# A Tactical Planning Model for a Job Shop with Unreliable Work Stations and Capacity Constraints 

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#### Abstract

We develop an analytic and a simulation model for a job shop with unreliable work stations and production constraints. In the complex batch manufacturing operation of the factory, smooth production of each work station is required. In the previous work the Tactical Planning Model was proposed for this purpose. In that model, the production of each work station should be proportional to the queueing level of the input work flow. In this paper, the model is extended to the work station with production constraints and with given unreliability of its operation, because in the real world situation, the work stations cannot be operated perfectly without any trouble nor infinite productivity. For the analysis of multiple unreliable work stations, we develop an analytical model and solution. The break down of the work station is modeled as a Bernoulli process. For the analysis with the production constraints with or without the unreliable work station model, we develop a dynamic simulation model. We show some examples of this problem, and show the effect of production constraints and unreliable work stations.


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To my family I dedicated this thesis.

## Chapter 1. Introduction

The purpose of this work is to extend an analytical model and to develop a simulation model of a job shop problem. The focus is on the extension of the Tactical Planning model ${ }^{1}$ to the unreliable multiple work stations with production constraints.

A job shop is a very flexible production facility composed of several machines or work stations. Unlike the assembly line facility, different jobs with various kinds of work flow and completion times are managed in a job shop ${ }^{2}$. An analytical model of job shop problem was proposed by Stephen C. Graves in his "A Tactical Planning Model for a Job Shop" (1985) ${ }^{1}$. He modeled this job shop problem as a network of queues. The work flow was modeled as the discrete-time, continuous-flow of the tasks. The task units were not expressed in terms of the number of parts to be produced but were expressed as the necessary service time to complete the job. The control law for production of each work station was modeled as proportional to the queueing level of the input work flow and as inversely proportional to the planned lead time. The model provides the steady state distribution of the production levels at each work station, the distribution of queue lengths and the distribution of backlogs. In the Tactical Planning Model, Graves took into account the production capability, the inherent variability and uncertainty of the production requirements.

For the production capability, the production constraints were treated implicitly. When the expected level of the production exceeded the capacity of one facility, he increased the number of the facility to satisfy the requirement. For example if the capacity is 2 units of production by one facility and the requirement of the production is 5 , he assumed that there should be three facilities, in parallel, at the
work station. In order to make the variation of the production requirements be within the constraints of the production capability, the planned lead time of the heavily-loaded work station was increased, because the increase of the planned lead time will reduce the variation of the production requirements.
In order to analyze more precisely the situation of the job shop, the saturation of the production without sufficient production capacity should be taken into account. One of the purposes of our research is to investigate this point. We allow the model of heavily-loaded work station if the average requirement of the production is within the capability.

The inherent variation of the production was modeled as an additional independent random input to the work station. But the production itself was assumed to operate properly. For the purpose of the extensive analysis of the job shop problem, we have to consider not only the input variation but also the break down of work stations. In the real world situation, the work station cannot be operated perfectly without any trouble nor infinite productivity. Sometime the work station has to stop its operation because of maintenance, even if it has high reliability. When the work station is stopped, the incoming tasks will be delayed and may result in some backlog. For this problem, the case with single input and single output for the single work station was also analyzed by Graves ${ }^{3}$. He showed that the effect of the work station break down causes a longer expected length of queue and a larger variation in the queue length. In this paper, we extend the unreliable job shop problem to the multiple work stations model with production constraints.

In Chapter 2, we review the outline of the Tactical Planning Model proposed by Graves, and show the model with unreliable multiple work stations and capacity constraints.

In Chapter 3, we demonstrate the dynamic simulation model to examine the performance of the system. For the analysis of the complicated net work of queues, a simulation is the only way to solve this problem without any simplification, because of complicated interactions between work stations and nonlinear constraints. In this paper, we use the software named STELLA ${ }^{\mathrm{TM}}+$ to model and carry out the simulation. STELLA was designed to make it possible to simulate a System Dynamics model on the personal computer ${ }^{4}$. With the application of the software to this problem, the analysis of the complicated network queue problem is completed without the use of the large computer.

In Chapter 4, we show the result of the simulation and analysis. At first we show the validation of the simulation model with no production constraints and perfectly reliable work stations. We compare the result of the simulation to the result of the analytical work. The same job shop model is used as was used in the Graves' paper. It is the ten work stations job shop model for the production of components for grinding machines. After that we show the example of the simulation of the unreliable work stations with the production constraints.
In Chapter 5, we show the conclusion of this analysis and simulation.

[^0]
## Chapter 2. Tactical Planning Model and extension

### 2.1 The Tactical Planning Model

A job shop is a very flexible production facility that consists of a set of versatile machine centers or work stations and is capable of producing a wide variety of jobs. Because of its inherent complexity, it is often difficult to manage the production control in a sophisticated manner. In 1985 Graves ${ }^{1}$ proposed a Tactical Planning Model to help address this problem. He developed the problem by making use of the planned lead time for its production.
In this section we would like to describe briefly about the Tactical Planning Model.

At first we would like to note the basic assumption of the model.
(1) The job shop works as discrete time model.

Every transaction is carried out at the specified time, and production is completed within the given period of time.
(2) The work flow is continuous.

At each work station, the arriving jobs to the station, the queue of work at the station, and the production by the station are expressed in terms of the work load on the station. This differs from the usual queueing model in which these variables would be expressed in terms of number of jobs.
(3) The work station does not break down.
$100 \%$ reliability was assumed.
(4) There are no explicit capacity constraints.

Constraints were considered implicitly.
(5) The arrival stream to a work station contains some degree of uncertainty.

The arrival stream to a work station contains two types of input. One consists of the work flow from the other work stations. The other consists of the random noise which simulates the production variation of the system, and includes new work which enters the shop.

Fig 2.1-1 Example of multiple work stations (Work flow)


The above drawing is the example of the multiple work stations model shown in the Graves article. Jobs arrive to work station \# 1, and leave from work station \# 10. The processing of a job may entail visits to several different work stations.

Second, we would like to describe the relationship and steady state analytical solution of the performance of the model.
In the Tactical Planning model, the production of a work station is set to equal a fraction of the work-in-process (WIP) queue. The control rule is described as follows.

$$
P_{i, t}=\alpha_{i} Q_{i, t}
$$

where $P_{i, t}$ is the production level of the work station $i$, during the time period of $t$, $Q_{i, t}$ is the WIP queue level, and $\alpha_{i}$ is the control parameter of the Tactical Planning model. $\alpha_{i}$ is the inverse of the planned lead time and is restricted to $0<\alpha \leqq 1$. For example if a planned lead time is 4 periods of time then $\alpha_{i}$ is 0.25 . The balance equation is

$$
Q_{i, t}=Q_{i, t-1}-P_{i, t-1}+A_{i, t}
$$

where $A_{i, t}$ is the amount of work that arrives at work station $i$ at the start of time period $t$. These arrivals may come from many other sectors, and the flow from work station $j$ to work station $i$ is modeled by

$$
A_{i, j, t}=\phi_{i j} P_{j, t-1}+\varepsilon_{i, j, t}
$$

where $\phi_{i j}$ is the expected number of hours of work generated for work station $i$ by every hour of work completed by work station $j$, and $\varepsilon_{i, j, t}$ is a random variable with zero mean. The term $\varepsilon_{i, j, t}$ is a noise term which simulates the uncertainty in the arrival stream. It is assumed that the terms of the time series $\left\{\varepsilon_{i, j, t}\right\}$ are i.i.d. The total arrivals to a work station $i$ are the sum over all preceding sectors of equation above.

$$
A_{i, t}=\sum_{j=1}^{n} \phi_{i, f} P_{j, t-1}+\varepsilon_{i, t}
$$

where

$$
\begin{gathered}
\varepsilon_{i, t}=N_{i, t}+\sum_{j=1}^{n} \varepsilon_{i j, t} \\
A_{i, t}=\sum_{j=1}^{n} A_{i, j, t}+N_{i, t}
\end{gathered}
$$

where $N_{i, t}$ is a random variable that represents the work load from new jobs that enter the shop at time $t$ directly from outside. The elements of each time series $\left\{N_{i, t}\right\}$ are assumed to be i.i.d. Thus $\varepsilon_{i, t}$ represents those arrivals that are not predictable
from the previous history and it consists of random noise and new arrivals. By substituting these equations the following vector-matrix equation can be derived.

$$
\mathbf{P}_{\mathrm{t}}=(\mathbf{I}-\mathbf{D}+\mathbf{D} \Phi) \mathbf{P}_{\mathrm{t}-1}+\mathbf{D} \varepsilon_{\mathrm{t}}
$$

where $\mathbf{P}_{\mathrm{t}}$ is the vector of elements $P_{i, t}, \varepsilon_{\mathrm{t}}$ is the vector of elements $\varepsilon_{i, t}, \mathbf{D}$ is the diagonal matrix with the control parameter $a_{i}$ on the diagonal, and $\Phi$ is the matrix whose elements are $\phi_{i, j}, \mathbf{I}$ is the identity matrix. By successively substituting the above formula, the equation can be rewritten as the geometric series

$$
\mathbf{P}_{\mathrm{t}}=\sum_{\mathrm{s}=0}^{\infty}(\mathrm{I}-\mathrm{D}+\mathrm{D} \Phi)^{\mathrm{s}} \mathrm{D} \varepsilon_{\mathrm{t}-\mathrm{s}}
$$

The expectation of production vector, $\rho^{\prime}=\left\{\rho_{1}, \rho_{2}, \ldots \rho_{n}\right\}$ is given by

$$
E\left(\mathbf{P}_{\mathcal{V}}\right)=\rho=\sum_{s=0}^{\infty}(\mathbf{I}-\mathbf{D}+\mathbf{D} \Phi)^{s} \mathbf{D} \mu
$$

where $\mu$ is the expected value of the vector $\varepsilon_{t}$. It was shown that the geometric series converges, provided that the spectral radius (maximal absolute eigenvalue) of the matrix $\Phi$ is less than 1 , which is necessary and sufficient for the spectral radius of ( $\mathbf{I}-\mathbf{D}+\mathrm{D} \Phi)$ to be less than 1 . Then the above equation can be written as the following form.

$$
E\left(\mathbf{P}_{\mathrm{t}}\right)=\rho=(\mathbf{I}-\Phi)^{-1} \mu
$$

The covariance matrix of $\mathbf{P}_{\mathrm{t}}$ is

$$
\operatorname{Var}\left(\mathbf{P}_{\ell}\right)=\sum_{\mathrm{s}=0}^{\infty} \mathbf{B}^{\mathrm{s}} \mathbf{D} \Sigma \mathbf{D} \mathbf{B}^{{ }^{s}}
$$

where $\mathbf{B}=(\mathbf{I}-\mathbf{D}+\mathbf{D} \Phi)$ and $\Sigma$ is the covariance matrix of the vector $\varepsilon_{t}$. The expected queue vector and covariance matrix can be written down as follows.

$$
\begin{aligned}
\mathbf{Q}_{t} & =\mathrm{D}^{-1} \mathbf{P}_{t} \\
\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right) & =\mathrm{D}^{-1} \rho \\
\operatorname{Var}\left(\mathrm{Q}_{\mathrm{t}}\right) & =\mathrm{D}^{-1}\left[\operatorname{Var}\left(\mathbf{P}_{\mathrm{t}}\right)\right] \mathrm{D}^{-1}
\end{aligned}
$$

The queue at each work station is assumed to be served as first in, first out. The oldest input is processed first. The backlog is defined as the portion of the queue that has waited for $m$ periods. Thus, the backlog can be written as the following equation.

$$
\begin{aligned}
& Q_{i t}^{m}=Q_{i, t-1}^{m-1}-P_{i, t-1} \\
& =Q_{i, t-m}-\sum_{s=1}^{m} P_{i, t-s}
\end{aligned}
$$

where $Q_{i t}^{m}<0$ means that paticular backlog is zero, and $Q_{i t}^{m}=Q_{i t}$ for $m=0$. The first term indicates the queueing level at the period of $t-m$ and the second summation is the total production from the time period of $t-m$ up to the last production. Then in matrix notation, we have
$\mathbf{Q}_{\mathrm{t}}^{\mathrm{m}}=\mathbf{D}^{-1} \mathbf{P}_{\mathrm{t}-\mathrm{m}}-\sum_{\mathrm{s}=1}^{\mathrm{m}} \mathbf{P}_{\mathrm{t}-\mathrm{s}}$
and expected backlog is as follows.

$$
E\left(\mathbf{Q}_{\mathrm{t}}^{\mathrm{m}}\right)=\left(\mathbf{D}^{-1}-m \mathbf{I}\right)(\mathbf{I}-\Phi)^{-1} \mu
$$

The covariance of $Q_{i t}^{m}$ can also be found from the previous results.

### 2.2 Unreliable work station

In the previous section, we discussed the model of multiple work stations. There were assumptions that no work station would fail to work, nor would trouble develop. But in the real world situation, the machines in the factory sometimes fail to work, and for some period of time the machines have to be inoperable because of maintenance. The original analysis of the problem was conducted by Graves 3 for a single work station model. In this section, we would like to extend the concept of the unreliable work station to this Tactical Planning Model for multiple work stations.

The definition of work station break down is the condition in which the work station produces nothing for a given period of time. The in-coming material consists of queue in the input side of the work station. The break down of a work station occurs as a Bernoulli process, with the probability $p_{i}$. That is, each period work station $i$ fails with probability $p_{i}$. When a work station fails, its production for that time period is zero. The state of the work station does not provide any influence on the other work stations, neither at its production level nor at the stage of the production.

Let $i$ be the subscript indicating the work station $i$. The work station $i$ has the following relations.

$$
\begin{aligned}
& Q_{i, t}=Q_{i, t-1}-P_{i, t-1}+A_{i, t} \\
& \begin{aligned}
A_{i, t} & =\phi_{i l} P_{1, t-l}+\phi_{i 2} P_{2, t-I}+\ldots+\phi_{i n} P_{n, t-l}+\varepsilon_{i, t} \\
P_{i, t} & =\alpha_{i} Q_{i, t} \quad \\
& -- \text { with probability } \quad 1-p_{i} \\
& =0.0 \quad-- \text { with probability } \quad p_{i}
\end{aligned} \\
& \quad i=1,2, \cdots, n
\end{aligned}
$$

Let $\mathrm{D}_{\mathrm{pt}}$ be the diagonal matrix with $a_{i t}$, which is defined as the random variable

$$
a_{i, t}=\alpha_{i} \quad-- \text { With probability }\left(1-p_{i}\right)
$$

$$
=0 \quad-- \text { With probability } p_{i}
$$

$$
\mathbf{D}_{\mathrm{p} \mathrm{p}}=\left[\begin{array}{cccc}
a_{1, t} & 0 & - & 0 \\
0 & a_{2, t} & - & 0 \\
- & - & - & 0 \\
0 & 0 & 0 & a_{n, t}
\end{array}\right]
$$

$p_{i}$ denotes the probability of work station break down. This random variable has following characteristics.

$$
\begin{aligned}
& E\left(a_{i t}\right)=\alpha_{i}\left(1-p_{i}\right) \\
& E\left(a_{i t}{ }^{2}\right)=\alpha_{i}^{2}\left(1-p_{i}\right) \\
& \operatorname{Var}\left(a_{i t}\right)=\alpha_{i}^{2} p_{i}\left(1-p_{i}\right) \\
& E\left(a_{i t} a_{j t}\right)=\alpha_{i} \alpha_{j}\left(1-p_{i}\right)\left(1-p_{j}\right) ; i \neq j \\
& E\left(a_{i t} a_{i t-s}\right)=\alpha_{i}^{2}\left(1-p_{i}\right)^{2} ; s \neq 0 \\
& E\left(a_{i t} X_{i t}\right)=\alpha_{i}\left(1-p_{i}\right) E\left(X_{i t}\right) ; X_{i t} \text { is independent from } a_{i t} \\
& E\left(\mathrm{D}_{\mathrm{p} t}=\left[\begin{array}{ccc}
\alpha_{1}\left(1-p_{1}\right) & 0 & - \\
0 & \alpha_{2}\left(1-p_{2}\right) & - \\
- & - & - \\
0 & 0 & - \\
0 & - \\
\quad \\
=\mathrm{D}\left(\mathrm{I}-\mathrm{P}_{\mathrm{r}}\right)
\end{array}\right.\right.
\end{aligned}
$$

$\mathbf{P}_{\mathrm{r}}$ denotes a diagonal matrix with elements, $\left\{p_{1}, p_{2}, \ldots, p_{n}\right\}$, and $\mathbf{D}$ denotes a diagonal matrix with its elements being the of inverse of planned lead time, $\left\{\alpha_{1}, \alpha_{2}, \ldots, \alpha_{n}\right\}$. Now the job shop system can be analyzed by the following set of equations:

The control rule is now

$$
P_{t}=D_{p t} Q_{t}
$$

The balance equation is then

$$
\begin{aligned}
\mathbf{Q}_{\mathrm{t}} & =\mathrm{Q}_{\mathrm{t}-1}-\mathbf{P}_{\mathrm{t}-1}+\mathbf{A}_{\mathrm{t}} \\
& =\mathrm{Q}_{\mathrm{t}-1}-\mathbf{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1}+\Phi \mathrm{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1}+\varepsilon_{\mathrm{t}} \\
& =\varepsilon_{\mathrm{t}}+\left\{\mathbf{I}-(\mathbf{I}-\Phi) \mathbf{D}_{\mathrm{pt}-1}\right\} \mathrm{Q}_{\mathrm{t}-1} \\
& \Phi=\left[\begin{array}{ccc}
\phi_{11} \phi_{12} & -\phi_{1 n} \\
\phi_{21} \phi_{22} & -\phi_{2 n} \\
- & - & - \\
\phi_{n 1} \phi_{n 2} & -\phi_{n n}
\end{array}\right]
\end{aligned}
$$

2.2.1 The average and variance of queue

The expectation of queue can be derived by taking expectation of both sides.

$$
\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right)=\mathrm{E}\left(\varepsilon_{\mathrm{t}}\right)+\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{E}\left(\mathrm{D}_{\mathrm{pt}-1}\right)\right\} \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right)
$$

At the steady state condition, the expectations of $\mathbf{Q}_{\mathrm{t}}$ and $\mathrm{Q}_{\mathrm{t}-1}$ are the same. $\left\{\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right)=\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right)\right\}$ Therefore

$$
\begin{aligned}
\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right) & =\left\{(\mathrm{I}-\Phi) \mathrm{E}\left(\mathrm{D}_{\mathrm{pt}-1}\right)\right\}^{-1} \mathrm{E}\left(\varepsilon_{\mathrm{t}}\right) \\
& =\left\{(\mathrm{I}-\Phi) \mathrm{D}\left(\mathrm{I}-\mathrm{P}_{\mathrm{r}}\right)\right\}^{-1} \mu
\end{aligned}
$$

The covariance matrix can be obtained by the following manner. At first a quadratic form of $\mathrm{Q}_{\mathrm{t}}$ should be taken. The form consists of NxN matrix.

$$
\mathrm{Q}_{\mathbf{\imath}} \mathbf{Q}_{\mathrm{t}}^{\mathrm{T}}=\left[\begin{array}{cccc}
Q_{1,2} Q_{1, t} & Q_{1,,} Q_{2, t} & - & Q_{1, Q_{n, t}} \\
Q_{2, Q_{1, t}} & Q_{2, Q} Q_{2, t} & - & Q_{2, t} Q_{n, t} \\
- & - & - & - \\
Q_{n, 2} Q_{1, t} & Q_{n,} Q_{2, t} & - & Q_{n, 1} Q_{n, t}
\end{array}\right]
$$

which is expressed as following form.

