# Liquid Argon HEC Wheel Assembly Database 

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This document describes the details of the contents of the LAr Hadronic EndCap Wheel Assembly Database. This database contains the important data from the wheel assembly: mechanical alignment, electrical properties, cabling, and a summary of the readout gap failures. This document describes the final database that is intended mainly for archival purposes. This database should be viewed in conjunction with the HEC module production database that describes the modules that form the wheel and the Feedthrough database that describes the signal feedthroughs. This wheel database lists for instance the location of the modules, the amplifiers to which they are connected, and the details of the alignment measurements. It also details all non-conformances. It is important that for all non-conformances, whether they occurred during wheel assembly or in the B180 cold tests, that a single table be produced of all the non-conformances listing the non-conformance in a format suitable for making offline corrections to the data. This non-conformance table will be derived from a set of queries of this database.

This database covers the description of the HEC from the liquid argon gaps to the pins in the front end crate (FEC). As some non-conformances are described in terms of FEC module number and FEC module channel number some extension is included to this basic definition.

The database is initially being developed as a MS Access Database, initially maintained by the TRIUMF group. Now the data in this database is complete (as the work in B180 is completed), the data will be transferred to the CERN Oracle Database, maintained by the CERN IT group. This wheel assembly data will be maintained for the lifetime of ATLAS, and are useful for the experts who produced the HEC, and the end-users (technicians, physicists) to aid access to any or all pertinent details regarding a particular HEC module or component. In addition, it is required by the ATLAS Technical Coordination (TC) that any parts of the detector that will be moved to the ATLAS Cavern should have detailed data in the database at the time of installation.

## IMPLEMENTATION:

The LAr Hadronic EndCap Wheel Assembly data is currently residing in the MS Access database 'HEC_Wheel_Assembly_Database'. This effort is now completed. The database will soon be permanently handed over to the LAr database group. This database will be migrated to the official CERN production database infrastructure upon final review.

## Structure of the database:

The database covers four major areas:

- Mechanical information of the wheel such as alignment measurements.
- Electrical information such as the measurements of the pre-amplifiers on the wheel.
- Cabling information that details how individual towers are readout and transmitted to the front-end board.
- A non-conformance tables that detail such failures as channels that cannot hold full high voltage.

The critical aspect of this database is the HV, LV, calibration and signal cable wiring and the use of this information with the non-conformance tables. During the design of the database, it was decided to keep the input electrical and non-conformance data in tables natural to the recording of this data. So the input forms are just those provided by those who did the work with an extra first column that provides a unique identifier for each entry in the table, and some lines added for ease of cross reference within the database. For the cabling data, one summary table with a line for each readout tower was formed. From this summary table (Signal Line Summary) it is trivial to find which tower is connected to each pin of the front-end crate, and which towers are affected when for instance a HV line fails. While the database contains the details of the wiring, and some details must be described here, it is not our intent to describe in this document the complete wiring of the HEC. This is definitively described in full in "Cabling of the ATLAS liquid argon calorimeters ATL-A-EN-0001 v.2".

The mechanical aspects described in this database are for archival purposes. The alignment measurements are not detailed enough to describe exactly the location of each plate in the calorimeter, so it is not anticipated that these measurements will be used to describe alignment information for the "Conditions Database" of the calorimeter. The wheels are constructed to tolerances in the millimetre region. It would seem likely that variations within these tolerances will not affect the calorimeter operation. Alignment information used in data manipulation will likely be limited to design values and 6 numbers for each wheel (such as 3 positions and 3 rotations). These six numbers can only be measured when the wheels are in ATLAS. They are not part of this database.

The database architecture does not lend itself to be shown on a single page. So we will first show the overall structure then detail the various aspects in separate architecture charts. In the overall structure we will show how this database could be connected to the HEC Module Production Database and the Signal Feedthrough Production Database.


Figure 1 : Architecture for LAr HEC Wheel Assembly Database. The module serial number, allows this database to be connected to the HEC module production database, by making a relationship on this entry between to two databases. The Feedthrough Database connects through the feedthrough location identifier. Shown also is the highest level table the Wheels \& Cryostats Table that lists the four wheels and two cryostats described in the database.

## Mechanical Details

Tables:
Front Wheel Alignment Summary
Rear Wheel Alignment Summary
Inter-module Gaps
Alignment Details
Wheel Shim Details

| Front Wheel Alignment <br> Summary |
| :--- |
| Cryostat/Wheel/WheelLocation <br> Cryostat <br> Wheel <br> Wheel_Cryostat <br> Wheel Location <br> Date <br> Name <br> Comment <br> Outer Faces of the Two Sliding Rails <br> Maximum Inner Radius (Plates 1-8) <br> Minimum Inner Radius (Plates 1-8) <br> Maximum Inner Radius (Plates 9-24) <br> Minimum Inner Radius (Plates 9-24) |


| Wheel Shim Details |
| :--- |
| Cryostat/Wheel/Wedge1_2/PlateNumber |
| Cryostat |
| Wheel |
| Wheel_Cryostat |
| Wedge 1 |
| Wedge 2 |
| Plate Number |
| Shim Thickness Required |
| Installed Shim Thickness |


| Inter-module Gaps |
| :--- |
| Cryostat/Wheel/Wheel <br> Location/ModuleLoc1_2 |
| Cryostat |
| Wheel |
| Wheel_Cryostat |
| Wheel Location |
| Module Location 1 |
| Module Location 2 |
| Gap Top Inner |
| Gap Top Outer |
| Gap Bottom Inner |
| Gap Bottom Outer |



## Inter-module Gaps

Cryostat/Wheel/Wheel
Location/ModuleLoc1
Cryostat
Wheel
Wheel_Cryostat
Wheel Location
Module Location 1

Gap Top Inner
Gap Top Outer
ap Bottom Outer

Rear Wheel Alignment Summary

## Cryostat/Wheel/WheelLocation

Cryostat
Wheel
Wheel_Cryostat
Wheel Location
Date
Name
Comment
Outer Faces of the Two Sliding Rails
Maximum Inner Radius (Plates 25-40)
Minimum Inner Radius (Plates 25-40)

Figure 2 : Architecture for LAr Mechanical Aspects of the HEC Wheel Assembly Database. The Wheel-Cryostat identifier allows these tables to be connected, internally within the mechanical aspects and externally to the other tables of the HEC Wheel Assembly Database.

## Electrical Details

Tables:
Wheel Electrical Summary
PSB Locations
PSB Performance Summary
Module Locations

| Wheel Electrical Summary |
| :--- |
| Cryostat/Wheel/Wedge <br> Cryostat <br> Wheel <br> Wedge <br> Cryostat/Wedge <br> Wheel_Cryostat <br> Module Serial Number <br> HV test Passed? <br> Did HV problems have to <br> be addressed <br> Comment on HV fixes <br> Other Comments <br> Date of Final Check |

PSB Locations

| Cryostat/Wedge |
| :--- |
| PSB A Serial |
| PSB B Serial |
| PSB C Serial |
| PSB D Serial |
| PSB E Serial |

Module Locations

| Cryostat/Wheel/Wedge |
| :--- |
| Cryostat |
| Wheel |
| Wheel_Cryostat |
| Wedge |
| Module Serial Number |

PSB Performance Summary PSB Serial/Tower PSB Serial
Tower
\# Amplifiers in Tower
\% Non-Linearity
Average Transfer Coefficient kOhm
\% Uniformity of Preamplifier Gains RMS Noise (mV) at Nominal Vee RMS Noise (mV) at High Vee


Figure 3 : Architecture for LAr Electrical Aspects of the HEC Wheel Assembly Database. The Wheel-Cryostat, Cryostat/Wheel/Wedge and PSB Serial/Tower identifiers allow these tables to be connected, internally within the electrical aspects and externally to the other tables of the HEC Wheel Assembly Database.

Signal Feedthrough and Crate Positions
Quadrant
F/T and Crate Position
Cryostat

Figure 4A : Tables of signal feedthroughs and crate positions.

## Cabling Details

Tables:

## HV Cabling

| Cryostat/Wedge/Z/SubGap |
| :--- |
| Cryostat/Wedge/Z |
| Cryostat/FT conn \#/Pin \# |
| Cryostat |
| ISEG Module |
| Channel Number |
| Cable |
| Pin Number |
| FeedThrough |
| HV Patch Panel (Plug) |
| HV Patch Panel (Socket) |
| Wedge |
| Z |
| SubGap |
| Module Serial Number |
| Patch Panel Connector In |
| Patch Panel Pin In |
| Patch Panel Connector Out |
| Patch Panel Pin Out |
| Section of Module |

## Quadrant Signal \& Calibration Cabling

Cryostat/Qwedge/PSB_letter/Pad/SubZ Cryostat/Qwedge/PSB_letter/Tower
Cryostat
Qwedge
PSB Letter

## Tower

Pad

## Gap

Gap_new
ETA
PHI
PHI_letter
Z
SubZ
PSB

## INCON

INPIN
OUTCON

## OUTPIN

Signal Patch Panel Input Connector
Signal PP Input Connector Pin
Signal Patch Panel Output Connector
Signal PP Output Connector Pin
Signal Patch Panel
Cold flange pigtail Connector Pin
Feedthrough Connector Number
Front End Board Number
Front End Crate SLOT
Front End Board Connector
FEB input connector pin
FEB Shaper Channel Number
FEB ADC Number
FEB ADC Channel
FEB Output connector pin
Trigger Driver Board Number
Trigger Driver Channel
Trigger Driver input connector
Trigger Driver input connector pin
Trigger Driver output connector
Trigger Driver output connector pin
Calibration Generator Channel
Calibration Feedthrough connector \#
Calibration lines of Wedges
Calibration Patch Panel Number
Calibration PP Input Connector \#
Calibration PP Input Conn Pin \#
Calibration PP Output Connector \#
Calibration PP Output Conn Pin \#
Calibration distribution board on wheel Distribution board Input Connector Distribution board Input Connector Pin Distribution Board Output Connector Distribution Board Output Connector Pin Strip-line Type

Figure 4B : Tables of the Signal, LV and HV wiring. The identifiers shown in bold allow these tables to be connected, internally within the cabling aspects and externally to the other tables of the HEC Wheel Assembly Database.

