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Max Lesaffre, Salma Farahi, A.C. Boccara, François Ramaz, Michel Gross

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Theoretical study of Acousto-optical coherence tomography using random phase jumps on US and light

M. Lesaffre[1,2], S. Farahi[1], A.C. Boccara[1], F. Ramaz[1] and M. Gross[2,3,*]

[1]Institut Langevin, ESPCI ParisTech, CNRS UMR 7587,
10 rue Vauquelin F-75231 Paris Cedex 05.
[2]Laboratoire Kastler-Brossel de l'ENS, UMR 8552 (ENS, CNRS, UMPC),
24 rue Lhomond F-75231 Paris Cedex 05
[4]Laboratoire Charles Coulomb UMR 5221 CNRS-UM2 Université Montpellier
II place Eugène Bataillon 34095 Montpellier
[*]Corresponding author: gross@lkb.ens.fr

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Abstract

Acousto-Optical Coherence Tomography (AOCT) is variant of Acousto Optic Imaging (called also ultrasonic modulation imaging) that makes possible to get z resolution with acoustic and optic Continuous Wave (CW) beams. We describe here theoretically the AOCT effect, and we show that the Acousto Optic "tagged photons" remains coherent if they are generated within a specific z region of the sample. We quantify the z selectivity for both the "tagged photon" field, and for the M. Lesaffre et al. photorefractive signal.

OCIS codes : 170.3660, 110.7050, 110.7170, 160.5320, 170.3880

1 Introduction

Acousto-optic imaging (AOI) [1, 2, 3] is a technique that couples ultrasounds and light in order to reveal the local optical contrast of absorbing and/or scattering objects embedded within thick and highly scattering media, like human breast tissues.

First experiments used fast single detectors to record the modulation of the optical signal at the US frequency [4, 5, 6, 1, 7]. But, since the phase of the modulation is different for each grain of speckle, the detector can only process one grain of speckle. To increase the optical etendue of detection, Leveque et al. [8] have developed a camera detection technique that processes many speckles in parallel. This technique has been pulled to the photon shot noise limit by Gross et al. [9] using a holographic heterodyne technique [10] able to detect photons with optimal sensitivity [11, 12]. Since the US attenuation is low in tissues, the tagged photons are generated along the US propagation z axis with a nearly constant rate. This means that in a continuous regime of the US, the AO techniques give nearly no information on the location of the embedded objects along the z axis. To get such z information, Wang et al. [13], have developed a US frequency chirp technique with a single detector, which has been extended to camera detection [14, 15]. Unfortunately, these chirp techniques

cannot be used in living tissues, because the phase of light decorrelates very fast in them, since half frequency linewidth of light that travels through 4 cm of living breast tissue is about 1.5 kHz [16]. This phase decorrelation drastically lowers the detection efficiency, since the detection bandwidth is approximately equal to the camera frame rate. The bandwidth is then much narrower than the width of the scattered photon frequency spectrum, and most of the tagged photons are undetected. It is still possible to increase the detection bandwidth by using a faster camera, but in such systems this generally means that a smaller number of pixels should be used, and the optical etendue of detection decreases accordingly. To perform selective detection of the tagged photons with high optical etendue, narrow band incoherent detection techniques have been proposed. For example, Li et al. select the tagged photon by spectral holeburning [17, 18], while Rousseau uses a confocal Fabry-Perot interferometer [19]. This last experiment [19] benefits from a powerful long pulse laser, whose duration (0.5 ms) matches the 1.5 kHz signal bandwidth. Another way to get a detection bandwidth comparable with the signal bandwidth while keeping a large optical etendue, detection schemes involving photorefractive (PR) crystals have been proposed. Murray et al. [20, 21] use a PR crystal sensitive at 532 nm to select the untagged photons, which are detected by a single avalanche photodiode . In this case, the weight of the tagged photon signal is measured indirectly by using the conservation law of the total number of photons (tagged + untagged) [22]. Ramaz et al. selectively detect either the tagged or the untagged photons [23]. The Ramaz technique is also able to measure in situ the photorefractive writing time (τ_{PR}), which characterizes the detection frequency bandwidth [24].

In order to get information on the location of the object along the z axis, acoustic pulses can be used. The method has been extensively used both with single detectors [25, 26], cameras [3], PR crystals without [20, 21, 27, 28], or with long pulse laser [29]. Nevertheless, reaching a millimetric resolution with US pulses requires a typical duty cycle of 1%, corresponding to the exploration length within the sample (~ 10 cm) and the desired resolution (~ 1 mm). This

is problematic regarding the very small quantity of light that emerges from a clinical sample, since weak duty cycle yields low signal and poor Signal-to-Noise Ratio (SNR). When US pulses are used with photodiode detection, the SNR becomes lower, since fast photodetectors mean larger electronic noise. In a recent publication, Lesaffre et al. [30] overcome the duty cycle problem, and get z resolution with CW light and ultrasound by applying a random phase modulation on both the optical illumination and US beam. This so called Acousto-Optical Coherence Tomography (AOCT) technique is then demonstrated with photorefractive detection of the tagged photons.

Whatever the method used to obtain an axial resolution, the acousto-optic signal is sensitive to the quantity of photons tagged by the ultrasound : as shown in many previous studies, a strong absorber ("zero" transmission") within the US field will induce an important drop on the signal [30, 1, 11, 18, 19, 22]. It has been shown more recently that a small "quasi-transparent" inclusion having a scattering coefficient ($\mu'_s = 10$ cm^{-1}) different from the host matrix ($\mu'_s = 7$ cm^{-1}) can give a contrast in the acousto-optic signal [31]. In both cases, and to our knowledge, no quantitative measurements of this contrast have been performed as a function of the absorption coefficient nor the transport mean free path length l^*.

In the present paper, we will describe the AOCT effect theoretically. We show that the tagged photons remain coherent if they are generated within a specific z region of the sample. We will quantify the z selectivity for both the tagged photon field, and for the tagged photon photorefractive signal as detected by Lesaffre et al. [30]. The theoretical results we get here will be compared with experiment in another publication.

2 Theory of the Acousto Optic Coherent Tomography (AOCT).

The theoretical description of the Acousto Optic Coherent Tomography cannot be simply extrapolated from the theory made previously [22] to describe the
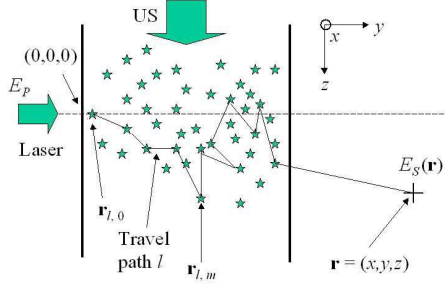
Figure 1: Light scattering along the travel path l, which involves scattering event located in $\mathbf{r}_{l,m}$, where m is the scattering event index.

photorefractive detection of the UltraSound Modulated photons (USM). Since we make tomography, we cannot consider that the USM photons are globally generated by the modulation of the length of a travel path. We must make a finer analysis by describing how the USM photons are locally generated within each specific region of the sample.

