## CARBONYL TRANSPORT OF METAL

## IN METEORITE PARENT BODIES

### **by**

## MARK **JOSEPH LUPO**

## **S.B.,** Massachusetts Institute of Technology **(1979)**

## SUBMITTED TO THE DEPARTMENT OF EARTH **AND** PLANETARY **SCIENCES IN** PARTIAL **FULFULLMENT** OF THE **REQUIREMENTS** FOR THE DEGREE OF

## MASTER OF **SCIENCE**

## at the

## **MASSACHUSETTS** INSTITUTE OF **TECHNOLOGY**

### June **1981**

Massachusetts Institute of Technology **1981**



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Submitted to the Department of Earth and Planetary Sciences on **May 8, <sup>1981</sup>**in partial fulfillment of the requi rements for the Degree of Master of Science in Earth and Plantary Science

### ABSTRACT

**A** new model for the formation of iron meteorites has been tested thermodynamically and has been found possible within the confines of our present knowledge of the kinetics of the breakdown of carbonyls. The model entails the production of carbonyl s in parent body asteroids from the interaction of metals and **CO.** The gaseous carbonyls flow upward and condense in the low temperature upper meters of the asteroid. When the **CO** gas has diffused away, the carbonyls, which maintain a vapor pressure with a large liquid sink, begin to slowly deposit the metals and release **CO.** Metal is deposited at low temperature, which unlike the igneous model, is consistent with the occurence of chondritic matter and silicate fragments with sharp edges that have been found in iron meteorites. Three sizes of hypothetical spherical asteroids were modeled with two different compositions.

Thesis Supervisor: Dr. John Simpson Lewis

Title: Professor of Geochemistry and Planetary Science **'**

# Carbonyl Transport of Metal in Meteorite Parent Bodies

## Introduction

The presently accepted model for the formation of most iron meteorites is a high temperature process involving the downward transport of liquid metal by gravity in a parent body of at least 50 km in radius. The differentiated body is later disrupted, and pieces of the core or shell become the iron meteorites. Studies of the Fe-Ni phase diagram and the cooling of metal from high temperatures have given a satisfactory explanation of the observed crystal structure of certain iron meteorites, such as type II A, B (Goldstein and Ogilvie, 1965; Wood, 1964)

Not all iron meteorites, however, are compatible with tnis igneous process. Chronaritic matter and crystals of lawrencite (FeCl<sub>2</sub>) enveloped in the iron phase, and silicate fragments with sharp broken corners are inconsistent with the high temperatures necessary to melt iron. In particular, the group I AB irons are very rich in silicate inclusions (Wasson, 1974), sometimes up to 15% by weight, as in Woodbine (Mason, 1967). This led Bloch and Müller (1971) to propose a low temperature model: carbonyls in comets decompose to form metals and CO gas during a perihelion passage enveloping silicates and iron chlorides at temperatures of 100°C rather than at iron's melting point. This model also has difficulties. The disseminating material of the comet is hydrous;

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water readily attacks iron pentacarbonyl to produce magnetite, hydrogen and carbon monoxide. It also reacts with iron to produce iron oxides and hydrogen. Further, it is doubtful that the time of perihelion passage is long enough to sublimate enough of the comet to produce significant amounts of iron. In the deposition of iron, nucleation sites are important and these seem to be lacking in space. Although strings of "swaddling kamacite" were obtained in the lab (Bloch and Wirth, **1980)** when an **Fe(CO) <sup>5</sup>-** Ni(CO) 4 gas mixture at **180 0C** was passed between the poles of a permanent magnet, the absence of water vapor makes this experiment less than realistic for a cometary enviornment. The rate of deposition of iron is retarded severely **by** low carbonyl pressures so that even at **1800C** and **1** dyne cm-2 pressure, the rate of deposition is **10~4 g** day~1 per square centimeter of metal.

It can easily be shown that carbonyl transport was not important in the solar nebula. The pressure **-** temperature profile was assumed to be an adiabat

$$
\left(\frac{P}{P_0}\right) = \left(\frac{T}{T}\right)^{C} P(T) / R \tag{1}
$$

where T and P were taken to be the pressure and temperature at **1AU,** 600K and **10~4** bars respectively (Lewis, **1972).** R is the gas constant and **Cp(T)** is the heat capacity of a mixture of **90%** H2 and **10%** He, which is a weak function of temperature. The **CO** pressure, fixed **by** cosmic abundances, is one thousandth the total pressure everywhere in this range in

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temperature. Then, since

$$
Fe + 5CO = Fe(C0)5, \t(2)
$$

we obtain

$$
P_{Fe(C0)5}
$$
 =  $K_{eq}(P_{C0})^{5}a_{Fe}$  (3)

where  $a_{F_{\mathbf{a}}}$  is the activity of iron, which approaches 0.94 by 600K and  $K_{eq}$  is the equilibrium constant of the reaction here. Using data from the **JANAF** table supplement **(1978),** we see that

$$
\log K_{eq} = \frac{8961.5}{T} - 29.177 . \qquad (4)
$$

We assume, fo llowing Lewis and Prinn **(1 980),** that most of the carbon in the solar nebula at all temperatures and pressures was **CO.** Fiqu re 1 demonstrates that the carbonyl pressure **is** so far below that of **CO** as to be insign ificant. This argument should n ot only lay to rest the id ea of iron transport **by** carbonyls in the nebula, but of the accretion of carbonyl into comets. Even with an increase in **CO** abundan ce, it woul be hard to im agine bare elemental iron available to react with **CO** in a cometary environment.

In this paper, the upward transpor t **of** iron and nickel **by** carbonyls in asteroid parent bodies will be investigated. Carbon monoxide is released from the center of a young asteroid. kinetics and thermodynamics, carbonyls form. The gas continues to rise. At a- higher leve **1,** the carbonyl dissociates and t flows past the level of the most favorable

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iron and nickle are deposited. An impact or any other disruption liberates iron-rich chunks, or even metal chunks into space and these fall to earth as meteorites.

#### Assumptions

Two compositions will be modeled, ordinary chondritic (H) and **C3** carbonaceous chondritic. The H group was chosen to represent the ordinary chrondi te **s,** and the C3's were chosen since other carbonaceous chrondites have a prohibitively high water content and lack metal, making iron transport impossible. These compositions bracket the ordinary chondr i tes. H group ordinary chondrites have a'mean iron weight pe rc ent of **27.61** (Mason, **1971)** and a mean nickel weight pe rc ent of **1.63** (Mason, **1965).** About half the iron is metal abou t half **is** in **Fe0 (as silicates) and** in **FeS.** We will use a 13 wt. percent metallic iron abundance. The median value for the concentration of carbon in ordina<mark>ry chon</mark>. drites is **1 000** ppm (Moore and Lewis, **1965, 1967;** Otting and **7 Y- i n** *o* o **-I , It** Tho wt er **A** h ind %ne **is S O,%** by mes o average (Ka **plan, 1971;** Boato, **1954)** and its source is presumably amphib oles, which have never been observed in meteorites, but are suspected on theoretical grounds to reside in the matrice **s** at these **1 ow** abundan ces. Type **3** carbonaceous chondrites are, on the average, 25.15 wt. <mark>%</mark> iron (Mason 1971) almost all of which is found in olivine and clinopyroxene as FeO. For this w ork **,** it wi **<sup>11</sup>**be assumed that the **C3** parent body is 4.02% ir on metal **b y** mass, as in Warrenton, an Ornans group chondrite (CO3). Since the nickel, which is 1.43 wt. **%** (Wiik, **1956)** is mostly found as metal, the metal phase is **26%** nickel and 74% iron. The carbon abundance is **0.19%** (Wiik, **1956)** and H20 is set at **0.1%** (Wiik, **1956).**

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Two surface temperatures have been modeled, **175K** and 150K. An object at the inner edge of the belt (2.3AU) with an albedo of **0.17** would have a surface temperature of **175K.** At the outer edge of the main belt **(3.3AU)** a body with an **al**bedo of **0.07** would have a temperature of 150K.

**A** central temperature of 1500K was chosen so that there would be a substantial core of material above the Fe-FeO-FeS eutectic melt temperature, which is 1200K. The source of heat is to be short-lived radio-active nuclides, such as **<sup>2</sup> 6A1 ,** for the purpose of generating the **CO** gas for the production of carbonyls. It would not be expected that temperatures much exceeded this value since convection in the liquid phase would tend to flatten the temperature gradient, and cool the asteroid interior.