## Calibration Lines (TDR Measurements) Table

| Quadrant1to4/cryostat/channel |
| :--- |
| Quadrant1to4 |
| Cryostat |
| Channel |
| Warm Cable Impedance (Ohm) |
| Vacuum Cable Impedance (Ohm) |
| Pigtail Impedance (Ohm) |
| Pigtail resistance (Ohm/ns) |
| Quadrant Cable Impedance (Ohms) |
| Quadrant Cable Resistance (Ohms/ns) |
| Stripline Impedance (Ohms) |
| Stripline Resistance (Ohms/ns) |
| Stripline Termination Impedance (Ohms) |

## FEB Input Lines TDR Measurements Table

| Quadrant1to4/cryostat/FEB/channel |
| :--- |
| Quadrant1to4 |
| Cryostat |
| FEB |
| Channel |
| Warm cable Impedance (Ohms) |
| Vacuum Cabe Impedance (Ohms) |
| Pigtail Impedance (Ohms) |
| Pigtail Resistance (Ohms/ns) |
| Quadrant Cable Impedance (Ohms) |
| Quadrant Cable Resistance (Ohms/ns) |
| Calibration Cable PSB Termination Impedance (Ohms) |

Quadrant Definition Table
Quadrant
Cryostat
Quadrant(1 to 4)

Quadrant-Wedge Definition Table
Cryostat/Wedge
Quadrant
Cryostat
Wedge
Qwedge

## FEB Definitions Table

FEB Shaper Channel
FEB Channel Number

Figure 4C : Tables of the FEB Input Lines TDR measurements and the Calibration Lines (TDR Measurements) tables. These TDR measurements were made in B180 with the cryostat cold.
Also shown to the right are the related Quadrant, Quadrant-Wedge and FEB definition Tables, that help connect these tables to the other cabling tables.

| Cryostat/Wedge/Z/Tower |
| :--- |
| Cryostat/Qwedge/PSB_letter/Tower |
| Cryostat/Wedge/Z |
| Cryostat/Wedge/PSB_letter |
| PSB_Serial/Tower |
| Wheel_Cryostat |
| Cryostat/Wheel/Wedge |
| Cryostat |
| Wedge |
| QWedge |
| Z |
| Wheel |
| Tower |
| ETA |
| PHI |
| PSB Letter |
| Module Serial |
| PSB Serial |
| Calibration Generator 1 |
| Calibration Generator 2 |
| Calibration Generator 3 |
| Calibration Generator 4 |
| Ntiles |
| HV Est1 |
| HV Est2 |
| HV Pad1 |
| HV Pad2 |
| LV1 Q Number -1,5v |
| LV1 Q Number GND |
| LV2 Q Number +3V |
| LV2 Q Number GND |
| LV3 Q Number +7V |
| LV3 Q Number GND |
| Feedthrough Location |
| FT Connector |
| FEC Slot |
| FEB Connector |
| FEC Pin |
|  |

Figure 5: The signal line summary table. This table describes for each readout volume in the HEC its corresponding pin in the Front End Crate. In addition it lists the serial numbers of all items that might fail, or be affected by a failure, that are associated with this readout volume. This table provides simple interconnection between the tables of the database. To the left of the table is shown the Signal \& Calibration table (truncated), along with the LV and HV cabling tables (truncated). To the right are the connections to the mechanical and electrical tables. The connecting lines show the database relationships.

## Non-Conformance Table

|  |
| :--- |
| Problem \# |
| Issue FEB=1, CAL=2, HV_Pin=3,HV_Line=4 |
| Cryostat |
| Quadrant(1 to 4) |
| Front End Board Number |
| Front End Board Channel |
| Calibration Board Channel |
| Comment |
| Wedge |
| Module |
| Gap with HV pin cut |
| Gap Cut |
| Z |
| Severity of Problem |
| Comment on Severity of Problem |

Figure 6: Table of non-conformance. The concept here is to have one table to list all known non-conformances of the system on leaving B180 (so hopefully as on arrival at the ATLAS pit).

Tables required to_interpret the Non-Conformance Table

## FEC Pin to FEB Channel Definitions

```
FEB Channel
```

FEC Pin
FEB Connector

## FEB Slot_Module Definitions

```
FEC Slot
FEB Module Number
```

Figure 7: The database describes all aspects of the HEC cabling from the liquid argon cell to the pins on the front end crate. However some information beyond this is required to understand the non-conformances as described by those making measurements in the front end crate.

## SUMMARY OF DATA ENTRIES:

A definition of each of the data entries in this database is given along with a short statistical summary to allow anyone interested to decide if the data is likely to contain pertinent information

## Data Definitions:

## Wheels \& Cryostats

This is the entry point into the database. All the tables describing the mechanical details, are directly related to this table through the Wheel_Cryostat entry.

| Cryostat/Wheel | A/HEC1 | A/HEC2 | C/HEC1 | C/HEC2 |
| :--- | :--- | :--- | :--- | :--- |
| Cryostat | A | A | C | C |
| Wheel | HEC1 | HEC2 | HEC1 | HEC2 |
| Wheel_Cryostat | HEC1A | HEC2A | HEC1C | HEC2C |

Complete listing of the Wheels \& Cryostats table

## Cryostat/Wheel

Unique identifier for this table. 2 cryostats and 2 wheels: 4 entries in total.

## Cryostat

This is the cryostat location in ATLAS: A end or C end. The A end is installed nearest the airport, the C end nearest to St Genis.

## Wheel

The HEC1 refers to the wheel being a front wheel. Only 1 (Front) and 2 (Rear) wheels were produced.

## Wheel_Cryostat

This is the identifier that is used to make the relationships between all the tables except the amplifier PSB board performance summary. It is also the unique identifier for this table. It has the typical format HEC1A, where:
The HEC1A refers to the wheel being a wheel manufactured for the A cryostat. HEC1 refers to this being a front wheel. Only 1 (Front) and 2 (Rear) wheels were produced.

## 1. MECHANICAL TABLES

Front Wheel Alignment Summary
Rear Wheel Alignment Summary
Alignment Details
Inter-module Gaps
Wheel Shim Details

## Front Wheel Alignment Summary

The table below gives the contents of this table in March 2004. The comment field has been truncated to allow easy reproduction of this table in this document. As row 1 is not completed at time of writing, row 2 will be used as table as our specimen value.


## Cryostat/Wheel/WheelLocation

Unique identifier for this table in the database: two cryostat, two wheel and two wheel locations: eight entries in this table.
Specimen value: A/HEC1/Table, where:
A : The A cryostat.

HEC1 : The front(1) wheel.
Table : The wheel was first constructed in the horizontal on a wheel assembly table. Then the wheel was rotated and placed on the cradle $T 6$ in front of the cryostat. At these two locations Table and $T 6$ alignment measurements were made. In this specimen line the measurement was made on the wheel assembly Table.

## Cryostat

Specimen value: $A$, where:
A : The A cryostat.

## Wheel

Specimen value: HEC1, where:
HEC1 : The front(1) HEC wheel.

## Wheel_Cryostat

Specimen value: HEC1A, where:
HEC1A : The front(1) wheel in the A cryostat.

## Wheel Location

Specimen value: Table, where:
Table $\quad:$ The wheel was first constructed in the horizontal on a wheel assembly table.
Then the wheel was rotated and placed on the cradle $T 6$ in front of the cryostat. At these two locations Table and $T 6$ alignment measurements were made. In this specimen line the measurement was made on the wheel assembly Table.

## Date

Date of the measurements.

## Name

Name of person recording measurements.

## Comment

Free format comment to encourage transfer of useful information.

## Outer Faces of the Two Sliding Rails

Specimen value: 4255 mm , this being the distance between the two outer faces of the two sliding rails (the rails at 3 and 9 o'clock on the wheel, on which the wheel is supported). This number is recorded because it partly defines the outer envelope of the HEC.

## Maximum Inner Diameter (Plates 1-8)

Specimen value: 746 mm , this being the maximum inner diameter of the hole in the middle of the HEC (for plates 1-8). This number is recorded because it partly defines the inner envelope of the HEC.

## Minimum Inner Diameter (Plates 1-8)

Specimen value: 745 mm , this being the minimum inner diameter of the hole in the middle of the HEC (for plates 1-8). This number is recorded because it partly defines the inner envelope of the HEC.

## Maximum Inner Diameter (Plates 9-24)

Specimen value: 952 mm , this being the maximum inner diameter of the hole in the middle of the HEC (for plates 9-24), in which the Forward Calorimeter sits. This number is recorded because it partly defines the inner envelope of the HEC.

## Minimum Inner Diameter (Plates 9-24)

Specimen value: 951 mm , this being the minimum inner diameter of the hole in the middle of the HEC (for plates 9-24), in which the Forward Calorimeter sits. This number is recorded because it partly defines the inner envelope of the HEC.

## Rear Wheel Alignment Summary

The table below gives the contents of this table in March 2004. The comment field has been truncated to allow easy reproduction of this table in this document. As row 1 is not completed at time of writing, row 2 will be used as table as our specimen value.

|  | $\begin{aligned} & 0 \\ & \underset{0}{0} \\ & \stackrel{n}{n} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & \sum_{\stackrel{\rightharpoonup}{\otimes}} \\ & \underline{\sim} \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\square}{2} \\ & \stackrel{\sim}{\nabla} \end{aligned}$ | $\begin{aligned} & \text { Z0 } \\ & \underset{\sim}{3} \end{aligned}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A/HEC2/T6 A | A | HEC2 | HEC2A | T6 |  |  | Measurement not made as of Feb04 |  |  |  |
| A/HEC2/Table A |  | HEC2 | HEC2A | Table | 04-Feb-04 | ROY LANGSTAFF | FOR SURVEY DETAILS REFER TO EDMS DOCUMENT ATL-AE-UR0029. | 4257 | 952 | 950 |
| C/HEC2/T6 C | C | HEC2 | HEC2C | T6 | 15-Apr-03 | ROY <br> LANGSTAFF | TOP' MEASUREMENTS FWERE ... | 4257 | 951 | 950 |
| C/HEC2/TableC |  | HEC2 | HEC2C | Table | 06-Nov-02 | ROY <br> LANGSTAFF | ALL GAP <br> MEASUREMENTS | 4256 | 951 | 950 |

This identical to the front wheel alignment summary except:
o Maximum Inner Diameter (Plates 1-8)
o Minimum Inner Diameter (Plates 1-8)
o Maximum Inner Diameter (Plates 9-24)
o Minimum Inner Diameter (Plates 9-24)
are not present. Instead the following two items are present:

## Maximum Inner Diameter (Plates 25-40)

Specimen value: 952 mm , this being the maximum inner diameter of the hole in the middle of the HEC2 (for plates 25-40), in which the Forward Calorimeter sits. This number is recorded because it partly defines the inner envelope of the HEC.

## Minimum Inner Diameter (Plates 25-40)

Specimen value: 950 mm , this being the minimum inner diameter of the hole in the middle of the HEC2 (for plates 25-40), in which the Forward Calorimeter sits. This number is recorded because it partly defines the inner envelope of the HEC.

## Alignment Details

|  | $\begin{aligned} & \text { ? } \\ & \text { ర } \\ & \stackrel{p}{\#} \\ & \stackrel{0}{2} \end{aligned}$ | $\begin{aligned} & \sum_{\stackrel{\rightharpoonup}{0}}^{\substack{0}} \end{aligned}$ |  |  |  | $\times$ | $\prec$ | N |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A/HEC1/Table/10 | A | HEC1 | HEC1A | Table | 10 | -783.1 | -1891.6 | 1000.9 |
| A/HEC1/Table/11 | A | HEC1 | HEC1A | Table | 11 | -1137.5 | -1702.4 | 999.6 |
| A/HEC1/Table/12 | A | HEC1 | HEC1A | Table | 12 | -1448.2 | -1447.5 | 1000 |
| A/HEC1/Table/13 | A | HEC1 | HEC1A | Table | 13 | -1702.6 | -1137 | 1000.4 |
| A/HEC1/Table/14 | A | HEC1 | HEC1A | Table | 14 | -1892 | 783.4 | 1001 |
| A/HEC1/Table/15 | A | HEC1 | HEC1A | Table | 15 | -2008.4 | -399.6 | 1000.8 |
| A/HEC1/Table/16 | A | HEC1 | HEC1A | Table | 16 | -2069.8 | -0.2 | 1006.9 |
| A/HEC1/Table/17 | A | HEC1 | HEC1A | Table | 17 | -2008.6 | 399.8 | 1000.9 |

## Cryostat/Wheel/Wheel Location/AlignmentLocNumber

Unique identifier for this table in the database: two cryostat, two wheel, two locations, 32 alignment locations: 256 entries in this table.
Specimen value: A/HEC1/Table/10, where:
A : The A cryostat.
HEC1 : The front(1) wheel.
Table : The wheel was first constructed in the horizontal on a wheel assembly table. Then the wheel was rotated and placed on the cradle $T 6$ in front of the cryostat. At these two locations Table and T6 alignment measurements were made. In this specimen line the measurement was made on the wheel assembly Table.
$10:$ The position number on the wheel of this alignment measurement.

