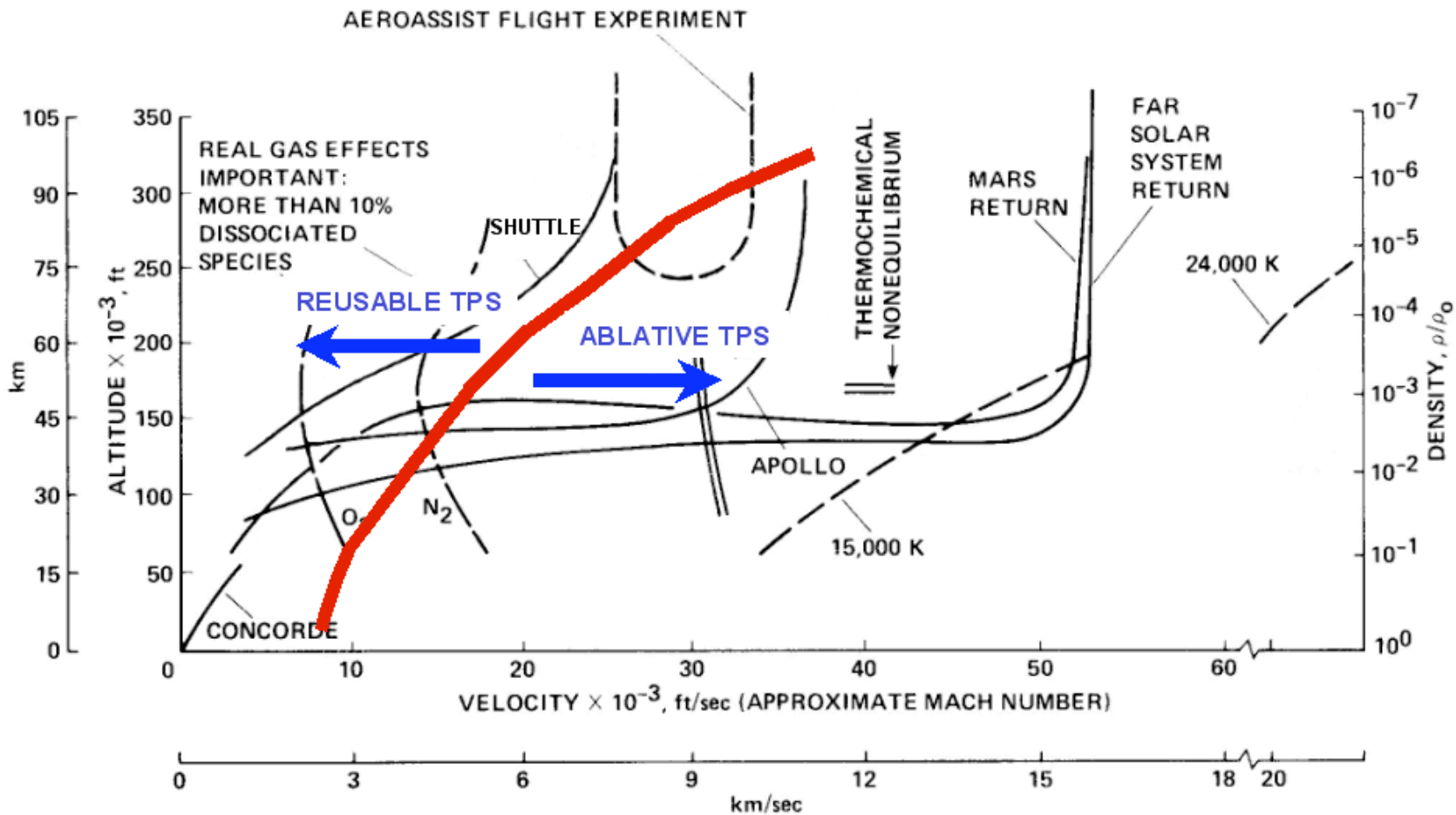
# Agenda

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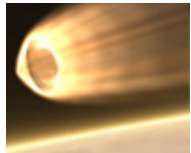
- Why Ablative TPS?
- What is ablative TPS?
- Entry environments for planetary probes
  - Key Physical Challenges
  - Sample Entry Environments
- TPS Selection
  - Failure modes
  - Heat flux, pressure, atmospheric composition
  - Heat load
- TPS Testing
- Summary