2.1 The generation of the "tagged photons"

Let us call E_P and E_S the fields coming into and out of the sample. Consider the point (x, y) located after the sample output interface. E_S is a quasi monochromatic wave at the frequency ω_0 of the incoming laser. Let's introduce the complex field amplitude $\underline{E}_P$ and $\underline{E}_S$ defined as:

$$E_P(t) = \Re\left\{\underline{E}_P e^{j\omega_0 t}\right\} \tag{1}$$

$$E_S(t) = \Re\left\{\underline{E}_S e^{j\omega_0 t}\right\} \tag{2}$$

where $\Re$ is the real part operator. E_S results from the sum (or the interference) of the field components $E_{S,l}$ scattered through the sample along many travel paths l from input plane ($z = 0$) to the detector. Moreover, as illustrated by Fig.1, each travel path l can be decomposed in a succession of scattering events (l, m)

located in $\mathbf{r}_{l,m}$ where m is the scattering events index.

$$\begin{aligned} E_S(t) &= \sum_l E_{S,l}(t) \tag{3}\\ &= \Re\left\{\sum_l a\,\underline{E}_P\,e^{j\omega_0(t - s_l/c)}\right\} \end{aligned}$$

where l is the travel path index, and s_l the corresponding effective travel path length. The length s_l is the product of the travel path length by the medium refractive index n. To simplify the discussion we consider that the field amplitude a is the same for all the travel paths. All travel paths have the same weight $a\underline{E}_P$, but different field phases: $e^{-j\,\omega_0 s_l/c} \equiv e^{-j\,2\pi s_l/\lambda}$. Since the travel path lengthes are large with respect to the optical wavelength λ, the factor $e^{-j2\pi s_l/\lambda}$ is random. Summing over the travel paths, one gets a speckle outgoing field.

2.1.1 The ultrasonic field of pressure

Let us now apply a CW (Continuous Wave) ultrasonic (US) wave to the system by using an ultrasonic piezoelectric (PZT) device. The PZT transducer excitation voltage is:

$$U_{PZT}(t) = \Re\left\{\underline{U}_{PZT}\,e^{j\omega_{US}t}\right\} \tag{4}$$

where $\underline{U}_{PZT}$ is the complex amplitude of U_{PZT}. Like in experiments, we consider here linear conditions where the acoustic pressure P_{US} is proportional to the excitation voltage. By this way, we get in any point $\mathbf{r}$ of the sample:

$$P_{US}(\mathbf{r}, t) = A(\mathbf{r})\,U_{PZT}\,(t - z/c_{US}) \tag{5}$$

where c_{US} is the sound velocity in the sample, and z/c_{US} the time delay from the US emission point (the PZT) to the zone of coordinate z that is considered. Let us introduce the US pressure complex amplitude $\underline{P}_{US}$:

$$P_{US}(\mathbf{r}, t) = \Re\left\{\underline{P}_{US}(\mathbf{r})\,e^{j\omega_{US}t}\right\} \tag{6}$$

with

$$\underline{P}_{US}(\mathbf{r}) = A(\mathbf{r})\,\underline{U}_{PZT}\,e^{-j\omega_{US}z/c_{US}} \tag{7}$$

The pressure $\underline{P}_{US}$ is periodic with respect to the US propagation axis, the period being $\lambda_{US} = 2\pi c_{US}/\omega_{US}$.

2.1.2 The acousto optic modulation

Because of the US beam the scatterers vibrate. Moreover, the sample refractive index is modulated. These two effects yield a modulation of the length s_l of the travel paths of the photons that are scattered by the medium (where l is the travel path index) at the US frequency ω_{US}:

$$s_l(t) = s_{l,0} - \Re\left\{\underline{\delta s_l}\, e^{j\omega_{US}\,t}\right\} \quad (8)$$

where $\underline{\delta s_l}$ is the complex amplitude of the modulation of the travel path l. We get from Eq.3:

$$E_S(t) = \Re\sum_l a\,\underline{E_P}\,e^{j\,\omega_0(t-s_{l,0}/c)} \quad (9)$$
$$\times \exp\left[j\,\frac{\omega_0}{c}\Re\left\{\underline{\delta s_l}\,e^{j\omega_{US}\,t}\right\}\right]$$

Let us introduce the complex amplitude $\underline{\delta s}_{l,m}$ of the mth scatterer contribution to the travel path modulation, whose modulus and phase are $\beta_{l,m}$ and $\phi_{l,m}$ respectively.

$$\underline{\delta s_l} = \sum_m \underline{\delta s}_{l,m} = \sum_m \beta_{l,m} e^{j\phi_{l,m}} \quad (10)$$

The sample outgoing field $E_S(t)$ is then modulated by the US at frequency ω_{US}.

$$E_S(t) = a\,\Re\sum_l \underline{E_P}\,e^{j\,\omega_0(t-s_{l,0}/c)} \quad (11)$$
$$\times \exp\left[j\,\frac{\omega_0}{c}\sum_m \Re\left[\underline{\delta s}_{l,m} e^{j\omega_{US}t}\right]\right]$$

2.1.3 The tagging of the scattered photons

In typical experiments, the vibration amplitude is much lower than the optical wavelength $\lambda = 2\pi c/\omega_0$: for example, the vibration amplitude is 60 nm for 1 MPa acoustic pressure at $\omega_{US} = 2$ MHz. We can then make the hypothesis of a weak acousto optic modulation:

$$\frac{\omega_0}{c}\sum_m \Re\left\{\underline{\delta s}_{l,m} e^{j\omega_{US}t}\right\} \ll 1 \quad (12)$$

We get in Eq.11:

$$\exp\left[j\,\frac{\omega_0}{c}\sum_m \Re\left\{\underline{\delta s}_{l,m} e^{j\omega_{US}t}\right\}\right] \simeq \quad (13)$$
$$1 + j\,\frac{\omega_0}{c}\sum_m \Re\left\{\underline{\delta s}_{l,m} e^{j\omega_{US}t}\right\}$$