## Cryostat

Specimen value: A, where:
A : The A cryostat.

## Wheel

Specimen value: HEC1, where:
HEC1 : The front(1) wheel.

## Wheel_cryostat

Specimen value: HEC1A, where:
HEC1A : The front(1) wheel in the A cryostat.

## Wheel Location

Specimen value: Table, where:
Table : The wheel was first constructed in the horizontal on a wheel assembly table. Then the wheel was rotated and placed on the cradle $T 6$ in front of the cryostat. At these two locations Table and $T 6$ alignment measurements were made. In this specimen line the measurement was made on the wheel assembly Table.

## Alignment Location Number

Specimen value: 10, where:
10 : The position number on the wheel of this alignment measurement.
X
Specimen value: -783.1, where:
-783.1 mm : The x position of the alignment location.
Y
Specimen value: -783.1, where:
-1891.6 mm : The y position of the alignment location.
Z
Specimen value: 1000.9 , where:
-1891.6 mm : The z position of the alignment location.
To give the reader a feel for the typical variation in x and y , we determine the average and RMS radius:

|  | Radius (excluding 16 \& 32) | Radius of points 16 \& 32 |
| :---: | :---: | :---: |
| Radius $(\mathrm{mm})$ | 2279.27 | 2302.04 |
| RMS $(\mathrm{mm})$ | 0.49 | 0.85 |

and for the z variation, the corresponding values:

|  | $Z$ (excluding 16 \& 32) | $Z$ of points $16 \& 32$ |
| :---: | :---: | :---: |
| $Z(\mathrm{~mm})$ | 1000.00 | 1007.31 |
| RMS $(\mathrm{mm})$ | 0.57 | 1.49 |

For details on the alignment please refer to:

| HEC1C | Wheel on Assembly Table <br> HEC1C | ATL-AE-UR-0005 <br> ATL-AE-UR-0006 |
| :--- | :--- | :--- |
| HEC2C | Wheel on Assembly Table | ATL-AE-UR-0007 |
| HEC2C | Wheel vertical | ATL-AE-UR-0011 |
| HEC1A | Wheel on Assembly Table | ATL-AE-UR-0025 |
| HEC1A | Wheel vertical | ATL-AE-UR-0028 |
| HEC2A | Wheel on Assembly Table | ATL-AE-UR-0029 |
| HEC2A | Wheel vertical | (NOT YET DONE) |

## Inter-module Gaps

These are the gaps between the 32 modules that form the wheel. The nominal inter-module gap is 2 mm . A sample section of this table is given below. We will use the first column as our specimen entry.

| Cryostat/Wheel/Wheel <br> Location/Wedge1_2 |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| A/HEC1/Table/31_32A/HEC1/Table/32_1 | C/HEC1/T6/1_2 | C/HEC1/T6/2_3 |  |  |
| Cryostat | A | A | C | C |
| Wheel | HEC1 | HEC1 | HEC1 | HEC1 |
| Wheel_Cryostat | HEC1A | HEC1A | HEC1C | HEC1C |
| Wheel Location | Table | Table | T6 | T6 |
| Wedge 1 | 31 | 32 | 1 | 2 |
| Wedge 2 | 32 | 1 | 2 | 3 |
| Gap Top Inner | 1.45 | 1.27 | 2.68 | 2.15 |
| Gap Top Outer | 2.77 | 1.78 | 2.01 | 2.01 |
| Gap Bottom Inner | 2.16 | 1.81 | 1.81 | 2.46 |
| Gap Bottom Outer | 2.36 |  | 2.25 | 2.53 |

## Cryostat/Wheel/Wheel Location/Wedge1_2

Unique identifier for this table in the database, four wheel_cryostats, two locations, 32 gaps: 256 entries in this table.
Specimen value: A/HEC1/Table/31_32, where:
A : The A cryostat.
HEC1 : The front(1) HEC wheel.
Table : The measurements were made when the wheel was horizontal on the HEC wheel assembly table.
31_32 : The gap between the modules in the wheel at wedge locations 31 and 32. The nominal $\phi$ location of the centre of module in location $n$ is given by :

$$
\phi=2 \pi(n-0.5) / 32
$$

## Cryostat

A or C cryostat. The A end is nearest Geneva airport. Specimen value: A, where:
A : The A cryostat.

## Wheel

HEC1 is the front wheel, HEC2 is the rear wheel.

## Wheel_Cryostat

Specimen value: HEC1A, where:
HEC1A : The front(1) HEC wheel destined for the A cryostat.

## Wheel Location

Specimen value: Table, where:
Table : The measurements were made when the wheel was horizontal on the HEC wheel assembly table.

## Wedge 1

Specimen value: 31, where:
31 : The module on the first side of the gap is part of wedge 31.

## Wedge 2

Specimen value: 32 , where:
32 : The module on the second side of the gap is part of wedge 32.

## Gap Top Inner

Specimen value: 1.45 , where:
$1.45 \mathrm{~mm} \quad$ : The gap measured in mm at the inner radius of the wheel, between plates 1 (for a front wheel) or 26 (for a rear wheel) of the two adjacent modules.

## Gap Top Outer

Specimen value: 2.77, where:
$2.77 \mathrm{~mm} \quad$ : The gap measured in mm at the outer radius $(\sim 2.03 \mathrm{~m})$ of the wheel, between plates 1 (for a front wheel) or 26 (for a rear wheel) of the two adjacent modules.

## Gap Bottom Inner

Specimen value: 2.16, where:
$2.16 \mathrm{~mm} \quad$ : The gap measured in mm at the inner radius ( $\sim 475 \mathrm{~mm}$ ) of the wheel, between plates 25 (for a front wheel) or 42 (for a rear wheel) of the two adjacent modules.

## Gap Bottom Outer

Specimen value: 2.36, where:
$2.36 \mathrm{~mm} \quad$ : The gap measured in mm at the outer radius ( $\sim 2.03 \mathrm{~m}$ ) of the module, between plates 25 (for a front module) or 42 (for a rear module) of the two adjacent modules.

To give the reader a feeling for the variance in this value we have calculated the mean and RMS values. After ignoring null entries (where the position was not accessible), the mean and RMS for the entries is given in the table below.

|  | Gap Top Inner | Gap Top Outer | Gap Bottom Inner | Gap Bottom Outer |
| :--- | ---: | ---: | ---: | ---: |
| Average $(\mathrm{mm})$ | 1.72 | 1.78 | 1.77 | 1.62 |
| RMS $(\mathrm{mm})$ | 1.09 | 0.92 | 0.96 | 0.90 |

## Wheel Shim Details

The connecting bar that connects the adjacent modules together at the outer radius is a large flat bar. To marry this flat connecting bar to the many copper plates of the module which do not present a perfectly flat face, it was anticipated that shims would be used. One shim for each plate was anticipated. However it was found that these shims were not mechanically necessary, and as they were a potential source of metal material that can cause HV shorts, it was decided NOT to use them. We leave in the database the record of the measurements made to check that these shims were not required at any location. All these measurements were made on the wheel assembly table, prior to rotation.

| Cryostat/Wheel/Wedge1_2/PlateNumber | A/HEC1/4_5/10 | A/HEC1/4_5/11 |
| :--- | :---: | :---: |
| Cryostat | HEC1 | A |
| Wheel | HEC1A | HEC1 |
| Wheel_Cryostat | 4 | 4 |
| Wedge 1 | 5 | 5 |
| Wedge 2 | 10 | 11 |
| Plate Number | 0.718 | 0.656 |
| Shim Thickness Required | 0 | 0 |
| Installed Shim Thickness |  |  |

## Cryostat/Wheel/Wedge1_2/PlateNumber

Unique identifier for this table in the database. Two cryostats, two wheels, 32 wedges, and 41 plates/wheel pair (no shim on plate 1): 2624 entries in this table.
Specimen value: A/HEC1/4_5/10, where:
A : The A cryostat
HEC1 : The front(1) HEC wheel.
4_5 : The measurements were made when the wheel was horizontal on the HEC wheel assembly table between modules locations 4 and 5 .
20 : This is the shim measurement for plate \# 10 (plate \#'s go from 1 to 42)

## Cryostat

Specimen value: A where:
A : Wheel destined for the A cryostat.

## Wheel

Specimen value: HEC1 where:
HEC1 : Front HEC wheel.

## Wheel_Cryostat

Specimen value: HEC1A where:
HEC1A : Front HEC wheel destined for the A cryostat.

## Wedge 1

Specimen value: 4 where:
4
:Wedge location. Connecting bar goes between the module in wedge location 4 and that specified in wedge 2.

## Wedge 2

Specimen value: 5 where:
5 : Wedge location. Connecting bar goes between the module in wedge location 5 and that specified in wedge 1 .

## Plate Number

Specimen value: 10 where:
10 : Plate number for which spacer thickness required is being measured.

## Shim Thickness Required

Specimen value: 0.718 where:
$0.718 \mathrm{~mm} \quad$ : Required spacer thickness in mm
Note that positive (negative) spacer thickness implies a spacer is required under the connecting bar on the $\mathrm{n}+1(\mathrm{n})$ module side.

## Installed Shim Thickness

Specimen value: 0 where:
0.0 mm : Spacer thickness used in mm. The spacer thickness installed is always zero, because no spacers were installed.

The mean spacer thickness required was -0.036 mm , the average spacer thickness was 0.50 mm .

## 2. ELECTRICAL TABLES

Wheel Electrical Summary
PSB Locations
PSB Performance Summary
Module Locations

## Wheel Electrical Summary

This table provides a précis of HV problems encountered. Amplifier PSB boards were installed on modules during the final steps prior to wheel assembly, so these are the first tests with the final amplifiers present.

| Cryostat/Wheel/Wedge | A/HEC1/1 | A/HEC1/2 |
| :--- | :--- | :--- |
| Cryostat | A | A |
| Wheel | HEC1 | HEC1 |
| Wedge | 1 | 2 |
| Cryostat/Wedge | A/1 | A/2 |
| Wheel_Cryostat | HEC1A | HEC1A |
| Module Serial Number | AF21 | AF14 |
| HV test Passed ? | TRUE | TRUE |
| Did HV problems have to be addressed? | TRUE | TRUE |
| Comment on HV fixes | ET:EST1, gap 11-HV off | 3 trips at 900 V |
| Other Comments |  |  |
| Date of Final Check | 18-Feb-03 | $20-$ Feb-03 |

## Cryostat/Wheel/Wedge

Unique identifier for this table, four wheel_cryostat and 32 wedges: 128 entries in this table.

## Cryostat

A or C cryostat initially intended, for installation in the A or C end of ATLAS. The A end is nearest Geneva airport.
Wheel
HEC1 is the front wheel, HEC2 is the rear wheel.

## Wedge

This refers to the wedge location $n$ of the module in the wheel. The nominal $\phi$ location of the centre of module in location $n$ is given by :

$$
\phi=2 \pi(n-0.5) / 32
$$

## Cryostat/Wedge

Identifier to connect to the PSB location table.

## Wheel_Cryostat

Identifier to connect to the Module Location table.

## Module Serial Number

This has the typical format CF04, where:

- The C refers to the wheel (C or A) that the module was nominally built for. Two initially special, but actually standard series modules, SF01 and SF02 were also built.
- The F refers to the module being a Front module. Only F (Front) and R (Rear) modules were produced. Front modules have plate numbers 1 to 25 and rear 26 to 42 . Front modules have gaps (layers) 1 to 24 and rear 25 to 40 .
- 04 refers to the number of that series module 01 to 33

This number is written on the module, on the rear copper plate at the outer radius.

## HV test Passed ?

By definition .TRUE. otherwise the module was rejected!

