

# Predictive Modeling of Near Dry Machining

IAB Presentation  
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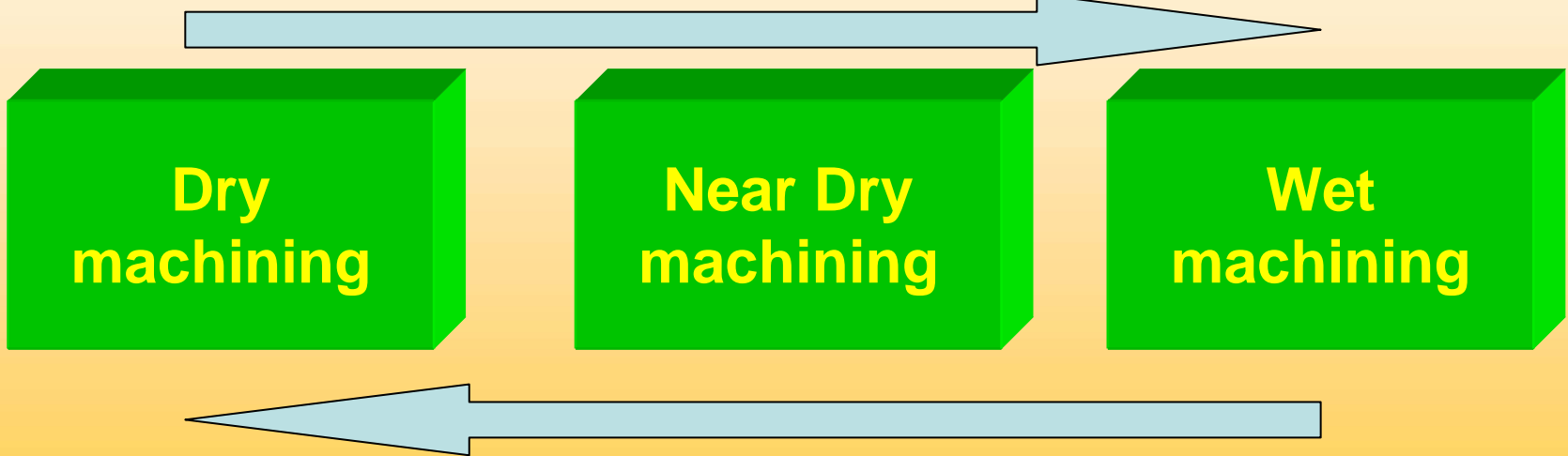
# OUTLINE

- INTRODUCTION
- PROPOSED RESEARCH PLAN
- ESTIMATED CUTTING FORCES AND CUTTING TEMPERATURES
- TOOL WEAR MODELING
- AEROSOL GENERATION MODELING
- RESULTS AND DISCUSSIONS
- CONCLUSION



# INTRODUCTION

- Lubricating
- Cooling
- Chip flushing



- Health
- Environment
- Cost



## INTRODUCTION (Cont'd)

- Near dry machining
  - Use only a small amount of cutting fluids
  - Typically 100 ml/hr or less [Diniz *et. al.*, 2003]
  - Three to four orders of magnitude less than the amount used in flood cooling condition
- Near dry machining has better performances than dry machining and close to traditional flood cooling
  - Turning [Klocke *et. al.*, 1997]
  - Milling [Rahman *et. al.*, 2001]
  - Drilling [Braga *et. al.*, 2002]
  - Reaming [Weinert *et. al.*, 2005]
  - Taping [Weinert *et. al.*, 2005]

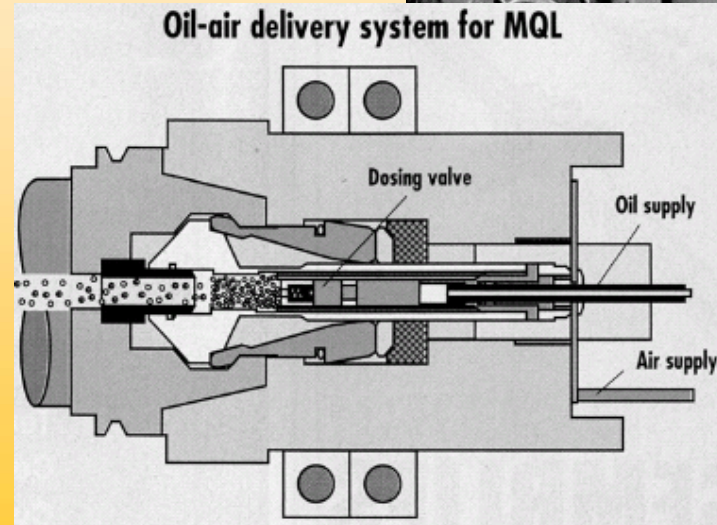
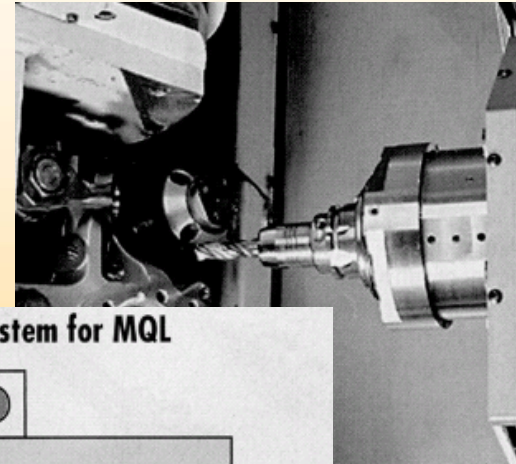


