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Time, Cost, and Environmental Impact Analysis for Sustainable Design at Multiple Building Levels

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FLORIDA INTERNATIONAL UNIVERSITY

Miami, Florida

TIME, COST, AND ENVIRONMENTAL IMPACT ANALYSIS FOR SUSTAINABLE
DESIGN AT MULTIPLE BUILDING LEVELS

A dissertation submitted in partial fulfillment of

the requirements for the degree of

DOCTOR OF PHILOSOPHY

in

CIVIL ENGINEERING

by

Peeraya Inyim

2015

To: Dean Amir Mirmiran
College of Engineering and Computing

This dissertation, written by Peeraya Inyim, and entitled Time, Cost, and Environmental Impact Analysis for Sustainable Design at Multiple Building Levels, having been approved in respect to style and intellectual content, is referred to you for judgment.

We have read this dissertation and recommend that it be approved.

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Date of Defense: March 23, 2015

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DEDICATION

This dissertation is dedicated to my parents, who have been a great support to me.

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ABSTRACT OF THE DISSERTATION
TIME, COST AND ENVIRONMENTAL IMPACT ANALYSIS FOR
SUSTAINABLE DESIGN AT MUTIPLE BUILDING LEVELS

by

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Construction projects are complex endeavors that require the involvement of different professional disciplines in order to meet various project objectives that are often conflicting. The level of complexity and the multi-objective nature of construction projects lend themselves to collaborative design and construction such as integrated project delivery (IPD), in which relevant disciplines work together during project conception, design and construction. Traditionally, the main objectives of construction projects have been to build in the least amount of time with the lowest cost possible, thus the inherent and well-established relationship between cost and time has been the focus of many studies. The importance of being able to effectively model relationships among multiple objectives in building construction has been emphasized in a wide range of research. In general, the trade-off relationship between time and cost is well understood and there is ample research on the subject. However, despite sustainable building designs, relationships between time and environmental impact, as well as cost and environmental impact, have not been fully investigated.

The objectives of this research were mainly to analyze and identify relationships of time, cost, and environmental impact, in terms of CO₂ emissions, at different levels of a building: material level, component level, and building level, at the pre-use phase, including manufacturing and construction, and the relationships of life cycle cost and life cycle CO₂ emissions at the usage phase. Additionally, this research aimed to develop a robust simulation-based multi-objective decision-support tool, called SimuleICon, which took construction data uncertainty into account, and was capable of incorporating life cycle assessment information to the decision-making process. The findings of this research supported the trade-off relationship between time and cost at different building levels. Moreover, the time and CO₂ emissions relationship presented trade-off behavior at the pre-use phase. The results of the relationship between cost and CO₂ emissions were interestingly proportional at the pre-use phase. The same pattern continually presented after the construction to the usage phase. Understanding the relationships between those objectives is a key in successfully planning and designing environmentally sustainable construction projects.

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CHAPTER 1 INTRODUCTION

1.1 Research Background

Construction projects are complex endeavors that require the application of different professional disciplines in order to meet various objectives that are often conflicting. The level of complexity and the multi-objective nature of construction projects lend themselves to the application of Integrated Project Delivery (IPD), in which relevant disciplines work together during project conception, design and construction (e.g., AIA, 2007; Hellmund et al., 2008). Traditionally, the main objectives of construction projects have been to build in the least amount of time with the lowest cost possible, and thus the inherent and well-established relationship between cost and time has been the focus of many studies. However, public concerns for the impact that human activities have on the environment has been growing steadily over the past decade; the construction industry is no exception and construction professionals are constantly facing the challenge of integrating environmental sustainability as one of the project objectives.

The environmental impact of buildings and their operations has been the subject of a significant amount of research. Buildings affect the environment in every stage of their lifespan, including manufacturing and transportation of materials, construction, usage, maintenance, disassembly and waste management; collectively, these stages are called the building lifecycle. Recent studies have also shown attempts to understand environmental impact of buildings and construction, as well as their relationships with cost and time. For example, Ofori (1992) suggested the adoption of environmental

performance of a construction project as a significant objective along with time, cost, and quality. Some studies, such as Morel et al. (2001), looked into the selection of materials and construction methods to reduce environmental impact of construction. Others were interested in developing algorithms for multi-objective optimization, such as Marzouk et al. (2008), Ozcan-Deniz et al. (2011) and Ashuri and Tavakolan (2012). Recently, Zhu et al. (2012) discussed a multi-objective analytical tool, SimuleICon, for studying time, cost and environmental impact. Inyim et al. (2014) further developed SimuleICon as a simulation-based approach for selecting design solutions that considered time, cost, and environmental impact of the whole building life cycle to support sustainable construction in the architecture, engineering and construction (AEC) industry.

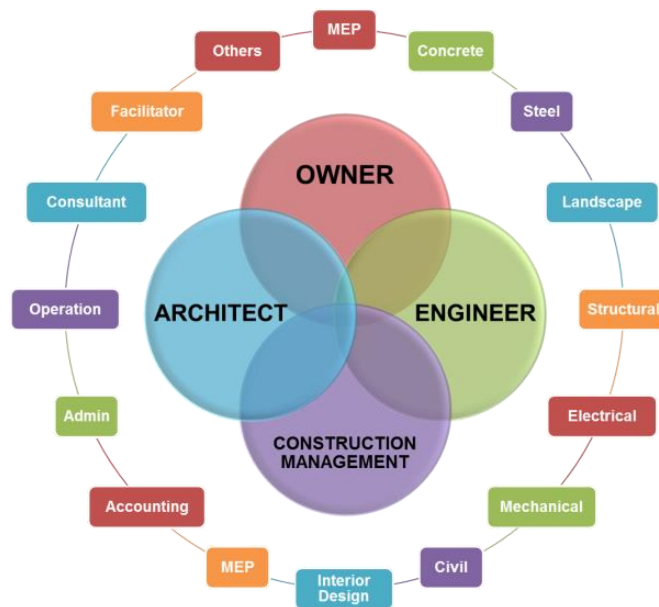


Figure 1 Integrated Project Delivery

To achieve sustainability, a tool or method capable of quantifying the environmental impact of a building's lifecycle is required (Rebitzer et al., 2004). Life

cycle assessment (LCA) is a quantitative method to determine the environmental impacts of materials, products, processes or buildings (Flager et al., 2012). LCA can evaluate and interpret environmental impacts of the building throughout its life stages, raw material acquisition, material manufacturing, construction, occupancy/maintenance, and demolition/waste management (e.g., Kruger & Seville, 2012; EPA, 2014). Greenhouse gas (GHG) emissions are one of the environmental impacts quantifiable by LCA, among others such as stratospheric ozone depletion, acidification potential, eutrophication potential, toxicological stress on humans and others.

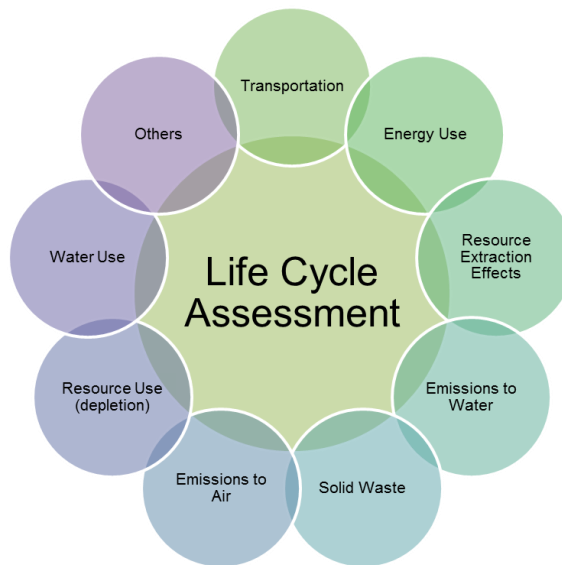


Figure 2 Life Cycle Assessment (LCA)

GHG emissions are considered to be the most significant cause of global warming (Ürge-Vorsatz et al., 2007). Carbon dioxide (CO₂) is the most important emission of GHG, and it accounts for approximately 80% of the total GHG emissions (Pachauri & Reisinger, 2007). Loh et al. (2009) also emphasized the importance of considering CO₂

emissions in the design phase. Attempting to reduce CO₂ emissions in the building's lifecycle often leads to increasing its energy efficiency. This happens because fuel, which is used to power buildings and the machines used to build them, is a critical source of CO₂ emissions (e.g., Thyholt & Hestnes, 2008; Gustavsson & Joelsson, 2010; Ramesh et al. 2010). Thus, energy consumption is an important factor as a source of GHG emissions, especially CO₂. Research acknowledged that buildings are responsible for a significant amount of energy consumption in the world. For example, in the United States, reports revealed that buildings account for 38% of CO₂ emissions (USGCB, 2008) and 40% of the energy consumption of the U.S. (DOE, 2012). LCA is essential in understanding and optimizing energy consumption in buildings and construction projects. However, it is often challenging to quantify the energy consumption of a building during the usage phase due to its dynamic nature. A feasible set of tools in dealing with the energy efficiency problem during design are energy simulation programs, which allow the evaluation of energy performance of different building designs and the selection of the most appropriate alternatives.

The selection of a building's materials, components and construction methods to achieve the required duration, cost and environmental impact is also a significant challenge for design and construction professionals. Selection of construction alternatives during design must be done at the material and component level, but with the possibility of assessing its impact at the building level. For example, in a small project having only ten construction activities and two design alternatives per activity, if all combinations of alternatives are considered, the project has a total of 1,024 possible solutions, each having

a unique cost, duration and environmental impact, from which a single solution must be selected for construction. Given the fact that most construction projects can have well over a million possible solutions, the need for a tool capable of systematical analysis and optimization of design alternatives selection becomes evident.

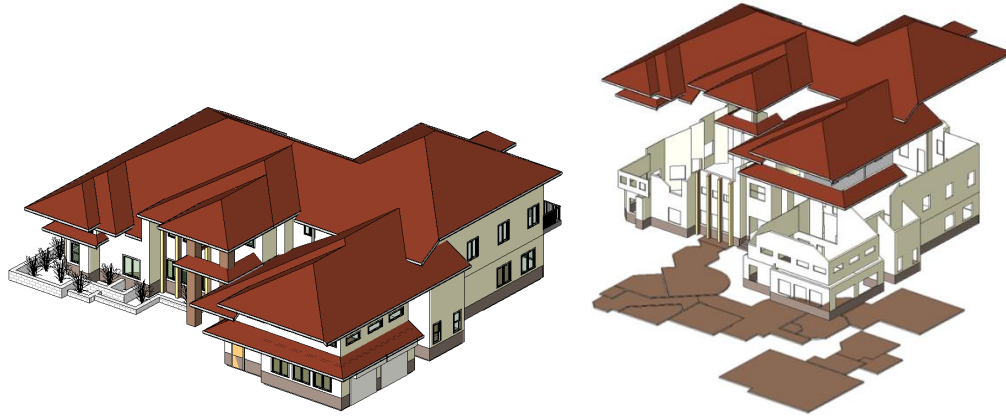


Figure 3 A Building and Components

Furthermore, during the early design stage, there are often multiple options for selecting materials and components that make up a building. This variety of options results in multiple possible solutions, which having a different building cost, construction time, and environmental impact. Decision-making support is often needed to help those professionals participating in the design phase to find optimal solutions that can best satisfy all project objectives. However, current optimization procedures do not consider data uncertainties in productivity, environmental impact, and unit costs of labor, building materials, and equipment; therefore, it is not known how data uncertainties may impact the determination of optimal solutions. Research carefully acknowledged the effect of uncertainties in multi-objective models (e.g., Ghanmi et al. 2007; Feng et al. 2000). Bruni

et al. (2011) addressed the importance of uncertainty and the availability of resources as a constraint to the project's schedule. Currently, there are many computer-based tools that are developed in the AEC industry for aid in sustainable design. However, there is no tool that can help design and construction professionals to optimize material and component selections to successfully satisfy multi-objectives at the building level (Zhu et al. 2012). Moreover, those optimization methods are focused on the pre-use phase without considering environmental impact and cost in the usage phase.

1.2 Problem Statement

The importance of being able to effectively model relationships between multiple objectives in building construction has been emphasized in a wide range of research. Traditionally, decisions have been made to satisfy two main objectives in the construction projects, which are cost and time. Many research studies were conducted to solve and examine the relationship between them (e.g., Hegazy, 1999; Feng et al., 2000; Leu et al., 2001; Chan, 2001; Choudhury & Rajan, 2003; Eshtehardin et al., 2009; Sonmez & Bettemir, 2012). In general, the trade-off relationship between time and cost is well understood and there is ample research on the subject. Moreover, several studies also reveal the trade-off between multiple objectives, such as time, cost, and quality (e.g., Babu et al., 1996; Khang & Myint, 1999; El-Rayes & Kandil, 2005; Afshar et al., 2007; Mungle et al., 2013) However, despite sustainable building designs, relationships between time and environmental impact, as well as cost and environmental impact, have not been fully investigated and further research is required to gain a complete understanding. The studies of time, cost and environmental impact are usually limited to

the pre-use phase. While the usage phase or the occupancy phase supportably account for the largest amount of energy consumption in the building's life cycle, this also contributes to environmental impact (e.g., Cole & Kernan, 1996; Thormark, 2006). Understanding the relationship between these objectives is a key in successfully planning and designing environmentally sustainable construction projects.

1.3 Research Objectives

The objectives of this research are:

1. To analyze and identify relationships of construction time, initial construction cost, and environmental impact, in terms of CO₂ emissions, within different levels of a building: material, component, and building, at the pre-use phase; the manufacturing and construction phase.
2. To analyze and identify relationships between life cycle cost, and life cycle environmental impact, in terms of CO₂ emissions, within the building level at the usage phase.
3. To develop a simulation-based multi-objective decision-support tool, Simulation of Environmental Impact of Construction (SimuleICon), which takes construction data uncertainty into account, and it is capable of incorporating life cycle assessment information to the decision-making process.

1.4 Research Questions and Hypothesis

This research is focused on answering the following questions:

Question #1 Is there an observable relationship between time, cost and CO₂ emissions at different levels of the building? Do the relationships exhibit a trade-off behavior?

Hypothesis #1 There are observable relationships between time and cost, and between CO₂ emissions and time, within each of the three levels of the building; both exhibit trade-off behaviors. There is an observable relationship between CO₂ emissions and cost; however, it does not exhibit a trade-off behavior. This finding can be advantageous to construction and design professionals during the decisions-making process and it encourages further research and analysis on the subject.

Question #2 Is it possible that a dominant solution exists at the material, component or building design level?

Hypothesis #2 The trade-off relationship, observed between time and cost, and between CO₂ emissions and time, greatly reduces the likelihood of the existence of a dominant solution at any level. However, the existence of data uncertainty at the material level allows for a

chance, albeit low, that a dominant solution appears at any of the three levels considered.

Question #3 Does energy consumption at the occupancy phase of a building affect the finding of optimal or near optimal solutions in sustainable building designs?

Hypothesis #3 Disregarding energy consumption leads to ignoring possible materials and components that may lead to savings at the occupancy phase of a building, and thus has a definite impact in the search process for optimal solutions and their outcome.

1.5 Research Significance and Methodology

The methodology presented enables to accurately analyze and identify those relationships. The methodology is applied in the developing of a simulation-based, multi-objective and decision support tool called SimuleICon. This analytical tool is capable of searching for near optimal building design solutions and studying the relationships of time, cost and CO₂ emissions at the material, component and building level of the designs. SimuleICon addresses uncertainty in construction data and integrates energy consumption data for the entire life cycle of a building.

The following steps are critical:

- The creation of a database that contains information on cost, time and CO₂ emissions of materials and components; furthermore, sufficient data for performing life cycle assessment were also gathered. Quantity of each components based on a case study is also needed as the database.
- The uncertainty in the material unit cost, equipment unit cost, labor unit cost, CO₂ emissions, and installation productivity is behaviorally modeled using probability distributions from literature reviews and historical data (Inyim & Zhu, 2013).
- The life cycle assessment and the consideration of energy consumption during the building's usage phase are achieved by performing a building energy simulation.
- The analysis at the building level is examined in two parts; pre-use phase and usage phase. In the pre-use phase, it considers three main objectives, which are construction time, initial construction, and CO₂ emissions. Only life cycle cost and CO₂ emissions are considered in the usage phase since construction time is not necessary. However, different life span of the building is estimated to see the impact to the relationship between life cycle cost and CO₂ emissions.
- The search for optimal design solutions at the building level entails the consideration of millions of possible solutions; optimization of the search process is achieved by using Genetic Algorithms.
- For validation of results generated by SimuleICon, the proposed methodology is applied to two case studies that are already designed and built.

- The relationships between time, cost and CO₂ emissions can be observed by using the pairwise graphs between parameters. These relationships are also tested using statistical models such as regression analysis.

1.6 Dissertation Organization

This dissertation is divided into seven chapters. The first chapter consists of research background, problem statement, research objectives, research questions and hypothesis, research significant and methodology, and organization of the dissertation. The literature review of sustainable building designs, trade-off problems in multiple objectives optimization, genetic algorithms, Monte Carlo simulation, building life cycle assessment tools and building energy simulation is in chapter 2. The framework and description of building levels are provided in the integrated simulation framework for sustainable design chapter. The following chapters are the analysis of relationships between time, cost and environmental impact in the different building levels at the pre-use phase, and the analysis of life cycle cost and life cycle environmental impact at the usage phase. The final chapter includes discussions, conclusions, limitation, and future studies.

CHAPTER 2 LITERATURE REVIEW

2.1 Sustainable Building Designs

Currently, the concept of sustainability is embraced by a wide variety of industries and business (Jung & Joo, 2011). It has been over 20 years since environmental issues became critical in those industries. In 1980, World Conservation Strategy by the International Union of the Conservation of Nature (UCN) in Gland, Switzerland firstly used the word ‘Sustainability’ to intentionally indicate to development of environment purpose (Steele, 1997). In 1987, World Commission on Environment and Development, afterward known as the Brundtland Commission or the Brundtland Report which is named after Gro Harlem Brundtland, reported the critical issues of environmental and development according to the world population growth problems (Brundtland, 1987). This report was aimed to incorporate the concept of sustainability with the principle of economic growth. The sustainability concept was introduced as an integration of environmental, social and economic issues and it was recognized for its significance in addressing the present policies among industries as well as future policies and developments. Moreover, the publication from the commission titled “Our Common Future” recommended that decision-making parties at all levels be required to participate in sustainable development.

In late spring 1992, Agenda 21 was published by Rio Earth Summit. Agenda 21 specially provided 12 recommendation of the management of human settlement as follows (Steele, 1997):

- 1) The use of local materials and indigenous building sources
- 2) Incentives to promote the continuation of traditional techniques, with regional resources and self-help strategies
- 3) Recognition of the toll that natural disasters take on developing countries, due to unregulated construction and use of inadequate materials and the need for improvements both in use and manufacture of materials and in construction techniques, as well as training programs
- 4) Regulation of energy-efficient design principles
- 5) Standards that would discourage construction in ecologically inappropriate areas
- 6) The use of labor-intensive rather than energy-intensive construction techniques
- 7) The restructuring of credit institutions to allow the poor to buy building materials and services
- 8) International information exchange on all aspects of construction related to the environment, among architects and contractors, particularly about nonrenewable resources
- 9) Exploration of methods to encourage and facilitate the recycling and reuse of building materials, especially those requiring intensive energy consumption in their manufacture
- 10) Financial penalties to discourage the use of materials that damage the environment

11) Decentralization of the construction industry, through the encouragement of smaller firms

12) The use of “Clean Technologies”

It is commonly acknowledged today that sustainable development has an important role and has been a significant factor in the architecture, engineering and construction (AEC) industry. Over the years, sustainability has been the focus of many studies. A search of ‘sustainable construction’ in the Google search engine yields over 80 million results. Many definitions of sustainable concept in the AEC industry were reported. Steele (1997) defined sustainable architecture as “a basic definition extends that of sustainability itself, an architecture that meets the needs of the present without compromising the ability of future generations to meet their own needs”. Matar et al. (2010) stated that sustainable construction is an emergent science that combines sustainable concept and construction projects. Several sustainable standards and guidelines for building designs, such as the Building Research Establishment Environmental Assessment Method (BREEAM), Leadership in Energy and Environmental Design (LEED), and Green Building rating System (GBRS), have been established within the AEC industry in order to encourage construction and designs of environmentally sustainable buildings. However, there are numerous research that identify and expose several technical and non-technical obstacles that still hinder widespread adoption.

The practice of sustainable designs in the building sector often referred to as green buildings and it includes features, such as low energy consumption, or low pollution

emissions (GhaffarianHoseini et al., 2013). It brings more players, new construction methods, and advanced designs and analysis into the projects. Furthermore, it requires inter-collaboration between all the involved parties to effectively communicate and share information, including making decisions to serve common goals. Most research and literature, dealing with the delivery of sustainable design projects, identify integrated design as a critical process for the optimization of building systems and fulfillment of project objectives (e.g., Pluaski et al., 2006; Raphael, 2011). When the traditional project system cannot handle the integration of designs, research support that and best performing project delivery practice in the sustainable construction is the integrated project delivery (IPD). It is the system, in which all design and construction professionals working in the building projects associate in the early stage of design construction. In addition, IPD can be developed to support the new trends in the sustainable development of the building designs (Hellmund et al., 2008).

The decision making process for sustainable design projects still relates to the selection of construction methods, materials, crews, and planning, such as resource leveling or scheduling. A particularly critical step in sustainable projects is the selection of the building's components and materials at the design stage, this selection involves the assessment of the impact that these components will have on the sustainable, economic and time related to the project's objectives. The difficulty of this selection process is compounded by the fact that these objectives are often conflicting. Often the wide range of sustainable design options challenges professionals in selecting appropriate building materials and components, which can best satisfy all project objectives. Furthermore,

choosing different construction material assemblies or systems, having different construction time, initial cost, maintenance cost, environmental impacts, etc., can be done in many ways. Moreover, considering these components at the building level presents the additional difficulty that thousands or even millions of design combinations, depending on project size, type and location, are possible; the designer is confronted with the challenge of selecting the optimum design combination of the building components in order to better meet required project's objectives. Cantoni et al. (2000) reported how significant the design phase is because there are many available and reliable options related to optimal plant design. It entails design professionals to encounter design problems in order to find the appropriate components for generating optimal design solutions. Moreover, ecologically sustainable designs are broad. In the AEC industry, the behaviors of the designs change in some such way when it considers environmentally efficient design objectives. This can substantially challenge design and construction professionals in finding suitable multi-objective design solutions.

Bunz et al. (2006) conducted a survey research comparing sustainable design programs and guidelines in North America, Europe and Asia. They posed that building designs should consider the whole life cycle of the buildings and, more importantly, sustainable designs should be implemented in all phases of the building life cycle. However, they highlighted that the most sustainable building programs and guidelines mainly place their focus on the design phase and they supported that these selection considerations in the design phase are essential.

2.2 Trade-off Problems in Multiple Objectives Optimization

The design and planning of construction projects often consider the successful satisfaction and completion of multiple objectives. Traditional objectives considered in construction are project cost and duration. The adoption of the sustainable construction paradigm has introduced another objective and also increased the difficulty of selecting design options that satisfy all objectives. This increment in difficulty calls for further development and optimization of the design, and perceptive decision making process.

There is a significant amount of literature discussing the interdependent relationship of time and cost (Kasprowicz, 1994). Many algorithms for studying time-cost trade-offs have been developed, including heuristic methods (Moselhi, 1993), mathematical programming (Jiang & Zhu, 2010) and more recently evolutionary algorithms including genetic algorithms (GAs) and ant colony optimization algorithms. Besides time-cost trade-off analysis, some studies had also incorporated other objectives into analysis. For example, Khang and Myint (1999) applied linear programming and network simulation to study the time, cost and quality trade-offs. El-Rayes and Kandil (2005) presented a GAs-based method for time, cost, and quantity trade-offs. Similarly, Rahimi and Iranmanesh (2008) discussed the application of the multi-colony ant algorithms and particle swarm optimization to the same subject. Recently, several studies on time, cost and environmental impacts were reported. For

example, Marzouk et al. (2008) applied genetic algorithms to the optimization of time, cost and pollution. Ozcan-Deniz et al. (2011) discussed an analytic framework for time, cost and carbon emission analysis of the building and construction processes by using genetic algorithms.

The advantages and disadvantages of optimization methods have been well-documented in previous studies. Most importantly, evolutionary algorithms have become popular because heuristic methods or mathematical programming methods often fail when dealing with a large number of variables or non-linear objective functions (Elbeltagi et al., 2005). In addition, evolutionary algorithms (EAs) are search-based so they do not need to address the structure of problems, which makes EAs very flexible in applications and easier to apply for trade-off problems.

2.3 Genetic Algorithms

Optimization according to a single objective perhaps rarely exists in existing sustainable building designs. On the contrary, most problems imply multiple objectives. This created a need of effective search techniques in order to find acceptable optimal solutions based on a set of objectives. Evolutionary Algorithms (EAs) are often used to solve multiple objectives' optimization problems because they are able to deal with complex issues, such as discontinuous objective functions, feasible disjoint patterns, and multimodality (Fonseca & Fleming, 1995). Examples of EAs are evolutionary programming, and evolution strategies (Bäck & Schwefel, 1993). Genetic Algorithms (GAs) are a type of evolutionary algorithms and an optimization method based on the

theory of evolution, survival of the fittest and adaptation. They were firstly developed by Holland (1975) with the idea of natural selection. In GAs, possible solutions are treated as individuals and by application of evolution operators this individuals can produce offspring (Magnier, 2008). The Genetic Algorithm (GA) is a stochastic optimization method based on the principles of Charles Darwin's theory of evolution, the survival of the fittest; the GA is comprised of four main parameters which are: number of generations, size of population, crossover rate and mutation rate (Elbeltagi et al., 2005). Many researches proposed this method because it can handle large-scale problems often found in construction projects. The basic functioning of genetic algorithms is as follows:

- 1) Initial solutions are generated
- 2) The fitness of each solution is analyzed and a probability of reproduction is assigned
- 3) Evolution operators are applied to obtain the next generation of solutions
- 4) The process is repeated with the solutions obtained.

The evaluation of the fitness of each solution is of utmost importance as it is the criteria used to ascertain whether generated solutions conform to the optimization objectives. Reproduction is the process by which solutions pass from one generation to another; keeping with the principle of evolution, the fittest solutions are the ones more likely survive. Crossover is an operator that allows the generation of solutions by exchanging characteristics from two other solutions. The mutation operator introduces the possibility of random changes when passing characteristics from parents to their offspring; this allows the possibility of exploring solutions that might be otherwise

overlooked (Camp et al., 1998). Genetic algorithms were utilized in many design optimizations, such as design optimization of trusses (e.g., Rajeev & Krishnamoorthy, 1997; Wang & Ohmori, 2010). Cieniawski et al. (1995) examined multi-objective issues in groundwater monitoring using genetic algorithms. They concluded that genetic algorithms had more advantages over traditional methods. They also used Monte Carlo simulation to randomly generate aquifer parameters and leakage events from presumed distributions. Wang et al. (2007) mentioned that GAs is a powerful technique for solving conflicting multiple objectives in pavement design. Jun and El-Rayes (2010) used GAs in multiple labor shifts problem in construction projects. Multi-objective genetic algorithms can overcome the hindrance of traditional resource leveling algorithms (Leu et al., 2000).

2.4 Monte Carlo Simulation

The Monte Carlo simulation is a method for obtaining solutions to problems where analytical techniques are not available (Farah, 1985). For the design, planning and construction stages of construction projects, there is an inherent uncertainty in the data of construction time, material unit cost, equipment unit cost and labor unit cost as well as in energy consumption and the overall environmental impact. This uncertainty in the data must be accounted in the multi-objective optimization process; otherwise, the validity of the obtained solutions is questionable. Monte Carlo simulations using behavioral modeling of data uncertainty through probability distributions can be applied to the process of determining the optimal solutions for a project.

Several studies acknowledged the effect of uncertainties in multi-objective

models (e.g., Ghanmi et al., 2007; Feng et al., 2000). Bruni et al. (2011) addressed the importance of uncertainty and availability of resources as a constraint to the project schedule. Monte Carlo simulation is a well-known stochastic technique applied commonly to uncertainty analysis. Monte Carlo simulation has been integrated with GAs in order to account for data uncertainty and availability in the real world situation. Lazo et al. (2003) proposed a decision-making model using genetic algorithms and Monte Carlo simulation for oil field development. Monte Carlo simulation was applied to simulate oil prices based on market uncertainties. Babayan et al. (2005) also combined Monte Carlo simulation and genetic algorithms to solve the design of a water distribution system. The results showed that oversight of uncertainty in the stochastic design problems could lead to risk in the design. Many other researchers have also presented their work which applied both genetic algorithms and Monte Carlo simulation, such as finding effective maintenance policies optimization (Marseguerra & Zio, 2000; Marseguerra et al., 2002), modeling knowledge management performance measurement (Kuah et al., 2012), and managing spare part inventories (Marseguerra et al., 2005). Cantoni et al. (2000) presented integration of GAs and Monte Carlo simulation to find optimal designs for several plant design alternatives. They proposed this approach to solve optimization problems under conflicting economic and safety issue.

2.5 Building Life Cycle Assessment Tools

Currently, building sector clearly understands and rapidly develops emerging of the sustainability concept to the building designs. The term of effective building performance is raised as well as the adaptation of standardization of environmental

assessment tools (Cole, 1998). A building performance is affected by many parameters of designs. Environmental considerations have substantially enhanced the number of performance paradigm, indicators, and potential material or product to develop environmental building assessment methods and there are many internationally life cycle assessment tools available raising the acknowledgement of sustainability. They vitally contribute to acknowledge and systematize the importance and linkage between the building and its environmental performance measurement, such as energy consumption (e.g., Cole, 1998; Ding, 2008). Many studies reviewed and provided characteristics of existing LCA tools. For instance, Ding (2008) listed twenty environmental building assessment methods and further summarized that there are two main characters of LCA tools, which are a rating tool and an assessment tool. The rating tool category aims to estimate a level of performances of the buildings based on different criteria, while the assessment tool comprehends environmental agenda in a quantitative measurement.

Examples of life cycle assessment tools are, such as Leadership in Energy and Environmental design (LEED), GreenStar originated from Australia, BEES developed by U.S. National Institute of Standards and Technology (NIST), USA, BREEAM by Building Research Establishment (BRE), UK, EcoEffect by Royal Institute of Technology (KTH), Sweden, ESCALE designed by CTSB and the University of Savoie, France, and Athena Building Impact Estimator by Athena Sustainable Materials Institute, Canada, presented in Table 1, which they greatly help to support sustainability in the building designs (Haapio & Viitaniemi, 2008).

Those tools are designed and developed for different purposes, such as for existing buildings, for new buildings, and building products. Haapio and Viitaniemi (2008) studied and categorized most life cycle assessment tools. Their study showed that the existing life cycle assessment tools were purposed on various types of buildings, they were relied on different guidelines. Some of them also might not completely cover the whole cycle life information. Table 2 summarized building types and life cycle phases covered by different life cycle assessment tools (e.g., Haapio & Viitaniemi, 2008; Ding, 2008).

Table 1 Example of Environmental Building Performance Assessment Methods

Environmental Assessment Methods		Developer/ Origin
ABGR	Australian Building Greenhouse Rating	Department of Commerce, NSW 2005
AccuRate		CRIRO 2006
Athena	Athena Impact Estimator for Buildings	Athena Sustainable Material Institute, Canada
BASIX	Building Sustainability Index	Department of Infrastructure, Planning and Natural Resources 2004
BEAT 2002		Danish Building Research Institute

Environmental Assessment Methods		Developer/ Origin
		(SBI), Denmark
BeCost	LCA-house	VTT, Finland
BEES 4.0		NIST, USA
BEPAC	Building environmental performance assessment criteria	Canada 1993
BREEAM	Building Research Establishment	UK
CASBEE	Comprehensive assessment system for building environmental efficiency	Japan 2004
CEPAS	Comprehensive environmental performance assessment scheme	HK 2001
CPA	Comprehensive project evaluation	UK 2001

Environmental Assessment Methods		Developer/ Origin
DQI	Design quality indicator	UK 2001
EcoEffect		Royal Institute of Technology, Sweden
EcoProfile		Norwegian Building Research Institute, Norway
EcoQuantum		Netherlands
EMGB	Evaluation manual for green buildings	Taiwan 1998
Envest 2		Building Research Establishment, UK
EPGB	Environmental performance guide for building	Department of Public Works and Services, NSW
ESCALE		France
GbTool	Green building challenge	International 1995
GHEM	Green home evaluation manual	China 2001
GreenStar		Green building council

Environmental Assessment Methods		Developer/ Origin
HKBEam	Hong Kong building environmental assessment method	Hong Kong 1996
LEED®	Leadership in energy and environmental design	USA 200
LEGEP®	Legoe	University of Karlsruhe, Germany
NABERS	National Australian building environmental rating system	Department of Environmental and Heritage 2001
NatHERS		CSIRO
PAPOOSE		TRIBU, France
SBAT	Sustainable building assessment tool	South Africa
SPeAR	Sustainable project appraisal routine	
TEAM ^{TMa}		Ecobilan, France

Table 2 Review of Building Environmental Assessment Tools

Life Cycle Assessment Tool	Assessed Buildings						Phases of Life Cycle								
	Other type of building	Office building	Residential building (single family)	Residential building (Multi-unit)	Buildings	Building product/ component	Refurbishment of a Building	New Building	Exiting Building	Production	Construction	Use/ Operation	Maintenance	Demolition	Disposal
BEES 4.0						✗									
TEAMTM					✗	✗									
ATHENA	✗	✗	✗	✗			✗	✗	✗						
BEAT 2002					✗	✗	✗	✗	✗						
BeCost					✗	✗									
Eco-Quantum			✗		✗										
Envest 2			✗												
EQUER	✗	✗	✗							✗	✗	✗	✗	✗	✗
LEGEP®									✗	✗	✗	✗	✗	✗	✗
PAPOOSE	✗	✗	✗	✗	✗	✗									
BREEAM	✗	✗	✗	✗			✗	✗	✗	✗	✗	✗	✗	✗	✗
EcoEffect	✗	✗	✗	✗			✗	✗	✗	✗	✗	✗	✗	✗	✗
EcoProfile	✗	✗	✗	✗					✗	✗	✗	✗	✗	✗	✗
ESCALE	✗	✗	✗	✗						✗	✗	✗	✗	✗	✗
LEED®	✗	✗	✗	✗					✗	✗	✗	✗	✗	✗	✗

2.6 Building Energy Simulation

The building energy simulation was firstly introduced and developed in the mid 1960's for the purpose of energy consumption calculation in buildings (Van der Veken et al., 2004). The first simulation methods used at that time neglected the building and the system synergy. By the end of 1970s, building energy simulation programs were further developed; examples of simulation methods are EPW, TRANSYS, ESP-r, DOE-2, and BLAST (Spencer, 2010). In the United States, the congress authorized the Energy Independence and Security Act of 2007 to support and persuade the construction of the zero-net-energy buildings by 2030 (Kassab, 2008). This encourages the use of energy simulation in the construction projects. There has been an improvement in energy simulation tools; for instance, DOE-2 and BLAST features were taken to develop a new building simulation tool called EnergyPlus, which was completely rewritten new in Fortran 90 language. Crawley et al. (2001) stated the significant of this new program over DOE-2 and BLAST, such as realistic system controls, and radiant heating, and cooling system. DOE-2 and BLAST are a step sequential simulation, while EnergyPlus is an integrated system simulation. It is not only a combination of previous features, but also a development of computation techniques, program, and structures.

Jingran Ma et al. (2011) studied the model predictive control (MPC) using EnergyPlus and a co-simulation program, the building controls virtual test bed (BCVTB), in the system framework in order to indicate an effectiveness of the reducibility in the energy cost and demand cost in the model. EnergyPlus was used, compared and integrated with computer algorithms in various researches (e.g., Andolsun et al., 2011;

Kämpf et al., 2010; Wang et al., 2009; Zhu, 2006). EnergyPlus is widely used because it can provide all general basic function in comparison with other energy simulation programs.

Another energy simulation program that is commonly applied in building energy simulation is eQUEST. The program was developed to be a user-friendly tool while it can incorporate features from DOE-2.2. The latest version of eQUEST is version 3.64 released in 2010. Yu et al. (2008) mentioned that eQUEST has expansion capabilities beyond DOE-2.2. He demonstrated these capabilities by applying eQUEST to residential building analysis for different climate zones in China. eQUEST can provide energy savings results as the effects of envelope factors. Sclafani (2010) also used eQUEST to predict future energy consumption based upon historical weather data. He focused on the effect of weather data and energy performance. Crawley et al. (2008) presented twenty building energy performance simulation programs, listed in table 3, and they also compared their performances in various features.