## Did HV problems have to be addressed?

TRUE if problems were encountered. Then the next field should describe the actions taken to overcome the problem(s).

## Comment on HV fixes

In free format here are described any problems that have to be overcome to obtain HV test passed status.

## Other Comments

Free format field to encourage useful information to be entered.

## Date of Final Check

This would point you to the logbook entry for this action.

## PSB Locations

| Cryostat/Wedge | A/1 | A/10 | A/11 |
| :--- | :--- | :--- | :--- |
| PSB A Serial | A51 | A11 | A69 |
| PSB B Serial | B48 | B60 | B70 |
| PSB C Serial | C57 | C44 | C68 |
| PSB D Serial | D49 | D06 | D73 |
| PSB E Serial | E45 | E65 | E64 |

## Cryostat/Wedge

Unique identifier for this table, with two cryostats and 32 wedges this table has 64 entries.

## PSB A Serial Number

The serial number of the printed circuit board (PSB) containing the pre-amplifiers and summing circuit, installed at the outer radius of the HEC $1(\sim 2 \mathrm{~m}$ radius) in the front position of the 3 PSB boards at this location. This board serves gaps 1-8.The A PSB boards are closest to the EMEC. (24 Channels on this board). See Fig. 7 and Appendix I.

## PSB B Serial Number

The serial number of the printed circuit board (PSB) containing the pre-amplifiers and summing circuit, installed at the outer radius of the HEC $1(\sim 2 \mathrm{~m}$ radius) in the middle position of the 3 PSB boards at this location. This board serves gaps 9-24 outer radius ( $\eta<1.9$ ) readout locations. (8 Channels on this board). See Appendix I.

## PSB C Serial Number

The serial number of the printed circuit board (PSB) containing the pre-amplifiers and summing circuit, installed at the outer radius of the HEC $1(\sim 2 \mathrm{~m}$ radius) in the rear position of the 3 PSB boards at this location. This board serves gaps 9-24 inner radius ( $\eta>1.9$ ) readout locations. (15 Channels on this board) . See Appendix I.

## PSB D Serial Number

The serial number of the printed circuit board (PSB) containing the pre-amplifiers and summing circuit, installed at the outer radius of the HEC $2(\sim 2 \mathrm{~m}$ radius) in the front position of the 2 PSB boards at this location. This board serves gaps 25-32 readout locations. (23 Channels on this board). See Appendix I

## PSB E Serial Number

The serial number of the printed circuit board (PSB) containing the pre-amplifiers and summing circuit, installed at the outer radius of the HEC $2(\sim 2 \mathrm{~m}$ radius) in the rear position of the 2 PSB boards at this location. This board serves gaps 33-40 readout locations. (24 Channels on this board). See Appendix I.

PSB 1 (LSEG 1)


## Figure 8:

Diagram of the PSB type A. Shown are many of the terms used in the Signal Quadrant Wiring Table. Further PSB diagrams are in ApendixII

## Module Locations

|  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Cryostat/Wheel/Wedge | A/HEC1/1 | A/HEC1/10 | A/HEC1/11 | A/HEC1/12 |
| Cryostat | A | A | A | A |
| Wheel | HEC1 | HEC1 | HEC1 | HEC1 |
| Wheel_Cryostat | HEC1A | HEC1A | HEC1A | HEC1A |
| Wedge | 1 | 10 | 11 | 12 |
| Module Serial Number | AF21 | CF23 | CF22 | AF15 |

This table connects this wheel assembly database with the database that describes the 128 modules that make up the four wheels. This is done through the serial number of the modules. The items in this table have already been described in the description of the mechanical detail tables. For completeness we give below the reference drawings of the locations of the modules in the four wheels.



## PSB Performance Summary

## Overview:

One HEC wedge is equipped with 5 PSBs:

| Amplifier Table <br> PSB type | A | B | C | D | E |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HEC Segment | Gaps1-8 | Gaps 9-24, <br> pads 1-8 | Gaps 9-24, <br> pads 9-23 | Gaps 25-32 | Gaps 33-40 |
| Quadrant Cabling Table <br> PSB type | 1 | $2-1$ | $2-2$ | 3 | 4 |

Table 1: PSB labeling conventions.
The production volume was 75 PSBs of each type. All PSBs are named like "A23", where " $A$ " is the PSB type, " 23 " is the serial number.

The PSB's A00, A01, A02, B01, B02, C00, C02, D00, D01, E00, E01 are "reference" PSBs, they were not used for HEC modules, so they are not included into data base.

During the QC tests, the main parameters of all preamplifiers were measured. A PSB passed the QC tests if all parameters were within the specified window. A summary of these parameters is given in the database. A review of the tests undertaken is given in: http://atlas.web.cern.ch/Atlas/GROUPS/LIQARGSTORE/HEC Calo/QC/Series.Production/PRR/QCDocu ments/MPI/elqc2000.pdf

Two pads are connected to every amplifier. So for instance 4 amplifiers are used to produce the signal for gaps 1-8, with gaps $1-2$, gaps $3-4$, gaps $5-6$, and gaps $7-8$ connected to them.

Given below are some typical values from this table. In what follows we will use the first row of this table as our specimen value.

| PSB <br> Serial/Tower | PSB Serial | Tower | \# Amplifiers in Tower | \% Non- <br> Linearity | Average Transfer Coefficient $\mathrm{k} \Omega$ | \% Uniformity of Preamplifier Gains | RMS <br> Noise ( mV ) at Nominal $\qquad$ | RMS Noise ( mV ) at High $\mathrm{V}_{\text {ee }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A06/1 | A06 | 1 | 8 | 0.76 | 0.74 | 1.62 | 0.52 | 0.58 |
| A06/2 | A06 | 2 | 8 | 0.82 | 0.70 | 0.96 | 0.55 | 0.53 |
| A06/3 | A06 | 3 | 8 | 0.85 | 0.72 | 1.53 | 0.47 | 0.59 |
| A06/4 | A06 | 4 | 8 | 0.87 | 0.73 | 1.56 | 0.48 | 0.43 |
| A06/5 | A06 | 5 | 4 | 0.68 | 0.77 | 0.69 | 0.53 | 0.55 |
| A06/6 | A06 | 6 | 4 | 0.61 | 0.73 | 0.99 | 0.65 | 0.59 |
| A06/7 | A06 | 7 | 4 | 0.89 | 0.78 | 1.45 | 0.56 | 0.73 |

## PSB Serial/Tower

Unique identifier for this table in the database. This table includes some spare amplifiers. There are typically about 67 amplifiers of each type ( 64 are required) and about 19 towers on average per
amplifier (A:24, B:8, C:15, D:23, E:24), total entries should be about 6000 entries in total. There are 6097 entries.
Specimen value: A06/1, where:
A06 : PSB board serial number as described above
1 : Tower number from 1 to 24 (at most)

## PSB Serial

Specimen value: A06, where:
A06 : PSB board serial number as described above

## Tower

Specimen value: 1 , where:
1 : Tower number from 1 to 24 (at most)
See Figure 8 for the definition of these tower numbers.

## \# Amplifiers in Tower

Specimen value: 8 , where:
8 : Number of amplifiers in tower (between 2 and 16)

## \% Non-Linearity

Specimen value: 0.76, where:
0.76 : Non-linearity in $\%$, measured when varying the input current from 0 to 1 mA The definition of the linearity was that the input current was varied from 0 to 1 mA ( 15 points), then the 15 points fit with linear $(\mathrm{y}=\mathrm{ax})$ function. Then the non-linearity is just the percentage deviation of the point furthest from the fitted line.


## Average Transfer Coefficient kOhm

Specimen value: $0.74 \mathrm{k} \Omega$, where:
$0.74 \mathrm{k} \Omega$ : The average transfer coefficient of this set of $n$ amplifiers ( $n=$ \# Amplifiers in Readout Channel).

\% Uniformity of Preamplifier Gains
Specimen value: 1.62, where:
1.62 : The difference between the maximum and minimum $\%$ amplifier gain of this set of $n$ amplifiers ( $n=$ \# Amplifiers in Readout Channel).


## RMS Noise (mV) at Nominal $V_{e e}$

Specimen value: 0.52 , where:
0.52 : The RMS noise $(\mathrm{mV})$ when using the standard $\mathrm{V}_{\mathrm{ee}}=-1.5 \mathrm{~V}$


## RMS Noise (mV) at High $V_{\text {ee }}$

Specimen value: 0.58 , where:
0.58 : Is the RMS noise ( mV ) when using the high $\mathrm{V}_{\mathrm{ee}}=-1.8 \mathrm{~V}$


## 3. CABLING TABLES

Quadrant Signal and Calibration Cabling

| Cryostat/Qwedge/PSB_letter/Pad/SubZ | A/1/C/P19/2 |
| :---: | :---: |
| Cryostat/Qwedge/PSB_letter/Tower | A/1/C/19 |
| Cryostat | A |
| Qwedge | 1 |
| PSB Letter | C |
| Tower | 19 |
| Pad | P19 |
| Gap | 10-16 |
| Gap_new | 17 to 24 |
| ETA | 11 |
| PHI | 1 |
| PHI_letter | A |
| Z | 2 |
| SubZ | 2 |
| PSB | 2-2 |
| INCON | 11 |
| INPIN | 5-8 |
| OUTCON | 3 |
| OUTPIN | 3 |
| Signal Patch Panel Input Connector | 2 |
| Signal PP Input Connector Pin | 6 |
| Signal Patch Panel Output Connector | 6 |
| Signal PP Output Connector Pin | 3 |
| Signal Patch Panel | 9 |
| Cold flange pigtail Connector Pin | 18 |
| Feedthrough Connector Number | 9A |
| Front End Board Number | 5 |
| Front End Crate SLOT | 30 |
| Front End Board Connector | J1 |
| FEB input connector pin | A24 |
| FEB Shaper Channel Number | 17 |
| FEB ADC Number | 3 |
| FEB ADC Channel | 2 |
| FEB Output connector pin | A9 |
| Trigger Driver Board Number | 2 |
| Trigger Driver Channel | 48 |
| Trigger Driver input connector | 2 |
| Trigger Driver input connector pin | 9 |
| Trigger Driver output connector | 7 |
| Trigger Driver output connector pin | 1 |
| Calibration Generator Channel | 11 |
| Calibration Feedthrough connector \# | 12A |
| Calibration lines of Wedges | 11 |
| Calibration Patch Panel Number | 1 |
| Calibration PP Input Connector \# | 2 |
| Calibration PP Input Connector Pin \# | 3 |
| Calibration PP Output Connector \# | 2 |
| Calibration PP Output Connector Pin \# | 1 |
| Calibration distribution board on wheel | FRONT |
| Distribution board Input Connector | 6 |
| Distribution board Input Connector Pin | 1 |
| Distribution Board Output Connector | 3 |
| Distribution Board Output Connector Pin | 4 |
| Strip-line Type | 16/B |

Each HEC calorimeter wedge has 5 PSB boards, three on the front wheel (1, 2-1, 2-2) and two on the rear wheel $(3,4)$ (see table 1, page 25). They correspond to the 4 longitudinal readout depths ( $\mathrm{Z}=1$ to 4 ). The PSB boards have 3 output connectors. Signals from the outer psuedo-rapidity $\eta$ region are collected at PSB OUTCON 1 (ETA=2-5), those from the middle psuedo-rapidity $\eta$ region at PSB OUTCON 2 (ETA=6-9), and those from the inner region (ETA $=10-15$ ) at PSB OUTCON 3 . Signals from 2 neighbouring wedges are transfered to patch panels with Harness A cables. There are 12 patch panels in a quadrant, four for each psuedo-rapidity $\eta$ region:

- P1, P2, P3, P4 - ETA=2-5 (OUTCON=1);
- P5, P6, P7, P8 - ETA=6-9 (OUTCON=2);
- P9, P10, P11, P12 - ETA=10-15 (OUTCON=3).