## INTRODUCTION (Cont'd)

- Current applications in the industrial



**Enterprise Automotive  
Services (EAS)**



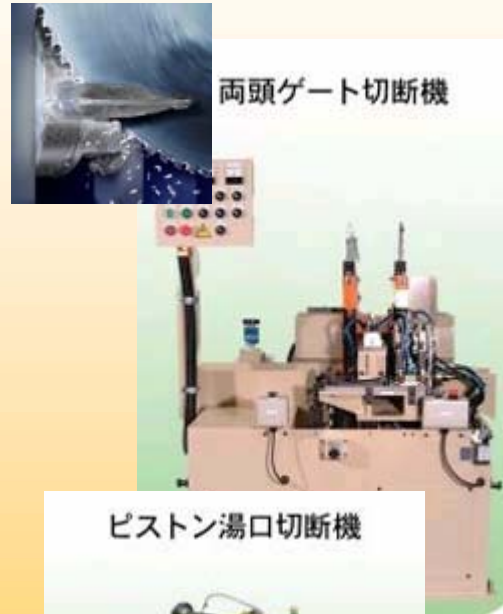
**Cross Huller (Germany)**



# INTRODUCTION (Cont'd)



**AMCOL**



**TATEKIT Engineering  
Co. LTD (Japan)**



**NACHI (Japan)**



## INTRODUCTION (Cont'd)

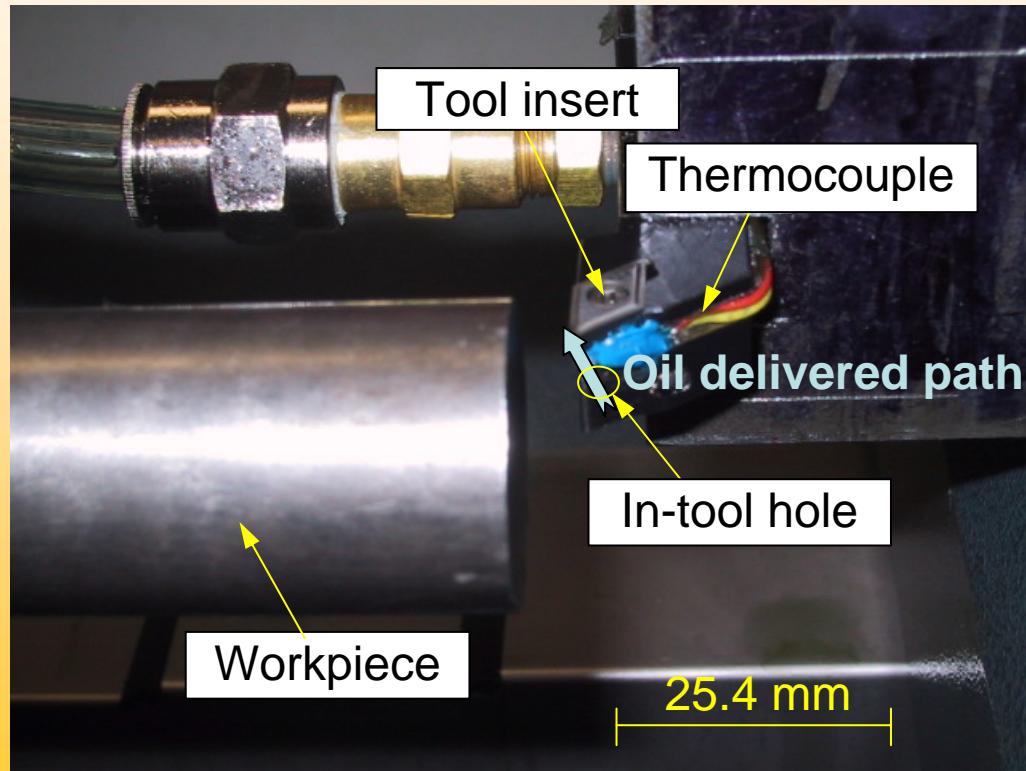
- Current researches are **ONLY** for **Experimental observations**.
- This research quantitatively investigates the *tool performance* and *air quality* for near dry turning with the in-tool hole configuration
- Including:
  - Temperature modeling
  - Force modeling
  - Tool wear modeling
  - Aerosol generation modeling





## INTRODUCTION (Cont'd)

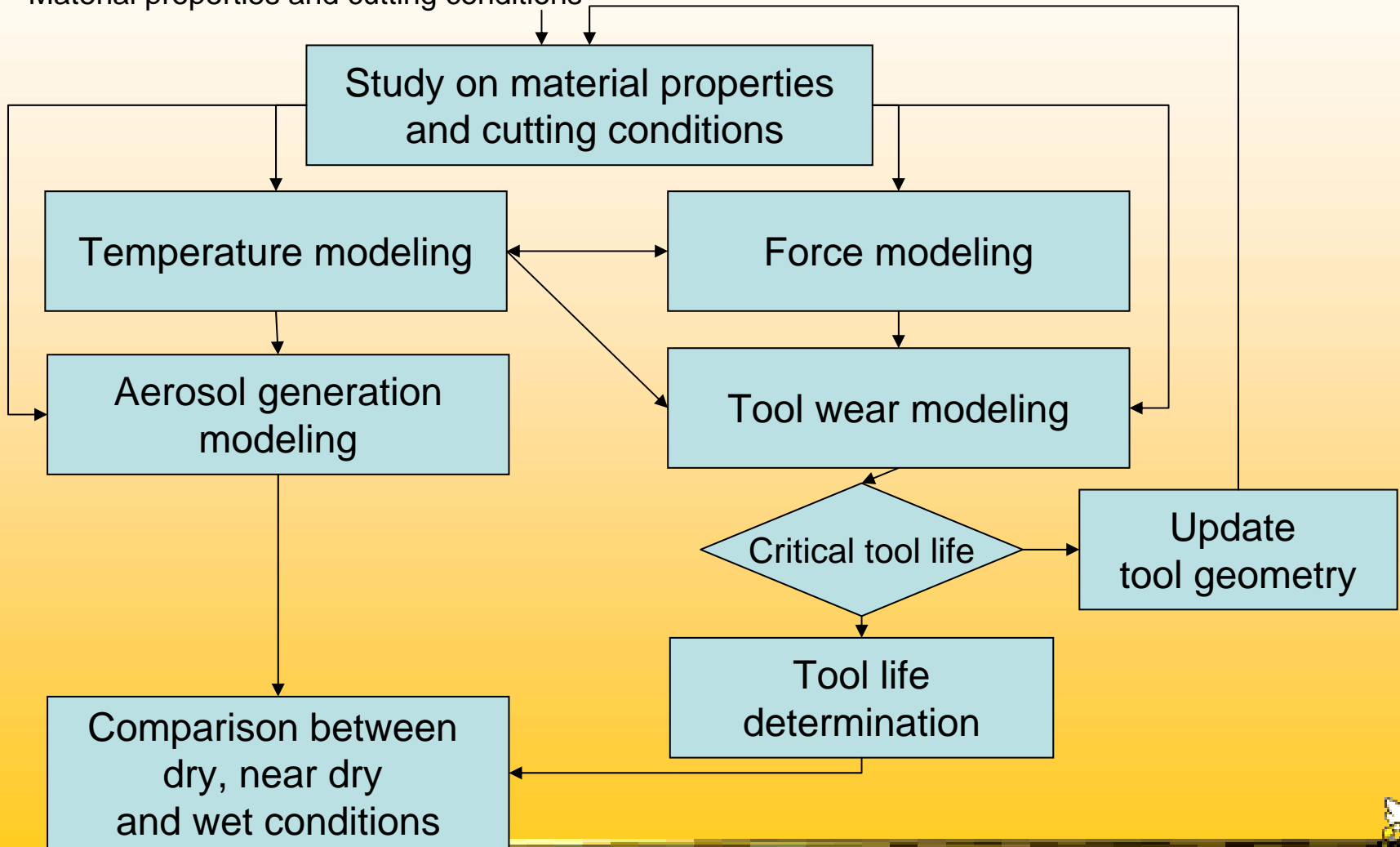
- In-tool hole configuration in this study