# Why Ablative TPS?

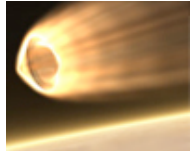
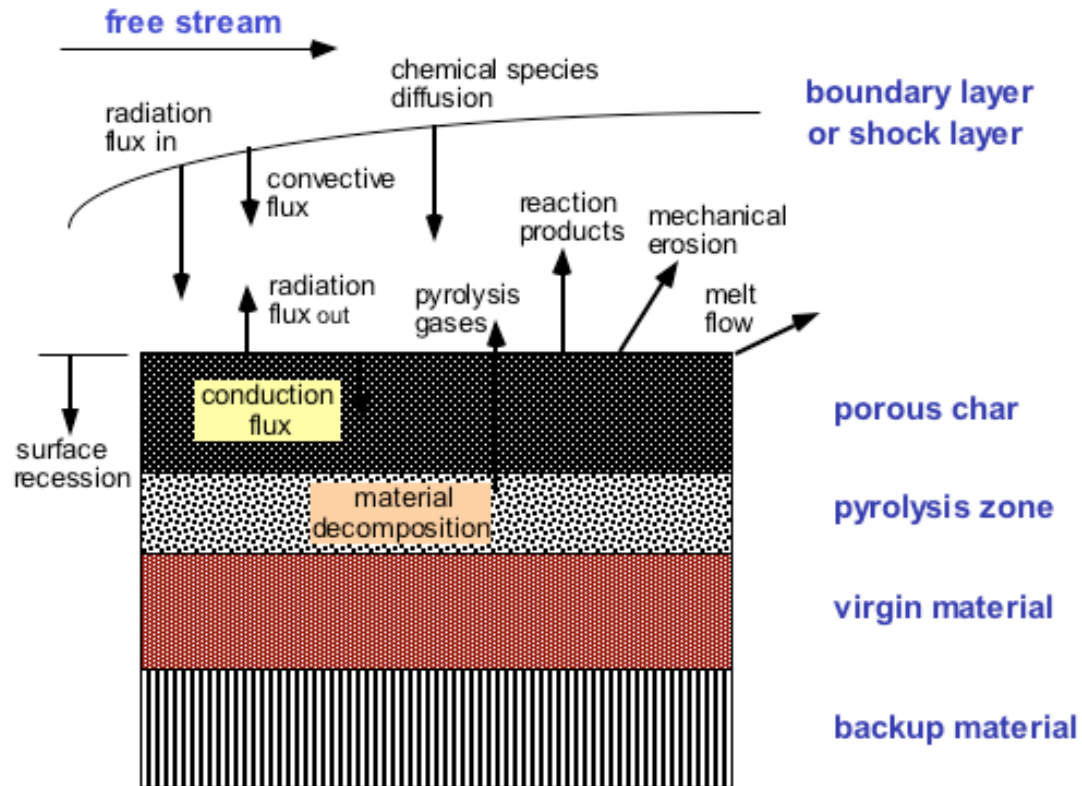


From John Howe, "Hypervelocity Atmospheric Flight: Real Gas Flow Fields,"  
 NASA TM 101055, 1989