Harness B (Pigtail) cables serve to connect the patch panels with the feedthroughs. At the patch panel end they have 8 ( 8 signal pin) MPI connectors J1 to J8, at the cold feedthrough end an ATI connector (64 signal pin) . Diagrams of patch panel connectors are shown in Appendix I. Connectors positoning at the HEC feedthrough warm flange and their mapping to FEC slots are shown in the figure below and Fig.?? .

Feedthrough connectors (FT) column A are connected with FEB input connector J1 (FEB channel 1 - 64), those of column B - with FEB input connector J3 (FEB channel 65 - 128).

## HEC FEEDTHROUGH WARM FLANGE



For FT column A the FEB channel number is equal to the ATI_Pin number and for FT column B the FEB channel number is equal to ATI_Pin number plus 64 . The shaper channel number is equal to the FEB channel number minus 1 .
There are 16 ADC's in the FEB. Each serves 8 channels. ADC $1-8$ belongs to FEB channels $1-64$, while ADC $9-16$ belongs to FEB channels $65-128$.
FEB connector J2 serves to transfer trigger sums from shaper mixer outputs to the baseplane.
Two trigger driver boards ( $\mathrm{TDr}=1$ and $\mathrm{TDr}=2$ ) are used to transfer trigger sums to reciever.
Cleland notations for TDr pins and channels are used (W.E.Cleland. Layer Sum Boards for the ATLAS Liquid Argon Calorimeters. EDMS Document ATL-AL-EN-0019)

《 $\quad \infty$


EMEC＋HEC FRONT END CRATE
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There is one calibration board (128 channels) in a quadrant. 16 generators are used for calibration of one wedge using 6 for the rear and 10 for a front module:

- Cal_Gen $=(1-6)+($ QWedge -1$) \times 16$ for rear module
- Cal_Gen $=(7-16)+($ QWedge-1 $) \times 16$ for front module

Initially there were two tables in the data base: EC_A_upd and EC_C_upd for the quadrant of end cap A and C respectively. They differed in 2 columns: Wedge and PHI. Both items are reversed for EC_C_upd compared to EC_A_upd. For simplicity these two tables have been combined in this database. The column Cryostat has been added to allow these tables to be appended to each other.

The calibration lines are arranged in such a way as to be able to calibrate the calorimeter with the minimum number of lines. To avoid signal saturation at the summing stage of amplifiers different calibration generators for different parts of readout channels formed with more than the normal 8 pads (such as tower 5 in the gaps $9-24$ depth, which is composed of 165 a pads and 165 b pads). Hence regions where tiles are split (into a and b) and/or the depth is 16 liquid argon gaps not the more normal 8, are calibrated by two or four independent calibration lines.

## Quadrant Signal and Calibration Cabling Table Entries:

## Cryostat/QWedge/Z/Sub_Z/Pad:

This is the unique identifier for this table. Cryostat is either A or C. QWedge (described below) goes from 1 to 8 . Z (described below) goes from 1 to 4 , and combines with Sub_Z (1 or 2) to give the possibility of two entries for each $Z=2$ entry. Pad (described below) is the descriptor for each type of pad in a HEC wedge. Table 3 lists all entries per wedge. At the bottom of table 3 the entries are summed. There are 28 Z $=1$ SubZ $=1$ entries, $27 Z=2$ SubZ $=1$ entries, $25 Z=2$ SubZ $=1$ entries, $25 Z=3$ SubZ $=1$ entries, 22 $Z=4$ SubZ $=1$ entries, giving at total of 127 entries in total per wedge. In addition there are 9 redundant entries (cables present but not attached to towers, denoted by SubZ $=0$ ) in this table per wedge. So in total there are 136 entries per wedge, giving with 8 wedges per quadrant and two cryostats: 2176 entries in this quadrant table.

## Cryostat/Qwedge/PSB_letter/Tower:

This is the entry to connect to the table with one entry per signal line. There can be up to four lines in this table for a line in the signal summary table.

## Cryostat:

A or C cryostats.

## QWedge:

A wedge is the combination of a front and rear HEC module. It has a $\varphi$ width of $2 \pi / 32$ radians. Eight wedges make a quadrant. Thus the value of quadrant wedge QWedge goes between $1-8$ in a quadrant. QWedge number increases with increasing $\varphi$.

## PSB Letter:

A letter between A and E, denoting the type of PSB board.

## Pad:

All the pads are labeled according to the notation on page 287, ATLAS Liquid Argon TDR (reproduced below in Figure 7). A typical value is P1A, where P stands for PAD and 1a is the label on the drawing. 1 is the lowest psuedo-rapidity pad, and 24 is the highest psuedo-rapidity pad (having psuedo-rapidity $=3.2$ as its nominal high psuedo-rapidity boundary).

## Gap:

Within each Z region the tiles are readout in pairs. The first pair in a Z region is called channel 2 , the second pair channel 4 etc.. The notation used by the gap identifier is the first pair channel dash last pair channel. Allowed values are: 2-4, 2-8, and 10-16. So for instance:

- $\mathrm{Z}=1, \mathrm{Gap}=2-8$ corresponds to gap_new 1 to 8 .
- $\mathrm{Z}=2$, $\mathrm{Gap}=2-8$ corresponds to gap_new 9 to 16 .
- $Z=2$, Gap $=10-16$ corresponds to gap_new 17 to 24 .
- $\mathrm{Z}=3$, Gap $=2-4$ corresponds to gap_new 25 to 28 . (see for instance pad P3 in table 2)

Gap_new:
The liquid argon filled gaps between the copper plates in the HEC are numbered from front to rear: 1 to 40. Gaps 1 to 24 are in the front wheel, and 25 to 40 in the rear wheel. In this database numbers of gaps summed to make towers or sub-towers are given. Allowed values are: 1 to 8,9 to 16,17 to 24,25 to 28,25 to 32,33 to 36 , and 33 to 40 .


Figure 9: Definition of the pads of the readout electrodes, as given in the ATLAS Liquid Argon TDR, Figure 8-5.

## ETA:

ETA is a number between 2 and 15 . Below is a lookup table (table 1) between this ETA number and the nominal range of psuedo-rapidity the entry lies within. This number indicates which output connector is used from the PSB board for this entry.

## PHI:

For the inner tiles where there is only one tile across the whole module (pads 21 to 24 ) this number is equal to wedge. Where the module is two tiles wide (pads 1 to 20) it is twice wedge if the tile is on the high $\varphi$ side of the module, and it is twice wedge minus one if it is on the low $\varphi$ side of the module

| ETA | Nominal Pseudo-Rapidity |  |
| :---: | :---: | :---: |
|  | Low Edge | High Edge |
| 2 | 1.50 | 1.60 |
| 3 | 1.60 | 1.70 |
| 4 | 1.70 | 1.80 |
| 5 | 1.80 | 1.90 |
| 6 | 1.90 | 2.00 |
| 7 | 2.00 | 2.10 |
| 8 | 2.10 | 2.20 |
| 9 | 2.20 | 2.30 |
| 10 | 2.30 | 2.40 |
| 11 | 2.40 | 2.50 |
| 12 | 2.50 | 2.70 |
| 13 | 2.70 | 2.90 |
| 14 | 2.90 | 3.10 |
| 15 | 3.10 | 3.20 |

Table 2: Look-up between the Offline Identifier ETA, and the nominal psuedo-rapidity range of tiles with that ETA.

|  |  |  | Nominal warm position |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Relative to front face <br> HEC Module | Relative to ATLAS <br> interaction Point |  |  |
| Z | Gap | Gap_new |  | Last Gap | First Gap | Last Gap |
|  |  |  |  | (mm) | (mm) | (mm) |
| 1 | $2-8$ | 1 to 8 | 16.75 | 251.25 | 4293.75 | 4528.25 |
| 2 | $2-8$ | 9 to 16 | 284.75 | 519.25 | 4561.75 | 4796.25 |
| 2 | $10-16$ | 17 to 24 | 552.75 | 787.25 | 4829.75 | 5064.25 |
| 3 | $2-4$ | 25 to 28 | 29.25 | 204.75 | 5163.25 | 5338.75 |
| 3 | $2-8$ | 25 to 32 | 29.25 | 438.75 | 5163.25 | 5572.75 |
| 4 | $2-4$ | 33 to 36 | 497.25 | 672.75 | 5631.25 | 5806.75 |
| 4 | $2-8$ | 33 to 40 | 497.25 | 906.75 | 5631.25 | 6040.75 |

Table 3: Nominal warm z position of the centre of the first and last readout gap in each Z/Gap volume. Note these are nominal positions that do not allow for the several centimetre setback of the end caps from their nominal design positions, nor for the thermal shrinkage during cool down.