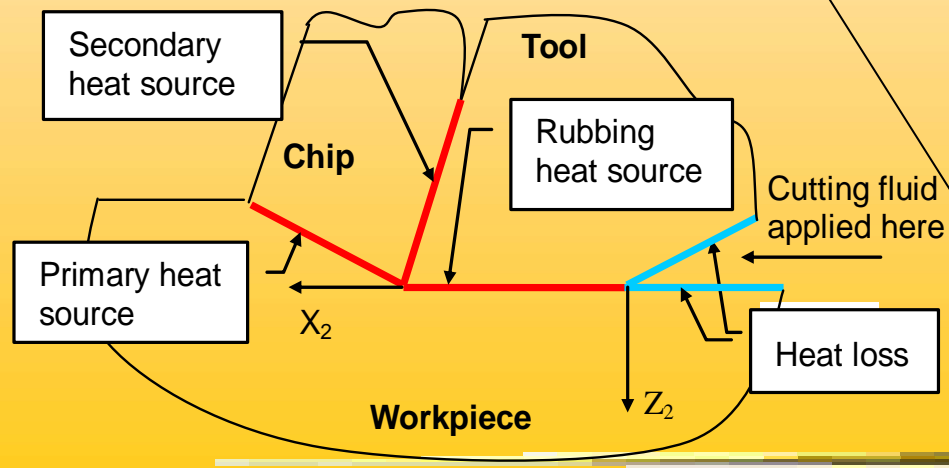
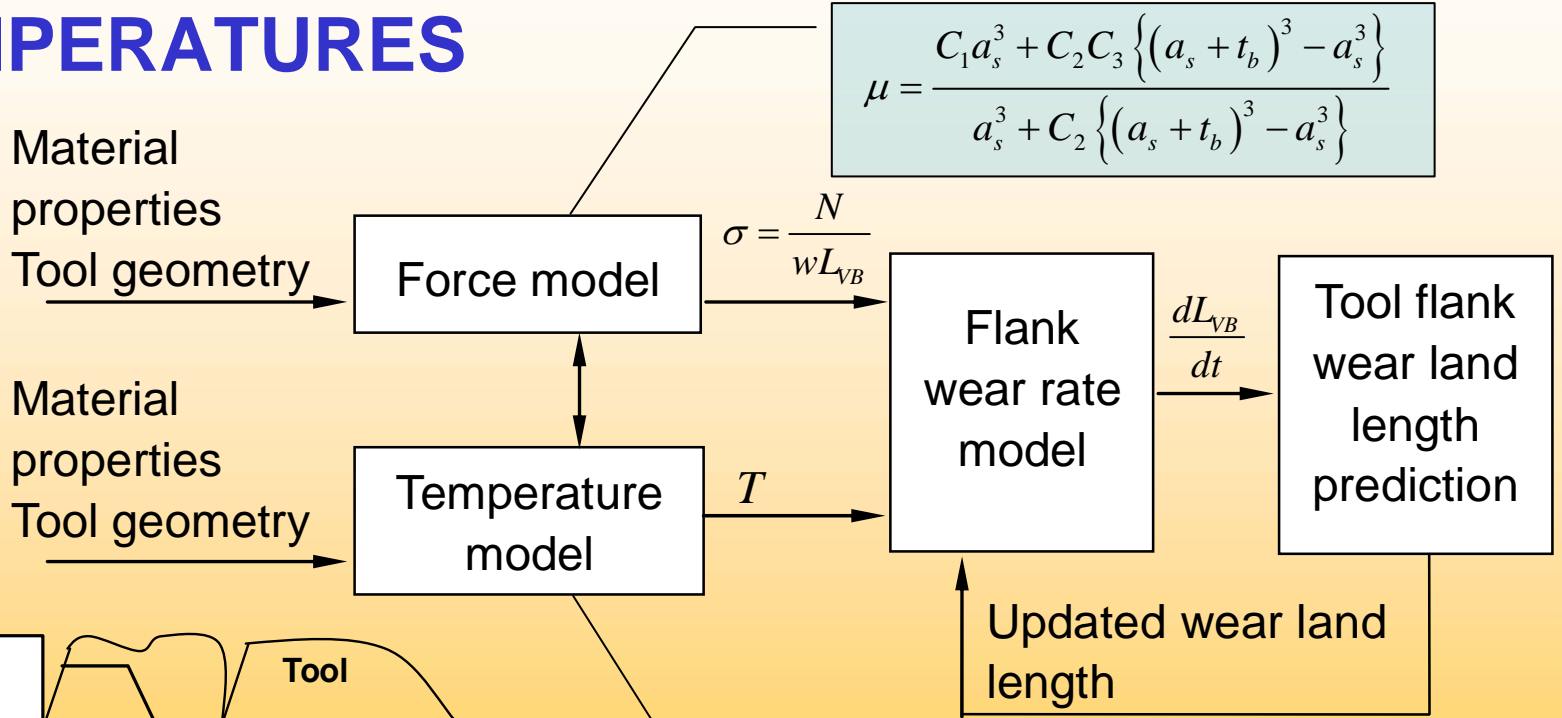


# PROPOSED RESEARCH PLAN

Material properties and cutting conditions



# ESTIMATED CUTTING FORCES AND CUTTING TEMPERATURES



Heat loss due to near dry cooling

$$T_{VB,avg} = \int \frac{(\Delta T_{t-f} - \Delta T_{t-hl} + \Delta T_{t-r}) dl_i}{L_{VB}} + T_o$$



# TOOL WEAR MODELING

- Abrasive wear mechanism

- Three-body abrasion:  $V_{abration} = K_{abration} K \left( \frac{H_a^{n-1}}{H_t^n} \right) V_c w L_{VB} \sigma \Delta t$
- Two-body abrasion:  $V_{abration} = K_{abration} \frac{1}{H_t} V_c w L_{VB} \sigma \Delta t$

- Adhesive wear mechanism

- $V_{adhesion} = K_{adhesion} e^{aT} V_c w \sigma \Delta t$

- Diffusive wear mechanism

- Dominant at high temperature:  $V_{diffusion} = K_{diffusion} \sqrt{V_c L_{VB}} e^{-\left(\frac{K_Q}{T+273}\right)}$

- Tool flank wear rate

- Two-body abrasion

$$\frac{dL_{VB}}{dt} = \frac{\cot \gamma - \tan \alpha}{L_{VB}} \left\{ K_{abration} \left( \frac{1}{H_t} \right) V_c L_{VB} \sigma + K_{adhesion} e^{aT} V_c \sigma \right.$$