The field $E_S(t)$ diffused by the sample becomes:

$$E_S(t) = \Re\left\{\left[a\sum_l \underline{E_P}\,e^{j\omega_0(t-s_{l,0}/c)}\right]\right.$$
$$\left.\times \left[1 + j\,\frac{\omega_0}{c}\sum_m \Re\left\{\underline{\delta s}_{l,m} e^{j\omega_{US}t}\right\}\right]\right\} \quad (14)$$

The field $E_S(t)$ diffused by the sample is the sum of a main component $E_{S,\omega_0}(t)$, whose frequency is ω_0, with the two sideband components $E_{S,\omega_{\pm 1}}(t)$, whose frequencies are $\omega_{\pm 1} = \omega_O \pm \omega_{US}$.

$$E_S(t) = E_{S,\omega_0}(t) + E_{S,\omega_1}(t) + E_{S,\omega_{-1}}(t) \quad (15)$$

Let us introduce $\underline{E}_{S,\omega_0}$ and $\underline{E}_{S,\omega_{\pm 1}}$, which are slow varying with time.

$$E_{S,\omega_0}(t) \equiv \Re\left\{\underline{E}_{S,\omega_0}\exp(j\omega_0 t)\right\} \quad (16)$$
$$E_{S,\omega_{\pm 1}}(t) \equiv \Re\left\{\underline{E}_{S,\omega_{\pm 1}}\exp(j\omega_{\pm 1}t)\right\}$$

We get from Eq.14:

$$E_{S,\omega_0}(t) = \Re\left\{a\sum_l \underline{E_P}\,e^{j\,\omega_0(t-s_{l,0}/c)}\right\} \quad (17)$$

$$E_{S,\omega_1}(t) + E_{S,\omega_{-1}}(t) = \Re\left\{a\underline{E_P}e^{j\omega_0 t}\right. \quad (18)$$
$$\left.\times\sum_{l,m}\left[j\frac{2\pi\beta_{l,m}}{\lambda}\,e^{-j2\pi s_{l,0}/\lambda}\left[e^{j\phi_{l,m}}\,e^{\,j\omega_{US}t} + c.c.\right]\right]\right\}$$

where $c.c.$ means the complex conjugate. We thus have for $\underline{E}_{S,\omega_{\pm 1}}$:

$$\underline{E}_{S,\omega_{\pm 1}}(t) = a\underline{E_P}\sum_l \quad (19)$$
$$\left[j\,e^{-j2\pi s_{l,0}/\lambda}\times\sum_m\left[\frac{2\pi\beta_{l,m}}{\lambda}e^{\pm j\phi_{l,m}}\right]\right]$$

Here, the main component E_{S,ω_0} does not depend on the travel path modulation (Eq.17), while the modulated components $E_{S,\omega_{\pm 1}}$ do. Moreover, whatever the modulation mechanism is: displacement of the scatterers or modulation of the refractive index, $\beta_{l,m}$ is directly related to the acoustic pressure $P_{US}(\mathbf{r}_{l,m})$ at the scatterer location $\mathbf{r}_{l,m}$.

Note that the phases $\phi_{l,m}$ and $\phi_{l,m'}$ of two scattering events m and m' of the same path l are partially correlated according to the position of the associated diffusers $\mathbf{r}_{l,m}$ and $\mathbf{r}_{l,m'}$, and according to the physical effect at the origin of the modulation.

For the displacement of the scatterers, the phases $\phi_{l,m}$ is related to the projection q_z of the scattering wave vector $\mathbf{q}_{l,m}$ along the US propagation direction (i.e z) with $\mathbf{q}_{l,m} = \mathbf{k}'_{l,m} - \mathbf{k}_{l,m}$ (where $\mathbf{k}_{l,m}$ and $\mathbf{k}'_{l,m}$ are the wave vectors of the photon before and after the scattering event l,m). The phases $\phi_{l,m}$ and $\phi_{l,m'}$ are not correlated, since q_z may change of sign from one scattering event (l,m) to the next $(l,m+1)$ within the same path l.

For the modulation of the refractive index, $\phi_{l,m}$ is mainly related to the US phase. In a typical experiment the scattering length l_s is about 0.1 mm, while the US wavelength λ_{US} is about 1 mm (0.75 mm for $\omega_{US} = 2$ MHz). This means that $\phi_{l,m}$ and $\phi_{l,m'}$ are correlated, if the scattering events (l,m) and (l,m') are close together ($|m - m'| <$ a few units), and uncorrelated if not.

This partial coherence allows us to use the acousto-optical modulation in scattering media. However, all the scatterers $\mathbf{r}_{l,m}$ in the acoustic column contribute to the tagged photons field $\underline{E}_{S,\omega_{\pm 1}}(t)$. Thus on the acoustic column, the information is not localized. So it is necessary to use a complementary technique in order to obtain an axial z resolution.

2.2 The axial resolution along z

To obtain an axial resolution along z, Lesaffre et al. [30] have used Acousto Optic Cohérent Tomography (AOCT). This technique is based on the control of the acoustic and optical coherence lengths using a random phase modulation on the acoustic and optical arms.

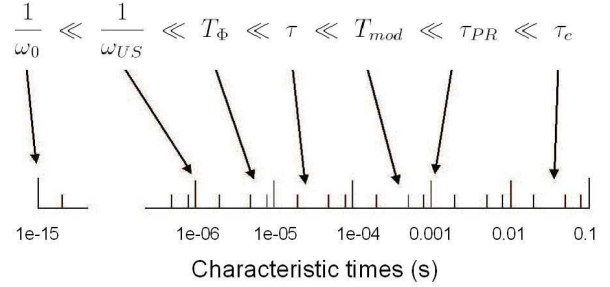### 2.2.1 The AOCT random modulation of the optical and acoustical field phases.

$$\frac{1}{\omega_0} \ll \frac{1}{\omega_{US}} \ll T_\Phi \ll \tau \ll T_{mod} \ll \tau_{PR} \ll \tau_c$$

Figure 2: Order of magnitude of the various times. $1/\omega_0$: optical period; $1/\omega_{US}$: acoustic period; T_Φ: acousto-optical correlation time; τ: time averaging characteristic time; T_{mod}: characteristic time of the modulation $H(t)$; τ_{PR}: photorefractive time; τ_c: Lock-in integration time.

The incoming optical field and the PZT excitation voltage are now:

$$E'_P(t) = \Re \left\{ \underline{E}_P e^{j(\omega_0 t + \psi_P(t))} \right\} \tag{20}$$

$$U'_{PZT}(t) = \Re \left\{ \underline{U}_{PZT} e^{j(\omega_{US} t - \psi_{US}(t))} \right\} \tag{21}$$

where ψ_P et ψ_{US} are random phase modulations applied to the optical incoming beam E'_P and to the PZT that generates the US beam. Since we consider the effect of a random phase modulation, fields are noted E'_P, E'_S. The random phases $\psi_P(t)$ and $\psi_{US}(t)$ are supposed to be fully correlated as follow:

$$\psi_P(t) = \psi_{US}(t - z_0/c_{US}) \tag{22}$$

where $z_0/c_{US} = \theta$ is a fixed temporal delay which determines the z selected zone $z \simeq z_0$.

