

SEISMIC WAVE-PROPAGATION IN A LAYER  
OVER A HALF-SPACE

by

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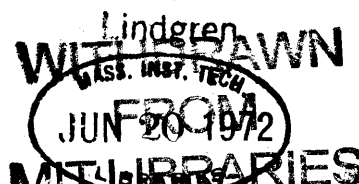
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## Abstract

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Seismic wave propagation in the near field of a point source is studied theoretically. Barker (1970) formulation is extended to include the horizontally polarized shear (SH) waves for the case of a layer over a half-space. Synthetic seismograms are then calculated for P, SV and SH sources using an approximation in the Cagniard-deHoop technique. Seismograms are displayed to show the effects of the variations of source type, source depth, range and structure on the wave-forms so obtained. Near surface P or SV sources are efficient generators of Rayleigh waves. Dispersion of Love waves become more prominent as the contrast between layer and half-space parameters increase.

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## Chapter I

### INTRODUCTION

With the advent of high-speed computers there has been an upsurge of interest in theoretical seismology. The extensive computations needed in this field seem to be less formidable now than in the past. Further, with the accumulation of large amounts of data, obtaining better and more accurate seismograms has become almost essential. Here in this thesis an attempt has been made in this direction.

HelMBERGER (1967) has shown how to compute seismic records in the high frequency range for long distances. He was mainly interested in the refractions of P and SV waves from the oceanic Mohorovicic discontinuity, well known as head waves. Harkrider (1964) also calculates theoretical seismograms for long ranges. Filson (1970), utilizing the technique developed by Pekeris et. al. (1963) computes long period  $SH_n$  records for long ranges.

Here in this thesis, an attempt has been made to compute synthetic seismograms for a simple case of a layer over a half-space. We consider a point source responsible for generating P, SV or SH wave types to be embedded in the layer. Barker (1970) has solved this problem using HelMBERGER's (1967)

approach for the case of P and SV sources. The author here incorporates an SH source into this problem and then computes seismograms for different models which could be synthesized by the use of the above sources. The Cagniard-deHoop method has been utilized to put the solution into operational form.

In order to compare synthetic seismograms with the observed ones we require a double convolution process with the response of the model. The source-function, a function describing the behavior of the source, is first convolved with the response of the model which in turn is again convolved with the instrument response to give us the synthetic seismograms. However, in this thesis we have only convolved the impulse response of the model with a source time function, a triangle of base 0.4 and area unity. This would allow us to see the effects of source type, source depth, range and structure on the wave forms thus obtained which is the main aim of this study.

The technique exposed in Barker (1970) and here requires less computer time and the results obtained are accurate for both high and low frequency ranges. Near field P, SV and SH wave seismograms computed in this thesis show the accuracy of our results. It should be remarked, however, that in order to obtain a more exact seismogram



at a distance of about 50 or 100 km for P, SV case a greater number of rays have to be incorporated, which increases the computation time considerably. As a further test, comparisons have been made with the results of Pekeris et. al. (1963,65) for P, SV and SH sources.

Chapter II deals with the statement and the formulation of the problem. Here we solve the inhomogeneous wave equation by the Laplace Transform technique, which is simple and straightforward. Chapter III deals with the computation of seismograms. Finally in Chapter IV we outline the conclusions reached by undertaking this study.

## Chapter II

### THEORETICAL FORMULATION OF THE PROBLEM

Let us consider a homogeneous, linearly isotropic, elastic half-space overlain by a homogeneous, linearly isotropic elastic layer. Further, let there be a point source of P, SV and SH waves in the layer. The geometry of the assumed model is shown in Figure 1. We would like to formulate the problem in circular cylindrical coordinates  $(r, \theta, z)$ . The angle  $\theta$  would not appear in the final form of the expression for the displacement because of the axial symmetry of the source. Let  $\lambda$  and  $\mu$  define Lamé's constants,  $\rho$  be density,  $\alpha$  and  $\beta$  denote compressional and shear (SV and SH both) wave velocities.

The response at the observation point A can be calculated by solving the inhomogeneous wave equation, e.g., for SH waves

$$\mu_1 \nabla^2 u_\theta(r, z, t) - \rho \frac{\partial^2 u_\theta(r, z, t)}{\partial t^2} = \frac{H(t) \delta(r) \delta(z-h)}{2\pi r} \quad (1)$$

where  $u_\theta(r, z, t)$  denotes the component of the displacement in the  $\theta$  direction.  $H(t)$  is the Heaviside unit step-function defined as

$$H(t) = \begin{cases} 0 & t < 0 \\ 1 & t > 0 \end{cases}$$

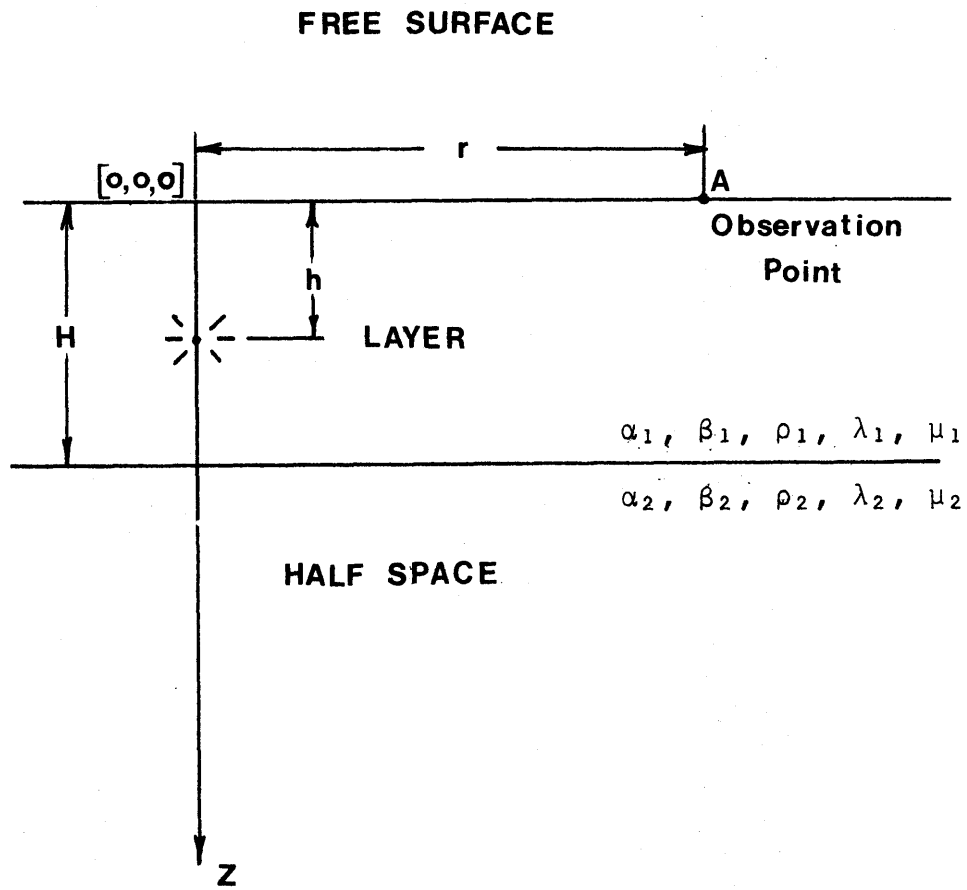


FIG. 1

and  $\delta$  denotes the Dirac-delta function. The quantity on the right-hand side of Equation 1 represents the force produced by the point source of torque about the z-axis in the layer. We then exploit Laplace Transform technique to solve Equation 1, as done by Helmberger (1967). The details have been given in Appendix A.

The once-transformed in time displacement due to the nth generalized ray can be written [Barker(1970)] as

$$\bar{u}_{z,n}(r,0,s) = s \operatorname{Im} \int_0^{i\infty} p F_{n,z}(p) K_0(spr) e^{-sg_n(p)} dp \quad (2)$$

$$\bar{u}_{r,n}(r,0,s) = s \operatorname{Im} \int_0^{i\infty} p F_{n,r}(p) K_1(spr) e^{-sg_n(p)} dp \quad (3)$$

and

$$\bar{u}_{\theta,n}(r,0,s) = s \operatorname{Im} \int_0^{i\infty} p F_n(p) K_0(spr) e^{-sj_n(p)} dp \quad (4)$$

where a bar has been placed over the quantity whose Laplace transform has been taken. In the above equations,  $s$  denotes the transform variable in complex frequency,  $p$  is the complex integration variable, and the  $\operatorname{Im}$  symbol means that only the imaginary part of the complex function is considered. Further,  $K_0(spr)$  and  $K_1(spr)$  are the modified Bessel functions of zero and first order respectively. The notation  $u_{z,n}(r,z,t)$  and

$u_{r,n}(r,z,t)$  represent the vertical and the radial components of displacement for P or SV source and similarly  $u_{\theta,n}(r,z,t)$  is the component of the displacement in the  $\theta$  direction for an SH source. However, in Equations 2, 3 and 4 these displacements have been Laplace transformed in time. The functions  $F_{n,z}(p)$ ,  $F_{n,r}(p)$  and  $F_n(p)$  are

$$F_{n,z}(p) = S R_z(p) \zeta_n(p)$$

$$F_{n,r}(p) = S R_r(p) \zeta_n(p)$$

and

$$F_n(p) = S R \zeta'_n(p)$$

where

$$\begin{cases} S = 1/2\pi^2\eta_1(\lambda_1+2\mu_1) & \text{for P source} \\ S = 1/2\pi^2\eta_1\mu_1 & \text{for SV \& SH source} \end{cases}$$

and

$$\eta_1 = \left(\frac{1}{\alpha_1^2} - p^2\right)^{1/2} \quad \eta_2 = \left(\frac{1}{\beta_1^2} - p^2\right)^{1/2}$$

where  $\alpha_1$  and  $\beta_1$  are the compressional and shear (SV and SH) wave velocities in the layer. The functions  $R_z(p)$ ,  $R_r(p)$  and  $R$  are the responses due to the presence of the free surface for an upgoing P or SV and SH wave.  $\zeta_n(p)$  and  $\zeta'_n(p)$  are the reflection coefficient for the  $n$ th generalized ray for P or SV and SH sources. These functions have been written out explicitly in the Appendix B. Finally, the function  $g_n(p)$  and  $j_n(p)$  are given by

For P and SV waves:

$$g_n(p) = (1 - HK_{ud} - h) [(1 - K_{sp}) \eta_1' + K_{sp} \eta_1] + l_s^{(n)} \eta_1' H + l_p^{(n)} \eta_1 H$$

and for SH waves

$$j_n(p) = [2h - H] K_{ud} \eta_1' + [H - h] \eta_1' + l_s^{(n)} \eta_1' H$$

where

$$K_{ud} = \begin{cases} 1 & \text{if, at the source, the ray is directed upward} \\ 0 & \text{if, at the source, the ray is directed downward} \end{cases}$$

and

$$K_{sp} = \begin{cases} 1 & \text{if the source emits P waves} \\ 0 & \text{if the source emits SV waves} \end{cases}$$

$l_s^{(n)}$  denotes the number of traverses made by the  $n$ th ray as an SV or SH wave. Similarly,  $l_p^{(n)}$  is the number of traverses as a P wave.

We choose to approximate  $K_0(\text{spr})$  and  $K_1(\text{spr})$  by its asymptotic expansion for large arguments and making use of the Laplace inversion formulae [See Barker (1970)] to get

$$u_{z,n}(r,0,t) = \text{Im} \frac{\partial}{\partial t} \left\{ \frac{1}{\sqrt{t}} * \left[ \sqrt{\frac{p}{2r}} F_{n,z}(p) \frac{dp}{dt} - \frac{1}{8} H(t) * \left( \frac{1}{\sqrt{2pr^3}} F_{n,z}(p) \frac{dp}{dt} \right) + \frac{9}{128t} * \left( \frac{1}{\sqrt{2p^3 r^5}} F_{n,z}(p) \frac{dp}{dt} \right) \right] \right\} \quad (5)$$

$$u_{r,n}(r,0,t) = \text{Im} \frac{\partial}{\partial t} \left\{ \frac{1}{\sqrt{t}} * \left[ \sqrt{\frac{p}{2r}} F_{n,r}(p) \frac{dp}{dt} - \frac{3}{8} H(t) * \left( \frac{1}{\sqrt{2pr^3}} F_{n,r}(p) \frac{dp}{dt} \right) + \frac{3}{128t} * \left( \frac{1}{\sqrt{2p^3 r^5}} F_{n,r}(p) \frac{dp}{dt} \right) \right] \right\} \quad (6)$$

$$\bar{u}_{\theta,n}(r,0,t) = \text{Im} \frac{\partial}{\partial t} \left\{ \frac{1}{\sqrt{t}} * \left[ \sqrt{\frac{p}{2r}} F_n(p) \frac{dp}{dt} - \frac{1}{8} H(t) * \right. \right. \\ \left. \left. \left( \frac{1}{\sqrt{2pr^3}} F_n(p) \frac{dp}{dt} \right) + \frac{9}{128} t * \left( \frac{1}{\sqrt{2p^3 r^5}} F_n(p) \frac{dp}{dt} \right) \right] \right\} \quad (7)$$

where \* denotes convolution. We have done calculations based on Equations 5, 6 and 7. We use only the first two terms in the modified Bessel function which holds good for large arguments, i.e. for long ranges. It seems that for long ranges we get most of the contribution in Bessel function's asymptotic expansion from the first term as it should be. A computer program for evaluating Equations 5, 6 and 7 has been given in Appendix C with a detailed listing. However, we would like to add that the computations for all cases discussed in this thesis, we have taken 64 generalized rays. Pekeris et al. (1963,65) have used almost as much as 5 times the number of rays we have used.

In order to get synthetic seismograms the impulse response obtained from evaluating Equations 5, 6 and 7 is convolved with a suitable source-time-function. (Figure 2a).

The step-function with rounded shoulders defined by Figure 2a is mathematically equivalent to (where  $\Delta$  is the digitization interval)

$$f(t) = 0 \quad t < 0 \\ = \frac{1}{2} t^2 \quad 0 < t < \Delta \quad (8)$$

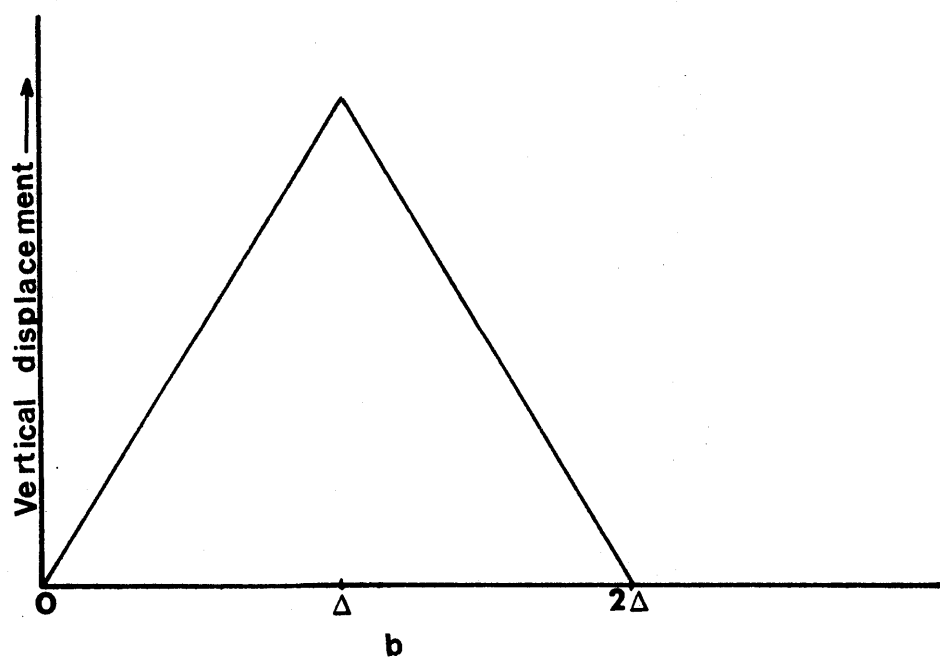
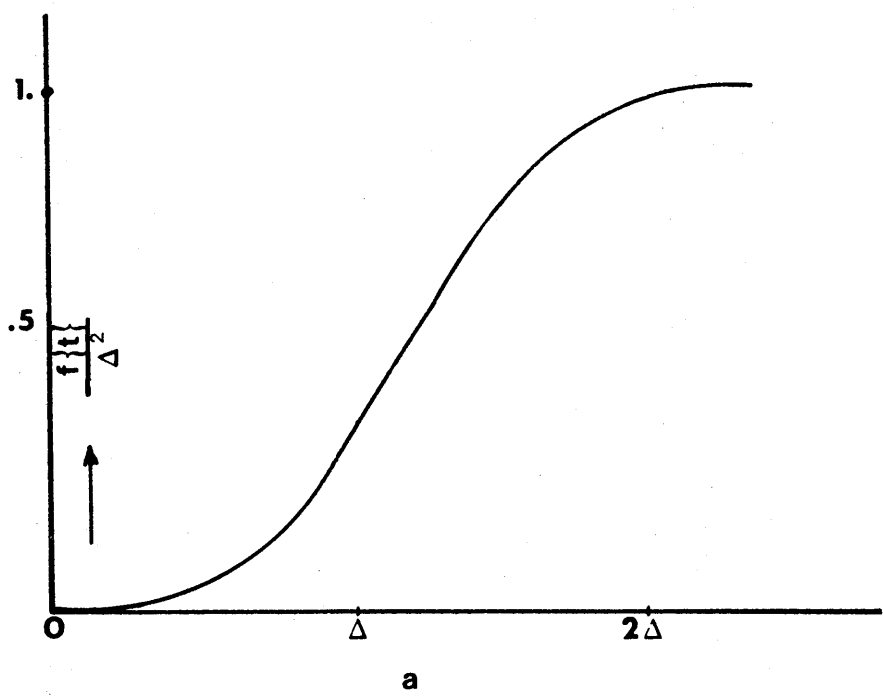


FIG. 2



$$\begin{aligned}
 f(t) &= \frac{1}{2}t^2 - (t-\Delta)^2 & \Delta < t < 2\Delta \\
 &= \frac{1}{2}t^2 - (t-\Delta)^2 + \frac{1}{2}(t-2\Delta)^2 = \Delta^2 & 2\Delta < t
 \end{aligned}
 \tag{8}$$

At long distances Equation 8 produces saw-tooth-like displacements, as shown in Figure 2b. The impulse response obtained by evaluating Equations 5, 6 and 7 was convolved with a triangle of base  $\cdot 4$ , and an area of unity. This is true of all the plots shown in this thesis.

We should be careful in using equations 5, 6 and 7 because they hold good for sufficiently long ranges and large times, otherwise we cannot justify the use of asymptotic expansion for the modified Bessel functions  $K_0(\text{spr})$  and  $K_1(\text{spr})$ .

## Chapter III

### COMPUTATION OF SEISMOGRAMS

Synthetic seismograms for a layer over a half-space have been computed in the distance range zero to 100 km using the numerical technique described in the previous chapter. Barker (1970) computer program was modified to take into consideration SH wave option. Seismograms have been calculated to investigate the effects of structure, source-type, source-depth and distance range. In all the synthetic seismograms presented in this thesis, the impulse response is convolved with a triangle of base 0.4 sec and area unity. For structure we chose two separate crustal models listed in Table I. Model I represents a 10 km thick granitic layer over a gabbroic half-space. Model II represents a sedimentary basin with a 2 km thick sedimentary layer overlying hard basement rock. To see the effect of source-type, we computed theoretical seismograms for P, SV and SH wave sources. We embedded each of these sources in case of Model I at 5, 2 and 5 km, while in Model II the source-depth was 1 km. We have made computations for 50 and 100 km distance range and in one case for 20 km.

Now let us examine each of the above-mentioned factors in detail. We start our discussion with source effects

beginning with a P source at different depths in the Model I (Figures 3, 4). The seismograms show that the record begins with P wave refractions, which is later followed by reflections and Rayleigh waves. Here it is very clear that shallow P sources generate Rayleigh waves quite efficiently. As we increase the source depth we see a change in the surface wave amplitude and spectral characteristics. Now to determine the range effect we use a P source and Model II. In Figures 5 and 6 we see that as we increase the range, we get well-defined P reflections arriving at  $t = 25.3$  sec. and also at later times.

To illustrate the effect of source type we go back to Model I but this time use an SV source at different depths for range 50 km. This is shown in Figures 7 and 8. Here we see that Rayleigh wave is an outstanding feature. In Figures 9 and 10 we consider the same model as has been used above, but now at the 100 km range. The first of these figures represents the early part of the seismogram showing the refracted and reflected arrivals. We did this just to show the similarity in body wave-forms for different source depths. Later in Figure 10 we display the generation of Rayleigh waves. These are so strong and large in amplitude that on a scale such as the one used in Figure 10, we could not see any other type of waveforms. In the real world, when we are actually recording the events, the response of the instrument can be

controlled, which enables us to see different sorts of waveforms, though they differ greatly in amplitudes. We computed for an SV source, Model II and a range of 50 km, both the early part and the later part of the seismograms (Figure 11a,b).

Further, we also compare records obtained for different ranges using Model II. This is shown in Figure 12, for body waves. Then we compare the z component of the seismogram for Model II for SV and P sources for a range of 50 km (Figure 13). We see a resemblance between the two waveforms which we should expect. We can also see that the Rayleigh wave generated by an SV source has a larger amplitude than for a P source. It is clear that an SV source is a more efficient generator of Rayleigh waves than a P source, for the simple reason that the integration contour comes closer to the real axis in the case of the SV source.

Following our earlier procedure we examine the source-depth effect on the computed model seismograms for an SH source. To begin with, we look at Model I and range 50 km. This is shown in Figure 14. There is a very close resemblance in waveform shape for source-depths 0.5, 2 and 5 kms. We can clearly see the  $SH_n$  arrival (in Figure 14 b,c), which is followed by SH reflections. There is no indication of dispersed Love waves. We again consider the same model but increase the range to 100 km (Figure 15). We see a long quiet period

beginning with refracted SH arrivals followed by SH reflections. Finally we consider Model II and here we investigate the range effect. Figure 16 shows the synthetic seismograms for the ranges 20, 50 and 100 km. In all of these seismograms we can see the generation of Love waves, which clearly stand out with their relatively larger amplitudes than the body waves.

## Chapter IV

### CONCLUSION

In this thesis, we investigated the effects of source type, source depth, range and structure on seismic wave propagation in a layer over a half-space. We considered compressional sources, vertical torque (SV) and horizontal torque (SH) as point source models. A close examination of the synthetic seismograms discussed in the last chapter revealed the following

(a) A relatively thin high-contrast layer accentuates the surface waves on the seismogram by increasing the dispersive effects in near-fields.

(b) Source-depth plays a very important role in determining the relative amplitude of the surface waves. Frequency content of these waves are also affected by the source-depth.

(c) For a given structure and source depth, SV type sources generate Rayleigh waves more efficiently than purely compressional (P type) sources.

(d) Body wave response (early portion of the seismogram) changes more rapidly with distance than the surface wave response.

(e) An extension of this work is to compare the theoretical seismograms with those of field data and to investigate earthquake source characteristics. However, before this can be done we need to incorporate the instrument response and realistic source-time function in the calculation of synthetic seismograms.

Table I

## MODELS FOR COMPUTATION

## Model I

Layer Thickness  $H = 10$  km.

	$\alpha$ (km/sec)	$\beta$ (km/sec)	$\rho$ (gm/cc)	$\sigma$
Layer	5.	2.9	2.7	.25
Half-Space	7.2	4.2	2.9	.25

## Model II

Layer Thickness  $H = 2$  km.

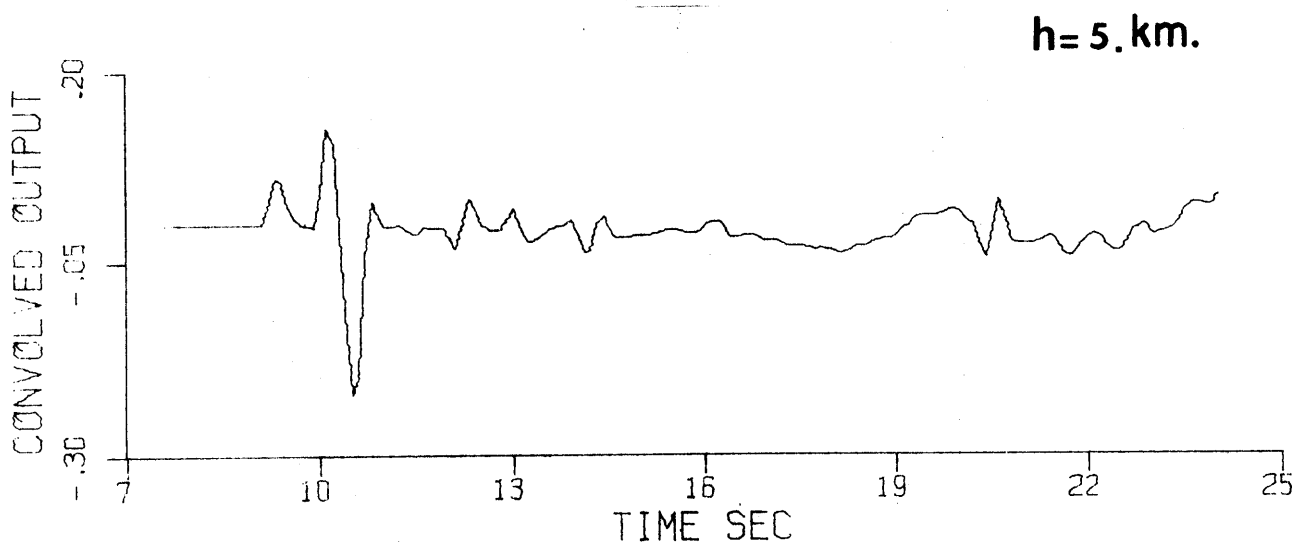
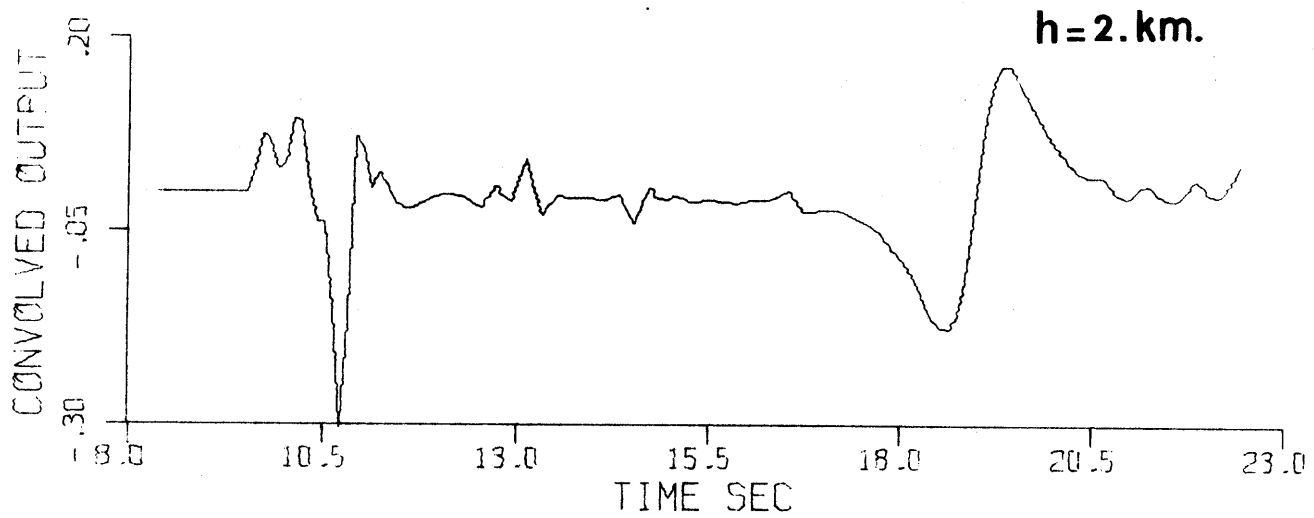
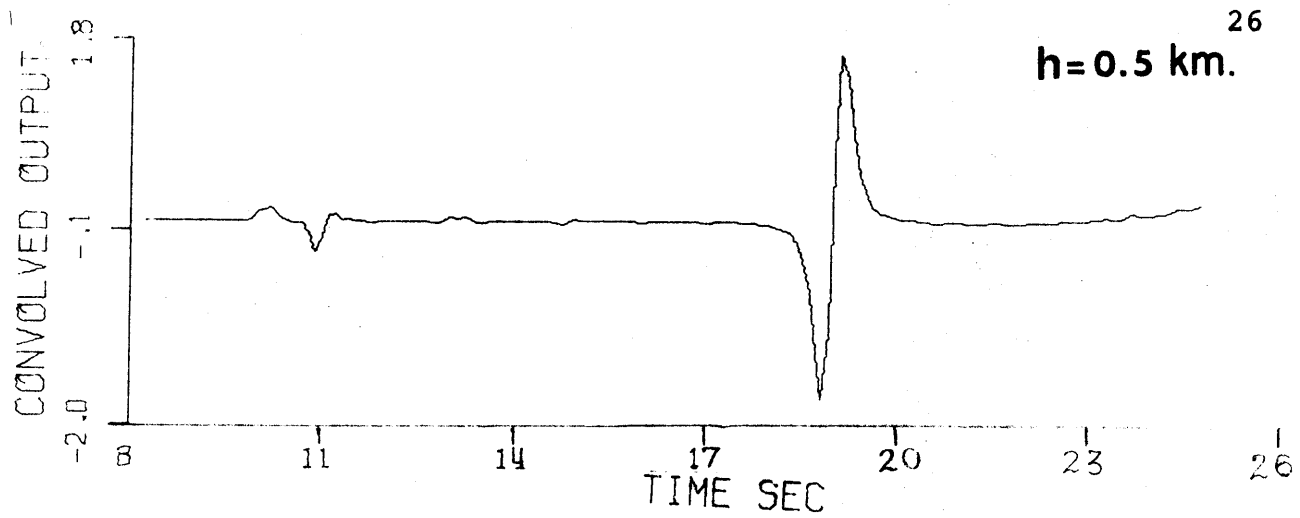
	$\alpha$ (km/sec)	$\beta$ (km/sec)	$\rho$ (gm/cc)	$\sigma$
Layer	4.0	2.9	2.2	.25
Half-Space	6.0	3.46	2.4	.25

In both Models I and II  $\alpha$  denotes a compressional wave velocity.  $\beta$  denotes shear wave velocity,  $\rho$  denotes density and  $\sigma$  denotes Poisson's ratio. Unless otherwise stated, source-depth is one-half the layer thickness.