$$
\begin{aligned}
\mathrm{Q}_{\mathrm{t}} \mathrm{Q}_{\mathrm{t}}^{\mathrm{T}}= & \left(\varepsilon_{\mathrm{t}}+\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\} \mathrm{Q}_{\mathrm{t}-1}\right)\left(\varepsilon_{\mathrm{t}}+\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\} \mathrm{Q}_{\mathrm{t}-1}\right)^{\mathrm{T}} \\
= & \varepsilon_{\mathrm{t}} \varepsilon_{\mathrm{t}} \mathrm{~T}^{+}+\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\} \mathrm{Q}_{\mathrm{t}-1} \varepsilon_{\mathrm{t}} \mathrm{~T}_{+} \varepsilon_{\mathrm{t}} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\}^{\mathrm{T}} \\
& +\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\} \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\}^{\mathrm{T}} \\
= & \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}-\left(\mathrm{I}-(\mathrm{D}) \mathrm{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{-} \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{D}_{\mathrm{pt}-1}} \mathrm{~T}_{(\mathrm{I}-\Phi)} \mathrm{T}^{\mathrm{T}}\right.
\end{aligned}
$$

$$
\begin{aligned}
& +(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{pt}-1} \mathrm{~T}(\mathrm{I}-\Phi)^{\mathrm{T}} \\
& +\varepsilon_{\mathrm{t}} \varepsilon_{\mathrm{t}}^{\mathrm{T}}+\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\} \mathrm{Q}_{\mathrm{t}-1} \varepsilon_{\mathrm{t}} \mathrm{~T}+\varepsilon_{\mathrm{t}} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{\left\{\mathrm{I}-(\mathrm{I}-\Phi) \mathrm{D}_{\mathrm{pt}-1}\right\}^{\mathrm{T}}}
\end{aligned}
$$

The expectation of this quadratic form is following.

$$
\begin{aligned}
& \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}} \mathrm{Q}_{\mathrm{t}} \mathrm{~T}^{\mathrm{T}}\right)=\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}^{\mathrm{T}}\right)+\mathrm{E}\left(\varepsilon_{\mathrm{t}} \varepsilon_{\mathrm{t}}^{\mathrm{T}}\right) \\
& -(I-\Phi) E\left(D_{p t-1} Q_{t-1} Q_{t-1} T\right)-E\left(Q_{t-1} Q_{t-1} T_{D t-1} T\right)(I-\Phi)^{T} \\
& +(\mathrm{I}-\Phi) \mathrm{E}\left(\mathrm{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{pt}-1} \mathrm{D}^{\mathrm{T}}\right)(\mathrm{I}-\Phi)^{\mathrm{T}}+\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \varepsilon_{\mathrm{t}} \mathrm{~T}\right) \\
& -(I-\Phi) E\left(D_{p t-1} Q_{t-1} \varepsilon_{t}^{T}\right)+E\left(\varepsilon_{t} Q_{t-1}^{T}\right)-E\left(\varepsilon_{t} Q_{t-1}{ }^{T} D_{p t-1}^{T}\right)(I-\Phi)^{T}
\end{aligned}
$$

As $\varepsilon_{\mathrm{t}}, \mathbf{Q}_{\mathrm{t}-1}$ and $\mathbf{D}_{\mathrm{pt}-1}$ are mutually independent, the expectation of mutual products are the products of mutual expectation.

$$
\begin{aligned}
& \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}} \mathrm{Q}_{\mathrm{t}} \mathrm{~T}^{\mathrm{T}}\right)=\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}^{\mathrm{T}}\right)+\mathrm{E}\left(\varepsilon_{\mathrm{t}} \varepsilon_{\mathrm{t}}^{\mathrm{T}}\right) \\
& -(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1} Q_{t-1}{ }^{T}\right)-E\left(Q_{t-1} Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi)^{T} \\
& +(I-\Phi) E\left(D_{p t-1} \mathbf{Q}_{t-1} \mathbf{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{pt}-1} \mathrm{~T}^{2}\right)(\mathrm{I}-\Phi)^{\mathrm{T}}+\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\varepsilon_{\mathrm{t}} \mathrm{~T}^{\mathrm{T}}\right)+\mathrm{E}\left(\varepsilon_{\mathrm{t}}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}^{\mathrm{T}}\right) \\
& -(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(\varepsilon_{t}^{T}\right)-E\left(\varepsilon_{t}\right) E\left(Q_{t-1}^{T}\right) E\left(D_{p t-1}^{T}\right)(I-\Phi)^{T}
\end{aligned}
$$

On the other hand $\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right) \mathrm{E}\left(\mathbf{Q}_{\mathrm{t}} \mathrm{T}^{\mathbf{T}}\right)$ is as follows.

$$
\begin{aligned}
& \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}{ }^{\mathrm{T}}\right)=\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}^{\mathrm{T}}\right)+\mathrm{E}\left(\varepsilon_{\mathrm{t}}\right) \mathrm{E}\left(\varepsilon_{\mathrm{t}}{ }^{\mathrm{T}}\right) \\
& -(I-\Phi) E\left(D_{p t-1} Q_{t-1}\right) E\left(Q_{t-1} T^{T}\right)-E\left(Q_{t-1}\right) E\left(Q_{t-1} T_{p t-1}^{T}\right)(I-\Phi)^{T} \\
& +(\mathbf{I}-\Phi) E\left(\mathbf{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{D}} \mathrm{D}_{\mathrm{pt}-1} \mathrm{~T}\right)(\mathrm{I}-\Phi)^{\mathrm{T}}+\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\varepsilon_{\mathrm{t}} \mathrm{~T}\right) \\
& -(I-\Phi) E\left(D_{p t-1} Q_{t-1}\right) E\left(\varepsilon_{t} T^{T}\right)+E\left(\varepsilon_{t}\right) E\left(Q_{t-1}^{T}\right)-E\left(\varepsilon_{t}\right) E\left(Q_{t-1} T_{p t-1}^{T}\right)(I-\Phi)^{T} \\
& =\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}\right)+\mathrm{E}\left(\varepsilon_{\mathrm{t}}\right) \mathrm{E}\left(\varepsilon_{\mathrm{t}} \mathrm{~T}^{\mathrm{T}}\right) \\
& -(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(Q_{t-1}{ }^{T}\right)-E\left(Q_{t-1}\right) E\left(Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi)^{T} \\
& +(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi) T \\
& +E\left(Q_{t-1}\right) E\left(\varepsilon_{t}^{T}\right) \quad-(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(\varepsilon_{t}^{T}\right)+E\left(\varepsilon_{t}\right) E\left(Q_{t-1} T\right) \\
& -E\left(\varepsilon_{t}\right) E\left(Q_{t-1}^{T}\right) E\left(D_{p t-1}^{T}\right)(I-\Phi)^{T}
\end{aligned}
$$

The covariance matrix of $Q_{t}$ can be calculated as the difference between $E\left(Q_{t} Q_{t} T\right)$ and $\mathrm{E}\left(\mathrm{Q}_{\mathrm{t}}\right) \mathrm{E}\left(\mathbf{Q}_{t}{ }^{T}\right)$. The diagonal elements of the matrix consist of variance of $\mathrm{Q}_{i t}$ and the other elements consist of covariance of $\mathrm{Q}_{\mathrm{it}}$ and $\mathrm{Q}_{\mathrm{jt}}$.

$$
\begin{aligned}
& \operatorname{Var}\left(Q_{t}\right)= E\left(Q_{t} Q_{t} T_{)}-E\left(Q_{t}\right) E\left(Q_{t}^{T}\right)\right. \\
&= E\left(Q_{t-1} Q_{t-1}^{T}\right)+E\left(\varepsilon_{t} \varepsilon_{t}^{T}\right) \\
&-(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1} Q_{t-1} T\right)-E\left(Q_{t-1} Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi)^{T} \\
&+(I-\Phi) E\left(D_{p t-1} Q_{t-1} Q_{t-1} T_{p t-1}^{T}\right)(I-\Phi)^{T}+E\left(Q_{t-1}\right) E\left(\varepsilon_{t} T\right) \\
&-(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(\varepsilon_{t} T\right)+E\left(\varepsilon_{t}\right) E\left(Q_{t-1} T\right) \\
&-E\left(\varepsilon_{t}\right) E\left(Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi)^{T} \\
&-\left\{E\left(Q_{t-1}\right) E\left(Q_{t-1} T\right)+E\left(\varepsilon_{t}\right) E\left(\varepsilon_{t} T\right)\right. \\
&-(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(Q_{t-1} T\right)-E\left(Q_{t-1}\right) E\left(Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi)^{T} \\
&+(I-\Phi) E\left(D_{p t-1}\right) E\left(Q_{t-1}\right) E\left(Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi)^{T}+E\left(Q_{t-1}\right) E\left(\varepsilon_{t} T\right) \\
&-(I-\Phi) E\left(D_{p t}\right) E\left(Q_{t-1}\right) E\left(\varepsilon_{t}^{T}\right)+E\left(\varepsilon_{t}\right) E\left(Q_{t-1} T\right) \\
&\left.-E\left(\varepsilon_{t}\right) E\left(Q_{t-1} T\right) E\left(D_{p t-1} T\right)(I-\Phi) T\right\}
\end{aligned}
$$

$$
=\operatorname{Var}\left(\mathrm{Q}_{\mathrm{t}-1}\right)+\operatorname{Var}\left(\varepsilon_{\mathrm{t}}\right)-(\mathrm{I}-\Phi) \mathrm{E}\left(\mathbf{D}_{\mathrm{pt}-1}\right) \operatorname{Var}\left(\mathrm{Q}_{\mathrm{t}-1}\right)-\operatorname{Var}\left(\mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathrm{D}_{\mathrm{pt}-1} \mathrm{~T}\right)(\mathrm{I}-\Phi)^{\mathrm{T}}
$$

$$
+(\mathrm{I}-\Phi)\left\{\mathrm{E}\left(\mathbf{D}_{\mathrm{pt}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{pt}-1} \mathrm{~T}^{\mathrm{T}}\right)-\mathrm{E}\left(\mathrm{D}_{\mathrm{pt}-1}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathrm{Q}_{\mathrm{t}-1} \mathrm{~T}_{)} \mathrm{E}\left(\mathbf{D}_{\mathrm{pt}-1} \mathrm{~T}_{)}\right)\right\}(\mathrm{I}-\Phi)^{\mathrm{T}}\right.
$$

The product of $D_{p t} Q_{t}$ and $Q_{t}{ }^{T} D_{p t} T^{T}$ is expressed by using the following formula. $D_{p t} Q_{t} Q_{t} T_{p t}{ }^{T}=$

Then the expectation of $D_{p t-1} Q_{t-1} Q_{t-1} T_{p t-1} T$ is

## $E\left(D_{p t-1} Q_{t-1} Q_{t-1} \mathrm{D}_{p t-1} T^{T}\right)=$

$$
\left[\begin{array}{cccc}
\overline{Q_{1, t-1}^{2}} \alpha_{1}^{2} p_{11}^{*} & \overline{Q_{1, t-1} Q_{2, t-1}} \alpha_{1} \alpha_{2} p_{12}^{*} & - & \overline{Q_{1, t-1} Q_{n, t-1}} \alpha_{1} \alpha_{n} p_{1 n}^{*} \\
\overline{Q_{2, t-1} Q_{1, t-1}} \alpha_{2} \alpha_{1} p_{21}^{*} & \overline{Q_{2, t-1}^{2}} \alpha_{2}^{2} p_{22}^{*} & - & \overline{Q_{2, t-1} Q_{n, t-1}} \alpha_{2} \alpha_{n} p_{2 n}^{*} \\
- & - & - & - \\
\overline{Q_{n, t-1} Q_{1, t-1}} \alpha_{n} \alpha_{1} p_{n 1}^{*} & \frac{-}{Q_{n, t-1} Q_{2, t-1}} \alpha_{n} \alpha_{2} p_{n 2}^{*} & - & \overline{Q_{n, t-1}^{2}} \alpha_{n}^{2} p_{n n}^{*}
\end{array}\right]
$$

where the probability $p_{i j}{ }^{*}$ denotes the joint probability that the pair of work stations is not broken down.

$$
\begin{aligned}
& p_{i i}^{*}=\left(1-p_{i}\right) \\
& p_{i j}^{*}=\left(l-p_{i}\right)\left(1-p_{j}\right) ; i \neq j
\end{aligned}
$$

Let $\mathbf{e}_{\mathrm{ij}}$ be matrix of only the $(i, j)$ element has value 1 , and all other elements are 0 . For example, $\mathbf{e}_{23}$ means

$$
\mathbf{e}_{23}=\left(\begin{array}{llll}
0 & 0 & 0 & 0 \\
0 & 0 & 1 & 0 \\
0 & 0 & 0 & 0 \\
0 & 0 & 0 & 0
\end{array}\right)
$$

Then the third term is as follows

$$
\begin{aligned}
& \mathrm{E}\left(\mathbf{D}_{\mathrm{pt}-1} \mathbf{Q}_{\mathrm{t}-1} \mathbf{Q}_{\mathrm{t}-1} \mathrm{~T}_{\mathrm{D} \mathrm{pt}-1} \mathrm{~T}\right)-\mathrm{E}\left(\mathbf{D}_{\mathrm{pt}-1}\right) \mathrm{E}\left(\mathbf{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathbf{Q}_{\mathrm{t}-1} \mathrm{~T}\right) \mathrm{E}\left(\mathbf{D}_{\mathrm{pt}-1} \mathrm{~T}\right) \\
& \quad=\sum_{i=1}^{n} \alpha_{i}^{2}\left\{\left(1-p_{i}\right) \overline{Q_{i, t-1}^{2}-\left(1-p_{i}\right)} \bar{Q}_{i, t-1}^{2}\right\} \mathrm{e}_{\mathrm{ii}} \\
& \quad+\sum_{i=1}^{n} \sum_{j=1, j \neq i}^{n} \alpha_{i} \alpha_{j}\left(1-p_{j}\right)\left(1-p_{j}\right)\left\{\overline{Q_{i, t-1} Q_{j, t-1}} \bar{Q}_{i, t-1} \bar{Q}_{j, t-1}\right\} \mathrm{e}_{\mathrm{ij}} \\
& =\sum_{i=1}^{n} \alpha_{i}^{2} p_{i}\left(1-p_{i}\right)\left\{\operatorname{Var}\left(Q_{i, t-1}\right)+\bar{Q}_{i, t-1}^{2}\right\} \mathrm{e}_{\mathrm{ii}}
\end{aligned}
$$

$$
\begin{aligned}
& +\sum_{i=1}^{n}\left\{\alpha_{i}^{2}\left(1-p_{i}\right)^{2} \operatorname{Var}\left(Q_{i, t-1}\right) \mathbf{e}_{\mathrm{i}+} \sum_{j=1, j \neq i}^{n} \alpha_{i} \alpha_{j}\left(1-p_{i}\right)\left(1-p_{j}\right) \operatorname{Cov}\left(Q_{i, t-1}, Q_{j, t-1}\right) \mathbf{e}_{\mathrm{ij}}\right\} \\
= & \sum_{i=1}^{n} \alpha_{i}^{2} p_{i}\left(1-p_{j}\right)\left\{\operatorname{Var}\left(Q_{i, t-1}\right)+\bar{Q}_{i, t-1}^{2}\right\} \mathbf{e}_{\mathrm{ii}}+\mathrm{E}\left(\mathbf{D}_{\mathrm{p} t}\right) \operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}-1}\right) \mathrm{E}\left(\mathbf{D}_{\mathrm{pt}}{ }^{\mathrm{T}}\right) \\
= & \mathrm{D} \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right) \mathrm{P}_{\mathrm{r}} \mathrm{E}_{2}\left(\mathbf{Q}_{\mathrm{t}-1}\right)+\mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right) \operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}-1}\right)\left(\mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\right)^{\mathrm{T}}
\end{aligned}
$$

$\mathrm{E}_{2}\left(\mathrm{Q}_{\mathrm{t}-1}\right)$ denotes diagonal matrix consists of the expectation of square of $\mathrm{Q}_{\mathrm{i}, \mathrm{t}-1}$.
$\left\{\mathbf{E}_{2}\left(\mathbf{Q}_{\mathrm{t}-1}\right)\right\}_{\mathrm{ii}}=E\left(Q_{i, t-1}\right)=\operatorname{Var}\left(Q_{i, t-1}\right)+E\left(Q_{i, t-1}\right)^{2}$

The covariance matrix of $Q_{t}$ is expressed as the following form.

$$
\begin{aligned}
& \operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}}\right)=\operatorname{Var}\left(\varepsilon_{\mathrm{t}}\right) \\
& \quad+\left\{\mathbf{I}-(\mathbf{I}-\Phi) \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\right\} \operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}-1}\right)\left\{\mathbf{I}-(\mathbf{I}-\Phi) \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\right\}^{\mathrm{T}} \\
& \quad+(\mathbf{I}-\Phi) \mathbf{D} \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right) \mathbf{P}_{\mathrm{r}} \mathbf{E}_{2}\left(\mathbf{Q}_{\mathrm{t}-1}\right)(\mathbf{I}-\Phi)^{\mathrm{T}}
\end{aligned}
$$

In order to get the steady state solution, let $\operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}}{ }^{\mathrm{k}}\right)$ be the k -th asymptotical solution. The first approximate solution is

$$
\operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}}^{1}\right)=\operatorname{Var}\left(\varepsilon_{\mathrm{t}}\right)+(\mathbf{I}-\Phi) \mathbf{D} \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right) \mathbf{P}_{\mathrm{r}} \mathbf{E}_{2}\left(\mathbf{Q}_{\mathrm{t}}^{0}\right)(\mathbf{I}-\Phi)^{\mathrm{T}}
$$

where $\mathbf{E}_{2}\left(\mathrm{Q}_{\mathrm{t}}{ }^{0}\right)$ is expressed as

$$
\left(\mathrm{E}_{2}\left(\mathrm{Q}_{\mathrm{t}-1}^{0}\right)\right)_{\mathrm{ii}}=E\left(Q_{i, t}\right)^{2}
$$

The k -th asymptotical solution is as follows.

$$
\begin{aligned}
& \operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}}^{\mathrm{k}}\right)=\operatorname{Var}\left(\varepsilon_{\mathrm{t}}\right) \\
& \quad+\left\{\mathbf{I}-(\mathbf{I}-\Phi) \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\right\} \operatorname{Var}\left(\mathbf{Q}^{\mathrm{k}-1}\right)\left\{\mathbf{I}-(\mathbf{I}-\Phi) \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\right\}^{\mathrm{T}} \\
& \quad+(\mathbf{I}-\Phi) \mathbf{D} \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right) \mathbf{P}_{\mathrm{r}} \mathbf{E}_{2}\left(\mathbf{Q}_{\mathrm{t}}^{\mathrm{k}-1}\right)(\mathbf{I}-\Phi)^{\mathrm{T}} \\
& \left\{\mathbf{E}_{2}\left(\mathbf{Q}_{\mathrm{t}}^{\mathrm{k}-1}\right)\right\}_{\mathrm{ii}}=E\left(\left(Q_{i}^{k-1}\right)^{2}\right)=\operatorname{Var}\left(Q_{i}^{k-1}\right)+E\left(Q_{i, t}\right)^{2}
\end{aligned}
$$

The aymptotical solution will converge if it can be shown that a finite K such that

$$
\left\|\operatorname{Var}\left(\mathbf{Q}_{\mathrm{t}}^{\mathrm{k}}\right)-\operatorname{Var}\left(\mathrm{Q}_{\mathrm{t}}^{\mathrm{k}-1}\right)\right\|<\left\|\operatorname{Var}\left(\mathrm{Q}_{\mathrm{t}}^{\mathrm{k}-1}\right)-\operatorname{Var}\left(\mathrm{Q}^{\mathrm{k}-2}\right)\right\|
$$

for all $\mathrm{k}>\mathrm{K}$.
2.2.2. The average and variance of production

As described above, the relationship between production and queue is defined in the Tactical Planning Model. It is

$$
\begin{array}{rlr}
P_{i, t}=\alpha_{i} Q_{i, t} & -- \text { with probability } & 1-p_{i} \\
& =0.0 & -- \text { with probability }
\end{array} p_{i}
$$

Therefore the average and the square average are calculated without any difficulty.

$$
\begin{aligned}
& E\left(P_{i, t}\right)=\left(1-p_{i}\right) \alpha_{i} E\left(Q_{i, t}\right) \\
& E\left(P_{i, t^{2}}\right)=\left(1-p_{i}\right)\left(\alpha_{i}\right)^{2} E\left(\left(Q_{i, t}\right)^{2}\right) \\
& \operatorname{Var}\left(P_{i, t}\right)=\left(1-p_{i}\right)\left(\alpha_{i}\right)^{2}\left[\operatorname{Var}\left(Q_{i i, t}\right)-p_{i} E\left(Q_{i, t}\right)^{2}\right]
\end{aligned}
$$

Using the result of the previous section, expectation of production can be written as

$$
\begin{aligned}
\mathrm{E}\left(\mathbf{P}_{\mathrm{t}}\right) & =\mathrm{E}\left(\mathrm{D}_{\mathrm{pt}}\right)\left\{(\mathbf{I}-\Phi) \mathrm{E}\left(\mathrm{D}_{\mathrm{pt}}\right)\right\}^{-1} \mathrm{E}\left(\varepsilon_{\mathrm{t}}\right) \\
& =\mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\left\{(\mathbf{I}-\Phi) \mathbf{D}\left(\mathbf{I}-\mathbf{P}_{\mathrm{r}}\right)\right\}^{-1} \mu \\
& =(\mathbf{I}-\Phi)^{-1} \mu
\end{aligned}
$$

This equation shows that the expectation of the production does not depend on the unreliability of the work station for the long run.