To simplify the discussion we will consider here, like in [30], that the US phase ψ_{US} is randomly drawn every T_Φ to be 0 or π with equal probability. The optical phase ψ_P follows the same random phase law than ψ_{US}, but the phase is dealyed in time by z_0/c_{US}. The incoming complex field is:

$$\underline{E}'_P(t) = \underline{E}_P e^{j\psi_P(t)} \tag{23}$$

5

and the US excitation ($\underline{U}'_{PZT}$), and US pressure ($\underline{P}'_{US}$) complex amplitudes are:

$$
\begin{aligned}
\underline{U}'_{PZT}(t) &= \underline{U}_{PZT}\ e^{j\psi_{US}(t)} \qquad\qquad (24)\\
\underline{P}'_{US}(\mathbf{r},t) &= A(\mathbf{r})\ \underline{U}_{PZT}\ e^{j\omega_{US}zt/c_{US}}\ e^{\ j\psi_{US}(t-z/c_{US})}
\end{aligned}
$$

2.2.2 The "tagged photons" field.

By making the calculations leading to Eq.19 with the random phases ψ_P and ψ_{US}, we get the tagged photons complex amplitude $\underline{E}'_{S,\omega_{\pm 1}}$:

$$
\underline{E}'_{S,\omega_{\pm 1}}(t) = a\underline{E}_P\ \sum_l \left[j\ e^{-j2\pi s_{l,0}/\lambda} \right. \quad (25)
$$

$$
\left. \times \sum_m \frac{2\pi\beta_{l,m}}{\lambda} e^{\ \pm j\phi_{l,m}}\ e^{\ \pm j\psi_{l,m}(t)} \right]
$$

where the phase $\psi_{l,m}$, which depends on time t, and on location $z_{l,m}$ of the mth scatterer along the axis z, is defined by:

$$
\psi_{l,m}(t) = \psi_P(t) + \psi_{US}\left(t - z_{l,m}/c_{US}\right). \qquad (26)
$$

Because of the random phase jumps, which occur every T_ϕ, the complex field $\underline{E}'_{S,\omega_{\pm 1}}(t)$ varies with a characteristic time T_ϕ, while, in absence of random modulation, the field $\underline{E}_{S,\omega_{\pm 1}}$ does not depend on time. In the following, we will detect the field $\underline{E}'_{S,\omega_{\pm 1}}(t)$ by photorefractive effect on a crystal.

We must notice that all the photorefractive detection $\underline{E}'_{S,\omega_{\pm 1}}(t)$ processes occur on times much larger than T_ϕ.

- The writing of photorefractive signal on the crystal occurs in a time $\tau_{PR} \gg T_\phi$.

- To get a modulated signal for the Lock-In amplifier, the phase of the US will be modulated at a frequency $\omega_{mod} = 1/T_{mod}$ with $T_{mod} \gg T_\phi$.

- The extraction of the modulated signal modulated at ω_{mod} will be made via Lock-In with an integration time $\tau_c \gg T_\phi$.

So one can replace in the following the field $\underline{E}'_{S,\omega_{\pm 1}}(t)$ by its temporal average $\langle \underline{E}'_{,\omega_{\pm 1}}(t)\rangle_\tau$ over the characteristic time τ chosen such as (see Fig.2):

$$
T_\phi \ll \tau \ll \tau_{PR},\ T_{mod},\ \tau_c \qquad (27)
$$

Thus we eliminate the fast varying components of $\underline{E}'_{S,\omega_{\pm 1}}(t)$ which anyway will have no effect on the final signal. To be complete let's define here the temporal average operator $\langle\ \rangle_\tau$:

$$
\langle ....\rangle_\tau \equiv \frac{1}{\tau}\int_{t'=t-\tau/2}^{t'=t+\tau/2}(....)dt' \qquad (28)
$$

The temporal average of the tagged photon field over the characteristic time τ is then:

$$
\langle \underline{E}'_{S,\omega_{\pm 1}}(t)\rangle_\tau = a\underline{E}_P\ \sum_l \left[j\ e^{-j2\pi s_{l,0}/\lambda} \right.
$$

$$
\left. \times \sum_m \left(\frac{2\pi\beta_{l,m}}{\lambda}e^{\pm j\phi_{l,m}} \times \langle e^{\pm j\psi_{l,m}(t)}\rangle_\tau \right) \right] \quad (29)
$$

As we can see on Eq.29, $\psi_{l,m}$ acts on the temporal average $\langle \underline{E}'_{S,\omega_{\pm 1}}(t)\rangle_\tau$ only through $\langle e^{\pm j\psi_{l,m}(t)}\rangle_\tau$, which depends only on the location along z of the scatterer of indexes l,m, i.e. on $z_{l,m}$. From Eq.22 and Eq.26, we have

$$
\begin{aligned}
\psi_{l,m}(t) &\simeq 0\\
\langle e^{\ \pm j\psi_{l,m}(t)}\rangle_\tau &\simeq 1 \qquad\qquad (30)
\end{aligned}
$$

$$
\begin{aligned}
\psi_{l,m}(t) &\simeq 0,\pi \quad \text{randomly}\\
\langle e^{\pm j\psi_{l,m}(t)}\rangle_\tau &\simeq 0 \qquad\qquad (31)
\end{aligned}
$$

for the scatterer l,m located in (Eq.30) and out (Eq.31) the selected zone $z \simeq z_0$ respectively.