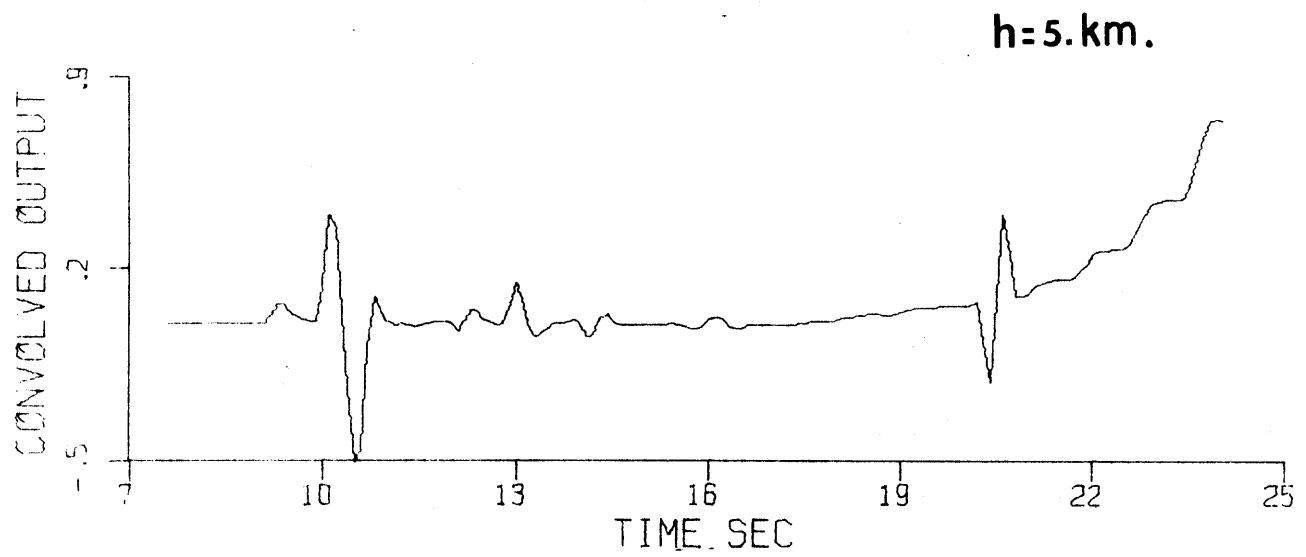
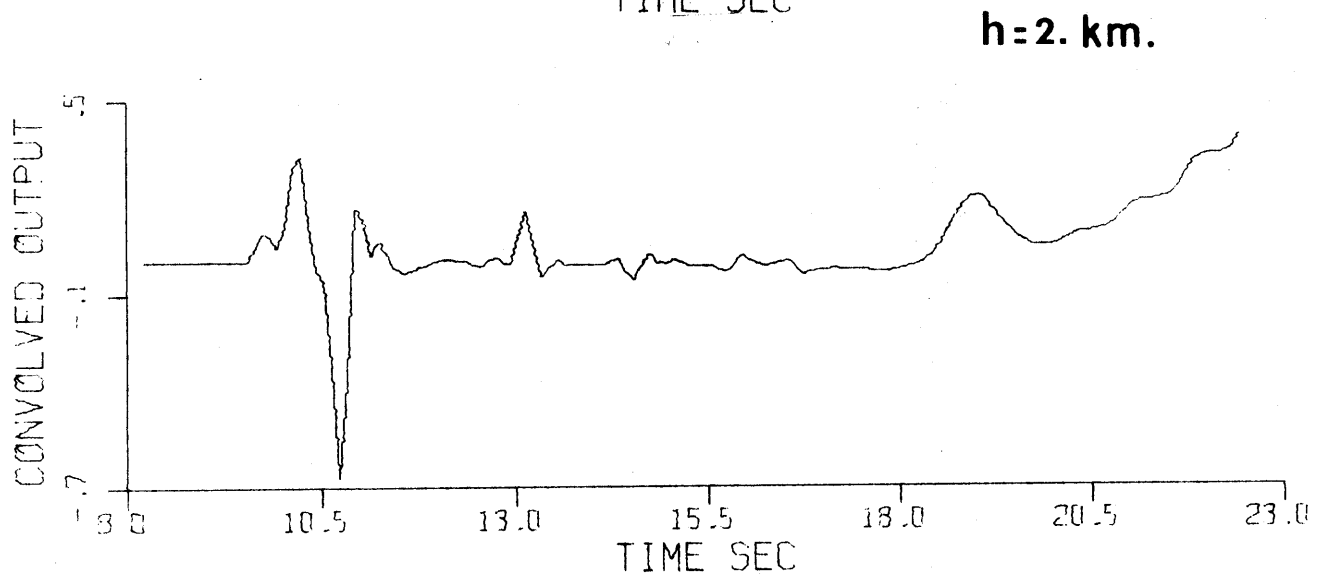
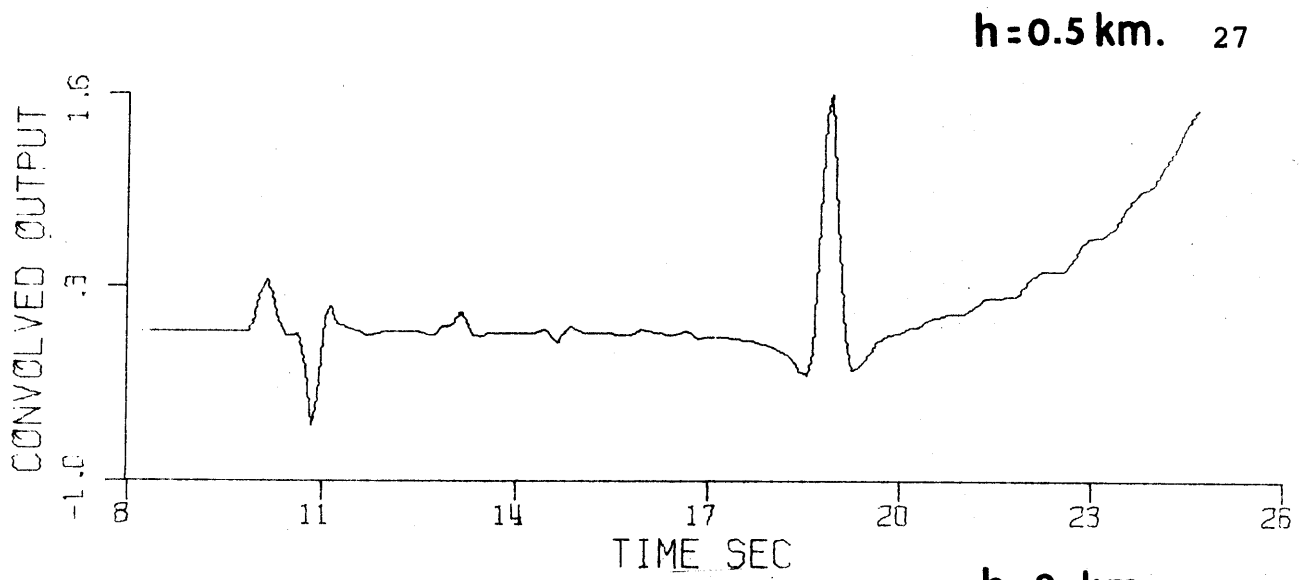


## COMPUTER PLOTS

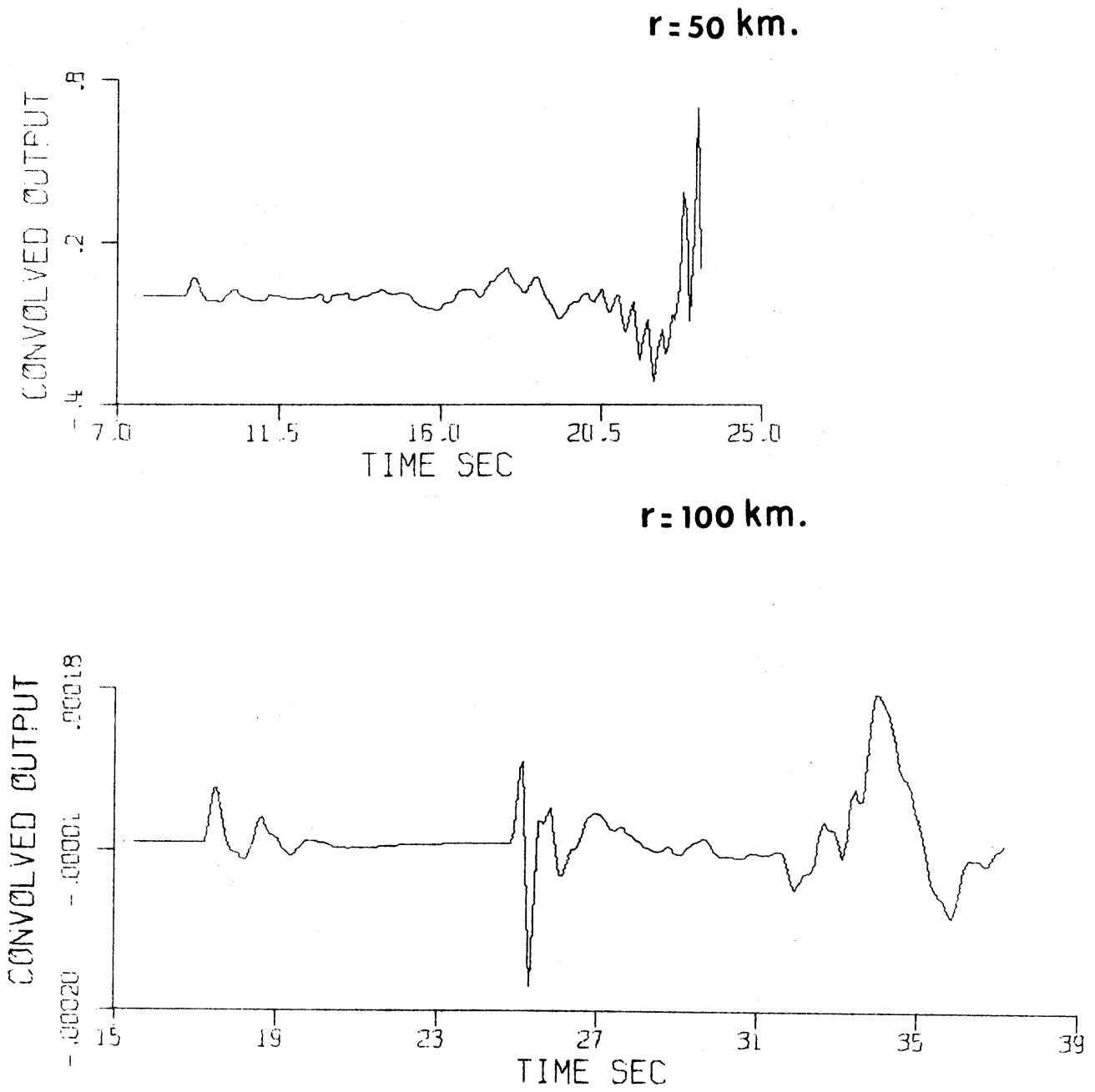
In the figure captions, the first entry refers to the source type (P, SV, SH and C<sub>0</sub>, where the last symbol means simultaneous comparison of two source types), second to component (Z and R for P and SV cases, otherwise omitted in SH case where only radial component can be plotted), third to the model (I or II) and finally fourth, to the range (20, 50 or 100 km. or C, in which case the seismograms are simultaneously compared at two ranges for the same model). Unless otherwise stated, source-depth is one-half the layer thickness. However, while examining the plots we should note the variation of the amplitude scale. It should also be emphasized that the horizontal (time) scale is not always uniform in all the plots.



**FIG. 3. P,Z,I,50**

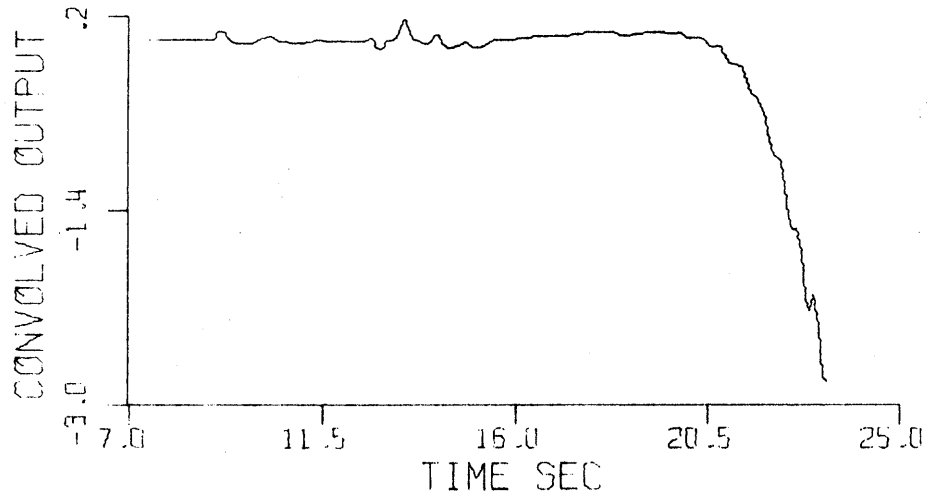


**FIG. 4. P,R,I,50**



**FIG. 5. P,Z,II,C**

r=50 km.



r=100 km.

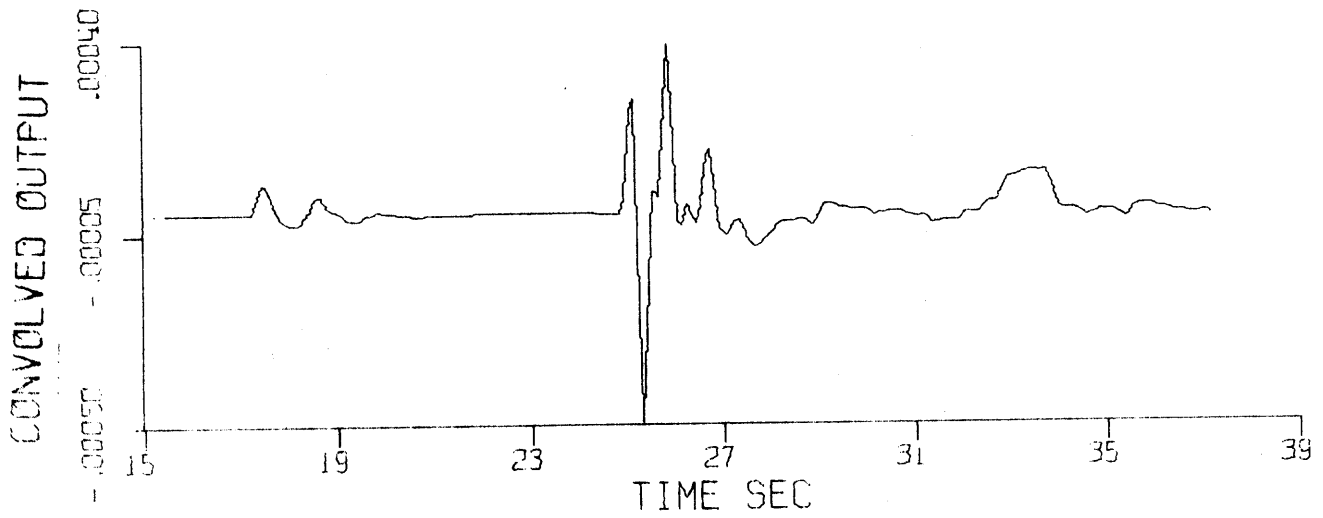


FIG. 6. P,R,II,C

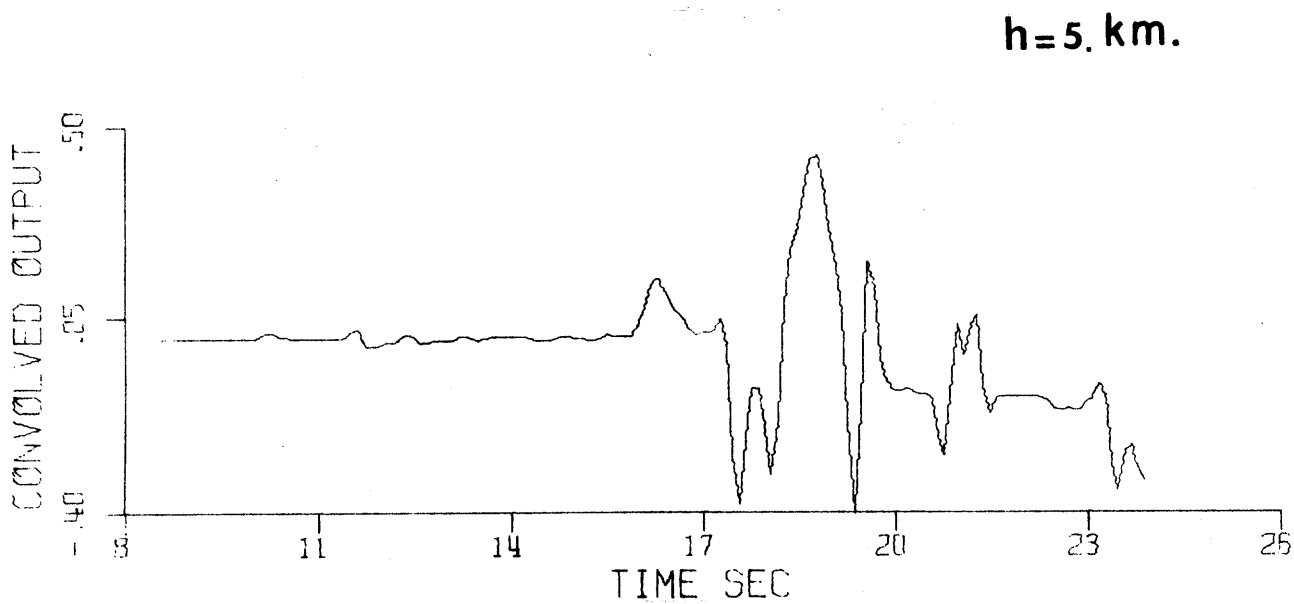
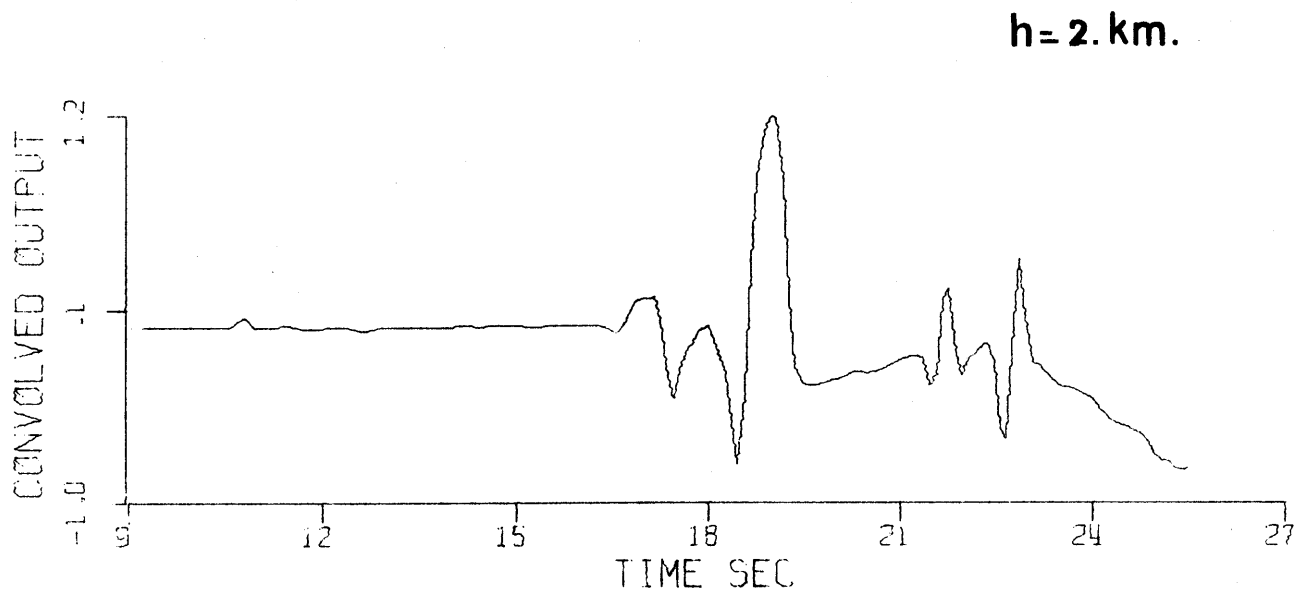
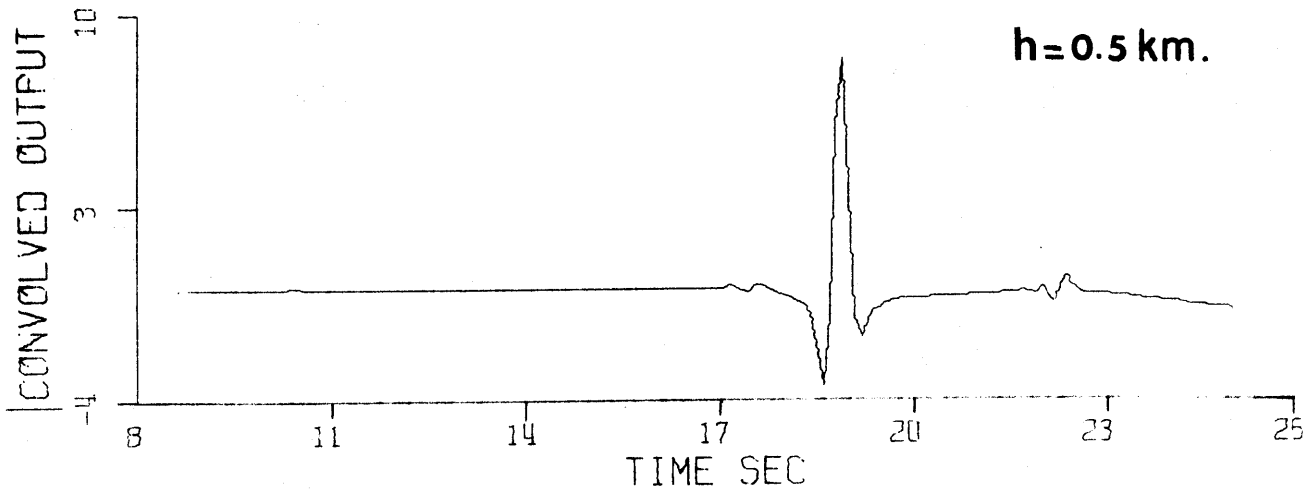
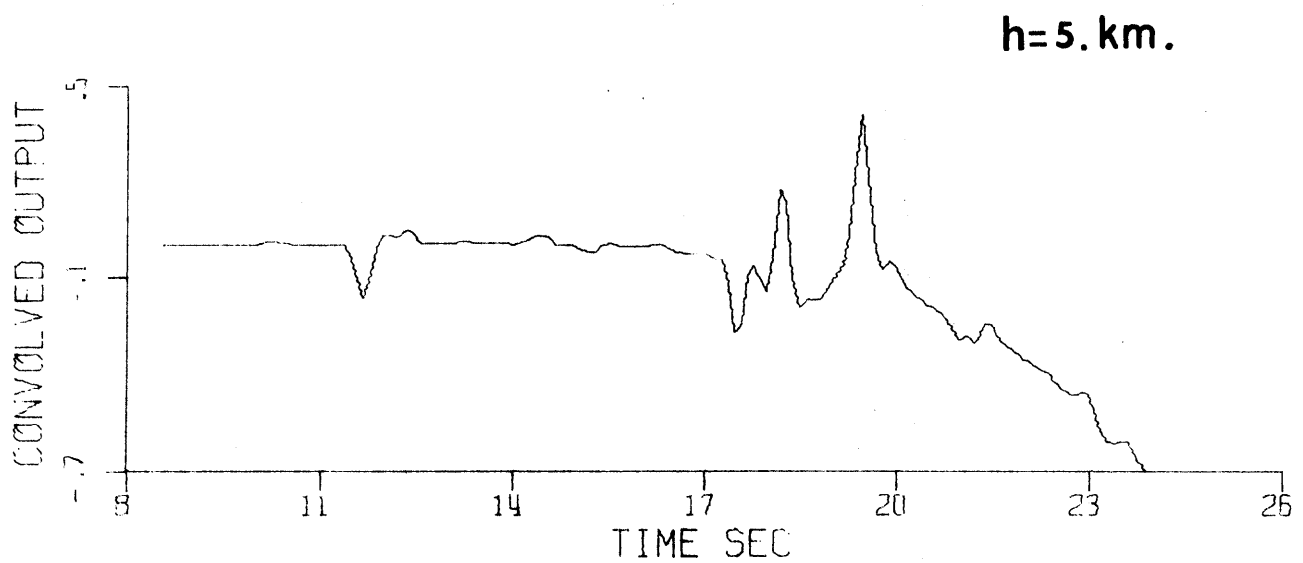
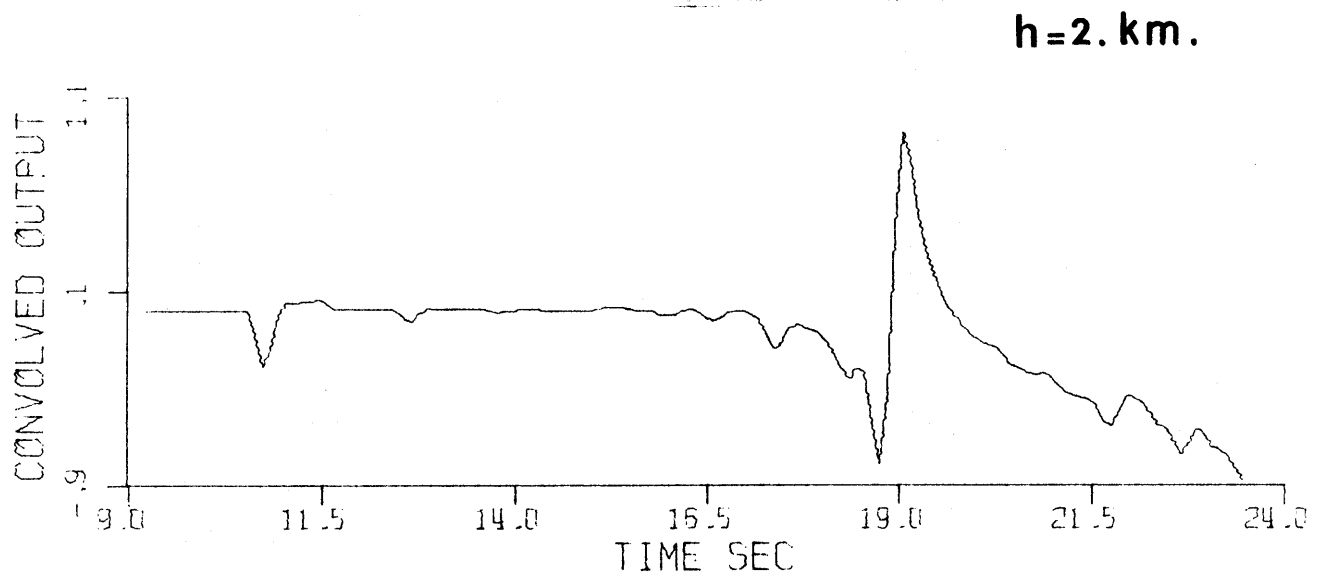
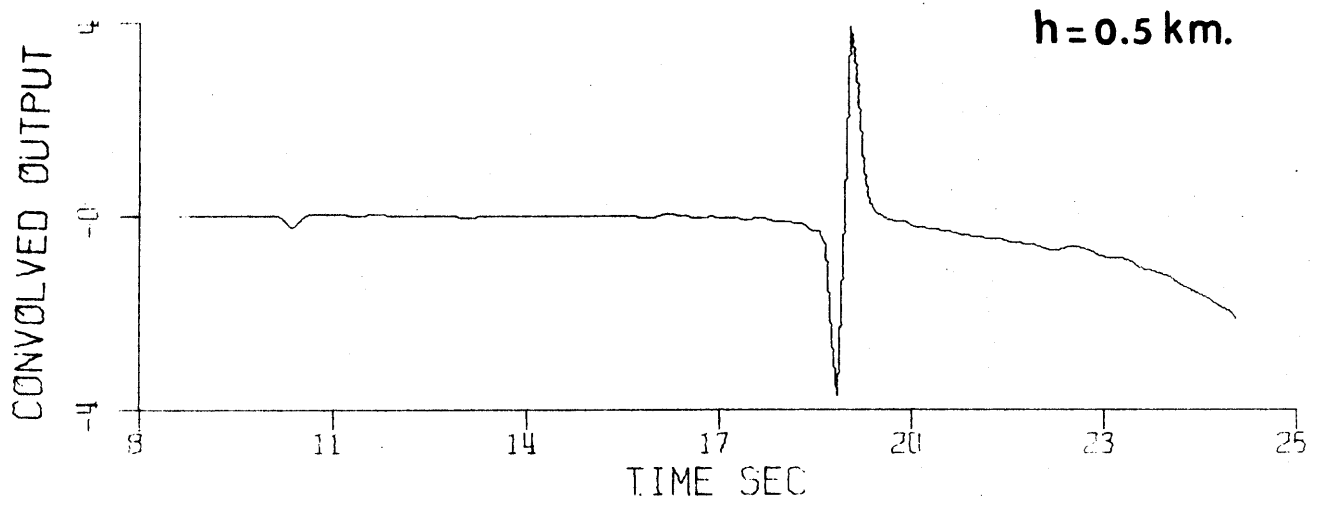