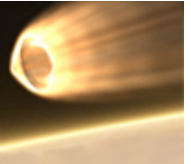
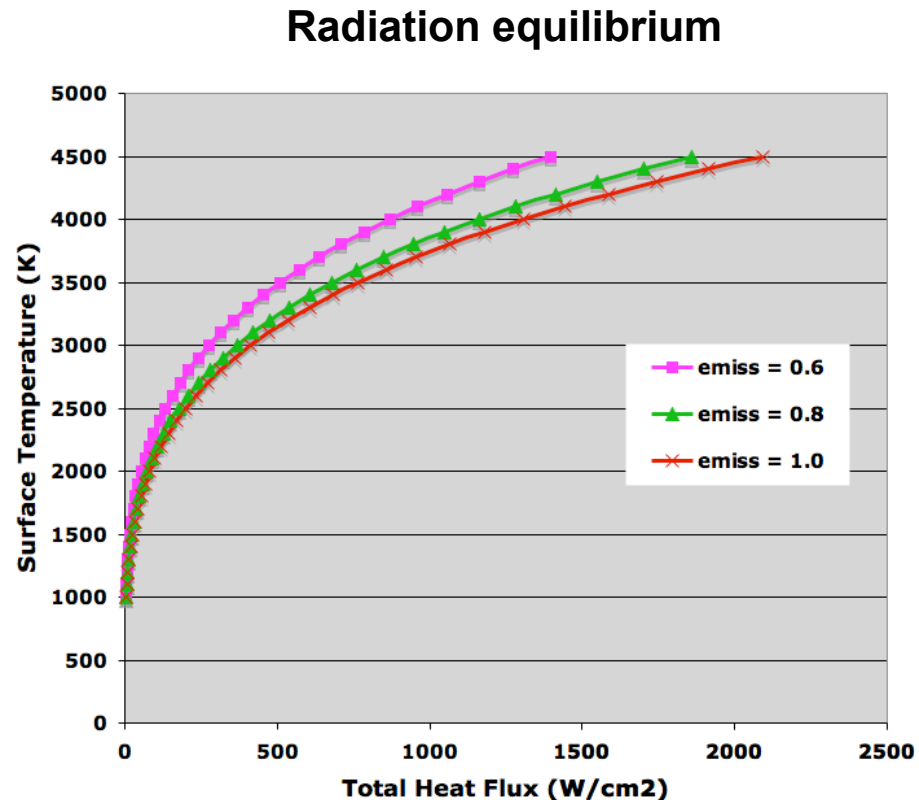
# What is ablative TPS?

## Energy management through material consumption



# How hot is *hot*?

- All materials are (potentially) ablative materials
  - If exposed to typical entry heating, any material will get to temperatures where it will either melt, vaporize, oxidize, sublime, etc.
- For comparison, the temperature of the sun is  $\approx 6000$  K
- The gas near the heated TPS surface (behind the shock) is at much *higher* temperature



# Aerothermodynamics of Planetary Entry

## Planetary Atmospheres

Mars&Venus: CO<sub>2</sub>/N<sub>2</sub>  
 Titan: N<sub>2</sub>/CH<sub>4</sub>  
 Giants: H<sub>2</sub>/He  
 Earth: N<sub>2</sub>/O<sub>2</sub>

## Hot Shock Layer (up to 20000 K)

Thermochemical nonequilibrium, Ionization, Radiation

## Boundary Layer (2-6000 K)

Turbulence, Ablation product mixing, Radiation blockage

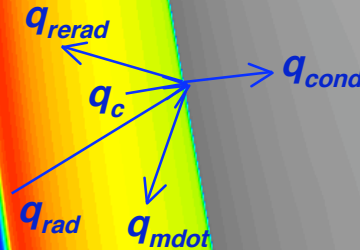
## "Cool" Surface (2-3000 K)