As for the body above the level of incipient melting, conduction is assumed to oe tne mecnanism of neat transport, so the steady state temperature profile is

$$
T(z) = \frac{sp}{3K} \left( \frac{1}{2} z^2 \right) + T_c \tag{5}
$$

T<sub>c</sub> is the central temperature, s is the heat production rate in erg **g~1** sec~1, p is the density of the material, (taken as **4g** cm- <sup>3</sup>for the ordinary chondritic body and **3.5** for the **C3),** and K is the thermal conductivity, which is  $m = 4 \times 10^5$  erg K<sup>-1</sup> sec<sup>-1</sup> cm<sup>-1</sup>. The heat production is chosen to give the proper surface temperature at the surface of the body and a central temperature (z **= 0)** of 1500K. Clearly s must be larger for

$$
-8-
$$

small bodies and for bodies with carbonaceous composition. To maintain the temperature profile for a 30km body with a **175K** surface temperature and an ordinary chondritic composition, s **= 8.83** x **10-5** erg **g~** sec~1, a value more than three orders of magnitude greater t han the modern value (Kaula, **1968, p 111),** but nonetheless easily attainable **by** the decay **of 26A1** alone if only 10ppm o **f** the **26Mg** observed in chon- drites today is radiogenic.

Three different size bod ies, have been modeled for each surface temperature and compo sition, a 10km, a 30km and a 100km radius body. The bodie s were assumed to be spherical and incompressible, with all of the constituents initially homogeneously distributed.

The lithostatic pressure at any level is given **by**

$$
P_{1\, \text{ith}} = \frac{2}{3} G \rho^2 \pi (R^2 - z^2)
$$
 (6)

where P<sub>lith</sub> is in dynes cm<sup>-2</sup>, G is the gravitational constant, R is the total radius of the body (cm), and z is the distance from the center. The gas pressure in our models cannot exceed the lithostatic pressure at any level. The central pressure of the 100km body with an ordinary chondritic composition is **223.5** bars. Given that the crushing strength of ordinary chondrites is often kilobars (Wasson 1974) the assumption of a constant density in the parent bodies is quite satisfactory.

Metal will be found in grains having a radius of 0.lym

$$
-9-
$$

to 100um. The grains are assumed to be spheres, with a homogenous mixture of iron, nickel and traces of other metals. The H-group metal grains are 94% iron, **6%** nickel. The **C3** group parent body is assumed to have taenite grains that are 74% iron, and **26%** nickel, as in the Warrenton chondrite.

 $\bullet$ 

 $\sim 100$  km s  $^{-1}$ 

 $\sim 10^7$ 

 $\mathcal{L}_{\mathcal{A}}$  and  $\mathcal{L}_{\mathcal{A}}$  are the set of the set of the set of the set of the  $\mathcal{L}_{\mathcal{A}}$ 

 $\sim$ 

 $\Delta$ 

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## Gas production

The three most important elements to consider in determining the gas composition are hydrogen, carbon and oxygen because of their abundance. The water in the parent bodies would be from water bearing silicates, such as tremolite. Below is a reaction which should account for much of the water in an ordinary chondrite:

$$
Mg_2SiO_4 + Ca_2Mg_5Si_8O_{22}(OH)_2 = 5MgSiO_3 + 2CaMgSi_2O_6 + H_2O (7)
$$
  
the transformation of tremolite to diopside at high tempera-  
ture. Using available thermodynamic data (Robie, et al.,  
1979) we find that

$$
\log K_{eq} = -\frac{5820.8}{T} + 7.580
$$
 (8)

If the activities of the minerals are unity, tnen the pressure of water at 1200K would be **536** bars, swamping the **CO** pressure. But this equilibrium could never be achieved since H20 is only 1000ppm in our parent body. In a cubic centimeter ( $p=4$  g  $cm^{-3}$ , pore volume =  $0.15$   $cm^{3}$ ), there are only 2.22 **x** 10~4 moles of water. Even if all of it were liberated into the gas at 1200K, the pressure would only be 148 bars. (At 900K, P<sub>H<sub>2</sub>0 = 111 bars; equilibrium would be possible). Even</sub> **so,** 148 bars is substantial as shall be shown below. To obtain the hydrogen to water ratio, the reaction

$$
Fe + H20 = Fe0 + H2
$$
 (9)

$$
-11-
$$

is studied. It has **AGO** of **-3367** cal mole-1 at 1200K **(JANAF, 1971),** that is, an equilibrium constant of 4.103.

$$
K = \frac{a_{Fe0} P_{H_2}}{a_{Fe} P_{H_2 0}}
$$
 (10)

At the Fe-FeO boundary  $a_{Fe}$   $m = 10a_{Fe0}$ , so  $X_{H_20}/X_{H_2} = 0.0259$ . Invoking mass balance and the limit to moles of H<sub>2</sub>,  $P_{H_2}$  = 144.3 and  $P_{H_2,0}$  = 3.7 bars. It is assumed that the carbon bearing gas in the asteroids was released at the Fe-FeO-FeS ternary eutectic temperature, 1200K, since the iron must melt and permit the carbon in it to contact the gas. This **high** temperature is not a necessary condition for the release of H2 and **H20** however.

To obtain the carbon monoxide pressure, the reaction

$$
C_{\text{gr}} + Fe0 = Fe + C0 \qquad (11)
$$

is considered. The **JANAF** tables ( **1971)** give the equilibrium constant at 1200K, **10.359.**

$$
K = \frac{a_{Fe} P_{CO}}{a_{Fe0} a_{qr}}
$$
 (12)

The activities of iron and FeO are 0.94 and **0.1** respectively in an H chondri te. **A** mole fraction of **0.06** of nickel in the iron nickel all oy and a carbon concentration of 1000ppm lead to an activity of **0.0623** for graphite (Lewis, Barshay and Noyes, **1979).** The **CO** pressure is therefore **0.0687** bars. The same procedure is used with the reaction

$$
-12-
$$

$$
C_{ar} + 2Fe0 = 2Fe + CO_2
$$
, (13)

which has an equilibrium constant of **2.068** at 1200K, to get the CO<sub>2</sub> pressure of 0.00146. The CO/CO<sub>2</sub> ratio is then 47.09. Turning these pressures into mole fractions , the composition of the gas is **0.05% CO,** 10ppm **CO2 , 2.50% H20** and **97.45%** H2.

**A** gas with the above composition would not transport metal. The CO would be rapidly converted to CH<sub>4</sub> via the reacti on

$$
CO + 3H2 = CH4 + H2O . (14)
$$

 $X_{CH_A}/X_{CO}$  would be 461 at 1200K and it increases as temperature decreases. Secondly, water destroys iron pentacarbonyl.

$$
3Fe(C0)5 + 4H20 = Fe304 + 4H2 + 15C0 , \t(15)
$$

although the hydrogen abundance may restrict the loss of carbonyls. The presence of water does not destroy the metallic iron since  $H_2$ 0 is only one thousandth of the mass and iron metal is fully one eighth. Nonetheless, this gas is definitely hostile to the transport model proposed.

However, outgassing experiments with meteorites and terrestrial rocks show that  $H_2$  and  $H_20$  will be outgassed at temperatures significantly below 1200K. Shepard **(1938)** experimented with two obsidians. The first outgassed **7%** of its water in **3** months at **<sup>400</sup> 0C (673K),** the second **70%** of its water in one hour at 300<sup>°</sup>C (573K). As powder, at 573K, the first lost **10%** of its water in **30** minutes **(30%** after **9** hours) and the second lost **70% (87%** after **9** hours). Emmons (1964) ob-

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tained his gas from greenstone within 24 hours at only 473K and obtained water from biotite, granite and diorite at **773K** in **3** hours. MacKenzie and Milne **(1953)** obtained the greatest moisture loss from **373K** to **673K.** At **773K** much hydrogen was also liberated. Boato (1954) worked with carbonaceous chondrites and found that already at 453K anywhere from **17%** to 47% of the water was released, and, nearly all of it was out **by 1073K,** but the water he got at T **<** 180K was terrestrial water that had been adsorbed **by** t he meteorite (he checked this **by** measuring the D/H ratio).