FIG. 7. SV, Z, I, 50



**FIG. 8. SV, R, I, 50**

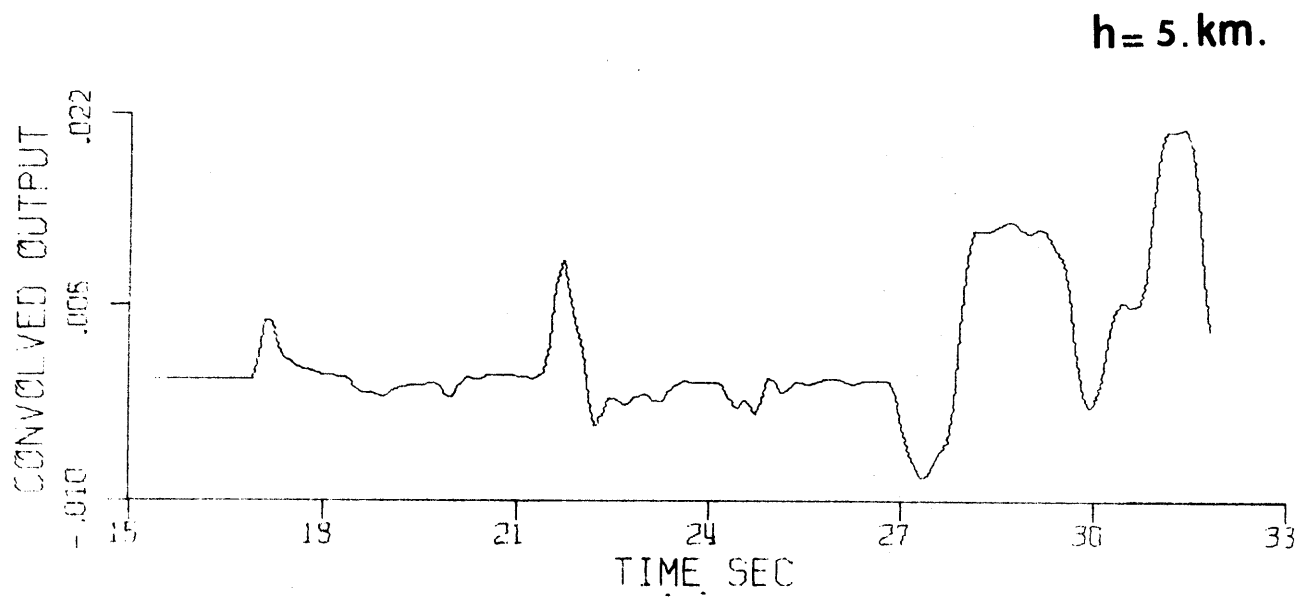
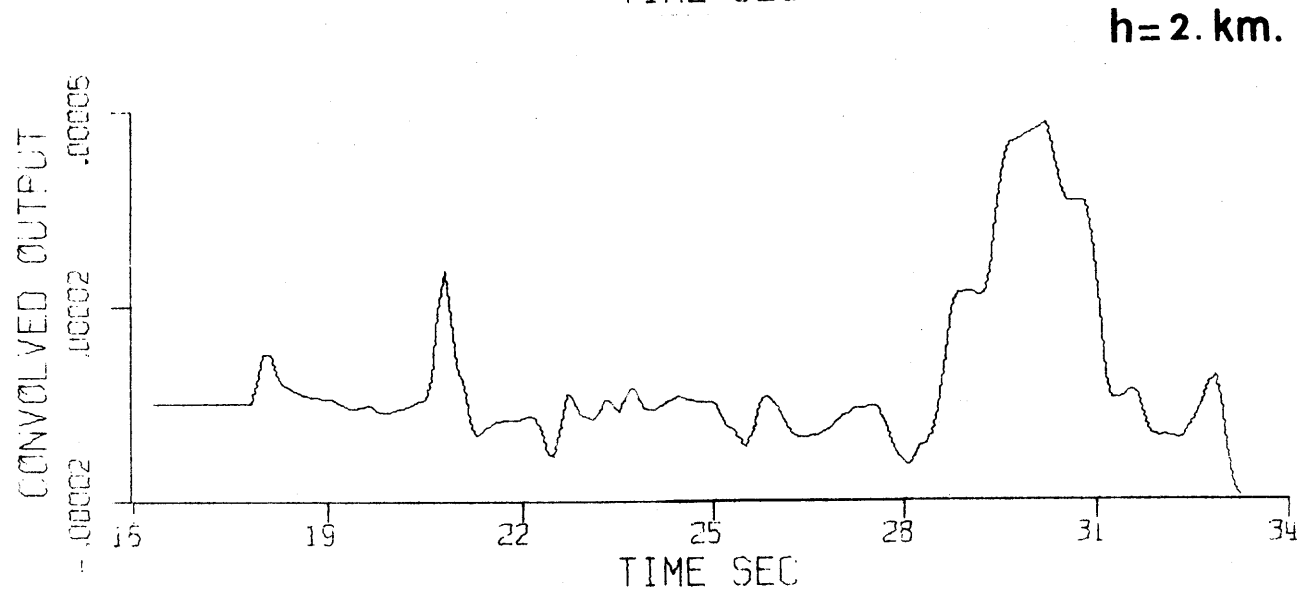
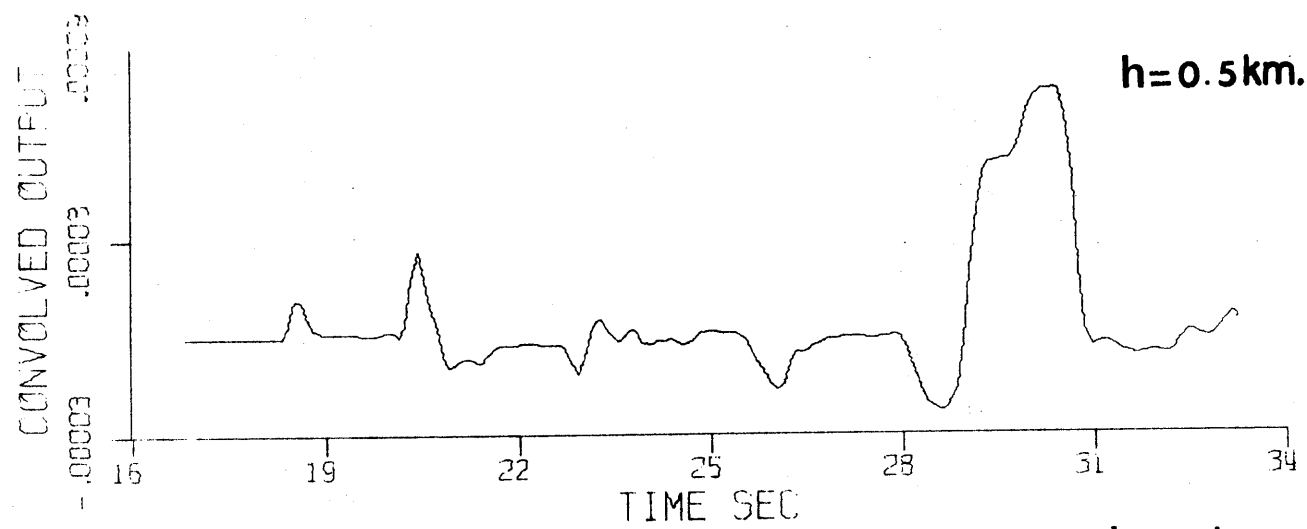
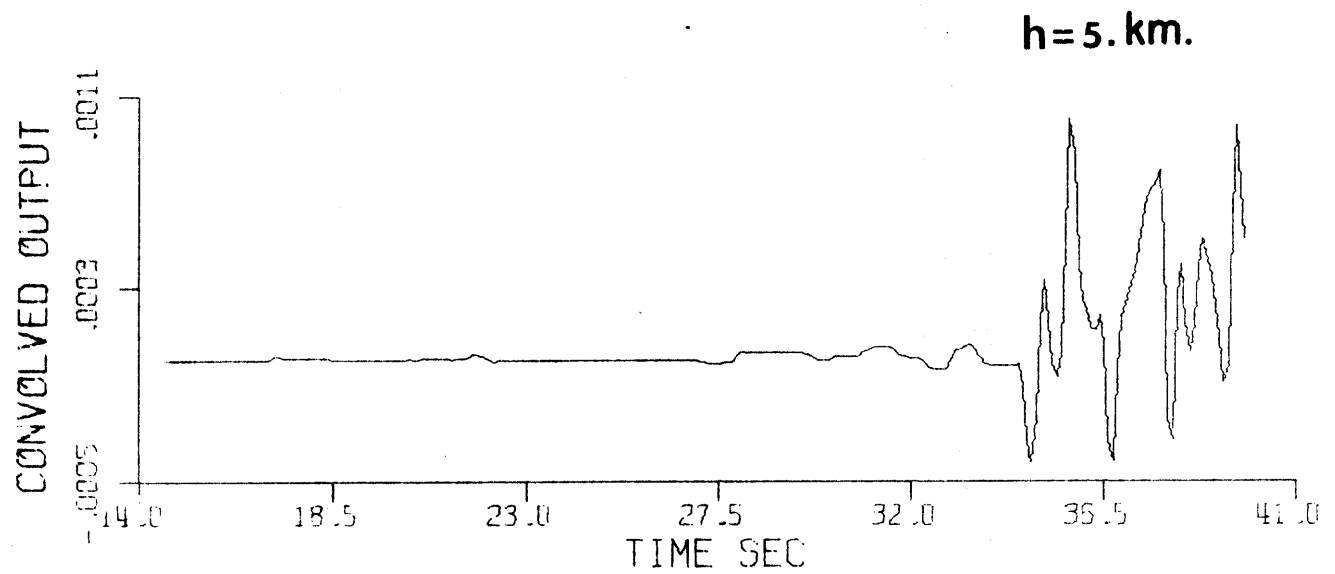
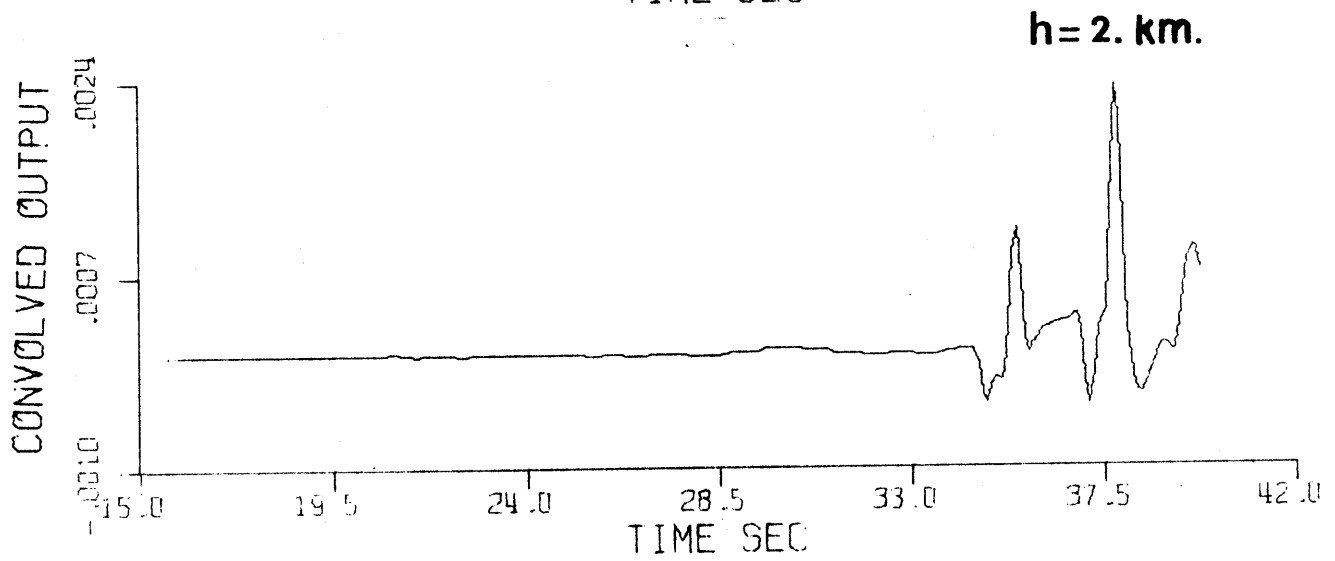
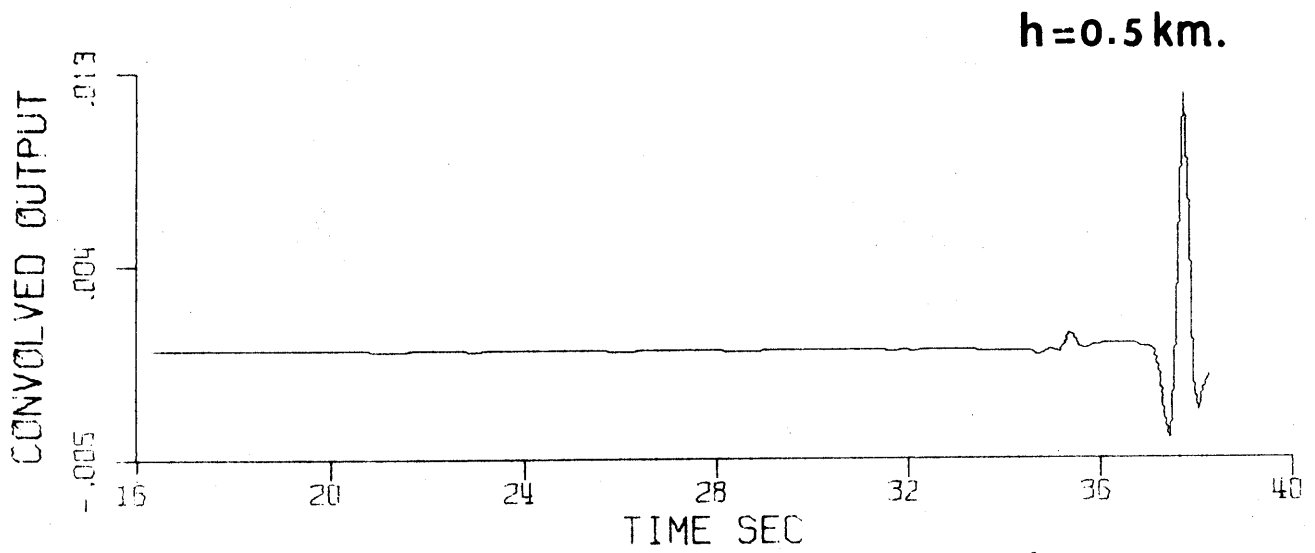
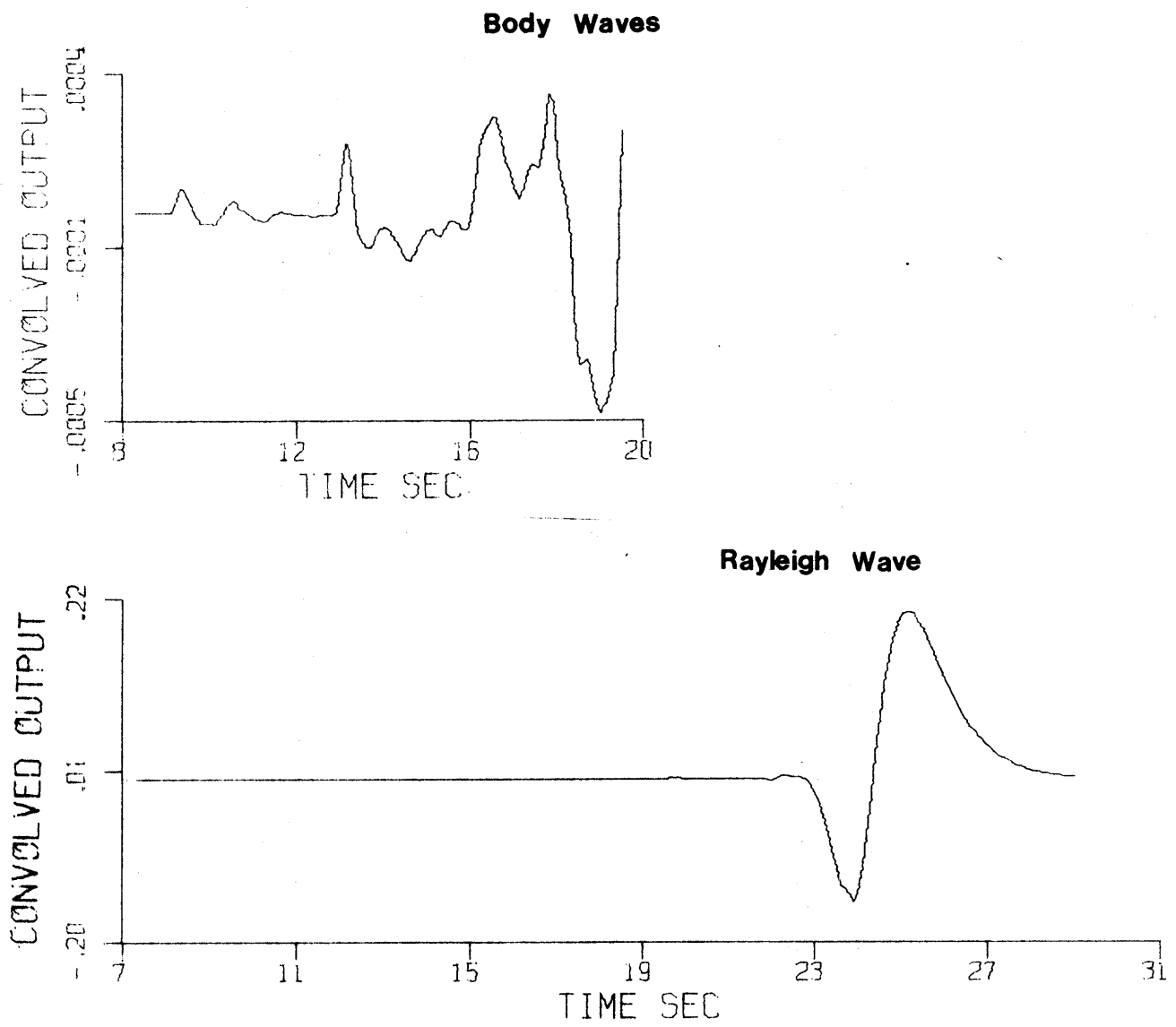


FIG. 9. SV, Z, I, 100

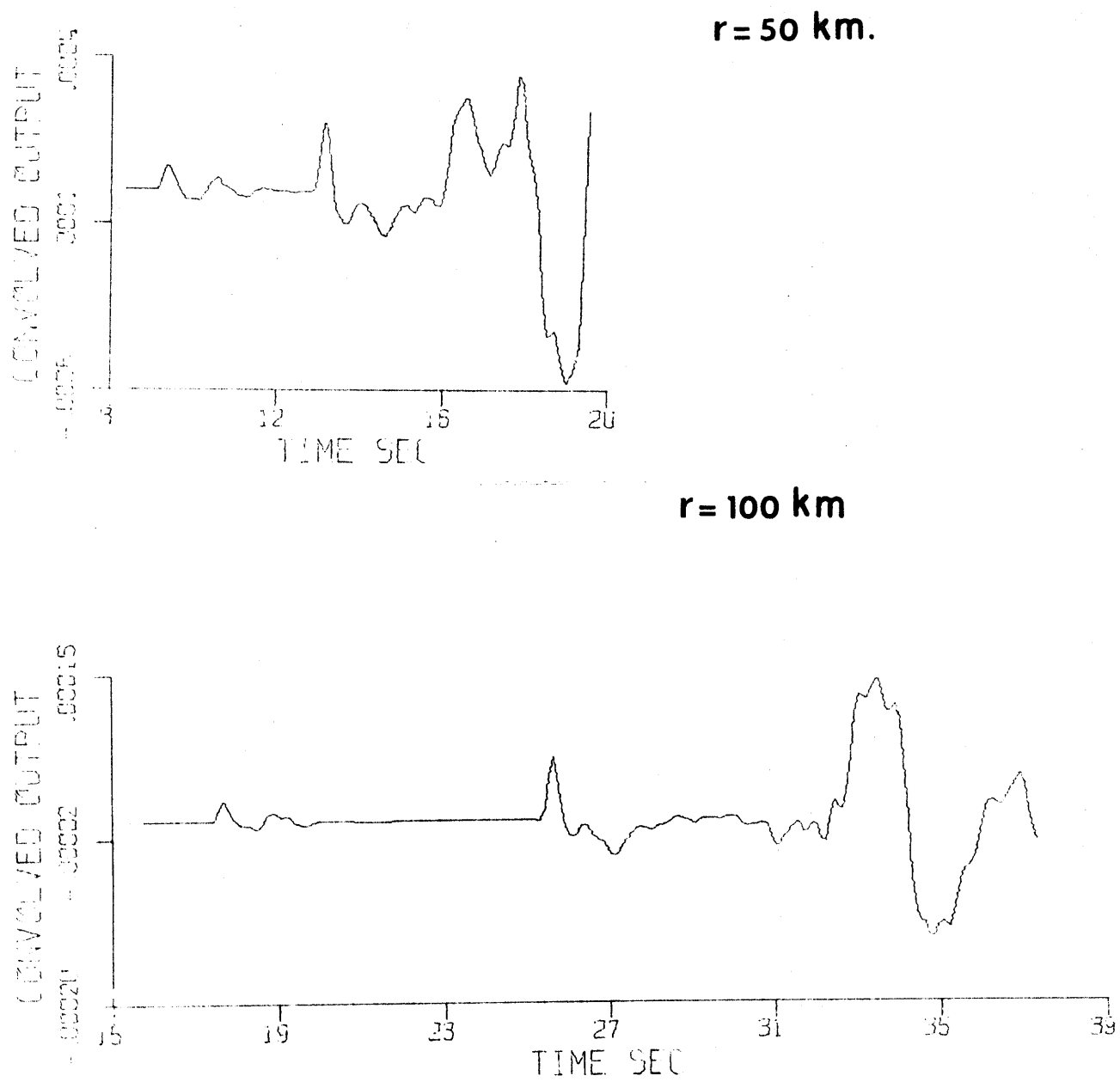




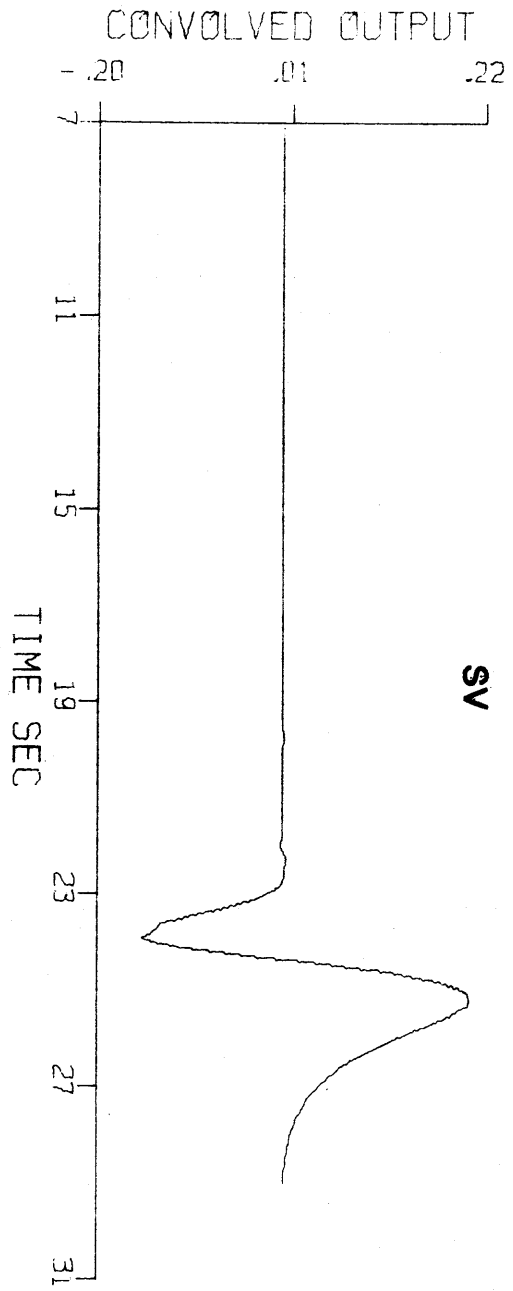
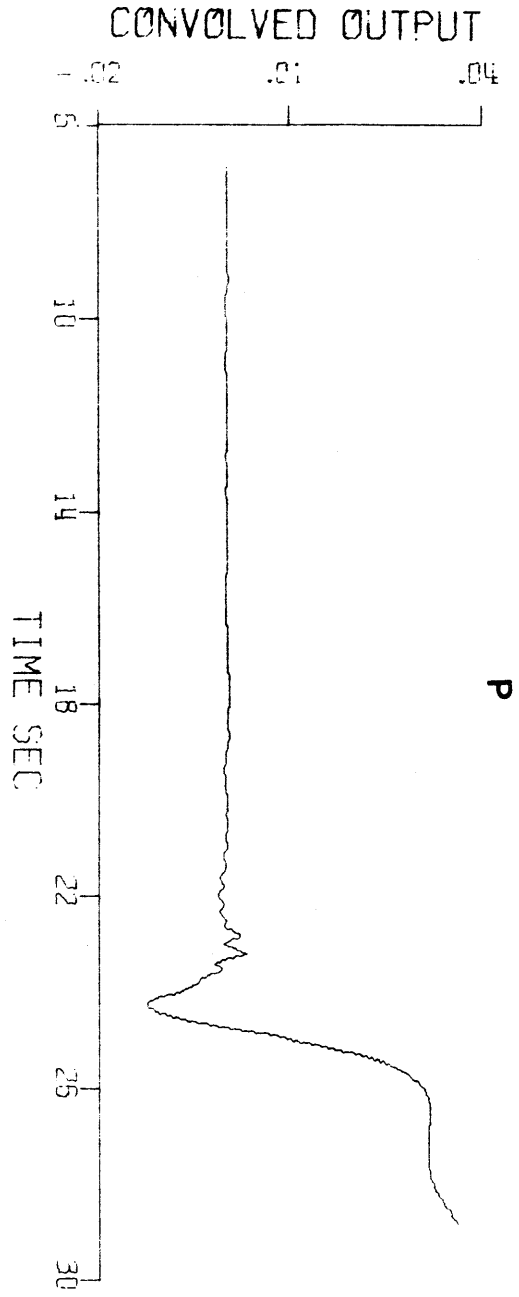
**FIG. 10 SV, Z, I, 100**



**FIG. 11. SV, Z, II, 50**



**FIG. 12. SV, Z, II, C**



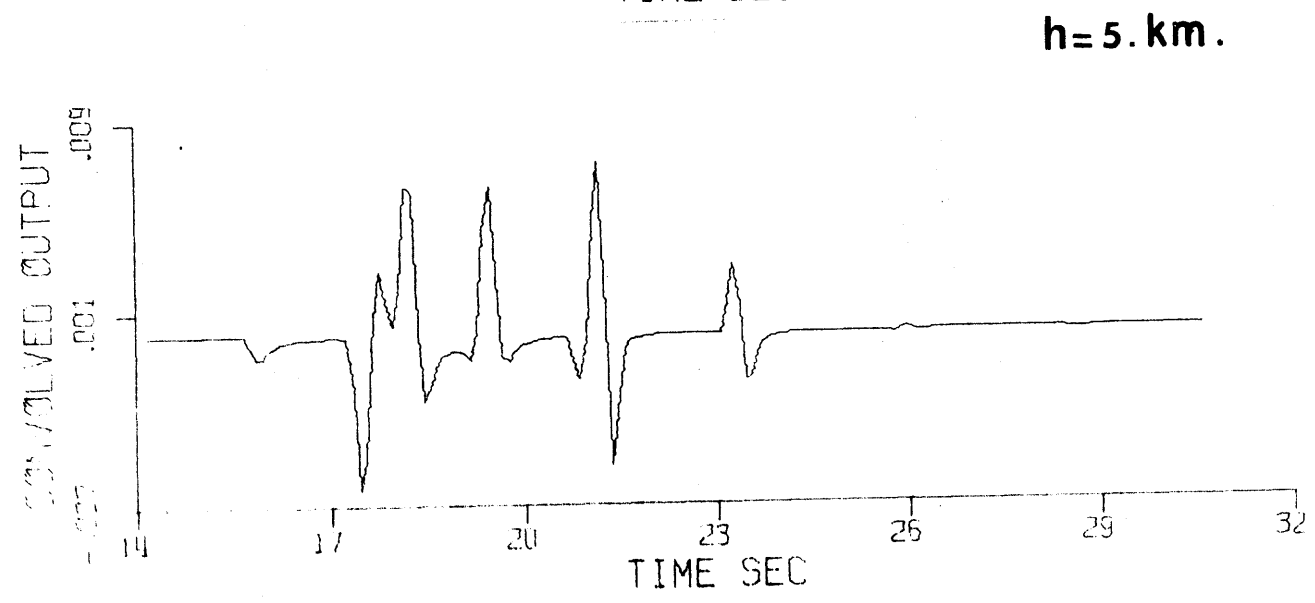
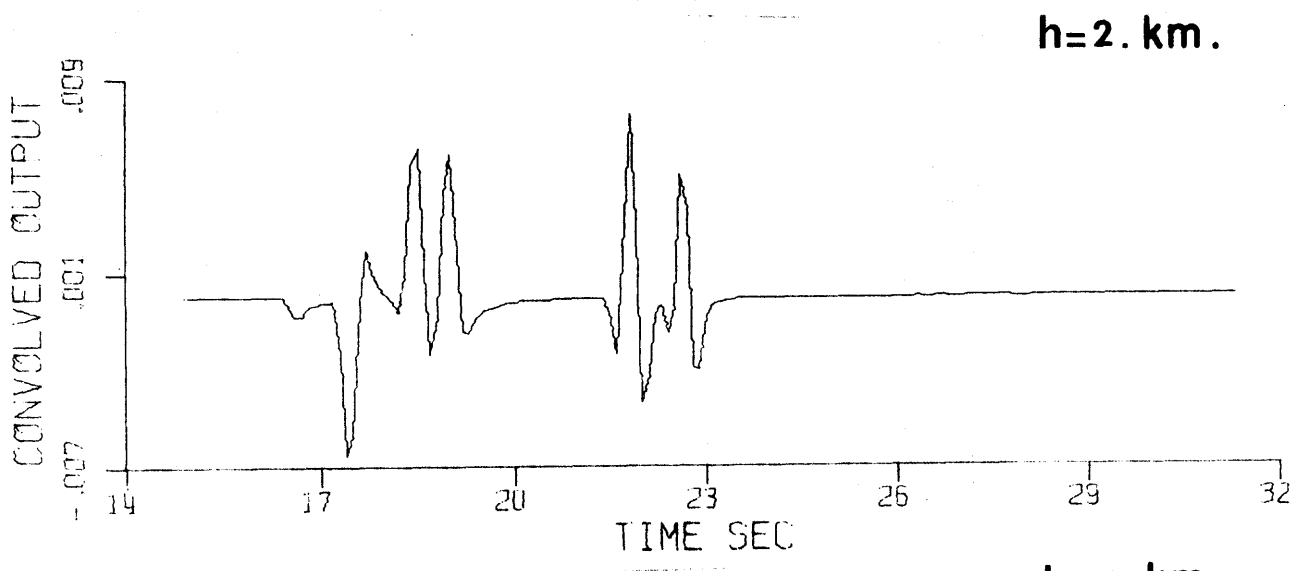
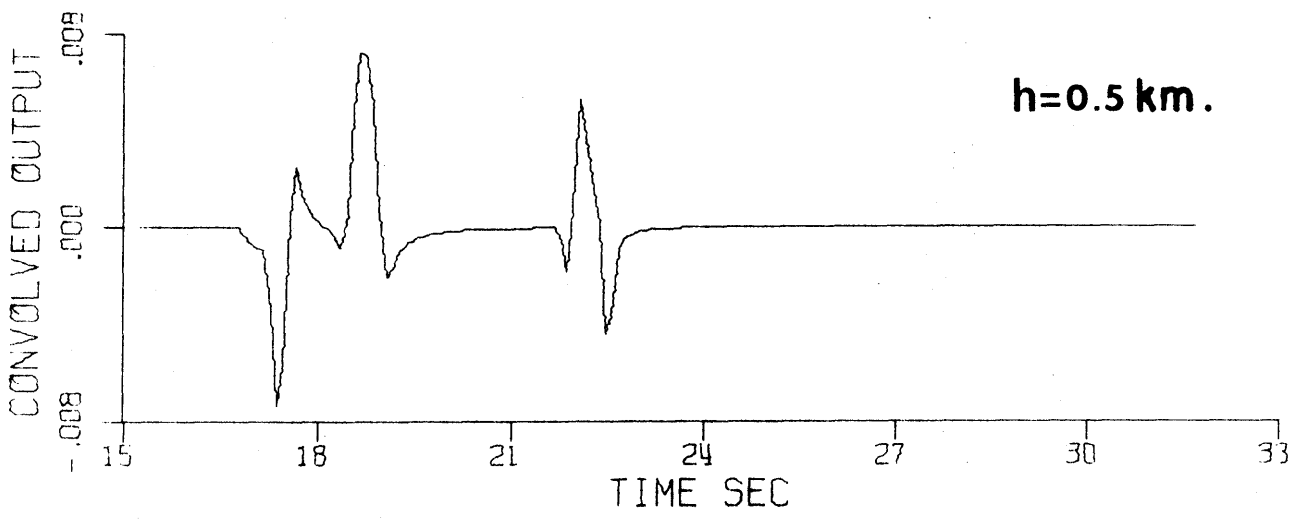