Surface kinetics, Ablation

## Afterbody Flow

Unsteady non-continuum vortical flowfield

## Surface Energy Balance

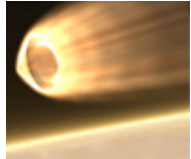


**Design Problem: Minimize conduction into vehicle to minimize TPS mass/risk**

$$q_{cond} = q_c + q_{rad} - q_{rerad} - q_{mdot}$$

Incident Aeroheating

Material Response



# Energy Loss over Time

- **Reentry generates a lot of energy:**

	Energy (MJ)		
	MER	Genesis	Galileo Probe
Atmospheric Interface	1260	1414	$1.07 \times 10^6$
Parachute Deploy	105 (92%)	84 (94%)	$1.28 \times 10^5$ (88%)
End	0.2 (99.98%)	0.9 (99.94%)	18 (99.998%)

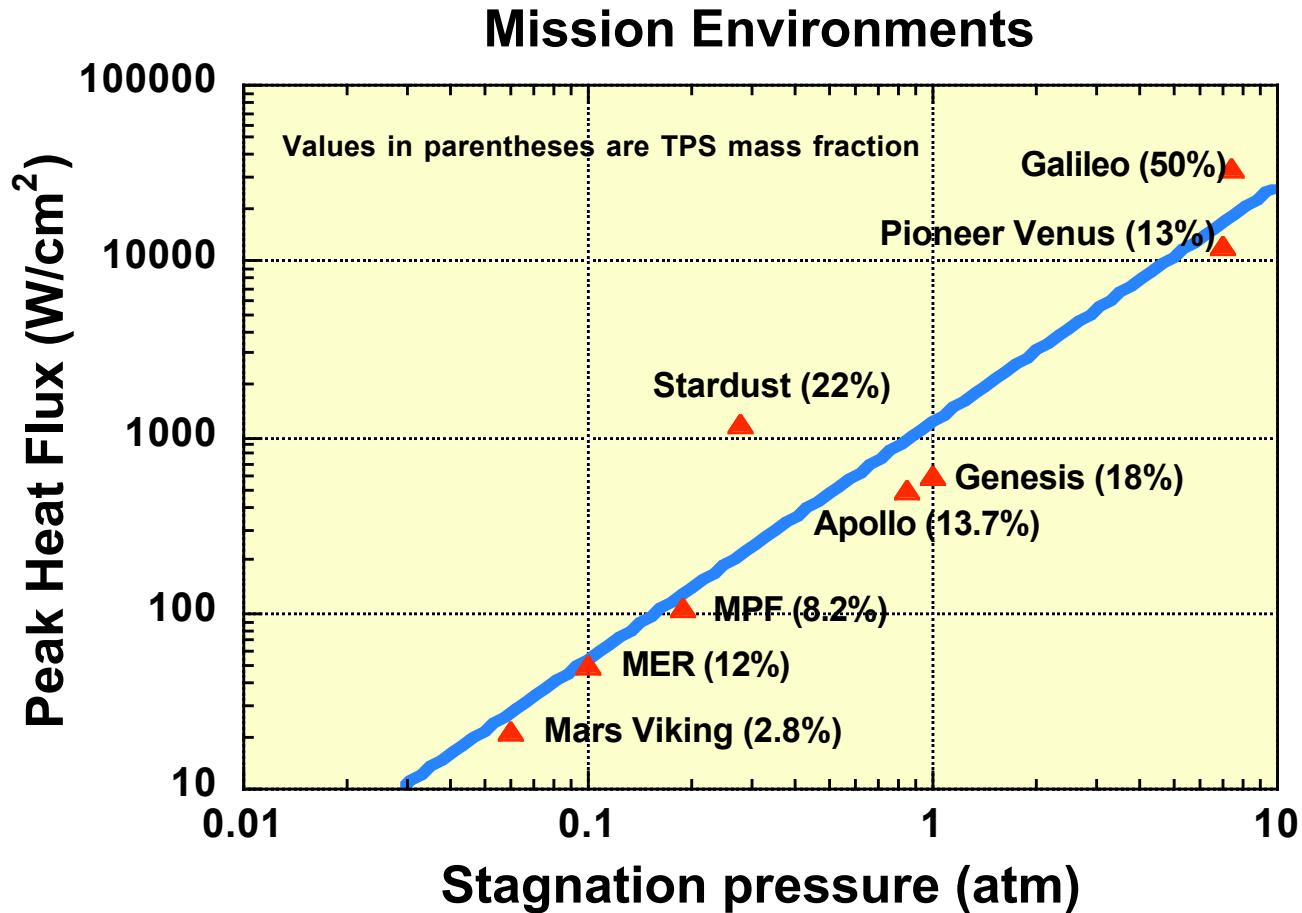
- **Fortunately, most of this energy does not reach the surface**
  - >90% of total energy is dissipated via the bow shock heating the atmospheric gases