Clearly H2 and **H20** outgassed before temperatures reached the Fe-FeO-FeS ternary eutectic. Diffusion of  ${\sf H_2}$  and  ${\sf H_2O_2}$ however, is also much faster than that of **CO** or of a carbonyl. To answer the question of whether or not these gases were totally gone **by** the time **CO** bega n to stream upward is a complex macter invoiving Cne time it took for tne central temperature to rise, the time it took **for** these gases to form, the average particle size i n th e asteriod and the porosity of the asteroid. For an ave rage internal temperature of 500K, and a pore radius o f **0.** 5um, the diffusivity of hydrogen is **7.7** cm2 sec~1 , and 94 % **of** it would be lost in **1000** years. The diffusivity of w ater is **2.6** cm2 sec **1** and i n **1000** years **72%** of it would be gon But in an asteroid only 10km in radius, lithostatic pressures range from **0** to 2.2 **bars.** This means that only **1.3** x **10-5** to **1.7** x **10-5** moles o **f** gas c an be in the gas phase at a time, per cubic centimeter. **If 10 -5** of it is hydrogen, and H2 **+** H2 0 is 1000ppm, **(0.004 g**

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cm<sup>-3</sup>), then only one percent of the gas could be in the gas phase at a time. **E** ven **if it** takes thou sands of **y** ears for these gases to come out, t he half life **of <sup>2</sup> 6A1** is 740,000 years. Tens of tho usands **of** years coul **d** ellapse between the time that 600K was attained and when the ternary eutectio temperature was reached. It will be assumed here that hydrogen and water were no long er present **by** the time **CO** began to outgas. Small quan tities of resid ual hydrogen will turn some of our precious **CO** into **CHg,** which is innocuous. Traces of **H20** will not damage the carbonyls since at the leveils carbonyls are abundant, water is beginning to condense and it probably would have reacted with an Fe to produce FeO and  $\text{H}_\text{2}$ before reaching suc h a level.

For an asteroid of C3 composition, the metal phase is clearly taen ite. From a compositi on of carbon of **1900** ppm and a nickel activity of **0.26,** we get an activity of **0.29 for** graphite (Le wis, Barshay and Noyes **1979)** . The activity of iron is 0.74. The activity of FeO is obtained from

$$
Fe + 1/2 \t02 = Fe0 \t(16)
$$

(Mueller, **1965). AGO** <sup>0</sup>-46.474 at 1200K (JANAF, **1971).** Since type **3** carbonaceous chondrites (which used to be called olivine-pigeonite chondrites) have their iron in olivine and pyroxene, and since some metal is present (though not much), the oxygen fugacity is. chosen to be on the FeO-Fe boundary *,* 10<sup>-17</sup>. This leads to a value of a<sub>Fe0</sub> of 0.80. Using the method above, P<sub>CO</sub> = 3.248 bars. P<sub>CO =</sub> 0.701 bars. The War-**CO** 3248bars **CO2**

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renton chondrite has a water content of **1000** ppm so the total of the H<sub>2</sub>0 and H<sub>2</sub> pressures will be similar to above. PH<sub>2</sub><sup>/P</sup>H<sub>2</sub>0 = 3.795, but the total pressure due to these gases cannot exceed 129.33 bars ( $p = 3.5$  g  $cm^{-3}$ ). If a different **C3** had been chosen, its water content could have been 2% and

nearly the full **<sup>563</sup>**bars of this gas would be possible. The

gas composition for our Warrenton parent body is  $X_{C,0} = 2.4\%$ ,  $X_{C0_2}$  = 0.5%,  $X_{H_20}$  = 20.2%,  $X_{H_2}$  = 76.9% and for a more water rich C3, it could well have been  $X_{\text{CO}} = 0.1\%$ ,  $X_{\text{CO}} = 271$  ppm, 2  $X_{H_{20}}$  = 20.8%,  $X_{H_{2}}$  = 79.0%. We will assume here that the hy**d** rogen and water escaped before the **CO** gas began to be released.

## Time factor

In the ordinary chondritic parent bodies **,** under the above assumptions, the gas is **97.9% CO** and 2.1% **CO2.** It has a pressure of **0.070** bars until lithostatic pressure drops to **0.070** bars (at r **=** 9.84 km in a 10km asteroid). It is of interest to determine the rate of flow of this gas, and also to determine the length of time that outgassing would be occuri **ng.**

In the ten kilomter asteroid, the average flow rate can be deduced from the equations for Knudsen diffusion since throughout the asteroid, the mean free path of the **CO** molecules exceeds the tube diameter. The velocity of a gas in a packed column in free molecular flow is given **by**

 $\ddot{\cdot}$ 

$$
v = \frac{\Phi}{\rho} = D \frac{dx}{dz}
$$
 (17)

where  $\Phi$  is the flux, pis the mass density, D is the Knudsen diffusivity of the gas and dx/dz is the gas concentration gradient.

$$
D = \frac{2}{3} \nabla r
$$
 (18)

where **7** is the average speed of the gas and r is the diameter of the pore. Since

$$
\rho = \frac{NM}{V} = \frac{MP}{RT}
$$
 (19)

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where V is volume, **N** is the number of molecules and M is the molecular weight, and since

$$
D = 9700 \, r \sqrt{T/M} \tag{20}
$$

and

$$
\Phi = \frac{D}{L} \frac{\Delta P}{RT}
$$
 (21)

the convenient relationship

$$
v = 9700 \text{ r} \sqrt{T M^{-3}} \frac{\Delta P}{LP}
$$
 (22)

is obtained, with L defined as the length over which the pressure changes **by** AP and P being the average pressure over that length. The velocity of the gas was found to be 3.4 x  $10^{-7}$  cm sec $^{-1}$  in the region where the temperature was between **1000 -** 1200K. It increased as a function of radius and is 1.9 x 10<sup>-6</sup> cm sec<sup>-1</sup> at the 300K level. The velocity at the surface  $(T=175K)$  is 4.4 x  $10^{-5}$  cm sec<sup>-1</sup>. Integrating the velocity over position, we see that it took **29,000** years for a parcel of gas at the 1200K level (z **=** 4.76 km) to reach the surface.

To answer the second question of how long outgassing occured, there are two aspects to be dealt with: the supply of the volatile and the cooling rate of the asteroid. If the asteroid has a carbon concentration of **1000** ppm (wt) then a cubic centimeter will contain  $(\rho=4)$  0.004 grams or 1.4 x 10<sup>-4</sup>

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moles. The ideal gas law is used, with P **= 0.0687** bars, V = **0.15 cm3** (the pore space) and T **=** 1200K. We see that the amount of carbon removed **by** having that **CO** gas flow upwards is equivalent to 0.3 ppm. It is the same if the CO<sub>2</sub> gas is included. With the carbon concentration down the activity **of** graphite falls a little, so does pressure of CO<sub>2</sub> and CO and the next drop is less severe. **If** the core is defined as the region in the asteriod where the temperature is over the eutectic melt tmperature of the Fe-FeO-FeS system, the core of the 10km asteroid contains  $4.5 \times 10^{17}$  cm<sup>3</sup>, each with  $10^{-7}$ moles of **CO** gas. To fill the whole pore volume of the asteroid according to the above pressure scheme, the number of moles of **CO** gas necessary is **7.8** x **1011** moles, so that each co're cubic centimeter must discharge its gas seventeen times to fill the asteroid. Each time the gas flows out of a cube's pores it is repiaced by a gas whose pressure is slightly lower. Each seventeen outflows constitutes an "iteration" of a gas, that **is,** a period of **29,000** years for the gas to completely come out and be replaced. Since the gas in a cube can replace itself several thousand times, and since seventeen of these is an iteration, there is enough carbon in the asteroid for 430 iterations with the pressure over **0.006** bars, and **860** iterations over **0.0006** bars.

Having shown that there is enough volatile component to have outgassing several millions of years, the question of cooling becomes important. If the heat capacity is taken as  $10^7$  erg gm<sup>-1</sup> deg<sup>-1</sup>, the temperature gradient discussed above

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implies a heat content of **1.18** x **1029** ergs. After the asteroid cooled, the heat content would be **2.93** x **1028** ergs **(it** would be **175K** to the center), so 8.88 x **1028** ergs must be dissipated.