# TOOL WEAR MODEL CALIBRATION

- Test cutting conditions

Test No.	Speed (m/min)	Feed (mm/rev)	Depth of cut (mm)
1	45.75	0.0508	0.508
2	45.75	0.0762	1.016
3	45.75	0.1016	0.762
4	91.5	0.0508	1.016
5	91.5	0.0762	0.762
6	91.5	0.1016	0.508
7	137.25	0.0508	0.762
8	137.25	0.0762	0.508
9	137.25	0.1016	1.016

- Tool flank wear rate equation (two-body abrasion)

$$\frac{dL_{VB}}{dt} = \frac{\cot \gamma - \tan \alpha}{L_{VB}} \left\{ 3.697 \times 10^{-7} \left( \frac{1}{H_t} \right) V_c L_{VB} \sigma + 3.6761 \times 10^{-16} e^{7.456 \times 10^{-4} T} V_c \sigma + 1.29 \times 10^5 \sqrt{V_c L_{VB}} e^{\frac{-20570}{T+273}} \right\}$$



# AEROSOL GENERATION MODEL

- Spin-off

- Centrifugal force on the workpiece in rotational motion
- Insignificant in near dry machining

- Runaway aerosol generation (overspray)

- Energy transformation, from kinetic energy to surface energy

- $TE = a + b(SMR) + C(SMR)^2 + d \times D_{32}$  ;  $SMR = \frac{(\dot{m}_l)^2}{\rho_l A_{nozzle}}$

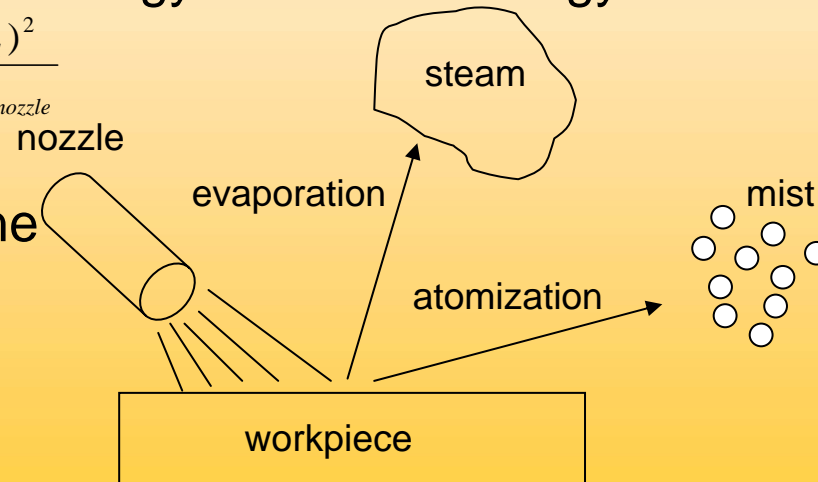
- Evaporation

- High temperature at the cutting zone

- $\eta_{evap} = k\Phi(D) \left( \frac{P_{tr}}{\sqrt{T_{tr}}} - \frac{P_{atm}}{\sqrt{T_v}} \right)$

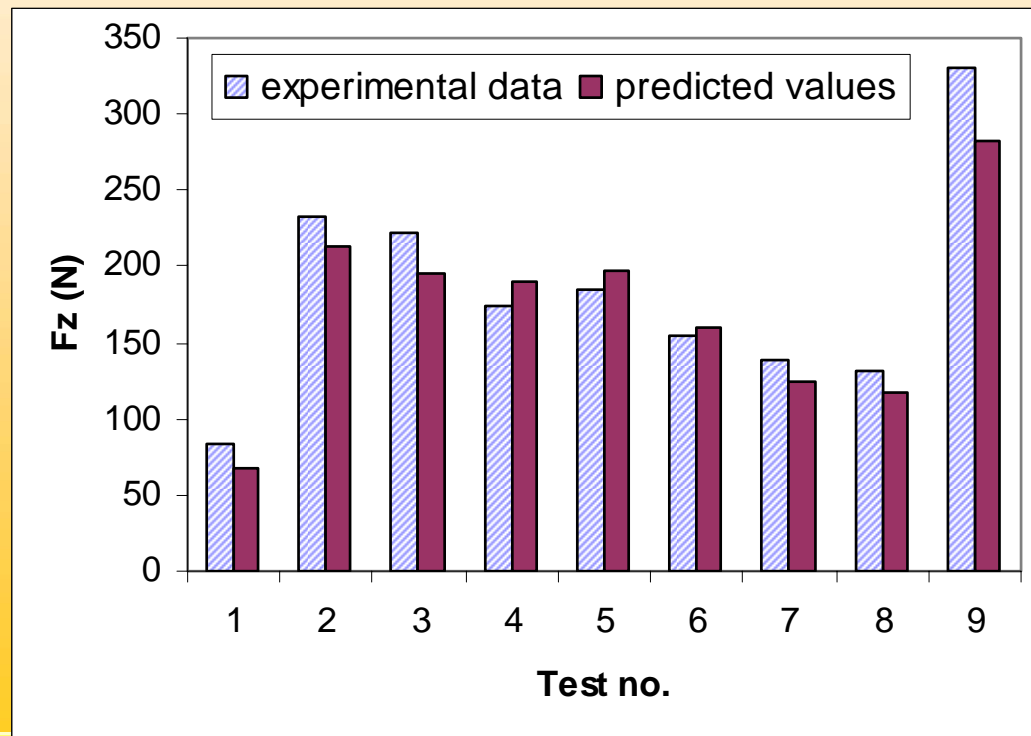
- Aerosol dissipation

- $D_{AB} \frac{1}{s^2} \frac{\partial}{\partial s} \left( s^2 \frac{\partial \eta}{\partial s} \right) = \frac{\partial \eta}{\partial t}$