### 2.3 Capacity Constraints

In the original Tactical Planning Model, the effect of the production constraints were treated as an implicit factor. It can be avoided by setting appropriate planned lead time and resource reallocation. But in the model discussed in the previous section, the explicit involvement of the production control should be taken into account, because after the work station break down, the queue of the station will increase, and it is likely that the production will exceed the production capacity.
Therefore we apply the following production capacity constraint in each work station.

$$
P_{i \Gamma}=\min \left\{\alpha_{i} Q_{i t} P_{c, i t}\right\}
$$

In this case $P_{c, i t}$ is the production capability at work center $i$ in time period $t$. This type of rule was tested by simulation by Cruickshanks, Drescher and Graves (1984) ${ }^{5}$ for a simpler case with one production stage. We apply this rule in the multiple work station case and see the effect by the use of dynamic simulation.

## Chapter 3. Simulation model.

### 3.1 Systems dynamics simulation

In this paper, we use a personal computer in order to carry out the analytical calculation and Monte Carlo simulation, because the development of the personal computer has made it possible for the manager to have his/her own tool to evaluate the management problems. As for the analytical approach described in the chapter 2, we use BASIC to model and implement the problem. The detail of the program is described in Appendix B. In this analytical approach, we model the unreliable job shop without the explicit production constraints. Because it is very difficult to apply analytical approach to the model with explicit constraints, we apply the dynamic simulation model to solve this problem.
There are several software packages available to carry out a simulation. For example, Banks and Carson ${ }^{5}$ describe GASP, SIMSCRIPT, GPSS, and SLAM as the special purpose simulation language. In this paper, we select the STELLA program to do simulation on the personal computer.
The STELLA, designed by Barry Richmond ${ }^{3}$, is a software to simulate the dynamics of social and physical systems. It stands for Structural Thinking, Experiential Learning Laboratory with Animation. It solves systems of differential or difference equations using the following operaters; Stock, Flow \& Flow Regulator, Input Link and Converter.
The first operator, Stock, is the variable to be differentiated by time. Let the differential equation be

$$
\frac{d x}{d t}=a y-b z
$$

where the stock should be $x$. When we want to represent a difference equation, such as a balance equation

$$
X_{i}=X_{i-1}+A_{i}-B_{i}
$$

the stock represents $X_{i}$.
The second operator, Flow and Flow Regulater, has two varieties. One is Source and Logic Receptacle. It represents "ay " of the above differential equation and can be interpretted as the "arrival" rate to the stock. The other is Sink and Logic Receptacle. It represents " $b z$ " and corresponds to the "departure rate" from the stock. The Logic Receptacle works as a control valve of the flow, and we can process the signal to the form of arrival and departure of the differential equations. An infinite amount of flow is assumed in the source. The sink is also assumed to have an infinite capability.

The third operater is Input Link which is the directed arc of the signal flow. In the above differential equation, Input Link brings the output of some other equation " $y$ " and " $z$ " to the Flow and Flow Regulator. In general it indicates signal flow relationship between one operator to another.
The fourth operator is a Converter. It converts several inputs into another form. Mathematical function, some logical operation, random variable generation can be used in this operator.

We can use these operators to make a simulation model of this problem.
Fig 3.1.1
Stock Flow \& Flow Regulator Input Link Converter


Source \& Sink \&
Logic Logic
Receptacle Receptacle

### 3.2 STELLA model

### 3.2.1 Multiple work stations model

In this section, we would like to show the multiple work stations simulation model in the Tactical Planning model. The following chart shows the example of work flow between the work stations.

Fig 3.2.1-1 Work Flow example


As described in Chapter 2, the balance equation of the each work station, in this case the \# i work station, is as follows

$$
\begin{aligned}
& Q_{i, t}=Q_{i, t-1}-P_{i, t-1}+A_{i, t} \\
& \qquad \begin{aligned}
& A_{i, t}=\phi_{i l} P_{1, t-1}+\phi_{i 2} P_{2, t-1}+\ldots+\phi_{i n} P_{n, t-1}+\varepsilon_{i, t} \\
& P_{i, t}=\alpha_{i} Q_{i, t} \\
&--- \text { with probability } \quad 1-p_{i} \\
&=0.0 \\
& \quad--- \text { with probability } \quad p_{i}
\end{aligned}
\end{aligned}
$$

Each work station has multiple inputs from the other work stations, $A_{i, t}$, and then its output(production: $P_{i, t}$ ) goes to several work stations.
The station receives the input flow with uncertain random inputs.
In this example, work station \#1 is the first work station which receives the initial material from the outside of the system. It also receives the work flow from work stations \#3 and \#5. The work flow goes to the other stations, work stations \#2, \#3, \#4, \#5 and \#8. After several stages, some of the work load goes back to the work station \#1 again.

The following shows the example of the work station model described by the STELLA operators. The noise term of the flow, $\varepsilon_{i, t}$, is modeled as the combination of gaussian normal noise and constant term.

Fig 3.2.1-2

3.2.2 Work station break down and the production constraints model

As discussed in Chapter 2 the unreliability of the work station is the probability of work station break down. When the work station breaks down, the productive activity will stop. The work in process inventory will be increased. The inverse of planned lead time, $\alpha_{i}$, is modeled as a Bernoulli random variable $\mathrm{a}_{\mathrm{i}, \mathrm{t}}$ as discussed in 2.2.

$$
\begin{array}{rrrr}
P_{i, t}=\alpha_{i} Q_{i, t} & --- \text { with probability } & 1-p_{i} \\
& =0.0 & & -- \text { with probability } \\
\leftrightarrow & p_{i} \\
\leftrightarrow P_{i, t}=a_{i, t} Q_{i, t} & & \\
a_{i, t}=\alpha_{i} & & -- \text { with probability } & 1-p_{i} \\
& =0.0 & \text {--- with probability } & p_{i}
\end{array}
$$

Fig 3.2.2.-1 unreliable work station


The production constraint is modeled as the simple constraint. If the level of the production given by the control rule exceeds the maximum capacity of the work station, the actual production is set to the maximum capacity.

$$
P_{i \sigma}=\min \left\{\alpha_{i} Q_{i v} P_{c, i t}\right\}
$$

where $P_{C, i t}$ is the maximam capacity of production of work station \# i.
In the STELLA simulation model, the unreliable work station is modeled by comparing a uniformly distributed random variable to a threshold level to decide working(1) or not working(0). If the random variable is more than $\mathrm{p}_{\mathrm{i}}$, the production is decided to be normal. This process is modeled in the node "Conversion". The production constraint is modeled as an "if" sentence. (IF required Production level is greater than the maximam value, let P be the maximum production.)

Fig3.2.2-2 STELLA model of work station break down and Production constrains


Work station break down Production constraints


### 3.2.3 Backlog model

The backlog is defined as the amount of the queue that has waited $m$ or more periods, for $m=0,1,2, \cdots n$. For a given $m$ units of time, then the backlog is defined by the following equation.

$$
\begin{aligned}
Q_{i t}^{m} & =Q_{i, t-1}^{m-1}-P_{i, t-1} \\
& =Q_{i, t-m}-\sum_{s=1}^{m} P_{i, t-s}
\end{aligned}
$$

For example, when the planned lead time $m$ is 3 , the equation can be written as the following flow chart. It needs $Q_{i, t-3}$, and the past three periods of production level.

Fig. 3.2.3-1
Backlog model
Example m=3


In the STELLA model, the lag element can be modeled by applying a STACK element. As the output of the lag element in time period of $t$ should be the input of the lag element at time $t-1$, the relation can be modeled as follows.

$$
\begin{gathered}
Q_{\operatorname{lag}(n), i, t}=Q_{\operatorname{lag}}(n), i, t-1+\left(Q_{\operatorname{lag}(n-1), i, t-1}-Q_{\operatorname{lag}(n), i, t-1}\right) \\
Q_{\operatorname{lag}(1), i, t}=Q_{\operatorname{lag}(1), i, t-1}+\left(Q_{i, t-1}-Q_{\operatorname{lag}(1), i, t-1}\right)
\end{gathered}
$$

$$
\begin{gathered}
P_{\operatorname{lag}(n), i, t}=P_{\operatorname{lag}(n), i, t-1}+\left(P_{\operatorname{lag}(n-1), i, t-1}-P_{\operatorname{lag}(n), i, t-1}\right) \\
P_{\operatorname{lag}(1), i, t}=P_{\operatorname{lag}(1), i, t-1}+\left(P_{i, t-1}-P_{\operatorname{lag}(1), i, t-1}\right)
\end{gathered}
$$

Then the flow diagram of the back log is represented as in the next figure.
Fig. 3.2.3-2


### 3.2.4 Output process

In order to evaluate the performance of the work station, it is necessary to take expectation and variance of the production and queue. Let $x$ be either production or queue, then $E(x)$, the expectation of $x$, and $\operatorname{Var}(x)$, the variance of $x$, are

$$
\begin{aligned}
E(x) & =\frac{1}{n} \sum_{i=1}^{n} x_{i} \\
\operatorname{Var}(x) & =\frac{1}{n-1} \sum_{i=1}^{n}\left(x_{i}-E(x)\right)^{2} \\
& =\frac{n}{n-1}\left(E\left(x^{2}\right)-E(x)^{2}\right)
\end{aligned}
$$

where $n$ denotes the number of data. Taking a sample every unit of time, $n$ is equivalent to time of the observation. Let $\mu_{n}$ be the expectation of $x$ up to $x_{n}, \mu_{2, n}$ be the expectation of $x^{2}$ up to $x_{n}^{2}$ and $\sigma_{n}^{2}$ be the sample variance up to $x_{n}$. The above equation can be modeled as the following difference equations.

$$
\begin{aligned}
\mu_{n} & =\mu_{n-1}+\frac{1}{n}\left(x_{n}-\mu_{n-1}\right) \\
\mu_{2, n} & =\mu_{2, n-1}+\frac{1}{n}\left(x_{n}^{-}-\mu_{2, n-1}\right) \\
\sigma_{n}^{2} & =\frac{n}{n-1}\left(\mu_{2, n-1}-\mu_{n-1}\right)
\end{aligned}
$$

The flow diagram of STELLA is following figure.
Fig 3.2.4-1 Expectation and variance


The full flow diagrams and equations are shown in Appendix A. And we also show some examples of outputs.

## Chapter 4.The result of the analysis and simulation

In this chapter, we show the result of the analysis and simulation. The analysis is based upon the equations derived in Chapter 2. We carry out our calculation using a BASIC program on the personal computer. The detail flow chart and program are described in Appendix A. The simulation is carried out using STELLA as described in Chapter 3. In each simulation, the duration of simulation is 2000 units of time, and the result is obtained from six simulation runs for each case. The full program and operation manual are described in Appendix B.
The applied model in this paper is based upon the examples in Graves's paper. The job shop consists of ten work stations and its work flow is described in Chapter 2 and 3. The flow matrix between each work station, average inputs $\mu$ and covariance matrix $\Sigma$ are in table 4-1.

Table 4-1

From work station (\#)

|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | 0.15 | 0.04 | 0.01 | 0.03 | 0.24 |  | 0.01 |  |  |
| 2 |  |  | 0.01 | 0.04 | 0.37 |  |  |  |  |  |
| 3 | 0.11 |  |  |  | 1.36 |  |  |  |  |  |
| 4 |  |  | 0.71 |  |  |  |  |  |  |  |
| 5 | 0.68 |  |  |  |  | 0.15 | 0.01 |  |  |  |
| 6 |  |  | 0.06 |  |  |  |  | 0.22 |  |  |
| 7 |  |  |  |  |  |  |  | 1.00 |  |  |
| 8 |  |  |  |  |  |  |  |  | 3.43 |  |
| 9 |  |  | 0.07 |  |  | 0.13 |  |  |  | 1.16 |
| 10 |  |  |  |  |  |  |  |  |  |  |
| $\mu$ | 4.0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| $\Sigma$ | 4.00 | 0.01 | 0.01 | 0.01 | 0.04 | 0.04 | 0 | 0.01 | 0.04 | 0.04 |

The work is assumed to flow from one work station to another in two hour periods. The capacities of work stations are 2 units of work, except work station \#1 and \#10.

As there are there machines are available in \#1, the capacity is assumed to be six units of work. Also it is assumed that there are 2.5 units of work capability at work station \#10. ( One unit of work needs one hour of machine operation. )

### 4.1 The validation of the simulation model

In this section, we would like to validate the simulation model by comparing its result to the result of Graves's paper. In order to compare the result, we select Case D of his paper. In this case, the planned lead times are given by the following table.
Table 4.1.-1 Planned lead time of case D
W.s. \#1 \#2 \#3 \#4 \#5 \#6 \#7 \#8 \#9 \# 10


At the following tables, "Original model" is the data of Graves's, and "95\% High (Low)" is the upper (lower) confidence level of the expected value.
(1) Work station \#1 (Planned lead time $=8$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 5.01 | 0.55 | 40.070 | 1.050 |
| 2.Simualtion (mean) | 5.031 | 0.547 | 40.312 | 1.028 |
| 95\% High | 5.074 | - | 40.702 | 1.052 |
| 95\%Low | 4.988 | - | 39.921 | 1.004 |
| Evaluation | ok | ok | ok | ok |

This result shows that the obtained expected production, expected queue and expected backlog are equivalent to the result of the Graves's model with the $95 \%$ confidence level ${ }^{6}$. And the standard deviation is effectively equivalent. The evaluation is the same on the following work stations. Therefore we can use the simulation model with confidence ${ }^{7}$.
(2) Work station \#2 $($ Planned lead time $=1)$

|  | $E(P)$ | $\sigma_{p}$ | $E(Q)$ | $E\left(Q^{m}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 0.75 | 0.13 | 0.75 | 0.0 |
| 2.Simualtion (mean) | 0.754 | 0.128 | 0.755 | 0.000 |
| $\quad$ 95\% High | 0.762 | - | 0.764 | 0.000 |
| 95\%Low | 0.746 | - | 0.746 | 0.000 |
| Evaluation | ok | ok | ok | ok |

(3) Work station \#3 (Planned lead time $=1$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :--- | :---: | :---: | :---: | :---: |
| 1.Original model | 0.69 | 0.14 | 0.69 | 0.0 |
| 2.Simualtion (mean) | 0.697 | 0.143 | 0.697 | 0.000 |
| 95\% High | 0.705 | - | 0.706 | 0.000 |
| 95\%Low | 0.688 | - | 0.688 | 0.000 |
| Evaluation | ok | ok | ok | ok |

(4) Work station \#4 (Planned lead time $=1$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 0.36 | 0.11 | 0.36 | 0.0 |
| 2.Simualtion (mean) | 0.359 | 0.115 | 0.359 | 0.000 |
| 95\% High | 0.364 | - | 0.363 | 0.000 |
| 95\%Low | 0.355 | - | 0.355 | 0.000 |
| Evaluation | ok | ok | ok | ok |

(5) Work station \#5 (Planned lead time $=2$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 1.37 | 0.20 | 2.74 | 0.06 |
| 2.Simualtion (mean) | 1.377 | 0.200 | 2.753 | 0.061 |
| 95\% High | 1.393 | - | 2.786 | 0.062 |
| 95\%Low | 1.360 | - | 2.720 | 0.061 |
| Evaluation | ok | ok | ok | ok |

(6) Work station \#6 (Planned lead time $=3$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 1.65 | 0.18 | 4.97 | 0.07 |
| 2.Simualtion (mean) | 1.659 | 0.170 | 4.987 | 0.066 |
| 95\% High | 1.672 | - | 5.034 | 0.067 |
| 95\%Low | 1.646 | - | 4.940 | 0.065 |
| Evaluation | ok | ok | ok | ok |

(7) Work station \#7 (Planned lead time $=1$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :--- | :---: | :---: | :---: | :---: |
| 1.Original model | 0.14 | 0.02 | 0.14 | 0.0 |
| 2.Simualtion (mean) | 0.138 | 0.020 | 0.138 | 0.000 |
| 95\% High | 0.140 | - | 0.140 | 0.000 |
| 95\%Low | 0.136 | - | 0.136 | 0.000 |
| Evaluation | ok | ok | ok | ok |

(8) work station \#8 (Planned lead time $=2$ )

$$
\mathrm{E}(\mathrm{P}) \quad \sigma_{\mathrm{p}} \quad \mathrm{E}(\mathrm{Q}) \mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)
$$

| 1.Original model | 0.55 | 0.08 | 1.10 | 0.02 |
| :---: | :---: | :---: | :---: | :---: |
| 2.Simualtion (mean) | 0.554 | 0.079 | 1.110 | 0.024 |
| 95\% High | 0.558 | - | 1.120 | 0.024 |
| 95\%Low | 0.550 | - | 1.099 | 0.023 |
| Evaluation | ok | ok | ok | ok |

(9) Work station \#9 (Planned lead time=4)

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{\mathrm{p}}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 1.89 | 0.22 | 7.56 | 0.12 |
| 2.Simualtion (mean) | 1.897 | 0.214 | 7.594 | 0.118 |
| 95\% High | 1.909 | - | 7.649 | 0.121 |
| 95\%Low | 1.885 | - | 7.539 | 0.116 |
| Evaluation | ok | ok | ok | ok |

(10) Work station \#10 (Planned lead time $=5$ )

|  | $\mathrm{E}(\mathrm{P})$ | $\sigma_{p}$ | $\mathrm{E}(\mathrm{Q})$ | $\mathrm{E}\left(\mathrm{Q}^{\mathrm{m}}\right)$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.Original model | 2.19 | 0.23 | 10.96 | 0.13 |
| 2.Simualtion (mean) | 2.200 | 0.226 | 11.016 | 0.129 |
| 95\% High | 2.212 | - | 11.087 | 0.131 |
| 95\%Low | 2.188 | - | 10.944 | 0.127 |
| Evaluation | ok | ok | ok | ok |

4.2 Analysis of the unreliable work station model

In 4.1, we validated the simulation model with reliable work stations by comparing the simulation results with the analytic results. In this section, first we validate the simulation of the unreliable work station model with the analytical model discussed in Chapter 2 by comparing both results. Next we show the result of the analysis of unreliable work station without production constraints.