It was implied earlier that in a **10** km asteroid,

$$
T(r) = 1500 - 13.25 r2
$$
 (23)

where r is in kilometers. With some differential equation solving, the actual equation as a function of time, is

$$
T(r,t) = 175 + (1325 - 13.25 r^2) e^{-\alpha^2 b^2 t}
$$
 (24)

where 175K is the steady state term,  $\alpha^2 = K/C_p\rho = 1.0 \times 10^{-2}$ .  $cm^2$  sec<sup>-1</sup> and  $b^2 = 7.5/R^2$  where R is 10 km (10<sup>6</sup> cm). It can **be** shown that once cooling has begun, after **108,000** years, no part of this asteroid is at 1200K and that after 422,000 **years** he wiole excess ihea content has **dropped by a** factOr of e. Therefore,.these models can go through at least two iterations, with just over **100,000** years for the process of cooling take place. See table **I.**

In the **30** km asteroid, the flow rate can be determined from equations for continuum diffusion, since only the uppermost **570** meters had the mean free path of the gas molecules exceeding the tube diameter. There, the flow is modeled as it was above, **by** Knudsen diffusion. To get the velocity of the gas we use the Blake-Kozeny equation

$$
\mathbf{v} = \frac{\Delta P}{L} \cdot \frac{D_p^2}{150\mu} \frac{\epsilon^3}{(1-\epsilon)^2}
$$
 (25)

where D<sub>n</sub> is the diameter of a particle, which was taken to be two microns;  $\mu$  is the viscosity which was assumed to be 10<sup>-</sup> poise, and **E** is the porosity, which was taken as 0.15 (Was son, 1974, p176). The results of the repeated use of this formula are in table I. It would take a parcel of gas at 14.27 km (T **=** 1200 K) 413,764 year to get to the surface the as teroid. Sin ce the cores's pore volume can contain 1.2 **x** 1012 moles of **CO** gas and 1.54 x **1013** moles are needed to fill t he pore volu me with the above pressure gradient, the pores in the core must produce gas **13** times to fill the asteroid and itself with the correct amount of **CO** gas. This will b e called one iteration, and it will last 414,000 years. Si nce it will take this asteroid at least **3.08** x **1013** sec **976 ,00 0** years to c ooi to the point that gas production will be impossible, the re is time for at least two iterations. **CO** gas **would** be large ty gone **by** tne time **1.5** x **10"** years nave ellapsed. It will **,** however take **3.80** million years for the excess heat to be dissipated **by** a factor of e.

In the case o **f** the **100** km asteroid, the gas can be treated as a conti nuum all the way through. Its velocity is shown in table I. The time it takes **for** a parcel of a gas to travel from the "c ore" to the surface is 420,208 years. To fill the asteroid with gas would require the pores in the "core" to empty themselves **13.6** times. This would be an "iteration **."l** Sinc e gas production could go on for **10,800,000** years after cooling began (before no place in the asteroid

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was melted) **26** iterations could occur and the pores would have to replenish themselves **350** times. It is clear that, near the end, the **CO** and **CO2** pressures would be down **by** a factor of **1.1.** After 42,250,000 years, the excess heat of **8.88** x **1031** ergs will be reduced **by** a factor of e, and the steady state solution will not be isothermal, but long lived radioactive nucl ides will hold the central temperature no less than eight degrees above the average surface temperature!

Perhaps **5** x **107** years may ellapse between the time the steady state temperature gradient is established and the time cooling begins. For **C3** chondrites, the pore gas pressure drops **by** an order **of** magnitude after 240 refillings, or every **<sup>25</sup>**iterations. The carbon concentration would be only **19** ppm after 2 x **107** years in the slowest (100km) asteroid, leaving piency of time **for** aeposiLion. In tne **30** ana IUO Kin oruinary chondrites, however, 430 iterations or **1.7** x **108** years are needed to reduce the carbon content of the "core" **by** an order of magnitude. If after **5** x **107** years cooling has set in to the point that no part of the core is melted, then **<sup>600</sup>**ppm carbon remain in the core and all of the deposition results must be multiplied **by** 0.4 and the deposition will occur at a somewhat greater depth.

It is of note that the time in seconds given in table I is a time limit for equilibration in each "zone" of the asteroid. As the subject of kinetics is addressed, table I should be consulted to judge whether or not a reaction went

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to completion. Reaction rates are usually given in gramshr<sup>-1</sup> cm<sup>-2</sup>. Given that in each cubic centimeter of material there is about **0.5** grams of metal upo n whi ch to nucleate or react, an **d** given our chosen grain rad **ius o f** one micron, the re are **1.5** x **1010** grains or **1875** cm2 **of** metal surface per cm3 **of** material. Further, there are **3600** se conds per hour, so a rule of t humb is that these numbers c an be divided **by** 2 anc they woul **d** be in convenient units of **g** sec **-1 (cm3 of** material)<sup>-1</sup>. For the C3 body, there are 0.2 grams of meta per cm<sup>3</sup> of material, so the "rule of thumb" would be to divide by **si X.**

The rates of formation of carbonyls and deposition of metals are **highly** pressure-de pendent. Five (or four for  $\texttt{Ni(C0)}_{\texttt{4}}$ ) moles of gas are reacting to form one mole of gas Iron pentacarbonyl and nickel carbonyl are both ideal gases so this reaction brings in a significant loss of volume

Kim, et al. (1973) prepared iron tailings which were **53.96%** iron **by** weight, and 26.54% meta **<sup>11</sup>**ic iron. The iron grains were of the size 44 um. Rhee, e t al **(1973)** took the material and exposed it to CO gas after first having reduced the iron. They found that 394 K was t he o ptimum temperature for forming iron pentacarbonyl and tha t th e reaction went **35%** to completion in only two hours, when the **CO** pressure was 21 atm. As temperature increased, the ca rbon **yl** was inclined to decompose and deposit the metal. As t empe rature decreased, the carbonyl was more stable but the r eact ion rate was reduced. At **366** K however, it was still quite rapid. Based

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a scanty set of data points, Rhee et al. were so bold as to propose the following formula for computing the rate:

$$
r_{s} = \frac{K_{s} a_{Fe}}{(RT)^{5}} \left(\frac{RT}{P_{CO}}\right)^{n} (P_{CO}^{5} - P_{Fe(C0)_{5}}/K_{e})
$$
 (26)

where K<sub>s</sub> is the reaction rate constant and K<sub>e</sub> is the equilibrium constant, and r<sub>e</sub> is the rate per unit area free iron surface. The variable n is t he number of **CO** molecules adsorbed on non-reacting iron sites and involved in forming an **Fe(CO) 5** molecule. They fou nd n to be a bout **3.** Thus, holding all else constant, the rate increases as T<sup>-2</sup>

Simil<mark>arly, the rate of Ni(CO)<sub>4</sub> formation decreases with</mark> an incre ase in temperature (Sykes and Townshend, **1955).** The carbonyl is more stable at lower temperatures. At 409 K, **0.06** gra ms of nickel were c onverted per hour. At **323** K, **1.60** g hr<sup>-1</sup> were converted. It should be pointed out, howeve that the equilibrium values demand less conversion at 409 K than at **323** K and the autho rs felt that equilibrium was m ost quickly achieved at temperatures of 398 to 409 K. Data below room temperature do not exist, but given the enormous lengths of time available on the asteroid and the laboratory time scale of the reaction even down to room temperature, it w ill be assumed here that the carbonyl forming reaction will attain equilibrium even at temperatures as **1** ow as **225** K.

At sufficiently low pressures, the de position reaction, that is, the breakdown of the carbonyl and the deposition of metals, will still proceed at a laboratory pace at room tem-

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perature. The actual quantitative expression for the rate of decomposition and deposition of iron pentacarbonyl is

$$
r = \frac{c_1 c_2 \exp(-E_0/RT) \exp(E_a/RT) (P_a - P_{C0}^5/K_{eq})}{(1 + c_2 \exp(E_a/RT) \times P_a + c_3 \exp(E_r/RT) P_{C0})^{1.8}}
$$
(27)

Where c<sub>1</sub>, c<sub>2</sub>, and c<sub>3</sub> are known constants, E<sub>a</sub>, E<sub>o</sub> and E<sub>r</sub> are known energies, P<sub>a</sub> is the carbonyl pressure in Torrs and r is the rate of deposition in g hr<sup>-1</sup> cm<sup>-2</sup> free iron surface (Carl ton and Oxley, 1965). K<sub>ed</sub> here is the equilibrium constant of deposition, and is given **by**

$$
K_{eq} = 3.34x10^{11} exp(24850/T + 16.06 log T - 1.76x10^{-3}T - 3.032x10^{5}/T^{2})
$$
 (28)

If the temperature were  $300$  K, with  $P_a = 29$  Torr and  $P_{C0}$  $= 285$  Torr, r =  $9.09 \times 10^{-16}$  g hr<sup>-1</sup> cm<sup>-2</sup>, or 1.6x10<sup>-3</sup> grams per **100,000** years given the iron content and **1** pm grain size. On the other hand, if all the  $CO$  gas were gone,  $r = 1.28x$   $10^{-6}$  g hr<sup>-1</sup> cm<sup>-2</sup> or 1.4 g year<sup>-1</sup> at room temperature.