## Stardust Capsule

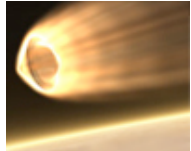




# Broad Range of Entry Environments



**NASA entry probes have successfully survived entry environments ranging from the very mild (Mars Viking ~25 W/cm<sup>2</sup> and 0.05 atm.) to the extreme (Galileo ~30,000W/cm<sup>2</sup> and 7 atm.)**





# Representative Environments

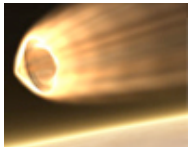
Planned missions will require TPS able to survive a broad range of entry conditions

## Direct Entry

	Venus	Earth	Mars	Jupiter	Saturn	Titan	Neptune
q (kW/cm <sup>2</sup> )	2-7	0.6-2	0.05-0.5	30-60	2-5	0.05-0.25	2-10
Q (kJ/cm <sup>2</sup> )	10-20	10-40	5-10	200-500	50-150	2-6	100-400
p (atm)	10	0.25-0.5	0.25-0.5	5-10	0.5-5	0.25	0.5-5

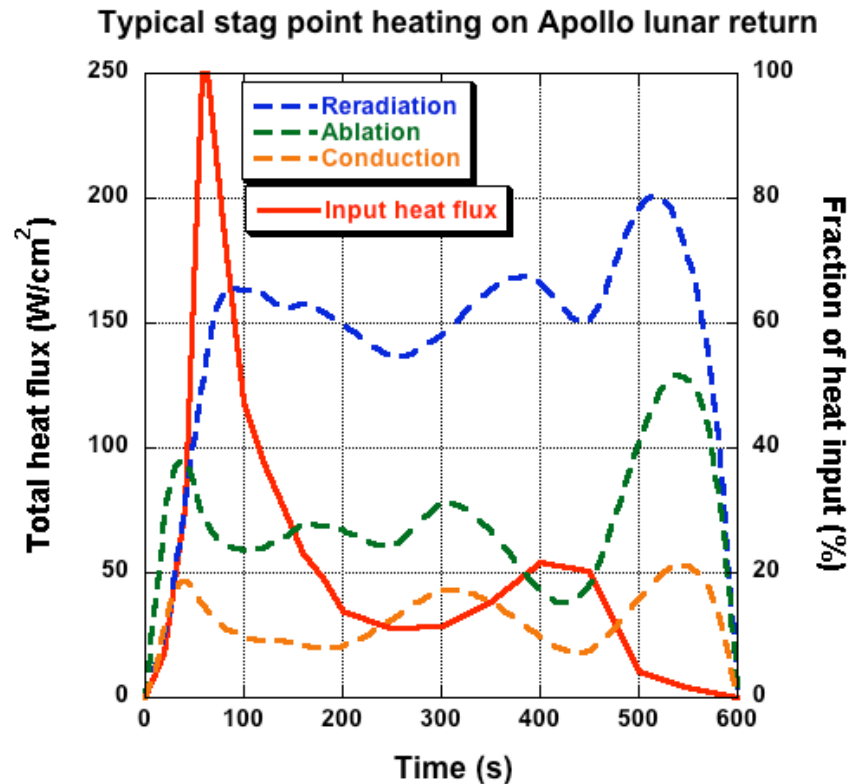
## Aerocapture

	Venus	Earth	Mars	Jupiter	Saturn	Titan	Neptune
q (kW/cm <sup>2</sup> )	1-2	0.5-1	0.05-0.3	N/A	3-10	0.05-0.15	3-10
Q (kJ/cm <sup>2</sup> )	40-80	20-50	10-30	N/A	200-500	5-12	500-2000
p (atm)	0.3	0.25	0.25	N/A	0.5-1	0.1	0.5-1.5