### 4.2.1 The validation of the analytical model

We choose case D to compare results. The probabilities of break down are set to 0.1 for each work station, except work station \#9 whose probability is set to 0.05 . In the Table 4.2.1.-1, "work S." denotes work station, "P.L.T." denotes planning lead time, " $\mathrm{P}(\mathrm{B}, \mathrm{d})$ " denotes probability of break down, " $95 \% \mathrm{H}$ " denotes upper bound of $95 \%$ confidence level and "95\% L" denotes lower bound of $95 \%$ confidence level. Evaluation is based upon whether the result of the analysis is within the $95 \%$ confidence level of the result of the simulation. These results show that the analytical solution is within $95 \%$ confidence level of the estimated solution derived by the result of the simulation. From the above results, we can conclude that it is appropriate to apply both simulation model and analytical model to evaluate the performance of unreliable work stations.

## Table 4.2.1-1

| Work S. | 1 |  | 2 |  | 3 |  | 4 |  | 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 8 |  | 1 |  | 1 |  | 1 |  | 2 |  |
| P(B.d) | 0.1 |  | 0.1 |  | 0.1 |  | 0.1 |  | 0.1 |  |
| Method | Ana. | Sim. | Ana. | Sim. | Ana. | Sim. | Ana. | Sim. | Ana. | Sim. |
| E(P) m | 5.009 | 4.981 | 0.751 | 0.747 | 0.694 | 0.69 | 0.358 | 0.357 | 1.372 | 1.364 |
| $95 \%$ H | - | 5.064 | - | 0.759 | - | 0.701 | - | 0.364 | - | 1.385 |
| $95 \%$ L | - | 4.897 | - | 0.734 | - | 0.679 | - | 0.349 | - | 1.343 |
| $\sigma_{\text {p }}$ | 1.805 | 1.853 | 0.457 | 0.462 | 0.403 | 0.4000 | 0.269 | 0.269 | 0.617 | 0.622 |
| E(Q) m. 44.525 | 44.557 | 0.835 | 0.816 | 0.771 | 0.766 | 0.398 | 0.396 | 3.048 | 3.043 |  |
| $95 \%$ H. | - | 45.715 | - | 0.865 | - | 0.777 | - | 0.406 | - | 3.097 |
| $95 \%$ L. | - | 43.399 | - | 0.766 | - | 0.756 | - | 0.385 | - | 2.988 |
| Eval. | ok |  | ok |  | ok |  | ok |  | ok |  |


| Work S. | 6 |  | 7 |  | 8 |  | 9 |  | 10 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 3 |  | 1 |  | 2 |  | 4 |  | 5 |  |
| P(B.d) | 0.1 |  | 0.1 |  | 0.1 |  | 0.05 |  | 0.1 |  |
| Method | Ana. | Sim. | Ana. | Sim. | Ana. | Sim. | Ana. | Sim. | Ana. | Sim. |
| E(P) m | 1.654 | 1.640 | 0.137 | 0.137 | 0.551 | 0.546 | 1.890 | 1.872 | 2.193 | 2.171 |
| $95 \% \mathrm{H}$ | - | 1.668 | - | 0.138 | - | 0.555 | - | 1.900 | - | 2.206 |
| $95 \%$ L | - | 1.611 | - | 0.135 | - | 0.538 | - | 1.844 | - | 2.137 |
| $\sigma_{\text {p }}$ | 0.650 | 0.635 | 0.089 | 0.089 | 0.242 | 0.237 | 0.556 | 0.557 | 0.823 | 0.799 |
| E(Q) m. | 5.512 | 5.444 | 0.152 | 0.151 | 1.225 | 1.209 | 7.958 | 7.898 | 12.181 | 12.002 |
| $95 \%$ H. | - | 5.544 | - | 0.154 | - | 1.226 | - | 8.024 | - | 12.234 |
| $95 \%$ L. | - | 5.343 | - | 0.149 | - | 1.191 | - | 7.771 | - | 11.770 |
| Eval. | ok |  | ok |  | ok |  | ok |  | ok |  |

### 4.2.2. The result of analysis

(1) The expectation of production and queue

In Chapter 2, we have shown that the expectation of production and queue can be written as following form.

$$
\begin{aligned}
& \mathrm{E}\left(\mathrm{P}_{\mathrm{t}}\right)=(\mathrm{I}-\Phi)-1 \mu \\
& E\left(Q_{i, t}\right)=\left\{\left(1-p_{i}\right) \alpha_{i}\right\}^{-1} E\left(P_{i, t}\right)
\end{aligned}
$$

From these two equations, the following facts can be derived.
(a) The unreliability of the work station does not have any influence on the expectation of production.
(b) The expected queueing level of the each work station depends on the planning lead time $\left(\alpha_{i}^{-1}\right)$ and the probability of break down of its own work station. The break down of the other work stations do not affect the expectation of the queue.
These results are based on the fact that because there are infinite capability of the production and queue, the effect of the break down is compensated by large production after recovering from the break down. Thus it is possible to catch up with the production requirement of the system.
(2) The variance of production and queue

The effect of the break down of the work station increases the variance of the production and queue. As we have shown in Chapter 2, there are mutual and complicated interactions on the variance of production and queue. In order to show the effect of the unreliable work stations, we show the results of the calculation by the analytical model. The model shows the relationship due to increasing the unreliability at work station \#1 on the standard deviation of each work station. At first, this is shown as the ratio $\left(\mathrm{Sr}-1_{\mathrm{i}}\right)$ of the standard deviation and the expected production in Fig. 4.2.2.-1 and Fig. 4.2.2.-2. Second, this is shown as the ratio $\left(\mathrm{Sr}-2_{\mathrm{i}}\right)$ of standard deviation with unreliable work station and reliable work station in Fig 4.2.2-3 and Fig 4.2.2-4. In order to check the effect of planned lead time, the case A and case D of Graves's example are calculated. The difference between case A and case D is the planned lead time of each work station, as shown in the Table 4.2.2.-2.

Table 4.2.2.-2 Planned lead time W.s. \#1 \#2 \#3 \#4 \#5 \#6 \#7 \#8 \#9 \# 10

| $\mathrm{n}(\mathrm{A})$ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{n}(\mathrm{D})$ | 8 | 1 | 1 | 1 | 2 | 3 | 1 | 2 | 4 | 5 |

In the following figures, the data of the work stations are shown by the following symbols.

| Symbols | (1) | $\checkmark$ | $\checkmark$ | $\rangle$ | $\Lambda$ | $\theta$ | $\theta$ | $\bigoplus$ | M | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of WS | \# 1 | \# 2 | \# 3 | \# 4 | \# 5 | \# 6 | \# 7 | \# 8 | \# 9 | \# 10 |

The following table is the example of numerical output of the analytical model.
Tabel 4.2.2.-3 Example of numerical output of case D

| $\left\lvert\, \begin{aligned} & * * * \\ & \cdots * \end{aligned}\right.$ | A Tactical Planning Model for a Job Shop * With Unreliable Work Station |  |  |  |  |  |  |  | Unreliable | le Wor | ation |  | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| W |  | P-BD | $E(Q)$ | S(Q) | $E(P)$ | S(P) | W |  | P -BD | $E(Q)$ | S(Q) | E(P) | S(P) |
| 1 | 8 | 0.020 | 40.890 | 4.678 | 5.009 | 0.920 | 1 |  | 80.800 | 200.362 | 36.785 | 5.009 | 10.227 |
| 2 | 1 | 0.000 | 0.751 | 0.170 | 0.751 | 0.170 | 2 | 1 | 0.000 | 0.751 | 1.537 | 0.751 | 1.537 |
| 3 | 1 | 0.000 | 0.694 | 0.148 | 0.694 | 0.148 | 3 | 1 | 0.000 | 0.694 | 0.649 | 0.69 | 0.649 |
| 4 | 1 | 0.000 | 0.358 | 0.123 | 0.358 | 0.123 | 4 | 1 | 0.000 | 0.358 | 0.644 | 0.358 | 0.644 |
| 5 | 2 | 0.000 | 2.743 | 0.419 | 1.372 | 0.209 | 5 | 2 | 0.000 | 2.743 | 1.950 | 1.372 | 0.975 |
| 6 | 3 | 0.000 | 4.961 | 0.565 | 1.654 | 0.188 | 6 | 3 | 0.000 | 4.961 | 3.342 | 1.654 | 1.114 |
| 7 | 1 | 0.000 | 0.137 | 0.021 | 0.137 | 0.021 | 7 |  | 0.000 | 0.137 | 0.097 | 0.137 | 0.097 |
| 8 | 2 | 0.000 | 1.102 | 0.161 | 0.551 | 0.080 | 8 |  | 0.000 | 1.102 | 0.590 | 0.551 | 0.295 |
| 9 | 4 | 0.000 | 7.561 | 0.882 | 1.890 | 0.221 | 9 |  | 0.000 | 7.561 | 3.237 | 1.890 | 0.809 |
| 10 | 5 | 0.000 | 10.963 | 1.127 | 2.193 | 0.225 | 10 | 5 | 0.000 | 10.963 | 3.858 | 2.193 | 0.772 |

$\mathrm{Sr}-\mathrm{1}_{\mathrm{i}}=\frac{\text { Standard de viation of production at work station } \# \mathrm{i}: \# 1 \text { unreliable }}{\text { Expected production of work station } \# \mathrm{i}}$
Fig 4.2.2.-1 Sr-1 case A


Probability of break down at work station \#1
Fig 4.2.2.-2 Sr-1 case D

$\mathrm{Sr}-2 \mathrm{i}=\frac{\text { Standard deviation of production at work station } \# \mathrm{i}: \# 1 \text { unreliable }}{\text { Standard deviation of production (case } \mathrm{A}) \text { at work station } \# \mathrm{i}: \# 1 \text { reliable }}$
Fig 4.2.2-3 Sr-2 (Case A)


Probability of break down at work station \#1
Fig 4.2.2-4 Sr-2 (Case D)


These graphs show the robustness of the case D on the variance of the production. If an appropriate planned lead time is applied to the unreliable job shop, it can make the production smooth. As for the variance of queue, we can derive the relationship from Chapter 2.

$$
\operatorname{Var}\left(Q_{i i, t}\right)=\left\{\left(1-p_{i}\right)\left(\alpha_{i}\right)^{2}\right\}^{-1}\left[\operatorname{Var}\left(P_{i, t}\right)+p_{i}\left(1-p_{i}\right)^{-1} E\left(P_{i, t}\right)^{2}\right]
$$

Thus in the reliable work station, the standard deviation of queue is just proportional to the standard deviation of production and planned lead time.

$$
E\left(Q_{i, t}\right)=\left\{\left(1-p_{i}\right) \alpha_{i}\right\}^{-1} E\left(P_{i, t}\right)
$$

From the above result, we can conclude following.
(1) If it is required to smooth the level the production, it is necessary to increase the planned lead time for the appropriate work station. This method will work when there are unreliable work stations.
(2) If the work station is unreliable and planned lead time is applied, then the work in process inventory (queue to be produced) will increase and its variation will also increase.
(3) The average production of the work station does not change even if the work station is unreliable.
(4) The average queue of the work station is not affected by the other unreliable work stations. It is affected by the unreliability of the own work station.

We should mention that these conclusions are based upon having no capacity constraints at each work station.

In the following sections, we show the effect of production capacity constraints to this problem.
4.3 Simulation of the capacity constraints

In this section, we would like to show the example of the capacity constraints with reliable work stations. For the infinite capacity case, we applied the analytical approach. But for the finite capacity case, it is necessary to analyze the system with a help of the simulation. In order to show the characteristics of the capacity constraints we apply the model of the Graves where he applied implicit consideration about the constraints. The capacity constraints are shown in the following table.

| w.s\# | Table | $3 .-1$ | apa |  | tr |  | or | ation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 |  | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| Const | 6 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2.5 |
| E (P) | 5.01 | 0.75 | 0.69 | 0.36 | 1.37 | 1.65 | 0.14 | 0.55 | 1.89 | 2.19 |
| $\rho$ | 0.835 | 0.375 | 0.345 | 0.18 | 0.685 | 0.825 | 0.07 | 0.275 | 0.945 | 0.876 |
| $\mathrm{n}(\mathrm{A})$ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |  | 1 |
| n (D) | 8 | 1 | 1 | 1 | 2 | 3 | 1 | 2 | 4 | 5 |

where $\rho$ denotes the utilization load factor which is the ratio of expectation of production and capacity constraints. Capacity is defined as the production in the unit time period. At work station \#1, it is possible to produce 6 units per time period, and at \#10, it is possible to produce 2.5 units per time period. The other work station can produce or process 2 units per time period. $\mathrm{E}(\mathrm{P})$ is expected production of work in each work station. If the load factor is greater than one, the work station cannot complete its job within a given period of time. This table shows that work stations \#1, \#5, \#6, \#9 and \#10 are heavily loaded, especially at work station \#9, where the utilization load factor is 0.945 . The queueing theory tells us, that there will be large amount of queue at the heavily loaded work station. The planned lead time of the example, case D, was applied mainly for these work stations. In the table above, $n(A)$ and $n(D)$ are planned lead time of simulation case A and case $D$.

The simulation was carried out and we show the result of the simulation in Fig 4.3.1 and Table 4.3.-2. Fig 4.3.-1 shows the relationship between load factor and the effect of capacity constraints, and Table 4.3.-2 shows the result of simulation.

Fig 4.3.-1 The effect of the constraints on production variance of reliable work stations


Fig 4.3-1 shows that the capacity constraints give large effect on the case A which uses a planned lead time of one for every work station. The capacity constraints give a smaller effect on the case D . When the appropriate planned lead time is applied, the variance of the production is decreased as shown on the table 4.3.-2. But at the work station \#9, the change of the variance of production becomes the most significant, because the load factor at the work station \#9 is the heaviest. This work station is the most saturated. On the other hand, there are no significant differences in the other
work stations when the case $D$ is applied. Thus it is not necessary to calculate with constraints in these work stations.

Therefore if proper planned lead time and the capacity are selected, it is possible to avoid the use of a complicated full scale simulation.

Tabel 4.3.-2-A Simulation result of Case A

| Work S. | 1 |  | 2 |  | 3 |  | 4 |  | 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 1 |  | 1 |  | 1 |  | 1 |  | 1 |  |
| P(B.d) | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
| Const. | $\infty$ | 6 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 6 |
| E(P) m | 5.01 | 4.982 | 0.75 | 0.747 | 0.69 | 0.69 | 0.36 | 0.357 | 1.37 | 1.365 |
| $95 \%$ H | - | 5.067 | - | 0.760 | - | 0.703 | - | 0.364 | - | 1.386 |
| $95 \%$ L | - | 4.896 | - | 0.735 | - | 0.678 | - | 0.349 | - | 1.343 |
| $\sigma_{\text {P }}$ | 2.02 | 1.397 | 0.32 | 0.234 | 0.19 | 0.166 | 0.17 | 0.142 | 0.39 | 0.340 |
| E(Q) m. | 5.01 | 6.206 | 0.75 | 0.747 | 0.69 | 0.690 | 0.36 | 0.357 | 1.37 | 1.368 |
| $95 \%$ H. | - | 6.446 | - | 0.760 | - | 0.703 | - | 0.364 | - | 1.390 |
| $95 \%$ L. | - | 5.965 | - | 0.735 | - | 0.678 | - | 0.349 | - | 1.346 |
| E(Qn)m. | 0 | 1.224 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.003 |
| $95 \%$ H. | - | 1.418 | - | 0 | - | 0 | - | 0 | - | 0.004 |
| $95 \%$ L. | - | 1.031 | - | 0 | - | 0 | - | 0 | - | 0.003 |


| Work S. | 6 |  | 7 |  | 8 |  | 9 |  | 10 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 1 |  | 1 |  | 1 |  | 1 |  | 1 |  |
| P (B.d) | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
| Const. | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2.5 |
| $\mathrm{E}(\mathrm{P}) \mathrm{m}$ | 1.65 | 1.641 | 0.14 | 0.137 | 0.55 | 0.546 | 1.89 | 1.876 | 2.19 | 2.175 |
| 95\% H | - | 1.670 | - | 0.139 | - | 0.555 | - | 1.905 | - | 2.212 |
| 95\% L | - | 1.612 | - | 0.135 | - | 0.537 | - | 1.846 | - | 2.138 |
| $\sigma_{p}$ | 0.54 | 0.378 | 0.04 | 0.034 | 0.17 | 0.144 | 0.61 | 0.292 | 0.74 | 0.381 |
| $\mathrm{E}(\mathrm{Q}) \mathrm{m}$. | 1.65 | 1.685 | 0.14 | 0.137 | 0.55 | 0.546 | 1.89 | 4.830 | 2.19 | 2.199 |
| 95\% H. | - | 1.718 | - | 0.139 | - | 0.555 | - | 6.172 | - | 2.239 |
| 95\% L. | - | 1.651 | - | 0.135 | - | 0.537 | - | 3.487 | - | 2.159 |
| $\mathrm{E}(\mathrm{Qn}) \mathrm{m}$. | 0 | 0.043 | 0 | 0 | 0 | 0 | 0 | 2.957 | 0 | 0.024 |
| 95\% H. | - | 0.051 | - | 0 | - | 0 | - | 4.286 | - | 0.029 |
| 95\% L. | - | 0.036 | - | 0 | - | 0 | - | 2.159 | - | 0.020 |