| Pad | ETA | Psuedo-Rapidity |  | PHI | Z |  |  |  | Gaps |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Low | High | (A End) | 1 | 2 | 3 | 4 | $\begin{gathered} 1 \text { to } 8 \\ \text { SubZ }=1 \end{gathered}$ | $\left.\begin{gathered} 9 \text { to } 16 \\ \text { SubZ }=1 \end{gathered} \right\rvert\,$ | $\left\lvert\, \begin{aligned} & 17 \text { to } 24 \\ & \text { SubZ } 24 \end{aligned}\right.$ | $\begin{array}{\|l\|} 25 \text { to } 28 \\ \text { SubZ }=1 \\ \hline \end{array}$ | $\left\|\begin{array}{c} 29 \text { to } 32 \\ \text { SubZ }=1 \end{array}\right\|$ | $\left.\begin{aligned} & 33 \text { to } 36 \\ & \text { SubZ }=1 \end{aligned} \right\rvert\,$ | $\left\|\begin{array}{l} 37 \text { to } 40 \\ \text { SubZ }=1 \end{array}\right\|$ |
| P1A | 2 | 1.5 | 1.6 | 2 wedge-1 | x |  |  |  | 1 |  |  |  |  |  |  |
| P1B | 2 | 1.5 | 1.6 | 2 wedge-1 | x |  |  |  | 1 |  |  |  |  |  |  |
| P1 | 2 | 1.5 | 1.6 | 2 wedge-1 |  | x |  |  |  | 1 |  |  |  |  |  |
| P2A | 2 | 1.5 | 1.6 | 2 wedge | x |  |  |  | 1 |  |  |  |  |  |  |
| P2B | 2 | 1.5 | 1.6 | 2 wedge | x |  |  |  | 1 |  |  |  |  |  |  |
| P2 | 2 | 1.5 | 1.6 | 2 wedge |  | x |  |  |  | 1 |  |  |  |  |  |
| P3A | 3 | 1.6 | 1.7 | 2 wedge-1 | x | x |  |  | 1 | 1 | 1 |  |  |  |  |
| P3B | 3 | 1.6 | 1.7 | 2 wedge-1 | x | x |  |  | 1 | 1 | 1 |  |  |  |  |
| P3 | 3 | 1.6 | 1.7 | 2 wedge-1 |  |  | x |  |  |  |  | 1 |  |  |  |
| P4A | 3 | 1.6 | 1.7 | 2 wedge | x | x |  |  | 1 | 1 | 1 |  |  |  |  |
| P4B | 3 | 1.6 | 1.7 | 2 wedge | x | x |  |  | 1 | 1 | 1 |  |  |  |  |
| P4 | 3 | 1.6 | 1.7 | 2 wedge |  |  | x |  |  |  |  | 1 |  |  |  |
| P5A | 4 | 1.7 | 1.8 | 2 wedge-1 |  | $x$ | x |  |  | 1 | 1 | 1 | 1 |  |  |
| P5B | 4 | 1.7 | 1.8 | 2 wedge-1 |  | x | x |  |  | 1 | 1 | 1 | 1 |  |  |
| P5 | 4 | 1.7 | 1.8 | 2 wedge-1 | x |  |  | x | 1 |  |  |  |  | 1 |  |
| P6A | 4 | 1.7 | 1.8 | 2 wedge |  | x | x |  |  | 1 | 1 | 1 | 1 |  |  |
| P6B | 4 | 1.7 | 1.8 | 2 wedge |  | x | x |  |  | 1 | 1 | 1 | 1 |  |  |
| P6 | 4 | 1.7 | 1.8 | 2 wedge |  |  |  | x | 1 |  |  |  |  | 1 |  |
| P7A | 5 | 1.8 | 1.9 | 2 wedge-1 |  |  | x | x |  |  |  | 1 | 1 | 1 | 1 |
| P7B | 5 | 1.8 | 1.9 | 2 wedge-1 |  |  | x | x |  |  |  | 1 | 1 | 1 | 1 |
| P7 | 5 | 1.8 | 1.9 | 2 wedge-1 | x | x |  |  | 1 | 1 | 1 |  |  |  |  |
| P8A | 5 | 1.8 | 1.9 | 2 wedge |  |  | x | x |  |  |  | 1 | 1 | 1 | 1 |
| P8B | 5 | 1.8 | 1.9 | 2 wedge |  |  | x | x |  |  |  | 1 | 1 | 1 | 1 |
| P8 | 5 | 1.8 | 1.9 | 2 wedge | x | x |  |  | 1 | 1 | 1 |  |  |  |  |
| P9 | 6 | 1.9 | 2 | 2 wedge-1 | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P10 | 6 | 1.9 | 2 | 2 wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P11 | 7 | 2 | 2.1 | 2 wedge-1 | x | $x$ | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P12 | 7 | 2 | 2.1 | 2 wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P13 | 8 | 2.1 | 2.2 | 2 wedge-1 | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P14 | 8 | 2.1 | 2.2 | 2 wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P15 | 9 | 2.2 | 2.3 | 2 wedge-1 | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P16 | 9 | 2.2 | 2.3 | 2 wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P17 | 10 | 2.3 | 2.4 | 2 wedge-1 | x | x | X | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P18 | 10 | 2.3 | 2.4 | 2 wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P19 | 11 | 2.4 | 2.5 | 2 wedge-1 | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P20 | 11 | 2.4 | 2.5 | 2 wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P21 | 12 | 2.5 | 2.7 | Wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P22 | 13 | 2.7 | 2.9 | Wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P23 | 14 | 2.9 | 3.1 | Wedge | x | x | x | x | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| P24 | 15 | 3.1 | 3.2 | Wedge | x |  |  | x | 1 |  |  |  |  | 1 | 1 |
|  |  |  |  |  |  |  |  | UM | 28 | 27 | 25 |  | 5 | 2 | 2 |

Table 4: Description of all entries for a wedge in the Signal and Calibration Table.

## PHI_letter:

This is the same as PHI except the notation instead of being from 1 to 16 is from A to P . $\mathrm{PHI}=1$ is equivalent to PHI_letter=A. This letter along with ETA defines the Trigger Towers in "Colas-Clelend notation". (W.E.Cleland. Layer Sum Boards for the ATLAS Liquid Argon Calorimeters.
EDMS Document ATL-AL-EN-0019)

## Z:

This is the readout depth. $Z=1$ is the readout depth gaps $1-8, Z=2$ is the readout depth gaps $9-24, Z=3$ is the readout depth gaps $25-32, \mathrm{Z}=4$ is the readout depth gaps $33-40$. See table 2 for conversion from Z to nominal position in ATLAS in mm.

## SubZ :

This is 1 for all entries except:

- For entries with $\mathrm{Z}=2$ where it is 1 for the gaps 9-16 and 2 for gaps 17-24.
- For entries where the cable is not connected to a tower it is set to 0 .


## PSB:

Pre-amplifier and summing board (PSB) type used. Allowed values are : 1, 2-1, 2-2, 3, 4. Where 1, 2-1, 22 are on the front wheel and 3 and 4 are on the rear wheel. PSB n contains the amplifiers for readout depth n. PSB boards 2-1 and 2-2 are used for readout depth 2 (inner and outer regions). (See Appendix I)

## INCON:

PSB input connector ( value 1 to 15 ).

## INPIN:

PSB input connector pin this has a notation of the type: 1-2, 1-4, 5-6 and 5-8. Each of these represents a set of pins: 5-8 means pins $5,6,7$, and 8 are used. Connected to each pin are a pair of readout pads. Each pin has an amplifier attached to it. Inside the PSB the various signals from the various pad pairs that make up a readout tower are summed and the anologue signal is sent out on a single output pin. As an example of this pin assignment notation in table 4 below we take tower 7 in the third readout depth where we sum pads 7 a and 7 b for gaps 25 to 32 .

## OUTCON:

PSB output connector ( value 1 to 3 ).

## OUTPIN:

PSB output connector pin (1 to 8)

## Tower:

This is the tower as defined on page 287 Figure 8-5 of the TDR (or the number in the Pad entry defined above). Note at this point in the readout chain divided pads such as 2 a and 2 b have been summed to provide a single tower (number 2 in the case of 2 a and 2 b ). The tower can be derived from OUTCON and OUTPIN by:

Tower $=8($ OUTCON-1 $)+$ OUTPIN
Except in the case of PSB readout channels, 22 and 23 where the output pin is switched, so:
Tower 22 is connected to OUTCON 3 and OUTPIN 7
Tower 23 is connected to OUTCON 3 and OUTPIN 6
This switching of the OUTPIN for these two pads was required due to engineering constraints in the layout of the PSB board and the mechanical design of the HEC modules (that did not allow all even numbered pads to be on the wiring harness on one side of the module and all odd numbered on the other side).

| Pad | Gap | Input Pin Number | INCON | INPIN | OUTCON | OUTPIN | Tower |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7a | 25 | 1 | 1 | 1-4 | 1 | 7 | 7 |
| 7 a | 26 |  |  |  |  |  |  |
| 7a | 27 | 2 |  |  |  |  |  |
| 7a | 28 |  |  |  |  |  |  |
| 7a | 29 | 3 |  |  |  |  |  |
| 7a | 30 |  |  |  |  |  |  |
| 7a | 31 | 4 |  |  |  |  |  |
| 7a | 32 |  |  |  |  |  |  |
| 7b | 25 | 5 |  | 5-8 |  |  |  |
| 7b | 26 |  |  |  |  |  |  |
| 7b | 27 | 6 |  |  |  |  |  |
| 7b | 28 |  |  |  |  |  |  |
| 7b | 29 | 7 |  |  |  |  |  |
| 7b | 30 |  |  |  |  |  |  |
| 7b | 31 | 8 |  |  |  |  |  |
| 7b | 32 |  |  |  |  |  |  |

Table 5: Example of how a readout tower is summed in the PSB board. Here we give the information for pad 7 that, for amplifier noise reasons, is split into two pads (7a and 7b) on the pad board.

## Signal Patch Panel input connector (1-4) (LS)

## Signal Patch Panel input connector pin (1-8) (LS_Pin)

Signal Patch Panel output connector (1-8) (JF)
Signal Patch Panel output connector pin (1-8) (JF_Pin)
Signal Patch Panel (1-12) (PP) See Appendix I
Cold flange (Pig tail) connector pin (1-64) (ATI_Pin)
Feedthrough connector number (A5-B10) (FT)
Front-End Board number (1-6) (FEB)
FEB input connector (J1 or J3) (FEB_Con)
FEB input connector pin (J_Pin)
FEB Shaper channel number ( 0 - 127) (Shaper)
FEB ADC number (1-16) (ADC)

FEB ADC channel number $(1-8)(\mathrm{ADC} C h)$
FEB Output connector pin For trigger sums signals (A1-C32) (J2_Pin)
Trigger driver board number (1-2) (TDr)
Trigger driver channel (0-95) (TDr_Ch)
Trigger driver input connector (1-3) (TINC)
Trigger driver input connector pin (1-96) (TINP)
Trigger driver output connector (4-9) (TOUC)
Trigger driver output connector pin (1-16) (TOUP)
Calibration generator channel ( 1 - 128) (Cal_Gen)
Calibration feedthrough connector number (12A or 12B) (Cal_FT)
Calibration lines of wedge $(1-16)($ Cal_line $)$
Calibration patch panel number ( $1-2$ ) (Cal_PP)
Calibration patch panel input connector number ( $1-8$ ) (Cal_In)
Calibration patch panel input connector pin number ( $1-8$ ) (Cal_In_Pin)
Calibration patch panel output connector number (1-12) (Cal_Out)
Calibration patch panel output connector pin number (1-8) (Cal_Out_Pin)
Calibration distribution board on module (FRONT or REAR) (Cal_DB)
Distribution board input connector (5 or 6) (DB_In)

Distribution board input connector pin (1-8) (DB_In_Pin)
Distribution board output connector (1-4) (DB_Out_Pin)
Strip line type (1/A to 32/D) (Str_Line)

## HV Cabling Table

| Cryostat/Wedge/Z/SubGap | A/1/1/EST1 | A/1/1/EST2 | A/1/1/PAD1 | A/1/1/PAD2 |
| :--- | :--- | :--- | :--- | :--- |
| Cryostat/Wedge/Z | A/1/1 | A/1/1 | A/1/1 | A/1/1 |
| Cryostat/FT conn \#/Pin \# | A/0/2 | A/0/1 | A/0/3 | A/0/0 |
| Cryostat | A | A | A | A |
| SEG Module | 64 | 64 | 64 | 64 |
| Channel Number | 2 | 1 | 3 | 0 |
| Cable | ALL-POS-40 | ALL-POS-40 | ALL-POS-40 | ALL-POS-40 |
| Pin Number | 2 | 1 | 3 | 0 |
| FeedThrough | 0 | 0 | 0 | 0 |
| HV Patch Panel (Plug) | Q1-P1-J1 | Q1-P1-J1 | Q1-P1-J1 | Q1-P1-J1 |
| HV Patch Panel (Socket) | Q1_HV_P1 | Q1_HV_P1 | Q1_HV_P1 | Q1_HV_P1 |
| Wedge | 1 | 1 | 1 | 1 |
| Z | 1 | 1 | 1 | 1 |
| SubGap | EST1 | EST2 | PAD1 | PAD2 |
| Module Serial Number | AF21 | AF21 | AF21 | AF21 |
| Patch Panel Connector In | $1-1-1$ | $1-1-1$ | $1-1-1$ | $1-1-1$ |
| Patch Panel Pin In | 3 | 2 | 4 | 1 |
| Patch Panel Connector Out | J8 A | J8 A | J8 A | J8 A |
| Patch Panel Pin Out | C | B | D | A |
| Section of Module | Est1-Cell 1-8 | Est2-Cell 1-8 | Pad1-Cell 1-8 | Pad2-Cell 1-8 |

## Description

Two unique identifiers exist for each entry. The first defines the calorimeter volume served, the second the location of the pin on the cryostat serving this HV volume.

- The first unique identifier for this table is Cryostat/Wedge/Z/subgap, with 2 cryostats, 32 wedges, 4 Z depths and 4 subgaps, there are 1024 entries in this table. The table gives the wiring details for these lines.
- The second unique identifier for this table is Cryostat/HVfeedthrough/Pin, with 2 cryostats, 16 feedthroughs and 32 pins, there are 1024 entries in this table. The figures below define the locations of the pins and HV feedthroughs.