Table 3 Examples of Building Energy Simulation Programs

Programs		Developers
BLAST		University of Illinois at Urbana-Champaign
BSim	Building Simulation	Danish Building Research Institute

Programs		Developers
DeST		Tsinghua University
DOE-2		Lawrence Berkeley National Laboratory
ECOTECT	Autodesk® Ecotect® Analysis	AUTODESK
Ener-Win	Energy Simulation Software for Buildings	Texas A&M University & Degelman Engineering Group, Inc.
Energy Express		CSIRO
Energy-10		National Renewable Energy Laboratory
EnergyPlus	EnergyPlus Energy Simulation Software	U.S. Department of Energy
eQuest	The Quick Energy Simulation Tool	U.S. Department of Energy
ESP-r	Energy Systems Research	University of Strathclyde
HAP	Hour Analysis Program	Carrier Software Systems, Carrier Corporation

	Programs	Developers
HEED	Home Energy Efficient Design	University of California, Los Angeles

CHAPTER 3 AN INTEGRATED SIMULATION FRAMEWORK FOR SUSTAINABLE DESIGN ANALYSIS

The proposed methodology enables to accurately analyze and identify relationships of time, cost and environmental impact, in terms of CO₂ emissions. The methodology is applied in the developing of a tool named Simulation of Environmental Impact of Construction or SimuleICon. This tool is designed to help construction and design professionals in the construction projects to find the optimal or near optimal design solutions during the selection process of a building components based on multiple objectives. SimuleICon simulates and generates results using non-dominated sorting genetic algorithm-II (NSGA-II), which is one of well-known GAs. Sets of optimal or near optimal solutions are obtained by considering multiple objectives. SimuleICon can be used to observe those relationships at the different levels; material, component and building level. SimuleICon addresses the uncertainty in the construction data by applying Monte Carlo simulation to database and integrates energy consumption information, in terms of energy consumption cost and energy related CO₂ emissions, for the entire life cycle of a building. The following steps are critical:

- The creation of a database that contains information on cost, time and CO₂ emissions of materials and components; furthermore, sufficient data for performing life cycle assessment were also gathered. Quantity of each components based on a case study is also needed as the database.

- The uncertainty in the material unit cost, equipment unit cost, labor unit cost, CO₂ emissions, and installation productivity is behaviorally modeled using probability distributions from literature reviews and historical data.
- The life cycle assessment and the consideration of energy consumption during the building's usage phase are achieved by performing a building energy simulation.
- The analysis at the building level is examined in two parts; pre-use phase and usage phase. In the pre-use phase, it considers three main objectives, which are construction time, initial construction, and CO₂ emissions. Only life cycle cost and CO₂ emissions are considered in the usage phase since construction time is not necessary. However, different life span of the building is estimated to see the impact to the relationship between life cycle cost and CO₂ emissions.
- The search for optimal design solutions at the building level entails the consideration of millions of possible solutions; optimization of the search process is achieved by using Genetic Algorithms.
- For validation of results generated by SimuleICon, the proposed methodology is applied to two case studies that are already designed and built.
- The relationships between time, cost and CO₂ emissions can be observed by using the pairwise graphs between parameters. These relationships are also tested using statistical models such as regression analysis.

3.1 Material Level

Data granularity of the SimuleICon database starts at the building material level, such as the quantity of each material used in an activity, unit cost, productivity, and environmental impact per unit, shown in figure 4, as an input to Monte Carlo simulation. Examples of data are the mean unit costs obtained from RS Means and the average CO₂ emissions per material unit from the Athena Impact Estimator for Buildings software tool. Most importantly, all data are behaviorally modeled using probability distributions based on various parameters and used to simulate CO₂ emissions per material unit, productivity and unit cost of materials. In order to use the Monte Carlo simulation technique, established distributions of parameters are needed, which can be simply generated from historical data. However, in reality, the historical data of unit cost, productivity and CO₂ emissions of the same material, component or building and construction operations are very difficult to obtain due to the one-time nature of the buildings and their construction. Instead of using the historical data, the recommended probability distributions from the literature were used to derive the probability distributions of the database in order to describe its likelihood to occur. For example, triangular distributions, beta distributions and lognormal distributions have been commonly used to describe the construction cost function. Back et al. (2000) used the triangular distribution to fit the cost data for a case study project in Texas. They also tested the fitness of the distribution with three methods, the least-square method, the maximum likelihood method, and the moment matching method, to find the most accurate technique for estimating distribution parameters. On the other hand, Sonmez

(2005) reviewed that the beta distribution was the best fit for construction cost. The example of using the lognormal distribution simulating the construction cost comparing with other distributions was also conducted by Touran and Wiser (1992). The beta distribution was suggested for suitably presenting construction time as well (e.g., AbouRizk et al., 1991; Fente et al., 1991; Schexnayder et al., 2005). The normal distribution was suggested for modeling data of CO₂ emissions since the maximum and the minimum of CO₂ emissions were not always obvious to define (e.g., Rypdal & Winiwarter, 2001; Goedkoop et al., 2009; Peña-Mora et al., 2009). All parameters in the database including the quantity, unit cost, productivity, and CO₂ emissions per material unit along with their probability distributions are required as an initial input to the application. The database from the material level is also analyzed and described in detail in the next chapter.

3.2 Component Level

The data at the material level are used to calculate construction time, initial construction cost, and carbon emissions for alternatives at the component, or assembly level. For each component, there are possibly several material options to form different assembly or component solutions. For example, exterior walls can be structure insulation panels (SIPs) or a steel studs wall, or a wood studs wall, with different types of drywalls and insulations. The data from the material level are incorporated with quantities of components in order to get the output at this level, which are construction duration, cost and CO₂ emissions of component's alternatives. Generally, quantity can be festinated by

performing quantity taking-off from the project's drawings or retrieving a data from a BIM model if the model is available.

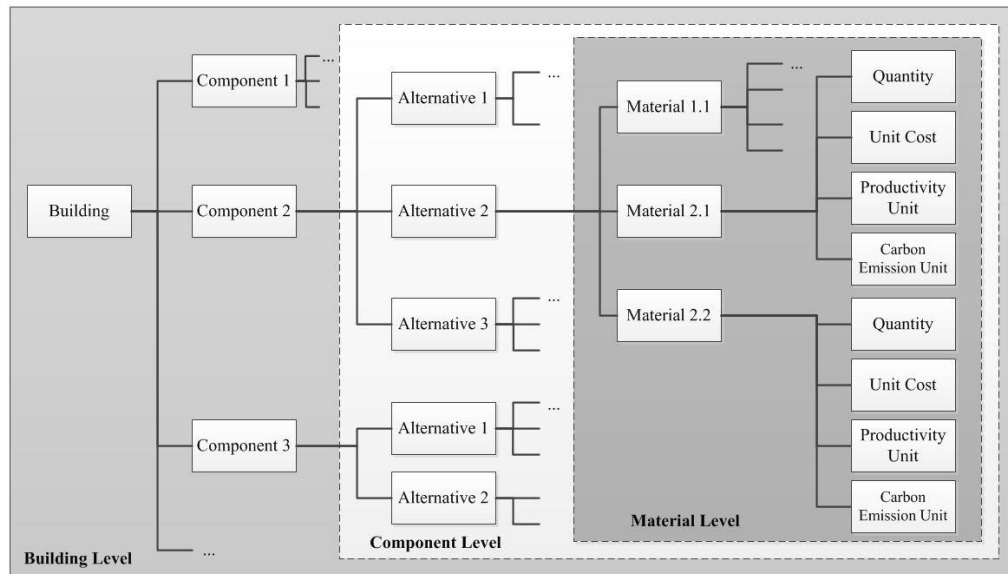


Figure 4 Information at the Different Levels from the Material Level, the Component Level, to the Building Level.

3.3 Building Level

The components' alternatives are the basic unit of analysis and the variables for GAs at this level. Different optimal or near optimal building designs based on available components' alternatives are searched in the optimization process. In this research, Non-Dominating Sort Genetic Algorithm-II (NSGA-II) is used as an optimization model. NSGA-II can greatly handle non-linear programming problem. It is the most commonly applied to the multiple objectives' optimization and it is also widely used in sustainable building design (Evins, 2013). NSGA-II provides optimal or near optimal solutions based on the number of population and generation. In this research, building life cycle was

separated into two phases which are the pre-use phase and the usage phase. At the pre-use phase analysis, three objective functions are considered which are 1) minimizing initial construction cost (C), 2) minimizing construction time (T), and 3) minimizing CO₂ emissions in the project (EI). Optimization models for NSGA-II are shown below.

Decision Variables:

$$x_i^m \triangleq \text{Alternatives of component } i \text{ and } m = \text{alternative number}$$

$$i = 1, 2, 3, \dots, k, \text{ where } k = \text{number of project components}$$

Objective Functions:

$$C = \min\left\{\sum_{i=1}^k c_{x_i^m} \times Q_i\right\}$$

$$T = \min\{\max(st_i + d_i | i = 1, 2, \dots, k)\}$$

$$EI = \min\left\{\sum_{i=1}^k ei_{x_i^m} \times Q_i\right\}$$

$$\text{s.t. } st_j > st_i + d_i, > i \forall j \in S_i, \text{ and } ES_i < st_i < LS_i$$

where $d_i = \frac{Q_i}{P_{x_i^m}}$; T= Total construction time; st_i = Start date of component i ; d_i =

Duration of component i ; Q_i = Quantity of component i ; $P_{x_i^m}$ = Productivity of component i and alternative m ; ES_i = Early start of component i ; LS_i = Late start of component i ; C = Total initial construction cost, $c_{x_i^m}$ = Initial construction cost of component i and

alternative m ; EI = Total CO_2 emissions of the project; $ei_{x_i^m}$ = CO_2 emissions of component i and alternative m .

Moreover, Mont Carlo simulation is utilized at this phase. The number of sets of optimal solutions generated by the NSGA-II algorithm is directly related to the 'n' number of Monte Carlo simulations inputted by the users. For the usage phase, the construction time is not considered as the main objective since it does not have an effect on the operation of the building. However, different year-life spans of the building are considered to see the impact of operating time to the relationship between life cycle cost and CO_2 emissions. Also different year-life span will provide different maintenance cost, energy consumption cost, and energy consumption related CO_2 emissions. The energy simulation is incorporated in the usage phase at the building level to find yearly energy consumption based on different building designs. The two objective functions are 1) minimizing life cycle cost (C), and 2) minimizing life cycle CO_2 emissions (EI) in the project. Optimization models for NSGA-II are shown below.

Decision Variables:

$$x_i^m \triangleq \text{Alternatives of component } i \text{ and } m = \text{alternative number}$$

$$i = 1, 2, 3, \dots, k, \text{ where } k = \text{number of project components}$$

Objective Functions:

$$C_l = \min\{\sum_{i=1}^k \left((c_{x_i^m} \times Q_i) + (C_{x_i^m}^e + C_{x_i^m}^m) \times Y \right)\}$$

$$EI_l = \min\left\{\sum_{i=1}^k \left((ei_{x_i^m} \times Q_i) + (ei_{x_i^m}^e \times Y) \right)\right\}$$

where $d_i = \frac{Q_i}{P_{x_i^m}}$; T = Total project duration; st_i = Start date of component i ; d_i = Duration of component i ; Q_i = Quantity of component i ; C_1 = Total life cycle cost, $c_{x_i^m}$ = Initial construction cost of component i and alternative m ; $C_{x_i^m}^e$ = Energy consumption cost per year of component i and alternative m ; $C_{x_i^m}^m$ = Maintenance cost per year of component i and alternative m ; EI_1 = Total life cycle CO₂ emissions of the building; $ei_{x_i^m}$ = CO₂ emissions of component i and alternative m ; $ei_{x_i^m}^e$ = Energy related CO₂ emissions of component i and alternative m ; Y = Life span of the building.

Figure 5 shows the time, cost and environmental impact analysis for sustainable design at multiple building levels in the flowchart. Three different levels of the building analysis are presented. The process, input and output of each analysis are displayed as well.

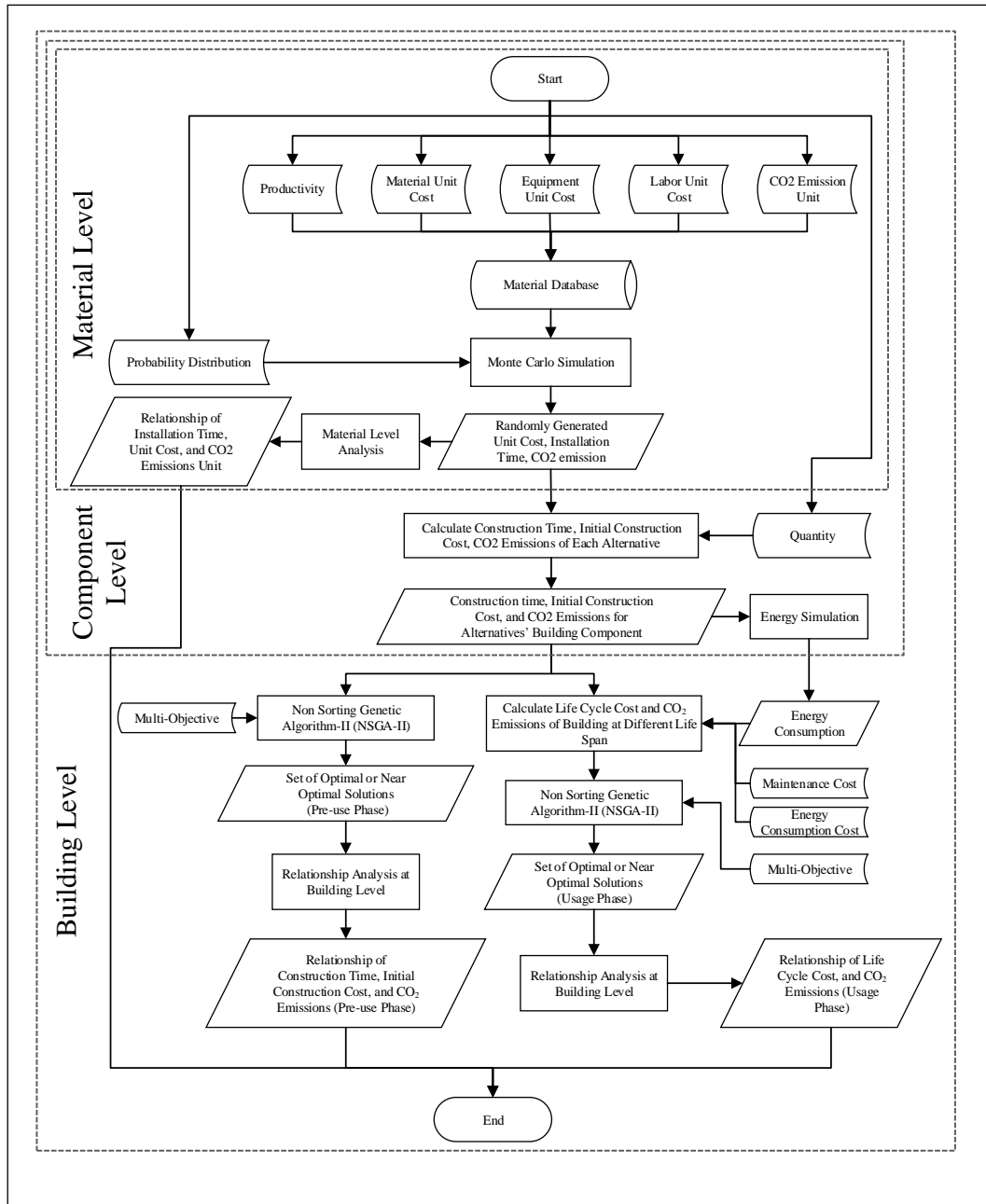


Figure 5 Time, Cost, and Environmental Impact Analysis for Sustainable Design at Multiple Building Levels Flowchart

CHAPTER 4 ANALYSIS OF TIME, COST AND ENVIRONMENTAL IMPACT RELATIONSHIPS AT BUILDING MATERIAL LEVEL

The objectives of this chapter are mainly to determine data patterns of time, cost and environmental impact, in terms of CO₂ emissions, and observe the level of confidence that a dominant alternative exists in any material category at the material level. In this study, time, cost and CO₂ emissions of a material alternative are represented by productivity, unit cost and CO₂ emissions per material unit respectively. To achieve the objectives, this study was designed to answer the following questions:

- 1) What is the level of confidence that a dominant alternative exists in a material category selected for this study? A dominant alternative is the one in a material category, whose unit cost and CO₂ emissions per material unit are the smallest, and the installation productivity is the largest, among all other alternatives in the same category. As an optimization process always seeks a dominant alternative in each material category, if there is a dominant alternative in each material category, the optimal solutions at building level most likely converge to a limited number of options. Given the fact that the previous case study did not show such a convergence (Zhu et al, 2012), it was believed that it is highly likely that not all material categories have a dominant solution. The key issue is the level of confidence to this observation. If the level of confidence is high, it can be inferred that trade-off relationships of time, cost and CO₂ emissions also exist at the material level.

- 2) If productivity and unit cost of all material in the same category are sorted by CO₂ emissions per material unit, are there any clear data patterns? Answers to this question can help to demonstrate relationships of time, cost and CO₂ emissions of all materials in a material category, which complements any observations or answers to the first question.

In addition, the study consists of two scenarios to observe the impact of machine and equipment use during the construction or installation phase of a project. In other words, one scenario only includes unit costs and CO₂ emissions per material unit without considering the installation data of materials. The second scenario not only includes unit costs and CO₂ emissions per material unit, but also considers corresponding data of operator unit cost, equipment unit cost, CO₂ emissions per material unit from the installation phase or construction phase of materials, and installation time. The comparison of the two scenarios helps to understand how much installation methods contribute to changes in any relationship of time, cost and environmental impact that is observed in the first scenario.

4.1 Data Collection and Preparation

4.1.1 Data Scope and Sources

In this chapter, six categories of building envelope materials are studied, including structural components, exterior cladding, insulation, roofing, concrete footings, and concrete slabs-on-grade. All material alternatives in each category are compared at the same functional unit. For example, exterior cladding materials are compared using per

square foot, insulation materials are compared using the same thermal resistance value or R-value, and concrete materials are studied in per cubic foot. Table 1 shows the alternatives in each category.

Each alternative has three important pieces of data: unit cost, productivity, and CO₂ emissions per material unit. Unit cost data include material unit cost, labor unit cost, and equipment unit cost. Productivity and unit cost data were mostly collected from the RS Means Building Construction Cost Data. Market productivity and cost data were also collected for verification purposes. The CO₂ emission data were derived from the Athena Impact Estimator for Buildings, which cover life cycle phases mainly up to the manufacturing phase of building materials. CO₂ emissions due to construction phase were estimated based on hours of equipment use and the environmental impact of fuel consumption. The selection of data was also constrained by the availability of life cycle inventory data published in third-party sources and literature such as Athena handbook. In many cases, environmental impact data were not available for many construction materials or processes, even though cost and productivity data were mostly available. Therefore, only the materials listed in table 1 were selected for this study. Details of data processing are discussed in the following section.

Table 4 Material Alternatives and Categories

Category	Description	Alt.	Description

Category	Description	Alt.	Description
1	Structural Component	1	Steel Stud
		2	Wood Stud
		3	Concrete Block Wall
2	Exterior Cladding	1	Cedar Bevel
		2	Concrete Brick
		3	Fiber Cement
		4	Metric Modular Brick
		5	Natural Stone
		6	Stucco
		7	Vinyl
3	Insulation	1	Expanded Polystyrene
		2	Extruded Polystyrene
		3	Blown Cellulose

Category	Description	Alt.	Description
		4	Batt Rockwool
		5	Batt Fiberglass
		6	Foam Polyisocyanurate
4	Roofing	1	Clay Tiles
		2	Concrete Tiles
		3	Organic Felt Shingles 30 yr
		4	Roof Steel Panels
5	Concrete Footing	1	3000 psi, average flyash
		2	3000 psi, 25% flyash
		3	3000 psi, 35% Flyash
		4	4000 psi, average Flyash
		5	4000 psi, 25% Flyash
		6	4000 psi, 35% Flyash

Category	Description	Alt.	Description
6	Concrete Slab-on-grade	1	4 inches, 3000 psi, average Flyash
		2	4 inches, 3000 psi, 25% Flyash
		3	4 inches, 3000 psi, 35% Flyash
		4	4 inches, 4000 psi, average Flyash
		5	4 inches, 4000 psi, 25% Flyash
		6	4 inches, 4000 psi, 35% Flyash
		7	8 inches, 3000 psi, average Flyash
		8	8 inches, 3000 psi, 25% Flyash
		9	8 inches, 3000 psi, 35% Flyash
		10	8 inches, 4000 psi, average Flyash
		11	8 inches, 4000 psi, 25% Flyash
		12	8 inches, 4000 psi, 35% Flyash

4.1.2 Data Preparation

1) Material Installation Time Since this chapter is focused on the building materials, the construction time was only referred to as a material installation time, which can be estimated by using the productivity of material installation, and the quantity of a particular material or, in this case, the functional unit of material. The RS Means Building Construction Cost Data provides productivity data of building materials, in terms of a daily output (unit/day). Additionally, installation time is only considered in the second scenario of this study.

2) Construction Cost Construction cost can be estimated by multiplying the unit cost and the quantity of materials. In scenario 1, the unit cost only refers to the material unit cost, as shown in table 2; while, in scenario 2, the unit cost, including material, labor and equipment unit costs, are considered.

3) Environmental Impact The Athena Impact Estimator for Buildings (version 4.5) was used in this study to generate data of environmental impact, in terms of CO₂ emissions, as kg CO₂ equivalent per material unit. The database of Athena can capably model a construction project with over 1,500 structural components and building envelopes (Athena Sustainable Material Institute, 2013). Results from the program include typical impact categories, fossil fuel consumption (MJ), global warming potential (kg CO₂ eq), acidification potential (kg SO₂ eq), HH Particulate (kg PM_{2.5} eq), eutrophication potential (kg N eq), ozone depletion potential (kg CFC-11 eq), and smog

potential (kg O₃ eq). Currently, as mentioned before, the only environmental impact considered in this research was CO₂ emissions.

CO₂ emissions, reflecting the manufacturing phase of materials, were used in Scenario 1; while scenario 2 also included CO₂ emissions from the use of equipment during the installation phase. Crew types, provided by the RS Mean Building Cost Data, were used to gather equipment information in order to estimate CO₂ emissions from equipment used during construction. Table 5 shows a summary of the two scenarios.

Table 5 Summary of the Two Scenarios

Scenario	Time (hours)	Cost (\$)	CO ₂ Emission (kg CO ₂ eq)
1	-	Material unit cost	CO ₂ emissions per material unit from the manufacturing phase
2	Installation time	Material unit cost + labor unit cost + equipment unit cost	CO ₂ emissions per material unit from manufacturing + CO ₂ emissions per material unit from installation

Additionally, input data for each material need to be aligned because data disparities had been identified between the two major data sources, the RS Means Building Construction Cost Data and Athena Impact Estimator for Building, which

occasionally provide data in different units. For instance, insulation materials need to have the same equipotential function for meaningful comparisons. Thus, instead of using area in square foot or thickness in inch, thermal resistance value (R-value) was applied as a functional unit for the insulation category. However, all six chosen alternatives had varied R-values. The foam polyisocyanurate had lowest conductivity (Btu/h-ft-F) or the highest R-value (h-ft-F/Btu), which was selected as the base value in this category. All other alternatives were adjusted to match this R-value. Since Athena allows users to input the desired thickness of materials to derive environmental impact data based on a specific R-value ($\text{h-}^\circ\text{F- ft}^2/\text{Btu}$), the thickness (inches) of other insulation materials was first calculated to match the R-5.15 of foam polyisocyanurate by using thermal conductivity data ($\text{Btu/h-ft-}^\circ\text{F}$), and it was also used as input data to derive CO₂ emissions from Athena. On the other hand, RS Means provides cost data based on specific thicknesses and R-values, such as fiberglass 3 ½ inches thick with R-11, or fiberglass 6 inches thick with R-19. Cost data and thickness values from RS Means were plotted to find relationship functions between them by using the traditional curve fitting technique. Without any other information, unit cost data for insulation materials were estimated by interpolation based on the curve fitting function and the previously calculated thicknesses data of insulation materials in Athena.

Another example is fiber cement siding in the exterior cladding category. There are more than ten options of fiber cement siding with different textures at the MasterFormat level 4 in RS Means; while Athena only provides information at the MasterFormat level 2. To match the CO₂ emission scope of Athena (MasterFormat level

2), costs at the MasterFormat level 4 from RS Means were first grouped to match the level 3 and level 2 classifications for CO₂ emissions; then costs in each level of classification were averaged to match the CO₂ emission data. The roofing category used the same approach for matching data as well as exterior cladding, while structural component, concrete footing, and concrete slab-on-grade category can similarly match data from RS Means and Athena at the same level of information.

4.2 Additional Data Generation

In general, data sources, such as the Athena database and RS Means, provide average data in a local or nation context. In order to determine the level of confidence regarding an observed pattern, uncertainties in unit costs, CO₂ emissions, and construction productivities need to be addressed. Due to limitations of data availability, the Monte Carlo simulation was used for additional data generation and uncertainty propagation. In this research, the beta distribution was used for describing the functions of unit costs and productivities, and the normal distribution was applied to model data distribution of CO₂ emissions per material unit.

The mean values (\bar{x}) of probability functions in both beta distributions and normal distributions were defined by using data from Athena and RS Means. Moreover, in this research, historical data from 25 school projects, which are located in the Miami-Dade county area, were collected to identify the maximum and minimum possible range of unit costs and installation time. The total cost of the projects ranged from \$63,000 to \$12,000,000. If the historical data from school projects existed, maximum and minimum

values were set based on the historical data, otherwise a range of 20% from the mean value was utilized (e.g., Nasir et al., 2003; Rypdal & Winiwarter, 2001; Rypdal & Flugsrud, 2001; Winiwarter & Rypdal, 2001). For example, from historical data, there was maximum duration to install one square foot of fiberglass insulation, as well as minimum and maximum unit cost of fiberglass insulation. Thus, the missing data of minimum installation time was determined at 20% less than the average installation time derived from RS Means' data. Mean, maximum, and minimum values were used to calculate the standard deviation (ρ) of the normal distribution and the variance (s^2) of the beta distribution. Moreover, alpha (α) and beta (β) were also calculated as input parameters for the beta distribution as shown in Table 3 (e.g., Owen, 2008; MathWorks, 2014). Furthermore, installation time (hours) was estimated by using productivity from RS Means and a quantity of material.

In the Monte Carlo simulation, inverse cumulative distribution functions were utilized in order to find representative unit costs, time, and CO₂ emissions per material unit. The Monte Carlo simulation started by randomly generating a number ranging from 0 to 1 for variables, i.e., material unit cost, labor unit cost, productivity, and CO₂ emissions per material unit. Thus, by using the inverse cumulative distribution functions, the generated numbers are interpolated to represent unit costs, productivity, and also CO₂ emissions per material unit in each simulation run.

Table 6 Summary Functions Representing Variables' Distribution

Variables	Inverse Cumulative Distribution Function	Input Parameter	Source
Cost	Beta Distribution; $x = F^{-1}(p \alpha, \beta) = \{x: F(x \alpha, \beta) = p\}$ where $p = F(x \alpha, \beta) = \frac{1}{B(\alpha, \beta)} \int_0^x ty^{\alpha-1} (1-t)^{\beta-1} dy$ and $B(\alpha, \beta)$ is called beta function converges for $\alpha > 0$ and $\beta > 0, 0 < p < 1$	\bar{x} (mean)	RS Means
		max	historical data and literature review
		min	historical data and literature review
		s^2 (variance)	mean, max, and min value
		α	$\bar{x} \left(\frac{\bar{x}(1-\bar{x})}{s^2} - 1 \right)$
		β	$(1-\bar{x}) \left(\frac{\bar{x}(1-\bar{x})}{s^2} - 1 \right)$
Time	Beta Distribution; $x = F^{-1}(p \alpha, \beta) = \{x: F(x \alpha, \beta) = p\}$ where $p = F(x \alpha, \beta) = \frac{1}{B(\alpha, \beta)} \int_0^x ty^{\alpha-1} (1-t)^{\beta-1} dy$ and $B(\alpha, \beta)$ is called beta function converges for $\alpha > 0$ and $\beta > 0, 0 < p < 1$	\bar{x} (mean)	RS Means
		max	historical data and literature review
		min	historical data and literature review
		s^2 (variance)	mean, max, and min value

Variables	Inverse Cumulative Distribution Function	Input Parameter	Source
		α	$\bar{x} \left(\frac{\bar{x}(1 - \bar{x})}{s^2} - 1 \right)$
		β	$(1 - \bar{x}) \left(\frac{\bar{x}(1 - \bar{x})}{s^2} - 1 \right)$
CO ₂ emissions per material unit	Normal Distribution; $x = F^{-1}(p \mu, \sigma) = \{x: F(x \mu, \sigma) = p\}$ where $p = F(x \mu, \sigma) = \frac{1}{\sigma\sqrt{2\pi}} \int_{-\infty}^x e^{-\frac{(t-\mu)^2}{2\sigma^2}} dy, -\infty < \mu < \infty, \sigma > 0, \text{ and } 0 < p < 1$	μ (corresponding mean)	Athena Impact Estimator
		max	literature review
		min	literature review
		σ (standard deviation)	corresponding mean, max, and min value

4.3 Level of Confidence

The level of confidence of material alternatives were evaluated based on the frequency of a material alternative being selected as a dominant option using the Monte Carlo simulation. In scenario 1, the formula that was used to determine the frequency of dominant occurrence of materials in each material category is,

$$\sum_{j=1}^m f(x_j^i) = \begin{cases} 1 & \text{if } \begin{cases} C_{x_j^i} = \min(C_{x_j^1}, \dots, C_{x_j^n}) \\ EI_{x_j^i} = \min(EI_{x_j^1}, \dots, EI_{x_j^n}) \end{cases} \\ 0 & \text{for other} \end{cases}$$

subject to $i = 1, \dots, n$ and $j = 1, \dots, m$

where x_j^i = variable alternative i with j^{th} Monte Carlo simulation, $C_{x_j^i}$ = unit cost of x_j^i (\$), $EI_{x_j^i}$ = CO₂ emissions per material unit of x_j^i (kg CO₂ eq), n = number of alternative in category, and m = number of Monte Carlo simulation.

In scenario 2, the material installation time was included in the analysis. Thus, objective function will consider the third parameter as shown below.

$$\sum_{j=1}^m f(x_j^i) = \begin{cases} 1 & \text{if } \begin{cases} T_{x_j^i} = \min(T_{x_j^1}, \dots, T_{x_j^n}) \\ C_{x_j^i} = \min(C_{x_j^1}, \dots, C_{x_j^n}) \\ EI_{x_j^i} = \min(EI_{x_j^1}, \dots, EI_{x_j^n}) \end{cases} \\ 0 & \text{for other} \end{cases}$$

subject to $i = 1, \dots, n$ and $j = 1, \dots, m$

where x_j^i = variable alternative i with j^{th} Monte Carlo simulation, $T_{x_j^i}$ = installation time of x_j^i (hours), $C_{x_j^i}$ = unit cost of x_j^i (\$), $EI_{x_j^i}$ = CO₂ emissions per material unit of x_j^i (kg CO₂ eq), n = number of alternative in category, and m = number of Monte Carlo simulation.

4.4 Pattern Analysis

In order to study patterns among cost, installation time and CO₂ emissions, the average value of those data generated from the Monte Carlo simulation were first plotted in pairwise graphs between time and CO₂ emissions per material unit, as well as unit cost and CO₂ emissions per material unit. Observable patterns were then further analyzed by using the concept of trade-off patterns.

Firstly, the analysis studied the patterns using average values, as shown in the examples of structural component, roofing and concrete footing 3,000 psi in figures 6, 7 and 8. The average values were derived based on the Monte Carlo simulation as discussed previously. Examples show that, when all materials in each category are considered, trade-off relationship does not obviously exist. However, trade-off relationships do seem to exist in subsets of materials in each category. For example, in figure 6, the wood stud alternative dominates the other two options based on average values. Nevertheless, if the wood stud alternative is not considered, it seems that a trade-off relationship exists between the concrete block alternative and the steel stud alternative. Other material categories have a similar pattern.

Moreover, in one material category, multiple data patterns may exist. For example, in the roofing category, options such as organic felt shingles, concrete tiles and clay tiles may form non-trade-off relationships or direct variation relationships between them, but roof steel panels may have trade-off relationships with other options as shown

in figure 7. Figure 8 presents an example of general relationship behaviors for the concrete material.

For each of the above data patterns, a statistical analysis was performed to determine its probability using the data from the Monte Carlo simulation, including

1. A trade-off relationship when all materials are considered,
2. A trade-off relationship when a subset of materials is considered, and
3. Existence of multiple relationships when all materials are considered.

In scenario 1, a trade-off relationship exists when one alternative has one higher variable and one lower variable than another. In scenario 2, if an alternative does not have all three variables higher or lower than another, there is a trade-off relationship between two alternatives. The equations used to determine trade-off relationships in scenarios 1 and 2 are shown below.

Scenario 1:

$$\sum_{j=1}^m f(p_j^{(i,i+1)}) = \begin{cases} 1 \text{ if } \begin{cases} C_{x_j^i} > C_{x_j^{i+1}} \\ EI_{x_j^i} < EI_{x_j^{i+1}} \end{cases} \\ 1 \text{ if } \begin{cases} C_{x_j^i} < C_{x_j^{i+1}} \\ EI_{x_j^i} > EI_{x_j^{i+1}} \end{cases} \\ 0 \text{ for two other cases} \end{cases}$$

(Eq.3)

subject to $i = 1, \dots, n-1$ and $j = 1, \dots, m$

where $p_j^{(i,i+1)}$ = pairwise alternatives ($i, i+1$) for j^{th} Monte Carlo simulation, x_j^i = variable alternative i with j^{th} Monte Carlo simulation, x_j^{i+1} = variable alternative $i+1$ with j^{th} Monte Carlo simulation, $C_{x_j^i}$ = unit cost of x_j^i (\$), $C_{x_j^{i+1}}$ = unit cost of x_j^{i+1} (\$), $EI_{x_j^i}$ = CO₂ emissions per material unit of x_j^i (kg CO₂ eq), $EI_{x_j^{i+1}}$ = CO₂ emissions per material unit of x_j^{i+1} (kg CO₂ eq), n = number of alternative in category, and m = number of Monte Carlo simulation.

Scenario 2:

$$\sum_{j=1}^m f(p_j^{(i,i+1)}) = \begin{cases} 1 & \text{for six other cases} \\ 0 & \text{if } \begin{cases} T_{x_j^i} > T_{x_j^{i+1}} \\ C_{x_j^i} > C_{x_j^{i+1}} \\ EI_{x_j^i} > EI_{x_j^{i+1}} \end{cases} \\ 0 & \text{if } \begin{cases} T_{x_j^i} < T_{x_j^{i+1}} \\ C_{x_j^i} < C_{x_j^{i+1}} \\ EI_{x_j^i} < EI_{x_j^{i+1}} \end{cases} \end{cases}$$

subject to $i = 1, \dots, n-1$ and $j = 1, \dots, m$

where $p_j^{(i,i+1)}$ = pairwise alternatives ($i, i+1$) for j^{th} Monte Carlo simulation, x_j^i = variable alternative i with j^{th} Monte Carlo simulation, x_j^{i+1} = variable alternative $i+1$ with j^{th} Monte Carlo simulation, $T_{x_j^i}$ = installation time of x_j^i (hours), $T_{x_j^{i+1}}$ = installation time of x_j^{i+1} (hours), $C_{x_j^i}$ = unit cost of x_j^i (\$), $C_{x_j^{i+1}}$ = unit cost of x_j^{i+1} (\$), $EI_{x_j^i}$ = CO₂

emissions per material unit of x_j^i (kg CO₂ eq), $EI_{x_j^{i+1}}$ = CO₂ emissions per material unit of x_j^{i+1} (kg CO₂ eq), n = number of alternative in category, and m = number of Monte Carlo simulation.

In both scenarios, percentages of direct variation relationships also calculated. A direct variation relationship exists when one alternative has all variables' values higher than another alternative. Thus, trade-off patterns and direct variation patterns are exclusive to each other in all pairwise alternatives.