Tabel 4.3.-2-D Simulation result of Case D

| Work S. | 1 |  | 2 |  | 3 |  | 4 |  | 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 8 |  | 1 |  | 1 |  | 1 |  | 2 |  |
| P(B.d) | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
| Const. | $\infty$ | 6 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 6 |
| E(P) m | 5.01 | 4.982 | 0.75 | 0.747 | 0.69 | 0.69 | 0.36 | 0.357 | 1.37 | 1.365 |
| $95 \%$ H | - | 5.066 | - | 0.760 | - | 0.702 | - | 0.364 | - | 1.386 |
| $95 \%$ L | - | 4.897 | - | 0.734 | - | 0.679 | - | 0.349 | - | 1.344 |
| $\sigma_{\text {p }}$ | 0.55 | 0.554 | 0.13 | 0.131 | 0.14 | 0.140 | 0.11 | 0.116 | 0.20 | 0.197 |
| E(Q) m. | 40.07 | 39.977 | 0.75 | 0.747 | 0.69 | 0.690 | 0.36 | 0.357 | 2.74 | 2.730 |
| $95 \% \mathrm{H}$. | - | 40.682 | - | 0.760 | - | 0.702 | - | 0.364 | - | 2.772 |
| $95 \%$ L. | - | 39.271 | - | 0.734 | - | 0.679 | - | 0.349 | - | 2.687 |
| E(Qn)m. | 1.05 | 1.127 | 0 | 0 | 0 | 0 | 0 | 0 | 0.06 | 0.061 |
| $95 \%$ H. | - | 1.213 | - | 0 | - | 0 | - | 0 | - | 0.063 |
| $95 \%$ L. | - | 1.041 | - | 0 | - | 0 | - | 0 | - | 0.059 |


| Work S. | 6 |  | 7 |  | 8 |  | 9 |  | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 3 |  | 1 |  | 2 |  | 4 |  | 5 |
| P(B.d) | 0 |  | 0 |  | 0 |  | 0 |  | 0 |
| const. | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ |
| E(P) m | 1.65 | 1.641 | 0.14 | 0.137 | 0.55 | 0.546 | 1.89 | 1.876 | 2.19 |
| 95\% H | - | 1.670 | - | 0.138 | - | 0.555 | - | 1.905 | - |
| 95\% L | - | 1.613 | - | 0.135 | - | 0.537 | - | 1.846 | - |
| $\sigma_{\text {p }}$ | 0.18 | 0.167 | 0.02 | 0.020 | 0.08 | 0.078 | 0.22 | 0.166 | 0.23 |
| E(Q) m. | 4.97 | 4.726 | 0.14 | 0.137 | 1.10 | 1.093 | 7.56 | 9.472 | 10.96 |
| 95\% H. | - | 5.012 | - | 0.138 | - | 1.110 | - | 10.633 | - |
| 95\% L. | - | 4.840 | - | 0.135 | - | 1.075 | - | 8.310 | - |
| E(Qn)m. | 0.07 | 0.067 | 0 | 0 | 0.02 | 0.023 | 0.12 | 2.039 | 0.13 |
| 95\% H. | - | 0.068 | - | 0 | - | 0.024 | - | 3.144 | - |
| 95\% L. | - | 0.066 | - | 0 | - | 0.023 | - | 0.934 | - |

4.4 Simulation of unreliable work stations and capacity constraints

In the previous sections, we have shown the individual effect of the unreliable work station and of the capacity constraint. In this section, we show an example of the simulation with both unreliable work stations and capacity constraints. We carry out the simulation for following eight cases which are denoted as $A / D(u / c, r / u)$. $A / D$ indicates case A or case $\mathrm{D}, \mathrm{u} / \mathrm{c}$ indicates whether the capacity is unconstrained or constrained and $\mathrm{r} / \mathrm{u}$ indicates whether it has reliable work stations or not.

|  | Unconstrained | Constrained |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Case A | Case D | Case A | Case D |
| Reliable | $\mathrm{A}(\mathrm{u}, \mathrm{r})$ | $\mathrm{D}(\mathrm{u}, \mathrm{r})$ | $\mathrm{A}(\mathrm{c}, \mathrm{r})$ | $\mathrm{D}(\mathrm{c}, \mathrm{r})$ |
| Unreliable | $\mathrm{A}(\mathrm{u}, \mathrm{u})$ | $\mathrm{D}(\mathrm{u}, \mathrm{u})$ | $\mathrm{A}(\mathrm{c}, \mathrm{u})$ | $\mathrm{D}(\mathrm{c}, \mathrm{u})$ |

The parameters in these simulations are the same as that of previous sections. The unreliable work stations are modeled as having $10 \%$ of unreliablity for all but \#9 work station. \#9 work station is modeled as having $5 \%$ of unreliability. The load factor of the unreliable work station is modeled as

$$
\rho=\frac{\mathrm{E}(\mathrm{P})}{\left(1-\mathrm{P}_{\mathrm{b}}\right) \mathrm{C}_{\mathrm{p}}}
$$

where $\mathrm{P}_{\mathrm{b}}$ denotes the probability of break down, and $\mathrm{C}_{\mathrm{p}}$ denotes production capacity. The next table shows the data of unreliable work station model and load factor. We select $\mathrm{P}_{\mathrm{b}}$ of \#9 work station as 0.05 in order to keep the load factor below 1.0 .

Table 4.4-1

| W.s \# | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Const | 6 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2.5 |
| $\mathrm{E}(\mathrm{P})$ | 5.01 | 0.75 | 0.69 | 0.36 | 1.37 | 1.65 | 0.14 | 0.55 | 1.89 | 2.19 |
| $\mathrm{P}_{\mathrm{b}}$ | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.05 | 0.1 |
| $\mathrm{n}(\mathrm{A})$ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| $\mathrm{n}(\mathrm{D})$ | 8 | 1 | 1 | 1 | 2 | 3 | 1 | 2 | 4 | 5 |
| $\rho$ | 0.928 | 0.417 | 0.383 | 0.200 | 0.761 | 0.917 | 0.078 | 0.306 | 0.995 | 0.973 |

Table 4.4-2-A,-D and following figures show the results of these simulation. In order to see the relationship, we choose $\mathrm{E}(\mathrm{P})$; expectation of production, $\sigma_{\mathrm{p}}$; standard deviation of production, $\mathrm{E}(\mathrm{Q})$; expectation of queue, $\mathrm{E}(\mathrm{Qn})$; backlog of the production.
Fig 4.4-1-A,D show the standard deviation of production of each work station. The results are normalized by the standard deviation from the unconstrained and reliable cases, that is case $A(u, r)$ or case $D(u, r)$. The figures show that the case with appropriate planned lead time (case D ) is insensitive to the capacity constraint. It also provides a smaller standard deviation for both reliable and unreliable work station. Fig 4.4-2-A,D show the expectation of queue of each work station. The results are normalized by the expectation of queue from the reliable and unconstrained case of case A or case D. Increasing the planned lead time always leads to longer queue. But the longer queue provides a benefit by smoothing the stochastic variation of the input flow. Therefore when we use the planned lead time, we have to trade off the benefit of the smooth production versus the increase in work-in-process inventory.

Fig 4.4-1-A $\sigma_{p} / \sigma_{p}($ Case $A(u, r))$ : Standard deviation of the production


Fig 4.4-1-D $\quad \sigma_{p} / \sigma_{p}($ Case $D(u, r))$ : Standard deviation of the production


Fig 4.4-2-A $\quad \mathrm{E}(\mathrm{Q}) / \mathrm{E}(\mathrm{Q} ; \mathrm{A}(\mathrm{u}, \mathrm{r})$ ): Expected queue


Fig 4.4-2-D $\mathrm{E}(\mathrm{Q}) / \mathrm{E}(\mathrm{Q} ; \mathrm{D}(\mathrm{u}, \mathrm{r}))$ : Expected queue


Fig 4.4-3 shows the expectation of the backlog of each work stations. The figure suggests that when the work stations are heavily loaded, the expectation of the back $\log$ is large. And when the work stations are unreliable, the back $\log$ will be larger.

Fig 4.4-3-A $\mathrm{E}(\mathrm{Qn}):$ Expected backlog


Fig 4.4-3-D E(Qn): Expected backlog


Table 4.4-2-A Simulation result: Unreliable work station Case A

| Work S. | 1 |  | 2 |  | 3 |  | 4 |  | 5 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 1 |  | 1 |  | 1 |  | 1 |  | 1 |  |
| P(B.d) | 0.1 |  | 0.1 |  | 0.1 |  | 0.1 |  | 0.1 |  |
| Const. | $\infty$ | 6 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 6 |
| E(P) m | 4.981 | 4.983 | 0.747 | 0.747 | 0.690 | 0.690 | 0.357 | 0.357 | 1.364 | 1.364 |
| $95 \%$ H | 5.066 | 5.065 | 0.759 | 0.759 | 0.702 | 0.701 | 0.364 | 0.364 | 1.386 | 1.384 |
| $95 \%$ L | 4.896 | 4.901 | 0.734 | 0.735 | 0.678 | 0.679 | 0.349 | 0.350 | 1.343 | 1.344 |
| $\sigma_{\text {p }}$ | 3.219 | 1.968 | 0.601 | 0.460 | 0.430 | 0.392 | 0.306 | 0.270 | 0.944 | 0.675 |
| E(Q) m. | 5.568 | 15.038 | 0.835 | 0.841 | 0.766 | 0.769 | 0.395 | 0.395 | 1.526 | 1.864 |
| 95\% H. | 5.724 | 19.221 | 0.853 | 0.858 | 0.777 | 0.779 | 0.406 | 0.406 | 1.561 | 1.959 |
| 95\% L. | 5.412 | 10855 | 0.816 | 0.823 | 0.755 | 0.759 | 0.384 | 0.385 | 1.490 | 1.769 |
| E(Qn)m. | 0.587 | 10.057 | 0.088 | 0.093 | 0.076 | 0.079 | 0.039 | 0.039 | 0.161 | 0.499 |
| 95\% H. | 0.687 | 14.174 | 0.095 | 0.100 | 0.079 | 0.085 | 0.044 | 0.044 | 0.186 | 0.586 |
| 95\% L. | 0.487 | 5.941 | 0.081 | 0.086 | 0.073 | 0.073 | 0.034 | 0.034 | 0.136 | 0.412 |


| Work S. | 6 |  | 7 |  | 8 |  | 9 |  | 10 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 1 |  | 1 |  | 1 |  | 1 |  | 1 |  |
| P(B.d) | 0.1 |  | 0.1 |  | 0.1 |  | 0.05 |  | 0.1 |  |
| Const. | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2.5 |
| E(P) m | 1.640 | 1.640 | 0.137 | 0.137 | 0.547 | 0.546 | 1.873 | 1.871 | 2.172 | 2.173 |
| 95\% H | 1.669 | 1.668 | 0.139 | 0.138 | 0.555 | 0.555 | 1.903 | 1.893 | 2.210 | 2.200 |
| $95 \%$ L | 1.611 | 1.612 | 0.135 | 0.135 | 0.538 | 0.538 | 1.843 | 1.850 | 2.133 | 2.145 |
| $\sigma_{\text {p }}$ | 1.107 | 0.650 | 0.112 | 0.092 | 0.387 | 0.321 | 1.466 | 0.471 | 1.925 | 0.780 |
| E(Q) m. | 1.817 | 3.097 | 0.152 | 0.152 | 0.605 | 0.607 | 1.983 | 14.775 | 2.392 | 6.816 |
| $95 \% \mathrm{H}$. | 1.856 | 3.535 | 0.154 | 0.153 | 0.616 | 0.617 | 2.014 | 20.085 | 2.442 | 8.865 |
| $95 \%$ L. | 1.777 | 2.659 | 0.149 | 0.150 | 0.595 | 0.597 | 1.953 | 9.466 | 2.342 | 4.766 |
| E(Qn)m. | 0.177 | 1.457 | 0.015 | 0.015 | 0.059 | 0.058 | 0.110 | 12.902 | 0.222 | 4.646 |
| 95\% H. | 0.195 | 1.887 | 0.016 | 0.015 | 0.066 | 0.063 | 0.119 | 18.191 | 0.247 | 6.685 |
| 95\% L. | 0.158 | 1.027 | 0.014 | 0.014 | 0.052 | 0.053 | 0.101 | 7.613 | 0.197 | 2.606 |

Table 4.4-2-D Simulation result: Unreliable work station Case D

| Work S. | 1 |  | 2 |  | 3 |  | 4 |  | 5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 8 |  | 1 |  | 1 |  | 1 |  | 2 |
| P(B.d) | 0.1 |  | 0.1 |  | 0.1 |  | 0.1 |  | 0.1 |
| Const. | $\infty$ | 6 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ |
| E(P) m | 4.981 | 4.978 | 0.747 | 0.746 | 0.690 | 0.689 | 0.357 | 0.357 | 1.364 |
| 95\% H | 5.064 | 5.023 | 0.759 | 0.754 | 0.701 | 0.697 | 0.364 | 0.360 | 1.385 |
| 95\% L | 4.897 | 4.933 | 0.734 | 0.739 | 0.679 | 0.681 | 0.349 | 0.354 | 1.343 |
| $\sigma_{\text {p }}$ | 1.853 | 1.730 | 0.462 | 0.435 | 0.400 | 0.394 | 0.269 | 0.265 | 0.622 |
| E(Q) m. | 44.557 | 47.969 | 0.816 | 0.831 | 0.766 | 0.773 | 0.396 | 0.400 | 3.043 |
| 95\% H. | 45.715 | 49.488 | 0.865 | 0.848 | 0.777 | 0.783 | 0.406 | 0.402 | 3.097 |
| 95\% L. | 43.399 | 46.450 | 0.766 | 0.814 | 0.756 | 0.764 | 0.385 | 0.397 | 2.988 |
| E(Qn)m. | 4.963 | 8.323 | 0.086 | 0.086 | 0.076 | 0.085 | 0.039 | 0.043 | 0.412 |
| 95\% H. | 5.614 | 9.585 | 0.092 | 0.100 | 0.081 | 0.090 | 0.044 | 0.048 | 0.444 |
| 95\% L. | 4.312 | 7.062 | 0.080 | 0.071 | 0.072 | 0.080 | 0.035 | 0.038 | 0.379 |


| Work S. | 6 |  | 7 |  | 8 |  | 9 |  | 10 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P.L.T. | 3 |  | 1 |  | 2 |  | 4 |  | 5 |  |
| P(B.d) | 0.1 |  | 0.1 |  | 0.1 |  | 0.05 |  | 0.1 |  |
| const. | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2 | $\infty$ | 2.5 |
| E(P) m | 1.640 | 1.642 | 0.137 | 0.136 | 0.546 | 0.546 | 1.872 | 1.866 | 2.171 | 2.163 |
| $95 \%$ H | 1.668 | 1.661 | 0.138 | 0.138 | 0.555 | 0.552 | 1.900 | 1.885 | 2.206 | 2.192 |
| $95 \%$ L | 1.611 | 1.623 | 0.135 | 0.135 | 0.538 | 0.540 | 1.844 | 1.847 | 2.137 | 2.133 |
| $\sigma_{\text {p }}$ | 0.635 | 0.576 | 0.089 | 0.087 | 0.237 | 0.239 | 0.557 | 0.449 | 0.799 | 0.731 |
| E(Q) m. | 5.444 | 6.719 | 0.151 | 0.152 | 1.209 | 1.215 | 7.898 | 22.978 | 12.002 | 15.711 |
| $95 \%$ H. | 5.544 | 7.449 | 0.154 | 0.154 | 1.226 | 1.234 | 8.024 | 37.077 | 12.234 | 17.980 |
| 95\% L. | 5.343 | 5.988 | 0.149 | 0.150 | 1.191 | 1.197 | 7.771 | 8.879 | 11.770 | 13.442 |
| E(Qn)m. | 0.591 | 1.842 | 0.015 | 0.016 | 0.145 | 0.150 | 0.599 | 15.529 | 1.251 | 4.929 |
| 95\% H. | 0.631 | 2.529 | 0.016 | 0.017 | 0.153 | 0.159 | 0.623 | 29.542 | 1.355 | 7.089 |
| 95\% L. | 0.550 | 1.156 | 0.014 | 0.014 | 0.137 | 0.140 | 0.575 | 1.517 | 1.147 | 2.768 |

## Chapter 5. Conclusion

The purpose of this work was to extend an analytical model and to develop a simulation model for a job shop planning problem. The focus was on the extension of the Tactical Planning Model ${ }^{1}$ to permit unreliable multiple work stations with production constraints.
The analytical model provides the steady state distribution of the production levels and the work in process inventory at each work station without capacity constraints. The simulation model also provides the steady state distribution of the production levels and the work in process inventory and steady state expectation of backlogs with capacity constraints.

In Chapter 2, we reviewed the Tactical Planning Model proposed by Graves, and extended the analysis to allow unreliable multiple work stations.
In Chapter 3, we showed the dynamic simulation model to examine the performance of the system.

In Chapter 4, we showed the result of the simulation and analysis. We showed the validation of the simulation model and analytical model. After the validation we showed the example of the simulation and analysis of the model with unreliable work stations and with capacity constraints.
We have obtained following results:
(1) If the work station is unreliable, the steady state of the work station will become as follows.
(a) The average production of each work station does not change even if there are unreliable work stations, provided that the load factor of the work station does not
exceed one. If the load factor is more than one the system cannot satisfy the requirement.
(b) The variance of production will be larger with the increase of the unreliability.
(c) The variance and expectation of the work in process inventory or queue will increase. The average queue of the work station is not affected by the other unreliable work stations. It is affected by the unreliability of the own work station.
(d) The expectation of the back log will be large. And at the heavily loaded work station, the back log will be larger.
(2) The capacity constraints of the work station makes the variance of the production smaller, especially when the work station is heavily loaded and/or the variance of production is large. Therefore simulation with capacity constraint is essential tool for analysis, when there are some heavily loaded work stations without an appropriate planned lead time and/or high unreliability.
(3) Applying a larger planned lead time makes it possible to analyze the system without the help of complicated and time consuming simulation.
(4) If it is required to make the level the production smooth in case of unreliable work stations, it is necessary to apply appropriate planned lead time especially for the heavily loaded work stations. Larger planned lead time makes the work station insensitive to the variance of input work flow.
(5) If the job shop is highly reliable and the work in process inventory is very costly, tactics like "Just-in-time" system will work because of its low level of queue.

Therefore when we use the planned lead time, we have to trade off the benefit of the smooth production and the cost of the work-in-process inventory.

## References

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## Appendix A. The analytical calculation program

## A. 1 Flow Chart

This program is desinged to calculate expectation and variance of production and queue of unreliable work station problem without production constraints. The inputs are stored by the form of DATA sentence of the main program and the file form of outside the program. In order to avoid the time consuming calculation of $(\mathrm{I}-\Phi)^{-1}$, it is stored in the outside data file. Therefore this matrix should be calculated at the first time when the new transient matrix $\Phi$ comes in. The algorithm of the matrix inversion and determinant are from M.R. Rosenthal ${ }^{8}$ (1966).
The outputs are obtained as the display form and data file form. The display form is on the screen of the personal computer, and the data file is on the "CLIP BOARD". The latter form makes it possible to use the output in the word processing software. But these output devices can be changed with ease by changing the assignment sentences.


## A. 2 Operation manual

(1) Data

The following data sets are in the main program. They should be changed in case of need.
a.Planned lead time

This term is inverse of $a_{i}$ and the input order is from work station one to ten. For example if it is the case D of Chapter 4, then

DATA 8,1,1,1,2,3,1,2,4,5
b. Probability of the work center break down

This term is the probabilities of break down of each workstation. For example if $\mathrm{p}_{1}$ is 0.8 and the others are 0 then

DATA $0.80,0,0,0,0,0,0,0,0,0$
c.Average input noise

This term is the average input noise. For example DATA 4,0,0,0,0,0,0,0,0,0

## d. Transition matrix

This term is the transition matrix of the work flow. In this paper it was described as $\Phi$ (Phai). This matrix is described by ten data sentenses. For example, DATA 0,0,0.11,0,0.68,0,0,0,0,0
*
*
DATA $0,0,0,0,0,0,0,0,1.16,0$

## e. Variance of input noise

This term is the diagonal elements of the Covariance matrix of the input noise. For example,

DATA $4.00,0.01,0.01,0.01,0.04,0.04,0,0.01,0.04,0.04$

## f. Flag for matrix output

This flag is used to command whether matrix elements in the calculation be printed out or not. When it is set as one, the print out of the matrix will come out. For example, when it is unnecessary to print out, DATA 0
g.Flag for calculate inverse transition matrix.