To characterize this z selection mechanism in a more quantitative way, let us define the time correlation function:

$$
\begin{aligned}
\underline{g}_1(\theta) &= \frac{\langle \underline{E}'_P(t)\underline{E}'^*_P(t+\theta)\rangle_\tau}{\langle |\underline{E}'_P(t)|^2\rangle_\tau} \qquad\qquad (32)\\
&= \left\langle e^{j\psi_P(t)}e^{-j\psi_P(t+\theta)}\right\rangle_\tau\\
&= \left\langle e^{j\psi_{US}(t)}e^{-j\psi_{US}(t+\theta)}\right\rangle_\tau\\
&= \frac{\langle \underline{U}'_{US}(t)\underline{U}'^*_{US}(t+\theta)\rangle_\tau}{\langle |\underline{U}'_{US}(t)|^2\rangle_\tau}
\end{aligned}
$$

In the case of $0,\pi$ random phase jumps considered here, $\underline{g}_1(\theta)$ is a triangular function that corresponds
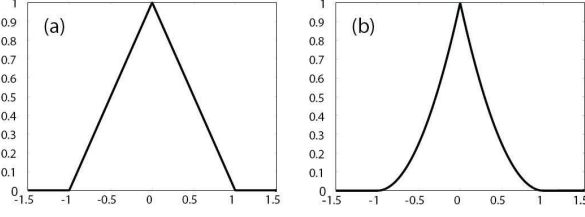
Figure 3: Plot of correlation function $\underline{g}_1(\theta)$ (a), and its square $|\underline{g}_1(\theta)|^2$ (b). The horizontal axis Units is either θ/T_Φ (for time correlation), or $(z-z_0)/\Delta z$ with $\Delta z = c_{US}\, T_\Phi$ (for z resolution).

Figure 4: Principle of the photorefractive detection.

to the convolution of two rectangles of width T_{Phi}. The correlation function $\underline{g}_1(\theta)$ is plotted on Fig.3 (a).

The field $\langle \underline{E}'_{S,\omega_{\pm 1}} \rangle$ can be expressed as a function of $\underline{g}_1$:

$$\langle \underline{E}'_{S,\omega_{\pm 1}}(t) \rangle_\tau = a\underline{E}_P \sum_l \left[j\ e^{-j2\pi s_{l,0}/\lambda} \right. \qquad (33)$$

$$\left. \times \sum_m \left[\underline{g}_1\left(\frac{z_{l,m}-z_0}{c_{US}} \right) \frac{2\pi\beta_{l,m}}{\lambda} e^{\pm j\phi_{l,m}} \right] \right]$$

Let us note here that the second member of Eq. 33 does not depend on time. It means that, when we apply the random modulations of phase, the field $\underline{E}'_{S,\omega_{\pm 1}}(t)$ reaches, after a brief transitory regime, a stationary regime in which the slow field components do not depend on time any more.

Furthermore, the results of the calculations do not depend on τ as soon as the condition $T_\phi \ll \tau \ll (\tau_{PR},\ T_{mod},\ \tau_c)$ of Eq.27 is fulfilled. So one should write: $\langle \underline{E}'_{S,\omega_{\pm 1}}(t) \rangle_\tau \equiv \langle \underline{E}'_{S,\omega_{\pm 1}} \rangle$.

2.3 The photorefractive detection of the tagged photons

We will now consider the photorefractive detection of the tagged photons in order to quantify the z selection process for the photorefractive detected signal (and not just for the tagged field $\underline{E}'_{S,\omega_{\pm 1}}$ itself). The calculations we will make are similar to the ones
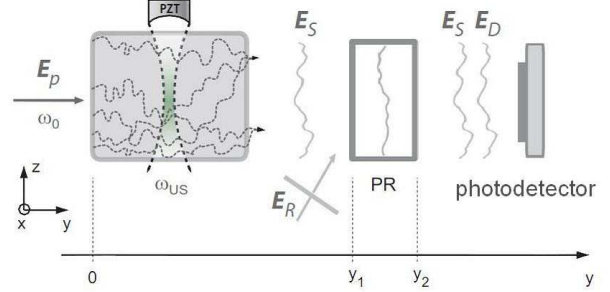
made by Gross at al. [22], but in a slightly different context.

2.3.1 The detection principle

The principle of the photorefractive detection is illustrated on Fig.4. The signal E_S, the wave front of which is distorted, is collected in a photorefractive crystal. A reference beam E_R, considered as plane wave, which is also called pump beam, interferes with it within the crystal. By photorefractive effect, the interferogram grooves a hologram corresponding to a weak modulation $\delta n(\mathbf{r})$ of the local refractive index within the volume of the crystal. This effect having a finite response time τ_{PR}, only the static component of the interferogram contributes to the recording of the hologram.

To simplify the analysis, we will consider the detection of tagged photons of the $+1$ sideband at $\omega_1 = \omega_0 + \omega_{US}$. So we will shift the beam reference frequency by $\omega_{US} = \omega_1 - \omega_0$ in order to perform the photorefractive detection at frequency ω_1. Let us introduce the complex amplitude $\underline{E}_{R,\omega_1}$ of the reference field.

$$E_R(t) = \Re\left[\underline{E}_{R,\omega_1} e^{j\omega_1 t} \right] \qquad (34)$$

The photorefractive effect selects, in the signal field $E'_S = E'_{S,\omega_0} + E'_{S,\omega_1} + E'_{S,\omega_{-1}}$, the field component E'_{S,ω_1}. The reference beam is then diffracted by the holographic grating grooved within the crystal yielding the field E'_D, whose wavefront is the same for

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$\underline{E}'_{S,\omega_1}$. At the exit of the crystal, one gets then both the transmitted signal beam E'_S, and the beam diffracted by the crystal, which will be noted E'_D.

2.3.2 The reference field diffracted by the crystal E'_D

Let us introduce the complex amplitude of the diffracted field defined by

$$E'_D(t) = \Re\left[\underline{E}'_{D,\omega_1}(t)e^{j\omega_1 t}\right] \tag{35}$$

Let us call $y = y_1$ and $y = y_2$ the crystal entrance and exit planes respectively, and $t = 0$ the origin of time, when no photorefractive hologram is recorded. Let us consider that the reference field $\underline{E}_R$ is constant. Within the crystal, the signal field $\underline{E}'_{S,\omega_1}(y_1 < y < y_2, t)$ can be written as a function of the entrance field $\underline{E}'_{S,\omega_1}(y_1, t)$ [32, 33]

$$\underline{E}'_{S,\omega_1}(y,t) = e^{-\alpha(y-y_1)/2} \tag{36}$$
$$\times\left[\underline{E}'_{S,\omega_1}(y_1,t) + \int_0^t dt'\underline{E}'_{S,\omega_1}(y_1,t')G(y,t-t')\right]$$

where, under conditions of weak recording efficiency and weak absorption, the transfer function $G(y,t)$ can be written as [34]

$$G(y,t) = \frac{\gamma(y - y_1)}{\tau_{PR}}e^{-\frac{t}{\tau_{PR}}} \tag{37}$$

Here, τ_{PR} is the photorefractive response time and γ the photorefractive gain. Equation 36 is established for two plane waves, but it can be generalized to distorted wavefront by decomposing the wavefront in plane waves. Several approximations are made to establish this equation: (i) the reference beam is a monochromatic wave with constant frequency ω_1 (i.e. it is not temporarily modulated), (ii) it is not perturbed by the recording of the hologram although it can be attenuated by the crystal, and (iii) its power is larger than the signal beam one.