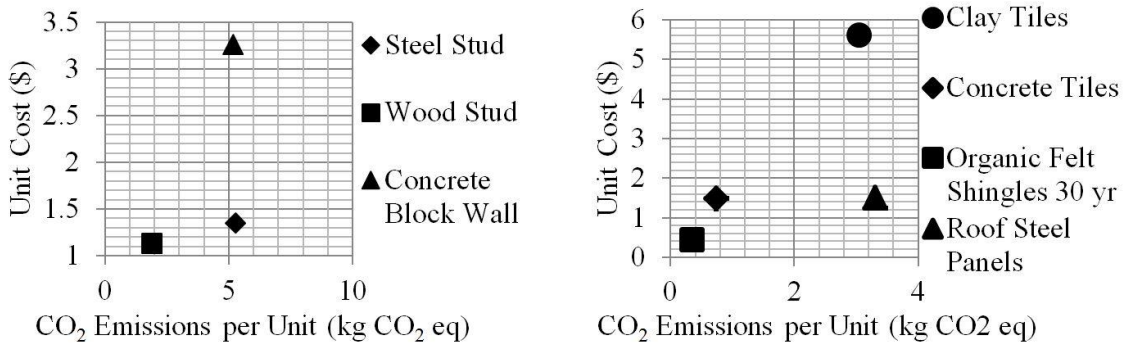


Figure 6 Graph Relationship between Average CO₂ Emissions per Material Unit and Average Unit Cost for Structural Component (left) and Roofing (right) in Scenario 1

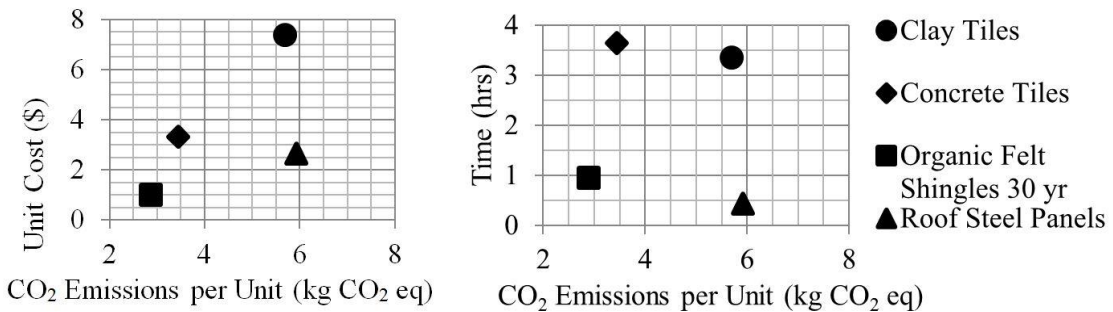


Figure 7 Graph Relationship between Average CO₂ Emissions per Material Unit and Average Unit Cost (left), and between Average CO₂ Emissions per Material Unit and Installation time (right) for Roofing in Scenario 2

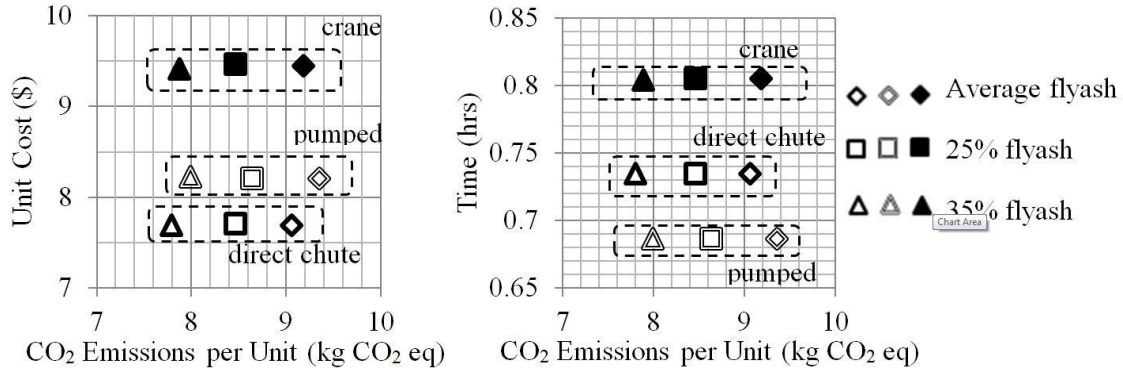


Figure 8 Graph Relationship between Average CO₂ Emissions per Material Unit and Average Unit Cost (left), and between Average CO₂ Emissions per Material Unit and Installation Time (right) for Concrete Footing 3000 psi in Scenario 2

4.5 Significance Test

To determine how significant an observed pattern is, this research hypothesized that the probability of a certain pattern between pairwise alternatives in each category is significantly greater than an assumed mean at 5% confidence level. Since outcomes of pairwise analysis followed binomial probability distributions, i.e., there are only two possible values, ‘trade-off’ or ‘non-trade-off’. Z-tests were applied in the study to determine the statistical significance of analysis.

To determine the assumed mean in each scenario, fair chance outcomes were firstly formulated using above corresponding equations of scenarios due to the lack of historical data. In scenario 1, since two of the four cases represent the existence of a trade-off relationship, the fair chance of outcomes is 50%. In other words, the probability (p) that trade-offs significantly exist is equal to 500 times out of 1,000 Monte Carlo simulation runs. This ratio is selected as the assumed value for Scenario 1. Thus, in

scenario 1, the z-test investigated null hypothesis, $H_0: p = 500$, against alternative hypothesis, $H_a: P > 500$ at the 5% significance level. The rejection of null hypothesis represents there is a significant level of trade-offs.

In scenario 2, there are eight cases in total from the pattern analysis. In two out of the eight cases, 1) all three variables are lower or 2) all three variables are higher, trade-off relationships do not exist between pairwise alternatives, and there are six other cases where trade-off relationships exist. Thus, the probability for the significant existence of trade-off relationships is 750 out of 1,000 simulation runs. Consequently, the null hypothesis is $H_0: p = 750$ and alternative hypothesis is $H_a: p > 750$ at the 5% significance level. Again, rejection of the null hypothesis represents there is a significant level of trade-offs. If a z-test returns that 'h' equals to 1 and 'p' converges to 0, the null hypothesis is falsified at the 5% significance level and a result is significantly better than the assumed value. If a z-test shows the value of 'h' as 0, the results fail to reject null hypothesis.

4.6 Analysis and Results

Table 7 shows a summary of the dominant alternatives of materials in the six categories with their respective percentages of being selected as a dominant alternative. It is interesting to observe that, in the structural component category, the wood stud alternative was selected as a dominant alternative at 92.3% and 70.1%, respectively, in the two scenarios. In addition, when installation time was considered in scenario 2, the percentage dropped almost 22%. This is because wood studs produced comparatively low

CO₂ emissions in the manufacturing phase or less than approximately 50% compared to steel studs and concrete blocks. However, when the installation phase was considered, concrete blocks delivered almost 80% less CO₂ emissions than wood studs in this phase. Thus, the concrete blocks alternative might have a chance to be more competitive than wood studs, if its CO₂ emissions per material unit are relatively low in a simulation run.

In the exterior cladding category, stucco only had a small chance, 0.5%, of being selected as a dominant material among six alternatives, but when installation cost and time were taken into account, there was no dominant alternative that occurred in Scenario 2. This is because cedar bevel and metric modular brick had a similar amount of CO₂ emissions per material unit in scenario 2.

In the insulation category, the blown cellulose alternative had the highest probability of being chosen as a predominant alternative in both scenarios. The probabilities of this category were the second highest among all material categories under study. Also, between scenarios 1 and 2, the probabilities in the two scenarios were obviously similar. The reason is that the blown cellulose alternative had the highest productivity; or the shortest installation time. Both the unit cost and CO₂ emissions per material unit of the blown cellulose alternative were lower than others as well. In the roofing category, only scenario 1 showed that the organic shingle with 30 years of warranty was the dominant alternative at a percentage of 99.8%. However, it is interesting to see that there was no dominant material alternative in scenario 2. These points out that material installation in the construction phase may have an important impact on the selection of dominant alternatives.

For all concrete categories including the concrete footing and the concrete slab-on-grade categories, the level of confidence of all categories was fairly low with a highest of 32.9% (4000 psi 8" slab-on-grade in scenario 1). In scenario 2, the level of confidence being a dominant alternative was even lower with a highest of 0.6% (3000 psi 8" slab-on-grade). Alternatives of concrete with different percentages of flyash, average flyash, 25% flyash, and 35% flyash, and different design strength, 3000 psi and 4000 psi, were also compared. The results showed that concrete with a 35% flyash mix had a higher chance to be a dominant solution in all scenarios. The main reason is that concrete with different flyash mixes has the same unit cost and construction productivity from the RS Means database. Therefore, the distinction between them is only the CO₂ emissions per material unit. Concrete with 35% flyash had the lowest carbon emissions per material unit compared to the other two, thus, concrete with 35% flyash tended to show the highest possibility to be chosen as a dominant alternative. However, the difference of CO₂ emissions per material unit between different fly ash mixes was less than 20%. The percentage of concrete with 35% flyash being a dominant alternative was not considered large.

In addition, in scenario 2, three methods of placing concrete were analyzed. From the RS Means Building Construction Cost Data, the pumped method had the best daily output approximately 40% more than the crane and bucket method, and its cost was almost 60% less than the crane and bucket method. Thus, concrete with the pumped method had a higher probability to be treated as a dominant option in all concrete alternatives with different flyash mixes. However, the direct chute method had slightly

higher cost and lower productivity than the pumped method. Thus, both methods could be competitive, which led to that concrete with the pumped method had a small advantage of being chosen as a dominant option.

Table 7 Summary of Dominant Alternatives and Probability in Percentage

Categories	Sub	Unit	Scenario	Dominant Alternative (%)
	Categories	Function		
Structural Component		S.F.	1	Wood Stud (92.3%)
			2	Wood Stud (70.1%)
Exterior Claddings		S.F.	1	Stucco (0.5%)
			2	-
Insulation		R-value	1	Blown Cellulose (67.5%)
			2	Blown Cellulose (66.5%)
Roofing		S.F.	1	Organic Shingle 30 yr (99.8%)
			2	-
Concrete Footing	Footing	C.F.	1	35% flyash (33.9%)

Categories	Sub Categories	Unit Function	Scenario	Dominant Alternative (%)
	3000 psi		2	-
	Footings	C.F.	1	35% flyash (36.1%)
	4000 psi		2	-
Concrete Slab-on-Grade	Slab 4"	C.F.	1	average flyash (2.8%), 25% flyash (8.3%), and 35% flyash (21.3%)
	3000 psi		2	average flyash pumped (0.1%) and 35% flyash, pumped (0.6%)
	Slab 4"	C.F.	1	25% flyash (1.3%), and 35% flyash 31.9%)
	4000 psi		2	35% flyash, pumped (0.3%)
	Slab 8"	C.F.	1	25% flyash (0.3%), and 35% flyash (31.4%)
	3000 psi		2	35% flyash, pumped (0.6%)
	Slab 8"	C.F.	1	35% flyash (32.9%)

Categories	Sub	Unit	Scenario	Dominant Alternative (%)
	Categories	Function		
	4000 psi		2	35% flyash, pumped (0.3%)

Tables 8-17 contain probabilities of trade-off relationships between pairwise alternatives of all categories in the upper triangle and probabilities of direct variations in the lower triangle. The probabilities were derived pattern analysis equations. The results showed that there was no perfect trade-off relationship when all materials in each category were considered. Trade-off relationships of pairwise alternatives in concrete-based category were high or greater than 75% in all cases. By comparing unit cost across placing concrete methods, the crane method gave greatly higher unit cost in terms of labor cost and equipment cost, since it might need more workers, operators and instruments than others. While the direct chute method had importantly low equipment cost or it had almost 93% less equipment unit cost than crane and pumped techniques. Percentages of flyash still showed the same pattern in different placing concrete methods.

From the tables, a trade-off relationship was also observed when a subset of materials was considered. Moreover, there were noticeable multiple relationships between alternatives. Tables 8-17 also present z-test results. The numbers with ‘*’ indicate that z-test rejected the null hypothesis at the 5% significance level and the results were significantly greater than pure chances.

Figure 9 presents values of average CO₂ emissions per material unit and average unit cost in both scenarios, as well as changes of the percentage of CO₂ emissions (value below arrow) and unit cost (value above arrow) due to the effect for material installation. This highlights the importance of material installation that needed to be considered in the early decision making process of material selections in the project. For example, the foam polyisocyanurate insulation option had lower unit cost than the batt fiberglass insulation option in Scenario 1. However, the foam polyisocyanurate insulation unit cost option had increased almost 200%, when material installation cost (labor unit cost and equipment unit cost) was considered, while the unit cost of the batt fiberglass insulation option had increased only 41.9%. Thus, in scenario 2, the foam polyisocyanurate insulation option showed higher unit cost than the batt fiberglass insulation option.

Table 8 Alternative Pairwise Analysis in Structural Component Category

		Percentage of Trade-off					
		Scenario 1			Scenario 2		
	Alt.	1	2	3	1	2	3
Percentage	1	-	7.7	86.8*	-	29.9	100*
of Direct	2	92.3	-	0	70.1	-	0
Variation	3	13.2	100	-	0	100	-

Table 9 Alternative Pairwise Analysis in Exterior Cladding Category

		Percentage of Trade-off													
		Scenario 1							Scenario 2						
Alt.		1	2	3	4	5	6	7	1	2	3	4	5	6	7
Percentage of Direct Variation	1	-	78.7*	100*	50.1*	0	97.1*	94.4*	-	0	100*	55.9	0	99.2*	100*
	2	21.3	-	0	88.1*	0	0	0	100	-	0	0	90.9*	0	0
	3	0	100	-	100*	0	0.2	93.8*	0	100	-	100*	0	94.9*	99.8*
	4	49.9	11.9	0	-	0	97.8*	95.7*	44.1	100	0	-	0	98.9*	98*
	5	100	100	100	100	-	0	0	100	9.1	100	100	-	0	0
	6	2.9	100	99.8	2.2	100	-	61.1*	0.8	100	5.1	1.1	100	-	74.6
	7	5.6	100	6.2	4.3	100	38.9	-	0	100	0.2	2	100	25.4	-

Table 10 Alternative Pairwise Analysis in Insulation Category

		Percentage of Trade-off											
		Scenario 1					Scenario 2						
Alt.		1	2	3	4	5	6	1	2	3	4	5	6
Percentage of Direct Variation	1	-	2	10.5	30.2	66.7*	49.0		26.8	13.7	96.0*	79.3*	57.8
	2	98.0	-	0	43.1	14.2	1.3	73.2	-	0	42.9	4.4	99.7*
	3	89.5	100	-	0	22.1	9.1	86.3	100	-	0.1	22.8	10.6
	4	69.8	56.9	100	-	98.4*	48.1	4.0	57.1	99.9	-	97.2*	95.4*
	5	33.3	85.8	77.9	1.6	-	67.8*	20.7	95.6	77.2	2.8	-	66.8
	6	51.0	98.7	90.9	51.9	32.2	-	42.2	0.3	89.4	4.6	33.2	-

Table 11 Alternative Pairwise Analysis in Roofing Category

		Percentage of Trade-off							
		Scenario 1				Scenario 2			
Alt.		1	2	3	4	1	2	3	4
Percentage of Direct Variation	1	-	0	0	96.9*	-	88.0*	0	95.0*
	2	100	-	0.2	44.0	12.0	-	0	100*
	3	100	99.8	-	0	100	100	-	100*
	4	3.1	56.0	100	-	5.0	0	0	-

Table 12 Alternative Pairwise Analysis in Concrete Footing 3000 psi Category

Percentage of Trade-off													
Alt.	Scenario 1			Scenario 2									
				Direct Chute			Pumped			Crane and Bucket			
	1	2	3	1	2	3	1	2	3	1	2	3	
Percentage of Direct Variation	1	-	49.1	50.7*	-	76.2*	73.9	-	74.3	76.3*	-	74.8	72.7
	2	50.9	-	49.9	23.8	-	74.8	25.7	-	76.7*	25.2	-	74.5
	3	49.3	50.1	-	26.1	25.2	-	23.7	23.3	-	27.3	25.5	-

Table 13 Alternative Pairwise Analysis in Concrete Footing 4000 psi Category

Percentage of Trade-off													
Alt.	Scenario 1			Scenario 2									
				Direct Chute			Pumped			Crane and Bucket			
	4	5	6	4	5	6	4	5	6	4	5	6	
Percentage of Direct Variation	4	-	48.8	47.7	-	77.5*	75.5*	-	74.6	73.4	-	73.6	75.1*
	5	51.2	-	48.8	22.5	-	72.6	25.4	-	73.6	26.4	-	73.6
	6	52.3	51.2	-	24.5	27.4	-	26.6	26.4	-	24.9	26.4	-

Table 14 Alternative Pairwise Analysis in Concrete Slab 4 inches 3000 psi Category

Percentage of Trade-off													
Alt.	Scenario 1			Scenario 2									
				Direct Chute			Pumped			Crane and Bucket			
	1	2	3	1	2	3	1	2	3	1	2	3	
Percentage of Direct Variation	1	-	49.6	47.7	-	85*	93.5*	-	76.1*	76.7*	-	74.4	74.2
	2	50.4	-	52.9*	15	-	74.5	23.9	-	76.2*	25.6	-	74.9
	3	52.3	47.1	-	6.5	25.5	-	23.3	23.8	-	25.8	25.1	-

Table 15 Alternative Pairwise Analysis in Concrete Slab 4 inches 4000 psi Category

Percentage of Trade-off													
		Scenario 1			Scenario 2								
					Direct Chute			Pumped			Crane and Bucket		
Alt.		4	5	6	4	5	6	4	5	6	4	5	6
Percentage of Direct Variation	4	-	48.7	50.1*	-	78.4*	77.6*	-	76.3*	75.6*	-	75.9*	74.0
	5	51.3	-	50.7*	21.6	-	75.2*	23.7	-	76.9*	24.1	-	73.5
	6	49.9	49.3	-	22.4	24.8	-	24.4	23.1	-	26.0	26.5	-

Table 16 Alternative Pairwise Analysis in Concrete Slab 8 inches 3000 psi Category

Percentage of Trade-off													
		Scenario 1			Scenario 2								
					Direct Chute			Pumped			Crane and Bucket		
Alt.		7	8	9	7	8	9	7	8	9	7	8	9
Percentage of Direct Variation	7	-	51.0*	50.9*	-	74.3	73.3	-	75.3*	73.9	-	75.8*	77.2*
	8	49.0	-	48.5	25.7	-	74.3	24.7	-	76.8*	24.2	-	76.1*
	9	49.1	51.5	-	26.7	25.7	-	26.1	23.2	-	22.8	23.9	-

Table 17 Alternative Pairwise Analysis in Concrete Slab 8 inches 4000 psi Category

Percentage of Trade-off													
		Scenario 1			Scenario 2								
					Direct Chute			Pumped			Crane and Bucket		
Alt.		10	11	12	10	11	12	10	11	12	10	11	12
Percentage of Direct Variation	10	-	48.5	49.6	-	76*	73.4	-	74.8	74.8	-	74.1	76.7*
	11	51.5	-	50.5*	24	-	75	25.2	-	77.4*	25.9	-	76.1*
	12	50.4	49.5	-	26.6	25	-	25.2	22.6	-	23.3	23.9	-

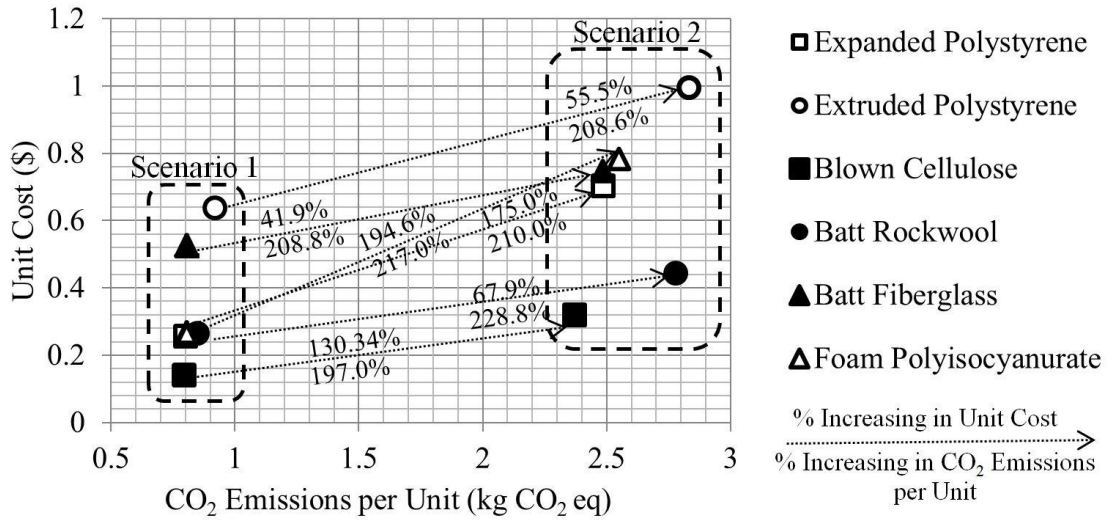


Figure 9 Graph Relationships between Average CO₂ Emissions per Material Unit and Average Unit Cost for Insulation Shows Effect of Material Installation in Percentage

**CHAPTER 5 ANALYSIS OF CONSTRUCTION TIME, INITIAL
CONSTRUCTION COST, AND ENVIRONMENTAL IMPACT RELATIONSHIP
AT COMPONENT AND BUILDING LEVEL AT PRE-USE PHASE**

This chapter presents the application of SimuleICon, during the pre-use phase, that can help to define relationships between construction time, initial construction cost, and CO₂ emissions. Two case studies are used to compare the results. The databases consist of material unit cost, labor unit cost, crew types, equipment unit cost, productivity, and CO₂ emissions per material unit. Total initial construction cost and total CO₂ emissions are aggregately calculated to the project level. The Critical Path Method (CPM) approach is used to estimate total construction time. The NSGA-II is applied as the optimization technique in this stage. The construction time is significantly considered at this level, as well as cost and CO₂ emissions, because it substantially has a major impact on the decision-making process during the construction phase. Delay in construction time can also cost the project in various ways, including money.

Two case studies' components for building design are selected based on studied material from the previous chapter. For instance, the four inches slab on grade have several alternatives based on different percentages of flyash mixes, e.g., average flyash, 25% flyash, and 35% flyash, and different methods of placing concrete, e.g., the direct chute or the pump method. As well as roofing, there are a few options that are used in this chapter, such as clay tiles, concrete tiles, organic felt shingles.

5.1 Data Collection and Case Study Descriptions

Information of case studies was collected to define possible alternatives. Database was stored based on the construction activity or component level of the building, such as site cleaning activity, excavation, stem wall construction, etc. Each activity or component has its alternatives. One alternative can be combined from two or more materials. For example, one of the exterior wall alternatives consists of fiberglass insulation, steel stud, and drywall. Each of them separately has unit cost, productivity, and CO₂ emissions per material unit.

The first case study is a zero net energy building named the Zero Energy Research Laboratory. The building was built at the University of North Texas, providing advantageous utilities for researchers and students (Gregorski, 2012). It has the 1,200 square feet of spacing and it offers a wide range of advanced technologies, such as solar panels, and a building energy monitoring and controlling system. In this research, the laboratory building, presented in figure 10, has 17 established components or activities, including start activity and finish activity. The example of building activities and their alternatives are shown in table 18.

The second case study is a project called the Future House USA, shown in figure 10. It is a two-story residential building, which was built and located in Beijing, China. The building has approximately 1,200 square feet as well. Based on the design of the project, many possible components can be chosen to achieve the efficient design during the early design stage. The total number of options for building components is 185

alternatives. Within all possible options of the building components, there are over 31 billion possible combinations that professional designers should consider.

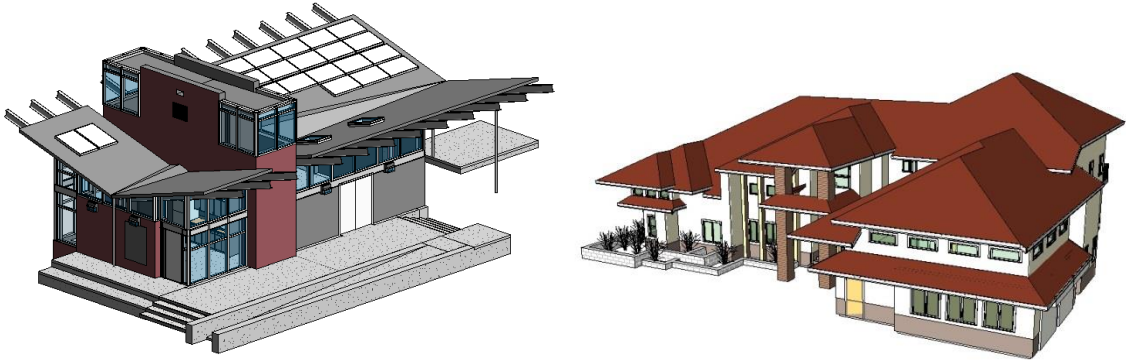


Figure 10 Three-dimension Models of Case Study 1 (left) and Case Study 2 (right)

Both buildings were designed as zero-net-energy (ZNE) houses that aim to maximize building energy efficiency and generate balance energy between their energy consumption and renewable resources. Summary of case studies is provided in table 18. Alternatives of building components and materials in both cases are chosen based on the comparable function of assemblies, construction methods, and available combinations among materials. For example, all exterior wall construction options in this research represented the same thermal resistance value (R-Value).

Table 18 Examples of the Zero Energy Research Laboratory Activities and Their Alternatives

Activity Number	Activity Name	Alternative Number	Alternative Description
4	Footing Construction	1	3000 psi, average flyash, pumped, reinforcing in place, footings
		2	3000 psi , 25% flyash, pumped, reinforcing in Place, footings
		3	3000 psi, 30% flyash, pumped, reinforcing in Place, footings
		4	3000 psi, average flyash, direct chute, reinforcing in Place, footings
		5	3000 psi , 25% flyash, direct chute, reinforcing in Place, footings
		6	3000 psi, 30% flyash, direct chute, reinforcing in Place, footings
6	Subgrade	1	Blown Cellulose Board

Activity Number	Activity Name	Alternative Number	Alternative Description
	Insulation	2	Batt Rockwool
		3	Batt Fiberglass
8	Slab-on-Grade Construction	1	4", 3000 psi, average flyash, pumped, reinforcing in Place, walls
		2	4", 3000 psi , 25% flyash, pumped, reinforcing in Place, walls
		3	4", 3000 psi, 35% flyash, pumped, reinforcing in Place, walls
		4	4", 3000 psi, average flyash, direct chute, reinforcing in Place, walls
		5	4", 3000 psi , 25% flyash, direct chute, reinforcing in Place, walls
		6	4", 3000 psi, 35% flyash, direct chute, reinforcing in Place, walls

Activity Number	Activity Name	Alternative Number	Alternative Description
9	Exterior Wall Construction (Conditioned Zone)	1	SIP, 5.5" thickness, curtain wall
		2	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8, expanded polystyrene board, 5/8" FR drywall, 3/8" Plywood, concrete brick, curtain walls
		3	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8, extruded polystyrene, 5/8" FR drywall, 3/8" Plywood, concrete brick, curtain walls
		4	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8, Batt Rockwool, 5/8" FR drywall, 3/8" Plywood, concrete brick, curtain walls
		5	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8, Batt Figerglass, 5/8" FR drywall, 3/8" Plywood, concrete brick, curtain walls
15	Roofing	1	Clay tiles

Activity Number	Activity Name	Alternative Number	Alternative Description
		2	Concrete tiles
		3	Organic felt shingles 30yr
		4	Steel Roof Panel 30 GA (Residential)
16	Flooring	1	Bamboo flooring
		2	Wood flooring

Table 19 Summary of Case Studies

	Case Study 1	Case Study 2
Description	Zero Net Energy Building	Future House Project
Building Spacing (S.F.)	1,200	1,250
Location	Texas, United States	Beijing, China
Total Number of Activities	17	16

	Case Study 1	Case Study 2
Total Number of Alternatives	54	171
Total Possible Design Solutions	5,832,000	27,214,258,176

5.2 Analysis and Results

In both case studies, results were obtained from 200 Monte Carlo simulation runs. In each Monte Carlo simulation, there were 20 populations and 200 generations utilized in the NSGA-II. Most of the results obtained with the NSGA-II exhibited a balanced behavior, where construction time, initial construction cost, and CO₂ emissions tended to be medium or low magnitude; the results which show a higher value for any of these parameters also show reduced values in the other two, this trade-off behavior is to be expected when using the genetic algorithms. Figures 11 and 12 show 200 sets of 20 optimal solutions generated from the NSGA-II in three dimensions, as well as graph relationships between construction time and initial construction cost, graph relationships between construction time and CO₂ emissions, and graph relationship between initial construction cost and CO₂ emissions during the pre-use phase for both case studies. There is no point that is located in the lowest values; most of optimal solutions are located in the middle, where they show a balanced behavior and a trade-off between all three parameters. The graph showing relationship between construction time and initial construction cost indicated general trade-off behavior, i.e., shorter construction time

results in higher project cost. However, when considering all three parameters, one could not observe a clear pattern from the results. The solutions giving high value in one parameter are also seen in middle or low values range of others.

From graphs of simulations' results, different markers represent different Monte Carlo simulation runs and thus they are different sets of results. As can be seen, solutions tend to exhibit similar behavior across simulation runs. The different occurs due to the random input variables generated by the Monte Carlo simulation to account for data uncertainty. By running different simulations the effect that data uncertainty could have on the project becomes apparent, for different simulations, the set solutions changed to reflect the new set of random variables generated by the Monte Carlo simulation. For instance, variations of construction material can have a significant impact on the outcome of the overall project design as significantly presented in the previous chapter. Moreover, lowest construction time or high productivity alternatives might not always be desirable since they showed ostentatiously great value in others.

From the total 4,000 optimal solutions, the results from SimuleICon showed that only 2,390 combined solutions in the case study 1 and 1,376 combined solutions in the case study 2 were occurred and accounted for optimal solutions based on multiple objectives. Figures 13 and 14 show histograms of unique optimal solutions with their frequencies. Those solutions had the highest frequency, which were however only 20 times out of the total 4,000 solutions. If each Monte Carlo simulation can be related to a different construction context defined key project features such as a productivity rate,

unit cost and material selections, this observation shows that in theory there does not exist an absolute optimal solution, which may appear in the majority of simulations

Furthermore, the results were analyzed in order to statistically observe the relationship between multiple objectives. Regression techniques were used to fit the data derived from each simulation. Data patterns from 200 Monte Carlo simulation runs were then compared to determine the consistency of observations. Three expectation data patterns were used in this case study, linear, second-order polynomial and third-order polynomial functions. Comparing the fits of different functions in this searched is presented by R-squared measures (R^2) or coefficient of determination. R-squared is a statistical model widely used to determine the fitness of studied models (e.g., Nagelkerke, 1991; Cameron & Windmeijer, 1997). It is well known in regression analysis as well as goodness of fit or Pearson chi-square. Chi-square illustrates the observed data follow a particular function while R-square is useful in comparing models of different fitness functions. Values of R-squared are in the range of 0 to 1. The closer of an R-squared value to 1, the better fit of the data pattern. Moreover, the confidence of results is examined by dissimilarity measurements between the data pattern of each simulation using Procrustes analysis. This analysis is used to compare two set of data in term of shape (Ross 2004). The results from the analysis are shown as dissimilarity measures (d). 1,000 simulations are paired and estimated d values are calculated. The value of 'd' closer to 0 signifies the greater similarity between the data patterns of two simulations.

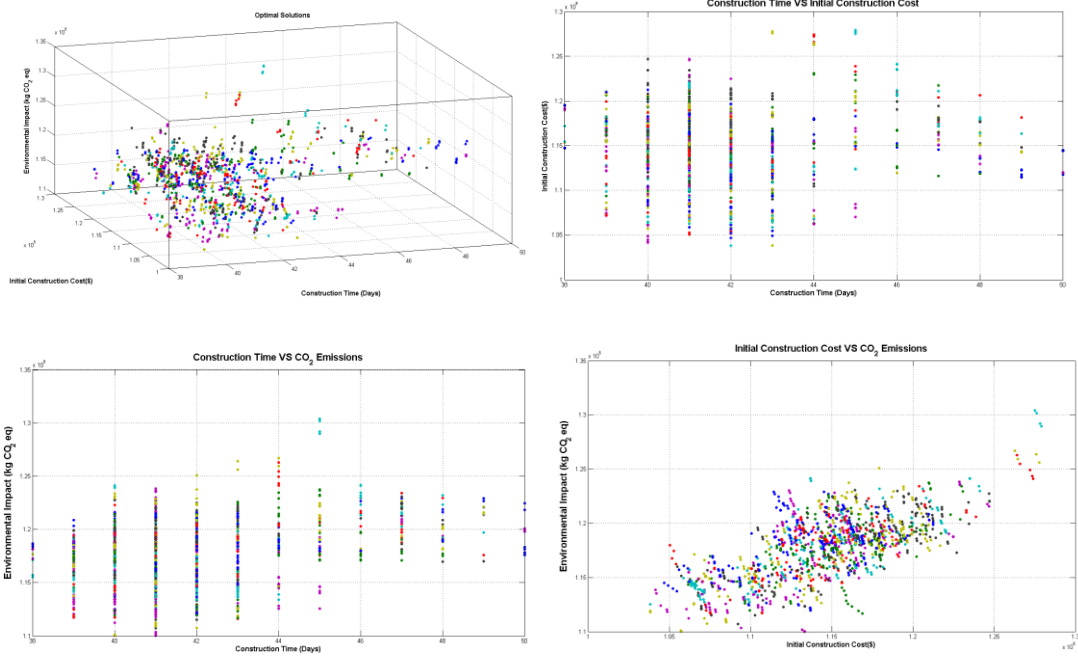


Figure 11 Optimal Solutions Shown in Graphs Relationships between Construction Time, Initial Construction Cost, and CO₂ Emissions of Case Study 1

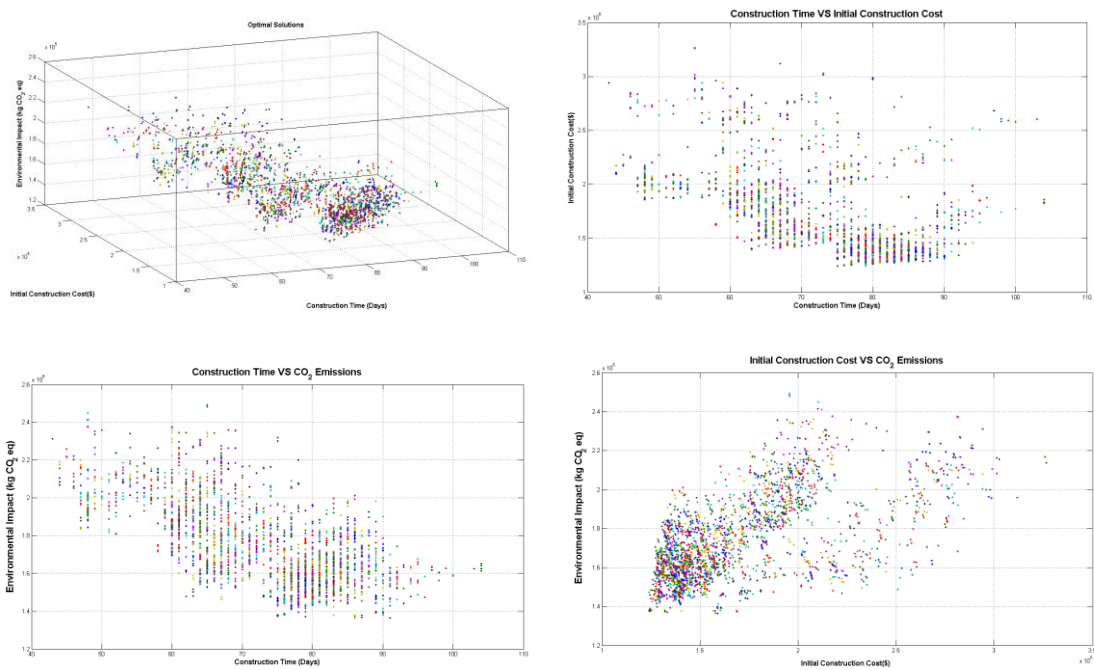


Figure 12 Optimal Solutions Shown in Graphs Relationships between Construction Time, Initial Construction Cost, and CO₂ Emissions of Case Study 2

From Table 20 and 21, one can observe that:

- Regarding construction time and initial construction cost – if R^2 is set to 0.9 or better, the third-order polynomial distribution function seemed to be the most frequent best fit to data in the case study 2. While both second-order polynomial and third-order polynomial showed approximately similar percentages in the case study 1. However, the frequencies were still relatively low, about 45-48%. This means there are other data patterns observed as well. On the other hand, similarity of data patterns between simulations was highest using the linear function.
- Regarding construction time and CO_2 emissions, there were not many data patterns that fitted to one particular regression function. Similarity of data patterns between simulations was relatively high.
- Regarding initial construction cost and CO_2 emissions, the third-order polynomial function provided the highest percentage of the best fit in both cases. However, it did not serve the best similarity between simulations. The linear function seemed to give the better similarity but the percentages are still comparatively low.