This flag is used to command whether it is necessary to calculate the inverse of the transition matrix ( $\mathrm{I}-\Phi)^{-1}$. When the matrix of $\Phi$ is changed this matrix has to be recalculated. This flag should be one when calculation is required, else it should be zero. When it is zero stored matrix (I- $\Phi)^{-1}$ can be obtained. For example, DATA 0
h. Number of iteration of the calculation of $\operatorname{Var}(\mathrm{Q})$

This term command the number of iteration of the calculation block of variance of queue. If it is necessary to calculate 16 times to get the convergence, it should be DATA 16
(2) Output devices

The outputs of this program is assigned to the screen and data file.

Followings are sentences of the assignment. The first assigns CRT of personal computer, and the second assigns "Clipboard" as a output data file.

OPEN "SCRN:" FOR OUTPUT AS \#1 OPEN "CLIP:" FOR OUTPUT AS \#5

## A. 3 Program list (BASIC)

The applied personal computer is Macintosh ${ }^{\mathrm{TM} @}$
1***** A Tactical Planning Model for a Job Shop

-***** This program was designed to calculate expected value and *
$1 * * * * * \quad$ standard deviation of the production and the queue.
'***** The work stations were modeled to break down by Bernoulli*
****** process.
'***** This work is a part on the master thesis of the writer.
*
****** November 12, 1987 © Shoichiro Mihara *
' Output port select. Select clipboard as a out put file. OPEN "SCRN:" FOR OUTPUT AS \#1
OPEN "CLIP:" FOR OUTPUT AS \#5
'Declare of double precision
DEFDBL A-H,O-Z

- Definition of dimention of vectors and matrixes
- Dim : Input variables

DIM XNV(10), PV(10),XMUIV(10), $\mathrm{PHI}(10,10), \operatorname{SIGV}(10)$

- Dim : for convinuence
$\operatorname{DIM} \operatorname{EI}(10,10), \operatorname{EIMPHI}(10,10), \operatorname{REIMPH}(10,10), \operatorname{XCHECK}(10,10)$
DIM ALPHA(10,10),PHISQ(10,10),EIPPHS(10,10), $\operatorname{PMAT}(10,10), \mathrm{C}(10,10)$
DIM EIMPMT(10,10),EMPTTD(10,10),REMPTD(10,10), $\operatorname{REPDEP}(10,10)$
DIM $\operatorname{QMEAN}(10), \operatorname{RALPHA}(10,10), \operatorname{PMEAN}(10)$
'
DIM EIPSPH(10,10), $\operatorname{EPSPHD}(10,10), \operatorname{SIGMAT}(10,10), \operatorname{SQMEAN}(10)$
DIM EI2 $(10,10)$, $\operatorname{E2MEPD}(10,10), \operatorname{R2MEPD}(10,10), \operatorname{RPDRPH}(10,10)$

[^1]DIM ESPDPD $(10,10), \operatorname{ESPPPP}(10,10), \operatorname{RPDPPP}(10,10), \operatorname{RPPSEQ}(10)$
DIM R2MVAS(10),VARQUE(10),STAQUE(10),STAPRO(10)
DIM EMPDD(10,10), EMPDDP(10,10),EPDPSQ(10),PDDVAQ(10),VARPRO(10)
DIM EIPHPD $(10,10), \operatorname{BBEPDP}(10,10), \operatorname{TRBBED}(10,10)$
DIM SIGMA $(10,10), \operatorname{BN}(10,10), \operatorname{TBN}(10,10)$
DIM WR1 $(10,10)$,WR2 $(10,10)$,WR3 $(10,10)$
DIM SBN(10,10), $\operatorname{APEIP}(10), \operatorname{ADDSIG}(10,10), \operatorname{TREPHI}(10,10), \operatorname{ADDVAR}(10,10)$
DIM ADDWR1 $(10,10)$

- Input (1) Planned lead time

FOR $\mathrm{l}=1$ TO 10
READ XNV(I)
NEXT I

- Input (2): Probabilities of break down of work centers FOR $\mathrm{J}=1$ TO 10
READ PV(J)
APEIP $(\mathrm{J})=\mathrm{PV}(\mathrm{J})^{*}(1-\mathrm{PV}(\mathrm{J})) / X N V(\mathrm{~J}) / X N V(\mathrm{~J})$
NEXT J
'Input (3): Expected value of inputs into the work centers from outside source. Muiu
FOR J=1 TO 10
READ XMUIV(J)
NEXT J
'Input (4): Work flow matrix
FOR K=1 TO 10
FOR L=1 TO 10
READ PHI(K,L)
NEXT L
NEXT K
'Input (5): Covariance of inputs into the work centers from outside source. Sigma
FOR J=1 TO 10
READ SIGV(J)
NEXT J
' Debug mode or not/ if Drbug=1 then print many parameters READ IDBUG
- If Flag is zero output (1-phi)-1 to data file after calculation.
' else input data and not calculate.


## READ Flag

## PRINT Flag

IF Flag=1 THEN OPEN "InvEmPhi.Data" FOR OUTPUT AS \#2
IF Flag=0 THEN OPEN "InvEmphi.Data" FOR INPUT AS \#2

- Definition of the size of matrixes $\mathrm{N}=10: \mathrm{N} 1=1$
- Input data and title GOSUB Titlepage
- Unit matrix

CALL UNIT(EI(),N)
'Equations; (1) Basic matrix
' (1-phi), (1-phi)-1

- If Flag is 1 output ( 1 -phi)-1 to data file after calculation. 0 input data and not calculate.

CALL MINUS(EI(),PHI(),EIMPHI(),N,N) :' EIMPHI=1-PHI
IF Flag = 0 GOTO jumpinv
CALL INVERS(REIMPH(),EIMPHI(),C(),N) :' REIMPH=EIMPHI^-1
FOR $\mathrm{j} 1=1$ TO N
FOR $\mathrm{i} 1=1$ TO N
WRITE \#2,REIMPH (j1,i1)
NEXT ${ }^{11}$
NEXT 11
GOTO outofinv
jumpinv:
FOR $\mathrm{j} 1=1$ TO N
FOR $i 1=1$ TO $N$
INPUT \#2,REIMPH(j1,i1)
NEXT ${ }^{11}$
NEXT 11
outofinv:
CLOSE \#2
' XCHECK=REIMPH*EIMPHI
'CALL MULTI (REIMPH(),N,N,EIMPHI(),N,N,XCHECK())
CALL DIAG(XNV(),RALPHA(),N) :' Trans from vec to diag matrix

CALL DIAINV(ALPHA(),RALPHA(),N) : 'Alpha = 1/ planned lead time CALL DIAG(SIGV(),SIGMAT(),N) :' Trans v to d-mat --- noise var. CALL DIAG(PV(),PMAT(),N) :' Trans v to d-mat --- prob. break CALL MINUS(EI(),PMAT(),EIMPMT(),N,N) :' Eipmt=Ei-Pmat
'Empttd=Eimpmt*Alpha
CALL MULTI (EIMPMT(),N,N,ALPHA(),N,N,EMPTTD())
' Eiphpd=(Ei-phi)*D*(1-p)
CALL MULTI(EIMPHI(),N,N,EMPTTD(),N,N,EIPHPD())
' Bbepdp=Ei-Eiphpd
CALL MINUS(EI(),EIPHPD(),BBEPDP(),N,N)
CALL TRANS(BBEPDP(),N,N,TRBBED())
CALL TRANS(EIMPHI(),N,N,TREPHI())
'calculation of expectation (Production and Queue )
'Remptd=Empttd^-1
CALL DIAINV(REMPTD(),EMPTTD(),N)
'Repdep=Remptd*Reimph
CALL MULTI(REMPTD(),N,N,REIMPH(),N,N,REPDEP())
' $\mathrm{E}(\mathrm{Q})=$ Repdep*Xmuiv
CALL MULTIV(REPDEP(),N,N,XMUIV(),N,QMEAN())
' $\mathrm{E}(\mathrm{P})=E m p t t d^{\star} \mathrm{E}(\mathrm{Q})$
CALL MULTIV(EMPTTD(),N,N,QMEAN(),N,PMEAN())
' Output1
GOSUB Printoutput1
'Print for debug
IF IDBUG=1 THEN GOSUB Printdebug1
' calculation of variance of queue.
FOR J=1 TO 10
$\operatorname{SQMEAN}(J)=\operatorname{QMEAN}(J)^{*} \operatorname{QMEAN}(\mathrm{~J}) \quad \therefore \quad$ Sqmean $(\mathrm{i})=\mathrm{E}(\mathrm{Q}(\mathrm{i}))^{\wedge} 2$
NEXT J
XX=1\#
CALL KMULTMAT(XX,SIGMAT(),SIGMA(),N,N) : ' Sigma=Sigmat
CALL KMULTMAT(XX,BBEPDP(),BN(),N,N) :'Bn=Bbepdp
CALL KMULTMAT(XX,TRBBED(),TBN(),N,N) :' Tbn= transpose (Bn)
' loop of the approximation
READ Ite
FOR I=1 TO Ite

```
    PRINT USING " I= ##";|
        FOR J=1 TO 10
            ADDSIG(J,J)=APEIP(J)*(SIGMA(J,J)+SQMEAN(J))
        NEXT J
    ' Addvar1=(1-phi)*addsig
        CALL MULTI(EIMPHI(),N,N,ADDSIG(),N,N,ADDWR1())
        'Addvar=Addvar1*(1-phi)T=(1-phi)*addsig*(1-phi)T
        CALL MULTI(ADDWR1(),N,N,TREPHI(),N,N,ADDVAR())
    ' Wr1=Bn*Sigma
        CALL MULTI(BN(),N,N,SIGMA(),N,N,WR1())
    'Wr2=Wr1*Tbn=Bn*Sigma*Tbn
        CALL MULTI(WR1(),N,N,TBN(),N,N,WR2())
    'Wr3= Bn*Sigma*Tbn+Addvar
        CALL PLUS (ADDVAR(),WR2(),WR3(),N,N)
    ' Sigma=Wr3+Sigmat
        CALL PLUS(SIGMAT(),WR3(),SIGMA(),N,N)
    NEXT I
FOR I=1 TO 10
    VARQUE(I)=SIGMA(I,I) :' Var(Q)=SIGMA
    STAQUE(I)=SQR(VARQUE(I)) :' Stand. Dev (Q)=Root (Var(Q))
    NEXT I
'End of the calculation 1
' Variance of production and standard deviation
    ' Empdd=Empttd*Alpha
        CALL MULTI (EMPTTD(),N,N,ALPHA(),N,N,EMPDD())
    'Empddp=Empdd*Pmat
        CALL MULTI (EMPDD(),N,N,PMAT(),N,N,EMPDDP())
    'Epdpsq=Empddp*Sqmean
        CALL MULTIV(EMPDDP(),N,N,SQMEAN(),N,EPDPSQ())
    'Pddvaq=Empdd*Varque
        CALL MULTIV(EMPDD(),N,N,VARQUE(),N,PDDVAQ())
    FOR I=1 TO 10
    VARPRO(I)=EPDPSQ(I)+PDDVAQ(I) :'Var(p)=Epdpsq+Pddvaq
        STAPRO(I)=SQR(VARPRO(I)) :' Stand. dev. of p=Root(Var(p))
    NEXT I
' output
GOSUB Printoutput2
```


## GOSUB Printoutput3

## CLOSE \#1

## CLOSE \# 5

## BEEP:BEEP:BEEP

END

- Planned lead time

DATA 8,1,1,1,2,3,1,2,4,5
'DATA $1,1,1,1,1,1,1,1,1,1$

- Probability of the work center break down
' DATA 0.1,0.1,0.1,0.1,0.1,0.1,0.1,0.1,0.05,0.1
DATA $0.80,0,0,0,0,0,0,0,0,0$
' Average input noise
DATA $4,0,0,0,0,0,0,0,0,0$
' Phi -- Work flow matrix
DATA 0,0,0.11,0,0.68,0,0,0,0,0
DATA $0.15,0,0,0,0,0,0,0,0,0$
DATA $0.04,0.01,0,0.71,0,0.06,0,0,0.07,0$
DATA $0.01,0.41,0,0,0,0,0,0,0,0$
DATA $0.03,0.37,1.36,0,0,0,0,0,0,0$
DATA $0.24,0,0,0,0.15,0,0,0,0.13,0$
DATA $0,0,0,0,0.1,0,0,0,0,0$
DATA $0.01,0,0,0,0,0.22,1,0,0,0$
DATA $0,0,0,0,0,0,0,3.43,0,0$
DATA $0,0,0,0,0,0,0,0,1.16,0$
'Variance of input noise
DATA $4.00,0.01,0.01,0.01,0.04,0.04,0,0.01,0.04,0.04$
'Debug or not (1--- print, else none)
DATA 0
' calculate inverse of (1-phi) flag $=1$ calculate flag=0 no DATA 0
' \# of iterations
DATA 32

```
SUB DIAINV(A(2),B(2),N) STATIC
    FOR \(\mathrm{J}=1\) TO N
            \(A(J, J)=1 / B(J, J)\)
    NEXT J
    END SUB
```

```
SUB INVERS(A(2),B(2),C(2),N) STATIC
    FOR I=1 TO N
    FOR J=1 TO N
            C(I,J)=B(I,J)
    NEXT J
    NEXT I
        CALL DETM(C(),N,E)
        IF E=0 THEN PRINT #1," NO INVERSE FOR THIS MATRIX" ELSE GOTO 10
                GOTO 20
1 0
        M=N-1
    FOR I=1 TO N
        FOR J=1 TO N
        FOR K=1 TO N
            FOR L=1 TO N
                C(K,L)=B(K,L)
                NEXT L
                NEXT K
                H=1
                FOR L=1 TO N
                C(I,L)=C(N,L)
                NEXT L
        FOR K=1 TO N
                C(K,J)=C(K,N)
            NEXT K
    IF NOT ((N=J AND N=1) OR (N<>J AND N<>1)) THEN H=-1 ELSE H=1
                CALL DETM(C(),M,DET)
                    A(J,I)=DET/E*H
        NEXT J
        NEXTI
20 END SUB
SUB DETM(A(2),K,DET) STATIC
    Z=1
    FOR M=2 TO K
    IF A(M-1,M-1) <> 0! THEN GOTO 50
    FORI=M TO K
    IF A(M-1,I) <>0 THEN GOTO 40
        NEXT I
        DET=0!
        GOTO endreturn
40 13=M-1
            FOR I2=13 TO K
```

```
    TEMP=A(12,13)
        A(I2,I3)=A(I2,I)
        A(I2,I)=TEMP
    NEXT I2
    Z=Z*(-1!)
50 FOR I=M TO K
    R=A(I,M-1)/A(M-1,M-1)
    FOR J=M TO K
        A(I,J)=A(I,J)-A(M-1,J)*R
    NEXT J
    NEXTI
    NEXT M
    DET=1
FORI=1 TOK
    DET=DET*A(I,I)
    NEXTI
    DET=DET*Z
    endreturn:
END SUB
```

SUB MULTI(A(2),IA,KA,B(2),KB,JB,C(2)) STATIC
IF KA<> KB THEN PRINT \#1,"ARGUMENT ERROR" ELSE GOTO LOOPSTART GOTOLOOPEND

```
LOOPSTART: FOR I=1 TO IA
        FOR J=1 TO JB
            S=0
            FOR K=1 TO KA
                S=S+A(I,K)*B(K,J)
            NEXT K
            C(I,J)=S
        NEXT J
    NEXT I
    LOOPEND:
    END SUB
```

```
SUB MULTIV(A(2),IA,KA,B(1),KB,C(1)) STATIC
    IF KA<>KB THEN PRINT #1, "ARGUMENT ERROR"
LOOPSTART:
            FORI=1 TO IA
                S=0
            FOR K=1 TO KA
                        S=S+A(1,K)*B(K)
            NEXT K
            C(I)=S
        NEXT I
        LOOPEND:
    END SUB
SUB KMULTMAT(XK,B(2),C(2),N,M) STATIC
    FOR I=1 TO N
        FOR J=1 TO M
            C(I,J)=XK*B(I,J)
        NEXT J
    NEXTI
    END SUB
SUB PLUS(A(2),B(2),C(2),N,M) STATIC
    FORI=1 TO N
        FOR J=1 TO M
            C(I,J)=A(I,J)+B(I,J)
        NEXT J
    NEXTI
    END SUB
SUB MINUS(A(2),B(2),C(2),N,M) STATIC
    FORI=1 TO N
        FOR J=1 TO M
            C(I,J)=A(I,J)-B(I,J)
        NEXT J
    NEXT I
END SUB
```

```
SUB CLMAT(A(2),N,M) STATIC
    FOR I=1 TO N
        FOR J=1 TO M
            C(I,J)=0!
        NEXT J
    NEXTI
    END SUB
SUB UNIT(C(2),N) STATIC
    FOR I=1 TO N
        C(I,I)=1#
    NEXTI
ENDSUB
SUB DIAG(V(1),A(2),N) STATIC
FOR I=1 TO N
        A(I,I)=V(I)
    NEXTI
ENDSUB
```

SUB TRANS (A(2),N,M,ATR(2)) STATIC
FOR I=1 TO N
FOR $\mathrm{J}=1$ TO M
ATR(J,I)=A(I, J)
NEXT J
NEXT I
END SUB
SUB PRINTMAT(A(2),N,M) STATIC
FOR I=1 TO N
$\mathrm{L}=1$
loopprint:
IF L>10 THEN GOTO ENDLOOP
PRINT \#1, USING "\#\#.\#\#\# " ;A(I,L);
L=L+1
GOTO loopprint
endloop:
PRINT \#1
NEXT I
PRINT \#1, :PRINT \#1,
END SUB

SUB PRINTVEC(A(1),N)STATIC
FOR $1=1$ TO N
PRINT \#1, USING "\#\#.\#\#\# " ;A(I);
NEXT I
PRINT \#1,:PRINT \#1, END SUB

## SUB SQELM(A(2),N,M,SA(2)) STATIC

FOR I=1 TO N
FOR $\mathrm{J}=1$ TO M
$S A(I, J)=A(I, J)^{*} A(1, J)$
NEXT J
NEXT I
END SUB
Titlepage:
PRINT \#1,
PRINT \#1, "*** MacIntosh version of Tactical Planning Model *" PRINT \#1,
PRINT \#1, "*** A Tactical Planning Model for a Job Shop *" PRINT \#1, "*** With Unreliable Work Station *" PRINT \#1,
PRINT \#1, : PRINT \#1, PRINT \#1," 1. Input value" :PRINT \#1, PRINT \#1," a. Planned lead time"
CALL PRINTVEC(XNV(),N)
PRINT \#1," b. Probability of break down"
CALL PRINTVEC(PV(),N)
PRINT \#1," c. Average input noise"
CALL PRINTVEC(XMUIV(),N)
PRINT \#1, " d.Covariance of input noise (diagonal element)"
CALL PRINTVEC(SIGV(),N)
RETURN
Printoutput1:
PRINT \#1, : PRINT \#1,
PRINT \#1, " 2. Output value" :PRINT \#1,
PRINT \#1," a. Average of queue $E(Q)$ "
CALL PRINTVEC(QMEAN(),N)
PRINT \#1," b. Average of production $E(P)$ "
CALL PRINTVEC(PMEAN(),N)
RETURN

```
Printdebug1:
            PRINT #1, "MATRIX (1-PHI)"
    CALL PRINTMAT(EIMPHI(),N,N)
            PRINT #1, "MATRIX (1-PHI)^-1*(1-PHI)"
    CALL PRINTMAT(XCHECK(),N,N)
        PRINT #1, "MATRIX PMAT"
    CALL PRINTMAT(PMAT(),N,N)
        PRINT #1, "MATRIX PHI"
    CALL PRINTMAT(PHI(),N,N)
        PRINT #1,
    PRINT #1,
REIURN
```