In the AOCT experiment [30], the tagged photon signal is modulated at a frequency ω_{mod} of some kHz, and Lock-in detection is performed. So we are interested in the low-frequency evolution of $\underline{E}'_{S,\omega_1}$. So we can replace the $t' = 0$ lower limit of the integral $\int dt'$ of Eq. 36 by $t' = -\infty$, by neglecting the transient components. By making the transformation $t' \to (t - t')$, in the integral $\int dt'$ of Eq.3, we obtain:

$$\underline{E}'_{S,\omega_1}(y,t) = e^{-\alpha(y-y_1)/2} \tag{38}$$
$$\times\left[\underline{E}'_{S,\omega_1}(y_1,t) + \int_0^\infty dt'\,\underline{E}'_{S,\omega_1}(y_1,t-t')\,G(y,t')\right]$$

We can notice that the hologram is written with delayed time $t - t'$ with a delay t' varying from zero to some τ_{PR}. Also let us note that the first term of Eq. 38 corresponds to the signal wavefront that is transmitted by the crystal. Let us call E'_T its field and $\underline{E}'_T$ its complex amplitude (the index T means here transmitted). The second term corresponds to the reference field that is diffracted by the crystal we will note E'_D (where the index D means diffracted), and $\underline{E}'_D$ for the complex amplitude. We can write:

$$\begin{aligned}
E'_S(y,t) &= E'_T(y,t) + E'_D(y,t) \tag{39}\\
E'_T(y,t) &= E'_{T,\omega_{-1}}(y,t) + E'_{T,\omega_0}(y,t) + E'_{T,\omega_{+1}}(y,t)\\
E'_D(y,t) &= E'_{D,\omega_{+1}}(y,t)
\end{aligned}$$

$$\begin{aligned}
\underline{E}'_{S,\omega_1}(y,t) &= \underline{E}'_{T,\omega_1}(y,t) + \underline{E}'_{D,\omega_1}(y,t) \tag{40}\\
\underline{E}'_{T,\omega_1}(y,t) &= e^{-\alpha(y-y_1)/2}\underline{E}'_{S,\omega_1}(y_1,t)\\
\underline{E}'_{D,\omega_1}(y,t) &= e^{-\alpha(y-y_1)/2}\\
&\quad \times \int_0^\infty dt'\underline{E}'_{S,\omega_1}(y_1,t-t')G(y,t')
\end{aligned}$$

Note that since the photorefractive effect selects the field components of frequency ω_1, the diffracted field E'_D exhibit in Eq.39 a single frequency component $E'_{D,\omega_{+1}}$.

2.4 The acousto optic signal detected by a large area photodiode

We consider that the signal is detected by a photodiode of large area located near the cristal exit plane $y = y_2$. The photodiode signal S_{PD} is equal to the integral of $|\underline{E}'_S|^2$ over its area. We get from Eq.39.

$$S_{PD}(t) = c.c. + \tag{41}$$
$$\int dx \int dz \; \left|\underline{E}'_S(x,y_2,z,t)\right|^2$$

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$$S_{PD}(t) = c.c. + \qquad (42)$$

$$\int dx \int dz \ \left\{ \ \left| \underline{E}'_T(x, y_2, z, t) \right|^2 \right.$$
$$+ \ \left| \underline{E}'_D(x, y_2, z, t) \right|^2$$
$$+ \ \left(\ \underline{E}'_T(x, y_2, z, t) \ \underline{E}'^*_D(x, y_2, z, t) \right) \Big\}$$

Because the acousto-optical interaction does not modify the total number of photons, i.e. tagged + untagged photons, the term $|\underline{E}'_T|^2$ in Eq.42 does not depend on the acoustic modulation. Furthermore, because the gain is supposed to be low, i.e. $\eta_{PR} = \gamma(y_2 - y_1) < 1$, the term $|\underline{E}'_D|^2$ can be neglected in front of the crossed term $\underline{E}'_T \ \underline{E}'^*_D$. Therefore we can only consider the crossed term, which is the product of the diffracted field E'_D, which builts up with the characteristic time τ_{PR}, and the transmitted field E'_T, which can vary quickly. The photodiode modulated signal S'_{PD} is thus:

$$S'_{PD}(t) = c.c. + \qquad (43)$$
$$\int dx \int dz \ \underline{E}'_{T,\omega_1}(x, y_2, z, t) \underline{E}'^*_{D,\omega_1}(x, y_2, z, t)$$

From Eq.40, we get

$$S'_{PD}(t) = c.c. + \qquad (44)$$
$$e^{-\alpha(y_2-y_1)} \int dx \int dz \ \underline{E}'_{S,\omega_1}(x, y_1, z, t)$$
$$\times \int_0^\infty dt' \ \underline{E}'^*_{S,\omega_1}(x, y_1, z, t - t') \ G^*(y_2, t')$$

To keep a certain universality, we write G^* although G is supposed to be real. We can then develop $\underline{E}'_{S,\omega_1}$ by summing up all the paths (index l) and scattering events (index m) contributions by using Eq.33.

Averaging over a time τ, we get:

$$\langle S'_{PD}(t) \rangle_\tau = c.c. + e^{-\alpha(y_2-y_1)} |a\underline{E}_p|^2 \int dx \int dz$$
$$\left[\sum_l j e^{-j2\pi s_{l,0}/\lambda} \times \sum_m \frac{2\pi \beta_{l,m}}{\lambda} \ \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{v_{US}} \right) e^{j\phi_{l,m}} \right]$$
$$\times \left[\int_0^\infty dt' \ G^*(y_2, t') \times \left(\sum_{l'} -j \ e^{2j\pi s_{l',0}/\lambda} \right. \right.$$
$$\left. \left. \times \sum_{m'} \frac{2\pi \beta_{l',m'}}{\lambda} \ \underline{g}_1^* \left(\frac{z_0 - z_{l',m'}}{v_{US}} \right) \ e^{-j\phi_{l',m'}} \right) \right]$$
$$(45)$$

The equation 45 illustrates the complexity of the calculation of the signal. It involves a double summation over the optical paths (i.e. $\sum_{l,l'}$), a double summation over the scattering events (i.e. $\sum_{m,m'}$), a spatial integral over the photodiode area (i.e. $\int \int dx \, dz$), and a temporal integral over the delay t' (i.e. $\int dt'$).