The above observations seem to suggest that data sets from 200 simulation runs do not converge to a particular pattern. On the other hand, visual observations to data indicated that trade-offs between construction time and initial construction cost, as well

as construction time and CO₂ emissions existed in majority of the cases with few exceptions. On the other hand, data of initial construction cost and CO₂ emissions showed a different pattern, which this seems to suggest non-trade-off behaviors with exceptions.

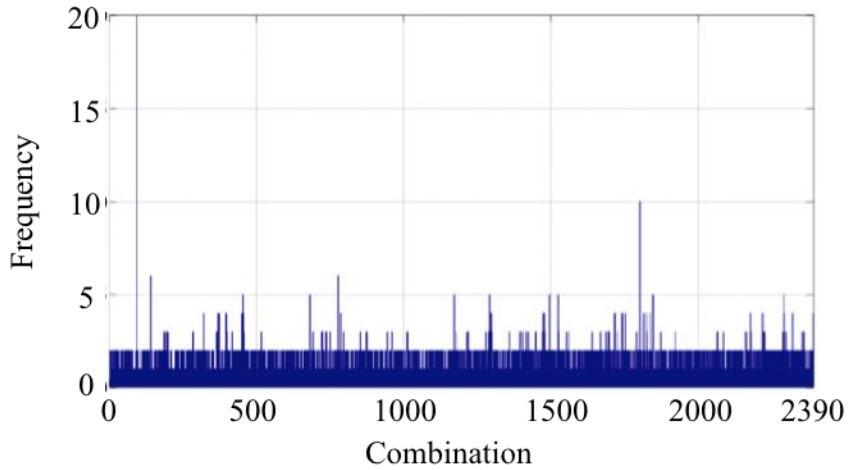


Figure 13 Combined Solutions and Their Frequencies Histogram: Case Study 1

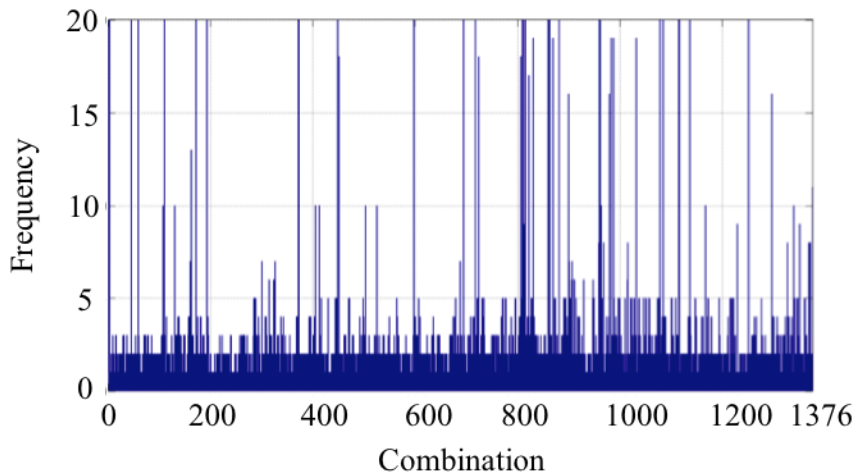


Figure 14 Combined Solutions and Their Frequencies Histogram: Case Study 2

Table 20 Summary of R-squared (R^2) and Dissimilarity Measures (d): Case Study 1

Percentage of graphs relationship between	Construction time and Initial Construction cost		Construction Time and CO ₂ Emissions		Initial Construction cost and CO ₂ Emissions	
	$R^2 > 0.9$	$d < 0.1$	$R^2 > 0.9$	$d < 0.1$	$R^2 > 0.9$	$d < 0.1$
Linear	33.00%	19.78%	12.00%	22.38%	20.00%	16.87%
Second-order Polynomial	47.50%	19.49%	19.5%	21.84%	30.00%	15.50%
Third-order Polynomial	45.00%	20.24%	18.50%	14.47%	55.50%	14.05%

Table 21 Summary of R-squared (R^2) and Dissimilarity Measures (d): Case Study 2

Percentage of graphs relationship between	Construction time and Initial Construction cost		Construction Time and CO ₂ Emissions		Initial Construction cost and CO ₂ Emissions	
	$R^2 > 0.9$	$d < 0.1$	$R^2 > 0.9$	$d < 0.1$	$R^2 > 0.9$	$d < 0.1$
Linear	20.5%	18.20%	10.5%	18.20%	20.00%	21.21%
Second-order Polynomial	35.00%	11.73%	24.00%	14.33%	32.00%	12.41%
Third-order Polynomial	48.50%	9.56%	38.50%	12.21%	45.00%	8.83%

CHAPTER 6 ANALYSIS OF LIFE CYCLE COST AND ENVIRONMENTAL IMPACT RELATIONSHIPS AT BUILDING LEVEL AT USAGE PHASE

Application of SimuleICon for the usage phase is presented in this chapter to find the relationship between life cycle cost and life cycle CO₂ emission. Different life spans of the building are also analyzed in order to find the effect of considering occupancy time of the building into the relationship. In this chapter, the case study, the Zero Net Energy Laboratory, is continually used to present and observe any change in the relationships of cost and CO₂ emissions between the pre-use phase and the usage phase. Energy simulation program, EnergyPlus, is a significant tool to find energy consumption of the building design in this chapter.

6.1 Integration of Energy Simulation

SimuleICon analysis is expanded to integrate energy simulation. Hence, the simulation can incorporate how much energy will be consumed with the selected optimal design alternatives. Over half of the total energy consumed by building stems, from its usage phase, specifically by heat ventilation and air conditioning HVAC systems. Building energy simulations are capable of estimating energy performance based on design parameters. The energy simulation software, EnergyPlus, is used in order to calculate energy consumption during the usage phase. EnergyPlus is written in the different programming language than SimuleICon and it requires the specific input file called *.idf file. Thus, the co-simulation is required to overcome this issue. Additional data of the building is requested as an input to the energy simulation, such as user

behavior, HVAC and lighting system. IDF Generator is a program that developed with SimuleICon to help create multiple IDFs based on many alternatives and also automatically run the energy simulation by directly using EnergyPlus. It extracts the required data and writes them out to one text file. This can help with the idea of limited storage because, if many IDFs are created and simulated, the storage space can be an issue. Consequently, SimuleICon can easily retrieve final energy consumption outputs from the IDF Generator and they can be converted to energy consumption cost and energy related CO₂ emissions as input to the optimization process.

Why is IDF generator needed? EnergyPlus has a function, named ParametricPreprocessor, to aid users in combining the objects with different options. However, ParametricPreprocessor cannot combine all parametric objects properly. For example, if two parametric objects, A and B, have two options, A1, A2, B1, and B2, the ParametricPreprocessor will create only two IDFs that would have A1B1 and A2B2 combinations. It does not describe all possible combinations. If object A has the third option, this option will not be considered. From the example, IDF Generator can create all four possible combinations, A1B1, A1B2, A2B1 and A2B2. IDF Generator requires a base IDF file and variable XML file. Figure 15 shows an example of two variables, which are the exterior wall and interior wall, with three alternatives each in XML file and the base IDF presented in figure 16 specifics variables in it. The '\$' is used to define variable in the base IDF file.

```

<Parametrics>
  <ParametricOption id="Exterior Wall">
    <Option value="1">Exterior Wall Option 1</Option>
    <Option value="2">Exterior Wall Option 2</Option>
    <Option value="3">Exterior Wall Option 3</Option>
  </ParametricOption>
  <ParametricOption id="Interior Wall">
    <Option value="1">Interior Wall Option 1</Option>
    <Option value="2">Interior Wall Option 2</Option>
    <Option value="3">Interior Wall Option 3</Option>
  </ParametricOption>
</Parametrics>

```

Figure 15 Example of XML file

```

BuildingSurface:Detailed.
Construction,
  Exterior Wall Option 1,      !- Name
  ...

BuildingSurface:Detailed,
  North Building Wall,        !- Name
  Wall,                        !- Surface Type
  $Exterior Wall,             !- Construction Name
  Zone1,                       !- Zone Name
  ...

```

Figure 16 Example of Base IDF file

6.2 Data Collection and Case Study Description

SimuleICon incorporates the energy consumption data and interprets it to cost and CO₂ emissions for each design. Those data are also considered in the NGS-II. The zero energy laboratory at University of North Texas is continually used as the case study in this section. The building consists of three zones; living zone, mechanic zone, and electrical zone, presented in figure 17. Each zone is used to define different building envelopes or exterior wall in this case; thus, all exterior walls in the same zone use the

same design alternative. Roofing is another variable in the EnergyPlus. Figure 18 shows an IDF file alternative. For this project, parametric XML file has 5 variables. The variables and their alternatives shown in figure 18 are created based on activity from the previous chapter.

Thus, from all five variables, IDF Generator created 500 combinations of IDFs. Output of yearly energy consumptions is provided in kilowatt-hour (kWh). Those outputs are used to calculate energy consumption cost and energy related CO₂ emissions from energy consumption. In this research, the CO₂ emissions factor is equal to 6.89551×10^4 metric tons CO₂ per kWh (EPA, 2014). This factor only considered CO₂ emissions of GHG emissions; other GHG emissions are not included. The emission factor of electricity reductions was calculated based on the non-baseload CO₂ output emission rate in 2010. The building is located in Texas; therefore, the energy consumption costs approximately 10.98 cents per kWh based on published electricity statistics (EIA, 2015). Additionally, maintenance cost from RS Means Building Construction and RS Means Facilities Maintenance & Repair Cost Data, and CO₂ emissions during the maintenance phase from the Athena impact estimator are considered in the analysis.

In this chapter, five scenarios are considered. All scenarios cover the ranges of possible solutions that can be generated in this building. The first scenario simulates the case of using lowest possible unit cost and CO₂ emissions per material unit from all building components' alternatives. Thus, from the probability distribution, lowest values of all unit cost and CO₂ emissions per material unit are selected. Scenario 2 applies the values possible highest unit cost and lowest CO₂ emissions per material unit. Scenario 3

represents mean value of both unit cost and CO₂ emissions per material unit of all building components' alternatives. Highest CO₂ emissions per material unit and lowest unit cost are input to scenario 4. The last scenario considers extreme situations, when all highest unit cost and CO₂ emission unit are applied to NSGA-II. Table 22 shows a summary of the five scenarios.

Moreover, building different life spans are utilized in order to observe relationships between life cycle costs and CO₂ emissions over time. The relationship at the beginning of occupancy, 0-year life span, is used as the base line. The other observation life spans are 5, 10, 15, 20, 25, 30, 35, 45, 40, 45, 50, 60, 70, 80, 90, 100, 120, 140, 160, 180, 200, 250, and 300 years.

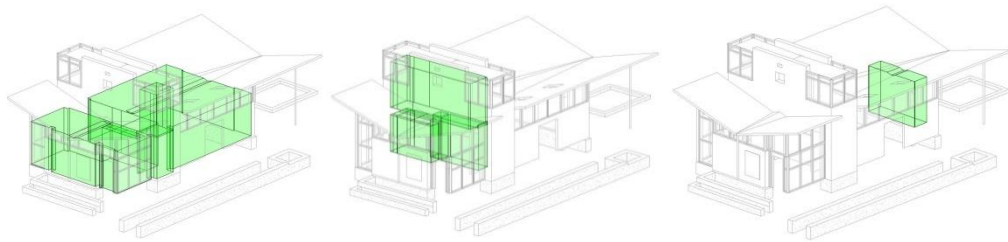


Figure 17 Building Zones; Living Zone, Mechanic Zone, and Electrical Zone

Table 22 Summary of the Five Scenarios

Scenario	Unit Cost	CO ₂ emissions per Material Unit
1	Lowest Value	Lowest Value

Scenario	Unit Cost	CO ₂ emissions per Material Unit
2	Highest Value	Lowest Value
3	Mean Value	Mean Value
4	Lowest Value	Highest Value
5	Highest Value	Highest Value

6.3 Analysis and Results

From the energy simulation, 500 IDF's provided different energy consumption data. For all five scenarios, 200 generations and 20 populations were utilized in the NSGA-II in all life spans. The results of 200 sets of 20 optimal solutions for each year are presented in figures 19-41. The lowest cluster represented the optimal solutions from scenario 1. On the other hand, results of scenario 5 provided the highest life cycle costs and CO₂ emissions cluster. Optimal solutions from scenario 3 exhibited in the middle between scenario 1 and scenario 5. When scenarios 2 and 4 were considered, they provided the range of possible solutions that could happen in all cases. An area between optimal solutions from scenario 1, 2, 4, and 5 can be acknowledged where uncertainty could take place in the data.

From figures 19-41, optimal solutions in each scenario exhibited trade-off behavior between them. However, the difference between them was too small. If all