Fig. 14. SH, 1, 50

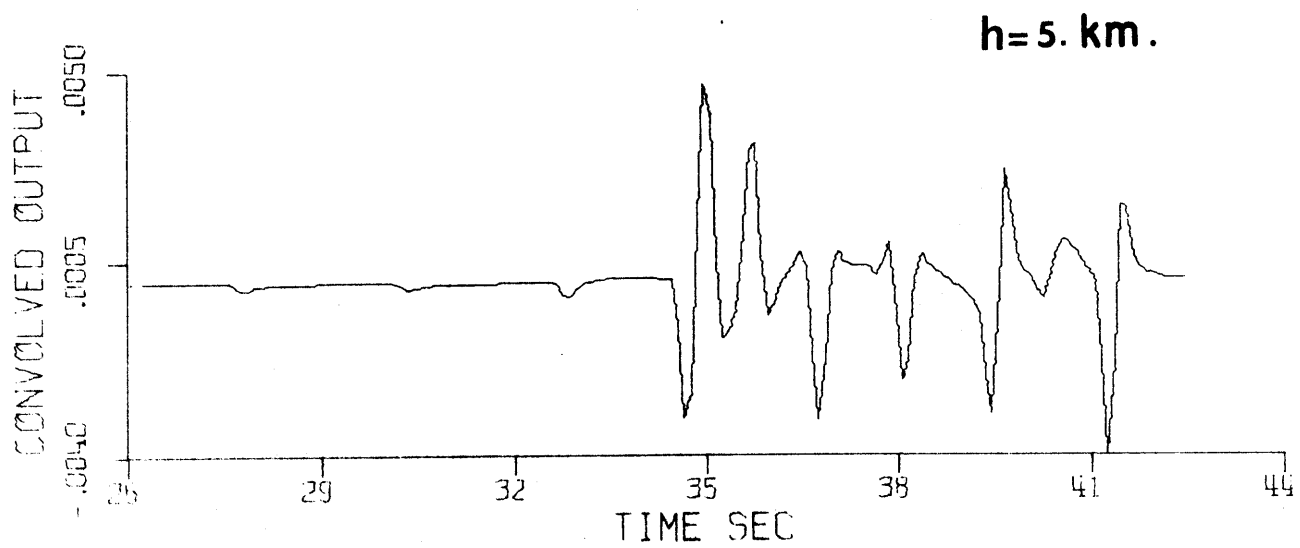
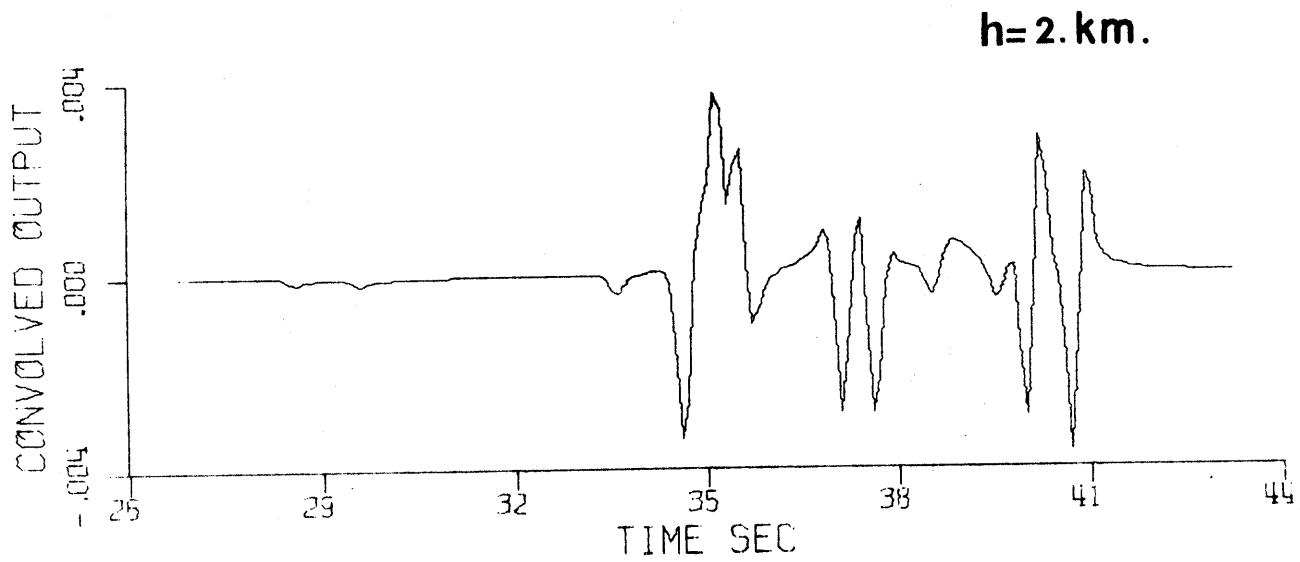
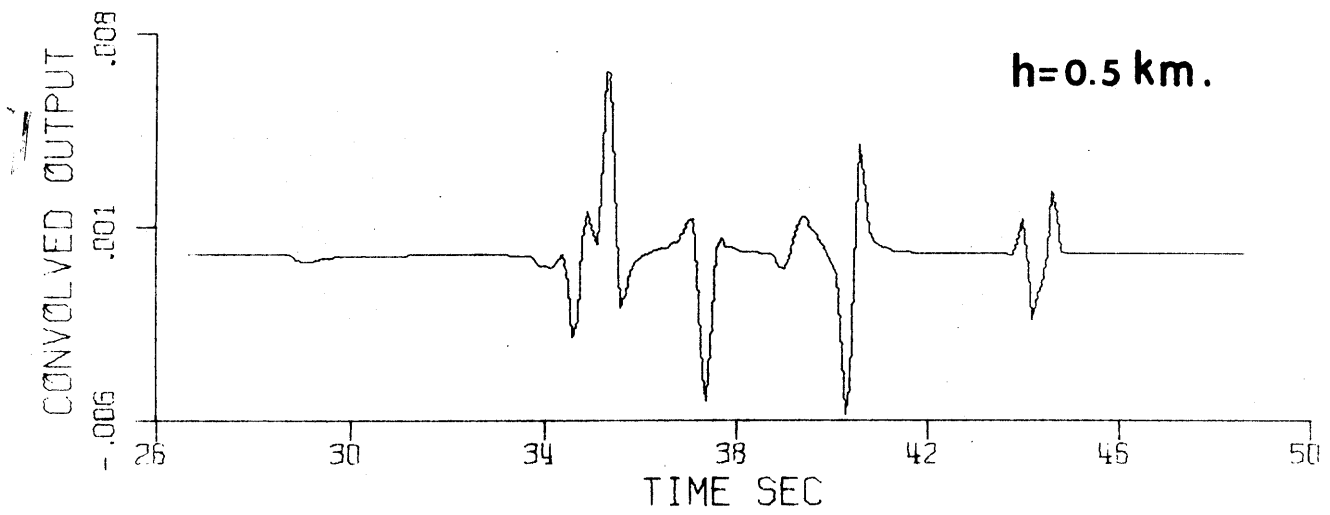


Fig. 15. SH, I, 100

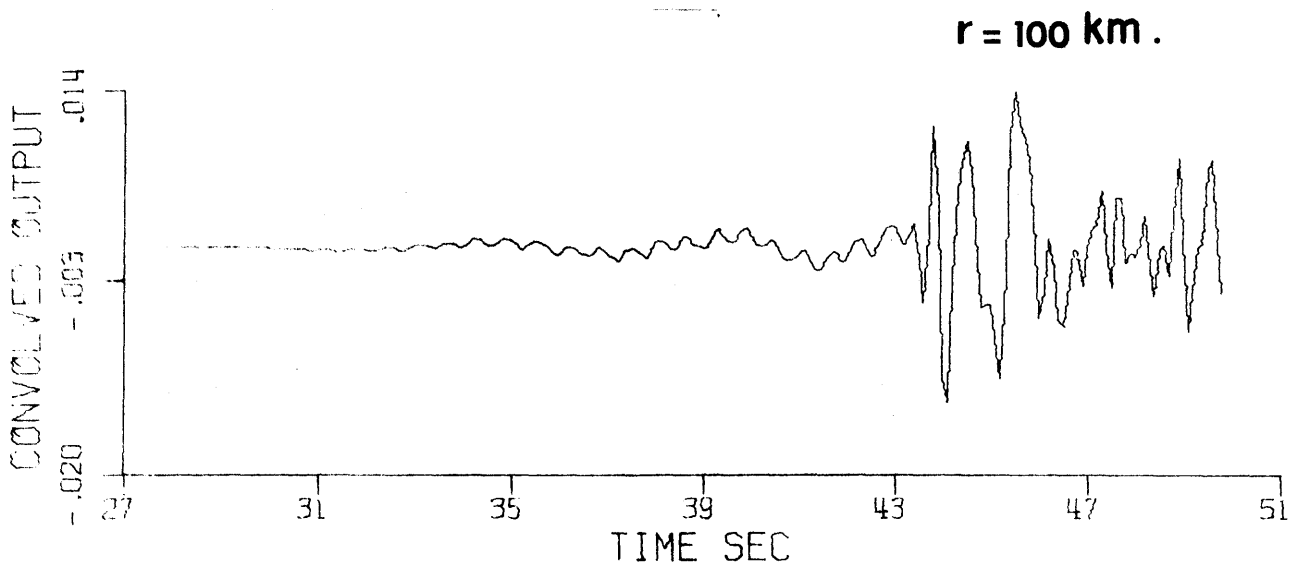
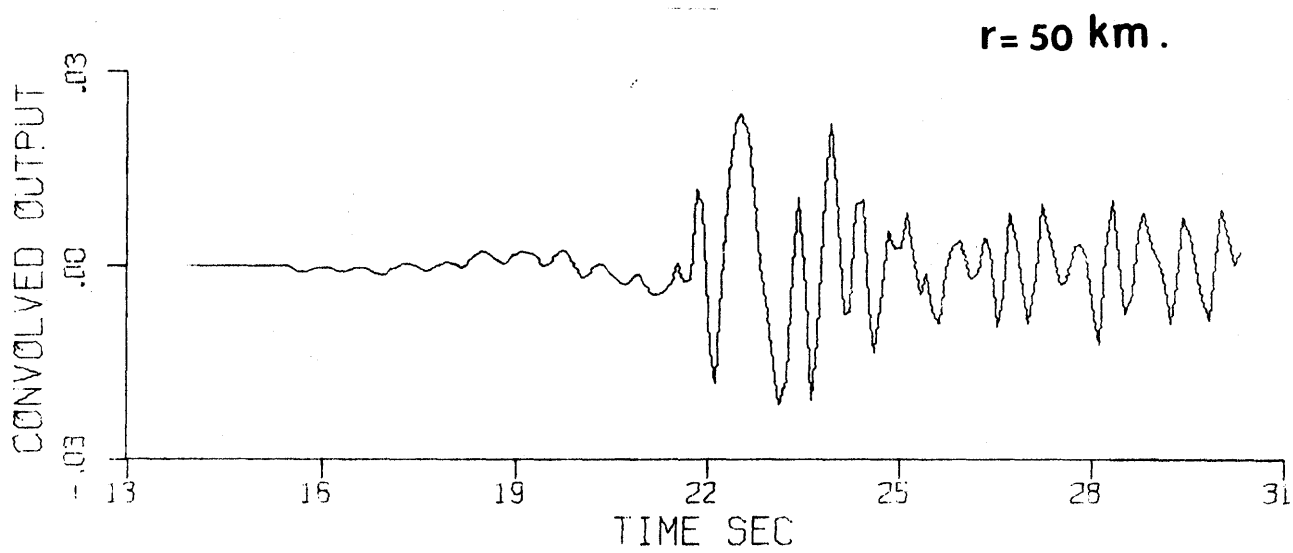
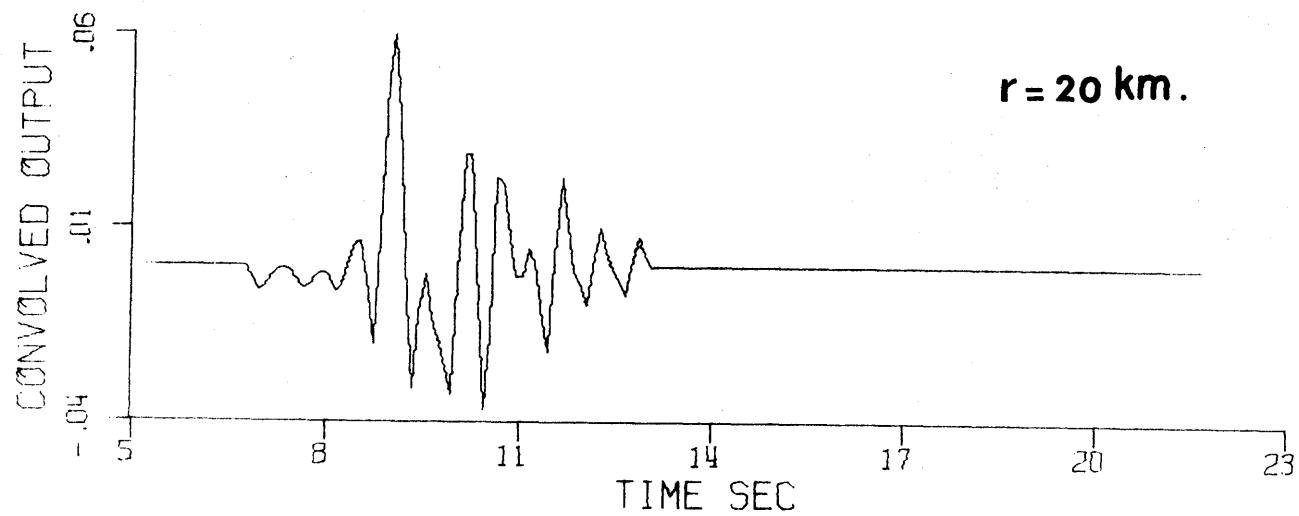


FIG. 16. SH, II, C

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## Appendix A

### SOLUTION OF THE INHOMOGENEOUS WAVE EQUATION

Here we would like to solve the inhomogeneous wave equation  
(1)

$$\mu \nabla^2 u_\theta(r, z, t) - \rho \frac{\partial^2}{\partial t^2} u_\theta(r, z, t) = \frac{-H(t) \delta(r) \delta(z-h)}{2\pi r} \quad (\text{A1})$$

The Laplace transform of (A1) in time domain is

$$\nabla^2 \bar{u}_\theta(r, z, s) - \frac{s^2}{\beta^2} \bar{u}_\theta(r, z, s) = \frac{-\delta(r) \delta(z-h)}{2\pi \mu r} \quad (\text{A2})$$

Note that

$$\nabla^2 \equiv \frac{1}{r} \frac{d}{dr} r \frac{d}{dr} + \frac{d^2}{dz^2} \equiv \nabla_r^2 + \frac{d^2}{dz^2}$$

And now let us define the bilateral Laplace transform as

$$\bar{u}_\theta(r, v, s) = \int_{-\infty}^{+\infty} \bar{u}_\theta(r, z, s) e^{vz} dz$$

When this is applied to (A2) we get as a consequence

$$\nabla_r^2 \bar{u}_\theta(r, v, s) - (K^2 - v^2) \bar{u}_\theta(r, v, s) = \frac{-\delta(r) e^{-vh}}{2\pi \mu r} \quad (\text{A3})$$

Define  $\zeta^2 = K^2 - v^2$ , where  $K^2 = s^2/\beta^2$ , radiation condition becomes  $\text{Re } \zeta \geq 0$  which has to be satisfied. Consider the equation

$$\nabla_r^2 V - \zeta^2 V = - \frac{\delta(r-r_0)}{r} \quad (\text{A4})$$

which has as its homogeneous solutions

$$V_1 = I_0(\zeta, r) \quad V_2 = K_0(\zeta, r)$$

which for large  $r$  behaves as

$$V_1 \approx \frac{e^{\zeta r}}{\sqrt{2\pi\zeta r}} \quad V_2 \approx \sqrt{\frac{\pi}{2\zeta r}} e^{-\zeta r}$$

$$V = c I_0(\zeta r_<) K_0(\zeta r_>) \quad (\text{A5})$$

where  $r_> \equiv \max(r, r_0)$ ,  $r_< \equiv \min(r, r_0)$  and  $c$ , a constant, to be determined from the continuity condition of  $V$  at  $r = r_0$ .

Multiplying (A4) by  $r$  and integrating from  $r_0 - \epsilon$  to  $r_0 + \epsilon$  we get

$$\lim_{\epsilon \rightarrow 0} \left[ r \frac{dV}{dr} \right]_{r_0 - \epsilon}^{r_0 + \epsilon} = -1 \quad (\text{A6})$$

Put (A5) into (A6) to get

$$c \zeta r_0 [I_0(\zeta r_0) K_0'(\zeta r_0) - I_0'(\zeta r_0) K_0(\zeta r_0)] = -1 \quad (\text{A7})$$

where the prime (') denotes differentiation with respect to  $r_0$ . The quantity in parenthesis in (A7) denotes the Wronskian of  $(I_0, K_0)$  and is found to be  $-1/\zeta r_0$ . Hence  $c = 1$ , giving the particular solution as

$$V = I_0(\zeta r_<) K_0(\zeta r_>) \quad (A8)$$

From (A3) we get  $r_0 = 0$  which gives us

$$u_\theta = K_0(\zeta r) \quad I_0(0) = 1$$

and therefore the particular solution of (A3) is

$$\bar{u}_\theta(r, v, s) = K_0(\zeta r) e^{-vh} / 2\pi\mu$$

The inversion from  $v$  to  $z$  gives us

$$\bar{u}_\theta(r, z, s) = \frac{1}{2\pi i} \frac{1}{2\pi\mu} \int_{-i\infty}^{+i\infty} K_0(\zeta r) e^{v(z-h)} dv \quad (A9)$$

Alternatively we can write (A9) as

$$\bar{u}_\theta(r, z, s) = \frac{1}{2\pi^2\mu} \operatorname{Im} \int_0^{i\infty} K_0(\zeta r) e^{v(z-h)} dv \quad (A10)$$

or

$$\bar{u}_\theta(r, z, s) = -\frac{1}{2\pi^2\mu} \operatorname{Im} \int_0^{i\infty} K_0(\zeta r) e^{v(z-h)} dv \quad (A11)$$

Keeping in mind the condition  $\operatorname{Re} \zeta \geq 0$  has to be satisfied, we cut the  $v$  plane as shown in Figure A1.

Shifting the path of integration in Equation A10 to the tip of the cut in the left half of the  $v$  plane for  $z > h$ , we get

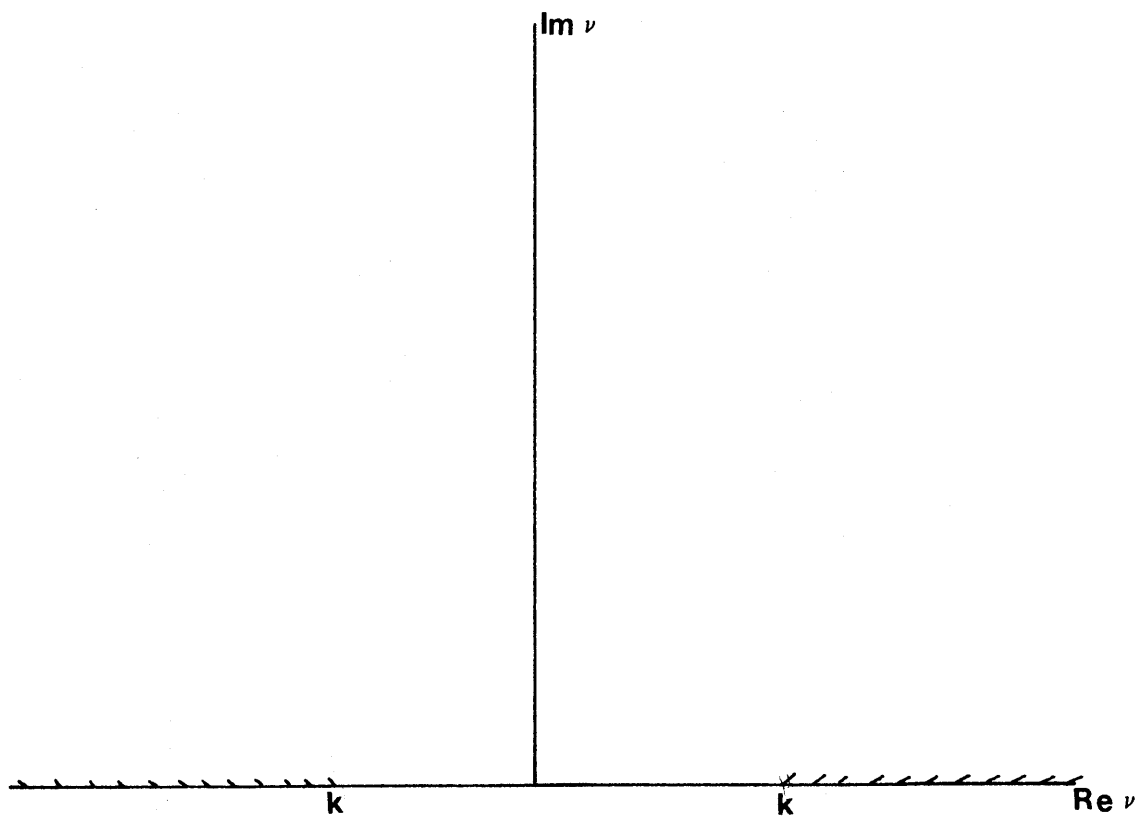


FIG. A1

$$\bar{u}_\theta(r, z, s) = \frac{1}{2\pi^2\mu} \operatorname{Im} \int_{-K}^{\infty} K_0(\zeta r) e^{\nu|z-h|} d\nu \quad (\text{A12})$$

or making a change in the variable of integration gives us

$$\bar{u}_\theta(r, z, s) = -\frac{1}{2\pi^2\mu} \operatorname{Im} \int_0^{i\infty} K_0(\zeta r) \frac{\zeta}{\nu} e^{+\nu|z-h|} d\zeta \quad (\text{A13})$$

for  $\operatorname{Re} \nu \leq 0$ .

If we put  $\nu = -\nu$  in (A12) we get

$$\bar{u}_\theta(r, z, s) = \frac{1}{2\pi^2\mu} \operatorname{Im} \int_0^{i\infty} K_0(\zeta r) \frac{\zeta}{\nu} e^{-\nu|z-h|} d\zeta \quad (\text{A14})$$

for  $\operatorname{Re} \nu \geq 0$ . If we again consider for  $z > h$  an appropriate equation corresponding to (A10), i.e. (A11), we would see that we get (A14). This shows that (A14) holds true for all  $z$ . Let  $\zeta = sp$ ,  $\nu = s\eta$  in (A14) to get

$$\bar{u}_\theta(r, z, s) = \frac{s}{2\pi^2\mu} \operatorname{Im} \int_0^{i\infty} \frac{p}{\eta} K_0(spr) e^{-s\eta|z-h|} dp \quad (\text{A15})$$

which is the solution for the homogeneous half-space. This formulation can easily be extended for layered media if we introduce a function  $F_n(p)$  in (A15) which takes into consideration the reflection coefficient at the interface, the receiver directivity function and the source radiation function to get

$$\bar{u}_{\theta,n}(r,0,s) = s \operatorname{Im} \int_0^{i\infty} p F_n(p) K_0(spr) e^{-sj_n(p)} dp \quad (\text{A16})$$

where  $j_n(p)$  describes the time taken by the  $n$ th generalized ray to traverse the layer. This is Equation 4 in the main text of this thesis. Proceeding in exactly the same way, we can obtain Equations 2 and 3 for P and/or SV sources.



## Appendix B

### CALCULATION OF REFLECTION COEFFICIENTS AND RECEIVER FUNCTIONS

P and SV Waves. The reflection function  $\zeta_n(p)$  is a measure of the attenuation of energy due to internal reflections and is given by

$$\zeta_n(p) = R_{DPP}^{1_{DPP}(n)} R_{DPS}^{1_{DPS}(n)} R_{DSP}^{1_{DSP}(n)} R_{DSS}^{1_{DSS}(n)} R_{UPP}^{1_{UPP}(n)} R_{UPS}^{1_{UPS}(n)} R_{USP}^{1_{USP}(n)} R_{USS}^{1_{USS}(n)}$$

where  $1_{DPP}^{(n)}$  denotes the number of P to P reflections off the lower boundary and similarly,  $1_{UPP}^{(n)}$  is the number of P to P reflections off the free surface. The functions  $R_{DPP}$ ,  $R_{DPS}$ , etc. denote the reflection coefficients and are given by [See for details Helmberger (1967), Barker (1970)]

$$R_{DPP} = (-[1] + [2] + [3] - [4] - [5] + [6])/D_1$$

$$R_{DPS} = 2p\eta_1 [(K_2 - p^2)(K_3 - p^2) - \eta_2\eta_2'(K_1 - p^2)]/D_1$$

$$R_{DSP} = 2p\eta_1' [(K_2 - p^2)(K_3 - p^2) - \eta_2\eta_2'(K_1 - p^2)]/D_1$$

$$R_{DSS} = (-[1] + [2] + [3] - [4] + [5] - [6])/D_1$$

where

$$D_1 = [1] + [2] + [3] + [4] - [5] - [6]$$

$$[1] = p^2(K_3 - p^2)^2$$

$$[2] = \eta_1\eta_2\eta_1'\eta_2'p^2$$

$$[3] = \eta_1 \eta_1' (K_3 - p^2)^2$$

$$[4] = \eta_2 \eta_2' (K_1 - p^2)^2$$

$$[5] = \eta_1 \eta_2' K_1 K_2$$

$$[6] = \eta_2 \eta_1' K_1 K_2$$

and

$$K_1 = -\frac{1}{2} \left( \frac{\rho_1}{\mu_2 - \mu_1} \right)$$

$$K_2 = \frac{1}{2} \left( \frac{\rho_2}{\mu_2 - \mu_1} \right)$$

$$K_3 = K_1 + K_2$$

Also

$$R_{UPP} = R_{USS} = [4\beta_1^4 p^2 \eta_1 \eta_1' - (1 - 2\beta_1^2 p^2)^2] / D_2$$

$$R_{UPS} = 4p\eta_1 (1 - 2\beta_1^2 p^2) / D_2$$

$$R_{USP} = -4p\eta_1' (1 - 2\beta_1^2 p^2) / D_2$$

$$D_2 = 4\beta_1^4 p^2 \eta_1 \eta_1' + (1 - 2\beta_1^2 p^2)^2$$

where

$$\eta_1 = \sqrt{\frac{1}{\alpha_1^2} - p^2}$$

$$\eta_1' = \sqrt{\frac{1}{\beta_1^2} - p^2}$$

$$\eta_2 = \sqrt{\frac{1}{\alpha_2^2} - p^2}$$

$$\eta_2' = \sqrt{\frac{1}{\beta_2^2} - p^2}$$

where  $\alpha_1$  and  $\beta_1$  are velocities of compressional and shear waves in the layer, and  $\alpha_2$  and  $\beta_2$  that in the half-space.  $\rho$  and  $\mu$  denote density and rigidity respectively and  $p$  is complex integration variable which has dimensions of sec/km.

For SH Waves. Taking Figure 1 of the main text into consideration, we have the following wave equations

$$\nabla^2 \chi_1(x, z, t) - \frac{1}{\beta_1^2} \frac{\partial^2 \chi_1}{\partial t^2} = -\delta(t) \delta(x) \delta(z-h) \quad (\text{B1})$$

and

$$\nabla^2 \chi_2(x, z, t) - \frac{1}{\beta_2^2} \frac{\partial^2 \chi_2}{\partial t^2} = 0 \quad (\text{B2})$$

where  $\chi_1$  and  $\chi_2$  are SH-potentials in the layer and half-space respectively.

We define unilateral and bilateral Laplace Transforms with respect to  $t$  for the function  $g(t)$  and similarly with respect to  $x$  for  $g(x)$  as follows

$$\bar{g}(s) = \int_0^{\infty} g(t) e^{st} dt \quad \text{where } s \text{ is positive real} \quad (\text{B3})$$

and

$$\hat{g}(\zeta) = \int_{-\infty}^{+\infty} g(x) e^{-\zeta x} dx \quad \text{where } \zeta \text{ is complex} \quad (\text{B4})$$

After transforming (B1) and (B2) with respect to  $s$  and  $\zeta$ , the solutions for SH wave displacements after Gilbert and Knopoff (1961) in the layer and the half-space respectively are given

by

$$\chi_1 = \frac{1}{2v_1} \left[ e^{-v_1 |z-h|} + A e^{-v_1 z} \right] \quad (\text{B5})$$

$$\chi_2 = \frac{B}{2v_1} e^{v_2 z} \quad (\text{B6})$$

where

$$v_1 = \sqrt{\frac{1}{\beta_1^2} - p^2} \quad v_2 = \sqrt{\frac{1}{\beta_2^2} - p^2}$$

Boundary conditions at the interface require continuity of displacement and stress, viz.

$$\chi_2 = \chi_2 \quad (B7)$$

$$p_{zy}|_1 = \mu_1 \frac{\partial \chi_1}{\partial z}|_2 = p_{zy}|_2 = \mu_2 \frac{\partial \chi_2}{\partial z}|_2 \quad (B8)$$

in order to determine A and B in (B5) and (B6). If we change the origin of the coordinate system to the top of the interface we get

$$e^{-v_1 h} + A = B$$

$$v_1 \mu_1 e^{-v_1 h} - \mu_1 v_1 A = \mu_2 v_2 B \quad (B9)$$

$$A = R_{DSH} = \frac{\mu_1 v_1 - \mu_2 v_2}{\mu_1 v_1 + \mu_2 v_2} e^{-v_1 h}$$

If we put  $v_1 = s\eta_1$   $v_2 = s\eta_2$

$$A = \frac{b\eta_1 - \eta_2}{b\eta_1 + \eta_2} e^{-s\eta_1 h} \quad \text{where } b = \frac{\mu_1}{\mu_2} \quad (B10)$$

and

$$B = \frac{2v_1 \mu_1}{\mu_1 v_1 + \mu_2 v_2} e^{-v_1 h} = \frac{2v_1 \mu_1}{\mu_1 \eta_1 + \mu_2 \eta} e^{-s\eta_1 h} \quad (B11)$$

The reflection coefficient given by (B10) turns out to be of the same form as given by Pekeris et.al. (1963) and Mitra (1963). Similarly, we can find out the reflection coefficient (c) for the free surface by requiring stress  $\bar{p}_{z\theta}$  to vanish at that surface.

$$C = R_{\text{USH}} = 1 \quad (\text{B12})$$

The reflection function  $\zeta_n(p)$  is, therefore given by

$$\zeta_n'(p) = R_{\text{USH}}^{l_{\text{USH}}^{(n)}} R_{\text{DSH}}^{l_{\text{DSH}}^{(n)}} \quad (\text{B13})$$

where  $R_{\text{USH}}$  and  $R_{\text{DSH}}$  are given by (B12) and (B10) respectively.  $l_{\text{USH}}^{(n)}$  is the number of SH to SH reflections off the free surface and similarly  $l_{\text{DSH}}^{(n)}$  is the number of SH to SH reflections off the lower boundary.