Clearly, the rate is dependent on free iron surface area available for deposition. Chemical kinetics is the limiting factor in deposition below 473 K. The rate limiting step is the decomposition of adsorbed iron carbonyl on the deposition surface and the activation energy of the decomposition reaction is about 20 Kcal **g~1** mole~1 (Carlton and Oxley, **1965).**

Nickel carbonyl deposition and nickel deposition is handled in Carlton and Oxley **(1967).** It is described **by** a similar equation

$$
r = \frac{c_1 c_2^2 \exp(-E_0/RT) \exp(2E_a/RT) (P_a^2 - P_{C0}^3/K_d^2)}{(1 + c_2 \exp(E_a/RT) \times P_a + c_3 \exp(E_r/RT) \times P_{C0})^2}
$$
(29)

where  $P_a$  is now the nickel carbonyl pressure in Torrs,

$$
K_{d} = \exp(64.2 - 10500/T). \qquad (30)
$$

This reaction rate is also dependent upon area of iron grains. It deposits upon nickel, iron of stainless steel. The rate of nickel deposition is generally orders of magnitude faster than iron at similar temperature pressure and CO pressure. If the CO pressure is low enough, nickel will be deposited at 273 K on a convenient laboratory time scale. But the reaction is strongly inhibited by carbon monoxide pressure (Garratt and Thompson, 1934a). Extrapolating to a temperature of 225 K, given a nickel carbonyl pressure of 5 Torr (the vapor pressure) and a CO pressure of 0.1 Torr, we see that  $r = 2.36 \times 10^{-11}$  g hr<sup>-1</sup> cm<sup>-2</sup>, so that even at these extreme conditions a gram of nickel could still be deposited in a cubic centimeter in less than 3000 years. If P<sub>CO</sub> is zero it deposits at twice the rate.

It should be pointed out that if the asteroid (in particular the 30 km and 100 km H type) cooled before it could use up its carbon, there is still plenty of time to deposit the metals before the whole asteroid cools to the point where kinetics prevent the decomposition of carbonyls and the deposition of metals.

Having determined the composition of the gas that will

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be flowing upwards in the asteroids, having disposed of harmful H<sub>2</sub>0, having established that the reactions forming carbonyls are not kinetically inhibited, having addressed the flow rates of gas and the kinetic deposition and having established that at bare minimum several iterations can occur in each asteroid, the actual transport of iron can be investigated.

### The Results

**A** computer program was run to depict the equilibrium conditions in each of the twelve parent bodies described above. Figures **2-7** show the equilibrium gas pressure for each of the gases CO; Fe(CO)<sub>5</sub> and Ni(CO)<sub>4</sub> and lithostatic pressure all as a function of temperature which is a function of depth. Presented here are the **10** km, **30** km and **100** km asteroids both of **C3** and H composition **,** but only at **175** K. The six asteroids whose surface temperature was **150** K so resembled their counterparts of **175** K that to treat them here would be redundant.

In the carbonaceous asteroids **,** the **CO** pressure is 3.248 bars until the lithostatic pressure drops to below **3.949 bars.** Below this, the **CO** pressure is maintained at **82.2%** of the lithostatic pressure. In the ordinary chondritic asteroid, the **CO** pressure would be **0.0687** bars until the lithostatic pressure dropped to **0.070** and would be maintained below this at **97.9%** lithostatic pressure. The iron pentacarbonyl pressure was determined **by** the following relationship

$$
P_{Fe(C0)5}
$$
 = K<sub>eq</sub> a<sub>Fe</sub> (P<sub>CO</sub>)<sup>5</sup> (31)

and the nickel carbonyl pressure **by**

$$
P_{Ni(C0)4} = K_{eq} a_{Ni} (P_{C0})4.
$$
 (32)

For the nickel reaction,

$$
\log K_{\text{eq}} = 8.148.3/T - 20.550 \tag{33}
$$

**(JANAF, 1971, 1978).** Mass balance was invoked so that the total pressure of these two carbonyl s and of **CO** would not exceed lithostatic pressure. It was found that nickel carbonyl was five orders of magnitude more abundant than iron pentacarbonyl, simply based upon equilibrium considerations and the assumption that nickel is readily available as is iron. But that assumption is not realistic. Nickel is not found in independent grains, but in iron nickel alloy. In ca'rbonaceous chondrites, where the iron is taenite, only **26%** of the metal atoms on the surface of a grain are nickel. Once the nickel is used up, no new nickel carbonyl molecules can form until the iron atoms on that layer react with **C0** to form iron pentacarbonyl , thus exposing new nickel atoms to the gas. In an iron nickel alloy, the diffusivity of nickel is given as

 $D = 2.11 \exp(-73 + 2.0 \text{ Kcal} \text{ mol} \text{e}^{-1}/RT)$  (34)

for an alloy that is **5.79%** nickel (McEwan , et al., **1959),** and **by**

 $D = 0.497 \text{ exp}(-66.40 + 1.52 \text{ Kcal mole}^{-1}/RT)$  (35)

for an alloy that is **9.21%** nickel (Hancock and Leak, **1967).** For the first alloy, typical of the kamacite found in ordinary chondrites, the diffusivity of nickel at 400 K is **10'40**  $cm^2$  sec<sup>-1</sup>. For the other alloy,  $D = 10^{-37}$  cm<sup>2</sup> sec<sup>-1</sup>. Given 40 million years  $(1.3x10^{15} \text{ sec})$  a nickel atom in the first alloy would be expected to move  $3.6 \times 10^{-13}$  cm and  $1.1 \times 10^{-11}$  cm

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in the other (interatomic spacing is on the order of  $10^{-8}$ cm). In a spherical grain one micron in radius, the amount of nickel diffused would be 3.38x10-6% given **317** million years in the first alloy, and  $1.07x10^{-4}$ % in the second. Carbonyls were most abundant at temperatures colder than 400 K. Clearly **,** the number **of** moles **of** nickel carbonyl that could form is constrained **by** diffusion of nickel in iron-nickel alloys to be **26%** of the total number of moles of carbonyl gas. This would be **6%** in the ordinary chondritic case. Mass balance for the gas is worked out in the following way. **All** three gases, CO, Fe(CO)<sub>5</sub> and Ni(CO)<sub>4</sub> are ideal, so

$$
P_{i}V = n_{i}RT, \qquad (36)
$$

where  $\mathsf{n}_{\mathbf{i}}$  is the number of moles of the particular gas. It has been shown that, in the ordinary chondrite case,

$$
n_{\rm Ni} = 6n_{\rm Fe}/94 \tag{37}
$$

The subscript Ni will stand for  $Ni(C0)<sub>4</sub>$  and Fe for Fe(CO)<sub>5</sub>, and T for total. Mass balance is given as

$$
n_{T} = n_{C0} + 5n_{Fe} + 4n_{Ni}
$$
 (38)

where  $n_{\sf T}$  is the total number of moles of CO available and  $n_{\sf CC}$ is the number that remain as CO gas. Since

$$
P_{Fe(C0)}_{5}
$$
 =  $a_{Fe} K_{eq} (P_{CO})^{5}$  (39)

and

$$
n_{Fe} = P_{Fe(C0)}V/RT, \qquad (40)
$$

we substitute **37** into **38,** then 40 into **38,** and yield

$$
n_{T} = n_{C0} + 5 \frac{P_{Fe(C0)}_{5}V}{RT} + 4 \frac{6}{94} \frac{P_{Fe(C0)}_{5}V}{RT}
$$
 (41)

The values of  $n_{\text{T}}$  and  $n_{\text{CO}}$  are given by 36 and V/RT is cancelled out to give

$$
P_T = P_{C0} + B a_{Fe} K_{eq} (P_{C0})^5
$$
 (42)

where B **= 5.255** for an ordinary chondritic composition and 6.405 for the **C3** composition.