scenarios were recognized and all data at the unit cost and productivity were randomly generated, optimal solutions would actively demonstrate a proportional relationship as in the pre-use phase. After 100 years, gaps between optimal solutions between scenario 1, 3, and 5 are smaller and differences between optimal solutions in each scenario are larger. The changing of pattern with time was displayed in figures 19-41.

```

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Figure 18 Parametric XML File of the Zero Energy Laboratory Building

In the figures, from the start to a 15 year-life span, the relationship between cost and CO₂ emissions was the same as shown in the pre-use phase. Lowest value in unit cost and CO₂ emissions gave the lowest set of optimal solutions. More life span can be competitive with a high value of parameters. For example, optimal solutions from a 5 year-life span in scenario 3 were approximately located as optimal solutions from a 15 year-life span in scenario 1. This means uncertainty in the data is larger than the increasing of cost and CO₂ emissions in years. Scenario 1 and scenario 5 are the extreme cases, which represent lowest possible values of optimal solutions and highest possible values of optimal solutions. Table 23 presents the longest distance between optimal solutions in scenario 1 and scenario 5. The longest distances between optimal solutions in scenario 1 and optimal solutions in scenario 5 are also calculated in all observed year-life spans. If the distance in the last column is larger than others, it means that the gap of uncertainty controls the relationship and the relationship between cost and CO₂ emissions has a proportional attitude. If the distance between optimal solutions within the scenario is greater, the trade-off relationship should be considered.

In all year-life spans, the relationships between cost and CO₂ emissions showed direct variation, in which one increases as another increases. There was no trade-off relationship between them. From tables 23, 5 and 40 year-life spans show no distance between optimal solutions in scenario 1. Only one optimal solution is found in both. Additionally, the optimal solutions use the same component combination. All 5 scenarios can provide the range of possible solutions that can happen in all cases. Figure 48 shows an example of possible solutions area. These areas are estimated in all year-life spans

presented in table 24. The areas are similar in value, which encourage the consistent pattern of relationship over time.

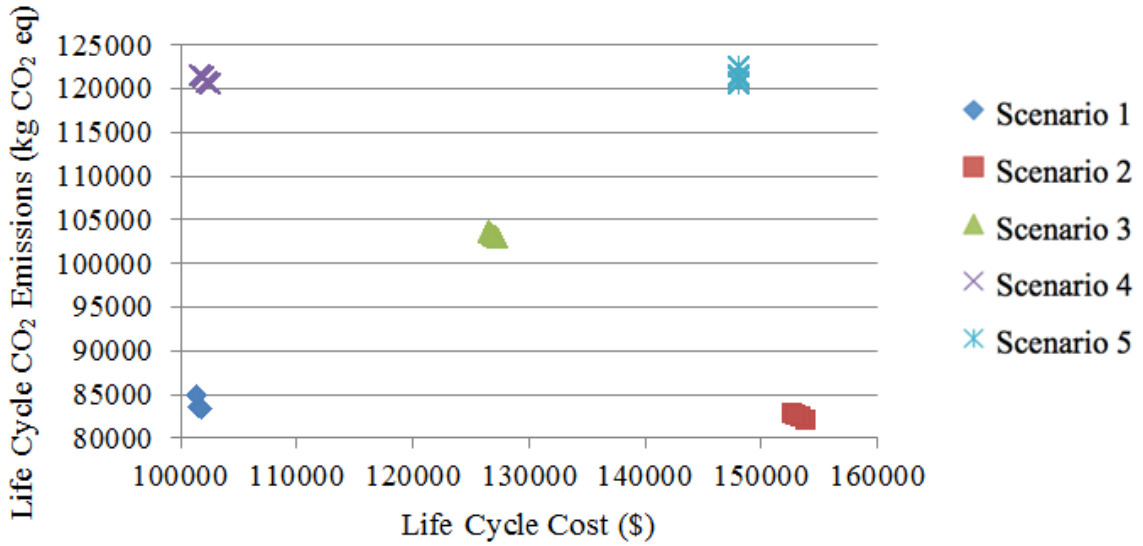


Figure 19 Graph Relationships between Cost and CO₂ Emissions for 0 Year-Usage Phase

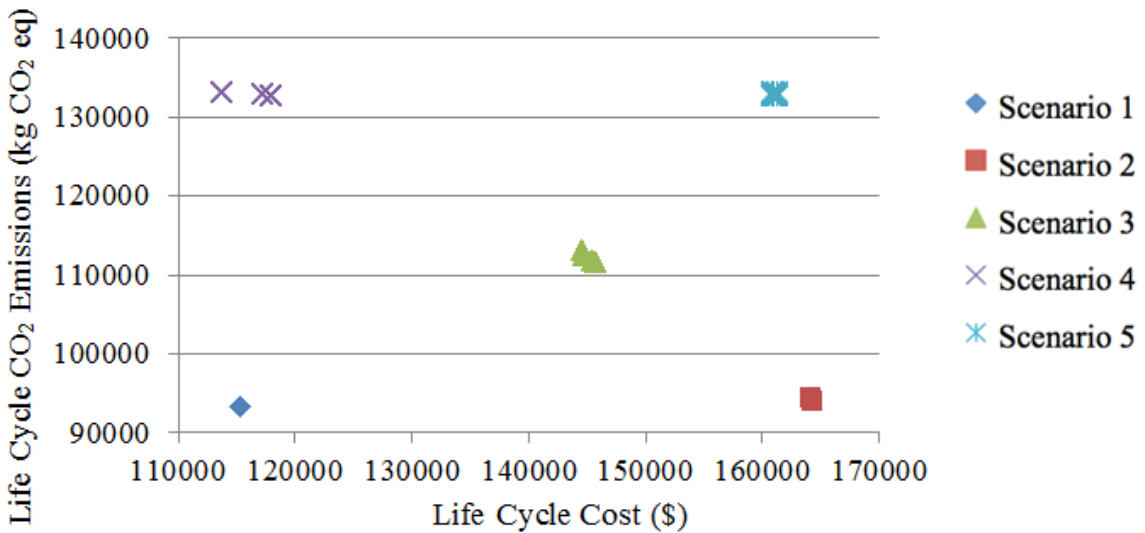


Figure 20 Graph Relationships between Cost and CO₂ Emissions for 5 Year-Usage Phase

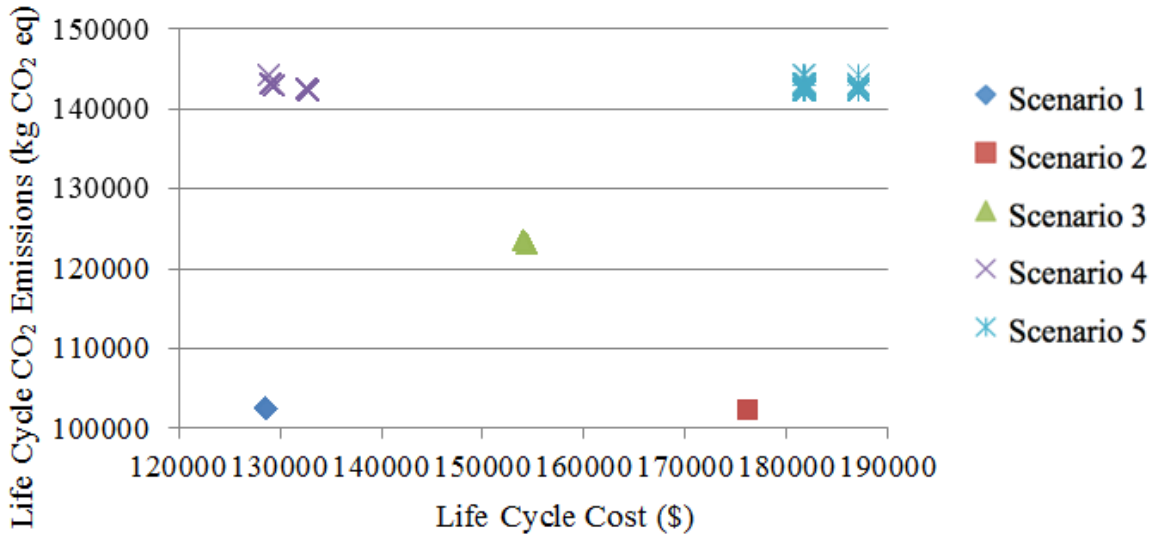


Figure 21 Graph Relationships between Cost and CO₂ Emissions for 10 Year-Usage Phase

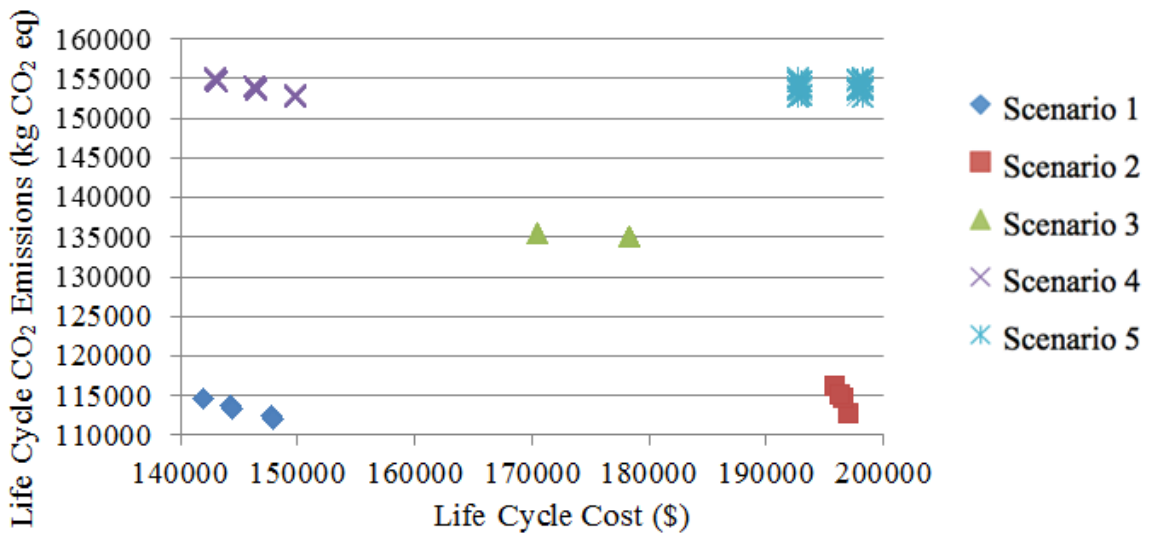


Figure 22 Graph Relationships between Cost and CO₂ Emissions for 15 Year-Usage Phase

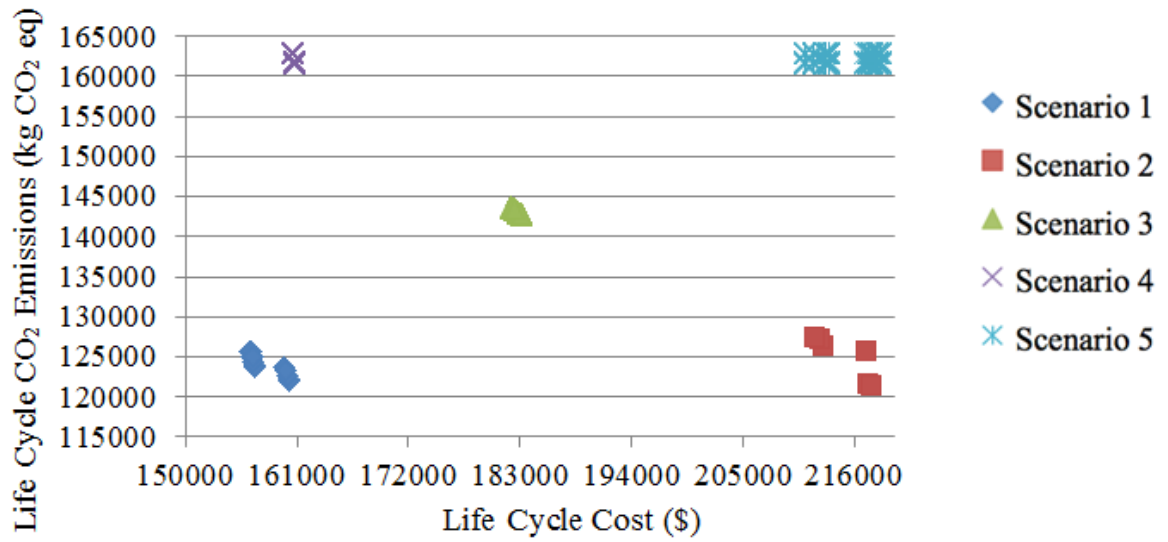


Figure 23 Graph Relationships between Cost and CO₂ Emissions for 20 Year-Usage Phase

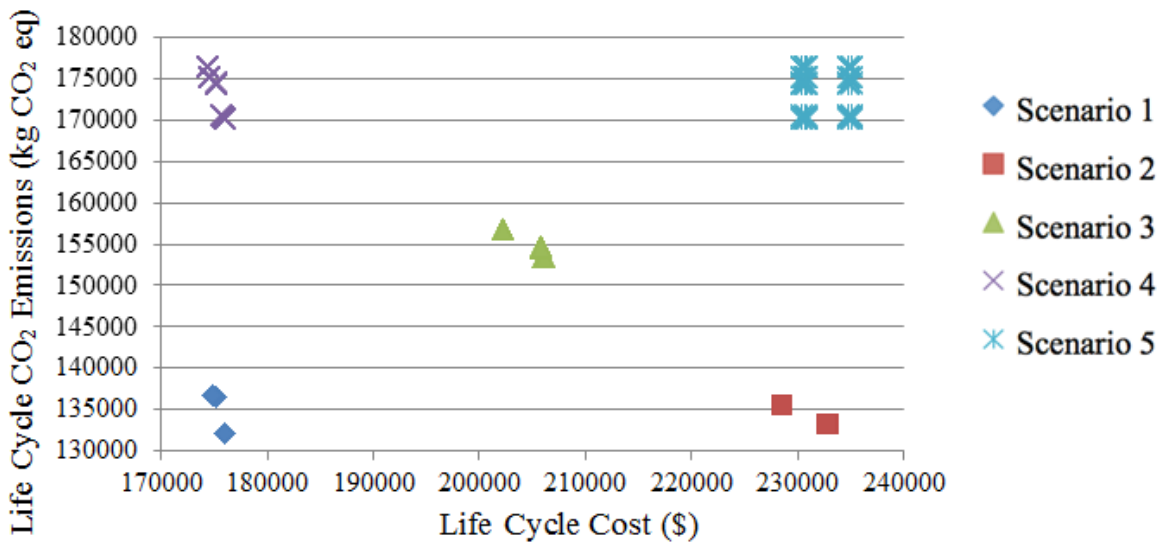


Figure 24 Graph Relationships between Cost and CO₂ Emissions for 25 Year-Usage Phase

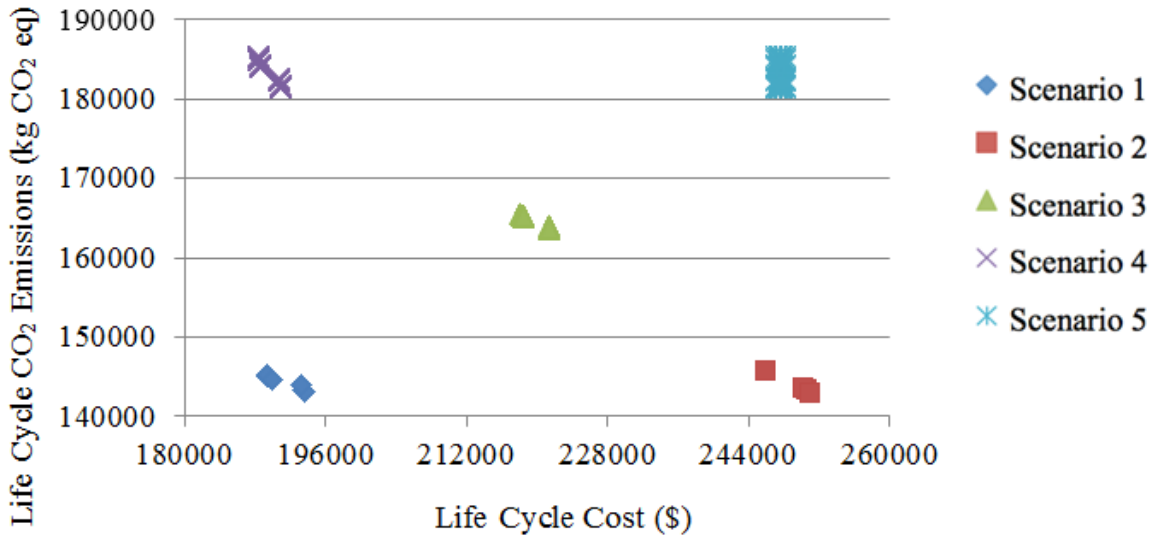


Figure 25 Graph Relationships between Cost and CO₂ Emissions for 30 Year-Usage Phase

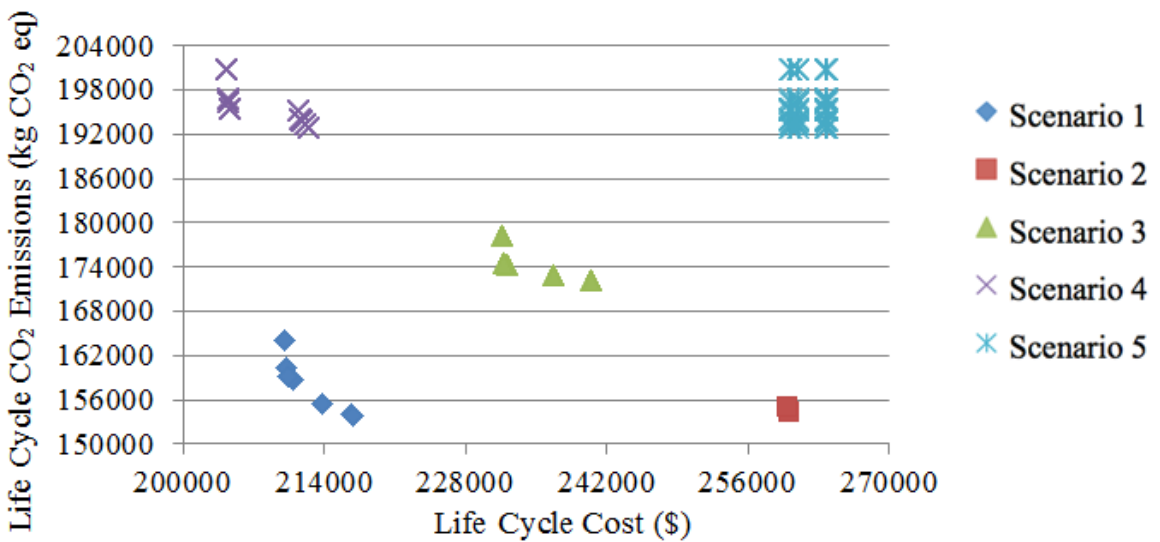


Figure 26 Graph Relationships between Cost and CO₂ Emissions for 35 Year-Usage Phase

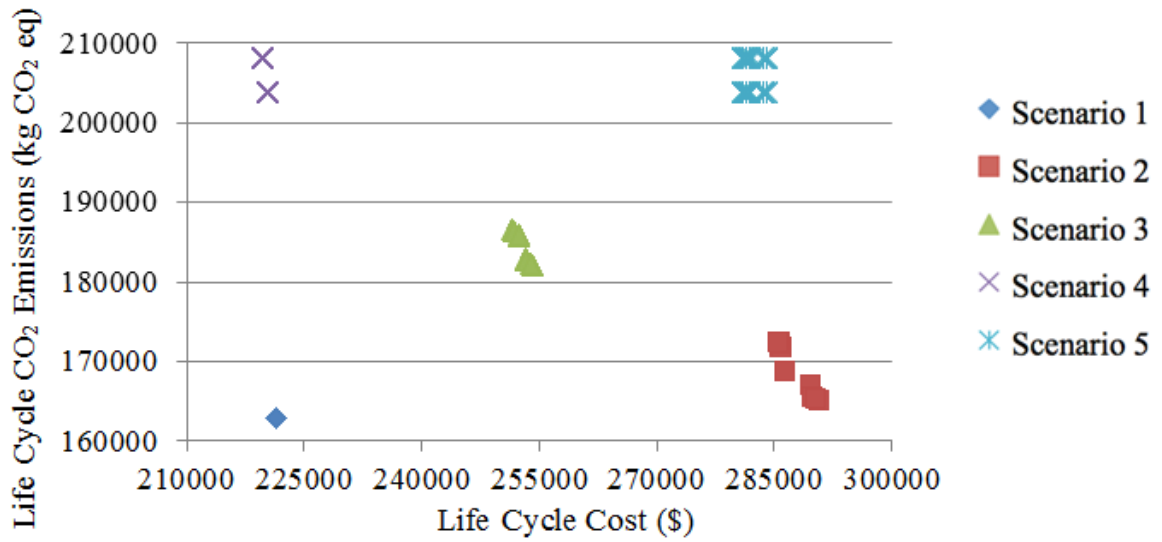


Figure 27 Graph Relationships between Cost and CO₂ Emissions for 40 Year-Usage Phase

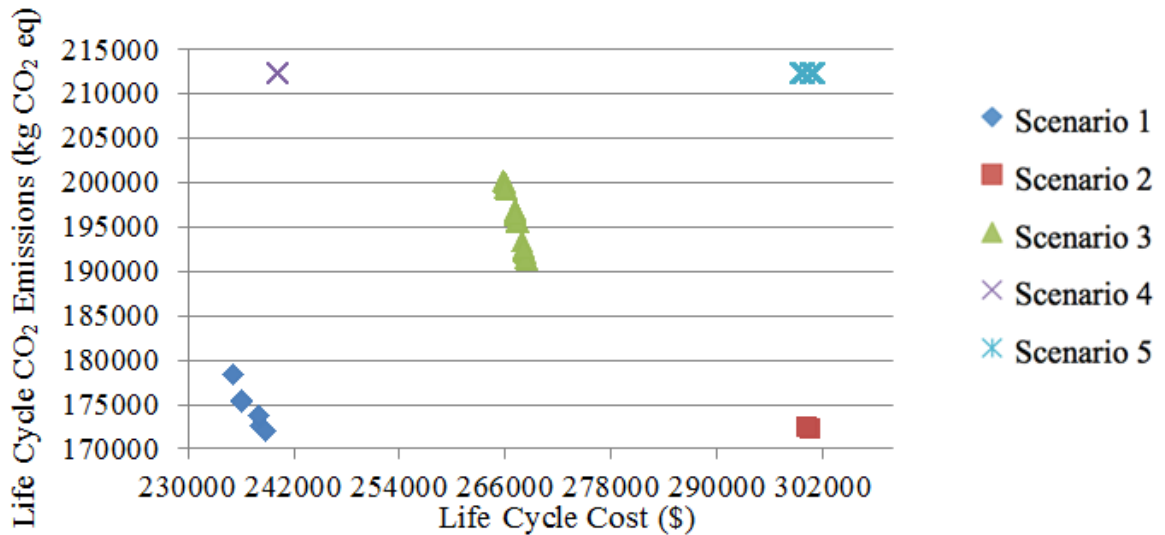


Figure 28 Graph Relationships between Cost and CO₂ Emissions for 45 Year-Usage Phase

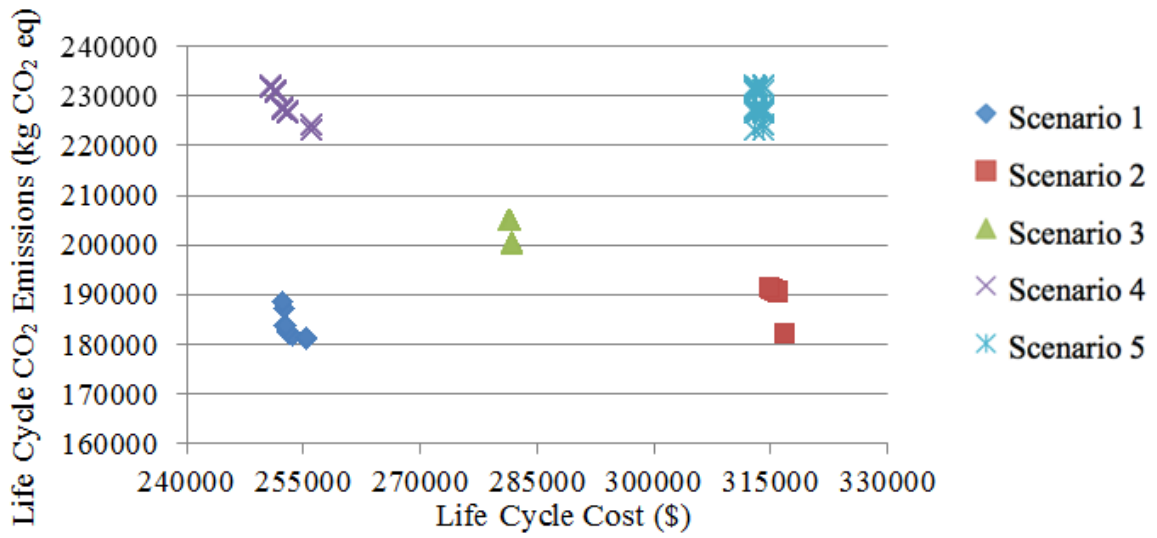


Figure 29 Graph Relationships between Cost and CO₂ Emissions for 50 Year-Usage Phase

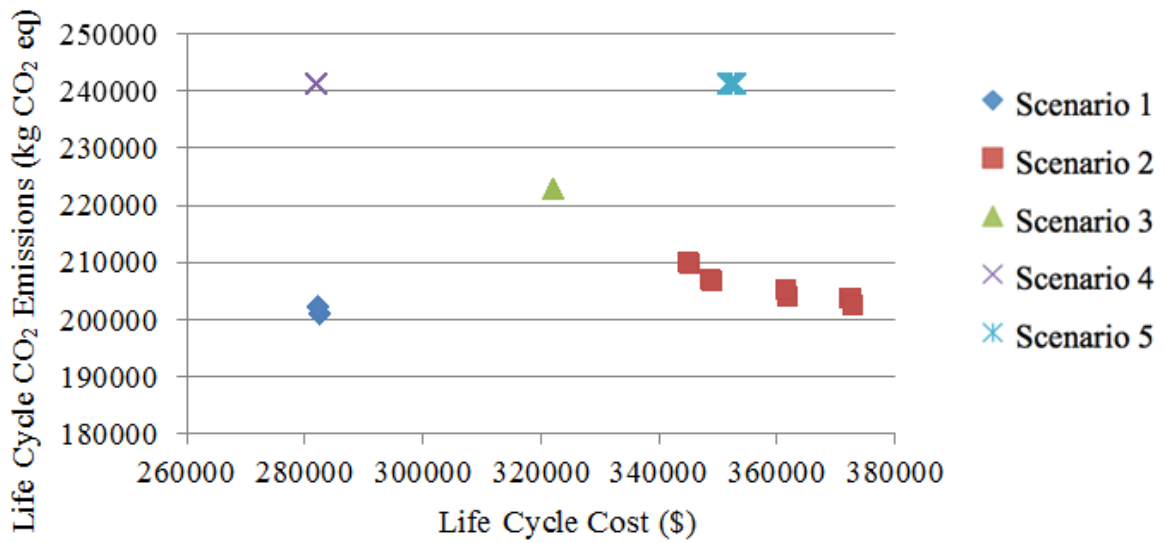


Figure 30 Graph Relationships between Cost and CO₂ Emissions for 60 Year-Usage Phase

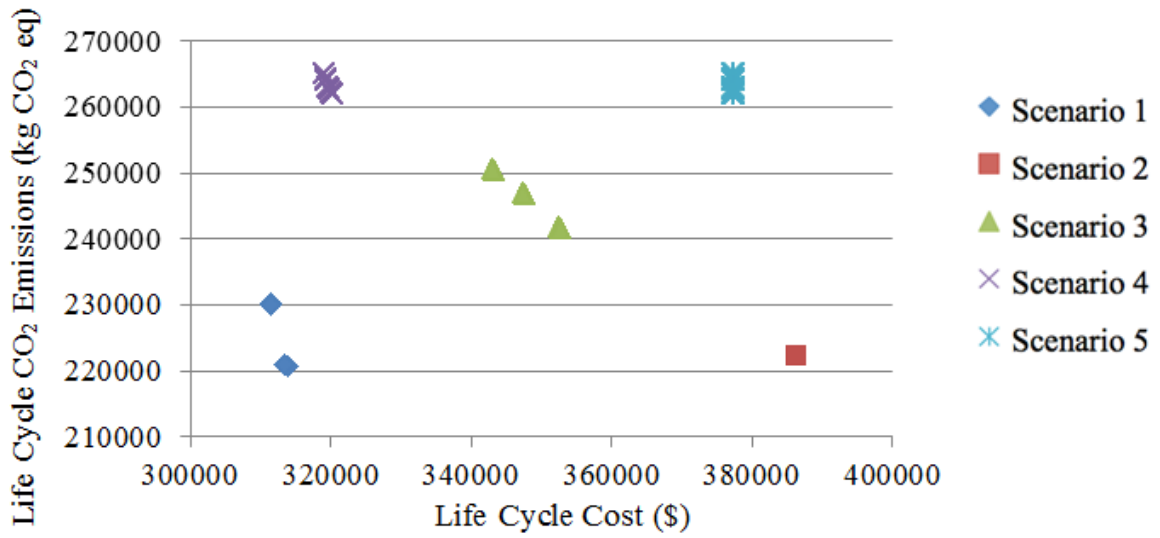


Figure 31 Graph Relationships between Cost and CO₂ Emissions for 70 Year-Usage Phase

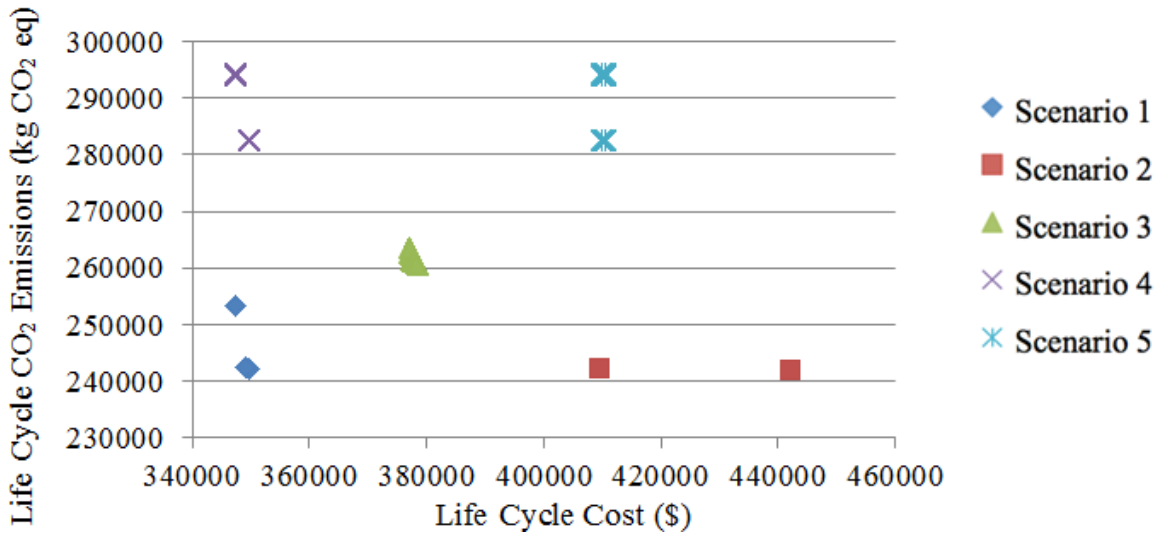


Figure 32 Graph Relationships between Cost and CO₂ Emissions for 80 Year-Usage Phase

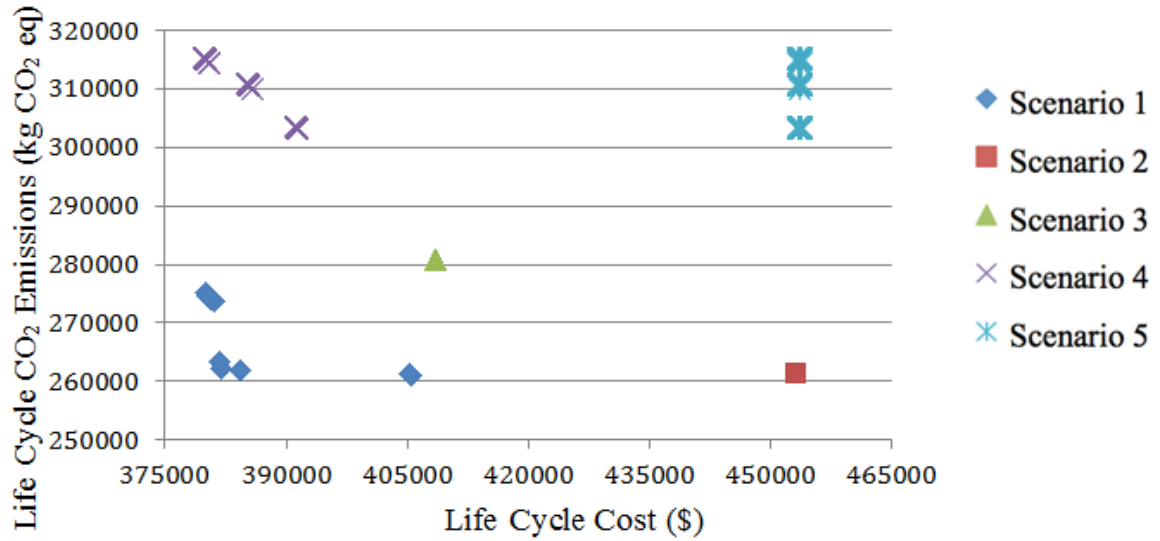


Figure 33 Graph Relationships between Cost and CO₂ Emissions for 90 Year-Usage Phase

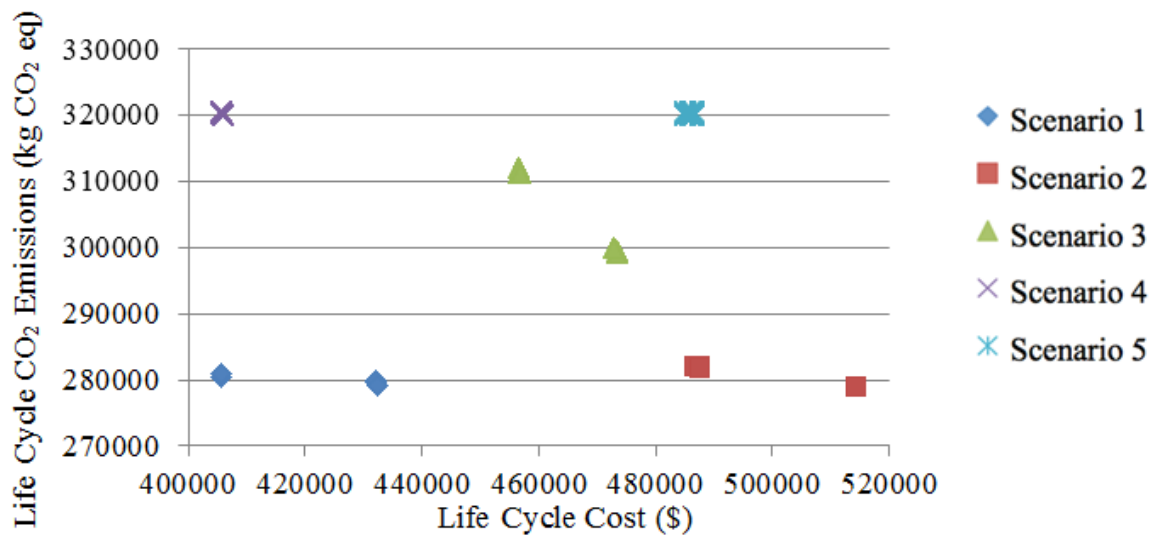


Figure 34 Graph Relationships between Cost and CO₂ Emissions for 100 Year-Usage Phase

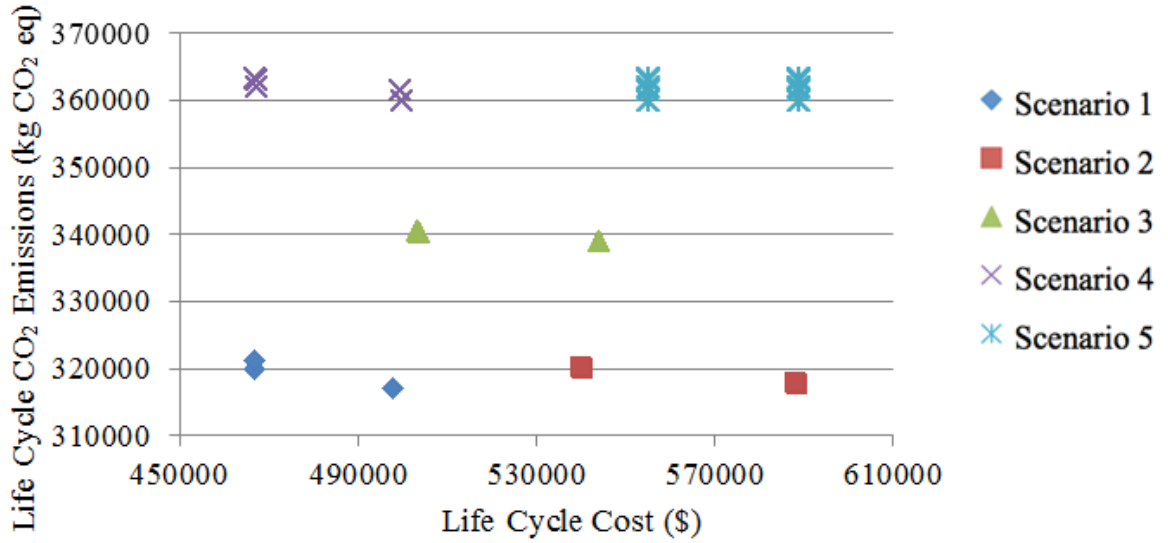


Figure 35 Graph Relationships between Cost and CO₂ Emissions for 120 Year-Usage Phase

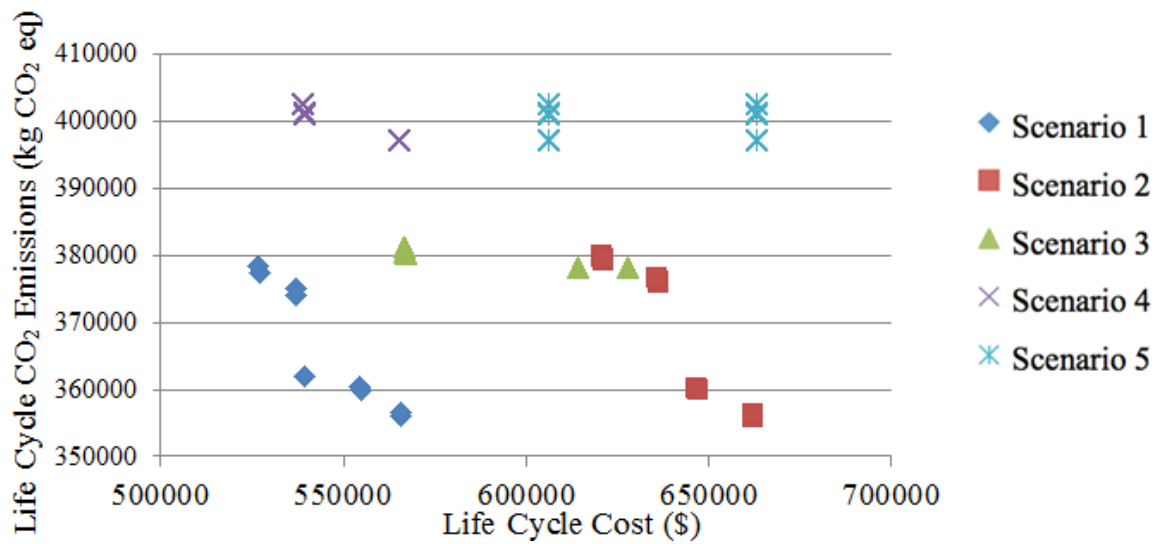


Figure 36 Graph Relationships between Cost and CO₂ Emissions for 140 Year-Usage Phase

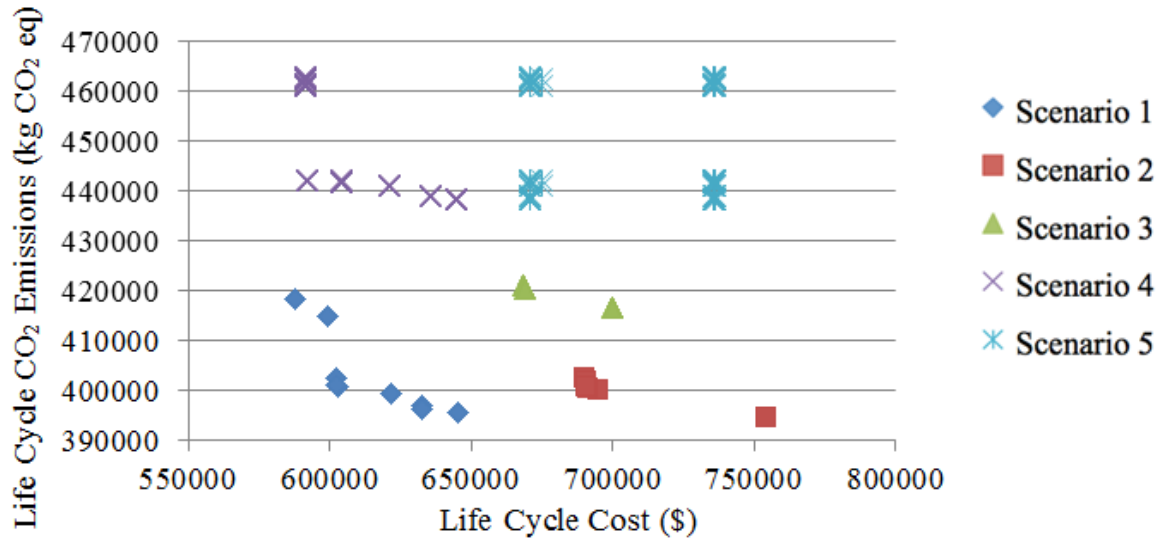


Figure 37 Graph Relationships between Cost and CO₂ Emissions for 160 Year-Usage Phase

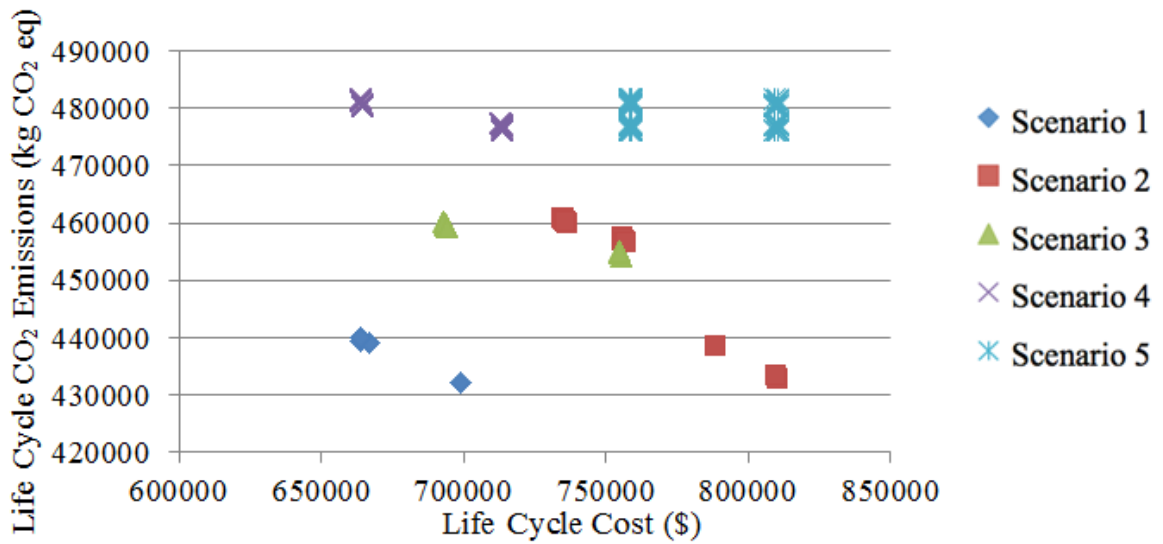


Figure 38 Graph Relationships between Cost and CO₂ Emissions for 180 Year-Usage Phase

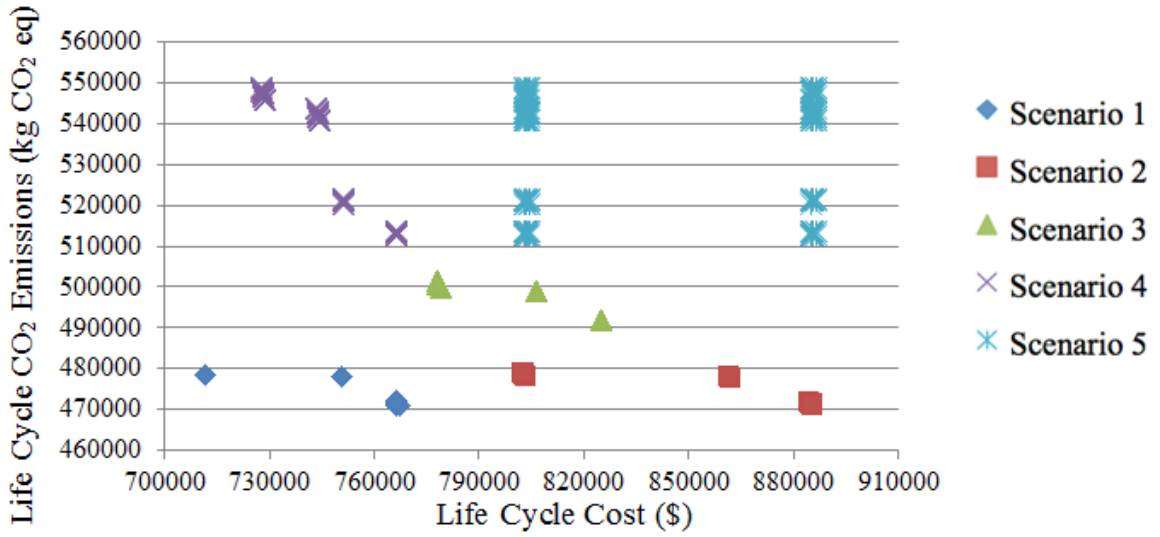


Figure 39 Graph Relationships between Cost and CO₂ Emissions for 200 Year-Usage Phase

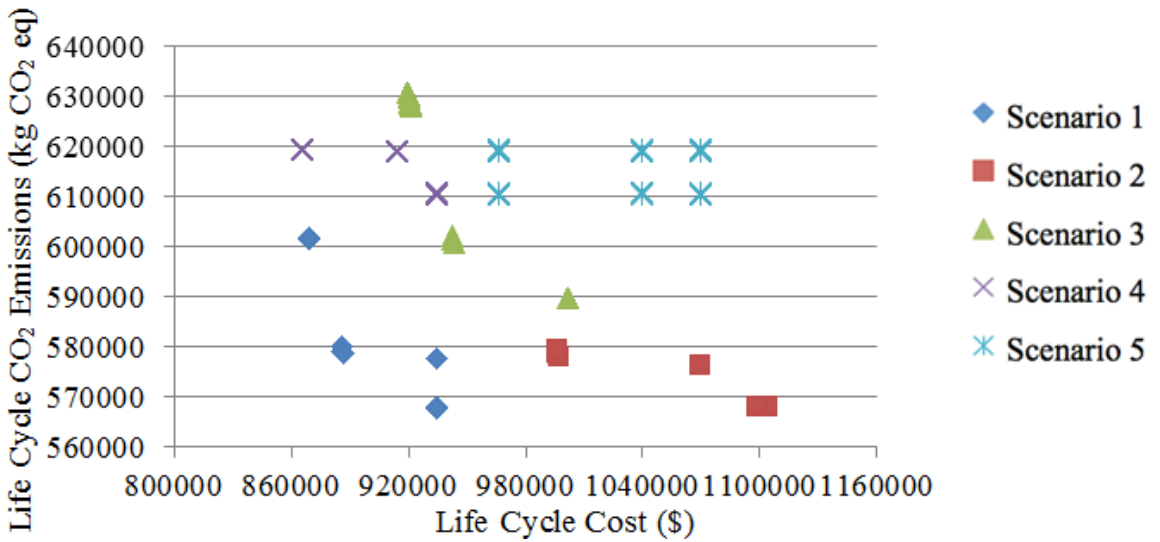


Figure 40 Graph Relationships between Cost and CO₂ Emissions for 250 Year-Usage Phase

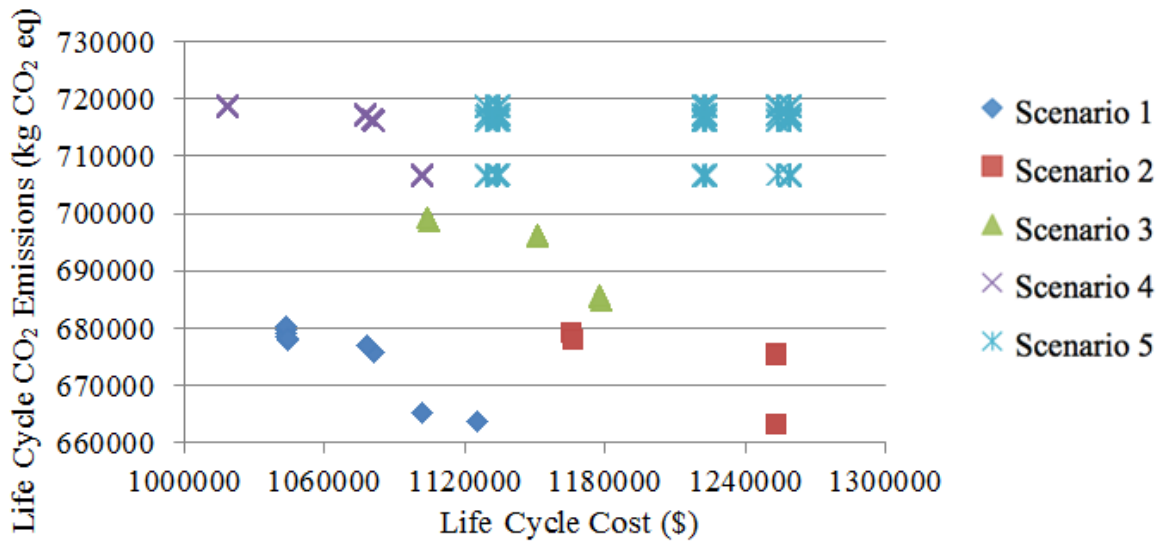


Figure 41 Graph Relationships between Cost and CO₂ Emissions for 300 Year-Usage Phase

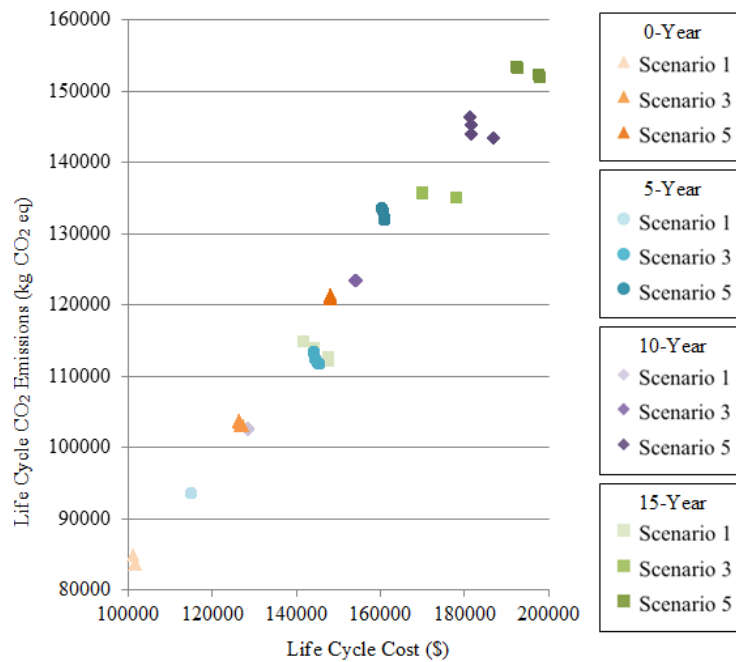


Figure 42 Graph Relationships between Cost and CO₂ Emissions for 0-15 Year-Usage Phase

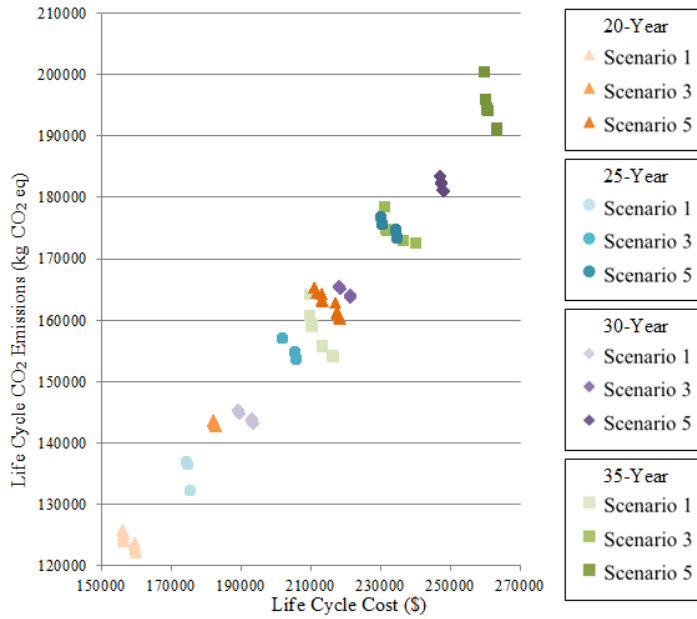


Figure 43 Graph Relationships between Cost and CO₂ Emissions for 20-35 Year-Usage Phase

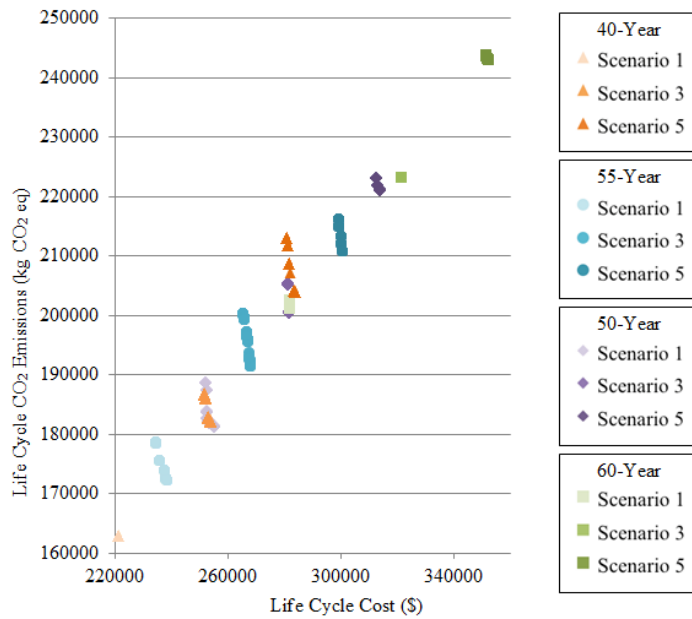


Figure 44 Graph Relationships between Cost and CO₂ Emissions for 40-60 Year-Usage Phase

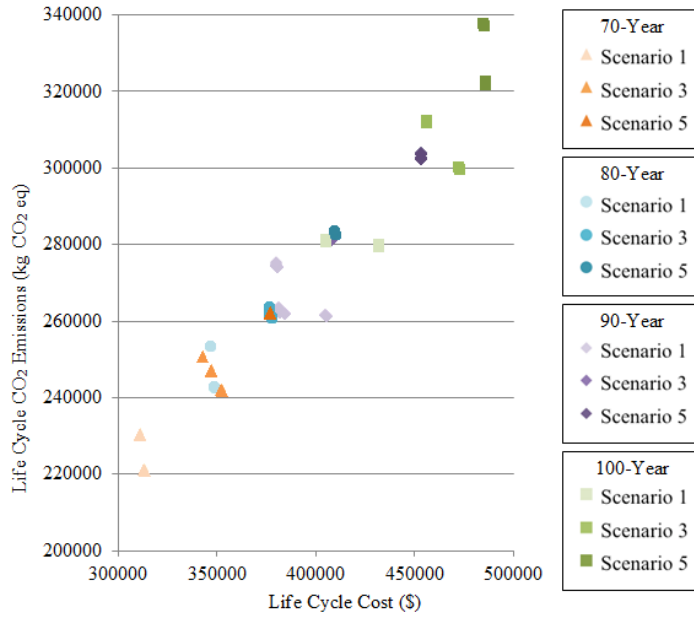


Figure 45 Graph Relationships between Cost and CO₂ Emissions for 70-100 Year-Usage Phase

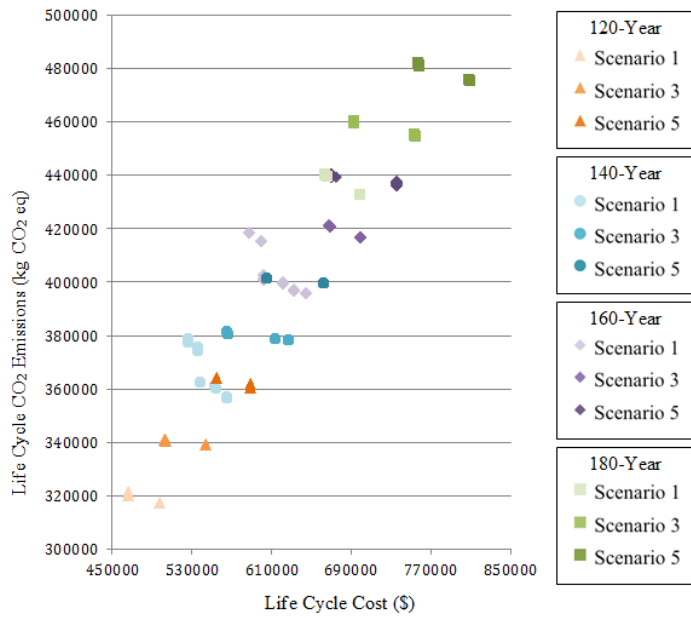


Figure 46 Graph Relationships between Cost and CO₂ Emissions for 120-180 Year-Usage Phase

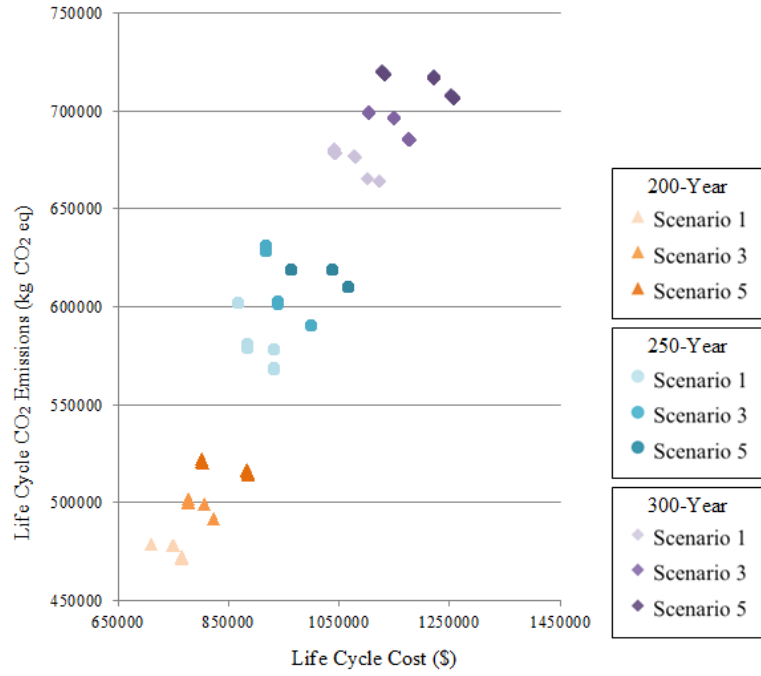


Figure 47 Graph Relationships between Cost and CO₂ Emissions for 200-300 Year-Usage Phase

Table 23 Longest Distance between Optimal Solutions

Year-life Span	Longest Distance in Scenario 1	Longest Distance in Scenario 2	Longest Distance between Scenario 1 and Scenario 5
0	1524.80	363.87	59706.00
5	0.00	1539.70	60521.00
10	212.82	6213.40	71270.00
15	6606.40	5685.30	67449.00

Year-life Span	Longest Distance in Scenario 1	Longest Distance in Scenario 2	Longest Distance between Scenario 1 and Scenario 5
20	5309.10	8974.70	71756.00
25	4676.40	5817.00	72524.00
30	4813.80	2567.40	69326.00
35	12196.00	10100.00	64434.00
40	0.00	9602.60	77891.00
45	7355.30	5694.80	75270.00
50	8021.50	2364.40	72366.00
60	1443.50	1544.40	81781.00
70	9950.30	363.87	75886.00
80	11354.00	868.31	73139.00
90	29070.00	1622.50	82584.00
100	26816.00	16096.00	98078.00

Year-life Span	Longest Distance in Scenario 1	Longest Distance in Scenario 2	Longest Distance between Scenario 1 and Scenario 5
120	31474.00	34208.00	128700.00
140	44917.00	56815.00	137960.00
160	61984.00	65628.00	149640.00
180	36145.00	52258.00	150410.00
200	55970.00	83808.00	178350.00
250	73802.00	103700.00	200470.00
300	83514.00	130920.00	217390.00

Table 24 Possible Solutions Area

Year-life Span	Area	Year-life Span	Area
0	4,624,322,259	70	2,487,263,500
5	1,884,892,437	80	2,567,941,584

Year-life Span	Area	Year-life Span	Area
10	2,136,728,498	90	3,022,607,567
15	2,005,638,557	100	3,831,183,598
20	1,997,452,267	120	3,467,015,776
25	2,225,180,820	140	1,827,117,616
30	2,241,579,858	160	3,582,412,096
35	2,157,759,259	180	2,456,031,705
40	2,717,006,625	200	4,820,645,408
45	2,417,392,774	250	3,051,588,804
50	2,333,636,211	300	4,624,322,259
60	2,396,333,904		

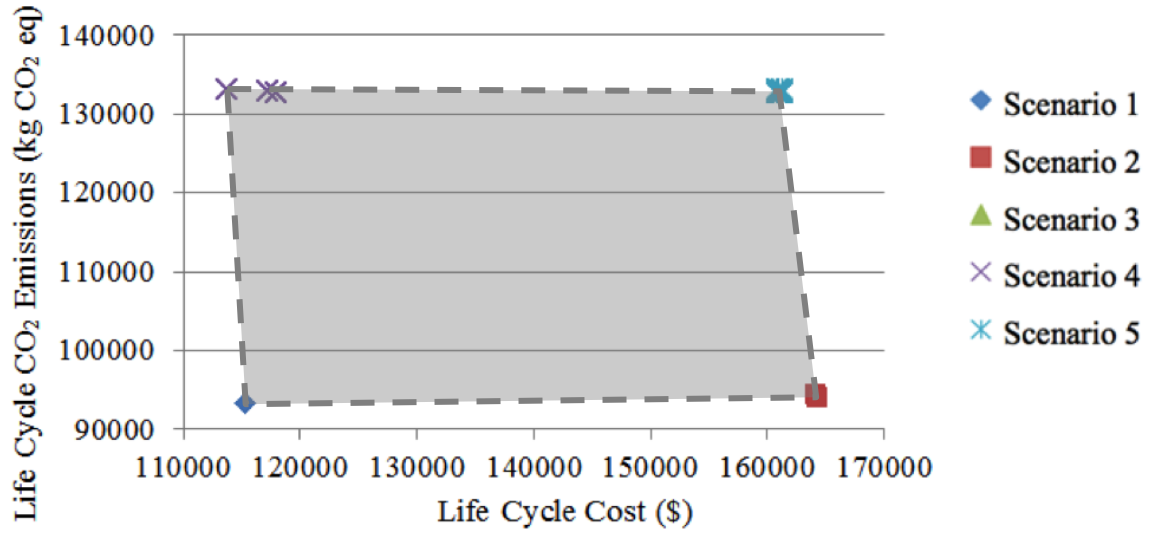


Figure 48 Graph Shows Area of Possible Solutions for 5 Year-Usage Phase

CHAPTER 7 CONCLUSIONS

7.1 Discussions and Conclusions

Sustainable building design is a rapidly emerging trend in the architecture, engineering, and construction (AEC) industry. The design process has resulted in greater integration of various AEC disciplines during the early design stages of construction projects. The delivery of sustainable building projects is a critical aspect of the AEC industry. These projects often face multiple and even conflicting objectives, such as time, cost, and environmental impact. A building design may have many options for using different materials, crews, and equipment, including construction methods that can be combined to meet project objectives. The number of possible design alternatives can be very large. Design professionals, construction professionals, and decision makers often face the challenge of selecting optimal building components and solutions in order to appropriately meet multi-objective and standard requirements. To effectively support the decision-making process during the early design phase, robust simulation-based technology is desirable.

Integrated applications in construction project management have been widely used in the AEC industry for many decades. Currently, there are many simulation-based tools that were developed in the industry for aid in sustainable design. Simulation of Environmental Impacts of Construction or SimuleICon is a multi-objective analytical tool for studying the relationships between time, cost, and environmental impact, which is capable of considering building life cycle information to optimization process and it

also takes data uncertainty and availability of data into account. Its functionality includes the ability to help design and construction professionals in the selection of building materials, components, and building design in order to find optimal design solutions based on the current three objectives: minimizing time, minimizing cost, and minimizing environmental impact, in terms of CO₂ emissions. The SimulEIcon application is developed to analyze the relationships between multiple objectives in different levels of a building: material, component, and building. The relationships between construction time, initial construction cost, and CO₂ emissions are considered in the pre-use phase analysis, while only life cycle cost and CO₂ emissions are accounted for in the usage phase within various building year-life spans. To address data uncertainty and availability, Monte Carlo simulation is applied in this research. Moreover, the selection process applies Genetic Algorithms, NSGA-II, to obtain a set of optimal solutions.

At the material level, six envelope material categories, which are structural component, exterior cladding, insulation, roofing, concrete footing, and concrete slab-on-grade, were chosen for SimulEIcon analysis. Two scenarios were investigated to understand the importance of material installation. Scenario 1 considered the relationship between cost and CO₂ emissions at the manufacturing phase. In scenario 2, installation time was considered in the analysis, along with cost and CO₂ emissions. Dominant alternatives were observed in all categories in scenario 1. However, the level of confidence for having a dominant alternative varied among categories from 99.8% to 0.3%. Only three categories had a level of confidence greater than 50%. Thus, the level of confidence that all categories had a dominant solution at the same time was very small.

The level of confidence consequently dropped in almost all categories of scenario 2. Additionally, in some categories, such as roofing, exterior cladding, and concrete footing, the level of confidence for having a dominant solution was near 0%. This is because there was commonly known trade-off behavior between time and cost. When installation was considered along with unit cost and CO₂ emissions per material unit, the level of confidence changed significantly. Categories did not provide a meaningful percentage of predominant alternatives. Material alternatives in those categories could have a fair chance to be chosen in the material selection process at the building design stage. In structural component and insulation categories, dominant alternatives still existed and they might have a potential impact on other levels. Thus, if those categories also quantitatively represented a major portion of materials in the building, the dominant alternatives of a structural component category and an insulation category should be carefully considered in a decision-making process.

The pattern analysis showed that the majority of data sets did not support the existence of trade-off patterns when all materials of a category are considered. Multiple relationships in subsets of a category made proper material decisions more complex. The study showed that the relationship between time, cost and CO₂ emissions at the material level is rather random. For example, installation time is mainly dependent upon the method of installation, which may not be directly and properly related to cost and CO₂ emissions; similarly, greener products may not be less expensive or faster to install. Such disconnections apparently exist in today's construction materials, which contributes to the "randomness" observed in this study. Therefore, the trade-off pattern at the material

level is not as obvious as many studies at building level claim. While market forces may sort out the randomness in material installation time, cost and environment impact in the long run, a more effective way to help decision makers properly select materials is important.

At the component and building level, during the pre-use phase, two case studies were used to demonstrate the relationships between construction time, initial construction cost, and CO₂ emissions. The results of case studies showed that if only considering three objectives without other design, engineering and construction constraints, there was not one design solution that was clearly dominating. It is thus unlikely that a chosen design option is absolutely dominant to others, or dominated by others, if the chosen design option is one of the optimal design solutions. This proposition is reflected in the real world where the decision of building design selection is often influenced by many factors other than construction time, cost, and environmental impact. It seems that trade-off relationships do exist between construction time and initial construction cost, and between construction time and CO₂ emissions in many cases. While the trade-off relationship between cost and time has been well understood, it is interesting to see the trade-off relationship between construction time and CO₂ emissions. The results showed that, in many cases, there was no trade-off relationship between cost and CO₂ emissions. This is mainly because the cost was an initial cost or direct cost, such as materials, equipment, and labor. As stated, adding more resources can result in higher CO₂ emission. Thus, higher costs may be associated with higher CO₂ emissions.

In the last analysis, maintenance and energy consumption from the usage phase were considered in the optimal solutions. The case study 1 with energy simulation information was used in this stage. Five scenarios were simulated to represent all possible solution ranges. Maintenance and energy consumption cost were accounted for completing life cycle cost of the building, while CO₂ emissions from energy consumption is used as energy-related CO₂ emissions data in the optimization process. Different building life spans were utilized to see if the relationship transformed with time. During the pre-use phase, as stated above, the trade-off relationship between initial construction cost and CO₂ emissions did not exist. Proportional relationship continually occurred after the construction phase to the usage phase. However, the relationship between life cycle cost and CO₂ emissions developed its interrelation and starts to compromisingly exhibit trade-off behavior. However, the results from the case study showed that there was no trade-off between life cycle cost and CO₂ emissions in all observed life span.

Validation of SimuleICon or similar approaches is difficult for several reasons (Sargent, 2005). Most validation approaches require experts or professionals to assess the validity of the simulation results and there is no exact test to determine the validity of the model because the results are not implemented. This problem is compounded by the fact that SimuleICon yields a wide array of different possible solutions that change with each different simulation due to the effects of uncertainty and the optimization process. Thus, in this research, instead of striving for a full-scale validation, two validity concepts were performed. Construct validity was accomplished by examining the reliability of SimuleICon's results (Lucko & Rojas, 2009). The tool was utilized with other research's

data to ensure the performance and accuracy of its output. The case studies using in the research are the real buildings that had already been constructed. Content validity was possible to calibrate the simulations' results with the real data. For example, the actual annual energy consumption of the case study 1 was used in comparison with results from energy simulation and to create a factor in order to match data.

To reach a conclusion, the proposed application, SimuleICon, is presented as an analytical tool for multi-objective optimization problems. This tool is meant to not only help identify the relationship between the project's objectives but also to aid design and construction professionals during the design phase of the buildings. It was pointed out that the construction project tends to have multiple objectives and those objectives should not be independently assessed during the decisions-making process. Understanding the relationships between those objectives is a key in successfully planning and designing environmentally sustainable construction projects.

7.2 Limitation and Future Studies

Within limited resources and data, this research did not identify factors at the material level that contributed to data patterns at the building level. Further studies should have a focus on this topic. In addition, since material quantities can have a significant impact on building-level data patterns, analysis should be performed to better understand the impact of material quantities on connecting material level time, cost and environment impacts to the building level. The study was based on limited data samples. Future studies should also focus on increasing the data samples. Moreover, conclusions are

derived based on two similar buildings case study, which limited the scope of work. Energy simulation for larger buildings takes time to calculate and construct. Most data is not available or ready to input to the simulation.

Finally, future studies should include more cases and a larger scope in each case study to derive better results. Furthermore, in reality, historical data is considerably hard to obtain and also not always available. A literature review can provide probability distributions to present the behavior of the data. Additional data is necessary for future studies to provide more accurate and appropriate design solutions.

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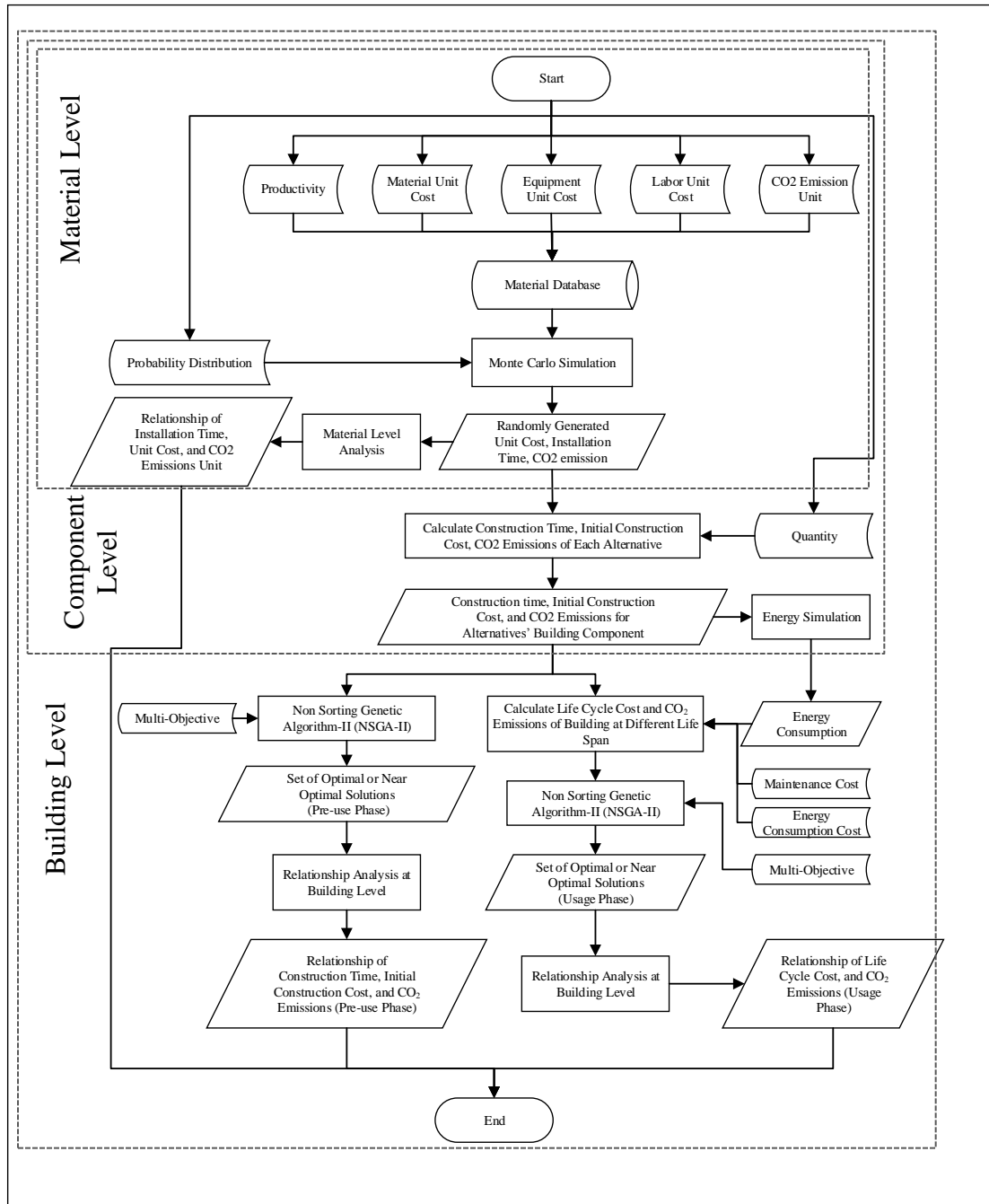
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APPENDICES

Appendix A: Flow Chart of SimuleICon



Simulation of Environmental Impact of Construction Framework

Appendix B: Data Collection Form

Activity Number	Activity Name	Alternative Number	Alternative Description	Quantity		Labor Cost (\$)		Productivity			
				Amount	Unit	Unit Cost	Total Cost	Productivity	Unit	Duration	

(1) Data Collection Form Part 1

Building Material	Total Emissions									
	Emissions per Unit									
	Operation Impact									
	End of Life Impact									
	Maintenance Impact									
	Construction Impact									
	Manufacturing Impact									
	Unit Emission									
	Total Cost									
	Unit Cost									
Quantity	Unit									
	Amount									
	Alternative Description									
	Alternative Number									
	Activity Name									
	Activity Number									

(2) Data Collection Form Part 2

Auxiliary Material	Total Emissions									
	Emissions per Unit									
	Operation Impact									
	End of Life Impact									
	Maintenance Impact									
	Construction Impact									
	Manufacturing Impact									
	Unit Emission									
	Total Cost									
	Unit Cost									
	Unit									
	Quantity									
Quantity	Unit									
	Amount									
	Alternative Description									
	Alternative Number									
	Activity Name									
	Activity Number									

(3) Data Collection Form Part 3

Activity Number	Activity Name	Alternative Number	Alternative Description	Quantity		Equipment					Total					
				Amount	Unit	Unit Cost	Total Cost	Unit Emission	Emissions per Unit	Total Emissions	Time	Cost	Environmental Impact (CO ₂ Emissions)			

(4) Data Collection Form Part 4

Appendix C: Case Studies Activates and Alternatives

Case Study 1: The Zero Net Energy Laboratory

Activity Number	Activity Name	Alternative Number	Alternative Description
1	Start	1	Start
2	Site Clearing		Cut & chip trees to 12" diam, Grading for small area
		2	Cut & chip trees to 12" diam, grub stumps and remove Grading for small area
		3	No tree, Grading for small area
3	Excavation	1	Excavation using 3/8 CY excavator
		2	Excavation using 1/2 CY excavator
		3	Manual excavation
4	Footing Construction	1	3000 psi, average flyash, pumped Reinforcing in Place, footings
		2	3000 psi , 25% flyash, pumped Reinforcing in Place, footings
		3	3000 psi, 30% flyash, pumped Reinforcing in Place, footings
		4	3000 psi, average flyash, direct chute Reinforcing in Place, footings
		5	3000 psi , 25% flyash, direct chute Reinforcing in Place, footings
		6	3000 psi, 30% flyash, direct chute Reinforcing in Place, footings
5	Stem Wall Construction	1	3000 psi, average flyash, pumped Reinforcing in Place, walls
		2	3000 psi , 25% flyash, pumped Reinforcing in Place, walls
		3	3000 psi, 30% flyash, pumped Reinforcing in Place, walls
		4	3000 psi, average flyash, direct chute Reinforcing in Place, walls
		5	3000 psi , 25% flyash, direct chute Reinforcing in Place, walls
		6	3000 psi, 30% flyash, direct chute Reinforcing in Place, walls
6	Subgrade Insulation	1	Blown Cellulose Board
		2	Batt Rockwool

Activity Number	Activity Name	Alternative Number	Alternative Description
		3	Batt Fiberglass
7	Backfill	1	FE loader, wheel mtd, 1 cy bucket
8	Slab-on-Grade Construction	1	4", 3000 psi, average flyash, pumped Reinforcing in Place, walls
		2	4", 3000 psi , 25% flyash, pumped Reinforcing in Place, walls
		3	4", 3000 psi, 35% flyash, pumped Reinforcing in Place, walls
		4	4", 3000 psi, average flyash, direct chute Reinforcing in Place, walls
		5	4", 3000 psi , 25% flyash, direct chute Reinforcing in Place, walls
		6	4", 3000 psi, 35% flyash, direct chute Reinforcing in Place, walls
9	Exterior Wall Construction (Conditioned Zone)	1	SIP, 5.5" thickness Maintenance Curtain Wall
		2	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board 5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick Curtain Wall
		3	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene 5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick Curtain Wall
		4	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 5/8" FR Drywall

Activity Number	Activity Name	Alternative Number	Alternative Description
			3/8" Plywood
			Concrete Brick
			Maintenance Concrete Brick
			Curtain Wall
		5	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Fiberglass
			5/8" FR Drywall
			3/8" Plywood
			Concrete Brick
			Maintenance Concrete Brick
			Curtain Wall
10	Exterior Wall Construction (Electrical Zone)	1	SIP, 5.5" thickness
			Maintenance
		2	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board
			5/8" FR Drywall
			3/8" Plywood
			Concrete Brick
			Maintenance Concrete Brick
		3	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Extruded Polystyrene
			5/8" FR Drywall
			3/8" Plywood
			Concrete Brick
			Maintenance Concrete Brick
		4	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool
			5/8" FR Drywall
			3/8" Plywood
			Concrete Brick
			Maintenance Concrete Brick
		5	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Fiberglass

Activity Number	Activity Name	Alternative Number	Alternative Description
11	Exterior Wall Construction (Mechanical Zone)	1	5/8" FR Drywall
			3/8" Plywood
			Concrete Brick Maintenance Concrete Brick SIP, 5.5" thickness
		2	Maintenance
			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board
			5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick
		3	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene
			5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick
			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool
		4	5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick
			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool
			5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick
		5	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass
			5/8" FR Drywall 3/8" Plywood Concrete Brick Maintenance Concrete Brick
			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass
12	Roof Framing	1	Wide Flange Beam
13	Roof Construction	1	SIP, 5.5" thickness
14	Interior Wall	1	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8

Activity Number	Activity Name	Alternative Number	Alternative Description
	Construction		Fiberglass Insulation 5/8" FR Drywall
15	Roofing	1	Clay tiles Maintenance Inspection Yearly Minor Repair
		2	Concrete tiles Maintenance Inspection Yearly Minor Repair
		3	Organic felt shingles 30yr Maintenance Inspection Yearly Minor Repair
		4	Install New Over Old Steel Roof Panel 30 GA (Residential) Maintenance Inspection Yearly Minor Repair
16	Flooring	1	Bamboo flooring
		2	Wood flooring
17	Finish	1	Finish

Case Study 2: The Future House Project USA

Activity Number	Activity Name	Alternative Number	Alternative Description
1	Start	1	Start
2	Site Clearing	1	Cut & chip trees to 12" diam, Grading for small area
		2	Cut & chip trees to 12" diam, grub stumps and remove
		2	Grading for small area
		3	No tree, Grading for small area
3	Excavation	1	Excavation using 3/8 CY excavator
		2	Excavation using 1/2 CY excavator
		3	Manual excavation
4	Footing Construction	1	3000 psi, average flyash, pumped Reinforcing in Place, footings
		2	3000 psi , 25% flyash, pumped Reinforcing in Place, footings

Activity Number	Activity Name	Alternative Number	Alternative Description		
5	Stem Wall Construction	3	3000 psi, 30% flyash, pumped Reinforcing in Place, footings		
		4	3000 psi, average flyash, direct chute Reinforcing in Place, footings		
		5	3000 psi , 25% flyash, direct chute Reinforcing in Place, footings		
		6	3000 psi, 30% flyash, direct chute Reinforcing in Place, footings		
		1	3000 psi, average flyash, pumped Reinforcing in Place, walls		
		2	3000 psi , 25% flyash, pumped Reinforcing in Place, walls		
		3	3000 psi, 30% flyash, pumped Reinforcing in Place, walls		
		4	3000 psi, average flyash, direct chute Reinforcing in Place, walls		
		5	3000 psi , 25% flyash, direct chute Reinforcing in Place, walls		
		6	3000 psi, 30% flyash, direct chute Reinforcing in Place, walls		
		6	Subgrade Insulation	1	Expanded Polystyrene Board
				2	Extruded Polystyrene Board
3	Foam Polyisocyanurate Board				
4	Blown Cellulose Board				
7	Backfill	1	FE loader, wheel mtd, 1 cy bucket		
8	Slab-on-Grade Construction		4", 3000 psi, average flyash, pumped Reinforcing in Place, walls		
		2	4", 3000 psi , 25% flyash, pumped Reinforcing in Place, walls		
		3	4", 3000 psi, 35% flyash, pumped Reinforcing in Place, walls		
		4	4", 3000 psi, average flyash, direct chute Reinforcing in Place, walls		
		5	4", 3000 psi , 25% flyash, direct chute Reinforcing in Place, walls		
		6	4", 3000 psi, 35% flyash, direct chute		

Activity Number	Activity Name	Alternative Number	Alternative Description
		7	Reinforcing in Place, walls 8", 3000 psi, average flyash
		8	Reinforcing in Place, walls 8", 3000 psi , 25% flyash
		9	Reinforcing in Place, walls 8", 3000 psi, 35% flyash
		10	Reinforcing in Place, walls 8", 3000 psi, average flyash
		11	Reinforcing in Place, walls 8", 3000 psi , 25% flyash
		12	Reinforcing in Place, walls 8", 3000 psi, 35% flyash
9	Exterior Wall Construction	1	SIP, 5.5" thickness
		2	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board 1/2" Regular Drywall 3/8" Plywood
		3	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board 5/8" Regular Drywall 3/8" Plywood
		4	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board 1/2" FR Drywall 3/8" Plywood
		5	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board 5/8" FR Drywall 3/8" Plywood
		6	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board 1/2" WR Drywall 3/8" Plywood
		7	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board 5/8" WR Drywall

Activity Number	Activity Name	Alternative Number	Alternative Description
			3/8" Plywood
		8	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board 1/2" Regular Drywall 3/8" Plywood
		9	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board 5/8" Regular Drywall 3/8" Plywood
		10	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board 1/2" FR Drywall 3/8" Plywood
		11	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board 5/8" FR Drywall 3/8" Plywood
		12	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board 1/2" WR Drywall 3/8" Plywood
		13	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board 5/8" WR Drywall 3/8" Plywood
		14	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Rockwool 1/2" Regular Drywall 3/8" Plywood
		15	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Rockwool 5/8" Regular Drywall 3/8" Plywood
		16	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Rockwool 1/2" FR Drywall 3/8" Plywood

Activity Number	Activity Name	Alternative Number	Alternative Description
		17	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Rockwool 5/8" FR Drywall 3/8" Plywood
		18	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Rockwool 1/2" WR Drywall 3/8" Plywood
		19	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Roackwool 5/8" WR Drywall 3/8" Plywood
		20	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Fiberglass 1/2" Regular Drywall 3/8" Plywood
		21	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Fiberglass 5/8" Regular Drywall 3/8" Plywood
		22	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Fiberglass 1/2" FR Drywall 3/8" Plywood
		23	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Fiberglass
		23	5/8" FR Drywall 3/8" Plywood
		24	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Fiberglass 1/2" WR Drywall 3/8" Plywood
		25	Wood Stud Kiln Dired 16 o.c., 2x4 Batt Fiberglass 5/8" WR Drywall 3/8" Plywood
		26	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8

Activity Number	Activity Name	Alternative Number	Alternative Description
			Expanded Polystyrene Board
			1/2" Regular Drywall
			3/8" Plywood
27			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board
			5/8" Regular Drywall
			3/8" Plywood
28			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board
			1/2" FR Drywall
			3/8" Plywood
29			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board
			5/8" FR Drywall
			3/8" Plywood
30			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board
			1/2" WR Drywall
			3/8" Plywood
31			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board
			5/8" WR Drywall
			3/8" Plywood
32			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Extruded Polystyrene
			1/2" Regular Drywall
			3/8" Plywood
33			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Extruded Polystyrene
			5/8" Regular Drywall
			3/8" Plywood
34			Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8
			Extruded Polystyrene
			1/2" FR Drywall

Activity Number	Activity Name	Alternative Number	Alternative Description
			3/8" Plywood
		35	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene 5/8" FR Drywall 3/8" Plywood
		36	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene 1/2" WR Drywall 3/8" Plywood
		37	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene 5/8" WR Drywall 3/8" Plywood
		38	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 1/2" Regular Drywall 3/8" Plywood
		39	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 5/8" Regular Drywall 3/8" Plywood
		40	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 1/2" FR Drywall 3/8" Plywood
		41	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 5/8" FR Drywall 3/8" Plywood

Activity Number	Activity Name	Alternative Number	Alternative Description
		42	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 1/2" WR Drywall 3/8" Plywood
		43	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Rockwool 5/8" WR Drywall 3/8" Plywood
		44	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass 1/2" Regular Drywall 3/8" Plywood
		45	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass 5/8" Regular Drywall 3/8" Plywood
		46	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass 1/2" FR Drywall 3/8" Plywood
		47	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass 5/8" FR Drywall 3/8" Plywood
		48	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8 Batt Fiberglass 1/2" WR Drywall 3/8" Plywood
		49	Steel Stud (20 GA) 16 o.c., 1 5/8 x 3 5/8

Activity Number	Activity Name	Alternative Number	Alternative Description
			Batt Fiberglass
			5/8" WR Drywall
			3/8" Plywood
10	Roof Truss	1	Light Frame Wood Truss Roof, span 24' to 29', Light Frame Wood Truss Roof, span 30' to 33'
11	Roof Construction	1	SIP, 5.5" thickness
		2	Glass fiber batt (Deck) 3/8" Plywood (Deck) Glass fiber batt (Truss) 3/8" Plywood (Truss)
		3	Expanded Polystyrene Board (Deck) 3/8" Plywood (Deck) Expanded Polystyrene Board (Truss) 3/8" Plywood (Truss)
		4	Extruded Polystyrene Board (Deck) 3/8" Plywood (Deck) Extruded Polystyrene Board (Truss) 3/8" Plywood (Truss)
		5	Foam Polyisocyanurate Board (Deck) 3/8" Plywood (Deck) Foam Polyisocyanurate Board (Truss) 3/8" Plywood (Truss)
		6	Blown Cellulose Board (Deck) 3/8" Plywood (Deck) Blown Cellulose Board (Truss) 3/8" Plywood (Truss)
12	Interior Wall Construction	1	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board (1" thickness) 1/2" Regular Drywall
		2	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board (1" thickness) 5/8" Regular Drywall
		3	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board (1"

Activity Number	Activity Name	Alternative Number	Alternative Description
			thickness)
			1/2" FR Drywall
		4	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board (1" thickness)
			5/8" FR Drywall
		5	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board (1" thickness)
			1/2" WR Drywall
		6	Wood Stud Kiln Dired 16 o.c., 2x4 Expanded Polystyrene Board (1" thickness)
			5/8" WR Drywall
		7	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board (1" thickness)
			1/2" Regular Drywall
		8	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board (1" thickness)
			5/8" Regular Drywall
		9	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board (1" thickness)
			1/2" FR Drywall
		10	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board (1" thickness)
			5/8" FR Drywall
		11	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board (1" thickness)
			1/2" WR Drywall