## Printoutput2:

PRINT \#1, " c. Variance of queue ..... $\operatorname{Var}(\mathrm{Q}) "$

``` CALL PRINTVEC(VARQUE(),N)
    PRINT #1," d.Standard deviation of queue"
        CALL PRINTVEC(STAQUE(),N)
    PRINT #1," e. Variance of production Var(P)"
        CALL PRINTVEC(VARPRO(),N)
        PRINT #1," f.Standard deviation of production"
        CALL PRINTVEC(STAPRO(),N)
    RETURN
    Printoutput3:
        PRINT #5, "*****************************************"
    PRINT #5, "*** A Tactical Planning Model for a Job Shop *"
        PRINT #5, "*** With Unreliable Work Station *"
            PRINT #5, "*****************************************"
    PRINT #5,
        PRINT #5,USING " Ite=##";lte
        PRINT #5," W.S. ";" N ";" P -BD";" E(Q) ";" S(Q) ";" E(P) ";" S(P) "
    FOR I=1 TO 10
            PRINT #5,USING" ## ## ##.### ##.### ##.### ##.###
##.###";I;XNV(I);PV(I);QMEAN(I);STAQUE(I);PMEAN(I);STAPRO(I)
    NEXT I
RETURN
```


## Appendix B. The complete STELLA Model

## B. 1 Flow Diagram






Product_1 Product_6 Queue_8


Time_ave




## B. 2 Equations

$\cdot \underset{\text { AVE_BL_1 }}{ }=$ AVE_BL_1 $1+$ Pro_P1_av INIT(AVE_BL_1)=0
-AVE_BL_2=AVE_BL_2+Pro_P2_av INIT(AVE_BL_2)=0
-AVE_BL_3=AVE_BL_3+Pro_P3_av INIT(AVE_BL_1)=0

- AVE_BL_4=AVE_BL_4+Pro_P4_av INIT(AVE_BL_4) $=0$
-AVE_BL_5=AVE_BL_5+Pro_P5_av INIT(AVE_BL_5)=0
-AVE_BL_6=AVE_BL_6+Pro_P6_av INIT(AVE_BL_6)=0
-AVE_BL_7=AVE_BL_7+Pro_P7_av INIT(AV̄E_BL_7)=0
- AVE_BL_8=AVE_BL_8+Pro_P8_av INIT(AVE_BL_8)=0
-AVE_BL_9=AVE_BL_9+Pro_P9_av INIT(AVE_BL_9)=0
- AVE_BL_10=AVE_BL_10+Pro_P10_av INIT(AVE_BL_10)=0
- Ave_Q_1=Ave_Q_1+Q_1_av INIT(Ave_Q_1)=INIT(Queue_1)
- Ave_Q_2=Ave_Q_2+Q_2_av INIT(Ave_Q_2)=INTT(Queue_2)
- Ave_Q_3=Ave_Q_3+Q_3_av INIT(Ave_Q_3)=INIT(Queue_3)
Ave_Q_4=Ave_Q_4+Q_4_av INIT(Ave_Q_4)=INIT(Queue_4)
- Ave_Q_5=Ave_Q_5+Q_5_av INIT(Ave_Q_5)=INIT(Queue_5)
Ave_Q_6=Ave_Q_6+Q_6_av INIT(Ave_Q_6)=INIT(Queue_6)
- Ave_Q_7=Ave_Q_7+Q_7_av INIT(Ave_Q_7)=INIT(Queue_7)
- Ave_Q_8=Ave_Q_8+Q_8_av INIT(Ave_Q_8)=INIT(Queue_8)
Ave_Q_9=Ave_Q_9+Q_9_av

INIT(Ave_Q_9)=INIT(Queue_9)

- Ave_Q_10=Ave_Q_10+Q_10_av

INIT(Ave_Q_10)=INIT(Queue_10)

- Ave_xs_1=Ave_xs_1+Prol_av_xs

INIT(Ave_xs_1)=INIT(Queue_1)*INIT(Queue_1)*Alpha_1*Alpha_1

- Ave_xs_2=Ave_xs_2+Pro2_av_xs

INIT(Ave_xs_2)=INIT(Queue_2)*INIT(Queue_2)*Alpha_2*Alpha_2

- Ave_xs_3=Ave_xs_3+Pro3_av_xs

INIT(Ave_xs_3)=INIT(Queue_3)*INIT(Queue_3)*Alpha_3*Alpha_3

- Ave_xs_4=Ave_xs_4+Pro4_av_xs

INIT(Ave_xs_4)=INIT(Queue_4)*INIT(Queue_4)*Alpha_4*Alpha_4

- Ave_xs_5=Ave_xs_5+Pro5_av_xs

INIT(Ave_xs_5)=INIT(Queue_5)*INIT(Queue_5)*Alpha_5*Alpha_5

- Ave_xs_6=Ave_xs_6+Pro6_av_xs

INIT(Ave_xs_6)=INIT(Queue_6)*INIT(Queue_6)*Alpha_6*Alpha_6

- Ave_xs_7=Ave_xs_7+Pro7_av_xs

INIT(Ave_xs_7)=INIT(Queue_7)*INIT(Queue_7)*Alpha_7*Alpha_7

- Ave_xs_8=Ave_xs_8+Pro8_av_xs

INIT(Ave_xs_8)=INIT(Queue_8)*INIT(Queue_8)*Alpha_8*Alpha_8

- Ave_xs_9=Ave_xs_9+Pro9_av_xs

INIT(Ave_xs_9)=INIT(Queue_9)*INIT(Queue_9)*Alpha_9*Alpha_9

- Ave_xs_10=Ave_xs_10+Pro10_av_xs INIT(Ave_xs_10)=INIT(Queue_10)*INIT(Queue_10)*Alpha_10*Alpha_10
- Ave_x_1=Ave_x_1+Pro1_av_x

INIT(Ave_x_1)=INIT(Queue_1)*Alpha_1

- Ave_x_2=Ave_x_2+Pro2_av_x

INIT(Ave_x_2)=INIT(Queue_2)*Alpha_2

- Ave_x_3=Ave_x_3+Pro3_av_x

INIT(Ave_x_3)=INIT(Queue_3)*Alpha_3

- Ave_x_4=Ave_x_4+Pro4_av_x

INIT(Ave_x_4)=INIT(Queue_4)*Alpha_4

- Ave_x_5=Ave_x_5+Pro5_av_x

INIT(Ave_x_5)=INIT(Queue_5)*Alpha_5

- Ave_x_6=Ave_x_6+Pro6_av_x

INIT(Ave_x_6)=INIT(Queue_6)*Alpha_6

- Ave_x_7=Ave_x_7+Pro7_av_x

INIT(Ave_x_7)=INIT(Queue_7)*Alpha_7
Ave_x_8=Ave_x_8+Pro8_av_x

INIT(Ave_x_8)=INIT(Queue_8)*Alpha_8

- Ave_x_9=Ave_x_9+Pro9_av_x

INIT(Ave_x_9)=INIT(Queue_9)*Alpha_9
-Ave_x_10=Ave_x_10+Pro10_av_x
INIT(Ave_x_10)=INIT(Queue_10)*Alpha_10

```
·P10_LAG_1=P10_LAG_1+P10_CV_1
INIT(P10_LAG_1)=0
•P10_LAG_2=P10_LAG_2+P10_CV_2
INIT(P10_LAG_2)=0
PP10_LAG_3=P10_LAG_3+P10_CV_3
INIT(P10_LAG_3)=0
· P10_LAG_4=P10_LAG_4+P10_CV_4
INIT(P10_LAG_4)=0
· P10_LAG_5=P10_LAG_5+P10_CV_5
INIT(P10_LAG_5)=0
PP1_LAG_1=P1_LAG_1+P1_CV_1
INIT(P1_LAG_1)=0
P P1_LAG_2=P1_LAG_2+P1_CV_2
INIT(P1_LAG_2)=0
P P1_LAG_3=P1_LAG_3+P1_CV_3
INIT(P1_LAG_3)=0
'P1_LAG_4=P1_LAG_4+P1_CV_4
INIT(P1_LAG_4)=0
P P1_LAG_5=P1_LAG_5+P1_CV_5
INIT(P1_LAG_5)=0
'P1_LAG_6=P1_LAG_6+P1_CV_6
INIT(P1_LAG_6)=0
'P1_LAG_7=P1_LAG_7+P1_CV_7
INIT(P1_LAG_7)=0
'P1_LAG_8=P1_LAG_8+P1_CV_8
INIT(P1_LAG_8)=0
P P2_LAG_1=P2_LAG_1+P2_CV_1
INIT(P2_LAG_1)=0
`P3_LAG_1=P3_LAG_1+P3_CV_1
INIT(P3_LAG_1)=0
· P4_LAG_1=P4_LAG_1+P4_CV_1
INIT(P4_LAG_1)=0
'P5_LAG_1=P5_LAG_1+P5_CV_1
```

$\varepsilon^{-} \Lambda \supset^{-} I O+\varepsilon^{-} D \forall T^{-} I O=\varepsilon^{-} D \forall T^{-} I O$.
$0=\left(\tau^{-} ⿹ \forall \mathrm{~T}^{-} \mathrm{IO}\right) \mathrm{LINI}$
$\tau^{-} \Lambda Э^{-} I O+Z^{-} D V T^{-} I O=Z^{-} D V T^{-} I O$.
$0=\left(I^{-}\right.$OVT-IO)LINI
$I^{-} \Lambda Э^{-} I O+I^{-} D V^{-} I O=I^{-} D V T^{-} I O$.
$\varsigma^{-} \Lambda J^{-} 0 I O+\varsigma^{-} \mathrm{DVT}^{-} 0 I O=\varsigma^{-} D V \mathrm{~T}^{-} 0 I O$. $0=\left(\dagger^{-}\right.$DV7- 0 IO)LINI
 $0=\left(\varepsilon^{-}\right.$DV7 $\left.{ }^{-} 0 I O\right) L I N I$
 $0=\left(Z^{-}\right.$DVT $\left.{ }^{-} 0 I D\right) L I N I$
$Z^{-} \Lambda \beth^{-} 0 І \partial+Z^{-}$OVT $010=Z^{-}$DVT 0 IO . $0=\left(I^{-}\right.$DVT $\left.{ }^{-} 0 I D\right) L I N I$
$\mathrm{I}^{-} \Lambda \mathrm{J}^{-} 0 \mathrm{I} \partial+\mathrm{I}^{-}$- $\mathrm{VT}^{-} 0 \mathrm{IO}=\mathrm{I}^{-} \mathrm{OVT} 0 \mathrm{O}$.
$0=\left(\vdash^{-} \mathrm{DVT}^{-} 6 \mathrm{~d}\right) \mathrm{LINI}$
$\nabla^{-} \Lambda \mathrm{D}^{-} 6 \mathrm{~d}^{+t^{-}} \mathrm{DVT}^{-} 6 \mathrm{~d}=\nabla^{-}-\mathrm{DVT}$ - 6 d .
$0=\left(\varepsilon^{-}{ }^{-1 /-} 6 \mathrm{~d}\right) \mathrm{LINI}$

$0=\left(Z^{-}{ }^{-}{ }^{-1}{ }^{-} 6 \mathrm{~d}\right)$ LINI

$0=\left(\mathrm{I}^{-} \mathrm{DVT}^{-} 6 \mathrm{~d}\right) \mathrm{LINI}$
$I^{-} \Lambda \mathrm{J}^{-} 6 \mathrm{~d}^{2}+\mathrm{I}^{-} \mathrm{DVT}^{-} 6 \mathrm{~d}=\mathrm{I}^{-} \mathrm{DVT}^{-} 6 \mathrm{~d}$. $0=\left(\tau^{-}{ }^{-}{ }^{-1}{ }^{-8 d}\right)$ LINI
 $0=\left(\mathrm{I}^{-}\right.$- $\left.\mathrm{FV} \mathrm{T}^{-} 8 \mathrm{~d}\right) \mathrm{LINL}$
 $0=\left(\mathrm{I}^{-} \mathrm{OV} \mathrm{T}^{-} \angle \mathrm{d}\right) \mathrm{LINI}$
$\mathrm{I}^{-} \Lambda \mathrm{D}^{-} \angle \mathrm{d}^{+} \mathrm{I}^{-} \mathrm{DV} \mathrm{T}^{-} \angle \mathrm{d}=\mathrm{I}^{-} \mathrm{DV} \mathrm{T}^{-} \angle \mathrm{d}$. $0=\left(\varepsilon^{-}{ }^{-}{ }^{-1} 9 \mathrm{~d}\right) \mathrm{LINI}$
$\varepsilon^{-} \Lambda D^{-} 9 d^{-}+\varepsilon^{-} \emptyset \forall T^{-} 9 d^{-} \mathcal{\varepsilon}^{-}-\forall T^{-} 9 \mathrm{~d}$. $0=\left(\tau^{-}\right.$-OVT-9d)LINI
 $0=\left(\mathrm{I}^{-}\right.$DVT ${ }^{-9 \mathrm{~d})}$ LINI
$I^{-} \Lambda J^{-} 9 \mathrm{~d}^{-1}-2 \forall T^{-} 9 \mathrm{~d}=\mathrm{I}^{-}-\mathrm{DVT} 9 \mathrm{~d}$.
$0=\left(\tau^{-}-\mathrm{OV} \mathrm{I}^{-} \varsigma \mathrm{d}\right)$ LINI

$0=\left(\mathrm{I}^{-} \mathrm{O} \mathrm{T}^{-} \varsigma \mathrm{d}\right) \mathrm{LINI}$
$0=\left(t^{-} \mathrm{DVT}^{-60}\right) \mathrm{LINI}$

$0=\left(\varepsilon^{-}-\right.$VT $\left.^{-} 60\right)$ LINI
$\varepsilon^{-} \Lambda J^{-} 60+\varepsilon^{-}-9 \forall T^{-} 60=\varepsilon^{-} 9 \forall T^{-} 60$. $0=\left(\tau^{-}-\right.$VT $\left.^{-} 60\right)$ LINI
$\tau^{-} \Lambda د^{-} 60+\tau^{-}-V^{-} 60=\tau^{-} 9 V T^{-} 60$. $0=\left(\mathrm{I}^{-} \mathrm{DVI}\right.$ - 60$)$ LINI

$0=\left(\tau^{-}{ }^{-}\right.$VT $\left.^{-} 8 \mathrm{O}\right) \mathrm{LINI}$

$0=$ ( $\left.^{-} \mathrm{OVT} \mathrm{C}^{-} 8 \mathrm{O}\right) \mathrm{LINI}$
 $0=\left(\mathrm{I}^{-} \mathrm{O} \mathrm{VI}^{-} \mathrm{LD}\right) \mathrm{LINI}$

$0=\left(\varepsilon^{-}-V^{-} 9\right.$ D) LINI

$0=\left(\tau^{-} \mathrm{DV1} 9 \mathrm{C}\right) \mathrm{LINI}$

$0=\left(\mathrm{I}^{-} \mathrm{OVT}\right.$-9 C$) \mathrm{LINI}$
 $0=\left(\tau^{-}-1 V^{-} \varsigma 0\right)$ LINI
 $0=\left(\mathrm{I}^{-}-\mathrm{VVT}\right.$ - $\varsigma$ O)LINI
 $0=\left(\mathrm{I}^{-} \mathrm{OVT} \mathrm{T}^{-} \dagger \mathrm{O}\right) \mathrm{LINI}$
 $0=\left(\mathrm{I}^{-} \mathrm{DVT}\right.$ - CD$)$ LINI
 $0=\left(I^{-}-V^{-}\right.$とD) LINI
 $0=\left(8^{-}{ }^{-1}\right.$ VTI $^{-}$IO)LINI
 $0=\left(L^{-}\right.$DVI ${ }^{-}$ID)LINI
 $0=\left(9^{-}-\right.$VVI $^{-}$ID) LuNI

$0=\left(\varsigma^{-} \mathrm{OVI}^{-} \mathrm{I} \mathrm{O}\right) \mathrm{LNI}$

$0=\left(\dagger^{-} \mathrm{OVI} \mathrm{IO}\right) \mathrm{LIN}$


```
` Q9_LAG_4=Q9_LAG_4+Q9_CV_4
INIT(Q9_LAG_4)=0
```

- Queue_1=Queue_1+Arrival_1-Product_1
INIT(Queue_1)=5.01/Alpha_1*SET_IN
- Queue_2=Queue_2+Arrival_2-Product_2
INIT(Queue_2)=0.75/Alpha_2*SET_IN
- Queue_3=Queue_3+Arrival_3-Product_3
INIT(Queue_3)=0.69/Alpha_3*SET_IN
- Queue_4=Queue_4+Arrival_4-Product_4
INIT(Queue_4)=0.36/Alpha_4*SET_IN
- Queue_5=Queue_5+Arrival_5-Product_5
INIT(Queue_5)=1.37/Alpha_5*SET_IN
- Queue_6=Queue_6+Arrival_6-Product_6
INIT(Queue_6)=1.65/Alpha_6*SET_IN
- Queue_7=Queue_7+Arrival_7-Product_7
INIT(Queue_7)=0.14/Alpha_7*SET_IN
- Queue_8=Queue_8+Arrival_8-Product_8
INIT(Queue_8)=0.55/Alpha_8*SET_IN
- Queue_9=Queue_9+Arrival_9-Product_9
INIT(Queue_9)=1.89/Alpha_9*SET_IN
- Queue_10=Queue_10+Arrival_10-Product_10
INIT(Queue_10)=2.19/Alpha_10*SET_IN
Alpha_1=1/8
Alpha_2=1/1
Alpha_3=1/1
Alpha_4=1/1
Alpha_5=1/2
Alpha_6=1/3
Alpha_7=1/1
Alpha_8=1/2
Alpha_9=1/4
Alpha_10=1/5
Arrival_1=Phy_31+Phy_51+Ran_1
Arrival_2=Phy_12+Ran_2
Arrival_3=Phy_13+Phy_23+Phy_43+Phy_63+Phy_93+Ran_3
Arrival_4=Phy_14+Phy_24+Ran_4
Arrival_5=Phy_15+Phy_25+Phy_35+Ran_5