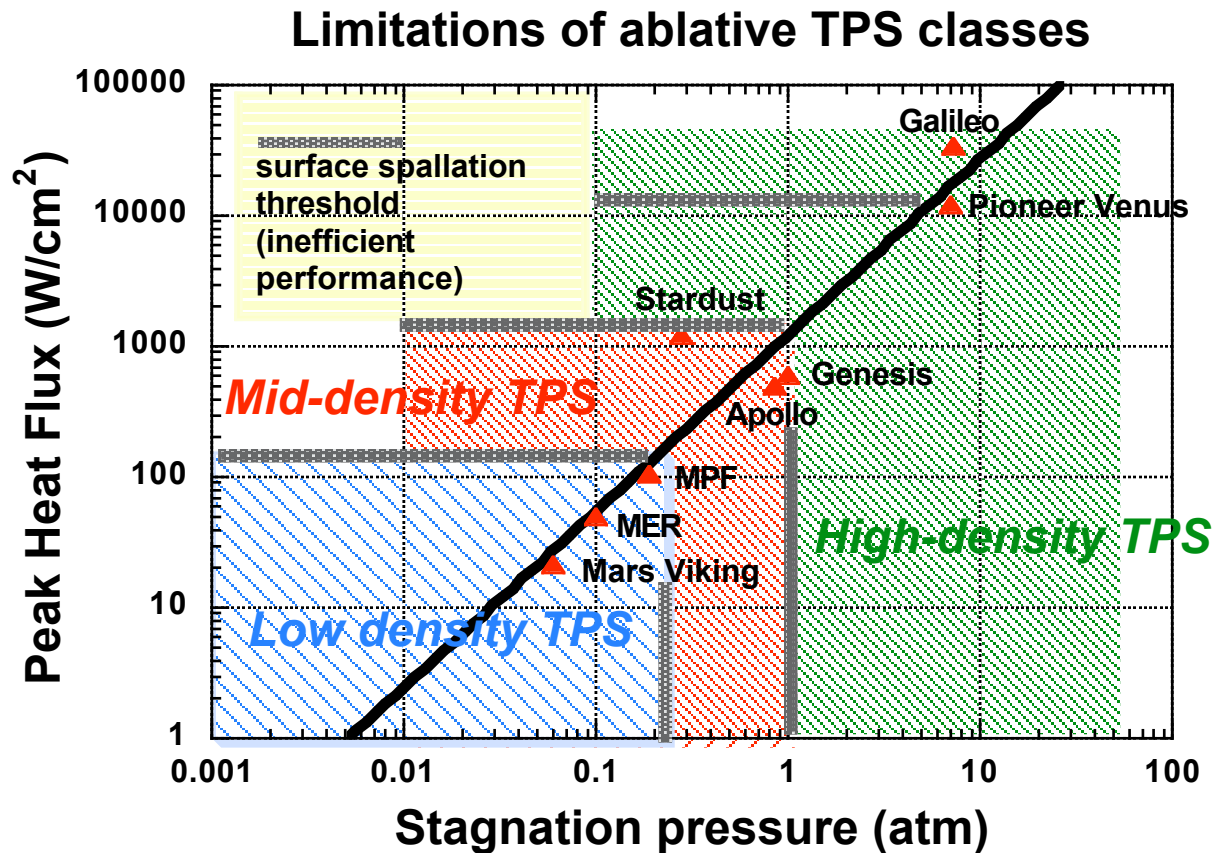


# How do ablative materials manage energy?

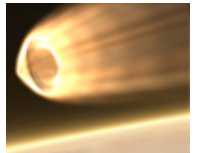
- Surface reradiation is the most effective energy rejection mechanism (60-80%)
  - Carbon or materials that form carbonaceous chars are desirable as they attain very high surface temperatures and have high emissivity
  - Ablation, even in the presence of exothermic oxidation, consumes energy (20-40%)