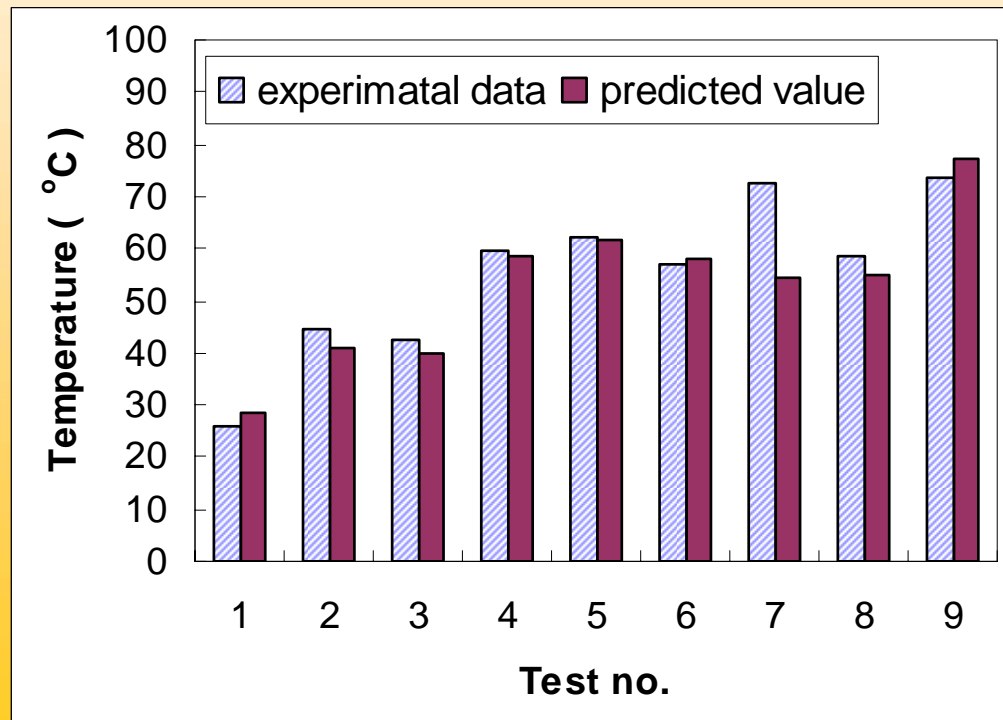
# RESULTS AND DISCUSSIONS

- Model-experiment comparison for cutting force in near dry turning
  - Force comparisons for the cutting velocity direction for sharp tools



## RESULTS AND DISCUSSIONS (Cont'd)

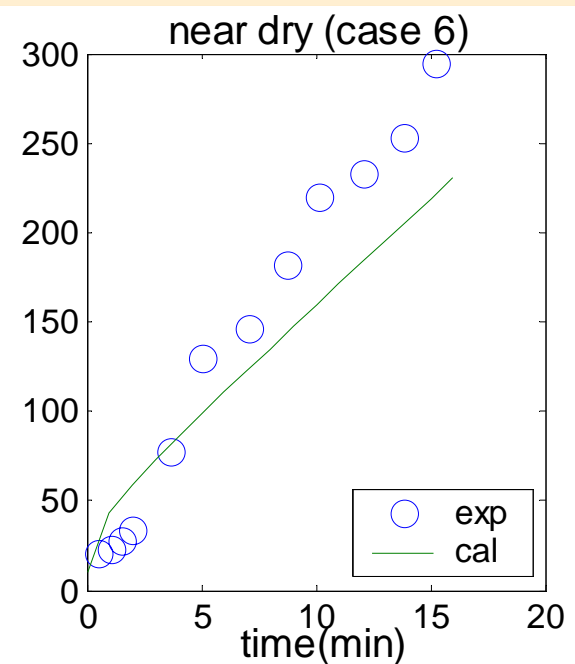
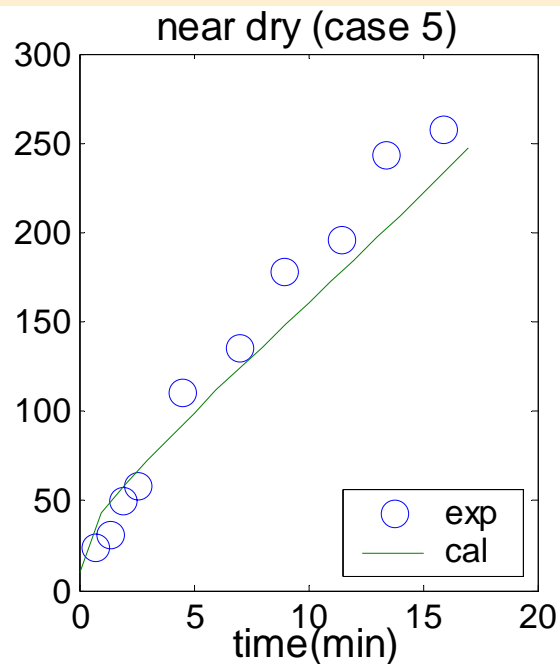
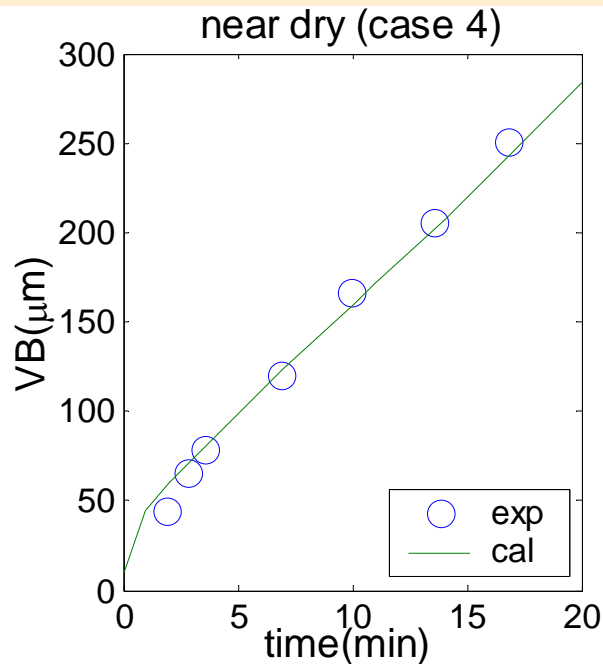
- Model-experiment comparison for cutting temperature in near dry turning
  - Temperature comparison between predicted values and measured values at thermocouple location for sharp tool





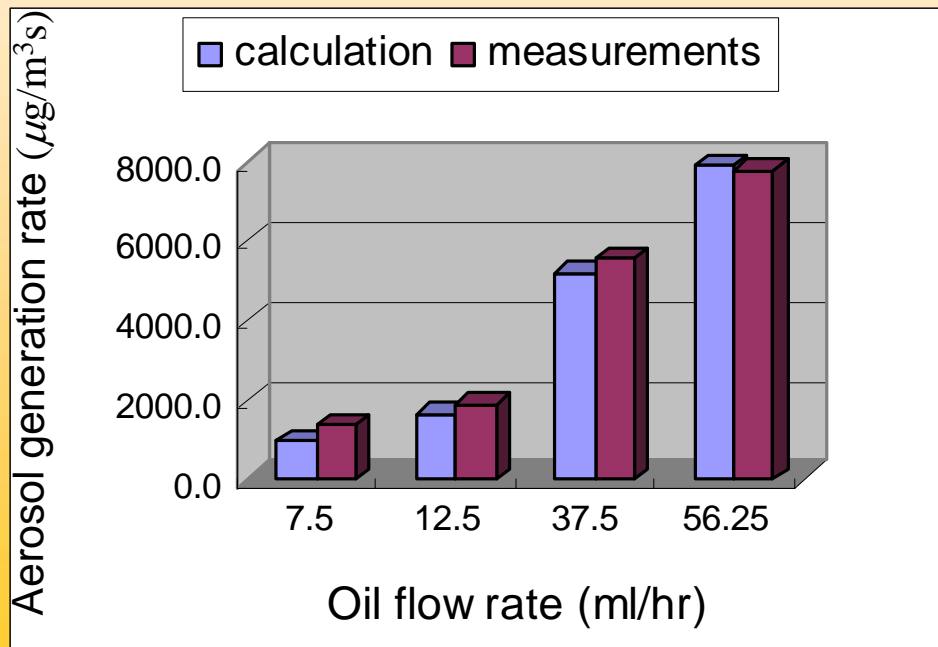
# RESULTS AND DISCUSSIONS

- Tool flank wear: Case 4 ~ 6 ( $V = 91.5 \text{ m/min}$ )
  - Good agreement with experimental data