The receiver function is calculated from stress-free boundary condition at the free surface (Phinney, 1967). The once transformed in time displacement due to an upgoing SH wave is

$$\bar{u}_{\theta,n}(r, \omega, s) = \frac{1}{2\pi^2\mu} \text{Im} \int_0^{i\infty} \frac{sp}{\eta_1} K_0(sp) \{1 + R_{\text{USH}}\} e^{-\eta_1 h} dp \quad (\text{B14})$$

The function in braces is our receiver function  $R$  which can be easily seen to be identical to

$$R = 2 \quad (\text{B15})$$

## Appendix C

### COMPUTER PROGRAM

Here we give a printout of the program that we have used in evaluating Equations 5, 6 and 7. We have incorporated into this listing a detailed explanation of various features of the program. It was originally written by Don Helmberger. Barker (1970) extended it for the P-SV problem valid for both high and low frequency ranges. We included the SH wave option in it. The main program produces the impulse response. A secondary program then convolves this with a suitable source-function to give the final results.

```

C          MAIN
C      IMPLICIT REAL*8 (A-H,C-Z)
C *****INTRODUCTION*****
C      BRUCE GORDON AND CHANDRA M. NAUTIYAL ,54-524, M. I. T.
C      MAY 12, 1972
C      THIS PROGRAM FOR DETERMINING THE THEORETICAL RESPONSE TO A POINT
C      SOURCE OF AN ELASTIC LAYER OVER AN ELASTIC HALF SPACE IS UNDER
C      REVISION TO EXTEND THE ORIGINAL MODEL OF TERRY BARKER TO INCLUDE
C      AN SH SOURCE.
C      THIS PROGRAM IS IN A FORM SUITED TO AN N-LAYER MODEL. THERE IS ALSO
C      PROVISION FOR MODELING A HALF-SPACE ALONE(THE KPEK OPTION) WHICH I
C      HAVE REMOVED FROM THIS PROGRAM FOR SIMPLICITY). SOME OF THESE
C      UNNECESSARY FEATURES HAVE BEEN REMOVED, BUT FURTHER CLEANING UP IS
C      REQUIRED TO OBTAIN A GOOD WORKING PROGRAM. WHERE POSSIBLE I HAVE
C      NOTED THE NECESSARY CHANGES.
C      AT PRESENT ALL COMMON STATEMENTS ARE NOT OF THE SAME LENGTH IN EACH
C      SUBPROGRAM NOR THE VARIABLES INTERFACED PROPERLY(I.E. IN ORDER OF
C      DECREASING LENGTH).CLEANING UP THE COMMON STATEMENTS WILL IMPROVE
C      THE EFFICIENCY OF THE PROGRAM.
C      ALL CALCULATIONS ARE DOUBLE PRECISION UNLESS OTHERWISE NOTED
C *****SUBPROGRAMS*****
C      THE PROGRAM IS DIVIDED INTO MAIN AND THE FOLLOWING SUBPROGRAMS IN
C      ALPHABETICAL ORDER:      ADJUST,CONTOR,CR,CURAY,DELPS,FA,FIND2,
C      HELP,HIGH,INTERP,PLN1,PLN2,PSICO,PTIM,RAYDEF,RECVR,REFFT,SETUP,SF2,
C      TIME2,TS
C      THE FUNCTIION OF EACH SUBPROGRAM WILL BE MADE CLEAR IN THE BODY OF THE
C      PROGRAM AND IN THE COMMENTS INCLUDED IN EACH.

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00000000 MAIN0001
00000010 MAIN0002
00000020 MAIN0003
00000030 MAIN0004
00000040 MAIN0005
00000050 MAIN0006
00000060 MAIN0007
00000070 MAIN0008
00000080 MAIN0009
00000090 MAIN0010
00000100 MAIN0011
00000110 MAIN0012
00000120 MAIN0013
00000130 MAIN0014
00000140 MAIN0015
00000150 MAIN0016
00000160 MAIN0017
00000170 MAIN0018
00000180 MAIN0019
00000190 MAIN0020
00000200 MAIN0021
00000210 MAIN0022
00000220 MAIN0023
00000230 MAIN0024
00000240 MAIN0025
00000250 MAIN0026
00000260 MAIN0027
00000270 MAIN0028
00000280 MAIN0029
00000290 MAIN0030
00000300 MAIN0031
00000310 MAIN0032
00000320 MAIN0033
00000330 MAIN0034
00000340 MAIN0035
00000350 MAIN0036

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C THE SUBPROGRAMS SETUP,CONTOR,TIME2,PSICD,REFFT, AND RECVR HAVE BEEN 00000360 MAIN0037
C REVISED SINCE THE LIBRARY WAS CREATED AND ARE NOW RUN AS SOURCE DECKS.00000370 MAIN0038
C 00000380 MAIN0039
C *****ADDITIONAL PROGRAMS*****00000390 MAIN0040
C 00000400 MAIN0041
C CONVOLUTION WITH A SPECIFIED SOURCE FUNCTION AND PLOTTING ON CALCOMP 00000410 MAIN0042
C ARE PERFORMED IN ANOTHER PROGRAM. 00000420 MAIN0043
C 00000430 MAIN0044
C *****INPUT*****00000440 MAIN0045
C 00000450 MAIN0046
C THE INPUTS TO THIS PROGRAM ARE AS FOLLOWS: THE NUMBER OF LAYERS,NMOD, 00000460 MAIN0047
C IN FORMAT (I10) ON THE FIRST CARD. IN THIS CASE NMOD IS ALWAYS 3, 00000470 MAIN0048
C INCLUDING THE HALF SPACE ABOVE THE LAYER,WHICH IS A VACUUM. 00000480 MAIN0049
C THE NEXT CARDS CONTAIN IN SUCCESSION: THE COMPRESSIONAL AND SHEAR 00000490 MAIN0050
C VELOCITIES IN EACH LAYER (KM/SEC), THE DENSITY (GM/CC),AND THE 00000500 MAIN0051
C THICKNESS (KM). THE UPPER HALF SPACE PARAMETERS AND THE THICKNESS 00000510 MAIN0052
C OF THE SOLID HALF SPACE MAY BE ASSIGNED ANY VALUES.EACH CARD CONTAINS 00000520 MAIN0053
C THE VALUES FOR ONE LAYER IN FORMAT (4F10.0) . 00000530 MAIN0054
C THE NEXT CARD CONTAINS THE RANGE IN FORMAT(F10.0) . 00000540 MAIN0055
C THE NEXT CARD CONTAINS THE DESIRED INTERVAL BETWEEN RECORD POINTS(DP) 00000550 MAIN0056
C IN SEC,THE LENGTH OF RECORD CALCULATED FOR EACH RAY(TMX, IN SEC), AND 00000560 MAIN0057
C THE NUMBER OF RECORD POINTS(NN) IN THE FINAL OUTPUT IN FORMAT(2F10.0, 00000570 MAIN0058
C I10). THIS COMPLETES THE DATA READ-IN IN THE MAIN PROGRAM. 00000580 MAIN0059
C 00000590 MAIN0060
C IN THE SUBROUTINE RAYDEF,THE PARAMETERS DESCRIBING THE PARTICULAR 00000600 MAIN0061
C MODEL ENTER THE PROGRAM.ON THE FIRST CARD THE LAYER THICKNESS IN 00000610 MAIN0062
C METERS,THE SOURCE DEPTH IN METERS,AND THE KIND OF SOURCE(KSSP=0 DESIGNN00000620 MAIN0063
C -ATES SHEAR SOURCE, AND KSSP=1 DESIGNATES COMPRESSIONAL SOURCE) ALL IN00000630 MAIN0064
C FORMAT(2F10.0,I10). NOTE THAT IN PUTTING THE PROGRAM IN FINAL FORM A 00000640 MAIN0065
C SEPERATE DESIGNATION FOR SH SOURCE MIGHT BE CONVENIENT. 00000650 MAIN0066
C THE NEXT CARDS CONTAIN THE RAY PARAMETERS FOR (19,LAST RAY USED), THE 00000660 MAIN0067
C FIRST EIGHTEEN RAYS ARE CURRENTLY DEFINED IN RAYDEF. AS THE SUBROUTINE00000670 MAIN0068
C RAYDEF HAS NO OTHER FUNCTION,IT WOULD BE CONVENIENT TO READ IN ALL THE00000680 MAIN0069
C RAY PARAMETERS AND ELIMINATE THIS SUBROUTINE. THE FIRST SET OF 00000690 MAIN0070
C PARAMETER CARDS CONTAIN THE FOLLOWING IN FORMAT(4I1): KUD(J) (X FOR 00000700 MAIN0071
C UPGOING RAY,X FOR DOWNGOING); LTS(J),THE NUMBER OF S-S REFLECTIONS; 00000710 MAIN0072

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REVERSE

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C LTP(J), THE NUMBER OF P-P REFLECTIONS, KRSP(J), THE MODE OF THE RECEIVER(=0 FOR S AND 1 FOR P)
C THE NEXT SET OF CARDS CONTAIN THE VALUES OF THE TWO DIMENSIONAL ARRAY LREF(I, J) WHICH DEFINE THE NATURE OF THE REFLECTIONS AT THE TOP AND THE BOTTOM OF THE LAYER, EIGHT VALUES FOR EACH RAY DEFINING GIVING FIRST THE NUMBER OF P TO P, S TO P, P TO S, AND S TO S INTERACTIONS AT THE BOTTOM INTERFACE, NEXT THE SAME VALUES FOR THE FREE SURFACE.
C THE SH PROGRAM SETS LTP AND KRSP ALWAYS EQUAL ZERO AND HAS NO PP, PS, OR SP INTERACTIONS
C *****OUTPUT*****
C THIS PROGRAM GENERATES PUNCHED OUTPUT FOR THE THEORETICAL RESPONSE UNCONVOLVED WITH ANY SOURCE FUNCTION, PRINTING FIRST THE STARTING TIME FOR THE RECORD IN SECONDS, TT(1), THE TIME INTERVAL BETWEEN DATA POINTS IN SECONDS, DP, AND THE NUMBER OF DATA POINTS IN THE RECORD, NN IN THE FORMAT(2E15.6, I10). THIS HEADING CARD IS FOLLOWED BY THE SURFACE RESPONSE IN FORMAT(5E15.6).
C THERE IS ALSO PRINTED OUTPUT, SOME OPTIONAL SOME NOT: FIRST A LISTING OF MODEL PARAMETERS; THEN FOR EACH RAY, THE VALUES OF P AT THE POINT OF REFLECTION (AN INTEGRATION PARAMETER) AND DP/DT AS COMPLEX NUMBERS; THEN THE TIME (IN SEC) OF THE REFLECTION ARRIVAL OF THE SURFACE RESPONSE -S, FOLLOWED BY THE SURFACE RESPONSE AT EVERY FIFTH CALCULATED VALUE. NOTE THE DESIRED RESPONSE IS HERE GIVEN BY PHIZ, THE VERTICAL COMPONENT -T, AS THAT COMPONENT INVOLVES THE K0 BESSEL FUNCTION REQUIRED FOR AN SH SOURCE. THE PHIR (RADIAL) COMPONENT USES THE K1 BESSEL FUNCTION. IN THIS APPROXIMATION ONLY THE FIRST TWO TERMS IN THE EXPANSION OF THESE FUNCTIONS ARE RETAINED. THEREFORE THE TWO ITEMS DIFFER ONLY IN THE SECOND TERM, AND IN THE FIRST-ORDER NOT AT ALL.
C THE RAY OUTPUT IS FOLLOWED BY A LISTING OF THE TIME SERIES OF THE OUTPUT SURFACE RESPONSE. NOTE THAT THIS PRINTED RECORD IS PADDED WITH ZEROS AT THE BEGINNING TO 10% OF ITS LENGTH
C *****THE ORDER OF EXECUTION*****

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00000720 MAIN0073
00000730 MAIN0074
00000740 MAIN0075
00000750 MAIN0076
00000760 MAIN0077
00000770 MAIN0078
00000780 MAIN0079
00000790 MAIN0080
00000800 MAIN0081
00000810 MAIN0082
00000820 MAIN0083
00000830 MAIN0084
00000840 MAIN0085
00000850 MAIN0086
00000860 MAIN0087
00000870 MAIN0088
00000880 MAIN0089
00000890 MAIN0090
00000900 MAIN0091
00000910 MAIN0092
00000920 MAIN0093
00000930 MAIN0094
00000940 MAIN0095
00000950 MAIN0096
00000960 MAIN0097
00000970 MAIN0098
00000980 MAIN0099
00000990 MAIN0100
00001000 MAIN0101
00001010 MAIN0102
00001020 MAIN0103
00001030 MAIN0104
00001040 MAIN0105
00001050 MAIN0106
00001060 MAIN0107
00001070 MAIN0108

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C THE PROGRAM IS EXECUTED APPROXIMATELY AS FOLLOWS: 00001080 MAIN0109
C MODEL PARAMETERS ARE READ IN OR OTHERWISE SPECIFIED IN MAIN. CONTROL 00001090 MAIN0110
C IS THEN PASSED TO SUBROUTINE SETUP. 00001100 MAIN0111
C IF THIS CALL IS FIRST TO SETUP,THE SUBROUTINE RAYDEF IS CALLED TO READ00001110 MAIN0112
C IN OR OTHERWISE ESTABLISH THE RAY PARAMETERS, THE ARRAYS WHICH CONTAIN00001120 MAIN0113
C THE OUTPUT ARE INITIALIZED, AND THE FUNCTION TS IS USED TO DETERMINE 00001130 MAIN0114
C THE TIME OF FIRSTARRIVAL,THE BEGINNING OF THE RECORD. THE PROGRAM THEN00001140 MAIN0115
C ITERATES OVER EACH RAY .FOR EACH RAY THE FIRST SUBROUTINE CALLED IS 00001150 MAIN0116
C HIGH. IN HIGH WE EMPLOY THE SUBROUTINE FIND2 TO DETERMINE THE VALUES 00001160 MAIN0117
C OF PC AND TD,THAT IS THE VALUE OF THE INTEGRATION PARAMETER P AND THE 00001170 MAIN0118
C TIME T AT THE REFLECTION ARRIVAL FOR THIS RAY.IN GENERAL EACH RAY 00001180 MAIN0119
C RESPONSE IS DIVIDED INTO TWO PARTS, AN INTEGRATION ALONG THE REAL 00001190 MAIN0120
C AXIS FOR THE REFRACTED RESPONSE, AND AN INTEGRATION ALONG THE COMPLEX 00001200 MAIN0121
C CONTOUR FOR THE RESPONSE AFTER REFLECTION. FOR A DISCUSSION OF THE 00001210 MAIN0122
C METHOD SEE THE REFERENCES. THE POINT OF REFLECTION IS FOUND WHERE THE 00001220 MAIN0123
C CONTOUR LEAVES THE REAL AXIS AND DP/DT HAS A POLE. 00001230 MAIN0124
C BEFORE THE REFRACTION ARRIVAL,THAT IS BEFORE THE FIRST BRANCH POINT 00001240 MAIN0125
C AS GIVENBY  $P=1/V$  (LARGEST VELOCITY OF PROPAGATION IN THE HALF SPACE), 00001250 MAIN0126
C THE INTEGRAL IS ZERO. THE FIRST BRANCH CUT MAY NOT OCCUR UNTIL AFTER 00001260 MAIN0127
C THE REFLECTION ARRIVAL .IF THIS IS SO THERE IS NO REFRACTED SIGNAL 00001270 MAIN0128
C THE SUBROUTINE HELP IS NOW CALLED TO FIND THE TIME OF ARRIVAL OF THE 00001280 MAIN0129
C REFRACTED SIGNAL AND THE VALUE OF DP/DT THERE. WE NOW COMPARE THIS 00001290 MAIN0130
C REFRACTED ARRIVAL TIME WITH THE REFLECTED ARRIVAL TIME AND CALCULATE 00001300 MAIN0131
C THE INTEGRATION INTERVAL DELP FOR THE REFRACTED RECORD,THAT IS UP TO 00001310 MAIN0132
C BUT NOT INCLUDING THE POINT OF REFLECTION. DEPENDING ON THE SEPERATION00001320 MAIN0133
C BETWEEN THE BRANCH CUT (REFRACTION ARRIVALS) AND THE POLE (REFLECTION 00001330 MAIN0134
C ARRIVAL) THE INTERVAL SIZE MAY BE CONSTANT OR CALCULATED IN SUBROUTINE00001340 MAIN0135
C DELPS USING A SINE RELATIONSHIP. IF THERE IS A REFRACTED ARRIVAL 00001350 MAIN0136
C CONTROL IS TRANSFERRED TO SUBROUTINE PLN1 TO PERFORM THIS PART OF THE 00001360 MAIN0137
C INTEGRATION.NOTE THAT IF THERE IS A REFRACTED ARRIVAL THE FIRST VALUE 00001370 MAIN0138
C OF THE TIME SERIES OF SURFACE RESPONSE IS ALWAYS SET TO ZERO. IN PLN1 00001380 MAIN0139
C WE USE THE ALREADY CALCULATED INTERVALS DELP AND THE SUBROUTINE HELP 00001390 MAIN0140
C TO CALCULATE THE TIME AND DP/DT FOR EACH VALUE OF THE INTEGRATION 00001400 MAIN0141
C PARAMETER P.FOR EACH P WE THEN CALL THE SUBROUTINE PSICO.IN PSICO 00001410 MAIN0142
C WE PERFORM THE INTEGRATION,CALCULATING THE TWO COMPLEX TERMS IN THE 00001420 MAIN0143
C EXPANSION USED BY TERRY BARKER TO APPROXIMATE THE INTEGRAL.FIRST WE 00001430 MAIN0144

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C CALL THE SUBROUTINE REFFT TO DETERMINE THE VALUE OF THE REFLECTION      00001440 MAIN0145
C FUNCTION, THEN THE SUBROUTINE RECVR TO DETERMINE THE RECEIVER FUNCTION00001450 MAIN0146
C WE THEN MULTIPLY THE REFLECTION FUNCTIYN BY ITSELF ACCORDING TO THE     00001460 MAIN0147
C NUMBER OF REFLECTIONS SPECIFIED IN ARRAY LREF.THE TWO COMPLEX TERMS    00001470 MAIN0148
C IN THE EXPANSION FOR THE RADIAL AND THE VERTICAL SURFACE RESPJNSE ARE  00001480 MAIN0149
C THEN CALCLATED CONTROL RETURNS TO PLN1. WE THEN COMPLETE SIMILAR      00001490 MAIN0150
C CALCULATIONS FOR GRADUALLY DECREASING INTERVALS APPROACHING BUT NOT    00001500 MAIN0151
C INCLUDING THE POINT OF REFLECTION.CONTROL IS RETURNED TO HIGH.THE      00001510 MAIN0152
C SUBROUTINE CONTOR IS NOW CALLED TO DEFINE THE COMPLEX CONTOR OF INTE    00001520 MAIN0153
C -GRATION FOR THE SIGNAL AFTER THE REFLECTION ARRIVAL.FIRST A SERIES    00001530 MAIN0154
C OF DECREASING INTERVALS IS CALCLATED ABOUT THE POINT OF REFLECTION.    00001540 MAIN0155
C THE INTEGRATION PARAMETER P IS NOW COMPLEX AND THIS COMPLEX CONTOUR   00001550 MAIN0156
C IS DEFINED BY REQUIRING THAT ANOTHER PARAMETER,THE TIME,BE REAL.      00001560 MAIN0157
C THEREFORE T THE CONTOUR IS DEFINED BY MINIMIZING THE IMAGINARY PART OF00001570 MAIN0158
C THE TIME PARAMETER IN SUBROUTINE TIME2. THE INTEGRATION INTERVALS      00001580 MAIN0159
C ABOUT THE SEVERAL BRANCH PJINTS ARE DEFINED USING THE SUBROUTINE DELPS00001590 MAIN0160
C FOR A VARYING INTERVAL SIZE.AFTER THE LAST BRANCH POINT THE INTERVALS  00001600 MAIN0161
C INCREASE IN SIZE UNTIL THE END OF THE RECORD.CONTROL IS RETURNED TO    00001610 MAIN0162
C HIGH.                                                                    00001620 MAIN0163
C THE SUBROUTINE PLN2 IS THEN CALLED TO COMPLETE THE INTEGRATION FOR      00001630 MAIN0164
C THE REST OF THE CONTOUR.PLN2 USES PSICO TO CALCULATE THE TWO COMPLEX   00001640 MAIN0165
C TERMS FOR THE RADIAL AND THE VERTICAL SURFACE RESPONSE FOR THE VALUES00001650 MAIN0166
C OF P DETERMINED IN CONTOUR. THIS NOW COMPLETE SET OF VALUES IS       00001660 MAIN0167
C CONVOLVED WITH THE APPROPRIATE TIME FUNCTIONS FOR THE ENTIRE CONTOUR.  00001670 MAIN0168
C NOTE THAT THE POINT OF REFLECTION IS SPECIALLY TREATED,USING THE      00001680 MAIN0169
C SUBROUTINE INTERP FOR INTERPOLATION AS NEEDED.CONTROL IS RETURNED TO   00001690 MAIN0170
C HIGH. THE OUTPUT IS PRINTED FOR EVERY FIFTH VALUE OF THE TIME SERIES  00001700 MAIN0171
C AND THE CONTROL IS RETURNED TO SETUP.WE NOW CALL USE THE SUBROUTINE    00001710 MAIN0172
C ADJUST.ORIGINALLY WE SPECIFIED A DESIRED OUTPUT,DESIGNATING LENGTH OF  00001720 MAIN0173
C RECORD FOR EACH RAY,TMX,THE TIME INTERVAL,DP,AND THE NUMBER OF POINTS00001730 MAIN0174
C IN THE SERIES,NN.WE NOW ADJUST THIS DESIRED SERIES SO THAT ONE PCINT   00001740 MAIN0175
C CF IT COINCIDES WITH THE REFLECTION ARRIVAL AT TO. WE NOW USE THE     00001750 MAIN0176
C SUBROUTINE INTERP TO INTERPOLATE THE OUTPUT TO THE DESIRED TIME SERIES00001760 MAIN0177
C THE SUBROUTINE DDGT3 IS THEN USED TO TAKE THE TIME DERIVETIVE ,AND    00001770 MAIN0178
C THE OUTPUT IS PRINTED AND PUNCHED ON CARDS.CONTROL RETURNS TO MAIN    00001780 MAIN0179
C AND PROGRAM ENDS.                                                       00001790 MAIN0180

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C 00001800 MAIN0181
C *** ***** 00001810 MAIN0182
C THE MAIN PROGRAM 00001820 MAIN0183
C 00001830 MAIN0184
C THE MAIN PROGRAM SERVES THREE FUNCTIONS, READ-IN OF PARAMETERS DESCRIBING THE MODEL, SETTING THE VALUES OF CONSTANTS, AND CALLING ONCE THE SUBROUTINE SETUP WHICH CONTROLS ALL ACTUAL CALCULATIONS. IT IS SUGGESTED THAT ALL THE PARAMETER READ-INS BE INCLUDED IN MAIN ELIMINATING, THE SUBROUTINE RAYDEF, WHICH DEFINES RAY PARAMETERS, AND THAT THE CONSTANTS MIGHT BE SET IN A BLOCK DATA SUBPROGRAM FOR CONVENIENCE, SO THAT THE MAIN SIMPLY READS IN PARAMETERS AND CALLS SETUP. THUS ALL THE SUBROUTINES MAY BE PLACED IN A DISC LIBRARY AND THE LENGTH OF THE MAIN PROGRAM MINIMIZED.
C 00001840 MAIN0185
C 00001850 MAIN0186
C 00001860 MAIN0187
C 00001870 MAIN0188
C 00001880 MAIN0189
C 00001890 MAIN0190
C 00001900 MAIN0191
C 00001910 MAIN0192
C 00001920 MAIN0193
C 00001930 MAIN0194
C THE MAIN PROGRAM CALLS THE SUBPROGRAMS CURAY AND SETUP 00001940 MAIN0195
C ***** 00001950 MAIN0196
COMMON/ORSTF/C(100),S(100),D(100),TH(100),X 00001960 MAIN0197
COMMON/CONFIX/DEL,NN,NDP,TMX,XDIM,YDIM,DP,KD 00001970 MAIN0198
COMMON/STUFF/CC(100),SS(100),DD(100),TTH(100),XX,RCSQ(100), 00001980 MAIN0199
1 RSSQ(100) 00001990 MAIN0200
COMMON/THY/T(1000),PP(1000),RP(600) 00002000 MAIN0201
COMMON/PLOT/CON,NNF,NPT,NSYN 00002010 MAIN0202
COMMON/FIXP/CDN(100),ARN(100),FLAT 00002020 MAIN0203
COMMON/STOR/P(1000),TD(1000) 00002030 MAIN0204
COMMON/THZ/TT(1000),PPZ(1000),PPR(1000) 00002040 MAIN0205
COMMON/TINP/DELT,DLTM,NDA,MTD,DLTP,NDB,JO,NDIRT 00002050 MAIN0206
COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET 00002060 MAIN0207
COMMON/CTRSTF/NCASE,NPRAY,NYT,NDUM,VRL2,VRL3 00002070 MAIN0208
COMMON/MYER/DTIM 00002080 MAIN0209
DIMENSION R(10) 00002090 MAIN0210
LOGICAL PRNT,PRNTS,PRNTC,FLAT 00002100 MAIN0211
FLAT=.TRUE. 00002110 MAIN0212
PRNT=.FALSE. 00002120 MAIN0213
PRNTS=.FALSE. 00002130 MAIN0214
PRNTC=.FALSE. 00002140 MAIN0215
C FLAT IS USED IN CURAY AND FOR THIS PROGRAM IS ALWAYS TRUE,INDICATING 00002150 MAIN0216

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C THAT THE MODEL USES A FLAT SECTION RATHER THAN AN ACTURAL SPHERICAL	00002160	MAIN0217
C MODEL OF THE EARTH	00002170	MAIN0218
C THESE THREE VARIABLES CONTROLS THE PRINTING OF INTERMEDIATE RESULTS	00002180	MAIN0219
C OF SOME DIAGNOSTIC IMPORTANCE. IN PARTICULAR PRNTC=TRUE.PRINTS ALL THE	00002190	MAIN0220
C ITERATION STEPS IN SUBROUTINE TIME2 FOR DETERMINING THE IMAGINARY	00002200	MAIN0221
C PART OF THE INTEGRATION VARIABLE T, THAT IS TIME ALONG THE COMPLEX	00002210	MAIN0222
C CONTOUR AFTER REFLECTION.DO NOT USE THIS OPTION IF RUNNING FOR MORE	00002220	MAIN0223
C THAN ONE RAY AS A PROHIBITIVE VOLUME OF OUTPUT IS PRODUCED.	00002230	MAIN0224
C IN GENERAL IT IS BEST NOT TO SET THESE OPTIONS TO TRUE FOR A RUN	00002240	MAIN0225
C INVOLVING MORE THAN A FEW RAYS	00002250	MAIN0226
C	00002260	MAIN0227
C INPUT MODEL PARAMETERS	00002270	MAIN0228
C	00002280	MAIN0229
READ (5,100) NMOD	00002290	MAIN0230
DO 200 J=1,NMOD	00002300	MAIN0231
200  READ (5,300) C(J),S(J),D(J),TH(J)	00002310	MAIN0232
100  FORMAT (I10)	00002320	MAIN0233
300  FORMAT (4F10.0)	00002330	MAIN0234
600  READ(5,500) X,IGD,KPEK	00002340	MAIN0235
500  FORMAT (F10.0,2I10)	00002350	MAIN0236
READ (5,501) DP,TMX,NN	00002360	MAIN0237
501  FORMAT (2F10.0,I10)	00002370	MAIN0238
C	00002380	MAIN0239
C ASSIGN VALUES TO CONSTANTS	00002390	MAIN0240
C	00002400	MAIN0241
NNF=1	00002410	MAIN0242
NPT=0	00002420	MAIN0243
JD=3	00002430	MAIN0244
C DESIGNATES A THREE LAYER MODEL	00002440	MAIN0245
CALL CURAY (JD)	00002450	MAIN0246
C CURAY IS APPARENTLY DESIGNED TO ALLOW FOR USE OF A SPHERICAL SECTION	00002460	MAIN0247
C OF THE EARTH AND IS REALLY UNNECESSARY HERE,IT CALCULATES A FEW	00002470	MAIN0248
C CONSTANTS SUCH AS THE SQUARES OF THE VELOCITIES. THESE CALCULATIONS	00002480	MAIN0249
C COULD EASILY BE INTEGRATED INTO THE MAIN PROGRAM	00002490	MAIN0250
CON =1.0/(2.*(3.14159**2)*D(2)*S(2)**2)	00002500	MAIN0251
C CON IS A FACTOR USED IN PSICO TO CALCULATE THE TERMS OF THE SURFACE	00002510	MAIN0252

C RESPONSE.	00002520	MAIN0253
XX=X	00002530	MAIN0254
C XX IS THE RANGE	00002540	MAIN0255
MTD=2	00002550	MAIN0256
C MTD IS USED IN CONTOR TO INCREASE THE INTERVAL SIZE BETWEEN THE LAST	00002560	MAIN0257
C BRANCHPOINT AND THE END OF THE RECORD	00002570	MAIN0258
DELTM=.0025	00002580	MAIN0259
C DELTM IS THE MINIMUM SIZE P(INTEGRATION VARIABLE) STEP,SEE CONTOR	00002590	MAIN0260
C SUBROUTINE	00002600	MAIN0261
DMAX=1.E-4	00002610	MAIN0262
DLTM=.1	00002620	MAIN0263
NDP=30	00002630	MAIN0264
C NDP IS A PARAMETER USED IN SUBROUTINE DELPS IN CALCULATING INTEGRATION	00002640	MAIN0265
C INTERVALS USING A SINE RELATIONSHIP	00002650	MAIN0266
DET=1.E-5	00002660	MAIN0267
DTIM=DP	00002670	MAIN0268
C IN CALCULATING INTEGRATION INTERVALS ON THE COMPLEX CONTOUR SIDE OF	00002680	MAIN0269
C REFLECTION POINT ,THE CALCULATION IS TERMINATED WHEN IT IS WITHIN	00002690	MAIN0270
C DTIM OF TO,THE TIME OF REFLECTION	00002700	MAIN0271
DEL=DP	00002710	MAIN0272
C DEL IS USED AS THE DELTA INTERVAL FOR THE TIME SERIES OF SURFACE	00002720	MAIN0273
C RESPONSE	00002730	MAIN0274
DLTP=DP	00002740	MAIN0275
NYT=3	00002750	MAIN0276
VRL2=.92*S(2)	00002760	MAIN0277
VRL3=.92*S(3)	00002770	MAIN0278
NPRAY=40	00002780	MAIN0279
K=NN/2	00002790	MAIN0280
NCASE = 0	00002800	MAIN0281
C NCASE REFERS TO THE SOURCE AND MODEL COMBINATION,NCASE=0 DESIGNATES	00002810	MAIN0282
C SH SOURCE AND THREE LAYER MODEL AS HERE,=1 P,SV,SOURCE AND SAME MODEL	00002820	MAIN0283
C ,=2 IS APPARENTLY USED FOR SOLID HALF SPACE RUNS,NOT RELEVANT HERE	00002830	MAIN0284
C SETUP EXECUTES THE PROGRAM AND GENERATES OUTPUT	00002840	MAIN0285
CALL SETUP(1,0,01,36,C,MPL0T,1)	00002850	MAIN0286
END	00002860	MAIN0287
ADJT		MAIN0288

	SUBROUTINE ACJUST(NN,NFIX)	00002870	MAIN0289
	IMPLICIT REAL*8 (A-H,O-Z)	00002880	MAIN0290
	COMMON/EXACT/PHIZ(1000),PHIR(1000),TD(1000),NEND,NM	00002890	MAIN0291
	COMMON/THZ/ T(1000),PPZ(1000),PPR(1000)	00002900	MAIN0292
	M = NM+1	00002910	MAIN0293
	TR = TC(M)	00002920	MAIN0294
	I = 0	00002930	MAIN0295
80	I = I+1	00002940	MAIN0296
	IF(I.GT.NN) GO TO 70	00002950	MAIN0297
	IF(T(I).GT.TR) GO TO 81	00002960	MAIN0298
	GO TO 80	00002970	MAIN0299
81	DNE = TR-T(I-1)	00002980	MAIN0300
	DPL = T(I)-TR	00002990	MAIN0301
	IF (DABS(DNE) .GT. DABS(DPL)) GOT O 83	00003000	MAIN0302
	DELTA = -DNE	00003010	MAIN0303
	NFIX = I-1	00003020	MAIN0304
	GO TO 85	00003030	MAIN0305
83	DELTA = DPL	00003040	MAIN0306
	NFIX = I	00003050	MAIN0307
85	DO 84 J=1,NEND	00003060	MAIN0308
	TD(J) = TD(J)+DELTA	00003070	MAIN0309
84	CONTINUE	00003080	MAIN0310
	RETURN	00003090	MAIN0311
70	NFIX = 0	00003100	MAIN0312
	RETURN	00003110	MAIN0313
	END	00003120	MAIN0314

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SUBROUTINE CONTOR(TM, M, KN, N, MO)
C *****
C THIS SUBROUTINE SPECIFIES THE COMPLEX CONTOUR OF INTEGRATION FOR THE
C REFLECTED ARRIVAL
C THE SUBPROGRAMS TIME2 AND DELPS ARE CALLED
C
C CALL LIST: TM IS THE LENGTH OF RECORD (IN SEC) TO BE CALCULATED AFTER
C THE REFLECTED ARRIVAL, M HAS NO APPARENT FUNCTION, NCR DOES KN, N IS THE
C RAY NUMBER, AND MO THE NUMBER OF POINTS FIRST FOLLOWING THE REFLECTION
C ARRIVAL.
C *****
IMPLICIT REAL*8 (A-H, O-Z)
COMMON/MAGIC/PP(1200), DDPT(1200), TT(1200)
COMMON/SPE/DELP(800), DD1, DD2, DD3, DD4, NU
COMMON/PATHC/PU, TO, K
COMMON/TINP/DELT, DLT, NDA, MTD, DLTP, NDB, JO, NDIRT
COMMON/TFIX/TN1, TN2, TN3, TN4, JN1, JN2, JN3, JN4
COMMON/CTRSTF/NCASE, NPRAY, NYT, NDUM, VRL2, VRL3
DIMENSION DER(400)
LOGICAL PRNT, PRNTS, PRNTC
COMMON/LPRINT/PRNT, PRNTS, KST, KEND, PRNTC, NDC, DET
COMMON/MYER/DTIM
COMPLEX*16 PP, DDPT, P, CT, DEV
DET = 1.D-5
JN = 10
1 Q = PG
I = MO-1
PIL = 1.E-6
PP(I) = PC
TT(I) = TO
KM = 100
IF (DELP(1).LE.DELT) DELP(1)=DELT
33 I = KM-1
L = 0
DO 10 J=1, JN
L = L+1

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00003130 CONT0001
00003140 CONT0002
00003150 CONT0003
00003160 CONT0004
00003170 CONT0005
00003180 CONT0006
00003190 CONT0007
00003200 CONT0008
00003210 CONT0009
00003220 CONT0010
00003230 CONT0011
00003240 CONT0012
00003250 CONT0013
00003260 CONT0014
00003270 CONT0015
00003280 CONT0016
00003290 CONT0017
00003300 CONT0018
00003310 CONT0019
00003320 CONT0020
00003330 CONT0021
00003340 CONT0022
00003350 CONT0023
00003360 CONT0024
00003370 CONT0025
00003380 CONT0026
00003390 CONT0027
00003400 CONT0028
00003410 CONT0029
00003420 CONT0030
00003430 CONT0031
00003440 CONT0032
00003450 CONT0033
00003460 CONT0034
00003470 CONT0035
00003480 CONT0036