  - Only a small fraction of the incident heating is conducted into the TPS material (10-20%)



# Material Performance Limits



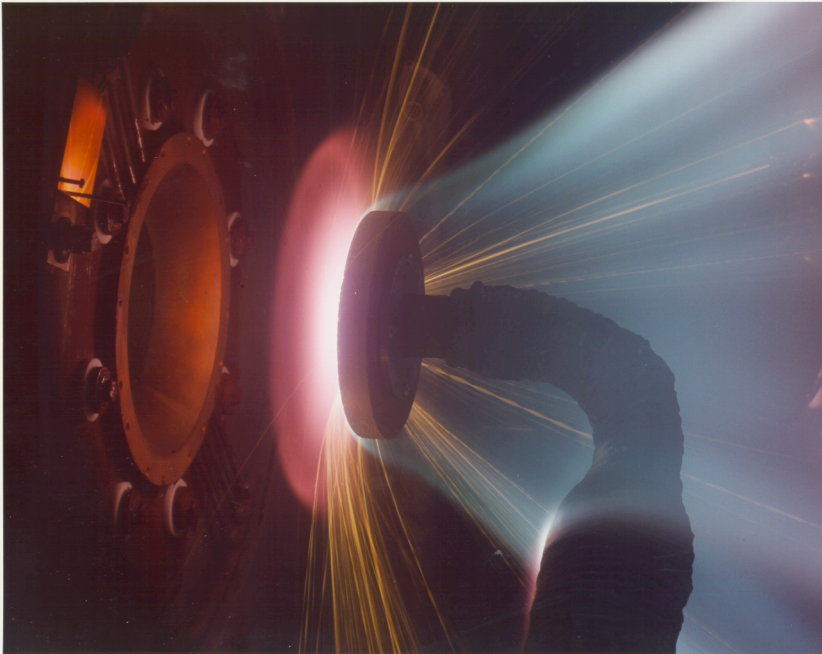
**Optimal performance regime is balanced between ablative and insulation efficiency. When material is used outside of optimal zone, inefficient performance leads to non-minimal mass fraction.**