The above equation is val id only unti **1** iron pentacarbonyl begins to condense. The carbonyl fo rms a liquid at less than **350** K, and its exact temperature of condensation is a function of pressure. Its pressure is h enceforth given **by**the vapor pressure equation

$$
\log P = -\frac{1966}{1} + 5.212 \tag{43}
$$

where P is pressure in bars. At this point, equilibrium must be re-established **by** equation **39** and much **CO** is converted to Fe(CO)<sub>s</sub>, which would condense. Of course, at the same time,  $\overline{\texttt{Ni}}(\texttt{CO})_{\texttt{A}}$  is being produced, but its pressure can increase. Eventually its vapor pressure is reached and  $\texttt{Ni(C0)}_{\texttt{4}}$  liquid begins to form. Its vapor pressure is given **by**

$$
\log P = -\frac{1517.7}{T} + 4.809
$$
 (44)

until the temperature drops to the freezing point, 248K. Then

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$$
\log P = -\frac{2078}{T} + 7.060 \tag{45}
$$

(Ander son, **1930).** After many iterations, much liquid carbonyl will build up. It was shown above that there was plenty **of** tim e before cooling in the **100** km H asteroid to deposit **most o f** the carbonyl that could be made even if cooling began before the completion of **CO** outgassing. That cooling would set in at this time is **by** no means necessary. In the smaller astero ids many iterations could occur before cooling began. There are 14 iterations in every **<sup>2</sup> <sup>6</sup> A1** half life. The T-Tauri ef fect on the interior could last tens of millions of years. It is assumed here that all the asteroids stayed warm long enough to outgas all of the **CO,** so that the mechanism for iron t ransport can **be fully** explored, an assumption that is not unrealistic. Although the C3 asteroids contain a greater concentration of carbon than **H** chondrites, the carbon is depleted at **30** times the rate. Should coolin **g** cause the melted region to disappear so that T<sub>c</sub> < 1200 K, deposition would begin 420,000 years later when the last of t he **CO** produced vacated the asteroid.

When the **CO** gas is gone, the carbonyl **s** wil 1 begin to decompose and deposit metals at a healthy rate. See table II. The liquid or solid carbonyls form a sink that wil maintain the carbonyl s at their vapor pres sures . **CO** gas e **x**its the asteroid at a rate that is 16 times that of the car bonyl gases since Knudsen diffusion flow is proportional to the mass of the molecule to the **3/2** power. The carbonyl speed is actually down **by** more than a factor of **16** when its

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condensation i s accounted for. Carbonyl solids are not mobile, but li quids could drip downward, but upon crossing the vaporizati on line, they would become a gas and diffuse back upwards, so the deposition should be most prevalent in the upper meters of the asteroid, where condensation occured Therefore, in quantitatively assessing the mass transport the asteroids can be divided into four zones. The innermost **85%** of each asteroid is divided into an unaltered zone (the bulk of the **85%)** and a depleted zone, where carbonyl pressures were sufficient to deplete this region of metals. The outer two zones are depicted in table II. The region above each dashed line is depleted in nickel, whose carbonyl has not condensed yet at **this** level, but enriched in iron, which has. The uppermost zone has both iron and nickel deposition **going** on. These zon es will henceforth be referred to as zones 1, 2, 3, and 4 in ascending order. Since much of the carbonyl deposited w ill have been formed in the upper zone from whence it origi nated, it is of interest to determine the state of the gas as it crossed zonal boundary lines. This is done in table III. We are interested only in the carbonyl groups that entered this region bonded to metal. The others produce a null net **e ffect.**

The volume of the "core" tells us the mass of carbon present. The percentage of CO<sub>2</sub> tells us how much carbon we can discount to this process. By determining the amount of CO that remained CO at the zone 2 - zone 3 boundary we can ge an idea of how much **CO** did not form a carbonyl until it en-

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tered the region where deposition would eventually occur, as well as the total production of iron pentacarbonyl. To quan**tify** the extra nickel production of zone **3,** the loss amount of **CO** needed to bring that gas into equilibrium with the vapor pressure of Fe(CC **<sup>5</sup>**is computed and knowing that **6** moles of Ni(CO)<sub>4</sub> should form for every 94 moles of Fe(CO)<sub>5</sub> (or 26 for every 74 in a C3 body), we get the nickel transport across the **3 -** 4 boundary.

Table III illustrates the net transport effects well. To place the metal deposits in a more detailed way than the zone system wi **<sup>11</sup>**require **f** urth er assumptions. Note that the zone boundary lines could be one kilometer lower in the case of an ordinary chondritic aste roid which cooled befo re the onset of deposition. For the deposition inhibiting CO to be out of the way, the central temperature must be below 1200 K. Thus the whole transient t e rm in equation 24 must be down **by** a factor of 1.3 so that where the temperature was 300 K, i is now 272 K, etc. This puts the zone boundaries about one kilometer deeper in a **100** km asteroid, and **300** meters deeper in the **30** km asteroid.

To notice that enrichments were on the order of a percent and discard this model as a small effect would be a mistake. It is too much to demand a perfectly even distribution of metal deposit throughout the entire volume of each zone. It is entirely possible that the metals were deposited in discrete sites, perhaps where a small amount of metal was present already as a nucleation site, or under favorable con-

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ditions. in metal could be **100%** or more. This process is autocatalytic. Local enrichments

One scenar io for "clumping" of iron would be for the liquid carbonyl s to flow downward to a point just above the zone boundary. **If** it were to flow below this point, it would become a gas and return to the condensation zone. The part of the zone just above the boundary has several advantages that make it a preferential place for deposition. First, it is at a lower gravitational potential, the liquids would flow there. Second, the higher temperatures permit the highest vapor pressures. It is from the gas phase that decomposition and deposition occur. Third, the deposition rates are eight orders of magnitude more favorable at the bottom than at the top of a deposition zone. Fourth, the upflow of liberated **CO** gas from the rapid deposition below could inhibit the rate of deposition above.

The numbers of moles of carbonyls given in table III are the net gain for a deposition zone, but the total carbonyl inventory is higher. It is entirely possible for carbonyls that formed higher up in the zone to flow downward, exaggerating the deposition below and depleting the upper parts of the metal with respect to its original abundance. This could account for the apparent trend in L-chondrites for a slight increase in nickel abundance with petrologic grade.

Some of the gas is sure to make its way to the surface. Escape velocity on the **100** km asteroid of ordinary chondritic composition is the greatest, yet it is only 14,900 cm sec<sup>-1</sup>.

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The peak velocity of a Maxwell velocity distribution of the heaviest gas  $(Fe(C0)_{5}$  whose weight is 196) at 100 K, which is well below the surface temperature of the asteroid, is 9200  $cm \text{ sec}^{-1}$ . Since this is better than 60% of the escape velocity, there are millions of escapes per second and the life time of this "atmosphere" is nil. If nickel carbonyl could linger, it could photodissociate to leave nickel, with CO escaping (Garratt and Thompson, 1934b).

Finally, after metal has been deposited, the gases have departed and the asteroid has cooled, a violent event such as an impact can occur, and metal-rich material or even metal chunks will be liberated into space, some of which eventually fall as meteorites to earth.

Iron meteorites formed in this way would show definite evidence of the carbonyl process. In industry, efforts are made to keep the carbon impurity down to a percent (Oxley, 1966). The IAB group is well known to contain cohenite  $(Fe<sub>3</sub>C)$ , as well as graphite nodules (Wasson, 1974). This class has nickel abundances that average about 7.55 wt %, which may tell us something about the oxidation state of iron in the parent body. It is also this class which could contain up to 15% silicates by weight. The IA iron El Taco has some silicate inclusions that are 9x10 cm and contains cracks (Buchwald, 1975). There is a definite limit to the amount of silicates and troilite that can be found in an iron meterorite, which in no way reflects upon its environment, but rather on its structural integrity since in a breakup of an iron,

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the exposed silicates would disperse. Evidence of this is seen in the hemispherical pits centimeters in diameter which can be seen on the surface of some iron meteorites, which on occasion contain traces **of** troilite (Lewis, **1968;** Read, et al., **1967).** This is evidence that these pits could represent cavities left behind **by** nodules of material inherent in the parent body at the deposition level other than iron and removes the requirement that this region be at least **85%** metal **by** mass.