Arrival_6=Phy_16+Phy_56+Phy_96+Ran_6
Arrival_7=Phy_57+Ran_7
Arrival_8=Phy_18+Phy_68+Phy_78+Ran_8
Arrival_9=Phy_89+Ran_9
Arrival_10=Phy_910+Ran_10
BPro_1=0.1
BPro_2=0.1
BPro_3=0.1
BPro_4=0.1
BPro_5=0.1
BPro_6=0.1
BPro_7=0.1
BPro_8=0.1
BPro_9=0.05
BPro_10=0.1
Input $=4$
OUT_BL=OUT_BL_1+OUT_BL_2
OUT_BL_1= IF T=1 THEN AVE_BL_1 ELSE IF T=5 THEN AVE_BL_5
ELSE IF T=6 THEN AVE_BL_6 ELSE IF T=8 THEN AVE_BL_8
ELSE IF T=9 THEN AVE_BL_9 ELSE IF T=10 THEN AVE_BL_10 ELSE 0
OUT_BL_2= IF T=2 THEN AVE_BL_2 ELSE IF T=3 THEN AVE_BL_3 ELSE IF T=4THEN AVE_BL_4 ELSE IF T=7 THEN AVE_BL_7 ELSE 0
OUT_EP=OUT_EP1+OUT_EP2
OUT_EP1= IF T=1 THEN Ave_x_1 ELSE IF T=2 THEN Ave_x_2
ELSE IF T=3 THEN Ave_x_3 ELSE IF T=4 THEN Ave_x_4
ELSE IF T=5 THEN Ave_x_5 ELSE 0
OUT_EP2 = IF T=6 THEN Ave_x_6 ELSE IF T=7 THEN Ave_x_7
ELSE IF T=8 THEN Ave_x_8 ELSE IF T=9 THEN Ave_x_9
ELSE IF T=10 THEN Ave_x_10 ELSE 0
OUT_EQ=OUT_EQ1+OUT_EQ2
OUT_EQ1 = IF T=1 THEN Ave_Q_1 ELSE IF T=2 THEN Ave_Q_2
ELSE IF T=3 THEN Ave_Q_3 ELSE IF T=4 THEN Ave_Q_4
ELSE IF T=5 THEN Ave_Q_5 ELSE 0
OUT_EQ2= IF T=6 THEN Ave_Q_6 ELSE IF T=7 THEN Ave_Q_7
ELSE IF T=8 THEN Ave_Q_8 ELSE IF T=9 THEN Ave_Q_9
ELSE IF T=10 THEN Ave_Q_10 ELSE 0
OUT_S=OUT_S1+OUT_S2
OUT_S1 = IF T=1 THEN Sigma_1 ELSE IF T=2 THEN Sigma_2

ELSE IF T=3 THEN Sigma_3 ELSE IF T=4 THEN Sigma_4 ELSE IF T=5 THEN Sigma_5 ELSE 0
OUT_S2= IF T=6 THEN Sigma_6 ELSE IF T=7 THEN Sigma_7
ELSE IF T=8 THEN Sigma_8 ELSE IF T=9 THEN Sigma_9 ELSE IF T=10 THEN Sigma_10 ELSE 0
P10_CV_1=Product_10-P10_LAG_1
P10_CV_2=P10_LAG_1-P10_LAG_2
P10_CV_3=P10_LAG_2-P10_LAG_3
P10_CV_4=P10_LAG_3-P10_LAG_4
P10_CV_5=P10_LAG_4-P10_LAG_5
P1_CV_1=Product_1-P1_LAG_1
P1_CV_2=P1_LAG_1-P1_LAG_2
P1_CV_3=P1_LAG_2-P1_LAG_3
P1_CV_4=P1_LAG_3-P1_LAG_4
P1_CV_5=P1_LAG_4-P1_LAG_5
P1_CV_6=P1_LAG_5-P1_LAG_6
P1_CV_7=P1_LAG_6-P1_LAG_7
P1_CV_8=P1_LAG_7-P1_LAG_8
P2_CV_1=Product_2-P2_LAG_1
P3_CV_1=Product_3-P3_LAG_1
P4_CV_1=Product_4-P4_LAG_1
P5_CV_1=Product_5-P5_LAG_1
P5_CV_2=P5_LAG_11-P5_LAG_2
P6_CV_1=Product_6-P6_LAG_1
P6_CV_2=P6_LAG_1-P6_LAG_2
P6_CV_3=P6_LAG_2-P6_LAG_3
P7_CV_1=Product_7-P7_LAG_1
P8_CV_1=Product_8-P8_LAG_1
P8_CV_2=P8_LAG_1-P8_LAG_2
P9_CV_1=Product_9-P9_LAG_1
P9_CV_2=P9_LAG_1-P9_LAG_2
P9_CV_3=P9_LAG_2-P9_LAG_3
P9_CV_4=P9_LAG_3-P9_LAG_4

Phy_12=Product_1*0.15
Phy_13=Product_1*0.04
Phy_14=Product_1*0.01
Phy_15=Product_1*0.03
Phy_16=Product_1*0.24
Phy_18=Product_1*0.01
Phy_23=Product_2*0.01

Phy_24=Product_2*0.41
Phy_25=Product_2*0.37
Phy_31=Product_3*0.11
Phy_35=Product_3*1.36
Phy_43=Product_4*0.71
Phy_51=Product_5*0.68
Phy_56=Product_5*0.15
Phy_57=Product_5*0.1
Phy_63=Product_6*0.06
Phy_68=Product_6*0.22
Phy_78=Product_7*1.0
Phy_89=Product_8*3.43
Phy_910=Product_9*1.16
Phy_93=Product_9*0.07
Phy_96=Product_9*0.13
Pro10_av_x=(Product_10-Ave_x_10)/Time_ave
Pro10_av_xs=(Sq_Pro_10-Ave_xs_10)/Time_ave
Prol_av_x=(Product_1-Ave_x_1)/Time_ave
Prol_av_xs=(Sq_Pro_1-Ave_xs_1)/Time_ave
Pro2_av_x=(Product_2-Ave_x_2)/Time_ave
Pro2_av_xs=(Sq_Pro_2-Ave_xs_2)/Time_ave
Pro3_av_x=(Product_3-Ave_x_3)/Time_ave
Pro3_av_xs=(Sq_Pro_3-Ave_xs_3)/Time_ave
Pro4_av_x=(Product_4-Ave_x_4)/Time_ave
Pro4_av_xs=(Sq_Pro_4-Ave_xs_4)/Time_ave
Pro5_av_x=(Product_5-Ave_x_5)/Time_ave
Pro5_av_xs=(Sq_Pro_5-Ave_xs_5)/Time_ave
Pro6_av_x=(Product_6-Ave_x_6)/Time_ave
Pro6_av_xs=(Sq_Pro_6-Ave_xs_6)/Time_ave
Pro7_av_x=(Product_7-Ave_x_7)/Time_ave
Pro7_av_xs=(Sq_Pro_7-Ave_xs_7)/Time_ave
Pro8_av_x=(Product_8-Ave_x_8)/Time_ave
Pro8_av_xs=(Sq_Pro_8-Ave_xs_8)/Time_ave
Pro9_av_x=(Product_9-Ave_x_9)/Time_ave
Pro9_av_xs=(Sq_Pro_9-Ave_xs_9)/Time_ave
Product_1=IF RANDOM $>=$ BPro_1 THEN MIN(Alpha_1*Queue_1, Product_Max_1) ELSE 0
Product_10=IF RANDOM $>=$ BPro_10 THEN MIN(Alpha_10*Queue_10, Product_Max_10) ELSE 0
Product_2=IF RANDOM>=BPro_2 THEN MIN(Alpha_2*Queue_2, Product_Max_2) ELSE 0

Product_3=IF RANDOM $>=$ BPro_3 THEN MIN(Alpha_3*Queue_3, Product_Max_3) ELSE 0
Product_4=IF RANDOM $>=$ BPro_4 THEN MIN(Alpha_4*Queue_4, Product_Max_4) ELSE 0
Product_5=IF RANDOM $>=$ BPro_ 5 THEN MIN(Alpha_5*Queue_5, Product_Max_5) ELSE 0
Product_6=IF RANDOM>=BPro_6 THEN MIN(Alpha_6*Queue_6, Product_Max_6) ELSE 0
Product_7=IF RANDOM $>=$ BPro_7 THEN MIN(Alpha_7*Queue_7, Product_Max_7) ELSE 0
Product_8=IF RANDOM>=BPro_8 THEN MIN(Alpha_8*Queue_8, Product_Max_8) ELSE 0
Product_9=IF RANDOM $>=$ BPro_9 THEN MIN(Alpha_9*Queue_9, Product_Max_9) ELSE 0
Product_Max_1= IF SET_MAX=1 THEN 6 ELSE 100
Product_Max_10= IF SET_MAX=1 THEN 2.5 ELSE 100
Product_Max_2= IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_3= IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_4= IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_5= IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_6= IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_7=IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_8= IF SET_MAX=1 THEN 2 ELSE 100
Product_Max_9= IF SET_MAX=1 THEN 2 ELSE 100
Pro_P1 $=($ Q1_LAG_1-P1_LAG_1)*0+(Q1_LAG_8-P1_LAG_1-P1_LAG_2 -P1_LAG_3-P1_LAG_4-P1_LAG_5-P1_LAG_6-P1_LAG_7 -P1_LAG_8)*1
\{alpha $=1$ then 1,0 alpha $=1 / 8$ then 0,1$\}$
Pro_P1_av =IF Pro_P1>=0 THEN ( Pro_P1-AVE_BL_4)/Time_ave ELSE (-AVE_BL_1)/Time_ave
Pro_P10 $=($ Q10_LAG_1-P10_LAG_1)*0+(Q10_LAG_5-P10_LAG_1 -P10_LAG_2-P10_LAG_3-P10_LAG_4-P10_LAG_5)*1
$\{$ alpha $=1$ then 1,0 alpha $=1 / 5$ then 0,1$\}$
Pro_P10_av =IF Pro_P10>=0 THEN ( Pro_P10-AVE_BL_4)/Time_ave ELSE (-AVE_BL_10)/Time_ave
Pro_P2 =( Q2_LAG_1-P2_LAG_1)
Pro_P2_av =IF Pro_P2>=0 THEN ( Pro_P2-AVE_BL_4)/Time_ave ELSE (-AVE_BL_2)/Time_ave
Pro_P3 =( Q3_LAG_1-P3_LAG_1)
Pro_P3_av $=\mathrm{IF}$ Pro_P3> $=0$ THEN ( Pro_P3-AVE_BL_4)/Time_ave ELSE (-AVE_BL_3)/Time_ave
Pro_P4 =( Q4_LAG_1-P4_LAG_1)

$$
\begin{aligned}
& \mathrm{I}^{-} \mathrm{OVT}^{-} \varsigma \mathrm{S}^{-} \varsigma^{-} \text {әnənØ }=\mathrm{I}^{-} \Lambda \mathrm{J}^{-} \text {ऽ }
\end{aligned}
$$

$8^{-}$OVT $^{-} \mathrm{LO}^{-} L^{-} \mathrm{OVT}^{-}$IO $=8^{-} \Lambda \mathrm{J}^{-}$IO
$L^{-} \mathrm{OVT}^{-}$IO-9- $\mathrm{DVT}^{-}$IO $=L^{-} \Lambda \mathrm{J}^{-}$IO
$9^{-}$DVT $^{-} I O-S^{-}$OVT $^{-} I O=9^{-} \Lambda J^{-} I O$
$\varepsilon^{-}$DVT $^{-} I \partial-Z^{-} D \forall T^{-} I \partial=\varepsilon^{-} \Lambda J^{-} I \partial$




$$
L *\left(t_{-}^{-} D V T^{-} 6 d^{-} \varepsilon^{-} D V T^{-} 6 d^{-}\right.
$$






$$
\mathrm{I} * \mathrm{Z}^{-} 0 \vee \mathrm{~T}^{-} 8 \mathrm{~d}^{-}
$$

$\left.\mathrm{I}^{-} \mathrm{DVT}^{-} 8 \mathrm{~d}^{-} \tau^{-} \mathrm{DVT}-80\right)+0 *\left(\mathrm{I}^{-} \mathrm{DVT}^{-} 8 \mathrm{~d}^{-} \mathrm{I}^{-} \mathrm{DVT}^{-} 8 \mathrm{O}\right)=8 \mathrm{~d}^{-} \mathrm{or}_{\mathrm{d}}$

 $\left(I^{-} D \forall T^{-} \angle d^{-} I^{-} D \forall T^{-} L O\right)=\angle d^{-} o_{d}$




$$
\mathrm{I} *\left(\varepsilon^{-} \bigcirc \forall \mathrm{T}^{-} 9 \mathrm{~d}^{-}\right.
$$





$\mathrm{I}_{*}\left(\mathrm{Z}^{-} \mathrm{D} V \mathrm{~T}^{-} \mathrm{c}^{-} \mathrm{d}^{-}\right.$




| Q5_CV_2=Q5_LAG_1-Q5_LAG_2 | Q5_CV_2=Q5_LAG_1-Q5_LAG_2 |
| :---: | :---: |
|  | Q6_CV_1=Queue_6-Q6_LAG_1 |
|  | Q6_CV_2=Q6_LAG_1-Q6_LAG_2 |
|  | Q6_CV_3=Q6_LAG_2-Q6_LAG_3 |
|  | Q7_CV_1=Queue_7-Q7_LAG_1 |
|  | Q8_CV_1=Queue_8-Q8_LAG_1 |
|  | Q8_CV_2=Q8_LAG_1-Q8_LAG_2 |
|  | Q9_CV_1=Queue_9-Q9_LAG_1 |
|  | Q9_CV_2=Q9_LAG_1-Q9_LAG_2 |
|  | Q9_CV_3=Q9_LAG_2-Q9_LAG_3 |
|  | Q9_CV_4=Q9_LAG_3-Q9_LAG_4 |
|  | Q_10_av=(Queue_10-Ave_Q_10)/Time_ave |
|  | Q_1_av=(Queue_1-Ave_Q_1)/Time_ave |
|  | Q_2_av=(Queue_2-Ave_Q_2)/Time_ave |
|  | Q 3_av=(Queue_3-Ave_Q_3)/Time_ave |
|  | Q_4_av=(Queue_4-Ave_Q_4)/Time_ave |
|  | Q_5_av=(Queue_5-Ave_Q_5)/Time_ave |
|  | Q_6_av=(Queue_6-Ave_Q_6)/Time_ave |
|  | Q 7 av=(Queue 7 -Ave Q 7 )/Time ave |
|  | Q_8_av=(Queue_8-Ave_Q_8)/Time_ave |
|  | Q 9_av=(Queue_9-Ave_Q_9)/Time_ave |
|  | Ran_1 =NORMAL*2+INPUT |
|  | Ran_10=NORMAL*0.2 |
|  | Ran_2=NORMAL*0.1 |
|  | Ran_3 =NORMAL*0.1 |
|  | Ran_4 =NORMAL*0.1 |
|  | Ran_5=NORMAL*0.2 |
|  | Ran_6 =NORMAL*0.2 |
|  | Ran_7 $=0$ |
|  | Ran_8 =NORMAL*0.1 |
|  | Ran_9 =NORMAL*0.2 |

SET_IN=1 \{If it is one the simulation is for steady state.\}
SET_MAX $=1$ \{If it is one the limiter will be applied.\}
SET_T_MAX=2000 \{Maximum simulation time should be set here in order to control out put data.\}

Sigma_1 = IF Var_1>=0 THEN EXP( $0.5^{*}$ LOGN(Var_1) ELSE 0 Sigma_10= IF Var_10>=0 THEN EXP(0.5*LOGN(Var_10) ELSE 0
Sigma_2 $=$ IF Var_2 $>=0$ THEN EXP( $0.5^{*}$ LOGN(Var_2) ELSE 0
Sigma_3 $=$ IF Var_3>=0 THEN EXP $\left(0.5^{*}\right.$ LOGN(Var_3) ELSE 0

Sigma_4 $=$ IF Var_4>=0 THEN EXP(0.5*LOGN(Var_4) ELSE 0 Sigma_5 = IF Var_5>=0 THEN EXP( $0.5^{*}$ LOGN(Var_5) ELSE 0 Sigma_6 = IF Var_6>=0 THEN EXP( $0.5 *$ LOGN(Var_6) ELSE 0 Sigma_7 = IF Var_7>=0 THEN EXP(0.5*LOGN(Var_7) ELSE 0 Sigma_8 $=$ IF Var_ $8>=0$ THEN EXP( $0.5^{*}$ LOGN(Var_8) ELSE 0 Sigma_9=IF Var_9>=0 THEN EXP ( $0.5 *$ LOGN(Var_9) ELSE 0

Sq_Pro1 =Product_1*Product_1
Sq_Pro10 =Product_10*Product_10
Sq_Pro2 =Product_2*Product_2
Sq_Pro3 =Product_3*Product_3
Sq_Pro4 =Product_4*Product_4
Sq_Pro5 =Product_5*Product_5
Sq_Pro6 =Product_6*Product_6
Sq_Pro7 =Product_7*Product_7
Sq_Pro8 =Product_8*Product_8
Sq_Pro9 =Product_9*Product_9
T=IF TIME,(SET_T_MAX-9) THEN 0 ELSE IF TIME $>$ (SET_T_Max) THEN
0 ELSE TIME-(SET_T_Max-10)
Time_ave $=$ IF TIME $<=500$ THEN 1 ELSE TIME-500
Var_1=IF Time_ave>2 THEN (Ave_xs_1-Ave_x_1*Ave_x_1 )*
(Time_ave/(Time_ave-1)) ELSE 0
Var_10=IF Time_ave>2 THEN (Ave_xs_10-Ave_x_10*Ave_x_10 )*
(Time_ave/(Time_ave-1)) ELSE 0
Var_2=IF Time_ave>2 THEN (Ave_xs_2-Ave_x_2*Ave_x_2 )* (Time_ave/(Time_ave-1)) ELSE 0
Var_3=IF Time_ave>2 THEN (Ave_xs_3-Ave_x_3*Ave_x_3 )* (Time_ave/(Time_ave-1)) ELSE 0
Var_4=IF Time_ave>2 THEN (Ave_xs_4-Ave_x_4*Ave_x_4 )* (Time_ave/(Time_ave-1)) ELSE 0
Var_5=IF Time_ave>2 THEN (Ave_xs_5-Ave_x_5*Ave_x_5 )* (Time_ave/(Time_ave-1)) ELSE 0
Var_6=IF Time_ave>2 THEN (Ave_xs_6-Ave_x_6*Ave_x_6 )* (Time_ave/(Time_ave-1)) ELSE 0
Var_7=IF Time_ave>2 THEN (Ave_xs_7-Ave_x_7*Ave_x_7)* (Time_ave/(Time_ave-1)) ELSE 0
Var_8=IF Time_ave>2 THEN (Ave_xs_8-Ave_x_8*Ave_x_8 )* (Time_ave/(Time_ave-1)) ELSE 0
Var_9=IF Time_ave>2 THEN (Ave_xs_9-Ave_x_9*Ave_x_9 )* (Time_ave/(Time_ave-1)) ELSE 0

## B. 3 Example of output

(1) Numerical output

| Time | T | OUT_EP | OUT_S | OUT_EQ | OUT_BL |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 990.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| 991.000 | 1.000 | 4.921 | 1.653 | 45.766 | 6.734 |  |
| 992.000 | 2.000 | 0.737 | 0.390 | 0.800 | 0.0637 |  |
| 993.000 | 3.000 | 0.683 | 0.387 | 0.764 | 0.0810 |  |
| 994.000 | 4.000 | 0.353 | 0.264 | 0.401 | 0.0483 |  |
| 995.000 | 5.000 | 1.351 | 0.577 | 3.138 | 0.520 |  |
| 996.000 | 6.000 | 1.624 | 0.545 | 5.981 | 1.163 |  |
| 997.000 | 7.000 | 0.135 | 0.0856 | 0.150 | 0.0148 |  |
| 998.000 | 8.000 | 0.540 | 0.238 | 1.201 | 0.146 |  |
| 999.000 | 9.000 | 1.861 | 0.426 | 14.194 | 6.821 |  |
| 000.000 | 10.000 | 2.171 | 0.689 | 14.611 | 3.833 |  |

## (2) Graphical output





[^0]:    + STELLA is a trademark licensed to High Performance Systems, Inc.

[^1]:    @ Macintosh is a trademark licensed to Apple Computer,Inc.