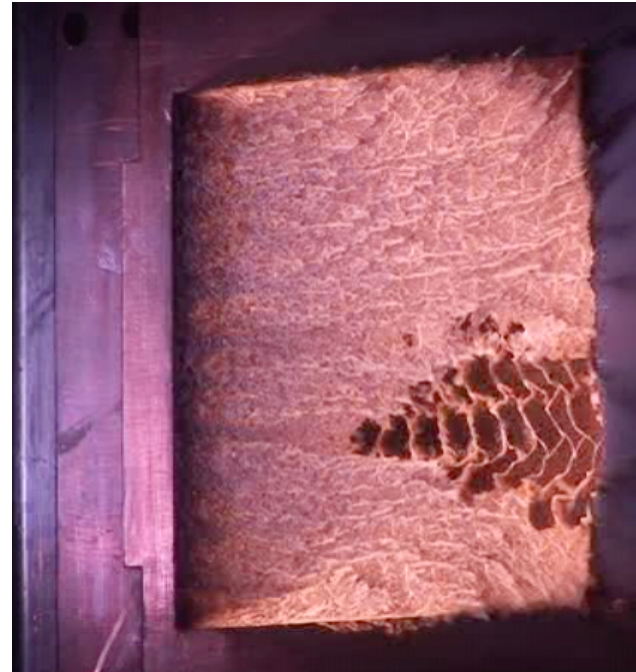
# Example failure modes

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## Spallation



## Loss of liquid layer



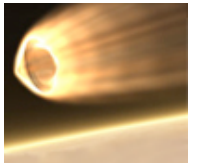
# TPS Selection

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- Objective is *minimum* TPS mass with reliable performance
  - *Reliable performance* implies that material failure modes are well understood and environmental conditions leading to failure will not be encountered (or approached) for the selected mission
  - Low density materials are (typically) better insulators than high density materials
  - High density materials are (typically) better ablators than low density materials
- Ablation is good - it absorbs energy
  - Too much ablation may not be good if it leads to shape change that influences aerodynamics
- TPS selection involves a balance between ablation and insulation performance and manufacturability
  - Select the lowest density material that can handle\* the range of environmental conditions (heat flux, pressure, shear, atmosphere)
  - Material should provide effective insulation for imposed heat load
  - Procedures for material fabrication, installation, inspection, etc., should be established and, preferably, demonstrated

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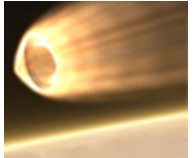
\*Material should have demonstrated reliability at extreme conditions of interest



# TPS Testing

## Arc Plasma Facilities

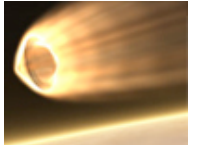
- Have been used for over 40 years to study TPS material performance
  - Two classes:
    - Low enthalpy, high pressure, high heat flux (high  $\beta$  vehicles)
    - High enthalpy, low pressure, low-moderate heat flux (low  $\beta$  vehicles; lifting entry, aeroassist, aerocapture, planetary entry, etc.)
- Significant flexibility
  - Pressure: nozzle geometry, test article design, gas mass flow rate
  - Enthalpy: gas mass flow rate, electrical power
  - Gas composition: most facilities operate with air, but tests have been conducted with  $N_2$ ,  $CO_2$ ,  $H_2/He$ , etc. gas streams
- Amenable to sophisticated (*non-intrusive*) diagnostics
  - Surface visibility (film or video), surface pyrometry, PLIF, emission spectroscopy, etc.
- **Capability to *simultaneously* simulate conditions representative of flight (e.g.,  $H, \dot{q}, p$ ) is rare.**
  - Requires strategic test planning
  - Typically, cannot simulate time-varying conditions (trajectories)



# TPS Testing (concluded)

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- Inability to simulate the actual flight environment in arc jets results in significant uncertainties in ground test to flight traceability
- Well-designed ground-test program should cover the *range of conditions* anticipated in flight
  - Typically, **ground tests cannot simulate some aspects of the flight environment**
    - Turbulent flow
    - High shear
    - High pressure gradient
    - Combined convective/radiative heating
- ***Mechanism-based modeling*** allows extrapolation with some confidence
  - Identification of surface response mechanisms and development of high fidelity model significantly reduces performance uncertainties in flight
  - Remaining uncertainties can only be addressed through flight test with instrumented TPS





# Summary & Conclusions

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- Atmospheric entry qualifies as an *extreme environment*
- Selection of an ablative TPS for a given mission is governed by the severity of the entry environment
  - High density materials minimize ablation but result in a heavy TPS
  - Low density materials minimize insulation thickness and result in a light TPS
  - Optimum material (among those available) is the lowest density material that does not produce excessive ablation while performance is far from failure thresholds
- Arc plasma facilities produce the best simulation of the entry environment
  - Actual flight conditions (typically) cannot be simulated
  - Requires testing over broad range of conditions to understand performance mechanisms
  - Mechanism (physics- and chemistry-) based models enable extrapolation from ground test to flight
- Ablative materials have been successfully used for thermal protection for 50 years and will continue to be used in the foreseeable future