The entries for ISEG module and channel number are included for completeness but this is not the definitive definition of these. If for technical reasons these assignments are changed this database will not be changed. The database seeks only to define the items that will not change, in this case: feedthrough and pin number.


Figures Defining the HV feedthrough connectors and pins. The picture below defines the feedthroughs, note the direction to the interaction point. Also in the picture the notches can be seen on some of the connectors. The diagram to the left shows the pin definitions. Note the key location that goes into the notch.


Interaction Point

1. Cryostat/Wedge/Z/subgap

Unique Identifier (A or C / 1 to 32 / 1 to $4 / \mathrm{EST} 1, \mathrm{PAD} 1, \mathrm{PAD} 2$, or EST2)
2. Cryostat/Wedge/Z

As previous entry
3. Cryostat/FeedThrough Connector\#/Pin \#

A unique identifier for the table, useful for describing or locating nonconformances observed after the cryostat is closed.
4. Cryostat

A or C
5. ISEG Module

The module number assigned to this line in the initial HV setup.
6. Channel Number

The channel number within the ISEG module assigned to this line in the initial HV setup.
7. Cable

ALL-POS- followed by a 2 digit number
8. Pin Number

Number of pin in cable or Feedthrough (see diagram above)
9. Feedthrough

HV Feedthroughs are numbered 0-27 see photograph above.
10. HV Patch Panel (Plug)

What is written on the plug
11. HV Patch Panel (Socket)

What is written on the patch panel next to the socket
12. Wedge

EC wedge number (1-32)
13. Z

Z section of module (1-4)
14. Subgap
(4 possible values: EST1, PAD1, PAD2, or EST2)
15. Module Serial Number

Serial Number of calorimeter module as defined at production site. Only included for information. (128 possible values: $\mathrm{AF}(\mathrm{R}) 1-\mathrm{AF}(\mathrm{R}) 32, \mathrm{CF}(\mathrm{R}) 1-\mathrm{CF}(\mathrm{R}) 32$ )
16. HV patch panel number
$(1-4)$ per quadrant (HV PP)
17. HV patch panel connector in

Three number designator such as: 2-3-16
18. HV patch panel input connector pin

Number between 1 and 4
19. HV patch panel output connector

16 possible connectors: J1A - J8A, J1H - J8H
20. HV patch panel output connector pin

8 possible pins: A-H
21. Section of module
(16 possible values, such as Est1-Cell 1-8)

## Low Voltage Cabling Tables

| Cryostat/Wedge/PSB_letter/Voltage | A/1/A/Minus1.5V_GNDA/1/A/Minus1.5Volts |  |
| :--- | :---: | :---: |
| Cryostat/Wedge/PSB_letter | $\mathrm{A} / 1 / \mathrm{A}$ | $\mathrm{A} / 1 / \mathrm{A}$ |
| Cryostat | A | A |
| Quadrant | 1 | 1 |
| Wedge | 1 | 1 |
| PSB Letter | A | A |
| Function | 60 | Minus1.5V_GND |
| Q number | 1 | Minus1.5Volts |
| Q line | 1 | 59 |
| Q LV Channel | 1 | 1 |
| Q PB Connector | 4 | 1 |
| Q PB Connector Pin | 37 | 1 |
| FEC slot | 1 | 23 |
| FEC Input Connector | J | $\mathrm{C}-30$ |
| FEC Back Plane Connector | $\mathrm{C}-3$ | 1 |
| FEC Back Plane Connector Pin | 14 A | J |
| Warm FT Cable pin | 3 | A |
| Signal Feedthrough | $\mathrm{LV}-\mathrm{PP} 1$ | 14 A |
| ATI Pin | A 1 | 4 |
| Quadrant LV patch panel | $15-16$ | LV_PP1 |
| Quadrant LV patch panel input connector | $9-10$ | A1 |
| Quadrant LV patch panel in-connector pins | 1 | $1-2$ |
| Quadrant LV patch panel out-connector pins | A | $7-8$ |
| PSB | $9-10$ | 1 |
| PSB Letter repeated | 1 | A |
| PSB Pin | $7-8$ |  |
| Q Wedge | 1 |  |

The unique identifier for this table is: Cryostat/Wedge/PSB/Voltage. There are 2 cryostats, 32 wedges, 5 PSB per wedge, and 6 voltage lines per PSB. In addition there are two shield lines per wedge: 2048 entries in this table ( $2 \times 32 \times(5 \times 6+2)$ entries).
This table describes the wiring of the low voltages that power the PSB boards which are mounted on the modules in the liquid argon. These low voltages are supplied from a power supply box, feed into the front end crate (in slots 37 and 38), and then through the signal feedthroughs to the PSB's of the HEC.

Description.
One Power Box is used to supply low voltage to each HEC quadrant. Each Power Box has 40 Low Voltage Channels (a channel being a set of 3 voltages suitable for supplying one PSB), produced on 8 output connectors each with 5 channels. The Power Box output cables 1 to 4 are connected to four inputs of LV FEB1 (slot 37), cables 5 to 8 to those of LV FEB2 (slot 38). Outputs of FEB1 are connected with signal feedthrough (FT) 14A (J1) and FT 14B (J3), and those of FEB2 with FT15A (J1) and FT15B (J3). In the cold the LV pigtail has an ATI connector at the feedthrough end and 10 MPI connectors A1-E1, A2E2 at the patch panel end. Each HEC quadrant is equipped with 4 Low Voltage patch panels (LV PP) each of these serves two neighbouring wedges ( $W$ edge $=n, n+1$ ) For both End-Caps the connectors (A1-E1) belong to a wedge n, and (A2-E2) to wedge n+1. Connectors sets 1 and 2 are swapped at End Cap C patch panels. Two MS Excel tables were produced describing this situation for each end-cap: HEC_LV_A and

HEC_LV_C. These have only one difference: in the table HEC_LV_A LV PP is ordered by wedge number, while in the table HEC_LV_C LV PP is in the inverse order. During feedthrough cabling installation it was found that some swapped voltage and ground lines had been produced. Two new tables HEC_LV_A_new and HEC_LV_C_new with swapped voltage and ground lines were produced and are used in this database. In the list of items below the label used in these files for each entry is given in brackets.

## List of items:

1. Cryostat/Wedge/PSB_letter/Voltage

Unique identifier for this table
2. Cryostat/Wedge/PSB_letter

Identifier for location signal lines affected if this line is off.
3. Cryostat

A or C.
4. Quadrant

1 to 8
5. Wedge

1 to 32
6. PSB Letter

A to E
7. Function

Description of type of LV line this is, such as: Minus1.5V_GND
8. Q Number

Unique identifier within a quadrant ( 1-256 ordered by FEB_InC and ATI_Pin) (Num)
9. Q Line

Quadrant low voltage line number ( $1-128$ ) (Line)
10. Q LV Channel

Quadrant LV channel number ( 1-40 ) (LV_Chan)
11. Q PB Connector

Power Box Output Connector number ( $1-8$ ) (PB_Con)
12. Q PB Output Connector Pin

Quadrant Power Box Connector pin number ( A1 to C32 ) (PB_Con_Pin)
13. FEC Slot

LV Front End Board position in Front End Crate ( 37 or 38 ) (FEC Slot)
14. FEB Input Connector
( 1-4 ) (FEB_InC)
15. FEC Back Plane Connector
( FEB Output Connector J1 or J3 ) (BP_Con)
16. FEC Back Plane Connector pin
( A1-A32, C1-C32 ) (BP_Con_Pin)
17. Warm FT connector pin
(A1-A32, C1-C32 ) (Warm-Cable_Pin)
18. Signal Feedthrough
( 14A, 14B, 15A, 15B ) (FT)
19. ATI Pin

LV Pig Tail connector pin, Also signal feedthrough pin ( 1-64 ) (ATI_Pin)
20. Quadrant LV Patch Panel
(LV_PP1 - LV_PP4 ) (LV PP)
21. Quadrant LV Patch Panel input connector
( A1-E1, A2-E2 ) (PP_InC)
22. Quadrant LV Patch Panel input connector pin
( 1-16) PP_InC_Pin
23. Quadrant $\overline{\mathbf{L} V} \overline{\text { Patch Panel output connector pin }}$ ( 1-16 ) PP_OutC_Pin
24. PSB

Preamplifier-Summing Board number (1, 2-1, 2-2, 3, 4)
25. PSB letter repeated

Preamplifier Summing Board letter. Same as PSB except in letter notation (A, B, C, D, E)
26. PSB Pin

PSB LV connector pin ( 1-16 ) (PSB_Pin)
27. Qwedge

Wedge number in quadrant (1-8), QWedge $=$ PB_Con (Wedge)

## Signal Feedthrough and Crate Positions

|  |  |  |
| :---: | :---: | :---: |
| 1 | AF-A-02L | A |
| 2 | AF-A-06L | A |
| 3 | AF-A-09L | A |
| 4 | AF-A-12L | A |
| 5 | AF-C-02L | C |
| 6 | AF-C-06L | C |
| 7 | AF-C-09L | C |
| 8 | AF-C-12L | C |

This table lists the positions of the feedthroughs and their associated crate positions. The above table is a complete listing of all 8 HEC feedthroughs. For more information please refer to the Feedthrough database.


## Calibration Lines (TDR Measurements) Table

| Quadrant1to4/cryostat/Calibration <br> Generator Channel | $1 / \mathrm{A} / 1$ | $1 / \mathrm{A} / 10$ | $1 / \mathrm{A} / 100$ |
| :--- | :---: | :---: | :---: |
| Quadrant1to4 | 1 | 1 | 1 |
| Cryostat | A | A | A |
| Calibration Generator Channel | 1 | 10 | 100 |
| Warm Cable Impedance (Ohm) | 37.00 | 37.03 | 36.55 |
| Vacuum Cable Impedance (Ohm) | 37.03 | 37.11 |  |
| Pigtail Impedance (Ohm) | 51.15 | 50.84 | 52.22 |
| Pigtail resistance (Ohm/ns) | 0.04 | 0.07 | 0.06 |
| Quadrant Cable Impedance (Ohms) | 53.67 | 46.97 | 51.78 |
| Quadrant Cable Resistance (Ohms/ns) | 0.03 | 0.03 | 0.05 |
| Calibration Impedance (Ohms) | 53.68 | 51.1 | 52.66 |
| Calibration Resistance (Ohms/ns) | -0.02 | 0.04 | -0.02 |
| Stripline Impedance (Ohms) | 56.47 | 55.85 | 56.36 |
| Stripline Resistance (Ohms/ns) | -0.11 | -0.09 | -0.11 |
| Stripline Termination Impedance (Ohms) | 54.82 | 54.44 | 54.95 |

## FEB Input Lines TDR Measurements Table

| Quadrant1to4/cryostat/FEB/Channel | $1 / \mathrm{C} / 1 / 1$ | $1 / \mathrm{C} / 1 / 10$ | $1 / \mathrm{C} / 1 / 100$ |
| :--- | :---: | :---: | :---: |
| Quadrant1to4 | 1 | 1 | 1 |
| Cryostat | C | C | C |
| FEB | 1 | 1 | 1 |
| Channel | 1 | 10 | 100 |
| Warm cable Impedance (Ohms) | 35.09 | 35.19 | 36.39 |
| Vacuum Cabe Impedance (Ohms) | 34.54 | 36.07 | 37.33 |
| Pigtail Impedance (Onms) | 50.14 | 50.15 | 51.62 |
| Pigtail Resistance (Ohms/ns) | 0.06 | 0.05 | 0.08 |
| Quadrant Cable Impedance (Ohms) | 44.56 | 45.05 | 45.79 |
| Quadrant Cable Resistance (Ohms/ns) | 0.05 | 0.06 | 0.05 |
| Calibration Cable PSB Termination Impedance (Ohms) | 355.27 | 375.27 | 438.42 |
| Propagation Time (ns) | 109.95 | 110.2 | 105.3 |

These two tables of TDR measurements have self explanatory labels. For more details see Appendix I that describes these measurements.