It is interesting to note that the famous siderophile elements almost all form carbonyls. There are  $\text{Ir(C0)}_{8}$  and  $\mathsf{Ir}_4(\mathsf{CO})_{12}$ , Re $(\mathsf{CO})_{\mathsf{S}}$ , Ru $(\mathsf{CO})_{\mathsf{S}}$ , for example. Cobalt (see table IV) forms complex carbonyl molecules, as does p<mark>latinum</mark> Osmium and rhodium form carbonyl chlorides, as does platinum. If these carbonyls were also formed and deposi ted these elements in I AB irons, it would make an interesting and worthwhile research project to determine the **f** ate of the chlorin<mark>e, and whether or not lawrencite (Fe,Ni)Cl<sub>2</sub> will form.</mark> **I** AB irons have a lower iridium content than o ther irons. Perhaps iridium octacarbonyl is not as'effecti ve a transporter of iridium as iron and nickel carbonyls, so that the ful<sup>'</sup> iridium content is not imparted into them. **Of** elements noted for carbonyl behavior, it is interesting that molybdenum is enriched in Ca<mark>nyon Diablo (Mason, 1971), a noted IA,</mark> and that bromine, which is a trace el emen meteorites, is seen in Odessa. Bromine is often in complex carbonyls, such as platinum carbonyl bromide. However, it is also true that

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chromium and tungsten which form carbonyl s are not particularly prevailing in I AB's compared to other irons, although a thorough kinetic and thermodynamic investigation might lead to the reason. It is hoped that some of the points raised here are investigated.

Work has been done with reacting carbonyls in the presence of CS<sub>2</sub> and H<sub>2</sub>S. Iron, nickel, troilite and pentlandite form, and the kamacite-taenite phases are enveloped **by** the sulfides much as observed in meteorites (Bloch and Wirth, 1980). If only H<sub>2</sub>S and Fe(CO)<sub>5</sub> are used, then the products obtained were iron and troilite.

In carbonaceous chondrites, metal is not common, needless to say. If any were found, particularly iron, in any large quantity, it would be safer to suspect carbonyl vapor deposition than the survival of iron at unfavorable oxygen fugacities. That meteorite would be due further investigation.

In ordinary chondrites, there are two trends of interest. There is an overall increase in metal content with petrologic grade (Schmitt, et al., **1972),** and there is a slight decrease in nickel in L4's. If ordinary chondrites come from the top kilometers of a parent body (say one H parent, one L parent and one LL parent) , and petrologic grade is assumed to represent temperature, so that the highest grades with the less-distinct chondrules were subjected to higher temperatures during formation, it is possible that they all came from a depostion zone whose lower parts were

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enriched in metal. In any case, higher temperatures, to which higher petrologic grade has been attributed, promote deposition of metals from carb onyls, as shown above. On the negative side, no clear trend could be observed in LL's. Further, the amount of iron ox ides in H's deCreases with petrologic grade. This is an effect that could be attributed to different conditions, such as temperature of condensation, or oxidation state of iron, an **d** would take away from a deposition depth argument.

The second trend is that in the L chondrites, the L4's have one nickel abundance, and the **L5** and **L6** chondrites have another. The L4 chondrites, presumably formed at lesser depth, have a lower nickel content (Greenland and Loverling This does not support the idea of nickel deposition in "zone 4" of their parent body, unless it was a 10 kilometer object, in which case the lower nickel abundances are expected (table III), or unless the L4 chondrites formed very near the surface, well above the zone 3 - zone 4 boundary<mark>.</mark> **1965).**

In the formation of large bodies of iron, it is easy to imagine the entrapping of silicate fragments and chondritic matter. Sharp edges in this material would remain, unlike in high temperature igne ous models where the me lting point of iron is reached.

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### Industrial Applications

If the events described in this thesis have actually occured, it would be expected that the upper layers of asteroids would contain more iron, especially if their original carbon content is higher that **0.1** wt **%.** Vigarano type composition will give it a **1%** carbon content.

If, in the future, it becomes more economically (or politically) feasible to exploit the resources in space, a process for mining asteroids-of metal could be devised using carbonyl s.

A space vehicle would p<mark>ark near a metal-rich asteroid</mark> surface. (Metal **-rich** material could have been pre-n *ined* orextracted from shallow depth by an advance crew, if neces<sub>t</sub> sary.) CO is then reacted with the ore at kinetically timum conditions (about 400 K and 20 atm) if possible. Iron oentacarbonyl gas i **s** then heated to **600** K on board the vessel, in a platin **g** chamber . The liberated **CO** gas is **p** umped back out to be reus ed until the sufficient metal quantit **y** has been taken aboard or the asteroid has been exhausted. Th vessel could then travel to earth, or more conveniently to a space station, where metals could be sorted. Nickel, iron chromium and tungsten would be easily obtainable, as well as molybdenum, if it i s availab le. If platinum is abundant more complicated techniques can be employed to form its carbonyl halides. T hese sorted metals could then be sent t **0** earth, or be used in space. If space industrialization be The comes a reality, it could well be cheaper to obtain raw ma-

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terials from asteriods than to blast dense metals off the surface of the earth, with its vastly larger escape velocity and potential well.

 $\label{eq:2.1} \frac{d\mathbf{y}}{dt} = \frac{1}{2} \left[ \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} \right] \mathbf{y} + \frac{d\mathbf{y}}{dt} = \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} = \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} = \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} + \frac{d\mathbf{y}}{dt} = \frac{d\mathbf{y}}$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$  , where  $\mathcal{L}^{\text{max}}_{\text{max}}$ 

 $\sim 100$ 

 $\mathcal{L}_{\mathcal{A}}$ 

 $\sim 10^{-1}$ 

 $\sim 10^4$ 

 $\mathcal{L}^{\text{max}}$  , where  $\mathcal{L}^{\text{max}}$ 

 $\sim$ 

 $\sim 10$ 

 $\mathcal{L}^{\text{max}}$  .

 $\bullet$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$  ,  $\mathcal{L}^{\text{max}}_{\text{max}}$ 

 $\label{eq:2.1} \frac{1}{2} \int_{\mathbb{R}^3} \frac{1}{2} \left( \frac{1}{2} \int_{\mathbb{R}^3} \frac{1}{2} \left( \frac{1}{2} \int_{\mathbb{R}^3} \$ 

### Conclusion

In conclusion, a new model for the formation of iron meterorites involving th e production of carbonyls at 300-400 K in an aste roid, their upward tr ansport as a gas, and their dissociation at low pressure after carbon monoxide has dif**fused** out, has been tested thermo dynamically, and has been found possible within the confines of our present knowledge of the kinetics of the breakdown of carbonyls at low temperatures. The iron nickel ratio in I AB irons tell us that the parent body was an ordinary chondrite or they would be on the order of **26%** nicke l **by** weight. Iron asteroids" must not be considered to be iron based on observations of their surfaces, until their bulk densities are known. The possibility cannot be overlook ed th at they ar e merely iron coated. **If** iron i s preferenti **ally** deposited at a depth of **290** met ers in a **10 k** m asteroid, it **is** possible that th e upper layer was stri **pp** ed away leav ing a n iron sur **face.**

T he chemical quest ions broug ht up c oncerning other carbonyls depositing siderophiles, bromine traces and chlorine, as wel **I** as the que stion of the a ppearanc e of lawrencite, should be investigated. Further , the de position rates at zero CO pressure were extrapolated below the experimenta data to below roo m temperature. **A** lthough very low rates were reported, this co uld be tested **by** considering a sample at **250** K for one year wi th sufficient dep osition area to obtain adetectable amount of iron.

This work is by no means intended to be the last word on

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## the subject of carbonyl transport of metal in asteroids.