		12	Wood Stud Kiln Dired 16 o.c., 2x4 Extruded Polystyrene Board (1" thickness)
			5/8" WR Drywall
		13	Wood Stud Kiln Dired 16 o.c., 2x4

Activity Number	Activity Name	Alternative Number	Alternative Description
			Batt Rockwool (1" thickness)
			1/2" Regular Drywall
		14	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt Rockwool (1" thickness)
			5/8" Regular Drywall
		15	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt Rockwool (1" thickness)
			1/2" FR Drywall
		16	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt Rockwool (1" thickness)
			5/8" FR Drywall
		17	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt Rockwool (1" thickness)
			1/2" WR Drywall
		18	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt Rockwool (1" thickness)
			5/8" WR Drywall
		19	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt fiberglass (1" thickness)
			1/2" Regular Drywall
		20	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt fiberglass (1" thickness)
			5/8" Regular Drywall
		21	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt fiberglass (1" thickness)
			1/2" FR Drywall
		22	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt fiberglass (1" thickness)
			5/8" FR Drywall
		23	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt fiberglass (1" thickness)
			1/2" WR Drywall
		24	Wood Stud Kiln Dired 16 o.c., 2x4
			Batt fiberglass (1" thickness)
			5/8" WR Drywall
		25	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Expanded Polystyrene Board (1"

Activity Number	Activity Name	Alternative Number	Alternative Description
			thickness)
			1/2" Regular Drywall
		26	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board (1" thickness)
			5/8" Regular Drywall
		27	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board (1" thickness)
			1/2" FR Drywall
		28	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board (1" thickness)
			5/8" FR Drywall
		29	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board (1" thickness)
			1/2" WR Drywall
		30	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Expanded Polystyrene Board (1" thickness)
			5/8" WR Drywall
		31	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene Board (1" thickness)
			1/2" Regular Drywall
		32	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene Board (1" thickness)
			5/8" Regular Drywall
		33	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene Board (1" thickness)
			1/2" FR Drywall
		34	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Extruded Polystyrene Board (1" thickness)
			5/8" FR Drywall
		35	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8

Activity Number	Activity Name	Alternative Number	Alternative Description
			Extruded Polystyrene Board (1" thickness)
			1/2" WR Drywall
36			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Extruded Polystyrene Board (1" thickness)
			5/8" WR Drywall
37			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool (1" thickness)
			1/2" Regular Drywall
38			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool (1" thickness)
			5/8" Regular Drywall
39			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool (1" thickness)
			1/2" FR Drywall
40			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool (1" thickness)
			5/8" FR Drywall
41			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool (1" thickness)
			1/2" WR Drywall
42			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt Rockwool (1" thickness)
			5/8" WR Drywall
43			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt fiberglass (1" thickness)
			1/2" Regular Drywall
44			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt fiberglass (1" thickness)
			5/8" Regular Drywall
45			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt fiberglass (1" thickness)
			1/2" FR Drywall
46			Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8
			Batt fiberglass (1" thickness)
			5/8" FR Drywall

Activity Number	Activity Name	Alternative Number	Alternative Description
		47	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Batt fiberglass (1" thickness) 1/2" WR Drywall
		48	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 Batt fiberglass (1" thickness) 5/8" WR Drywall
		49	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 5/8" FR Drywall
		50	Wood Stud Kiln Dired 16 o.c., 2x4 1/2" Regular Drywall
		51	Wood Stud Kiln Dired 16 o.c., 2x4 5/8" Regular Drywall
		52	Wood Stud Kiln Dired 16 o.c., 2x4 1/2" FR Drywall
		53	Wood Stud Kiln Dired 16 o.c., 2x4 5/8" FR Drywall
		54	Wood Stud Kiln Dired 16 o.c., 2x4 1/2" WR Drywall
		55	Wood Stud Kiln Dired 16 o.c., 2x4 5/8" WR Drywall
		56	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 1/2" Regular Drywall
		57	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 5/8" Regular Drywall
		58	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 1/2" FR Drywall
		59	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 5/8" FR Drywall
		60	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 1/2" WR Drywall
		61	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 5/8" WR Drywall
		62	Steel Stud (25 GA) 16 o.c., 1 5/8 x 3 5/8 5/8" FR Drywall
13	Roofing	1	Clay tiles
		2	Concrete tiles
		3	Organic felt shingles 20yr

Activity Number	Activity Name	Alternative Number	Alternative Description
		4	Organic felt shingles 25yr
		5	Organic felt shingles 30yr
		6	Steel Roof Panel 30 GA (Residential)
14	Flooring	1	Bamboo flooring
		2	Wood flooring
15	Exterior Siding	1	Concrete Brick
		2	Metric Modular Brick
		3	Cedar beval, 1/2, 6"
		4	Stucco
		5	Vinyl
		6	Fiber Cement
		7	Stucco (Top), Natural Stone (Bottom)
		8	Stucco (Top), Concrete Brick (Bottom)
16	Finish	1	Finish

Appendix D: Partial Base IDF File

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!-Generator IDFEditor 1.43
!-Option OriginalOrderTop UseSpecialFormat
!-NOTE: All comments with '!-' are ignored by the IDFEditor and are
generated automatically.
!-Use '!' comments if they need to be retained when using the
IDFEditor.

Version,7.2;

SimulationControl,
No,           !- Do Zone Sizing Calculation
No,           !- Do System Sizing Calculation
No,           !- Do Plant Sizing Calculation
No,           !- Run Simulation for Sizing Periods
Yes;         !- Run Simulation for Weather File Run Periods

Building,
UNT,         !- Name
0.0,        !- North Axis {deg}
City,       !- Terrain
0.04,       !- Loads Convergence Tolerance Value
0.4,        !- Temperature Convergence Tolerance Value
{deltaC}
MinimalShading, !- Solar Distribution
25,         !- Maximum Number of Warmup Days
;           !- Minimum Number of Warmup Days

SurfaceConvectionAlgorithm:Inside,TARP;

SurfaceConvectionAlgorithm:Outside,DOE-2;

HeatBalanceAlgorithm,ConductionTransferFunction,200,0.1,1000;

ZoneAirHeatBalanceAlgorithm,ThirdOrderBackwardDifference;

Timestep,4;

ConvergenceLimits,
,           !- Minimum System Timestep {minutes}
20,        !- Maximum HVAC Iterations
2,         !- Minimum Plant Iterations
8;        !- Maximum Plant Iterations

Site:Location,
DFW,       !- Name
32.9,     !- Latitude {deg}
-97.04,   !- Longitude {deg}
-6.0,     !- Time Zone {hr}
182;     !- Elevation {m}

SizingPeriod:DesignDay,
Dallas Fort Worth Intl Ap Ann Htg 99% Condns DB, !- Name
1,        !- Month
21,       !- Day of Month
WinterDesignDay, !- Day Type
-6.5,     !- Maximum Dry-Bulb Temperature {C}
0,        !- Daily Dry-Bulb Temperature Range {deltaC}
,         !- Dry-Bulb Temperature Range Modifier Type
,         !- Dry-Bulb Temperature Range Modifier

Schedule Name
WetBulb,  !- Humidity Condition Type
-6.5,    !- Wetbulb or DewPoint at Maximum Dry-Bulb
{C}
,        !- Humidity Condition Day Schedule Name
,        !- Humidity Ratio at Maximum Dry-Bulb
{kgWater/kgDryAir}
,        !- Enthalpy at Maximum Dry-Bulb {J/kg}
,        !- Daily Wet-Bulb Temperature Range {deltaC}
99158,   !- Barometric Pressure {Pa}
5.9,     !- Wind Speed {m/s}
340;    !- Wind Direction {deg}

RunPeriod,
Period,  !- Name
10,     !- Begin Month
28,     !- Begin Day of Month
10,     !- End Month

27,     !- End Day of Month
UseWeatherFile, !- Day of Week for Start Day
No,     !- Use Weather File Holidays and Special Days
Yes,    !- Use Weather File Daylight Saving Period
No,     !- Apply Weekend Holiday Rule
Yes,    !- Use Weather File Rain Indicators
Yes,    !- Use Weather File Snow Indicators
1;      !- Number of Times Runperiod to be Repeated

RunPeriodControl:SpecialDays,
New Years Day, !- Name
January 1,    !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Veterans Day, !- Name
November 11,  !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Christmas,    !- Name
December 25,  !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Independence Day, !- Name
July 4,       !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
MLK Day,      !- Name
3rd Monday in January, !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Presidents Day, !- Name
3rd Monday in February, !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Memorial Day,  !- Name
Last Monday in May, !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Labor Day,    !- Name
1st Monday in September, !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Columbus Day, !- Name
2nd Monday in October, !- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

RunPeriodControl:SpecialDays,
Thanksgiving, !- Name
4th Thursday in November,!- Start Date
1,           !- Duration {days}
Holiday;     !- Special Day Type

! Daylight Saving Period in US

RunPeriodControl:DaylightSavingTime,
2nd Sunday in March, !- Start Date
1st Sunday in November; !- End Date

Site:GroundTemperature:BuildingSurface,20.03,20.03,20.13,20.30,20
.43,20.52,20.62,20.77,20.78,20.55,20.44,20.20;

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ScheduleTypeLimits,
Any Number; !- Name

ScheduleTypeLimits,
Fraction, !- Name
0.0, !- Lower Limit Value
1.0, !- Upper Limit Value
CONTINUOUS; !- Numeric Type

ScheduleTypeLimits,
Temperature, !- Name
-60, !- Lower Limit Value
200, !- Upper Limit Value
CONTINUOUS; !- Numeric Type

ScheduleTypeLimits,
On/Off, !- Name
0, !- Lower Limit Value
1, !- Upper Limit Value
DISCRETE; !- Numeric Type

ScheduleTypeLimits,
Control Type, !- Name
0, !- Lower Limit Value
4, !- Upper Limit Value
DISCRETE; !- Numeric Type

ScheduleTypeLimits,
Humidity, !- Name
10, !- Lower Limit Value
90, !- Upper Limit Value
CONTINUOUS; !- Numeric Type

ScheduleTypeLimits,
Number; !- Name

Schedule:Compact,
Always On, !- Name
Fraction, !- Schedule Type Limits Name
Through: 12/31, !- Field 1
For: AllDays, !- Field 2
Until: 24:00, 1.0; !- Field 4

Schedule:Compact,
Always Off, !- Name
Fraction, !- Schedule Type Limits Name
Through: 12/31, !- Field 1
For: AllDays, !- Field 2
Until: 24:00, 0.0; !- Field 4

Material,
PI - Fiberglass, !- Name
MediumRough, !- Roughness
0.15342, !- Thickness {m}
0.041, !- Conductivity {W/m-K}
21.1, !- Density {kg/m3}
962.987, !- Specific Heat {J/kg-K}
0.9; !- Thermal Absorptance

Material,
PI - EPS, !- Name
MediumRough, !- Roughness
0.11989, !- Thickness {m}
0.032, !- Conductivity {W/m-K}
22, !- Density {kg/m3}
1500, !- Specific Heat {J/kg-K}
0.9; !- Thermal Absorptance

Material,
PI - XPS, !- Name
MediumRough, !- Roughness
0.13106, !- Thickness {m}
0.35, !- Conductivity {W/m-K}
29.2, !- Density {kg/m3}
1500, !- Specific Heat {J/kg-K}
0.9; !- Thermal Absorptance

Material,
PI - Rockwool, !- Name
MediumRough, !- Roughness
0.13106, !- Thickness {m}
0.041, !- Conductivity {W/m-K}
40, !- Density {kg/m3}
840, !- Specific Heat {J/kg-K}
0.9; !- Thermal Absorptance

Material,
PI - Clay tile, !- Name
MediumSmooth, !- Roughness
0.0191, !- Thickness {m}
1.6, !- Conductivity {W/m-K}
2275, !- Density {kg/m3}
852; !- Specific Heat {J/kg-K}

Material,
PI - Concrete tile, !- Name
MediumSmooth, !- Roughness
0.095, !- Thickness {m}
1.65, !- Conductivity {W/m-K}
2380, !- Density {kg/m3}
1200; !- Specific Heat {J/kg-K}

Material,
PI - Organic Felt, !- Name
MediumSmooth, !- Roughness
0.002, !- Thickness {m}
1, !- Conductivity {W/m-K}
2100, !- Density {kg/m3}
1000; !- Specific Heat {J/kg-K}

Material,
PI - Roofing Steel Panel,!- Name
MediumSmooth, !- Roughness
0.0003048, !- Thickness {m}
48, !- Conductivity {W/m-K}
7.86, !- Density {kg/m3}
453.6; !- Specific Heat {J/kg-K}

Material,
PI - Wood Flooring, !- Name
Smooth, !- Roughness
0.0159, !- Thickness {m}
0.12, !- Conductivity {W/m-K}
544, !- Density {kg/m3}
1210; !- Specific Heat {J/kg-K}

Material,
PI - Bamboo Flooring, !- Name
Smooth, !- Roughness
0.0191, !- Thickness {m}
0.188406, !- Conductivity {W/m-K}
850, !- Density {kg/m3}
1771; !- Specific Heat {J/kg-K}

Material,
PI - 30 Mil Mtl Stud 16 oc type C, !- Name
Smooth, !- Roughness
0.092075, !- Thickness {m}
45.28756, !- Conductivity {W/m-K}
7848.82, !- Density {kg/m3}
502.428, !- Specific Heat {J/kg-K}
0.9, !- Thermal Absorptance
0.7, !- Solar Absorptance
0.7; !- Visible Absorptance

Material,
PI - 3 5/8" Full Batt Insulation - Fiberglass, !- Name
MediumRough, !- Roughness
0.09275, !- Thickness {m}
0.04615292, !- Conductivity {W/m-K}
84.8954, !- Density {kg/m3}
962.987, !- Specific Heat {J/kg-K}
0.9; !- Thermal Absorptance

Material,

PI - 5/8" Thk Gyp Bd, !- Name 502.428, !- Specific Heat {J/kg-K}
 MediumSmooth, !- Roughness 0.9, !- Thermal Absorptance
 0.015875, !- Thickness {m} 0.7, !- Solar Absorptance
 0.16009296, !- Conductivity {W/m-K} 0.7; !- Visible Absorptance
 800.9, !- Density {kg/m3}
 1088.594, !- Specific Heat {J/kg-K}
 0.9; !- Thermal Absorptance

Material,
 PI - 30 Mil Mtl Stud 16 oc type D, !- Name
 Smooth, !- Roughness
 0.1524, !- Thickness {m}
 45.28756, !- Conductivity {W/m-K}
 7848.82, !- Density {kg/m3}
 502.428, !- Specific Heat {J/kg-K}
 0.9, !- Thermal Absorptance
 0.7, !- Solar Absorptance
 0.7; !- Visible Absorptance

Material,
 PI - 6" Full Batt Insulation - Fiberglass , !- Name
 Smooth, !- Roughness
 0.1524, !- Thickness {m}
 0.04615292, !- Conductivity {W/m-K}
 84.8954, !- Density {kg/m3}
 962.987; !- Specific Heat {J/kg-K}

Material,
 PI - Masonry Brick, !- Name
 MediumRough, !- Roughness
 0.0762, !- Thickness {m}
 0.865367334, !- Conductivity {W/m-K}
 1922.16, !- Density {kg/m3}
 785.511; !- Specific Heat {J/kg-K}

Material,
 PI - 1/2" thk Sheating OSB, !- Name
 Smooth, !- Roughness
 0.0127, !- Thickness {m}
 0.12, !- Conductivity {W/m-K}
 660, !- Density {kg/m3}
 1300; !- Specific Heat {J/kg-K}

Material,
 PI - 43 Mil Mtl Stud 16 oc , !- Name
 Smooth, !- Roughness
 0.1524, !- Thickness {m}
 45.28756, !- Conductivity {W/m-K}
 7848.82, !- Density {kg/m3}
 502.428, !- Specific Heat {J/kg-K}
 0.9, !- Thermal Absorptance
 0.7, !- Solar Absorptance
 0.7; !- Visible Absorptance

Material,
 PI - SIP OSB 7/16", !- Name
 MediumSmooth, !- Roughness
 0.0111125, !- Thickness {m}
 0.12, !- Conductivity {W/m-K}
 660, !- Density {kg/m3}
 1500, !- Specific Heat {J/kg-K}
 , !- Thermal Absorptance
 0.6; !- Solar Absorptance

Material,
 PI - SIP Core-Expanded Polystyrene, !- Name
 MediumRough, !- Roughness
 0.079375, !- Thickness {m}
 0.037, !- Conductivity {W/m-K}
 22, !- Density {kg/m3}
 1300; !- Specific Heat {J/kg-K}

Material,
 PI - SIP 30 Mil Mtl Stud 16 oc, !- Name
 Smooth, !- Roughness
 0.041275, !- Thickness {m}
 45.28756, !- Conductivity {W/m-K}
 7848.82, !- Density {kg/m3}

Material,
 PI - Metal surface, !- Name
 Smooth, !- Roughness
 0.0008, !- Thickness {m}
 45.28, !- Conductivity {W/m-K}
 7824, !- Density {kg/m3}
 500; !- Specific Heat {J/kg-K}

Material,
 M11 100mm lightweight concrete, !- Name
 MediumRough, !- Roughness
 0.1016, !- Thickness {m}
 0.53, !- Conductivity {W/m-K}
 1280, !- Density {kg/m3}
 840; !- Specific Heat {J/kg-K}

Material,
 F16 Acoustic tile, !- Name
 MediumSmooth, !- Roughness
 0.0191, !- Thickness {m}
 0.06, !- Conductivity {W/m-K}
 368, !- Density {kg/m3}
 590; !- Specific Heat {J/kg-K}

Material,
 M01 100mm brick, !- Name
 MediumRough, !- Roughness
 0.1016, !- Thickness {m}
 0.89, !- Conductivity {W/m-K}
 1920, !- Density {kg/m3}
 790; !- Specific Heat {J/kg-K}

Material,
 M15 200mm heavyweight concrete, !- Name
 MediumRough, !- Roughness
 0.2032, !- Thickness {m}
 1.95, !- Conductivity {W/m-K}
 2240, !- Density {kg/m3}
 900; !- Specific Heat {J/kg-K}

Material,
 M05 200mm concrete block, !- Name
 MediumRough, !- Roughness
 0.2032, !- Thickness {m}
 1.11, !- Conductivity {W/m-K}
 800, !- Density {kg/m3}
 920; !- Specific Heat {J/kg-K}

Material,
 G05 25mm wood, !- Name
 MediumSmooth, !- Roughness
 0.0254, !- Thickness {m}
 0.15, !- Conductivity {W/m-K}
 608, !- Density {kg/m3}
 1630; !- Specific Heat {J/kg-K}

Material,
 CONCRETE - DRIED SAND AND GRAVEL 4 IN, !- Name
 MediumRough, !- Roughness
 0.1000000, !- Thickness {m}
 1.290000, !- Conductivity {W/m-K}
 2242.580, !- Density {kg/m3}
 830.00000, !- Specific Heat {J/kg-K}
 0.9000000, !- Thermal Absorptance
 0.6000000, !- Solar Absorptance
 0.6000000; !- Visible Absorptance

Material,
 INS - EXPANDED EXT POLYSTYRENE R12 2 IN, !- Name
 Rough, !- Roughness
 5.0000001E-02, !- Thickness {m}
 2.0000000E-02, !- Conductivity {W/m-K}
 56.06000, !- Density {kg/m3}
 1210.000, !- Specific Heat {J/kg-K}

0.9000000, !- Thermal Absorptance
 0.5000000, !- Solar Absorptance
 0.5000000; !- Visible Absorptance

Material,
 G01 16mm gypsum board, !- Name
 MediumSmooth, !- Roughness
 0.0159, !- Thickness {m}
 0.16, !- Conductivity {W/m-K}
 800, !- Density {kg/m3}
 1090; !- Specific Heat {J/kg-K}

Material,
 I06 244mm batt insulation, !- Name
 VeryRough, !- Roughness
 0.2438, !- Thickness {m}
 0.05, !- Conductivity {W/m-K}
 19, !- Density {kg/m3}
 960; !- Specific Heat {J/kg-K}

Material,
 Sheathing - regular density - 12.7mm, !- Name
 Smooth, !- Roughness
 0.0127, !- Thickness {m}
 0.055, !- Conductivity {W/m-K}
 290, !- Density {kg/m3}
 1300; !- Specific Heat {J/kg-K}

Material,
 F10 25mm stone, !- Name
 MediumRough, !- Roughness
 0.0254, !- Thickness {m}
 3.17, !- Conductivity {W/m-K}
 2560, !- Density {kg/m3}
 790; !- Specific Heat {J/kg-K}

Material,
 I01 25mm insulation board, !- Name
 MediumRough, !- Roughness
 0.0254, !- Thickness {m}
 0.03, !- Conductivity {W/m-K}
 43, !- Density {kg/m3}
 1210; !- Specific Heat {J/kg-K}

Material,
 I02 50mm insulation board, !- Name
 MediumRough, !- Roughness
 0.0508, !- Thickness {m}
 0.03, !- Conductivity {W/m-K}
 43, !- Density {kg/m3}
 1210; !- Specific Heat {J/kg-K}

Material,
 G01a 19mm gypsum board, !- Name
 MediumSmooth, !- Roughness
 0.019, !- Thickness {m}
 0.16, !- Conductivity {W/m-K}
 800, !- Density {kg/m3}
 1090; !- Specific Heat {J/kg-K}

Material,
 G02 16mm plywood, !- Name
 Smooth, !- Roughness
 0.0159, !- Thickness {m}
 0.12, !- Conductivity {W/m-K}
 544, !- Density {kg/m3}
 1210; !- Specific Heat {J/kg-K}

Material,
 Radiant Floor 3rd Layer, !- Name
 MediumRough, !- Roughness
 0.0635, !- Thickness {m}
 1.290000, !- Conductivity {W/m-K}
 2242.580, !- Density {kg/m3}
 830.00000, !- Specific Heat {J/kg-K}
 0.9000000, !- Thermal Absorptance
 0.6000000, !- Solar Absorptance

0.6000000; !- Visible Absorptance

Material,
 Radiant Floor 4th Layer, !- Name
 MediumRough, !- Roughness
 0.0635, !- Thickness {m}
 1.290000, !- Conductivity {W/m-K}
 2242.580, !- Density {kg/m3}
 830.00000, !- Specific Heat {J/kg-K}
 0.9000000, !- Thermal Absorptance
 0.6000000, !- Solar Absorptance
 0.6000000; !- Visible Absorptance

Material,
 Radiant Floor Outside Layer, !- Name
 MediumRough, !- Roughness
 0.025, !- Thickness {m}
 1.290000, !- Conductivity {W/m-K}
 2242.580, !- Density {kg/m3}
 830.00000, !- Specific Heat {J/kg-K}
 0.9000000, !- Thermal Absorptance
 0.6000000, !- Solar Absorptance
 0.6000000; !- Visible Absorptance

Material:AirGap,
 F04 Wall air space resistance, !- Name
 0.15; !- Thermal Resistance {m2-K/W}

Material:AirGap,
 F05 Ceiling air space resistance, !- Name
 0.18; !- Thermal Resistance {m2-K/W}

WindowMaterial:Glazing,
 PYR B CLEAR 3MM, !- Name
 SpectralAverage, !- Optical Data Type
 , !- Window Glass Spectral Data Set Name
 0.003, !- Thickness {m}
 0.06, !- Solar Transmittance at Normal Incidence
 0.090, !- Front Side Solar Reflectance at Normal Incidence
 0.100, !- Back Side Solar Reflectance at Normal Incidence
 0.820, !- Visible Transmittance at Normal Incidence
 0.110, !- Front Side Visible Reflectance at Normal Incidence
 0.120, !- Back Side Visible Reflectance at Normal Incidence
 0.0, !- Infrared Transmittance at Normal Incidence
 0.84, !- Front Side Infrared Hemispherical Emissivity
 0.20, !- Back Side Infrared Hemispherical Emissivity
 0.9; !- Conductivity {W/m-K}

WindowMaterial:Gas,
 ARGON 13MM, !- Name
 Argon, !- Gas Type
 0.0127; !- Thickness {m}

Construction,
 PI - Floor Wood, !- Name
 PI - Wood Flooring, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 M11 100mm lightweight concrete; !- Layer 3

Construction,
 PI - Floor Bamboo, !- Name
 PI - Bamboo Flooring, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 M11 100mm lightweight concrete; !- Layer 3

Construction,
 Exterior Wall, !- Name
 M01 100mm brick, !- Outside Layer
 M15 200mm heavyweight concrete, !- Layer 2
 I02 50mm insulation board, !- Layer 3
 F04 Wall air space resistance, !- Layer 4
 G01a 19mm gypsum board; !- Layer 5

Construction,
 PI - Masonry Wall EPS, !- Name

PI - Masonry Brick, !- Outside Layer
 PI - 1/2" thk Sheating OSB, !- Layer 2
 F04 Wall air space resistance, !- Layer 3
 PI - EPS, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction,
 PI - Masonry Wall XPS, !- Name
 PI - Masonry Brick, !- Outside Layer
 PI - 1/2" thk Sheating OSB, !- Layer 2
 F04 Wall air space resistance, !- Layer 3
 PI - XPS, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction,
 PI - Masonry Wall Rockwool, !- Name
 PI - Masonry Brick, !- Outside Layer
 PI - 1/2" thk Sheating OSB, !- Layer 2
 F04 Wall air space resistance, !- Layer 3
 PI - Rockwool, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction,
 PI - Masonry Wall FG, !- Name
 PI - Masonry Brick, !- Outside Layer
 PI - 1/2" thk Sheating OSB, !- Layer 2
 F04 Wall air space resistance, !- Layer 3
 PI - Fiberglass, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction,
 PI - Roof Clay Tiles, !- Name
 M11 100mm lightweight concrete, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 PI - Clay tile; !- Layer 3

Construction,
 PI - Roof Concrete Tiles, !- Name
 M11 100mm lightweight concrete, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 PI - Concrete tile; !- Layer 3

Construction,
 PI - Roof Organic Felt, !- Name
 M11 100mm lightweight concrete, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 PI - Organic Felt; !- Layer 3

Construction,
 PI - Roof Steel Panel, !- Name
 M11 100mm lightweight concrete, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 PI - Roofing Steel Panel; !- Layer 3

Construction,
 Exterior Floor, !- Name
 I02 50mm insulation board, !- Outside Layer
 M15 200mm heavyweight concrete; !- Layer 2

Construction,
 Interior Floor, !- Name
 F16 Acoustic tile, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 M11 100mm lightweight concrete; !- Layer 3

Construction,
 Interior Wall, !- Name
 G01a 19mm gypsum board, !- Outside Layer
 F04 Wall air space resistance, !- Layer 2
 G01a 19mm gypsum board; !- Layer 3

Construction,
 Exterior Roof, !- Name
 M11 100mm lightweight concrete, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 F16 Acoustic tile; !- Layer 3

Construction,
 Interior Ceiling, !- Name
 M11 100mm lightweight concrete, !- Outside Layer
 F05 Ceiling air space resistance, !- Layer 2
 F16 Acoustic tile; !- Layer 3

Construction,
 Exterior Window, !- Name
 PYR B CLEAR 3MM, !- Outside Layer
 ARGON 13MM, !- Layer 2
 PYR B CLEAR 3MM; !- Layer 3

Construction,
 Exterior Door, !- Name
 PI - Metal surface, !- Outside Layer
 I01 25mm insulation board; !- Layer 2

Construction,
 Interior Door, !- Name
 G05 25mm wood; !- Outside Layer

Construction,
 PI - Partition Wall Type C, !- Name
 PI - 5/8" Thk Gyp Bd, !- Outside Layer
 PI - 3 5/8" Full Batt Insulation - Fiberglass, !- Layer 2
 PI - 5/8" Thk Gyp Bd; !- Layer 3

Construction,
 PI - Partition Wall type D, !- Name
 PI - 5/8" Thk Gyp Bd, !- Outside Layer
 PI - 6" Full Batt Insulation - Fiberglass, !- Layer 2
 PI - 5/8" Thk Gyp Bd; !- Layer 3

Construction,
 PI - Masonry Wall, !- Name
 PI - Masonry Brick, !- Outside Layer
 PI - 1/2" thk Sheating OSB, !- Layer 2
 F04 Wall air space resistance, !- Layer 3
 PI - 6" Full Batt Insulation - Fiberglass, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction,
 PI - Metal Panel Wall, !- Name
 PI - Metal surface, !- Outside Layer
 PI - 1/2" thk Sheating OSB, !- Layer 2
 F04 Wall air space resistance, !- Layer 3
 PI - 3 5/8" Full Batt Insulation - Fiberglass, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction,
 PI - SIP Wall, !- Name
 PI - SIP OSB 7/16", !- Outside Layer
 PI - SIP Core-Expanded Polystyrene, !- Layer 2
 PI - SIP OSB 7/16", !- Layer 3
 F04 Wall air space resistance, !- Layer 4
 PI - 5/8" Thk Gyp Bd; !- Layer 5

Construction:InternalSource,
 Slab Floor with Radiant, !- Name
 2, !- Source Present After Layer Number
 2, !- Temperature Calculation Requested After Layer Number
 1, !- Dimensions for the CTF Calculation
 0.1524, !- Tube Spacing {m}
 Radiant Floor Outside Layer, !- Outside Layer
 INS - EXPANDED EXT POLYSTYRENE R12 2 IN, !- Layer 2
 Radiant Floor 3rd Layer, !- Layer 3
 Radiant Floor 4th Layer; !- Layer 4

GlobalGeometryRules,
 UpperLeftCorner, !- Starting Vertex Position
 Counterclockwise, !- Vertex Entry Direction
 Relative; !- Coordinate System

Zone,
 Conditioned, !- Name
 0.0, !- Direction of Relative North {deg}
 1.940596, 0.24045, 0.0, !- X,Y,Z {m}
 , !- Type
 1; !- Multiplier

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Zone,
MechanicalRoom,      !- Name
0.0,                 !- Direction of Relative North {deg}
6.001068, 1.795088, 0.0,      !- X,Y,Z {m}
,                   !- Type
1;                   !- Multiplier

Zone,
ElecRoom,            !- Name
0.0,                 !- Direction of Relative North {deg}
15.218588, 4.081086, 0.0,     !- X,Y,Z {m}
,                   !- Type
1;                   !- Multiplier

BuildingSurface:Detailed,
ElecFloor,           !- Name
Floor,               !- Surface Type
Exterior Floor,      !- Construction Name
ElecRoom,            !- Zone Name
Ground,              !- Outside Boundary Condition
,                   !- Outside Boundary Condition Object
NoSun,               !- Sun Exposure
NoWind,              !- Wind Exposure
0.0,                 !- View Factor to Ground
4,                   !- Number of Vertices
-1.028588000000, 2.098914000000, 0.000000000000,
!- X,Y,Z 1 {m}
-1.028588000000, -2.441086000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.688588000000, -2.441086000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.688588000000, 2.098914000000, 0.000000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
ElecNorthEX,         !- Name
Wall,                !- Surface Type
$ExteriorWallOption_02, !- Construction Name
ElecRoom,            !- Zone Name
Outdoors,            !- Outside Boundary Condition
,                   !- Outside Boundary Condition Object
SunExposed,          !- Sun Exposure
WindExposed,         !- Wind Exposure
,                   !- View Factor to Ground
4,                   !- Number of Vertices
-1.028588000000, 2.098914000000, 2.640000000000,
!- X,Y,Z 1 {m}
-1.028588000000, 2.098914000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.688588000000, 2.098914000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.688588000000, 2.098914000000, 2.640000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
ElecRoomInterzonetoMain, !- Name
Wall,                !- Surface Type
$InteriorWallOption_01, !- Construction Name
ElecRoom,            !- Zone Name
Surface,             !- Outside Boundary Condition
InterzonewallToElecRoom, !- Outside Boundary Condition Object
NoSun,               !- Sun Exposure
NoWind,              !- Wind Exposure
0.0,                 !- View Factor to Ground
4,                   !- Number of Vertices
-1.688588000000, 2.098914000000, 2.640000000000,
!- X,Y,Z 1 {m}
-1.688588000000, 2.098914000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.688588000000, -2.441086000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.688588000000, -2.441086000000, 2.640000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
ElecSouthEx,         !- Name
Wall,                !- Surface Type
$ExteriorWallOption_02, !- Construction Name
ElecRoom,            !- Zone Name
Outdoors,            !- Outside Boundary Condition
,                   !- Outside Boundary Condition Object
SunExposed,          !- Sun Exposure
WindExposed,         !- Wind Exposure
,                   !- View Factor to Ground
4,                   !- Number of Vertices
-1.688588000000, -2.441086000000, 2.640000000000,
!- X,Y,Z 1 {m}
-1.028588000000, -2.441086000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.028588000000, 2.098914000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.028588000000, 2.098914000000, 2.640000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
ElecWestEx,          !- Name
Wall,                !- Surface Type
$ExteriorWallOption_02, !- Construction Name
ElecRoom,            !- Zone Name
Outdoors,            !- Outside Boundary Condition
,                   !- Outside Boundary Condition Object
SunExposed,          !- Sun Exposure
WindExposed,         !- Wind Exposure
,                   !- View Factor to Ground
4,                   !- Number of Vertices
-1.028588000000, -2.441086000000, 2.640000000000,
!- X,Y,Z 1 {m}
-1.028588000000, -2.441086000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.028588000000, 2.098914000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.028588000000, 2.098914000000, 2.640000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
ElecRoofEx,          !- Name
Roof,               !- Surface Type
$RoofingOption_01,  !- Construction Name
ElecRoom,            !- Zone Name
Outdoors,            !- Outside Boundary Condition
,                   !- Outside Boundary Condition Object
SunExposed,          !- Sun Exposure
WindExposed,         !- Wind Exposure
,                   !- View Factor to Ground
4,                   !- Number of Vertices
-1.688588000000, 2.098914000000, 2.640000000000,
!- X,Y,Z 1 {m}
-1.688588000000, -2.441086000000, 2.640000000000,
!- X,Y,Z 2 {m}
-1.028588000000, -2.441086000000, 2.640000000000,
!- X,Y,Z 3 {m}
-1.028588000000, 2.098914000000, 2.640000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
InterMechtoMain,     !- Name
Wall,                !- Surface Type
$InteriorWallOption_01, !- Construction Name
MechanicalRoom,      !- Zone Name
Surface,             !- Outside Boundary Condition
InterMaintoMech,     !- Outside Boundary Condition Object
NoSun,               !- Sun Exposure
NoWind,              !- Wind Exposure
0.0,                 !- View Factor to Ground
7,                   !- Number of Vertices
-0.451068000000, -0.685088000000, 3.743657289003,
!- X,Y,Z 1 {m}
-0.451068000000, -0.685088000000, 0.000000000000,
!- X,Y,Z 2 {m}
-0.451068000000, 3.964912000000, 0.000000000000,
!- X,Y,Z 3 {m}
-0.451068000000, 3.964912000000, 2.440000000000,
!- X,Y,Z 4 {m}
-0.451068000000, 6.024912000000, 2.440000000000,
!- X,Y,Z 5 {m}
-0.451068000000, 6.024912000000, 4.090000000000,
!- X,Y,Z 6 {m}

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                !- X,Y,Z 6 {m}
-0.451068000000, 2.114912000000, 2.870000000000;
                !- X,Y,Z 7 {m}

BuildingSurface:Detailed,
MechWestExWall, !- Name
Wall, !- Surface Type
$ExteriorWallOption_03, !- Construction Name
MechanicalRoom, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
7, !- Number of Vertices
-2.551068000000, 6.534912000000, 6.910000000000,
!- X,Y,Z 1 {m}
-2.551068000000, 6.534912000000, 2.440000000000,
!- X,Y,Z 2 {m}
-2.551068000000, 6.024912000000, 2.440000000000,
!- X,Y,Z 3 {m}
-2.551068000000, 6.024912000000, 4.090000000000,
!- X,Y,Z 4 {m}
-2.551068000000, 2.114912000000, 2.870000000000,
!- X,Y,Z 5 {m}
-2.551068000000, -0.685088000000, 3.743657289003,
!- X,Y,Z 6 {m}
-2.551068000000, -0.685088000000, 6.910000000000;
!- X,Y,Z 7 {m}

BuildingSurface:Detailed,
InterChimneytoMech, !- Name
Wall, !- Surface Type
$InteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Surface, !- Outside Boundary Condition
InterMechtoChimney, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
6, !- Number of Vertices
1.509404000000, 0.869550000000, 6.910000000000,
!- X,Y,Z 1 {m}
1.509404000000, 0.869550000000, 2.440000000000,
!- X,Y,Z 2 {m}
2.699404000000, 0.869550000000, 2.440000000000,
!- X,Y,Z 3 {m}
2.699404000000, 0.869550000000, 0.000000000000,
!- X,Y,Z 4 {m}
3.609404000000, 0.869550000000, 0.000000000000,
!- X,Y,Z 5 {m}
3.609404000000, 0.869550000000, 6.910000000000;
!- X,Y,Z 6 {m}

BuildingSurface:Detailed,
Living left side wall, !- Name
Wall, !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
5, !- Number of Vertices
-1.940596000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 1 {m}
-1.940596000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.940596000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.940596000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 4 {m}
-1.940596000000, 3.669550000000, 2.870000000000;
!- X,Y,Z 5 {m}

BuildingSurface:Detailed,
D502FE, !- Name

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Wall, !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
3.609404000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 1 {m}
3.609404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 2 {m}
11.589404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 3 {m}
11.589404000000, 7.579550000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
NorthMasonryToiletWall, !- Name
Wall, !- Surface Type
$ExteriorWallOption_03, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
3.609404000000, 8.089550000000, 2.440000000000,
!- X,Y,Z 1 {m}
3.609404000000, 8.089550000000, 0.000000000000,
!- X,Y,Z 2 {m}
1.509404000000, 8.089550000000, 0.000000000000,
!- X,Y,Z 3 {m}
1.509404000000, 8.089550000000, 2.440000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
PartitionToilet, !- Name
Wall, !- Surface Type
$ExteriorWallOption_03, !- Construction Name
Conditioned, !- Zone Name
Adiabatic, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
4, !- Number of Vertices
3.609404000000, 5.519550000000, 2.440000000000,
!- X,Y,Z 1 {m}
3.609404000000, 5.519550000000, 0.000000000000,
!- X,Y,Z 2 {m}
3.609404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 3 {m}
3.609404000000, 7.579550000000, 2.440000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
ceilingtoMechRoom, !- Name
Ceiling, !- Surface Type
Interior Ceiling, !- Construction Name
Conditioned, !- Zone Name
Surface, !- Outside Boundary Condition
MechInterfloortoLiving, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
6, !- Number of Vertices
1.509404000000, 8.089550000000, 2.440000000000,
!- X,Y,Z 1 {m}
1.509404000000, 0.869550000000, 2.440000000000,
!- X,Y,Z 2 {m}
2.699404000000, 0.869550000000, 2.440000000000,
!- X,Y,Z 3 {m}
2.699404000000, 5.519550000000, 2.440000000000,
!- X,Y,Z 4 {m}
3.609404000000, 5.519550000000, 2.440000000000,

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```

!- X,Y,Z 5 {m}
3.609404000000, 8.089550000000, 2.440000000000;
!- X,Y,Z 6 {m}
BuildingSurface:Detailed,
InterKitchentoMech, !- Name
Wall, !- Surface Type
$InteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Surface, !- Outside Boundary Condition
InterMechtoKitchen, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
4, !- Number of Vertices
2.699404000000, 0.869550000000, 2.440000000000,
!- X,Y,Z 1 {m}
2.699404000000, 0.869550000000, 0.000000000000,
!- X,Y,Z 2 {m}
2.699404000000, 5.519550000000, 0.000000000000,
!- X,Y,Z 3 {m}
2.699404000000, 5.519550000000, 2.440000000000;
!- X,Y,Z 4 {m}