To simplify this equation, let us consider first the integral over the photodiode area $\int \int dx \, dz$. Every point (x, z) of the photodiode selects paths l and l', which finishes in (x, z). For the corresponding paths, the phase factor $e^{-j2\pi \, s_{l,0}/\lambda}$ is totally random from a route to the next one. So we can limit the summation over l and l' to the terms $l = l'$. The equation 45 becomes then:

$$\langle S'_{PD}(t) \rangle_\tau = c.c. + e^{-\alpha(y_2-y_1)} \left| \frac{2\pi a \underline{E}_p}{\lambda} \right|^2 \int dx \int dz$$
$$\times \sum_l \sum_m \left[\beta_{l,m} \ \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{c_{US}} \right) \int_0^\infty dt' G^*(y_2, t') \right.$$
$$\left. \times \sum_{m'} \beta_{l,m'} \ \underline{g}_1^* \left(\frac{z_0 - z_{l,m'}}{c_{US}} \right) e^{j(\phi_{l,m} - \phi_{l,m'})} \right] (46)$$

To simplify this equation further, it is necessary to study the mutual coherence of the phases $\phi_{l,m}$ and $\phi_{l,m'}$ that corresponds to two different scattering events m and m' of the same path l. According to the position of the scatterers, and according to the acousto-optical modulation mechanism, these phases are correlated or not. Nevertheless, when the two events (m and m') occur in two z coordinates $z_{l,m}$

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and $z_{l,m'}$ separated by more than an acoustic wavelength λ_{US} (i.e. $|z_{l,m'} - z_{l,m}| > \lambda_{US}$), the phases $\phi_{l,m}$ and $\phi_{l,m'}$ are weakly correlated. We can then write:

$$\langle S'_{PD}(t) \rangle_\tau = c.c. + \tag{47}$$

$$e^{-\alpha(y_2 - y_1)} \left| \frac{2\pi a \underline{E}_p}{\lambda} \right|^2 \int_0^\infty dt' G^*(y_2, t') \int dx \int dz$$

$$\sum_l \sum_m \sum_{m' \text{ with } |z_{l,m} - z_{l,m'}| < \lambda_{US}} \left[\beta_{l,m} \beta_{l,m'} \right.$$

$$\left. e^{j(\phi_{l,m} - \phi_{l,m'})} \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{c_{US}} \right) \underline{g}_1^* \left(\frac{z_0 - z_{l,m'}}{c_{US}} \right) \right]$$

Since the magnitude of the acoustic pressure vary weakly over λ_{US}, we have $\beta_{l,m} \simeq \beta_{l,m'}$ for $z_{l,m} - z_{l,m'} < \lambda_{US}$. Moreover, the random modulation of phases is chosen in such a way that the characteristic length $T_\phi c_{US}$ is larger than the acoustic wavelength λ_{US} (i.e. $T_\phi c_{US} > \lambda_{US}$. This implies that $\underline{g}_1 ((z_0 - z_{l,m})/c_{US}) \simeq \underline{g}_1 ((z_0 - z_{l,m'})/c_{US})$ for $z_{l,m} - z_{l,m'} < \lambda_{US}$. Therefore we obtain:

$$\langle S'_{PD}(t) \rangle_\tau = c.c. \tag{48}$$

$$+ e^{-\alpha(y_2 - y_1)} \left| \frac{2\pi a \underline{E}_p}{\lambda} \right|^2 \int_0^\infty dt' G^*(y_2, t') \int dx \int dz$$

$$\sum_l \sum_m \beta_{l,m}^2 \left| \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{c_{US}} \right) \right|^2$$

$$\times \sum_{m' \text{ with } |z_{l,m} - z_{l,m'}| < \lambda_{US}} e^{j(\phi_{l,m} - \phi_{l,m'})}$$

Here, the term $\left| \underline{g}_1 (z_0 - z_{l,m}/c_{US}) \right|^2$ selects the zone of imaging.

The z resolution one can expect is roughly equal to the half-width of $\underline{g}_1(z)$, i.e. to $0.5 \times c_{US} T_\Phi$ (see Fig.3). The expected resolution is thus about 7.5 mm for $T_\Phi = 10~\mu s$ (20 US periods at $\omega_{US} = 2$ MHz), and 1.1 mm for $T_\Phi = 1.5~\mu s$ (3 US periods at $\omega_{US} = 2$ MHz). The AOCT published experimental results [30] correspond to $T_\Phi \simeq 2~\mu s$. To improve the z resolution, one must thus decrease T_Φ. The acousto optic signal decreases accordingly, since it is proportional

to T_Φ: the scattering events that contribute to the signal must be within the $\underline{g}_1(z)$ selected region.

2.5 The Lock-in detection of the acousto optical signal

2.5.1 The modulation of the signal at ω_{mod}

Note that $\langle S_{PD}(t) \rangle_\tau$ given by Eq.48 is invariant with time. So the tagged photons photorefractive signal S_{PD} is a CW component, which adds to the total flow of transmitted light. To detect S_{PD} more efficiently with a Lock-in, AOCT adds an extra modulation of the ultrasonic wave. Like in the AOCT experiment [30], we will consider here an asymmetric 0 to π phase modulation $H_{U.S.}(t)$ at frequency $\omega_{mod} = 2\pi/T_{mod} \sim$ 3 kHz, with duty cycle $0 < r < 1$:

$$H_{US}(t) = +1 \quad \text{pour} \quad 0 \le t/T_{mod} \le r \tag{49}$$
$$H_{US}(t) = -1 \quad \text{pour} \quad r < t/T_{mod} \le 1$$

We consider that the modulation period T_{mod} is very large compared to the correlation time T_ϕ, but smaller than the photorefractive time τ_{PR}, i.e. $(2\pi/\omega_{US}) < T_\phi \ll T_{mod} < \tau_{PR}$. In practice, we typically use $T_{mod} \sim 100\mu s$ (see Fig.2). The modulation is applied according

$$\underline{U}'_{PZT}(t) \to \underline{U}''_{PZT}(t) = H_{US}(t) \underline{U}'_{PZT}(t) \tag{50}$$

The US signal is denoted $\underline{U}''_{PZT}(t)$, and the fields are denoted E''_P, E''_S and so on. The complex amplitude of the tagged photon field is now

$$\underline{E}'_{S,\omega_1}(t) \to \underline{E}''_{S,\omega_1}(t) = H(t) \underline{E}'_{S,\omega_1}(t) \tag{51}$$

where $H(t) = H_{US}(t - z_0/c_{US})$. Similarly with Eq.40, the diffracted complex amplitude becomes

$$\underline{E}''_{D,\omega_1}(y,t) = e^{-\alpha(y - y_1)/2} \int_0^\infty dt' [H(t - t')$$
$$\times \underline{E}'_{S,\omega_1}(y_1, t - t') G(y, t')] \tag{52}$$