 $\bullet$ 

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 $\ddot{\phantom{1}}$ 

 $\bullet$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$  and  $\mathcal{L}^{\text{max}}_{\text{max}}$ 

 $\sim 1$ 

 $\sim 10$ 

 $\sim 1$ 

 $\mathbf{v}^{\prime}$ 

### Acknowledgments

I would like to thank Prof.. John **S.** Lewis for timesaving suggestions and for his: support of this project. Robert Gonzalez rewrote a calculator program to run many times faster, and he and Mark Matson laboriously typed the text of this thesis. I would also like to thank my parents, whose support and encouragement over many years made it possible for me to participate one day in the graduate program at MIT. Their prayers and petitions, as well as those of the brothers and sisters of the church in Newton have been answered. This work was supported **by** the National Aeronautics and Space Administration through the Planetary Atmospheres Program under Grant **NGL 22-009-521.**

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Table I Velocity Time ...Temperature Location  $(m)$ cm sec  $($ sec $)$  $range (K)$ 10 km asteroid:  $4.1x10^{11}$  $3.4x10^{-7}$  $6.14 - 4.76$ 1000-1200  $2.4x10^{11}$  $4.8 \times 10^{-7}$  $7.27 - 6.14$ 800-1000  $6.2x10^{-7}$  $8.1x10^{10}$ 700-800  $7.77 - 7.27$  $6.4x10^{10}$  $7.4x10^{-7}$ 600-700  $8, 24 - 7, 77$  $4.9x10^{10}$  $9.2x10^{-7}$  $8.69 - 8.24$  $500 - 600$  $1.2x10^{-6}$  $3.5x10^{10}$  $9.11 - 8.69$ 400- 500  $1.5x10^{-6}$  $1.4x10^{10}$  $-350 - 400$  $9.32 - 9.11$  $1.1x10^{10}$  $1.9x10^{-6}$  $9.52 - 9.32$  $300 - 350$  $4.2x10<sup>9</sup>$  $2.4x10^{-6}$  $275 - 300$  $9.62 - 9.52$  $2.6x10<sup>9</sup>$  $3.4x10^{-6}$  $250 - 275$  $9.71 - 9.62$  $2.4x10<sup>9</sup>$  $4.2x10^{-6}$  $9.81 - 9.71$  $225 - 250$  $1.4x10<sup>9</sup>$  $7.4x10^{-6}$  $9.91 - 9.81$  $200 - 225$  $3.6x10^8$  $1.4x10^{-5}$  $9.96 - 9.91$  $185 - 200$  $9.1x10<sup>7</sup>$ 4.4x10 $-5$  $10.00 - 9.96$ 175-185 30 km asteroid:  $9.1x10^{-8}$  $4.6x10^{12}$  $18 - 43 - 14.27$ 1000-1200  $3.0x10^{12}$  $1.1x10^{-7}$  $21.81 - 18.43$ 800-1000  $1.2x10^{12}$  $1.3x10^{-7}$  $23.31 - 21.81$  $700 - 800$  $1.1x10^{12}$  $I.3x10^{-7}$  $24.72 - 23.31$ 600-700  $9 - 5 \times 10^{-11}$  $1.4x10^{-7}$ 26.06-24.72 500-600 8.5x10<sup>11</sup>  $1.5x10^{-7}$  $27.33 - 26.06$ 400- 500  $4.1x10^{11}$  $1.5x10^{-7}$  $27.95 - 27.33$  $350 - 400$  $3.8x10^{11}$  $1.6x10^{-7}$ 28.55-27.95 300-350  $1.9x10^{11}$  $1.6x10^{-7}$  $275 - 300$ 28.85-28.55  $1.8x10^{11}$  $1.6x10^{-7}$ 29.14-28.85  $250 - 275$  $1.8x10^{11}$  $1.6x10^{-7}$  $29.43 - 29.14$  $225 - 250$ \*\*\*\*\*\*\*\*\*\*  $1.3x10^{10}$  $2.2x10$  $200 - 225$  $29.72 - 29.43$  $3.7x10<sup>9</sup>$  $4.6x10^{-6}$ 185-200 29.89-29.72  $6.9x10^{8}$  $1.6x10^{-5}$ 175-185 30.00-29.89

 $100$   $km$  asteroid:



The **10** km asteroid had its velocities determined **by** the equation for Knudsen diffusion (22). The **30** km asteroid **had** its mean free nath exceeding the diameter of the tube for the last **570** meters. The rest of this asteroid and the whole **100** km asteroid underwent continuum diffusion (equation *25).*



 $\sim$   $\sim$ 

 $\ddot{\phantom{0}}$ 

 $\bar{\beta}$ 

 $\bullet$ 

Moles of CO exiting zone Location Asteroid Layer carrying Fe  $(m)$ carrying Ni total  $\mathcal{L}_{\mathcal{S}}(\mathbf{z},\mathbf{y})$  $2.06x10^{17}$  $0.00 - 91.11$ 100 km  $\mathbf{L}$  $3.54x10^{16}$  $1.30x10^{17}$  $4.08x10^{16}$ 91.11-95.17  $C<sub>3</sub>$  $\overline{2}$ 4.49x10<sup>16</sup>  $3.13x10^{16}$  $95.17 - 97.13$  $\mathbf{3}$ 97.13-100. 4  $5.54x10^{15}$  $0.00 - 27.33$  $30$  km I. 2.79x10<sup>15</sup> 3.82x10<sup>14</sup>  $2.00x10^{15}$  $C<sub>3</sub>$  $\overline{2}$  $27 - 33 - 28 - 55$  $3.90x10^{14}$ 1.99x10<sup>15</sup>  $28.55 - 29.43$  $\overline{3}$ 4  $29.43 - 30.00$  $2.06x10^{14}$  $0.00 - 9.52$ 10 km  $\mathbf{L}$  $1.51x10^{14}$  $3.91x10^{12}$ 5.07x10<sup>13</sup>  $9.52 - 9.71$  $C<sub>3</sub>$  $\overline{2}$  $4.16 \times 10^{12}$  $5.04x10^{13}$  $\overline{3}$  $-9.71 - 9.91$  $9.91 - 10.00$ 4  $I.47x10^{17}$  $0.00 - 95.17$ 100 km  $\mathbf{I}$  $1.16x10^{17}$  $6.17x10^{15}$  $2.51x10^{16}$  $95.17 - 97.13$  $\overline{\mathbf{H}}$  $\overline{2}$ 7.08x10<sup>15</sup>  $2.51x10^{16}$ 97.13-99.05  $\overline{\mathbf{3}}$ 00.05-100.  $\frac{4}{T}$  $3.97 \times 10^{15}$ 30 km  $\mathbf{r}$  $0.00 - 28.55$  $2.91x10^{15}$  $1.47x10^{14}$  $9.16x10^{14}$ 28.55-29.14 **H**  $\mathbf{z}$  $1.93x10^{14}$  $9.15x10^{14}$  $\mathbf{3}$ 29.14-29.72 29.72-30.00 4  $1.47x10^{14}$  $0.00 - 9.52$  $10 \text{ km}$  $\mathbf{L}$ 5.39x10<sup>12</sup>  $3.64x10^{13}$  $1.06x10^{14}$ H  $\mathbf{z}$  $9.52 - 9.71$  $7.09x10^{12}$  $3.64 \times 10^{13}$  $\overline{\mathbf{3}}$  $9.71 - 9.91$ 4  $9.91 - 10.00$ 

Table III



 $\hat{\mathcal{A}}$ 

 $\frac{1}{\sqrt{2}}$ 

## Table IV

 $\sim 10^{11}$ 

 $\Delta$ 

 $\downarrow$ 

 $\sim$ 

 $\mathcal{A}^{\pm}$ 

 $\frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2}$ 



(Emeléus and Anderson, 1938)

## Figure Captions

Figure 1: The pressure of iron pentacarbonyl is at least *35* orders of magnitude less than **CO.** At 600 K, the activity of iron begins to drop as magnetite appears. At **373 K,** iron dissappears and the activity of magnetite is one.

Figures  $2 - T$ : These figures show the equilibrium gas pressure for each of the gases CO, Fe(CO)<sub>5</sub>, and Ni(CO)<sub>4</sub>, and of lithostatic pressure which is a function of depth. These figures depict the situation before cooling has altered the temperature gradient given in equation **23** for the **10** km asteroid, and before outgassing has reduced the pressure of the gases.



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 $-58-$ 



 $-59-$ 



 $-60-$ 



 $-61-$ 



 $-62-$ 



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## Biographical Note

Mark Lupo was born on March **28, 1957** in~ Huntington, New York and grew up in Northport. He is a graduate of Northport High School, which he attended from **1972 - 1975.** Mark attended MIT from September **1975** to June **1979** as an undergraduate and earned two degrees: Bachelor of Science in Eatth and Planetary Science, and Bachelor of Science in Applied Mathematics. Readmitted in **1979** as a graduate student, ha has served as a teaching assistant and as a research assistant. His publications include Lupo, M., **J..,** and Lewis, *J..* **S. (1979).** Mass- radius relationships in icy satellites. icearus **40, 157-170.**

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