```

```

BuildingSurface:Detailed,
InterRestoMech, !- Name
Wall, !- Surface Type
$InteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Surface, !- Outside Boundary Condition
InterMechtoRest, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
4, !- Number of Vertices
2.699404000000, 5.519550000000, 2.440000000000,
!- X,Y,Z 1 {m}
2.699404000000, 5.519550000000, 0.000000000000,
!- X,Y,Z 2 {m}
3.609404000000, 5.519550000000, 0.000000000000,
!- X,Y,Z 3 {m}
3.609404000000, 5.519550000000, 2.440000000000;
!- X,Y,Z 4 {m}

```

```

BuildingSurface:Detailed,
WestMasonryToiletWall, !- Name
Wall, !- Surface Type
$ExteriorWallOption_03, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
1.509404000000, 0.809550000000, 2.440000000000,
!- X,Y,Z 1 {m}
1.509404000000, 0.809550000000, 0.000000000000,
!- X,Y,Z 2 {m}
1.509404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 3 {m}
1.509404000000, 7.579550000000, 2.440000000000;
!- X,Y,Z 4 {m}

```

```

BuildingSurface:Detailed,
EastChimneyWall, !- Name
Wall, !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
6, !- Number of Vertices
3.609404000000, 0.869550000000, 6.910000000000,
!- X,Y,Z 1 {m}
3.609404000000, 0.869550000000, 3.743657289003,

```

```

!- X,Y,Z 2 {m}
3.609404000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 3 {m}
3.609404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 4 {m}
3.609404000000, -0.750450000000, 0.000000000000,
!- X,Y,Z 5 {m}
3.609404000000, -0.750450000000, 6.910000000000;
!- X,Y,Z 6 {m}