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2.5.2 The modulated acousto-optical signal

The signal from the photodiode given by equation 44 becomes

$$S''_{PD}(t) = c.c.$$
$$+ \ e^{-\alpha(y_2-y_1)} \int dx \int dz \left[H(t)\underline{E}'_{S,\omega_1}(x,y_2,z,t) \right.$$
$$\left. \int_0^\infty dt' \ H(t-t') \ \underline{E}'^{*}_{S,\omega_1}(x,y_2,z,t-t') \ G^*(y_2,t') \right] \quad (53)$$

By making the calculation leading to Eq. 48 from to Eq. 44 with the additional modulation H_{US}, we get.

$$\langle S''_{PD}(t)\rangle_\tau = c.c. + \quad (54)$$
$$e^{-\alpha(y_2-y_1)} \left| \frac{2\pi a \underline{E}_p}{\lambda} \right|^2 H(t) \int_0^\infty dt' H(t-t') \, G^*(y_2,t')$$
$$\times \int dx \int dz \sum_l \sum_m \left[\beta_{l,m}^2 \left| \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{c_{US}} \right) \right|^2 \right.$$
$$\left. \times \sum_{m'/|z_{l,m}-z_{l,m'}|<\lambda_{US}} e^{j\left(\phi_{l,m}-\phi_{l,m'}\right)} \right]$$

Since we have consider $T_{mod} < \tau_{PR}$, the integration over t' can be simplified, and we obtain from Eq.37.

$$\int_0^\infty dt' H(t-t') \, G^*(y_2,t') = \quad (55)$$
$$\left[\frac{1}{T_{PR}} \int_0^{T_{PR}} dt' H(t-t') \right] \times \left[\int_0^\infty dt' G^*(y_2,t') \right]$$
$$= (1-2r) \, \gamma(y_2-y_1)$$

This means that for a modulation $H(t)$ faster than τ_{PR}, the photorefractive recorded hologram is proportional to the average $\langle H(t)\rangle_{\tau_{PR}}$. The asymmetric nature of the modulation $H(t)$ yields non-zero photorefractive grating. The modulated component of

the signal on a large area photodiode thus becomes.

$$\langle S''_{PD}(t)\rangle_\tau \simeq c.c + \quad (56)$$
$$e^{-\alpha(y_2-y_1)} \left| \frac{2\pi a \underline{E}_p}{\lambda} \right|^2 H(t)(1-2r)\,\gamma(y_2-y_1)$$
$$\times \int dx \int dz \sum_l \sum_m \beta_{l,m}^2 \left| \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{c_{US}} \right) \right|^2$$
$$\times \sum_{m'/|z_{l,m}-z_{l,m'}|<\lambda_{US}} e^{j\left(\phi_{l,m}-\phi_{l,m'}\right)}$$

By this way, the photodiode signal is modulated following $H(t)$.

Equation 56, which does not depend on τ can be slightly simplified as following:

$$\langle S''_{PD}(t)\rangle = (1-2r)H(t)\left|\underline{E}_p\right|^2 \gamma(y_2-y_1)e^{-\alpha(y_2-y_1)}$$
$$\int dx \int dz \sum_l \sum_m \left[\beta_{l,m}^2 \left| \underline{g}_1 \left(\frac{z_0 - z_{l,m}}{c_{US}} \right) \right|^2 \right.$$
$$\left. \sum_{m' \text{ with } |z_{l,m}-z_{l,m'}|<\lambda_{US}} \left(e^{j\left(\phi_{l,m}-\phi_{l,m'}\right)} + c.c.\right) \right]$$
$$\quad (57)$$

3 Conclusion

The mains results of the paper are Eq.33 and Eq.57. Equation 33 shows that the tagged photon field $\langle E'_{S,\omega_{\pm1}}\rangle$, which is

- proportional to the amplitude of the optical field E_P injected in the scattering medium,

- proportional to the acoustic power delivered by the PZT via the term $\beta_{l,m}^2$

- and proportional to the correlation function $\underline{g}_1(z_0 - z_{l,m}/c_{US})$.

The random phase modulation creates along the acoustic column a zone of coherence located near $z \simeq z_0 = c_{US}\theta$. The tagged photon signal from this zone adds up coherently, and can be further detected. For the tagged photon field, the random

phase jump z selection is quantified by the factor $\underline{g}_1(z_0 - z_{l,m}/c_{US})$, which is the correlation product of a rectangle of width T_ϕ. This correlation product, which has triangular shape, is plotted on Fig.3(a) as a function of time, in T_Φ Units, or as a function of the scatterer z relative coordinate (i.e. $z_0 - z_{l,m}$), in $\Delta z = c_{US}T_\Phi$ Units.

On the other hand, Eq.57 shows that the acousto-optical modulated signal on the large area photodiode surface $\langle S_{PD}(t) \rangle_\tau$ is

- proportional to the optical intensity $|E_P|^2$ injected in the scattering medium,

- proportional to the surface of the photodiode, i.e. $\int dx \int dz$,

- proportional to the acoustic power delivered by the PZT via the term $\beta_{l,m}^2$

- proportional to $(1 - 2r)H(t)$ where $H(t)$ is the additional time modulation, whose duty cycle is r. Because of this well controlled time modulation, the photodiode signal can be Lock-in detected at the frequency ω_{mod} with an integration time $\tau_c > T_{mod} = 2\pi/\omega_{mod}$.

- and proportional to the square of the correlation function $\underline{g}_1$, i.e. to $\left| \underline{g}_1(z_0 - z_{l,m}/c_{US}) \right|^2$.

For the photodiode signal, the random phase jump z selection is quantified by the factor $\left| \underline{g}_1(z_0 - z_{l,m}/c_{US}) \right|^2$, which is the square of the correlation product $\underline{g}_1$. This $|\underline{g}_1|^2$ factor is plotted on Fig.3(b). One must note also that the summation over m' of the phases factors $e^{j(\phi_{l,m} - \phi_{l,m'})}$, which can be limited to $|z_{l,m} - z_{l,m'}| < \lambda_{US}$, describes here the effect of partial coherence of the successive scattering events within a given travel path l. The corresponding proportionality factor does not depend on the US modulation, and does not provide any z selection.

In this paper, we have described the AOCT effect theoretically. We show that the tagged photons remain coherent if they are generated within a selected z region of the sample, and we have quantified this z selection effect for both the tagged photon field $E'_{S,\omega_{\pm 1}}$, and the photorefractive photodiode

signal $S''_{PD}(t)$. These theoretical results will be compared with experiment in another publication.

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