```



	I	= I+1	00003490	CONT0037
9	Q	= Q+DELP(J)	00003500	CONT0038
	PI	= PG*.2	00003510	CONT0039
	DL	= PI*.45	00003520	CONT0040
	CALL	TIME2(Q,PI,DL,P,DEV,CT,KN,N,PIL)	00003530	CONT0041
	RTIME	= CT	00003540	CONT0042
	TIMEI	= CT*(0.,-1.)	00003550	CONT0043
	DR	= DEV	00003560	CONT0044
	DDPT(I)	= DEV	00003570	CONT0045
	TT(I)	= RTIME	00003580	CONT0046
	PP(I)	= P	00003590	CONT0047
	IF(TT(I)-TO.LE.DTIM)	GO TO 32	00003600	CONT0048
	IF(DR.LE.0.)	GO TO 30	00003610	CONT0049
	IF(DABS(TIMEI).GT.1.E-3)	GO TO 30	00003620	CONT0050
	IF(RTIME-TO.LT..001)	GO TO 30	00003630	CONT0051
	JJ	= J+1	00003640	CONT0052
	DELP(JJ)	= ((PO-PP(I))/2.)	00003650	CONT0053
10		CONTINUE	00003660	CONT0054
30	IF(I.LE.KM)	DELP(1)=5.*DELP(1)	00003670	CONT0055
	IF(I.LE.KM)	GO TO 33	00003680	CONT0056
	PRINT	101	00003690	CONT0057
101	FORMAT(//'	EXIT LOOP CONDITION IN CONTOR: I.GT.KM- STATEMENT 30'/)	00003700	CONT0058
	I	= I-1	00003710	CONT0059
32	JJ	= I-KM+1	00003720	CONT0060
	DO	31 J=1,JJ	00003730	CONT0061
	LL	= MO+J-1	00003740	CONT0062
	NN	= I-J+1	00003750	CONT0063
	TT(LL)	= TT(NN)	00003760	CONT0064
	PP(LL)	= PP(NN)	00003770	CONT0065
	DDPT(LL)	= DDPT(NN)	00003780	CONT0066
31		CONTINUE	00003790	CONT0067
	I	= LL	00003800	CONT0068
	DELP(JN)	= (PP(LL)-PP(LL-1))	00003810	CONT0069
	J	= JN	00003820	CONT0070
	MM	= 1	00003830	CONT0071
	TM	= TMX+TO	00003840	CONT0072

```

PI          = PP(LL)*(0.,-1.)
Q           = PP(LL)
JF = LL
DER(JF) = PP(LL) - PP(LL-1)
IF(NCASE.EQ.0) GO TO 12
IF(NCASE.EQ.1)RG=DABS(1./VRL2-Q)
IF(NCASE.EQ.2)RG=DABS(1./VRL3-Q)
CALL DELPS(NPRAY,RG,1,NYT)
J1          = LL
J2          = J1+NO
IJ          = 0
DO 21 J=J1,J2
IJ          = IJ+1
21  DER(J)   = DELP(IJ)
JF         = J2
IF(NCASE.EQ.1) GO TO 23
RG         =DABS(1./VRL2-1./VRL3)
CALL DELPS(NPRAY,RG,1,NYT)
J1         = J2+1
J2         = J1+NO
IJ         = 0
DO 24 J=J1,J2
IJ         = IJ+1
24  DER(J)   = DELP(IJ)
JF         = J2
23  IF(PRNTC) WRITE(6,100) (DER(J),J=J1,J2)
100  FORMAT(6E12.4)
DO 25 J=LL,JF
Q         = Q+DER(J)
I         = I+1
DELPR     = (PP(I-1)-PP(I-2))
DELPI     = (PP(I-1)-PP(I-2)) *(0.,-1.)
PI        = (DELPI*DER(J) )/DELPR +PI
DL        = PI*.5
CALL TIME2(Q,PI,DL,P,DEV,CT,KN,N,PIL)
PP(I)     = P

```

```

00003850 CONT0073
00003860 CONT0074
00003870 CONT0075
00003880 CONT0076
00003890 CONT0077
00003900 CONT0078
00003910 CONT0079
00003920 CONT0080
00003930 CONT0081
00003940 CONT0082
00003950 CONT0083
00003960 CONT0084
00003970 CONT0085
00003980 CONT0086
00003990 CONT0087
00004000 CONT0088
00004010 CONT0089
00004020 CONT0090
00004030 CONT0091
00004040 CONT0092
00004050 CONT0093
00004060 CONT0094
00004070 CONT0095
00004080 CONT0096
00004090 CONT0097
00004100 CONT0098
00004110 CONT0099
00004120 CONT0100
00004130 CONT0101
00004140 CONT0102
00004150 CONT0103
00004160 CONT0104
00004170 CONT0105
00004180 CONT0106
00004190 CONT0107
00004200 CONT0108

```

	RTIME	= CT	00004210	CONT0109
	DDPT(I)	= DEV	00004220	CONT0110
	TT(I)	= RTIME	00004230	CONT0111
	IF(TT(I).GT.TM)	GO TO 13	00004240	CONT0112
25	CONTINUE		00004250	CONT0113
12	Q	= Q+MM*DER(JF)	00004260	CONT0114
	I	= I+1	00004270	CONT0115
	DELPR	= (PP(I-1)-PP(I-2))	00004280	CONT0116
	DELPI	= (PP(I-1)-PP(I-2)) *(0.,-1.)	00004290	CONT0117
	PI	= (DELPI*MM*DER(JF))/DELPR +PI	00004300	CONT0118
	DL	= PI*.5	00004310	CONT0119
	CALL TIME2(Q,PI,DL,P,DEV,CT,KN,N,PIL)		00004320	CONT0120
	PP(I)	= P	00004330	CONT0121
	RTIME	= CT	00004340	CONT0122
	DDPT(I)	= DEV	00004350	CONT0123
	TT(I)	= RTIME	00004360	CONT0124
	IF(TT(I).GT.TM)	GO TO 13	00004370	CONT0125
14	IF(TT(I)-TT(I-1).LE.DLTM)	MM=MTD*MM	00004380	CONT0126
	GO TO 12		00004390	CONT0127
13	CONTINUE		00004400	CONT0128
	M	= I	00004410	CONT0129
	RETURN		00004420	CONT0130
	END		00004430	CONT0131

```
COMPLEX FUNCTION CR*16 (P,C)
IMPLICIT REAL*8 (A-H,O-Z)
COMPLEX*16 P,CZ
CZ=1./C**2-P*P
U=CZ
X=CZ*(0.,-1.)
R=DSQRT(X*X + U*U)
W1= DABS(R+U)/2.
W2= DABS(R-U)/2.
R1=DSQRT(W1)
R2=DSQRT(W2)
CR=R1-R2*(0.,1.)
RETURN
END
```

```
00004440 CRFN0001
00004450 CRFN0002
00004460 CRFN0003
00004470 CRFN0004
00004480 CRFN0005
00004490 CRFN0006
00004500 CRFN0007
00004510 CRFN0008
00004520 CRFN0009
00004530 CRFN0010
00004540 CRFN0011
00004550 CRFN0012
00004560 CRFN0013
00004570 CRFN0014
```

	SUBROUTINE CURAY(JO)	00004580	CURY0001
	IMPLICIT REAL*8 (A-H,O-Z)	00004590	CURY0002
	COMMON /SENSE/ DRCSQ(100),DRSSQ(100)	00004600	CURY0003
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00004610	CURY0004
	COMMON/DRSTF/CC(100),SS(100),DD(100),TTH(100),XX	00004620	CURY0005
	COMMON/FIXP/DDN(100),ARN(100),FLAT	00004630	CURY0006
	LOGICAL FLAT	00004640	CURY0007
	DIMENSION DEPTH(100)	00004650	CURY0008
	DIMENSION DT(100)	00004660	CURY0009
	X = XX	00004670	CURY0010
	PRINT 2, X	00004680	CURY0011
2	FORMAT (1H1,10X,'CURAY' /11X,'RANGE',F10.0/16X,'THICKNESS',9X,'	00004690	CURY0012
	+DEPTH',5X,'P-VELOCITY',5X,'S-VELOCITY',8X,'DENSITY')	00004700	CURY0013
	DEPTH(1) = TTH(1)/2.0	00004710	CURY0014
	DO 10 J = 2,JO	00004720	CURY0015
10	DEPTH(J)= DEPTH(J-1)+(TTH(J)+TTH(J-1))/2.	00004730	CURY0016
	DO 5 J = 1,JC	00004740	CURY0017
	Q = 6371.0 / (6371.0-DEPTH(J))	00004750	CURY0018
	IF (FLAT) Q = 1.	00004760	CURY0019
	ARN(J) = 1./Q	00004770	CURY0020
	C(J) = CC(J)*Q	00004780	CURY0021
	S(J) = SS(J)*Q	00004790	CURY0022
	D(J) = DD(J)*Q	00004800	CURY0023
	TH(J) = TTH(J)*Q	00004810	CURY0024
	DRCSQ(J) = 1.0 / C(J) **2	00004820	CURY0025
	DRSSQ(J) = 1.0 / S(J) **2	00004830	CURY0026
	RCSQ(J) = DRCSQ(J)	00004840	CURY0027
	RSSQ(J) = DRSSQ(J)	00004850	CURY0028
5	CONTINUE	00004860	CURY0029
	DT(1) = TTH(1)	00004870	CURY0030
	DO 20 J=2,JO	00004880	CURY0031
	DT(J) = DT(J-1) +TTH(J)	00004890	CURY0032
20	CONTINUE	00004900	CURY0033
	DO 25 J=1,JC	00004910	CURY0034
	IF (FLAT) DT(J) = 0.0	00004920	CURY0035
	DDN(J) = (6371.-DT(J))/6371.	00004930	CURY0036

25     CONTINUE  
PRINT 1, (J, TH(J), DEPTH(J), C(J), S(J), D(J), ARN(J), DDN(J), J=1, JO)  
1     FORMAT (I5, 5X, 7G15.4)  
      RETURN  
      END

00004940 CURY0037  
00004950 CURY0038  
00004960 CURY0039  
00004970 CURY0040  
00004980 CURY0041

```

SUBROUTINE DELPS (NNN, RG, NN, N)
IMPLICIT REAL*8 (A-H, O-Z)
DIMENSION PP (200)
COMMON/SPE/DEL P (800), DD1, DD2, DD3, DD4, NO
RG      = RG-1.E-08
PI      = 3.141593
AN      = PI/(NNN*2.)
J       = NN
A       = AN
DEL P (J) = RG*(DSIN(A)**N)
TO      = DEL P (J)
A       = A+AN
K       = 1
PP (1)  = DEL P (1)
1      J   = J+1
      K   = K+1
PP (K)  = RG*DSIN(A)**N
DEL P (J) = PP (K)-PP (K-1)
DEL P (J) = DABS (DEL P (J))
TO      = TO+DEL P (J)
A       = A+AN
2      IF (TO.LT.RG) GO TO 1
      NO  = J-1
RETURN
END

```

```

00004990 DELP0001
00005000 DELP0002
00005010 DELP0003
00005020 DELP0004
00005030 DELP0005
00005040 DELP0006
00005050 DELP0007
00005060 DELP0008
00005070 DELP0009
00005080 DELP0010
00005090 DELP0011
00005100 DELP0012
00005110 DELP0013
00005120 DELP0014
00005130 DELP0015
00005140 DELP0016
00005150 DELP0017
00005160 DELP0018
00005170 DELP0019
00005180 DELP0020
00005190 DELP0021
00005200 DELP0022
00005210 DELP0023
00005220 DELP0024
00005230 DELP0025

```

	SUBROUTINE FIND2 (Q,K,DEL,DET,PQ,TQ,NRY)	00005240	FND20001
	IMPLICIT REAL*8 (A-H,O-Z)	00005250	FND20002
	DIMENSION E(100)	00005260	FND20003
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)	00005270	FND20004
	COMMON/PLACE/THIC,H,KSSP	00005280	FND20005
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X	00005290	FND20006
	COMMON /SENSE/ RCSQ(100),RSSQ(100)	00005300	FND20007
	COMMON / LPRINT/ PRNT,PRNTS	00005310	FND20008
	LOGICAL PRNT,PRNTS	00005320	FND20009
	TH(1) = (1.-KUD(NRY))*(THIC-H) + KUD(NRY)*H	00005330	FND20010
	TH(3) = 0.	00005340	FND20011
	TH(4) = 0.	00005350	FND20012
	IF (KSSP .EQ. 1) TH(4)=TH(1)	00005360	FND20013
	IF (KSSP .EQ. 0) TH(3)=TH(1)	00005370	FND20014
	KF = 1	00005380	FND20015
	KOUNT = 0	00005390	FND20016
	TDE = DEL	00005400	FND20017
8	P = Q	00005410	FND20018
	KOUNT = KCOUNT + 1	00005420	FND20019
5	P = P+DEL	00005430	FND20020
	PSQ = P ** 2	00005440	FND20021
	E(2) = DSQRT(DABS(RCSQ(2)-PSQ))	00005450	FND20022
	E(3) = DSQRT(DABS(RSSQ(2)-PSQ))	00005460	FND20023
	BLTEM = -TH(2)*LTP(NRY)/E(2) -TH(2)*LTS(NRY)/E(3)	00005470	FND20024
	BLTEM = BLTEM-TH(4)/E(2)	00005480	FND20025
	BLTEM = BLTEM-TH(3)/E(3)	00005490	FND20026
	BL = X + BLTEM*P	00005500	FND20027
	IF(DABS (DEL).LE.1.E-18) GO TO 1	00005510	FND20028
6	IF (DABS (BL).LE.X/DET) GO TO 1	00005520	FND20029
2	IF(BL)3,1,4	00005530	FND20030
3	DEL =-DABS (DEL*.5)	00005540	FND20031
	GO TO 5	00005550	FND20032
4	DEL =DABS(DEL*.5)	00005560	FND20033
	GO TO 5	00005570	FND20034
1	IF(DABS(BL).LT.1.E-8) GO TO 7	00005580	FND20035
	IF (KOUNT.GE.5) GO TO 7	00005590	FND20036



	Q	= 0/10.0	00005600	FND20037
	DEL	= TDE	00005610	FND20038
	GO TO 3		00005620	FND20039
7	PO	= P	00005630	FND20040
	TOTEM	= E(2)*TH(4)+E(2)*LTP(NRY)*TH(2)+E(3)*LTS(NRY)*TH(2)	00005640	FND20041
1		+E(3)*TH(3)	00005650	FND20042
	TO	= P*X + TOTEM	00005660	FND20043
	PO	= PO	00005670	FND20044
	TO	= TO	00005680	FND20045
	IF (DABS(BL).LT.1.0E-6)	RETURN	00005690	FND20046
	IF (.NOT.PRNT)	RETURN	00005700	FND20047
	WRITE (6,17)	PO,TO,BL	00005710	FND20048
17	FORMAT (1H0,4X,'PO ',E18.6,10X,'TO ',E18.6,10X,'BL ',E18.6)		00005720	FND20049
	RETURN		00005730	FND20050
	END		00005740	FND20051

	SUBROUTINE HELP(K,N,P,TTP,DTP,NRY)	00005750	HELP0001
	IMPLICIT REAL*8 (A-H,O-Z)	00005760	HELP0002
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00005770	HELP0003
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)	00005780	HELP0004
	COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET	00005790	HELP0005
	LOGICAL PRNT,PRNTS,PRNTC,FLAT	00005800	HELP0006
100	FORMAT(10X,'SUB. HELP,P,E,TOTEM,BLTEM,DTP,TTP',/,6(E16.6))	00005810	HELP0007
	PSQ = P**2	00005820	HELP0008
	J = 2	00005830	HELP0009
	E = DSQRT(DABS(RCSQ(J)-PSQ))	00005840	HELP0010
	TOTEM = E*(TH(4)+TH(2)*LTP(NRY))	00005850	HELP0011
	BLTEM = -(TH(4)+TH(2)*LTP(NRY))/E	00005860	HELP0012
	IF(PRNTC) WRITE(6,100) P,E,TOTEM,BLTEM,DTP,TTP	00005870	HELP0013
	E = DSQRT(DABS(RSSQ(J)-PSQ))	00005880	HELP0014
	TOTEM = TOTEM+TH(2)*LTS(NRY)*E +TH(3)*E	00005890	HELP0015
	BLTEM = BLTEM-TH(2)*LTS(NRY)/E -TH(3)/E	00005900	HELP0016
	BL = X + P*BLTEM	00005910	HELP0017
	TO = P*X + TOTEM	00005920	HELP0018
	DTP = 1./BL	00005930	HELP0019
	TTP = TO	00005940	HELP0020
	IF(PRNTC) WRITE(6,100) P,E,TOTEM,BLTEM,DTP,TTP	00005950	HELP0021
	RETURN	00005960	HELP0022
	END	00005970	HELP0023

```

SUBROUTINE HIGH(NDP, TMX, K, KI, N)
C *****
C THE SUBPROGRAM HIGH CALCULATES THE SURFACE RESPONSE FOR EACH RAY
C NDP IS USED IN CALCULATING THE INTEGRATION STEPS ABOUT REFLECTION ,
C TMX IS THE LENGTH OF THE RECORD READ IN MAIN, K AND KI DO NOT SEEM TO
C BE USED, N IS THE RAY NUMBER
C THE SUBPROGRAM FIND2, HELP, DELPS, PLN1, CONTOR, AND PLN2 ARE CALLED
C THE SURFACE RESPONSE IS PRINTED FOR EVERY FIFTH RAY
C *****
IMPLICIT REAL*8 (A-H, O-Z)
COMMON/ RAYPAR/ KUD(100), KRSP(100), LTS(100), LTP(100), LREF(100, 4)
COMMON/ PLACE/ THIC, H, KSSP
COMMON/ EXACT/ PHIZ(1000), PHIR(1000), TD(1000), NEND, NM
COMMON/ MAGIC/ PP(1200), DDPT(1200), TT(1200)
COMMON/ SPE/ DELP(800), CD1, DD2, DD3, DD4, NO
COMMON/ PATHC/ PO, TO, KK
COMMON/ TINP/ DELTM, DLTM, NDA, MTD, DLTP, NDB, JO, NDIRT
COMMON/ ORSTF/ CC(100), SS(100), DD(100), TTH(100), XX
COMMON / LPRINT/ PRNT, PRNTS
LOGICAL PRNT, PRNTS
COMPLEX*16 PP, DDPT
JN1 = 12
JN2 = 10
JN3 = 8
JN4 = 100
TN1 = .8
TN2 = .2
TN3 = .1
TN4 = .001
C THESE EIGHT PARAMETERS ARE USED IN CALCULATING THE INTEGRATION
C INTERVAL ABOUT PO , THE POINT OF REFLECTION
V2 = SS(3)
C V2 SHOULD BE THE LARGEST PROPAGATION VELOCITY USED IN THE MODEL,
C FOR P, SV MODEL , CC(3)
NRV = N
C NRV BECOMES THE RAY NUMBER

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```

00005980 HIGH0001
00005990 HIGH0002
00006000 HIGH0003
00006010 HIGH0004
00006020 HIGH0005
00006030 HIGH0006
00006040 HIGH0007
00006050 HIGH0008
00006060 HIGH0009
00006070 HIGH0010
00006080 HIGH0011
00006090 HIGH0012
00006100 HIGH0013
00006110 HIGH0014
00006120 HIGH0015
00006130 HIGH0016
00006140 HIGH0017
00006150 HIGH0018
00006160 HIGH0019
00006170 HIGH0020
00006180 HIGH0021
00006190 HIGH0022
00006200 HIGH0023
00006210 HIGH0024
00006220 HIGH0025
00006230 HIGH0026
00006240 HIGH0027
00006250 HIGH0028
00006260 HIGH0029
00006270 HIGH0030
00006280 HIGH0031
00006290 HIGH0032
00006300 HIGH0033
00006310 HIGH0034
00006320 HIGH0035
00006330 HIGH0036

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C	DEL IS THE INITIAL ITERATION STEP INP,THE INTEGRATION PARAMETER, FOR	00006340	HIGH0037
C	USE IN FIND2 IN DETERMINING THE VALUES OF P AND TIME AT THE REFLECTION	00006350	HIGH0038
C	ARRIVAL IF THE SIGNAL IS AT ANY TIME IN P OR COMPRESSIONAL MODE DEL =	00006360	HIGH0039
C	1./CC(I),IF NOT DEL =1./SS(2)	00006370	HIGH0040
	KNRY = NRY*KSSP	00006380	HIGH0041
	DEL = 1./SS(2)	00006390	HIGH0042
	IF(LTP(NRY).GT.0) GO TO 82	00006400	HIGH0043
	IF(KSSP.EQ.0) GO TO 81	00006410	HIGH0044
82	DEL = 1./CC(2)	00006420	HIGH0045
81	P = -1.E-9	00006430	HIGH0046
	DAT = 1.E+12	00006440	HIGH0047
	CALL FIND2(P, KK, DEL, DAT, PG, TO, N)	00006450	HIGH0048
	NNN = NDP	00006460	HIGH0049
	NK = 2	00006470	HIGH0050
	IF(NRY.EQ.1) V2=.9*SS(2)	00006480	HIGH0051
	P = 1./V2	00006490	HIGH0052
	RG =DABS(P0-P)	00006500	HIGH0053
	CALL HELP(K, N, P, TTP, DTP, N)	00006510	HIGH0054
	TC = TTP	00006520	HIGH0055
	TG = TC-TTP	00006530	HIGH0056
	IF(P0.LE.1./V2) GO TO 6	00006540	HIGH0057
	IF(TG.GT.TN1) GO TO 6	00006550	HIGH0058
	JN = JN1	00006560	HIGH0059
	IF(TG.GT.TN2) GO TO18	00006570	HIGH0060
	JN = JN2	00006580	HIGH0061
	IF(TG.GT.TN3) GO TO18	00006590	HIGH0062
	JN = JN3	00006600	HIGH0063
18	QZ = RG/(JN+1)	00006610	HIGH0064
	DO 15 J = 1, JN	00006620	HIGH0065
	DELP(J) = QZ	00006630	HIGH0066
15	CONTINUE	00006640	HIGH0067
	N0 = JN	00006650	HIGH0068
	IF(TG.LT.TN4) GO TO 2	00006660	HIGH0069
	GO TO 19	00006670	HIGH0070
6	CALL DELPS(NNN, RG, 1, NK)	00006680	HIGH0071
	IF (.NOT.PRNT) GO TO 19	00006690	HIGH0072

	PRINT 7, V2, XM, PO, RG, TC, TD, (DELP(J),J=1,NO)	00006700	HIGH0073
7	FORMAT (1H0,4X,'V2= ',G13.6,5X,'XM= ',G13.6,5X,'PO= ',	00006710	HIGH0074
	1G13.6/5X,'RG= ',G13.6,5X,'TC= ',G13.6,5X,'TD= ',G13.6/5X,'DELP'/	00006720	HIGH0075
	2(G15.6))	00006730	HIGH0076
19	IF(PO.LE.1./V2) GO TO 2	00006740	HIGH0077
	CALL PLN1(PO,TD,K,N,TC,N,V2)	00006750	HIGH0078
2	MO = NO+2	00006760	HIGH0079
	IF(TG.LT.TN4) MO=2	00006770	HIGH0080
	IF(PO.LT.1./V2) MO=2	00006780	HIGH0081
	CALL CONTOR(TMX,M,KN,N,MO)	00006790	HIGH0082
	IF (.NOT.PRINT) GO TO 620	00006800	HIGH0083
	WRITE (6,5)	00006810	HIGH0084
5	FORMAT (1H0,13X,'PP',27X,'DDPT',24X,'TT')	00006820	HIGH0085
	JJ = MO	00006830	HIGH0086
	WRITE(6,200) (PP(J),DDPT(J),TT(J),J=JJ,M)	00006840	HIGH0087
200	FORMAT(5E15.4)	00006850	HIGH0088
620	CALL PLN2(PO,TD,K,MO,M,N)	00006860	HIGH0089
	NEND = M	00006870	HIGH0090
	NM = NO	00006880	HIGH0091
	IF(PO.LT.1./V2) NM=0	00006890	HIGH0092
	IF(TG.LT.TN4)NM= 0	00006900	HIGH0093
	LK = -19	00006910	HIGH0094
	WRITE (6,98)	00006920	HIGH0095
	KJMP=5	00006930	HIGH0096
	LK = 1-KJMP	00006940	HIGH0097
97	LK =LK+KJMP	00006950	HIGH0098
	IF (LK .GT. NEND) GC TO 99	00006960	HIGH0099
	WRITE (6,100) TD(LK),PHIZ(LK),PHIR(LK),LK	00006970	HIGH0100
	GO TO 97	00006980	HIGH0101
99	CONTINUE	00006990	HIGH0102
98	FORMAT (12X,'SUB. HIGH TD,PHIZ,PHIR',2X)	00007000	HIGH0103
100	FORMAT (3E18.6,I10)	00007010	HIGH0104
	RETURN	00007020	HIGH0105
	END	00007030	HIGH0106

```

SUBROUTINE INTERP(XP,YP,N,X,Y)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION XP(1000),YP(1000)
1  IF (X .GT. XP(N)) GO TO 6
   IF (X .LT. XP(1)) GO TO 6
2  DO 10 I=1,N
   IF (XP(I) -X) 10,102,3
10  CONTINUE
3  K      = I-1
   DIF1   = XP(I) -XP(K)
   DIF2   = XP(I) -X
   RATIO  = DIF2/DIF1
   DIFY   =DABS (YP(I) - YP(K))
   DR     = DIFY*RATIO
   IF (YP(I) .GT. YP(K)) GO TO 4
5  Y      = YP(I) + DR
   RETURN
4  Y      = YP(I) - DR
   RETURN
102 Y      = YP(I)
   RETURN
6  Y      = 0.
   RETURN
END

```