```

```

BuildingSurface:Detailed,
SouthChimneyWall, !- Name
Wall, !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
3.609404000000, -0.750450000000, 6.910000000000,
!- X,Y,Z 1 {m}
3.609404000000, -0.750450000000, 0.000000000000,
!- X,Y,Z 2 {m}
1.509404000000, -0.750450000000, 0.000000000000,
!- X,Y,Z 3 {m}
1.509404000000, -0.750450000000, 6.910000000000;
!- X,Y,Z 4 {m}

```

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BuildingSurface:Detailed,
ChimneyRoof, !- Name
Roof, !- Surface Type
$RoofingOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
0.0, !- View Factor to Ground
4, !- Number of Vertices
1.509404000000, 0.869550000000, 6.910000000000,
!- X,Y,Z 1 {m}
1.509404000000, -0.750450000000, 6.910000000000,
!- X,Y,Z 2 {m}
3.609404000000, -0.750450000000, 6.910000000000,
!- X,Y,Z 3 {m}
3.609404000000, 0.869550000000, 6.910000000000;
!- X,Y,Z 4 {m}

```

```

BuildingSurface:Detailed,
InterLivingtoMech, !- Name
Wall, !- Surface Type
$InteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Surface, !- Outside Boundary Condition
InterMechtoLiving, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
5, !- Number of Vertices
1.509404000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 1 {m}
1.509404000000, 7.579550000000, 2.440000000000,
!- X,Y,Z 2 {m}
1.509404000000, 0.869550000000, 2.440000000000,
!- X,Y,Z 3 {m}
1.509404000000, 0.869550000000, 3.743657289003,
!- X,Y,Z 4 {m}
1.509404000000, 3.669550000000, 2.870000000000;
!- X,Y,Z 5 {m}

```

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BuildingSurface:Detailed,
SouthWindowFlameWallleft, !- Name
Wall, !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition

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, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
1.509404000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 1 {m}
1.509404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.940596000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.940596000000, -0.240450000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
NorthWindowFlameWallRight, !- Name
Wall, !- Surface Type
\$ExteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
-1.940596000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 1 {m}
-1.940596000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 2 {m}
1.509404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 3 {m}
1.509404000000, 7.579550000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
NorthWestRoof, !- Name
Roof, !- Surface Type
\$RoofingOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
-1.940596000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 1 {m}
-1.940596000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 2 {m}
1.509404000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 3 {m}
1.509404000000, 7.579550000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
SouthWestRoof, !- Name
Roof, !- Surface Type
\$RoofingOption_01, !- Construction Name
Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
4, !- Number of Vertices
1.509404000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 1 {m}
1.509404000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 2 {m}
-1.940596000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 3 {m}
-1.940596000000, -0.240450000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
WestChimneyWall, !- Name
Wall, !- Surface Type
\$ExteriorWallOption_01, !- Construction Name

Conditioned, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
6, !- Number of Vertices
1.509404000000, -0.750450000000, 6.910000000000,
!- X,Y,Z 1 {m}
1.509404000000, -0.750450000000, 0.000000000000,
!- X,Y,Z 2 {m}
1.509404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 3 {m}
1.509404000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 4 {m}
1.509404000000, 0.869550000000, 3.743657289003,
!- X,Y,Z 5 {m}
1.509404000000, 0.869550000000, 6.910000000000;
!- X,Y,Z 6 {m}

BuildingSurface:Detailed,
MechFloorEx, !- Name
Floor, !- Surface Type
Exterior Floor, !- Construction Name
MechanicalRoom, !- Zone Name
Ground, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
4, !- Number of Vertices
-0.451068000000, 3.964912000000, 0.000000000000,
!- X,Y,Z 1 {m}
-0.451068000000, -0.685088000000, 0.000000000000,
!- X,Y,Z 2 {m}
-1.361068000000, -0.685088000000, 0.000000000000,
!- X,Y,Z 3 {m}
-1.361068000000, 3.964912000000, 0.000000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
InterMechtoChimney, !- Name
Wall, !- Surface Type
\$InteriorWallOption_01, !- Construction Name
MechanicalRoom, !- Zone Name
Surface, !- Outside Boundary Condition
InterChimneytoMech, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
6, !- Number of Vertices
-2.551068000000, -0.685088000000, 6.910000000000,
!- X,Y,Z 1 {m}
-2.551068000000, -0.685088000000, 2.440000000000,
!- X,Y,Z 2 {m}
-1.361068000000, -0.685088000000, 2.440000000000,
!- X,Y,Z 3 {m}
-1.361068000000, -0.685088000000, 0.000000000000,
!- X,Y,Z 4 {m}
-0.451068000000, -0.685088000000, 0.000000000000,
!- X,Y,Z 5 {m}
-0.451068000000, -0.685088000000, 6.910000000000;
!- X,Y,Z 6 {m}

BuildingSurface:Detailed,
MechEastEx, !- Name
Wall, !- Surface Type
\$ExteriorWallOption_03, !- Construction Name
MechanicalRoom, !- Zone Name
Outdoors, !- Outside Boundary Condition
, !- Outside Boundary Condition Object
SunExposed, !- Sun Exposure
WindExposed, !- Wind Exposure
, !- View Factor to Ground
7, !- Number of Vertices
-0.451068000000, -0.685088000000, 6.910000000000,
!- X,Y,Z 1 {m}

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-0.451068000000, -0.685088000000, 3.743657289003,
    !- X,Y,Z 2 {m}
-0.451068000000, 2.114912000000, 2.870000000000,
    !- X,Y,Z 3 {m}
-0.451068000000, 6.024912000000, 4.090000000000,
    !- X,Y,Z 4 {m}
-0.451068000000, 6.024912000000, 2.440000000000,
    !- X,Y,Z 5 {m}
-0.451068000000, 6.534912000000, 2.440000000000,
    !- X,Y,Z 6 {m}
-0.451068000000, 6.534912000000, 6.910000000000;
    !- X,Y,Z 7 {m}

BuildingSurface:Detailed,
MechNorthEx,    !- Name
Wall,           !- Surface Type
$ExteriorWallOption_03, !- Construction Name
MechanicalRoom, !- Zone Name
Outdoors,      !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
SunExposed,    !- Sun Exposure
WindExposed,   !- Wind Exposure
,              !- View Factor to Ground
4,             !- Number of Vertices
-0.451068000000, 6.534912000000, 6.910000000000,
    !- X,Y,Z 1 {m}
-0.451068000000, 6.534912000000, 2.440000000000,
    !- X,Y,Z 2 {m}
-2.551068000000, 6.534912000000, 2.440000000000,
    !- X,Y,Z 3 {m}
-2.551068000000, 6.534912000000, 6.910000000000;
    !- X,Y,Z 4 {m}

BuildingSurface:Detailed,
InterMechtoLiving, !- Name
Wall,              !- Surface Type
$InteriorWallOption_01, !- Construction Name
MechanicalRoom,   !- Zone Name
Surface,          !- Outside Boundary Condition
InterLivingtoMech, !- Outside Boundary Condition Object
NoSun,            !- Sun Exposure
NoWind,           !- Wind Exposure
0.0,              !- View Factor to Ground
5,                !- Number of Vertices
-2.551068000000, 6.024912000000, 4.090000000000,
    !- X,Y,Z 1 {m}
-2.551068000000, 6.024912000000, 2.440000000000,
    !- X,Y,Z 2 {m}
-2.551068000000, -0.685088000000, 2.440000000000,
    !- X,Y,Z 3 {m}
-2.551068000000, -0.685088000000, 3.743657289003,
    !- X,Y,Z 4 {m}
-2.551068000000, 2.114912000000, 2.870000000000;
    !- X,Y,Z 5 {m}

BuildingSurface:Detailed,
InterMechtoKitchen, !- Name
Wall,                !- Surface Type
$InteriorWallOption_01, !- Construction Name
MechanicalRoom,     !- Zone Name
Surface,            !- Outside Boundary Condition
InterKitchentoMech, !- Outside Boundary Condition Object
NoSun,              !- Sun Exposure
NoWind,             !- Wind Exposure
0.0,                !- View Factor to Ground
4,                  !- Number of Vertices
-1.361068000000, 3.964912000000, 2.440000000000,
    !- X,Y,Z 1 {m}
-1.361068000000, 3.964912000000, 0.000000000000,
    !- X,Y,Z 2 {m}
-1.361068000000, -0.685088000000, 0.000000000000,
    !- X,Y,Z 3 {m}
-1.361068000000, -0.685088000000, 2.440000000000;
    !- X,Y,Z 4 {m}

BuildingSurface:Detailed,
MechInterfloortoLiving, !- Name
Ceiling,                !- Surface Type
Interior Ceiling,       !- Construction Name
MechanicalRoom,        !- Zone Name
Surface,                !- Outside Boundary Condition
ceilingtoMechRoom,    !- Outside Boundary Condition Object
NoSun,                  !- Sun Exposure
NoWind,                 !- Wind Exposure
0.0,                    !- View Factor to Ground
6,                       !- Number of Vertices
-0.451068000000, 6.534912000000, 2.440000000000,
    !- X,Y,Z 1 {m}
-0.451068000000, 3.964912000000, 2.440000000000,
    !- X,Y,Z 2 {m}
-1.361068000000, 3.964912000000, 2.440000000000,
    !- X,Y,Z 3 {m}
-1.361068000000, -0.685088000000, 2.440000000000,
    !- X,Y,Z 4 {m}
-2.551068000000, -0.685088000000, 2.440000000000,
    !- X,Y,Z 5 {m}
-2.551068000000, 6.534912000000, 2.440000000000;
    !- X,Y,Z 6 {m}

BuildingSurface:Detailed,
InterMechtoRest, !- Name
Wall,            !- Surface Type
$InteriorWallOption_01, !- Construction Name
MechanicalRoom, !- Zone Name
Surface,         !- Outside Boundary Condition
InterResttoMech, !- Outside Boundary Condition Object
NoSun,          !- Sun Exposure
NoWind,         !- Wind Exposure
0.0,            !- View Factor to Ground
4,              !- Number of Vertices
-0.451068000000, 3.964912000000, 2.440000000000,
    !- X,Y,Z 1 {m}
-0.451068000000, 3.964912000000, 0.000000000000,
    !- X,Y,Z 2 {m}
-1.361068000000, 3.964912000000, 0.000000000000,
    !- X,Y,Z 3 {m}
-1.361068000000, 3.964912000000, 2.440000000000;
    !- X,Y,Z 4 {m}

BuildingSurface:Detailed,
2D3C2B, !- Name
Floor,  !- Surface Type
Exterior Floor, !- Construction Name
Conditioned, !- Zone Name
Ground,      !- Outside Boundary Condition
,            !- Outside Boundary Condition Object
NoSun,      !- Sun Exposure
NoWind,     !- Wind Exposure
,           !- View Factor to Ground
4,          !- Number of Vertices
3.609404000000, 5.519550000000, 0.000000000000,
    !- X,Y,Z 1 {m}
3.609404000000, 0.869550000000, 0.000000000000,
    !- X,Y,Z 2 {m}
2.699404000000, 0.869550000000, 0.000000000000,
    !- X,Y,Z 3 {m}
2.699404000000, 5.519550000000, 0.000000000000;
    !- X,Y,Z 4 {m}

BuildingSurface:Detailed,
EastMasonryToiletWall, !- Name
Wall,                  !- Surface Type
$ExteriorWallOption_03, !- Construction Name
Conditioned,           !- Zone Name
Outdoors,              !- Outside Boundary Condition
,                      !- Outside Boundary Condition Object
SunExposed,            !- Sun Exposure
WindExposed,           !- Wind Exposure
,                      !- View Factor to Ground
4,                     !- Number of Vertices
3.609404000000, 7.579550000000, 2.440000000000,
    !- X,Y,Z 1 {m}
3.609404000000, 7.579550000000, 0.000000000000,
    !- X,Y,Z 2 {m}
3.609404000000, 8.089550000000, 0.000000000000,
    !- X,Y,Z 3 {m}
3.609404000000, 8.089550000000, 2.440000000000;
    !- X,Y,Z 4 {m}

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!- X,Y,Z 4 {m}
BuildingSurface:Detailed,
MainFloor,      !- Name
Floor,          !- Surface Type
Slab Floor with Radiant, !- Construction Name
Conditioned,    !- Zone Name
Ground,         !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
NoSun,          !- Sun Exposure
NoWind,         !- Wind Exposure
0.0,           !- View Factor to Ground
12,            !- Number of Vertices
11.589404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 1 {m}
11.589404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 2 {m}
3.609404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 3 {m}
3.609404000000, -0.750450000000, 0.000000000000,
!- X,Y,Z 4 {m}
1.509404000000, -0.750450000000, 0.000000000000,
!- X,Y,Z 5 {m}
1.509404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 6 {m}
-1.940596000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 7 {m}
-1.940596000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 8 {m}
1.509404000000, 7.579550000000, 0.000000000000,
!- X,Y,Z 9 {m}
1.509404000000, 8.089550000000, 0.000000000000,
!- X,Y,Z 10 {m}
3.609404000000, 8.089550000000, 0.000000000000,
!- X,Y,Z 11 {m}
3.609404000000, 7.579550000000, 0.000000000000;
!- X,Y,Z 12 {m}

BuildingSurface:Detailed,
InterMaintoMech, !- Name
Wall,            !- Surface Type
$InteriorWallOption_01, !- Construction Name
Conditioned,    !- Zone Name
Surface,        !- Outside Boundary Condition
InterMechtoMain, !- Outside Boundary Condition Object
NoSun,          !- Sun Exposure
NoWind,         !- Wind Exposure
0.0,           !- View Factor to Ground
7,             !- Number of Vertices
3.609404000000, 0.869550000000, 3.743657289003,
!- X,Y,Z 1 {m}
3.609404000000, 0.869550000000, 0.000000000000,
!- X,Y,Z 2 {m}
3.609404000000, 5.519550000000, 0.000000000000,
!- X,Y,Z 3 {m}
3.609404000000, 5.519550000000, 2.440000000000,
!- X,Y,Z 4 {m}
3.609404000000, 7.579550000000, 2.440000000000,
!- X,Y,Z 5 {m}
3.609404000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 6 {m}
3.609404000000, 3.669550000000, 2.870000000000;
!- X,Y,Z 7 {m}

BuildingSurface:Detailed,
NorthEastRoof, !- Name
Roof,          !- Surface Type
$RoofingOption_01, !- Construction Name
Conditioned,    !- Zone Name
Outdoors,      !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
SunExposed,    !- Sun Exposure
WindExposed,   !- Wind Exposure
,              !- View Factor to Ground
4,             !- Number of Vertices
3.609404000000, 7.579550000000, 4.090000000000,
!- X,Y,Z 1 {m}
3.609404000000, 3.669550000000, 2.870000000000,

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!- X,Y,Z 2 {m}
11.589404000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 3 {m}
11.589404000000, 7.579550000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
SouthEastRoof, !- Name
Roof,          !- Surface Type
$RoofingOption_01, !- Construction Name
Conditioned,    !- Zone Name
Outdoors,      !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
SunExposed,    !- Sun Exposure
WindExposed,   !- Wind Exposure
,              !- View Factor to Ground
4,             !- Number of Vertices
11.589404000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 1 {m}
11.589404000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 2 {m}
3.609404000000, 3.669550000000, 2.870000000000,
!- X,Y,Z 3 {m}
3.609404000000, -0.240450000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
MechRoofEx,    !- Name
Roof,          !- Surface Type
$RoofingOption_01, !- Construction Name
MechanicalRoom, !- Zone Name
Outdoors,      !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
SunExposed,    !- Sun Exposure
WindExposed,   !- Wind Exposure
,              !- View Factor to Ground
4,             !- Number of Vertices
-2.551068000000, 6.534912000000, 6.910000000000,
!- X,Y,Z 1 {m}
-2.551068000000, -0.685088000000, 6.910000000000,
!- X,Y,Z 2 {m}
-0.451068000000, -0.685088000000, 6.910000000000,
!- X,Y,Z 3 {m}
-0.451068000000, 6.534912000000, 6.910000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
SouthWindowFlameWallRightTop, !- Name
Wall,          !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned,    !- Zone Name
Outdoors,      !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
SunExposed,    !- Sun Exposure
WindExposed,   !- Wind Exposure
,              !- View Factor to Ground
4,             !- Number of Vertices
11.589404000000, -0.240450000000, 4.090000000000,
!- X,Y,Z 1 {m}
11.589404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 2 {m}
3.609404000000, -0.240450000000, 0.000000000000,
!- X,Y,Z 3 {m}
3.609404000000, -0.240450000000, 4.090000000000;
!- X,Y,Z 4 {m}

BuildingSurface:Detailed,
EastSolidWall, !- Name
Wall,          !- Surface Type
$ExteriorWallOption_01, !- Construction Name
Conditioned,    !- Zone Name
Outdoors,      !- Outside Boundary Condition
,              !- Outside Boundary Condition Object
SunExposed,    !- Sun Exposure
WindExposed,   !- Wind Exposure
,              !- View Factor to Ground
5,             !- Number of Vertices
11.589404000000, -0.240450000000, 4.090000000000,

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    !- X,Y,Z 1 {m}
11.589404000000, -0.240450000000, 0.000000000000,
    !- X,Y,Z 2 {m}
11.589404000000, 7.579550000000, 0.000000000000,
    !- X,Y,Z 3 {m}
11.589404000000, 7.579550000000, 4.090000000000,
    !- X,Y,Z 4 {m}
11.589404000000, 3.669550000000, 2.870000000000;
    !- X,Y,Z 5 {m}

BuildingSurface:Detailed,
InterzonewallToElecRoom, !- Name
Wall, !- Surface Type
$InteriorWallOption_01, !- Construction Name
Conditioned, !- Zone Name
Surface, !- Outside Boundary Condition
ElecroomInterzonetoMain, !- Outside Boundary Condition Object
NoSun, !- Sun Exposure
NoWind, !- Wind Exposure
0.0, !- View Factor to Ground
4, !- Number of Vertices
11.589404000000, 1.399550000000, 2.640000000000,
    !- X,Y,Z 1 {m}
11.589404000000, 1.399550000000, 0.000000000000,
    !- X,Y,Z 2 {m}
11.589404000000, 5.939550000000, 0.000000000000,
    !- X,Y,Z 3 {m}
11.589404000000, 5.939550000000, 2.640000000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Mechanical window left, !- Name
Window, !- Surface Type
Exterior Window, !- Construction Name
MechWestExWall, !- Building Surface Name
, !- Outside Boundary Condition Object
, !- View Factor to Ground
, !- Shading Control Name
, !- Frame and Divider Name
, !- Multiplier
4, !- Number of Vertices
-2.551068000000, 6.433312000000, 6.859200000000,
    !- X,Y,Z 1 {m}
-2.551068000000, 6.433312000000, 5.030400000000,
    !- X,Y,Z 2 {m}
-2.551068000000, 4.477512000000, 5.030400000000,
    !- X,Y,Z 3 {m}
-2.551068000000, 4.477512000000, 6.859200000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Solar Chimney window left, !- Name
Window, !- Surface Type
Exterior Window, !- Construction Name
WestChimneyWall, !- Building Surface Name
, !- Outside Boundary Condition Object
, !- View Factor to Ground
, !- Shading Control Name
, !- Frame and Divider Name
, !- Multiplier
4, !- Number of Vertices
1.509404000000, -0.648850000000, 6.859200000000,
    !- X,Y,Z 1 {m}
1.509404000000, -0.648850000000, 5.030400000000,
    !- X,Y,Z 2 {m}
1.509404000000, 0.869550000000, 5.030400000000,
    !- X,Y,Z 3 {m}
1.509404000000, 0.869550000000, 6.859200000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Solar Chimney window front, !- Name
Window, !- Surface Type
Exterior Window, !- Construction Name
SouthChimneyWall, !- Building Surface Name
, !- Outside Boundary Condition Object
, !- View Factor to Ground
, !- Shading Control Name
, !- Frame and Divider Name
, !- Multiplier
4, !- Number of Vertices
1.509404000000, -0.648850000000, 6.859200000000,
    !- X,Y,Z 1 {m}
1.509404000000, -0.648850000000, 5.030400000000,
    !- X,Y,Z 2 {m}
1.509404000000, 0.869550000000, 5.030400000000,
    !- X,Y,Z 3 {m}
1.509404000000, 0.869550000000, 6.859200000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Solar Chimney window right, !- Name
Window, !- Surface Type
Exterior Window, !- Construction Name
EastChimneyWall, !- Building Surface Name
, !- Outside Boundary Condition Object
, !- View Factor to Ground
, !- Shading Control Name
, !- Frame and Divider Name
, !- Multiplier
4, !- Number of Vertices
3.609404000000, 0.869550000000, 6.859200000000,
    !- X,Y,Z 1 {m}
3.609404000000, 0.869550000000, 5.030400000000,
    !- X,Y,Z 2 {m}
3.609404000000, -0.648850000000, 5.030400000000,
    !- X,Y,Z 3 {m}
3.609404000000, -0.648850000000, 6.859200000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Mechanical window left big, !- Name
Window, !- Surface Type
Exterior Window, !- Construction Name
MechEastEx, !- Building Surface Name
, !- Outside Boundary Condition Object
, !- View Factor to Ground
, !- Shading Control Name
, !- Frame and Divider Name
, !- Multiplier
4, !- Number of Vertices
-0.451068000000, 4.477512000000, 6.859200000000,
    !- X,Y,Z 1 {m}
-0.451068000000, 4.477512000000, 5.030400000000,
    !- X,Y,Z 2 {m}
-0.451068000000, 6.433312000000, 5.030400000000,
    !- X,Y,Z 3 {m}
-0.451068000000, 6.433312000000, 6.859200000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Mechanical window back, !- Name
Window, !- Surface Type
Exterior Window, !- Construction Name
MechNorthEx, !- Building Surface Name
, !- Outside Boundary Condition Object
, !- View Factor to Ground
, !- Shading Control Name
, !- Frame and Divider Name
, !- Multiplier
4, !- Number of Vertices
-0.552668000000, 6.534912000000, 6.859200000000,
    !- X,Y,Z 1 {m}
-0.552668000000, 6.534912000000, 5.030400000000,
    !- X,Y,Z 2 {m}
-2.449468000000, 6.534912000000, 5.030400000000,
    !- X,Y,Z 3 {m}
-2.449468000000, 6.534912000000, 6.859200000000;
    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Working door, !- Name
Door, !- Surface Type
Exterior Door, !- Construction Name
SouthWindowFlameWallRightTop, !- Building Surface Name
, !- Outside Boundary Condition Object

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,           !- View Factor to Ground
,           !- Shading Control Name
,           !- Frame and Divider Name
,           !- Multiplier
4,          !- Number of Vertices
9.123404000000, -0.240450000000, 2.133600000000,
           !- X,Y,Z 1 {m}
9.123404000000, -0.240450000000, 0.000000000000,
           !- X,Y,Z 2 {m}
6.075404000000, -0.240450000000, 0.000000000000,
           !- X,Y,Z 3 {m}
6.075404000000, -0.240450000000, 2.133600000000;
           !- X,Y,Z 4 {m}
FenestrationSurface:Detailed,
Living front window up, !- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
SouthWindowFlameWallleft,!- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
1.366166500000, -0.240450000000, 3.514848811965,
           !- X,Y,Z 1 {m}
1.366166500000, -0.240450000000, 2.397248811965,
           !- X,Y,Z 2 {m}
-1.838996000000, -0.240450000000, 2.397248811965,
           !- X,Y,Z 3 {m}
-1.838996000000, -0.240450000000, 3.514848811965;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living back window up, !- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
NorthWindowFlameWallRight, !- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
-1.838996000000, 7.579550000000, 3.514848811965,
           !- X,Y,Z 1 {m}
-1.838996000000, 7.579550000000, 2.397248811965,
           !- X,Y,Z 2 {m}
1.348704000000, 7.579550000000, 2.397248811965,
           !- X,Y,Z 3 {m}
1.348704000000, 7.579550000000, 3.514848811965;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Working back window, !- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
D502FE,          !- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
3.844386313328, 7.579550000000, 3.505200000000,
           !- X,Y,Z 1 {m}
3.844386313328, 7.579550000000, 2.387600000000,
           !- X,Y,Z 2 {m}
11.372311313328, 7.579550000000, 2.387600000000,
           !- X,Y,Z 3 {m}
11.372311313328, 7.579550000000, 3.505200000000;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Working front window, !- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
SouthWindowFlameWallRightTop, !- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
11.253328617860, -0.240450000000, 3.505200000000,
           !- X,Y,Z 1 {m}
11.253328617860, -0.240450000000, 2.387600000000,
           !- X,Y,Z 2 {m}
3.738103617860, -0.240450000000, 2.387600000000,
           !- X,Y,Z 3 {m}
3.738103617860, -0.240450000000, 3.505200000000;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living front window down,!- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
SouthWindowFlameWallleft,!- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
1.362991500000, -0.240450000000, 2.244848811965,
           !- X,Y,Z 1 {m}
1.362991500000, -0.240450000000, 0.073148811965,
           !- X,Y,Z 2 {m}
-1.838996000000, -0.240450000000, 0.073148811965,
           !- X,Y,Z 3 {m}
-1.838996000000, -0.240450000000, 2.244848811965;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living back window down, !- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
NorthWindowFlameWallRight, !- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
-1.813596000000, 7.579550000000, 2.244848811965,
           !- X,Y,Z 1 {m}
-1.813596000000, 7.579550000000, 0.111248811965,
           !- X,Y,Z 2 {m}
1.348704000000, 7.579550000000, 0.111248811965,
           !- X,Y,Z 3 {m}
1.348704000000, 7.579550000000, 2.244848811965;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living left window 1, !- Name
Window,           !- Surface Type
Exterior Window,  !- Construction Name
Living left side wall, !- Building Surface Name
,               !- Outside Boundary Condition Object
,               !- View Factor to Ground
,               !- Shading Control Name
,               !- Frame and Divider Name
,               !- Multiplier
4,               !- Number of Vertices
-1.940596000000, 7.463662500000, 2.244848811965,
           !- X,Y,Z 1 {m}
-1.940596000000, 7.463662500000, 0.111248811965,
           !- X,Y,Z 2 {m}
-1.940596000000, 5.939662500000, 0.111248811965,
           !- X,Y,Z 3 {m}
-1.940596000000, 5.939662500000, 2.244848811965;
           !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living left window 3, !- Name

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Window,                !- Surface Type
Exterior Window,      !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 0.064350000000, 2.244848811965,
                    !- X,Y,Z 1 {m}
-1.940596000000, 0.064350000000, 0.111248811965,
                    !- X,Y,Z 2 {m}
-1.940596000000, -0.138850000000, 0.111248811965,
                    !- X,Y,Z 3 {m}
-1.940596000000, -0.138850000000, 2.244848811965;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living door,          !- Name
Door,                !- Surface Type
Exterior Door,       !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 1.020780990802, 2.244848811965,
                    !- X,Y,Z 1 {m}
-1.940596000000, 1.020780990802, 0.000000000000,
                    !- X,Y,Z 2 {m}
-1.940596000000, 0.106380990802, 0.000000000000,
                    !- X,Y,Z 3 {m}
-1.940596000000, 0.106380990802, 2.244848811965;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living left window 2, !- Name
Window,              !- Surface Type
Exterior Window,    !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 1.195399817688, 2.232333822170,
                    !- X,Y,Z 1 {m}
-1.940596000000, 1.195399817688, 0.063808822170,
                    !- X,Y,Z 2 {m}
-1.940596000000, 1.062049817688, 0.063808822170,
                    !- X,Y,Z 3 {m}
-1.940596000000, 1.062049817688, 2.232333822170;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living left window up 1, !- Name
Window,              !- Surface Type
Exterior Window,    !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 7.463662500000, 2.828464534562,
                    !- X,Y,Z 1 {m}
-1.940596000000, 7.463662500000, 2.439000000000,
                    !- X,Y,Z 2 {m}
-1.940596000000, 3.699242073884, 2.439000000000,
                    !- X,Y,Z 3 {m}
-1.940596000000, 3.699242073884, 2.828464534562;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
Living left window up 2, !- Name
Window,              !- Surface Type
Exterior Window,    !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 3.640566687729, 2.828243386437,
                    !- X,Y,Z 1 {m}
-1.940596000000, 3.640566687729, 2.439000000000,
                    !- X,Y,Z 2 {m}
-1.940596000000, -0.138850000000, 2.439000000000,
                    !- X,Y,Z 3 {m}
-1.940596000000, -0.138850000000, 2.828243386437;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
75E66C,              !- Name
Window,              !- Surface Type
Exterior Window,    !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 7.416966472892, 3.449033100849,
                    !- X,Y,Z 1 {m}
-1.940596000000, 7.416966472892, 2.898170600849,
                    !- X,Y,Z 2 {m}
-1.940596000000, 5.754853972892, 2.898170600849,
                    !- X,Y,Z 3 {m}
-1.940596000000, 5.754853972892, 3.449033100849;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
A40630,              !- Name
Window,              !- Surface Type
Exterior Window,    !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 5.640285501700, 3.349477701601,
                    !- X,Y,Z 1 {m}
-1.940596000000, 5.640285501700, 2.928790201601,
                    !- X,Y,Z 2 {m}
-1.940596000000, 5.333898001700, 2.928790201601,
                    !- X,Y,Z 3 {m}
-1.940596000000, 5.333898001700, 3.349477701601;
                    !- X,Y,Z 4 {m}

FenestrationSurface:Detailed,
6E2063,              !- Name
Window,              !- Surface Type
Exterior Window,    !- Construction Name
Living left side wall, !- Building Surface Name
,                    !- Outside Boundary Condition Object
,                    !- View Factor to Ground
,                    !- Shading Control Name
,                    !- Frame and Divider Name
,                    !- Multiplier
4,                    !- Number of Vertices
-1.940596000000, 5.196115258902, 3.234606087084,
                    !- X,Y,Z 1 {m}
-1.940596000000, 5.196115258902, 2.936156087084,
                    !- X,Y,Z 2 {m}
-1.940596000000, 4.897665258902, 2.936156087084,
                    !- X,Y,Z 3 {m}
-1.940596000000, 4.897665258902, 3.234606087084;
                    !- X,Y,Z 4 {m}

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                !- X,Y,Z 4 {m}
FenestrationSurface:Detailed,
802E3E,          !- Name
Window,         !- Surface Type
Exterior Window, !- Construction Name
Living left side wall, !- Building Surface Name
,              !- Outside Boundary Condition Object
,              !- View Factor to Ground
,              !- Shading Control Name
,              !- Frame and Divider Name
,              !- Multiplier
4,             !- Number of Vertices
-1.940596000000, 7.378675934720, 3.831938482571,
                !- X,Y,Z 1 {m}
-1.940596000000, 7.378675934720, 3.509675982571,
                !- X,Y,Z 2 {m}
-1.940596000000, 6.950050934720, 3.509675982571,
                !- X,Y,Z 3 {m}
-1.940596000000, 6.950050934720, 3.831938482571;
                !- X,Y,Z 4 {m}

```

```

FenestrationSurface:Detailed,
D1B8FC,         !- Name
Window,         !- Surface Type
Exterior Window, !- Construction Name
Living left side wall, !- Building Surface Name
,              !- Outside Boundary Condition Object
,              !- View Factor to Ground
,              !- Shading Control Name
,              !- Frame and Divider Name
,              !- Multiplier
4,             !- Number of Vertices
-1.940596000000, 1.583129342773, 3.447214125062,
                !- X,Y,Z 1 {m}
-1.940596000000, 1.583129342773, 2.956676625062,
                !- X,Y,Z 2 {m}
-1.940596000000, -0.125020657227, 2.956676625062,
                !- X,Y,Z 3 {m}
-1.940596000000, -0.125020657227, 3.447214125062;
                !- X,Y,Z 4 {m}

```

```

FenestrationSurface:Detailed,
17DACE,         !- Name
Window,         !- Surface Type
Exterior Window, !- Construction Name
Living left side wall, !- Building Surface Name
,              !- Outside Boundary Condition Object
,              !- View Factor to Ground
,              !- Shading Control Name
,              !- Frame and Divider Name
,              !- Multiplier
4,             !- Number of Vertices
-1.940596000000, 1.972995782674, 3.316607683881,
                !- X,Y,Z 1 {m}
-1.940596000000, 1.972995782674, 2.956245183881,
                !- X,Y,Z 2 {m}
-1.940596000000, 1.720583282674, 2.956245183881,
                !- X,Y,Z 3 {m}
-1.940596000000, 1.720583282674, 3.316607683881;
                !- X,Y,Z 4 {m}

```

```

FenestrationSurface:Detailed,
CA26E4,         !- Name
Window,         !- Surface Type
Exterior Window, !- Construction Name
Living left side wall, !- Building Surface Name
,              !- Outside Boundary Condition Object
,              !- View Factor to Ground
,              !- Shading Control Name
,              !- Frame and Divider Name
,              !- Multiplier
4,             !- Number of Vertices
-1.940596000000, 2.379180539237, 3.194077961730,
                !- X,Y,Z 1 {m}
-1.940596000000, 2.379180539237, 2.949602961730,
                !- X,Y,Z 2 {m}
-1.940596000000, 2.080730539237, 2.949602961730,

```

```

                !- X,Y,Z 3 {m}
-1.940596000000, 2.080730539237, 3.194077961730;
                !- X,Y,Z 4 {m}
FenestrationSurface:Detailed,
6EC22E,         !- Name
Window,         !- Surface Type
Exterior Window, !- Construction Name
Living left side wall, !- Building Surface Name
,              !- Outside Boundary Condition Object
,              !- View Factor to Ground
,              !- Shading Control Name
,              !- Frame and Divider Name
,              !- Multiplier
4,             !- Number of Vertices
-1.940596000000, 0.350391165676, 3.837701590011,
                !- X,Y,Z 1 {m}
-1.940596000000, 0.350391165676, 3.523376590011,
                !- X,Y,Z 2 {m}
-1.940596000000, -0.102046334324, 3.523376590011,
                !- X,Y,Z 3 {m}
-1.940596000000, -0.102046334324, 3.837701590011;
                !- X,Y,Z 4 {m}

```

Appendix D: XML Option File

```

<Parametrics>
  <ParametricOption id="ExteriorWallOption_01">
    <Option value="1">PI - SIP Wall</Option>
    <Option value="2">PI - Masonry Wall EPS</Option>
    <Option value="3">PI - Masonry Wall XPS</Option>
    <Option value="4">PI - Masonry Wall Rockwool</Option>
    <Option value="5">PI - Masonry Wall FG</Option>
  </ParametricOption>
  <ParametricOption id="ExteriorWallOption_02">
    <Option value="1">PI - SIP Wall</Option>
    <Option value="2">PI - Masonry Wall EPS</Option>
    <Option value="3">PI - Masonry Wall XPS</Option>
    <Option value="4">PI - Masonry Wall Rockwool</Option>
    <Option value="5">PI - Masonry Wall FG</Option>
  </ParametricOption>
  <ParametricOption id="ExteriorWallOption_03">
    <Option value="1">PI - SIP Wall</Option>
    <Option value="2">PI - Masonry Wall EPS</Option>
    <Option value="3">PI - Masonry Wall XPS</Option>
    <Option value="4">PI - Masonry Wall Rockwool</Option>
    <Option value="5">PI - Masonry Wall FG</Option>
  </ParametricOption>
  <ParametricOption id="InteriorWallOption_01">
    <Option value="1">PI - Partition Wall Type D</Option>
  </ParametricOption>
  <ParametricOption id="RoofingOption_01">
    <Option value="1">PI - Roof Clay Tiles</Option>
    <Option value="2">PI - Roof Concrete Tiles</Option>
    <Option value="3">PI - Roof Organic Felt</Option>
    <Option value="4">PI - Roof Steel Panel</Option>
  </ParametricOption>
</Parametrics>

```

VITA

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- Mar 2006 – May 2006 Construction Management Engineer Intern
Unique Engineering and Construction Public Company
Limited
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- May 2007 – May 2008 Structural Engineer and Social Coordinator for Graduate
Development Organization (GDO)
WorleyParsons (Thailand) Limited, Thailand
- Aug 2009 – Dec 2010 Master of Science in Civil Engineering
Viterbi School of Engineering
University of Southern California (USC)
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- March 2014 Elevator Pitches People’s Choice Award
EPA P3 Competition and National Sustainable Design
Expo, the US Science and Engineering Festival (USA SEF)
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PUBLICATIONS

Inyim, P., Rivera, J., & Zhu, Y. (2014). Integration of Building Information Modeling and Economic and Environmental Impact Analysis to Support Sustainable Building Design. *Journal of Management in Engineering*, 31(1).

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