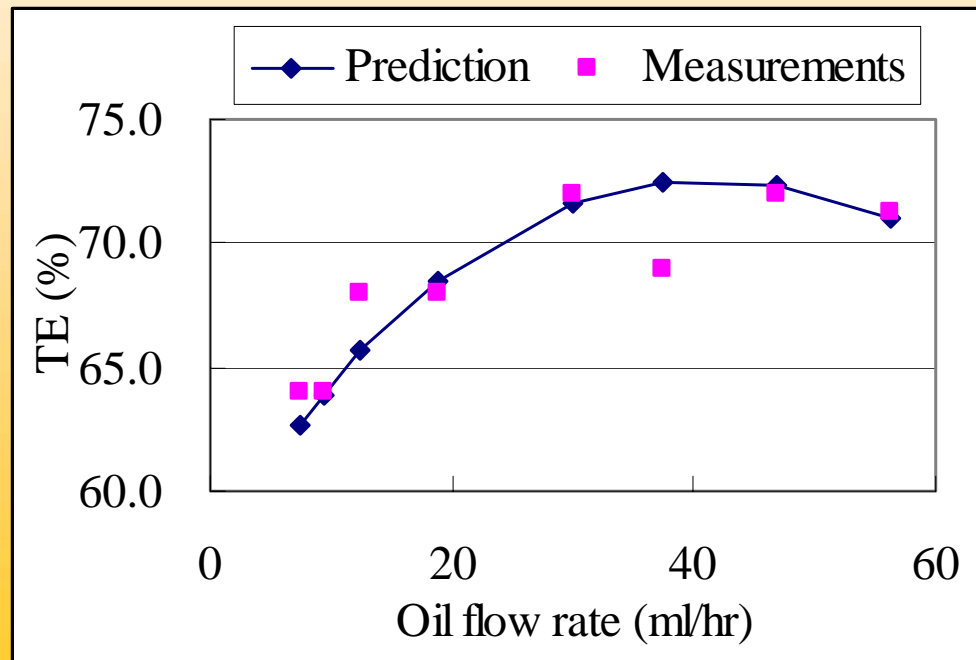
## RESULTS AND DISCUSSIONS (Cont'd)

- Cutting velocity = 61 m/min, feed rate = 0.0762 mm/rev, depth of cut = 0.508 mm
- Oil flow rate is the major factor for aerosol generation rate



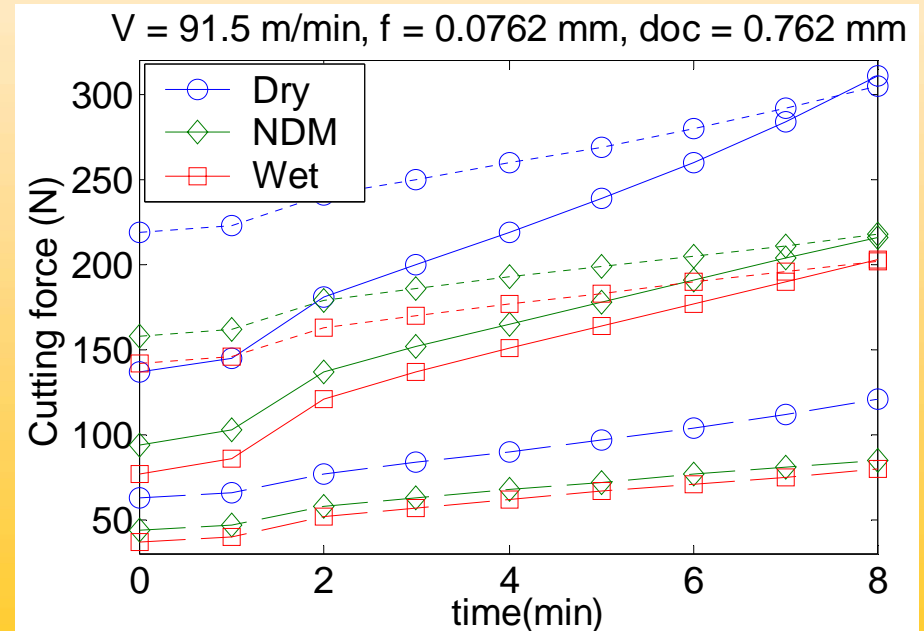
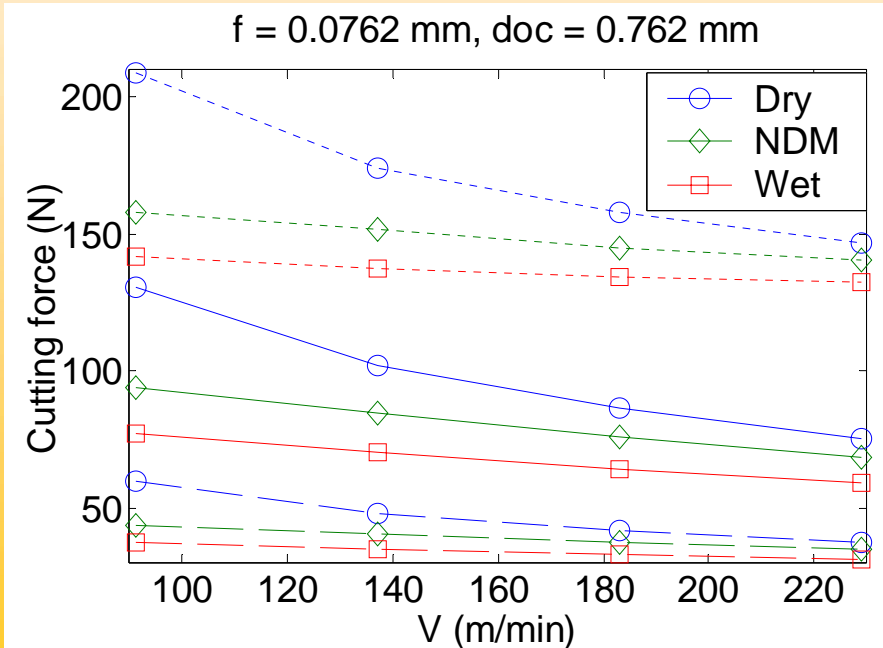
## RESULTS AND DISCUSSIONS (Cont'd)