```

00007040 INTP0001
00007050 INTP0002
00007060 INTP0003
00007070 INTP0004
00007080 INTP0005
00007090 INTP0006
00007100 INTP0007
00007110 INTP0008
00007120 INTP0009
00007130 INTP0010
00007140 INTP0011
00007150 INTP0012
00007160 INTP0013
00007170 INTP0014
00007180 INTP0015
00007190 INTP0016
00007200 INTP0017
00007210 INTP0018
00007220 INTP0019
00007230 INTP0020
00007240 INTP0021
00007250 INTP0022
00007260 INTP0023
00007270 INTP0024

```

SUBROUTINE PLN1(PD,TD,K,N,TC,NRY,V2)	00007280	PLN10001
IMPLICIT REAL*8 (A-H,O-Z)	00007290	PLN10002
COMMON/T INP/DELTM,DLTM,NDA,MTD,DLTP,NDB,JO,NDIRT	00007300	PLN10003
COMMON/SPE/DELP(800),DD1,DD2,DD3,DD4,ND	00007310	PLN10004
COMMON/DRSTF/C(100),S(100),D(100),TH(100),X	00007320	PLN10005
COMMON/TRESL/PZ1(500),PR1(500)	00007330	PLN10006
COMMON/MAGIC/PQ(1200),DDPT(1200),TTT(1200)	00007340	PLN10007
COMMON/EXACT/PHIZ(1000),PHIR(1000),TT(1000),NEND,NM	00007350	PLN10008
COMMON / LPRINT/ PRNT,PRNTS	00007360	PLN10009
LOGICAL PRNT,PRNTS	00007370	PLN10010
COMPLEX*16 PQ,DDPT,FNZ,FNR,FNZ1,FNR1,Q	00007380	PLN10011
P = 1./V2	00007390	PLN10012
DO 80 I=2,ND	00007400	PLN10013
J = I-1	00007410	PLN10014
P = P+DELP(J)	00007420	PLN10015
Q = P+0.*(0.,1.)	00007430	PLN10016
CALL HELP(K,N,P,TTP,DTP,NRY)	00007440	PLN10017
IF(PRNT) PRINT 100,Q,P,DTP,TTP	00007450	PLN10018
TT(I) = TTP	00007460	PLN10019
DDPT(I) = DTP	00007470	PLN10020
CALL PSICO(Q,FNZ,FNR,FNZ1,FNR1,I,NRY)	00007480	PLN10021
IF(PRNT) PRINT 100,FNZ,FNR,FNZ1,FNR1	00007490	PLN10022
PHIZ(I) = FNZ * (0.,-1.)	00007500	PLN10023
PHIR(I) = FNR * (0.,-1.)	00007510	PLN10024
PZ1(I) = FNZ1 * (0.,-1.)	00007520	PLN10025
PR1(I) = FNR1 * (0.,-1.)	00007530	PLN10026
IF ((TD-TTP).LT.DLTP) GO TO 5	00007540	PLN10027
80 CONTINUE	00007550	PLN10028
100 FORMAT(8E15.4)	00007560	PLN10029
WRITE(6,100) PD,TD	00007570	PLN10030
5 ND = J+1	00007580	PLN10031
I = ND	00007590	PLN10032
4 IF(TC-TTP.LT.DLTP) GO TO 3	00007600	PLN10033
PP = PD - P	00007610	PLN10034
P = P + PP/2.0	00007620	PLN10035
I = I+1	00007630	PLN10036

```

NO      = I
Q       = P
CALL HELP(K,N,P,TTP,DTP,NRY)
TT(I)   = TTP
DDPT(I) = DTP
CALL PSICG(Q,FNZ,FNR,FNZ1,FNR1,I,NRY)
PHIZ(I) = FNZ * (0.,-1.)
PHIR(I) = FNR * (0.,-1.)
PZ1(I)  = FNZ1 * (0.,-1.)
PR1(I)  = FNR1 * (0.,-1.)
IF(PRNT) PRINT 100,FNZ,FNR,FNZ1,FNR1
GO TO 4
3 TT(1)  = TC
  PHIZ(1) = 0.
  PHIR(1) = 0.
  PR1(1)  = 0.
  PZ1(1)  = 0.
RETURN
END

```

```

00007640 PLN10037
00007650 PLN10038
00007660 PLN10039
00007670 PLN10040
00007680 PLN10041
00007690 PLN10042
00007700 PLN10043
00007710 PLN10044
00007720 PLN10045
00007730 PLN10046
00007740 PLN10047
00007750 PLN10048
00007760 PLN10049
00007770 PLN10050
00007780 PLN10051
00007790 PLN10052
00007800 PLN10053
00007810 PLN10054
00007820 PLN10055

```



	SUBROUTINE PLN2(PQ,TC,K,MO,M,NRY)	00007830	PLN20001
	IMPLICIT REAL*8 (A-H,O-Z)	00007840	PLN20002
	COMMON/FIXP/DDN(100),ARN(100)	00007850	PLN20003
	COMMON/TINP/DELT,DLTM,NDA,MTD,DLTP,NDB,JG,NDIRT	00007860	PLN20004
	COMMON/MAGIC/PP(1200),DDPT(1200),TT(1200)	00007870	PLN20005
	COMMON/EXACT/PHIZ(1000),PHIR(1000),TTT(1000),NEND,NM	00007880	PLN20006
	COMMON/TRESL/PZ1(500),PR1(500)	00007890	PLN20007
	COMMON/URSTF/C(100),S(100),D(100),TH(100),X	00007900	PLN20008
	DIMENSION FF(50),GG(50)	00007910	PLN20009
	COMMON / LPRINT/ PRNT,PRNTS	00007920	PLN20010
	LOGICAL PRNT,PRNTS	00007930	PLN20011
	COMPLEX*16 PP,BT,DDPT,RP,RPP,GC,P	00007940	PLN20012
	COMPLEX*16 FNZ,FNR,FNZ1,FNR1	00007950	PLN20013
	DO 5 I=MO,M	00007960	PLN20014
	TTT(I) = TT(I)	00007970	PLN20015
	P = PP(I)	00007980	PLN20016
	CALL PSICO(P,FNZ,FNR,FNZ1,FNR1,I,NRY)	00007990	PLN20017
	PHIZ(I) = FNZ*(0.,-1.)	00008000	PLN20018
	PHIR(I) = FNR*(0.,-1.)	00008010	PLN20019
	PR1(I) = FNR1*(0.,-1.)	00008020	PLN20020
	PZ1(I) = FNR1*(0.,-1.)	00008030	PLN20021
	IF(PRNT) PRINT 100,FNZ,FNR,FNZ1,FNR1	00008040	PLN20022
5	CONTINUE	00008050	PLN20023
100	FORMAT(8E15.4)	00008060	PLN20024
3	NO = MO-2	00008070	PLN20025
	DP = DLTP	00008080	PLN20026
	P = PQ*(1.,0.)+0.*(0.,1.)	00008090	PLN20027
	I = MO-1	00008100	PLN20028
	Q = PQ	00008110	PLN20029
	DDPT(I) = SF2(Q,K,NRY,DP)	00008120	PLN20030
	TTT(I) = TO	00008130	PLN20031
	WRITE(6,100) P,DDPT(I)	00008140	PLN20032
	CALL PSICO(P,FNZ,FNR,FNZ1,FNR1,I,NRY)	00008150	PLN20033
	IF(PRNT) PRINT 100,FNZ,FNR,FNZ1,FNR1	00008160	PLN20034
	PREZ = FNZ	00008170	PLN20035
	PIMZ = FNZ*(0.,-1.)	00008180	PLN20036

```

PRER      = FNR
PIMR      = FNR * (0.,-1.)
IF (PRNT) PRINT 100,PREZ,PIMZ,PRER,PIMR
F1        = 0.
G1        = 0.
SUM       = 0.
TUM       = 0.
IF(MJ.LE.3) GO TO 46
TNN       = TO-DP
CALL INTERP(TTT,PHIZ,M,TNN,Y)
F1        = Y
FF(1)     = Y
CALL INTERP(TTT,PHIR,M,TNN,Y)
G1        = Y
GG(1)     = Y
SUM       = SUM+2.*PIMZ*DSQRT(TO-TTT(NO))
TUM       = TUM+2.*PIMR*DSQRT(TO-TTT(NO))
IF (PRNT) PRINT 4, SUM
IF (PRNT) PRINT 7, TUM
7  FJRMAT(5X,'TUM=',G18.6)
4  FFORMAT(5X,'SUM=',G18.6)
DELL      = (TTT(NO)-TNN )/5.
TT(1)     = TNN
FF(6)     = PHIZ(NO)
GG(6)     = PHIR(NO)
PHIZ(I)   = PHIZ(NO)
PHIR(I)   = PHIR(NO)
DO 41 J=2,6
TT(J)     = TT(J-1) +DELL
CALL INTERP(TTT,PHIZ,M,TT(J),Y)
FF(J)     = Y
CALL INTERP(TTT,PHIR,M,TT(J),Y)
GG(J)=Y
TUM       = TUM+(GG(J-1)+GG(J))/2.*DELL
SUM=SUM+(FF(J-1)+FF(J))/2.*DELL
IF (PRNT) PRINT 7, TUM

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00008190 PLN20037
00008200 PLN20038
00008210 PLN20039
00008220 PLN20040
00008230 PLN20041
00008240 PLN20042
00008250 PLN20043
00008260 PLN20044
00008270 PLN20045
00008280 PLN20046
00008290 PLN20047
00008300 PLN20048
00008310 PLN20049
00008320 PLN20050
00008330 PLN20051
00008340 PLN20052
00008350 PLN20053
00008360 PLN20054
00008370 PLN20055
00008380 PLN20056
00008390 PLN20057
00008400 PLN20058
00008410 PLN20059
00008420 PLN20060
00008430 PLN20061
00008440 PLN20062
00008450 PLN20063
00008460 PLN20064
00008470 PLN20065
00008480 PLN20066
00008490 PLN20067
00008500 PLN20068
00008510 PLN20069
00008520 PLN20070
00008530 PLN20071
00008540 PLN20072

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	IF (PRNT) PRINT 4, SUM	00008550	PLN20073
41	CONTINUE	00008560	PLN20074
46	TPP = TTT(MO)	00008570	PLN20075
	TT(1) = TTT(MO)	00008580	PLN20076
	IF (TTT(MO)-TO.GT.DP) GO TO 43	00008590	PLN20077
	SUM=SUM+2.*PREZ*DSQRT(TTT(MO)-TO)	00008600	PLN20078
	TUM = TUM+2.*PRER*DSQRT(TTT(MO)-TO)	00008610	PLN20079
	IF (PRNT) PRINT 4, SUM	00008620	PLN20080
	IF (PRNT) PRINT 7, TUM	00008630	PLN20081
	CALL INTERP(TTT,PHIZ,M,TPP,Y)	00008640	PLN20082
	FF(1) = Y	00008650	PLN20083
	CALL INTERP(TTT,PHIR,M,TPP,Y)	00008660	PLN20084
	GG(1) = Y	00008670	PLN20085
	DELL = (TO+DP-TTT(MO))/5.	00008680	PLN20086
	DO 42 J=2,6	00008690	PLN20087
	IF (PRNT) PRINT 4, SUM	00008700	PLN20088
	TT(J) = TT(J-1) +DELL	00008710	PLN20089
	CALL INTERP(TTT,PHIZ,M,TT(J),Y)	00008720	PLN20090
	FF(J) = Y	00008730	PLN20091
	CALL INTERP(TTT,PHIR,M,TT(J),Y)	00008740	PLN20092
	GG(J) = Y	00008750	PLN20093
	TUM = TUM+(GG(J-1)+GG(J))/2.*DELL	00008760	PLN20094
	SUM = SUM+(FF(J-1)+FF(J))/2.*DELL	00008770	PLN20095
	IF (PRNT) PRINT 4, SUM	00008780	PLN20096
	IF (PRNT) PRINT 7, TUM	00008790	PLN20097
42	CONTINUE	00008800	PLN20098
	F3 = FF(6)	00008810	PLN20099
	G3 = GG(6)	00008820	PLN20100
	PHIZ(I) = (3.*SUM/DP-F1-F3)/4.	00008830	PLN20101
	PHIR(I) = (3.*TUM/DP-G1-G3)/4.	00008840	PLN20102
	GO TO 44	00008850	PLN20103
43	TTT(MO) = TO+DP	00008860	PLN20104
	PHIZ(MO) = PREZ/(DP*.5)	00008870	PLN20105
	PHIR(MO) = PRER/(DP*.5)	00008880	PLN20106
	F3 = PHIZ(MO)	00008890	PLN20107
	G3 = PHIR(MO)	00008900	PLN20108

	SUM	=	SUM+2.*PREZ*DSQRT(DP)	00008910	PLN20109
	TUM	=	TUM+2.*PRER*DSQRT(DP)	00008920	PLN20110
	PHIZ(I)	=	(3.*SUM/DP-F1-F3)/4.	00008930	PLN20111
	PHIR(I)	=	(3.*TUM/DP-G1-G3)/4.	00008940	PLN20112
	IF (PRNT)	PRINT	4, SUM	00008950	PLN20113
	IF (PRNT)	PRINT	7, TUM	00008960	PLN20114
44	CONTINUE			00008970	PLN20115
	PREZ1	=	FNZ1	00008980	PLN20116
	PIMZ1	=	FNZ1 * (0.,-1.)	00008990	PLN20117
	PRER1	=	FNR1	00009000	PLN20118
	PIMR1	=	FNR1 * (0.,-1.)	00009010	PLN20119
	IF (PRNT)	PRINT	100, PREZ1, PIMZ1, PRER1, PIMR1	00009020	PLN20120
	IF (MO.LE.3)	GO TO	47	00009030	PLN20121
	DO 81	J=2,NO		00009040	PLN20122
	AREA	=	(PR1(J)+PR1(J-1))*(TTT(J)-TTT(J-1))	00009050	PLN20123
	PHIR(J)	=	PHIR(J)+AREA/2.	00009060	PLN20124
	AREA	=	(PZ1(J)+PZ1(J-1))*(TTT(J)-TTT(J-1))	00009070	PLN20125
	PHIZ(J)	=	PHIZ(J)+AREA/2.	00009080	PLN20126
81	CONTINUE			00009090	PLN20127
	PHIZ(I)	=	PHIZ(I)+2.*PIMZ1*DSQRT(TTT(I)-TTT(NO))	00009100	PLN20128
	PHIR(I)	=	PHIR(I)+2.*PIMR1*DSQRT(TTT(I)-TTT(NO))	00009110	PLN20129
47	CONTINUE			00009120	PLN20130
	PHIZ(MO)	=	PHIZ(MO)+2.*PREZ1*DSQRT(TTT(MO)-TTT(I))	00009130	PLN20131
	PHIR(MO)	=	PHIR(MO)+2.*PRER1*DSQRT(TTT(MO)-TTT(I))	00009140	PLN20132
	JM	=	MO+1	00009150	PLN20133
	DO 82	J=JM,M		00009160	PLN20134
	AREA	=	(PR1(J)+PR1(J-1))*(TTT(J)-TTT(J-1))	00009170	PLN20135
	PHIR(J)	=	PHIR(J)+AREA/2.	00009180	PLN20136
	AREA	=	(PZ1(J)+PZ1(J-1))*(TTT(J)-TTT(J-1))	00009190	PLN20137
	PHIZ(J)	=	PHIZ(J)+AREA/2.	00009200	PLN20138
82	CONTINUE			00009210	PLN20139
	WRITE (6,111)	TTT(I),PHIZ(I),PHIR(I)		00009220	PLN20140
111	FORMAT	(2X, 'CRITICAL TIME',G20.8,5X, 'PHIZ',G20.8, 'PHIR',G20.8)		00009230	PLN20141
	RETURN			00009240	PLN20142
	END			00009250	PLN20143

```

SUBROUTINE PSICO (P, FNZ, FNR, FNZ1, FNR1, I, NRY)
C *****
C PSICO CALCULATES THE TWO TERMS IN BARKERS EXPANSION OF THE SOLUTION
C
C THE SUBPROGRAM REFFT , RECVR ARE CALLED
C
C CALL LIST: P, THE INTEGRATION PARAMETER, FNZ, THE FIRST TERM IN THE
C VERTICAL RESPONSE , FNR, SIMILAR FOR THE RADIAL, FNZ1, SECOND TERM IN
C VERTICAL RESPONSE, FNR1, SAME FOR RADIAL, I INDICATES WHICH VALUE OF P
C ALONG THE CONTOUR (STORAGE ARRAY INDEX ), NRY IS THE RAY NUMBER
C *****
      IMPLICIT REAL*8 (A-H, J-Z)
      COMMON/ RAYPAR/ KUD(100), KRSP(100), LTS(100), LTP(100), LREF(100, 4)
      COMMON/ DRSTF/ C(100), S(100), D(100), TH(100), X
      COMMON/ MAGIC/ PP(1200), DDPT(1200), TT(1200)
      COMMON/ PLOTG/ CON, NNF, NPT
      COMMON/ PLACE/ THIC, H, KSSP
      COMMON /LPRINT/ PRNT, PRNTS
      LOGICAL PRNT, PRNTS
      DIMENSION RF(16)
      COMPLEX*16 P, RF, DR, G1, G2, G3, FNZ, FNR, FNZ1, FNR1, RC, DDPT, PP, RDS, DZ
      ROD=D(2)/D(3)
      CALL REFFT(P, S(2), S(3), ROD, RDS)
      RF(2)=RDS
      CALL RECVR(S(2), P, KRSP(NRY), DZ, DR, KSSP, RSS)
      RF(1)=RSS
      RC=(1., 0.)
      DO 100 J=1, 2
      IF (LREF(NRY, J) .EQ. 0) GO TO 200
      RC = RC*RF(J)**LREF(NRY, J)
200 CONTINUE
100 CONTINUE
      IF(KSSP.EQ.1) GO TO 3
      IF(NRY.EQ.1) KRSP(NRY)=0
3 CONTINUE
      G1 = DDPT(I)*RC*CON

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00009260 PSIC0001
00009270 PSIC0002
00009280 PSIC0003
00009290 PSIC0004
00009300 PSIC0005
00009310 PSIC0006
00009320 PSIC0007
00009330 PSIC0008
00009340 PSIC0009
00009350 PSIC0010
00009360 PSIC0011
00009370 PSIC0012
00009380 PSIC0013
00009390 PSIC0014
00009400 PSIC0015
00009410 PSIC0016
00009420 PSIC0017
00009430 PSIC0018
00009440 PSIC0019
00009450 PSIC0020
00009460 PSIC0021
00009470 PSIC0022
00009480 PSIC0023
00009490 PSIC0024
00009500 PSIC0025
00009510 PSIC0026
00009520 PSIC0027
00009530 PSIC0028
00009540 PSIC0029
00009550 PSIC0030
00009560 PSIC0031
00009570 PSIC0032
00009580 PSIC0033
00009590 PSIC0034
00009600 PSIC0035
00009610 PSIC0036

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	G2	= G1*CDSQRT(P/(2.*X))	00009620	PSIC0037
	FNZ	= DZ*G2	00009630	PSIC0038
	FNR	= DR*G2	00009640	PSIC0039
	G3	= G1/(-8.*CDSQRT(2.*P*X**3))	00009650	PSIC0040
	FNZ1	= G3*DZ	00009660	PSIC0041
	FNR1	= G3*DR*(-3.)	00009670	PSIC0042
	IF (PRNT)	WRITE (6,300) P,C(3),C(2),S(3),S(2),KUD(NRY),KRSP(NRY),	00009680	PSIC0043
	1	LTS(NRY),LTP(NRY)	00009690	PSIC0044
	IF (PRNT)	WRITE(6,400) (RF(J),LREF(NRY,J),J=1,4)	00009700	PSIC0045
400	FORMAT (1X,' RECVR ',4(2(E13.4),I2))		00009710	PSIC0046
	IF (PRNT)	WRITE (6,500) G1,G2,G3,RC	00009720	PSIC0047
300	FORMAT (1X,'RECVR',2(E15.4),4(F10.3),2X,4(I2))		00009730	PSIC0048
500	FORMAT (1X,'RECVR',8(E13.4))		00009740	PSIC0049
	RETURN		00009750	PSIC0050
	END		00009760	PSIC0051

REAL FUNCTION PTIM*8 (P,K,NRY)	00009770 PTIM0001
IMPLICIT REAL*8 (A-H,O-Z)	00009780 PTIM0002
COMMON/PAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)	00009790 PTIM0003
COMMON/PLACE/THIC,H,KSSP	00009800 PTIM0004
COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00009810 PTIM0005
PSQ = P ** 2	00009820 PTIM0006
J = 2	00009830 PTIM0007
E = DSQRT(DABS(RCSQ(J)-PSQ))	00009840 PTIM0008
PTIM = (TH(4) + LTP(NRY)*TH(2)) *E	00009850 PTIM0009
E =DSQRT(DABS(RSSQ(J)-PSQ))	00009860 PTIM0010
PTIM = PTIM + (TH(3) + LTS(NRY)*TH(2))*E	00009870 PTIM0011
PTIM = P*X + PTIM	00009880 PTIM0012
RETURN	00009890 PTIM0013
END	00009900 PTIM0014

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SUBROUTINE RAYDEF
COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)
COMMON/PLACE/THIC,H,KSSP
COMMON /LPRINT/ PRNT,PRNTS
LOGICAL PRNT,PRNTS
REAL*8 THIC,H
WRITE (6,800)
800  FORMAT (10X,'WHOOPIE, WE MADE IT TO RAYDEF')
READ (5,400) THIC,H,KSSP
400  FORMAT (2F10.0,I10)
WRITE (6,700) THIC,H
700  FORMAT (/10X,'LAYER THICKNESS ',F6.3/10X,'SOURCE DEPTH',F6.3)
IF (KSSP .EQ. 0) WRITE (6,1300)
IF (KSSP .EQ. 1) WRITE (6,1400)
1300  FORMAT (15X,'SHEAR SOURCE')
1400  FORMAT (15X,'COMPRESSIONAL SOURCE')
READ(5,1200) (KUD(J),LTS(J),LTP(J),KRSP(J),J=19,64)
1200  FORMAT(4I2)
      KUD(1)=1
      KUD(2)=0
      KUD(3)=1
      KUD(4)=0
      KUD(5)=1
      KUD(6)=0
      KUD(7)=1
      KUD(8)=0
      KUD(9)=1
      KUD(10)=0
      KUD(11)=1
      KUD(12)=0
      KUD(13)=1
      KUD(14)=0
      KUD(15)=1
      KUD(16)=0
      KUD(17)=1
      KUD(18)=0

```

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00012310 RYDF0001
00012320 RYDF0002
00012330 RYDF0003
00012340 RYDF0004
00012350 RYDF0005
00012360 RYDF0006
00012370 RYDF0007
00012380 RYDF0008
00012390 RYDF0009
00012400 RYDF0010
00012410 RYDF0011
00012420 RYDF0012
00012430 RYDF0013
00012440 RYDF0014
00012450 RYDF0015
00012460 RYDF0016
00012470 RYDF0017
00012480 RYDF0018
00012490 RYDF0019
00012500 RYDF0020
00012510 RYDF0021
00012520 RYDF0022
00012530 RYDF0023
00012540 RYDF0024
00012550 RYDF0025
00012560 RYDF0026
00012570 RYDF0027
00012580 RYDF0028
00012590 RYDF0029
00012600 RYDF0030
00012610 RYDF0031
00012620 RYDF0032
00012630 RYDF0033
00012640 RYDF0034
00012650 RYDF0035
00012660 RYDF0036

```



LTS(1)=0  
LTS(2)=1  
LTS(3)=2  
LTS(4)=3  
LTS(5)=4  
LTS(6)=5  
LTS(7)=6  
LTS(8)=7  
LTS(9)=8  
LTS(10)=9  
LTS(11)=10  
LTS(12)=11  
LTS(13)=12  
LTS(14)=13  
LTS(15)=14  
LTS(16)=15  
LTS(17)=16  
LTS(18)=17  
LTP(1)=0  
LTP(2)=0  
LTP(3)=0  
LTP(4)=0  
LTP(5)=0  
LTP(6)=0  
LTP(7)=0  
LTP(8)=0  
LTP(9)=0  
LTP(10)=0  
LTP(11)=0  
LTP(12)=0  
LTP(13)=0  
LTP(14)=0  
LTP(15)=0  
LTP(16)=0  
LTP(17)=0  
LTP(18)=0

00012670 RYDF0037  
00012680 RYDF0038  
00012690 RYDF0039  
00012700 RYDF0040  
00012710 RYDF0041  
00012720 RYDF0042  
00012730 RYDF0043  
00012740 RYDF0044  
00012750 RYDF0045  
00012760 RYDF0046  
00012770 RYDF0047  
00012780 RYDF0048  
00012790 RYDF0049  
00012800 RYDF0050  
00012810 RYDF0051  
00012820 RYDF0052  
00012830 RYDF0053  
00012840 RYDF0054  
00012850 RYDF0055  
00012860 RYDF0056  
00012870 RYDF0057  
00012880 RYDF0058  
00012890 RYDF0059  
00012900 RYDF0060  
00012910 RYDF0061  
00012920 RYDF0062  
00012930 RYDF0063  
00012940 RYDF0064  
00012950 RYDF0065  
00012960 RYDF0066  
00012970 RYDF0067  
00012980 RYDF0068  
00012990 RYDF0069  
00013000 RYDF0070  
00013010 RYDF0071  
00013020 RYDF0072

```
KRSP(1)=0
KRSP(2)=0
KRSP(3)=0
KRSP(4)=0
KRSP(5)=0
KRSP(6)=0
KRSP(7)=0
KRSP(8)=0
KRSP(9)=0
KRSP(10)=0
KRSP(11)=0
KRSP(12)=0
KRSP(13)=0
KRSP(14)=0
KRSP(15)=0
KRSP(16)=0
KRSP(17)=0
KRSP(18)=0
KR=18
  DO 200 NR=1,KR
  DO 100 K=1,2
100 LREF(NR,K)=0
200 CONTINUE
C SH SOURCE
LREF(2,2)=1
LREF(3,1)=1
LREF(3,2)=1
LREF(4,1)=1
LREF(4,2)=2
LREF(5,1)=2
LREF(5,2)=2
LREF(6,1)=2
LREF(6,2)=3
LREF(7,1)=3
LREF(7,2)=3
LREF(8,1)=3
```

```
00013030 RYDF0073
00013040 RYDF0074
00013050 RYDF0075
00013060 RYDF0076
00013070 RYDF0077
00013080 RYDF0078
00013090 RYDF0079
00013100 RYDF0080
00013110 RYDF0081
00013120 RYDF0082
00013130 RYDF0083
00013140 RYDF0084
00013150 RYDF0085
00013160 RYDF0086
00013170 RYDF0087
00013180 RYDF0088
00013190 RYDF0089
00013200 RYDF0090
00013210 RYDF0091
00013220 RYDF0092
00013230 RYDF0093
00013240 RYDF0094
00013250 RYDF0095
00013260 RYDF0096
00013270 RYDF0097
00013280 RYDF0098
00013290 RYDF0099
00013300 RYDF0100
00013310 RYDF0101
00013320 RYDF0102
00013330 RYDF0103
00013340 RYDF0104
00013350 RYDF0105
00013360 RYDF0106
00013370 RYDF0107
00013380 RYDF0108
```

```

LREF(8,2)=4
  LREF(9,1)=4
  LREF(9,2)=4
LREF(10,1)=4
LREF(10,2)=5
LREF(11,1)=5
LREF(11,2)=5
LREF(12,1)=5
LREF(12,2)=6
LREF(13,1)=6
LREF(13,2)=6
LREF(14,1)=7
LREF(14,2)=6
LREF(15,1)=7
LREF(15,2)=7
LREF(16,1)=7
LREF(16,2)=8
LREF(17,1)=8
LREF(17,2)=8
LREF(18,1)=8
LREF(18,2)=9
READ(5,1000) IB,IE
1000 FORMAT(2I5)
READ(5,1100) ((LREF(II,JJ),JJ=1,2),II=IB,IE)
1100 FORMAT(2I2)
IF(PRNT) WRITE(6,600) ((LREF(J,L),L=1,2),J=1,6)
IF(PRNT) WRITE(6,600) ((LREF(J,L),L=1,2),J=7,12)
600  FORMAT(' R2 ',6(2I2,2X))
500  FORMAT(' RAYDEF ',4(12I2,2X))
      RETURN
      END

```

```

00013390 RYDF0109
00013400 RYDF0110
00013410 RYDF0111
00013420 RYDF0112
00013430 RYDF0113
00013440 RYDF0114
00013450 RYDF0115
00013460 RYDF0116
00013470 RYDF0117
00013480 RYDF0118
00013490 RYDF0119
00013500 RYDF0120
00013510 RYDF0121
00013520 RYDF0122
00013530 RYDF0123
00013540 RYDF0124
00013550 RYDF0125
00013560 RYDF0126
00013570 RYDF0127
00013580 RYDF0128
00013590 RYDF0129
00013600 RYDF0130
00013610 RYDF0131
00013620 RYDF0132
00013630 RYDF0133
00013640 RYDF0134
00013650 RYDF0135
00013660 RYDF0136
00013670 RYDF0137
00013680 RYDF0138
00013690 RYDF0139

```

```
C SUBROUTINE RECVR(B1,P,KR,DZ,DR,KSSP,RSS)
C   TO COMPUTE SURFACE RECEIVER AND REFLECTION FUNCTIONS
C SH AT THE RECVR
  IMPLICIT COMPLEX*16 (A-H,O-Z)
  REAL*8 B1,RSS
  DZ=-2./CDSQRT(1/B1**2-P*P)
  DR = DZ
  RSS=1.
  RETURN
  END
```

```
00013700 RCVR0001
00013710 RCVR0002
00013720 RCVR0003
00013730 RCVR0004
00013740 RCVR0005
00013750 RCVR0006
00013760 RCVR0007
00013770 RCVR0008
00013780 RCVR0009
00013790 RCVR0010
```

```

SUBROUTINE REFFT(P,B1,B2,D,RDS)
C *****
C REFFT CALCULATES THE REFLECTION FUNCTION FOR RAY INTERACTION WITH AN
C SOLID INTERFACE.NOTE THAT THIS SUBROUTINE IS WRITTEN ESPECIALLY FOR
C A SH SOURCE
C
C THE SUBPROGRAM CR IS CALLED. CR CALCULATES THE RADIAL  $\eta = \sqrt{1/$ 
C  $(\text{VELOCITY})^2 - P^2}$ 
C
C CALL LIST: P,THE INTEGRATION PARAMETER ,B1 IS VELOCITY IN THE LAYER,B2
C ,IS VELOCITY IN THE HALF-SPACE,D RATIO OF THEIR DENSITIES,RDR,THE
C REFLECTION FUNCTION FOR THE LOWER(SOLID-SOLID) INTERFACE
C
C IF THE SEVERAL KINDS OF SCURCES ARE INTEGRATED IN ONE PROGRAM THIS
C SUBROUTINE MUST BE GIVEN A DISTINCT NAME
C *****
      IMPLICIT COMPLEX*16 (A-H,O-Z)
      REAL*8 B1,B2,D,DS
      EA = CR(P,B1)
      EB = CR(P,B2)
      DS = D*B1**2/B2**2
      EC = DS*EA
      RDS = (EC-EB)/(EC+EB)
      RETURN
      END

```

```

00013800 REFT0001
00013810 REFT0002
00013820 REFT0003
00013830 REFT0004
00013840 REFT0005
00013850 REFT0006
00013860 REFT0007
00013870 REFT0008
00013880 REFT0009
00013890 REFT0010
00013900 REFT0011
00013910 REFT0012
00013920 REFT0013
00013930 REFT0014
00013940 REFT0015
00013950 REFT0016
00013960 REFT0017
00013970 REFT0018
00013980 REFT0019
00013990 REFT0020
00014000 REFT0021
00014010 REFT0022
00014020 REFT0023
00014030 REFT0024
00014040 REFT0025

```

```

SUBROUTINE SETUP(K,MM,NS,NO,MO,MPL0T,MPUNCH)                                00009910 STUP0001
C *****                                                                    00009920 STUP0002
C THE PROGRAM IS EXECUTED THROUGH THIS SUBROUTINE ,WHICH CALLS THE          00009930 STUP0003
C FOLLOWING SUBPROGRAMS DIRECTLY; RAYDEF,TS,HIGH,ADJUST,INTERP.PRINTED        00009940 STUP0004
C AND PUNCHED OUTPUT OF THE TIME SERIES OF SURFACE RESPONSE ARE PRODUCED     00009950 STUP0005
C HERE :THE VARIABLE LIST: K IS ALWAYS 1,MM IS APPARENTLY NO LONGER USED    00009960 STUP0006
C NS DESIGNATES THE FIRST RAY,NO, THE LAST RAY;MO=0 INDICATES THAT THIS     00009970 STUP0007
C IS THE FIRST TIME SETUP CALLED,IF NOT THE FIRST TIME USE ANY OTHER        00009980 STUP0008
C NUMBER .GT.1,MPL0T IS NOT USED,MPUNCH.LT.1 PRODUCES PUNCHED OUTPUT       00009990 STUP0009
C *****                                                                    00010000 STUP0010
      IMPLICIT REAL*8 (A-H,O-Z)                                             00010010 STUP0011
      COMMON/CONFIX/DEL,NN,NDP,TMX,XDIM,YDIM,DP,KO                          00010020 STUP0012
      COMMON/FOURCT/MF,NMF,KMF,KNMF                                         00010030 STUP0013
      COMMON/THZ/TT(1000),PPZ(1000),PPR(1000)                               00010040 STUP0014
      COMMON/EXACT/PHIZ(1000),PHIR(1000),TD(1000),NEND,NM                  00010050 STUP0015
      COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)       00010060 STUP0016
      COMMON/PLACE/THIC,H,KSSP                                              00010070 STUP0017
      COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC                               00010080 STUP0018
      DIMENSION PPC(800)                                                    00010090 STUP0019
      REAL*4 ZZX(890),ZZY(890),ZXDIM,ZYDIM                                  00010100 STUP0020
      LOGICAL PRNT,PRNTS,PRNTC                                              00010110 STUP0021
      IF(MO.EQ.0) CALL RAYDEF                                               00010120 STUP0022
C IF MO.EQ.0 CALL RAYDEF TO ESTABLISH RAY PARAMETERS (SEE PREVIOUS           00010130 STUP0023
C COMMENTS ON READ IN OF RAY PARAMETERS)                                    00010140 STUP0024
      NF = 1                                                                  00010150 STUP0025
      IF(MO.GT.1) GO TO 11                                                  00010160 STUP0026
C IF MO.NE.0 DO NOT INITIALIZED THE ARRAYS WHICH CONTAIN THE OUTPUT        00010170 STUP0027
      I = K                                                                    00010180 STUP0028
      TT(I) = TS(I)                                                          00010190 STUP0029
C TS IS A SUBPROGRAM WHICH ESTABLISHES THE TIME OF FIRST SIGNAL ARRIVAL     00010200 STUP0030
      PPZ(I) = 0.                                                            00010210 STUP0031
      PPR(I) = 0.                                                            00010220 STUP0032
C PPZ AND PPR WILL CONTAIN THE VERTICAL AND HORIZONTAL SURFACE RESPONSE,    00010230 STUP0033
C RESPECTIVELY                                                            00010240 STUP0034
C TT IS AN ARRAY OF SAMPLING TIMES FOR THE TIME SERIES                    00010250 STUP0035
      DO 10 J=2,NN                                                           00010260 STUP0036

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      TT(J)      = TT(J-1) +DEL
C NOTE THAT DEL = DP SET IN MAIN
      PPZ(J)     = 0.
      PPR(J)     = 0.
10    CONTINUE
11    CONTINUE
C ITERATE OVER THE RAYS FROM NS TO NO
      DO 32 N=NS,NO
      WRITE (6,103) N
103   FORMAT (5X,'RAY NUMBER',I3)
      CALL HIGH(NDP,TMX,K,KI,N)
C THE SUBPROGRAMME HIGH CALCULATES THE SURFACE RESPONSE FOR EACH RAY
      CALL ADJUST(NN,NFIX)
      N2        = 1
      M         = NM+1
      IF(NFIX.LT.1) GO TO 37
      N2        = NFIX+1
      N1        = NFIX-1
      IF(N1.LE.2) GO TO 42
      DO 31 J=1,N1
      CALL INTERP(TD,PHIZ,NEND,TT(J),Y)
      PPZ(J)    = PPZ(J)+Y*NF
      CALL INTERP(TD,PHIR,NEND,TT(J),Y)
      PPR(J)    = PPR(J)+Y*NF
31    CONTINUE
42    CONTINUE
      PPZ(NFIX)= PPZ(NFIX)+NF*PHIZ(M)
      PPR(NFIX)= PPR(NFIX)+NF*PHIR(M)
37    CONTINUE
      DO 33 J=N2,NN
      CALL INTERP(TD,PHIZ,NEND,TT(J),Y)
      PPZ(J)    = PPZ(J)+Y*NF
      CALL INTERP(TD,PHIR,NEND,TT(J),Y)
      PPR(J)    = PPR(J)+Y*NF
33    CONTINUE
      L=0

```

```

00010270 STUP0037
00010280 STUP0038
00010290 STUP0039
00010300 STUP0040
00010310 STUP0041
00010320 STUP0042
00010330 STUP0043
00010340 STUP0044
00010350 STUP0045
00010360 STUP0046
00010370 STUP0047
00010380 STUP0048
00010390 STUP0049
00010400 STUP0050
00010410 STUP0051
00010420 STUP0052
00010430 STUP0053
00010440 STUP0054
00010450 STUP0055
00010460 STUP0056
00010470 STUP0057
00010480 STUP0058
00010490 STUP0059
00010500 STUP0060
00010510 STUP0061
00010520 STUP0062
00010530 STUP0063
00010540 STUP0064
00010550 STUP0065
00010560 STUP0066
00010570 STUP0067
00010580 STUP0068
00010590 STUP0069
00010600 STUP0070
00010610 STUP0071
00010620 STUP0072

```

32	CONTINUE	00010630	STUP0073
7	IF(.NOT.PRNT) GO TO 12	00010640	STUP0074
	PRINT 13,(TD(J),PHIZ(J),PHIR(J),J=1,NN)	00010650	STUP0075
	PRINT 14,(TT(J),PPZ(J),PPR(J),J=1,NN)	00010660	STUP0076
13	FORMAT (1H0,15X,'TD',15X,'PH',/,3(E18.6))	00010670	STUP0077
14	FORMAT (1H0,15X,'TT',15X,'PP',/,3(E18.6))	00010680	STUP0078
12	CONTINUE	00010690	STUP0079
	NQ = NN/10	00010700	STUP0080
	NP = NQ + 1	00010710	STUP0081
	NR = NN + NQ	00010720	STUP0082
	DO 20 I = 1, NQ	00010730	STUP0083
	ZZX(I) = TT(I) - (NQ-I+1)*DP	00010740	STUP0084
20	ZZY(I) = 0.0	00010750	STUP0085
	NDIM=NN	00010760	STUP0086
	IER=0	00010770	STUP0087
	CALL DDGT3(TT,PPZ,PPC,NDIM,IER)	00010780	STUP0088
	DO 300 IZ = NP, NR	00010790	STUP0089
	ZZX(IZ)=TT(IZ-NP+1)	00010800	STUP0090
300	ZZY(IZ)=PPC(IZ-NP+1)	00010810	STUP0091
	WRITE(6,202)(ZZX(IZ),ZZY(IZ),IZ=1,NR)	00010820	STUP0092
202	FORMAT(' DEBUG 202 ',2E20.10)	00010830	STUP0093
1	CONTINUE	00010840	STUP0094
	IF(MPUNCH.LT.1) GO TO 2	00010850	STUP0095
	WRITE(7,200) TT(1),DP,NN	00010860	STUP0096
	WRITE(7,100) (PPC(J),J=1,NN)	00010870	STUP0097
2	CONTINUE	00010880	STUP0098
100	FORMAT (5E15.6)	00010890	STUP0099
200	FORMAT(2E15.6,I10)	00010900	STUP0100
	RETURN	00010910	STUP0101
	END	00010920	STUP0102



REAL FUNCTION SF2*8 (P,K,NRY,DP)	00010930 SF020001
IMPLICIT REAL*8 (A-H,O-Z)	00010940 SF020002
COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RCSQ(100),RSSQ(100)	00010950 SF020003
COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)	00010960 SF020004
PSQ = P ** 2	00010970 SF020005
J = 2	00010980 SF020006
ESQ =DABS (RCSQ(J)-PSQ)	00010990 SF020007
E =DSQRT(ESQ)	00011000 SF020008
TE = (TH(4)+TH(2)*LTP(NRY))*RCSQ(2)/(ESQ*E)	00011010 SF020009
ESQ =DABS (RSSQ(J)-PSQ)	00011020 SF020010
E =DSQRT(ESQ)	00011030 SF020011
TE = (TH(3) + TH(2)*LTS(NRY))*RSSQ(2)/(ESQ*E) + TE	00011040 SF020012
TE = TE*2.	00011050 SF020013
SR = 1.	00011060 SF020014
SF2 = SR/DSQRT(TE)	00011070 SF020015
RETURN	00011080 SF020016
END	00011090 SF020017

```

SUBROUTINE TIME2(PR,PI,DL,Q,DPT,T,KN,N,PL)
C *****
C FOR A PARTICULAR VALUE OF THE COMPLEX INTEGRATION PARAMETER P,TIME2
C FINDS A VALUE FOR THE COMPLEX PARAMETER TIME SUCH THAT THE IMAGINARY
C PART OF TIME IS MINIMIZED
C
C NO SUBPROGRAMS ARE CALLED
C
C CALL LIST:PR,THE SPECIFIED REAL PART OF P;PI,A GUESS AT THE IMAGINARY
C PART,DL,A SPECIFIED FRACTION OF PI USED AS AN ITERATION STEP,Q IS THE
C FINAL VALUE OF THE COMPLEX INTEGRATION PARAMETER P,DPT IS DP/DT FOR
C THIS VALUE,T IS THE COMPLEX INTEGRATION PARAMETER T FOR THIS VALUE OF
P,KN HAS NO APPARENT USE,N IS THE RAY NUMBER,AND PL IS A MINIMUM VALUE
C FOR PI
C *****
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)
COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET
COMMON/STUFF/C(100),S(100),D(100),TH(100),R
COMMON/PATHC/PO,TD,K
DIMENSION E(100)
COMPLEX*16 P,E,BL,T,PC,DPT,Q
DIMENSION Y1(100),Y4(100),X1(100),X4(100)
LOGICAL PRNT,PRNTS,PRNTC
NRY = N
X1M = 1.E+4
X4M = 0.0
NNN = 0
I = 0
6 P = PR*(1.,0.)+PI*(0.,1.)
T = P*R
J = 2
BL = 1./(C(J)**2)-P*P
E(J) = CDSQRT(BL)
T = T+E(J)*(TH(4)+TH(2)*LTP(NRY))
J = 3

```

```

00011100 TME20001
00011110 TME20002
00011120 TME20003
00011130 TME20004
00011140 TME20005
00011150 TME20006
00011160 TME20007
00011170 TME20008
00011180 TME20009
00011190 TME20010
00011200 TME20011
00011210 TME20012
00011220 TME20013
00011230 TME20014
00011240 TME20015
00011250 TME20016
00011260 TME20017
00011270 TME20018
00011280 TME20019
00011290 TME20020
00011300 TME20021
00011310 TME20022
00011320 TME20023
00011330 TME20024
00011340 TME20025
00011350 TME20026
00011360 TME20027
00011370 TME20028
00011380 TME20029
00011390 TME20030
00011400 TME20031
00011410 TME20032
00011420 TME20033
00011430 TME20034
00011440 TME20035
00011450 TME20036

```

```

BL      = 1./ (S(2)**2)-P*P
E(J)   = CDSQRT(BL)
T      = T+E(J)*(TH(3)+TH(2)*LTS(NRY))
IF (PRNTC) WRITE(6,110) P,E(2),T
IF (PRNTC) WRITE(6,111) E(3),I,NNN
111  FORMAT('0E(3)=',2G18.6,' I=',I5,' NNN=',I5)
TI     = T*(0.,-1.)
IF (DABS(TI) .LE. DET) GO TO 2
IF (I.GT.90) GO TO 2
I      = I+1
X1(I)  = 100.
X4(I)  = 0.0
IF (TI.GT.0.) Y1(I)=TI
IF (TI.GT.0.) X1(I)=PI
IF (TI.LT.0.) Y4(I)=TI
IF (TI.LT.0.) X4(I)=PI
IF (I.EQ.1) GO TO 43
IF (NNN.GT.1) GO TO 44
IF (TI*TL .LE.0.) GO TO 44
43    IF (TI.GT.0.) PI=PI-DL
      IF (TI.LE.0.) PI=PI+DL
      IF (PI.LE.1.E-5) PI=PK/2.
      NNN      = 1
      PK      = PI
      TL      = TI
      GO TO 6
44    DO 52 J=1, I
      IF (X1(J).GT.X1M) GO TO 53
      X1M     = X1(J)
      NJ     = J
53    IF (X4(J).LE.X4M) GO TO 54
      X4M     = X4(J)
      MJ     = J
54    CONTINUE
52    CONTINUE
Y1M   = Y1(NJ)

```

```

00011460 TME20037
00011470 TME20038
00011480 TME20039
00011490 TME20040
00011500 TME20041
00011510 TME20042
00011520 TME20043
00011530 TME20044
00011540 TME20045
00011550 TME20046
00011560 TME20047
00011570 TME20048
00011580 TME20049
00011590 TME20050
00011600 TME20051
00011610 TME20052
00011620 TME20053
00011630 TME20054
00011640 TME20055
00011650 TME20056
00011660 TME20057
00011670 TME20058
00011680 TME20059
00011690 TME20060
00011700 TME20061
00011710 TME20062
00011720 TME20063
00011730 TME20064
00011740 TME20065
00011750 TME20066
00011760 TME20067
00011770 TME20068
00011780 TME20069
00011790 TME20070
00011800 TME20071
00011810 TME20072

```

Y4M	= Y4(MJ)	00011820	TME20073
DPI	= (X1M-X4M)/(Y1M-Y4M)	00011830	TME20074
DPM	= Y1M*DPI	00011840	TME20075
PI	= X1M-DPM	00011850	TME20076
NNN	= 2	00011860	TME20077
	IF(PI.LE.PIL) PI=PIL	00011870	TME20078
	GO TO 6	00011880	TME20079
2	CONTINUE	00011890	TME20080
	BL = 0.	00011900	TME20081
	BL = BL-(TH(4)+TH(2)*LTP(NRY))/E(2)	00011910	TME20082
	BL = BL-TH(2)*LTS(NRY)/E(3)-TH(3)/E(3)	00011920	TME20083
	BL = R+P*BL	00011930	TME20084
	Q = P	00011940	TME20085
	DPT = 1./BL	00011950	TME20086
	IF(PRNTC) WRITE(6,110) P,E(2),T,DPT	00011960	TME20087
110	FORMAT(1H0,4X,'P= ',2G18.6/5X,'E(1) =',2G17.6/5X,'T= ',2G18.6/	00011970	TME20088
1	5X,'DPT= ',2G18.6)	00011980	TME20089
	RETURN	00011990	TME20090
	END	00012000	TME20091

	REAL FUNCTION TS*8 (K)	00012010	TS010001
	IMPLICIT REAL*8 (A-H,O-Z)	00012020	TS010002
	COMMON/PLACE/THIC,H,KSSP	00012030	TS010003
	COMMON/RAYPAR/KUD(100),KRSP(100),LTS(100),LTP(100),LREF(100,4)	00012040	TS010004
	COMMON/DRSTF/CC(100),SS(100),DD(100),TTH(100),XX	00012050	TS010005
	COMMON/STUFF/C(100),S(100),D(100),TH(100),X,RC SQ(100),RSSQ(100)	00012060	TS010006
	DIMENSION T(200)	00012070	TS010007
	COMMON/LPRINT/PRNT,PRNTS,KST,KEND,PRNTC,NDC,DET	00012080	TS010008
	LOGICAL PRNT,PRNTS,PRNTC	00012090	TS010009
	DO 10 N=1,2	00012100	TS010010
	DEL = 1./SS(2)	00012110	TS010011
	IF(KSSP.EQ.0) GO TO 81	00012120	TS010012
	IF(LTS(N).GT.0) GO TO 81	00012130	TS010013
	DEL = 1./CC(2)	00012140	TS010014
81	P = -1.E-9	00012150	TS010015
	DAT = 1.E+12	00012160	TS010016
	CALL FIND2(P,M,DEL,DAT,PO,TO,N)	00012170	TS010017
	P=1/SS(N+1)	00012180	TS010018
	TTP = TO	00012190	TS010019
	IF(PO.LE.P) GO TO 6	00012200	TS010020
	CALL HELP(K,N,P,TTP,DTP,N)	00012210	TS010021
6	T(N) = DMIN1(TO,TTP)	00012220	TS010022
10	CONTINUE	00012230	TS010023
	TS = DMIN1(T(1),T(2))	00012240	TS010024
	N = 2	00012250	TS010025
	IF (PRNT)WRITE (6,1) (T(J),J=1,N)	00012260	TS010026
1	FORMAT (5X,'T 1,2,3',3(E18.6))	00012270	TS010027
100	FORMAT(I10,2E18.6)	00012280	TS010028
	RETURN	00012290	TS010029
	END	00012300	TS010030

```

C *****
C
C B. GORDON AND C.M. NAUTIYAL
C
C MAY 12, 1972
C
C THIS PROGRAM GENERATES CALCOMP PLOTS OF THE OF TERRY BARKER'S
C PROGRAM MODELING THE RESPONSE OF AN ELASTIC LAYER OVER AN ELASTIC
C HALF-SPACE AS CONVOLVED WITH A SPECIFIED SOURCE FUNCTION.
C
C THREE PLOTS ARE PRODUCED,THE UNCONVOLVED OUTPUT,THE CONVOLVED OUTPUT,
C AND THE SOURCE FUNCTION, ALL PLOTS ARE IN SAME SCALE IN TIME.
C
C THE SUBROUTINE CONVLV IS USED.
C
C THE SOURCE FUNCTION, SRC, A LINEAR ARRAY, IS SPECIFIED IN A DATA
C STATEMENT
C
C XDIM, YDIM SPECIFY THE SIZE OF THE OUTPUT
C
C DELTA IS HALF WIDTH OF THE SOURCE ASSUMED SYMMETRIC
C NOTE THAT THE BEGINNING OF THE OUTPUT IS PADDED WITH ZEROS TO 10%
C OF ITS LENGTH
C *****
C REAL*8 P, SRC, PC
C DIMENSION P(1000), SRC(1000), PC(2000), PPLCT(1000), TPLCT(1000)
C DIMENSION XL(2), YL(4), YM(4)
C DIMENSION SRCP(1000)
C DIMENSION PPL(1000)
C DATA XL/'TIME', ' SEC' /
C DATA YL/'CONV', 'OLVE', 'D OU', 'TPUT' /
C DATA YM/'UNCO', 'NVOL', 'V OU', 'TPUT' /
C SPECIFY SOURCE FUNCTION
C DATA SRC/0., 2.5, 5., 2.5, 0., 995*0. /
C SPECIFY PROGRAM PARAMETERS
C XDIM=6.

```

```

MAIN0001
MAIN0002
MAIN0003
MAIN0004
MAIN0005
MAIN0006
MAIN0007
MAIN0008
MAIN0009
MAIN0010
MAIN0011
MAIN0012
MAIN0013
MAIN0014
MAIN0015
MAIN0016
MAIN0017
MAIN0018
MAIN0019
MAIN0020
MAIN0021
MAIN0022
MAIN0023
MAIN0024
MAIN0025
MAIN0026
MAIN0027
MAIN0028
MAIN0029
MAIN0030
MAIN0031
MAIN0032
MAIN0033
MAIN0034
MAIN0035
MAIN0036

```

```

YDIM=2.
DELTA=.4
C READ IN PUNCHED DATA
  READ(5,100) TT,DP,NN
  PRINT 200, TT, DP, NN
  200 FORMAT(' TT=',G15.6,' DP=',G15.6,' NN=',I10)
  READ(5,101)(P(I),I=1,NN)
  100 FORMAT(2E15.6,I10)
  101 FORMAT(5E15.6)
  102 FORMAT(3(I10,G15.6))
C PERFORM CONVOLUTION WITH SOURCE FUNCTION
  NS = 2*DELTA/DP +1.5
  CALL CONVLV(NN,P,NS, SRC, PC)
C PAD RECORD WITH ZEROES
  NQ = NN/10
  NA = NQ + 1
  NB = NN + NQ
  DO 15 I = 1, NQ
  SRCP(I) = 0.0
  TPLT(I) = TT-(NQ-I+1)*DP
  PPL(I) = 0.0
  15 PPLT(I) = 0.0
  DO 16 I = NA,NB
  SRCP(I) = SRC(I-NA+1)
  TPLT(I) = TT + (I-NA)*DP
  PPL(I) = P(I-NA+1)
  16 PPLT(I) = PC(I-NA+1)
C LIST OUTPUT
  PRINT 201
  201 FORMAT('OUTPUT AFTER CONVOLUTION-BEFORE CONV-SOURCE FUNC'//)
  PRINT 202,(TPLT(I),PPLT(I),PPL(I),SRCP(I),I=1,NB)
  202 FORMAT(4G15.6)
C PLOT ON CALCOMP
  CALL NEWPLT('M8800','6894','WHITE ','BLACK')
  CALL PICTUR(XDIM,YDIM,XL,8,YM,16,TPLT,PPL ,NB,0.,0)
  CALL PICTUR(XDIM,YDIM,XL,8,YL,16,TPLT,PPLT,NB,0.,0)

```

```

MAIN0037
MAIN0038
MAIN0039
MAIN0040
MAIN0041
MAIN0042
MAIN0043
MAIN0044
MAIN0045
MAIN0046
MAIN0047
MAIN0048
MAIN0049
MAIN0050
MAIN0051
MAIN0052
MAIN0053
MAIN0054
MAIN0055
MAIN0056
MAIN0057
MAIN0058
MAIN0059
MAIN0060
MAIN0061
MAIN0062
MAIN0063
MAIN0064
MAIN0065
MAIN0066
MAIN0067
MAIN0068
MAIN0069
MAIN0070
MAIN0071
MAIN0072

```

```
DO 17 I = 1, NB
17 TPLOT(I) = TPLOT(I) - TT
CALL PICTUR(XDIM,YDIM,XL,8,'SOURCE FUNCTION ',16,TPLOT,SRCP,NB,0.,
1 0)
CALL ENDPLT
CALL EXIT
STOP
END
```

```
MAIN0073
MAIN0074
MAIN0075
MAIN0076
MAIN0077
MAIN0078
MAIN0079
MAIN0080
```



C	SUBROUTINE CONVLV(LX,XX,LY,YY,CC)	00000020 CONV0001
C		00000030 CONV0002
C	TITLE - CONVLV = CONVOLVE	00000040 CONV0003
C	COMPLETE CONVOLUTION OF TWO TRANSIENTS	00000050 CONV0004
C		00000060 CONV0005
C		00000070 CONV0006
C	--- <td>00000080 CONV0007</td>	00000080 CONV0007
C		00000090 CONV0008
C	CONVLV CONVOLVES TWO TRANSIENTS, X(I) I=0,1,...,LX-1	00000100 CONV0009
C	AND Y(I) I=0,1,...,LY-1 , TO PRODUCE THE COMPLETE	00000110 CONV0010
C	CONVOLUTION FUNCTION	00000120 CONV0011
C		00000130 CONV0012
C		00000140 CONV0013
C	LX-1	00000150 CONV0014
C	C(I) = SUM ( X(J)*Y(I-J) )	00000160 CONV0015
C	J=0	00000170 CONV0016
C		00000180 CONV0017
C	FOR I = 0,1,...,LX+LY-2	00000190 CONV0018
C	WHERE	00000200 CONV0019
C	LX AND LY ARE INPUT PARAMETERS	00000210 CONV0020
C	Y(K) IS ASSUMED = 0.0 FOR K OUTSIDE OF	00000220 CONV0021
C	THE RANGE 0 TO LY-1	00000230 CONV0022
C	NOTE THAT THE CONVOLUTION IS INDEPENDENT OF THE ORDER	00000240 CONV0023
C	OF THE INPUTS X AND Y.	00000250 CONV0024
C		00000260 CONV0025
C	TECHNIQUE USED IS AN ALGORITHM BASED ON ANALOGY TO	00000270 CONV0026
C	MULTIPLICATION OF POLYNOMIALS	00000280 CONV0027
C		00000290 CONV0028
C		00000300 CONV0029
C		00000310 CONV0030
C	LANGUAGE - FORTRAN IV	00000320 CONV0031
C	EQUIPMENT - NO SPECIAL REQUIREMENTS	00000330 CONV0032
C	STORAGE -	00000340 CONV0033
C	AUTHOR - J.F. CLAERBOUT. TRANSLATED FROM FORTRAN II TO FORTRAN	00000350 CONV0034
C	BY R.A. WIGGINS, 6/65	00000360 CONV0035
C		00000370 CONV0036

C	LIBRARY ROUTINES REQUIRED - NONE	00000380	CONV0037
C		00000390	CONV0038
C		00000400	CONV0039
C	-----USAGE-----	00000410	CONV0040
C		00000420	CONV0041
C	SAMPLE CALL	00000430	CONV0042
C	CALL CONV LV(LX,XX,LY,YY,CC)	00000440	CONV0043
C		00000450	CONV0044
C	INPUTS	00000460	CONV0045
C		00000470	CONV0046
C	LX IS NO. OF TERMS IN X VECTOR	00000480	CONV0047
C		00000490	CONV0048
C	XX(I) I=1,...,LX CONTAINS X(0),...,X(LX-1) RESPECTIVELY	00000500	CONV0049
C		00000510	CONV0050
C	LY IS NO. OF TERMS IN Y VECTOR	00000520	CONV0051
C	MUST EXCEED ZERO (PROGRAM EXITS IF ZERO OR LESS)	00000530	CONV0052
C		00000540	CONV0053
C	YY(I) I=1...LY CONTAINS Y(0),...,Y(LY-1) RESPECTIVELY	00000550	CONV0054
C	EQUIVALENCE (XX,YY) IS PERMITTED	00000560	CONV0055
C		00000570	CONV0056
C	OUTPUTS	00000580	CONV0057
C		00000590	CONV0058
C	CC(I) I=1,...,LX+LY-1 CONTAINS C(0),...,C(LX+LY-2) RESPECTIVELY	00000600	CONV0059
C	WHERE C(I) IS GIVEN IN ABSTRACT	00000610	CONV0060
C	EQUIVALENCE (XX,CC) ALLOWED IF XX NOT EQUIVALENT TO YY.	00000620	CONV0061
C		00000630	CONV0062
C	EXAMPLES	00000640	CONV0063
C		00000650	CONV0064
C	1. SHOWING REVERSIBILITY OF X AND Y	00000660	CONV0065
C	INPUTS - LX = 3 XX(1...3) = 1.,2.,3.	00000670	CONV0066
C	LY = 2 YY(1...2) = 10.,1.	00000680	CONV0067
C		00000690	CONV0068
C	USAGE - CALL CONV LV(LX,XX,LY,YY,CC1)	00000700	CONV0069
C	CALL CONV LV(LY,YY,LX,XX,CC2)	00000710	CONV0070
C	OUTPUTS - CC1(1...4) = CC2(1...4) = 10.,21.,32.,3.	00000720	CONV0071
C		00000730	CONV0072

C 2. ILLEGAL INPUT CASES (NO OUTPUT)	00000740 CONV0073
C    INPUTS - SAME AS EXAMPLE 1. EXCEPT START WITH OUTPUT VECTORS	00000750 CONV0074
C            CLEANED, I.E. CC1(1...4) = CC2(1...4) = 0.,0.,0.,0.	00000760 CONV0075
C    USAGE -        CALL CCNVLV(-2,XX,LY,YY,CC1)	00000770 CONV0076
C                    CALL CCNVLV(LX,XX,0,YY,CC2)	00000780 CONV0077
C    OUTPUTS - CC1(1...4) = 0.,0.,0.,0.    (ILLEGAL LX)	00000790 CONV0078
C                    CC2(1...4) = 0.,0.,0.,0.    (ILLEGAL LY)	00000800 CONV0079
C	00000810 CONV0080
C PROGRAM FOLLOWS BELOW	00000820 CONV0081
C	00000830 CONV0082
C	00000840 CONV0083
C        SUBROUTINE CCNVLV(LX,XX,LY,YY,CC)	00000850 CONV0084
C        IMPLICIT REAL*8 (A-H,O-Z)	CONV0085
C	00000860 CONV0086
C DUMMY DIMENSION STATEMENTS	00000870 CONV0087
C        DIMENSION XX(2),YY(2),CC(2)	00000880 CONV0088
C CHECK LEGALITIES	00000890 CONV0089
C        IF (LX.LE.0) GO TO 9999	00000900 CONV0090
C        IF (LY.LE.0) GO TO 9999	00000910 CONV0091
C CLEAR PORTION OF OUTPUT AREA	00000920 CONV0092
C        LC        = LX+LY-1	00000930 CONV0093
C        IB        = LX+1	00000940 CONV0094
C        DO 10 I=IB,LC	00000950 CONV0095
10    CC(I)        = 0.	00000960 CONV0096
C	00000970 CONV0097
C DO CONVOLUTION	00000980 CONV0098
C	00000990 CONV0099
C        IX        = LX	00001000 CONV0100
C        DO 30 I=1,LX	00001010 CONV0101
C        X        = XX(IX)	00001020 CONV0102
C        CC(IX)    = 0.	00001030 CONV0103
C        DO 20 J=1,LY	00001040 CONV0104
C        K        = IX+J	00001050 CONV0105
C        CC(K-1)   = CC(K-1)+X*YY(J)	00001060 CONV0106
20    CONTINUE	00001070 CONV0107
30    IX        = IX-1	00001080 CONV0108

C  
C EXIT  
C  
9999 RETURN  
END

00001090 CONV0109  
00001100 CONV0110  
00001110 CONV0111  
00001120 CONV0112  
00001130 CONV0113