- Predicted transfer efficiency for different oil flow rate
- TE has a maximum value around 40 ml/hr oil flow rate
- The variation of TE is small compared with that of oil flow rate



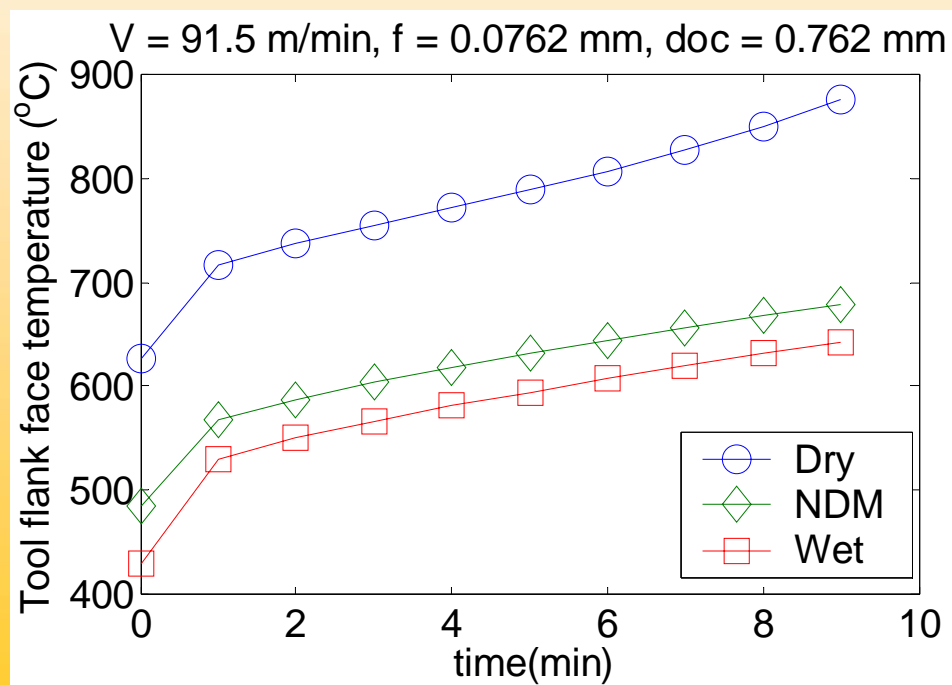
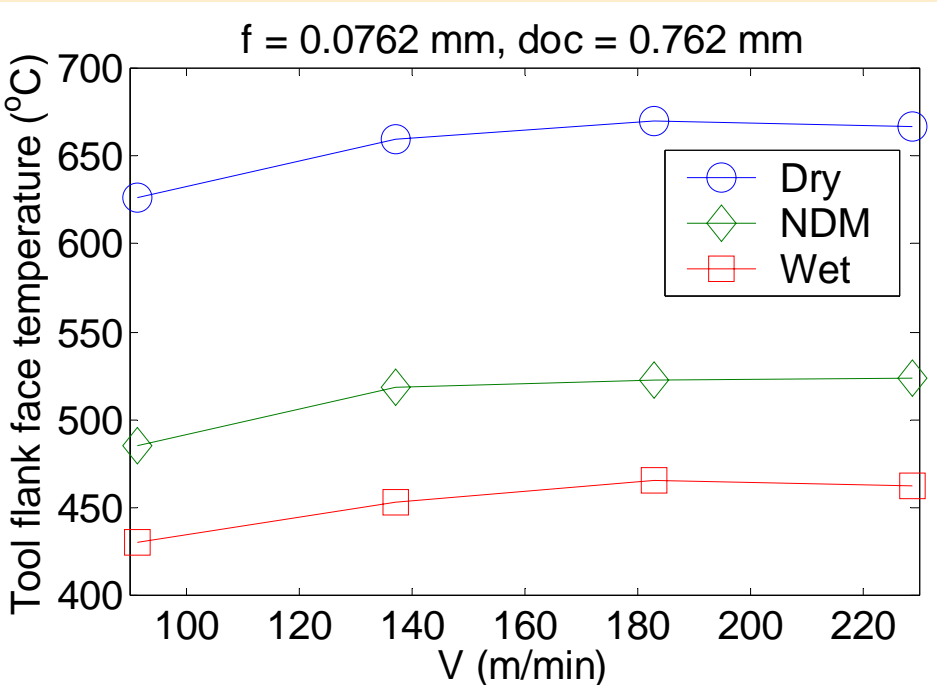
# RESULTS AND DISCUSSIONS (Cont'd)

- Predicted cutting forces
- Dry > NDM > Wet
- The difference becomes small when cutting velocity increases



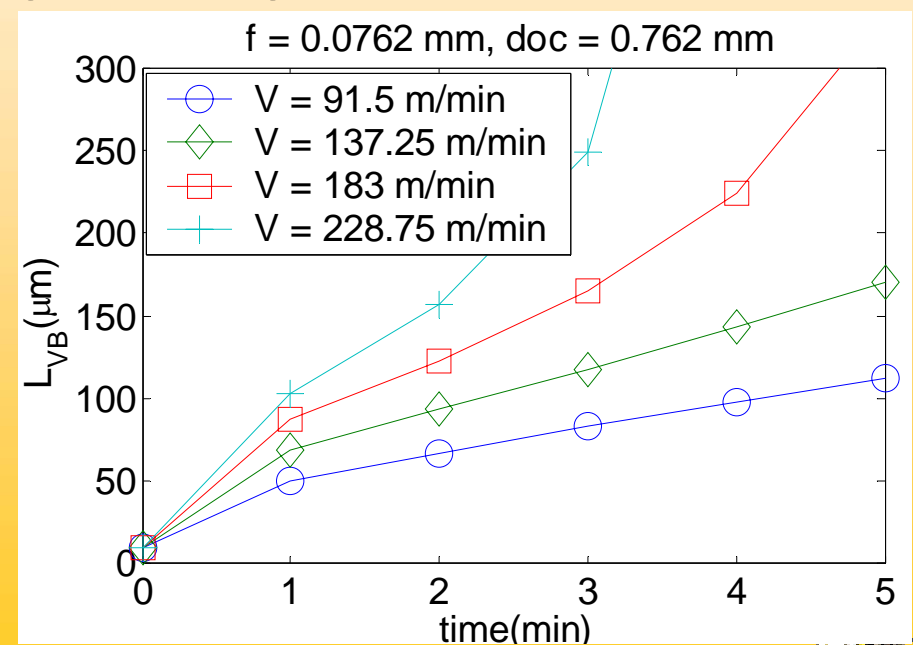
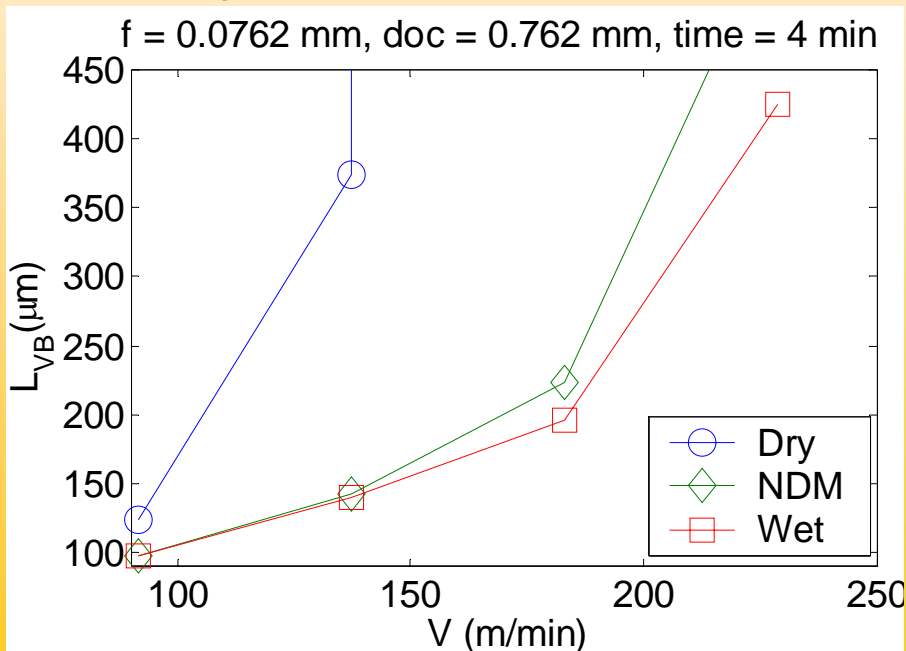
# RESULTS AND DISCUSSIONS (Cont'd)

- Predicted tool flank face temperatures
- Dry > NDM > Wet
- NDM close to Wet



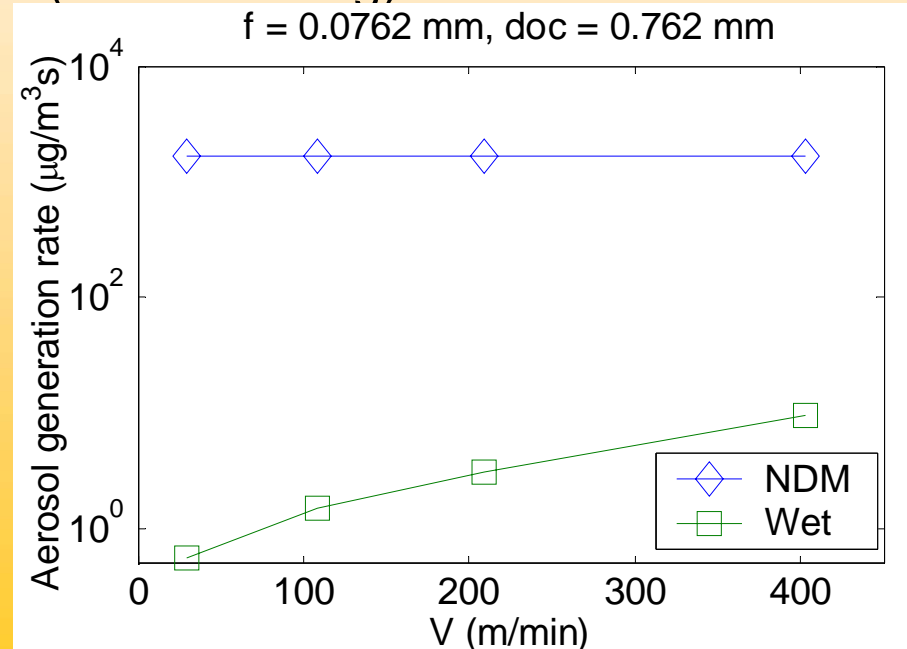
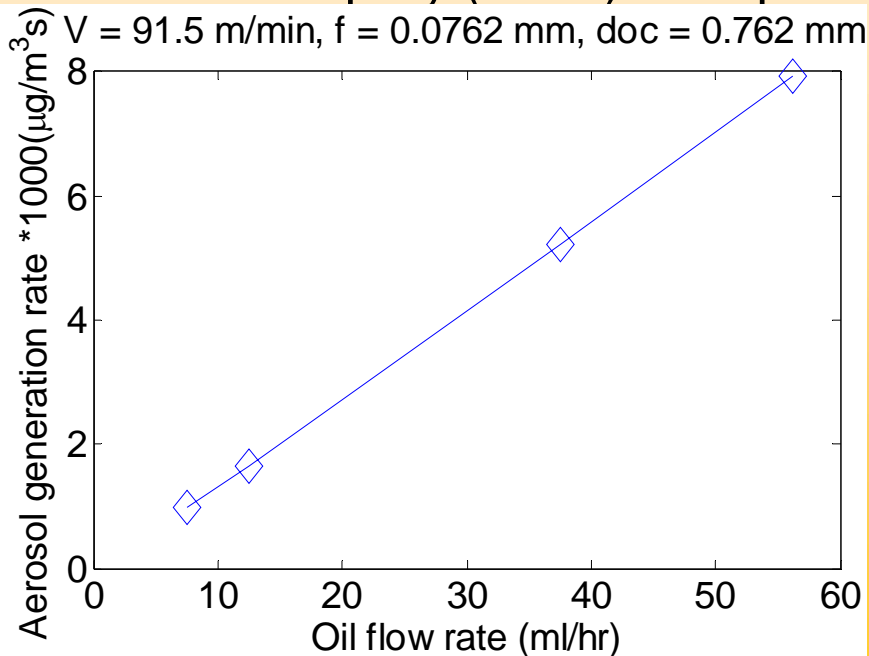
# RESULTS AND DISCUSSIONS (Cont'd)

- Predicted tool flank wear
- Dry > NDM > Wet
- NDM close to Wet
- Significant differences for high cutting velocity



# RESULTS AND DISCUSSIONS (Cont'd)

- Aerosol generation
- Much higher aerosol generation rate under NDM
- Major aerosol generation mechanism
  - Overspray (NDM) VS Spin-off (Flood cooling)





# CONCLUSION

- Analytical models
  - Force, temperature, tool wear and aerosol generation models
- No measured data were required for predicting the tool wear rate
- Consider both **lubricating** and **cooling**
- Different major aerosol generation mechanism for NDM and wet cutting
- Future researches: apply the developed models for different tool/work materials and machining processes



Thank you. Any questions?