## Quadrant Definitions Table

| Quadrant | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cryostat | A | A | A | A | C | C | C | C |
| Quadrant(1 to 4) | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 |

This table simply defines the somewhat un-orthodox quadrant. Unlike the normal definition of quadrant that goes from 1 to 4 , this Quadrant goes from 1 to 4 in the A cryostat and 5 to 8 in the C cryostat. For clarity when the more orthodox quadrant is called Quadrant(1 to 4) in this database.

## Quadrant-Wedge Definition Tables

| Cryostat/Wedge | $\mathrm{A} / 1$ | $\mathrm{~A} / 10$ | $\mathrm{~A} / 11$ |
| :--- | :---: | :---: | :---: |
| Quadrant | 1 | 2 | 2 |
| Cryostat | A | A | A |
| Wedge | 1 | 10 | 11 |
| Qwedge | 1 | 2 | 3 |

This table simple makes a definition for Qwedge. Qwedge is 1 for the first wedge in a quadrant and goes up to 8 for the final wedge in the quadrant.

Hence:
Qwedge $=$ Wedge $-0 \quad$ for Quadrant $(1$ to 4$)=1$
Qwedge $=$ Wedge $-8 \quad$ for Quadrant $(1$ to 4$)=2$
Qwedge $=$ Wedge -16 for Quadrant $(1$ to 4$)=3$
Qwedge $=$ Wedge -24 for Quadrant $(1$ to 4$)=4$

## FEB Definitions Table

| FEB Shaper Channel | 0 | 1 | 2 |
| :--- | :--- | :--- | :--- |
| FEB Channel Number | 1 | 2 | 3 |

This table simply makes the definition:
FEB Shaper Channel $=$ FEB Channel Number - 1

Signal Line Summary Table

| Cryostat/Wedge/Z/Tower | A/1/1/1 | A/1/1/10 | A/1/1/11 |
| :---: | :---: | :---: | :---: |
| Cryostat/Qwedge/PSB_letter/Tower | A/1/A/1 | A/1/A/10 | A/1/A/11 |
| Cryostat/Wedge/Z | A/1/1 | A/1/1 | A/1/1 |
| Cryostat/Wedge/PSB_letter | A/25/A | A/25/A | A/25/A |
| PSB_Serial/Tower | A51/1 | A51/10 | A51/11 |
| Wheel_Cryostat | HEC1A | HEC1A | HEC1A |
| Cryostat/Wheel/Wedge | A/HEC1/25 | A/HEC1/25 | A/HEC1/25 |
| Cryostat | A | A | A |
| Wedge | 1 | 1 | 1 |
| QWedge | 1 | 1 | 1 |
| Z | 1 | 1 | 1 |
| Wheel | HEC1 | HEC1 | HEC1 |
| Tower | 1 | 10 | 11 |
| ETA | 2 | 6 | 7 |
| PHI | 1 | 2 | 1 |
| PSB Letter | A | A | A |
| Module Serial | CF20 | CF20 | CF20 |
| PSB Serial | A51 | A51 | A51 |
| Calibration Generator 1 | 11 | 15 | 9 |
| Calibration Generator 2 | 10 |  |  |
| Calibration Generator 3 |  |  |  |
| Calibration Generator 4 |  |  |  |
| Ntiles | 16 | 8 | 8 |
| HV Est1 | 3 | 3 | 3 |
| HV Est2 | 2 | 2 | 2 |
| HV Pad1 | 4 | 4 | 4 |
| HV Pad2 | 1 | 1 | 1 |
| LV1 Q Number -1,5v | 59 | 59 | 59 |
| LV1 Q Number GND | 60 | 60 | 60 |
| LV2 Q Number +3V | 61 | 61 | 61 |
| LV2 Q Number GND | 62 | 62 | 62 |
| LV3 Q Number +7V | 63 | 63 | 63 |
| LV3 Q Number GND | 64 | 64 | 64 |
| Feedthrough Location | AF-A-02L | AF-A-02L | AF-A-02L |
| FT Connector | 5A | 7A | 7A |
| FEC Slot | 25 | 28 | 28 |
| FEB Connector | J1 | J1 | J1 |
| FEC Pin | C32 | C30 | C24 |

The following table lists the items already described in this document:

| Cryostat/Wedge/Z/Tower |
| :--- |
| Cryostat/Qwedge/PSB_letter/Tower |
| Cryostat/Wedge/Z |
| Cryostat/Wedge/PSB_letter |


| PSB_Serial/Tower |
| :--- |
| Wheel_Cryostat |
| Cryostat/Wheel/Wedge |
| Cryostat |
| Wedge |
| QWedge |
| Z |
| Wheel |
| Tower |
| ETA |
| PHI |
| PSB Letter |
| Module Serial |
| PSB Serial |
| Feedthrough Location |
| FT Connector |
| FEC Slot |
| FEB Connector |
| FEC Pin |

The Calibration Generator 1 to 4 lists the calibration generator lines (see table Quadrant Signal \& Calibration Cabling) attached to this signal line.

Ntiles lists the number of gaps on this readout line.
When Ntiles is 4 or 8 there is only one calibration line attached. When Ntiles is 16 there are two calibration lines attached. When Ntiles is 64 there is four calibration line attached. Calibration Generator 1 pulses the first 8 gaps on a readout line. Calibration Generator 2 pulses the gaps 9 to 16 on a readout line. When a tile is split into two tiles as is the case with tile 5, gaps 9-24 (see figure 9, page 36) Ntiles can be 4 , with one generator attached to the first 8 gaps of tile 5 a , one to the second 8 gaps of tile 5 a.

HV EST1(2) is the high voltage channel that provides HV to the first(second) EST board in each gap.

HV Pad1(2) is the high voltage channel that provides HV to the front(back) face of the PAD board in each gap.

LV1 Q Number $\mathbf{- 1 , 5 v}$ is the low voltage line number that supplies the negative 1.5 V to the PSB board that contains the amplifiers and summation circuit for this signal line.

LV1 Q Number GND is the low voltage line number that supplies the ground return of the 1.5 V line to the PSB board that contains the amplifiers and summation circuit for this signal line.

LV2 Q Number $+3 \boldsymbol{V}$ is the low voltage line number that supplies the 3 V to the PSB board that contains the amplifiers and summation circuit for this signal line.

LV2 Q Number GND is the low voltage line number that supplies the ground return of the 3 V line to the PSB board that contains the amplifiers and summation circuit for this signal line.

LV3 Q Number 7V is the low voltage line number that supplies the 7 V to the PSB board that contains the amplifiers and summation circuit for this signal line.

LV3 Q Number GND is the low voltage line number that supplies the ground return of the 7 V line to the PSB board that contains the amplifiers and summation circuit for this signal line.

## Non-Conformance Table

| Problem \# | 1 | 4 | 38 | 64 |
| :---: | :---: | :---: | :---: | :---: |
| Issue $\mathrm{FEB}=1, \mathrm{CAL}=2$, HV_Pin=3,HV_Line=4 | 1 | 2 | 3 | 4 |
| Cryostat | C | C | A | A |
| Quadrant(1 to 4) | 1 | 1 |  |  |
| Front End Board Module Number | 2 |  |  |  |
| Front End Board Channel | 24 |  |  |  |
| Calibration Generator Channel |  | 13 |  |  |
| Comment | No termination at PSB. Channel not used | C cable high impedance | HV Pin... disconnected at Module one sub gap OFF | $\begin{gathered} \text { EC_A CT Fall } \\ 2005 \\ \text { Short } \end{gathered}$ |
| Wedge |  |  | 1 | 2 |
| Module |  |  | AF21 | AF14 |
| Gap with HV pin cut |  |  | 11 |  |
| Gap Cut |  |  | EST1 | EST1 |
| Z |  |  | 2 | 2 |
| Severity of Problem |  |  |  | 0 |
| Comment on Severity of Problem |  |  |  | Short |

## Problem \# :

There are 91 problems numbered from 1 to 91

## Issue :

1 for a Front End Board (FEB) problem. In the example given there is no termination at the cold PSB board.
2 For a calibration line problem. In the example given the calibration cable has a high impedance.
3 For the case where a HV pin was cut due to a short in that sub gap. If this gap belongs to a tower of 8 tiles then $1 /(8 \times 4)$ of the signal on average will be missing from this tower. The signal from this channel should on average be multiplied by $32 / 31$
4 For this case one sub-gap has not got voltage. $1 / 4$ of the signal will be lost. The signal from this channel should be multiplied by $4 / 3$.

Cryostat: Already described in this document.
Quadrant( 1 to 4 ): Already described in this document.
Front End Board Module Number: See FEB module number in table FEB Slot_Module Definitions.

Front End Board Channel: See FEB Channel in table FEB Slot_Module Definitions.
Calibration Generator Channel: See Quadrant and Signal and Calibration Cable Table.
Comment: Short helpful comment.
Wedge: Already described in this document.

Module: Already described in this document.
Gap with HV pin cut: This is the gap number within the module where the HV pin was cut.
Gap Cut: This was the type of sub-gap cut: EST1, PAD1, PAD2, or EST2
Z: $\quad$ This is the depth of the readout where the problem is present $Z=1,2,3$, or 4 .
Severity of problem: This describes the nature of the short as observed in B180 prior to transport of cryostat to the ATLAS pit:

0 Short, appears permanent.
1 Disappeared after warming cryostat in B180.
Present in warm in B180 prior to cool down of cryostat. Disappeared when cryostat
2 was cooled down in B180.

Comment on Severity of Problem: Short helpful comment.

## FEC Pin to FEB Channel Definitions

| FEB Channel | 1 | 2 | 3 |
| :--- | :---: | :---: | :---: |
| FEC Pin | C 32 | A 32 | C 31 |
| FEB Connector | J 1 | J 1 | J 1 |

This table give the FEB channel number (1-128) correspondence to the FEC connector (J1 or J3) and pin number.
(This table is not part of the core of the database as it describes items in the FEC where the database strictly only extends to the FEC connector and pin number.)

## FEB Slot_Module Definitions

| FEC Slot | 25 | 26 | 28 | 29 | 30 | 32 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | FEB Module Number | 1 | 2 | 3 | 4 | 5 |

This table lists the FEC slots that the FEB modules sit in. This information can be seen on page 34 where the FEC crate is drawn. So for instance FEB5 is in the slot marked as 30 in the FEC. (This table is not part of the core of the database as it describes items in the FEC where the database strictly only extends to the FEC connector and pin number.)

## Non-Conformance Reports (Queries)

Calibration Line Failure: List of towers affected by the 7 calibration line failures.

| $\begin{gathered} \text { \# } \\ \stackrel{E}{0} \\ \frac{0}{\circ} \\ \stackrel{0}{0} \end{gathered}$ |  |  |  | $\underset{\sim}{\leftarrow}$ | 픔 | N |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 37 | A | 4 | 42 | 6 | 5 | 2 |
| 37 | A | 4 | 42 | 11 | 5 | 1 |
| 37 | A | 4 | 42 | 2 | 5 | 1 |
| 37 | A | 4 | 42 | 6 | 5 | 1 |
| 37 | A | 4 | 42 | 3 | 5 | 2 |
| 37 | A | 4 | 42 | 7 | 5 | 2 |
| 37 | A | 4 | 42 | 10 | 5 | 2 |
| 37 | A | 4 | 42 | 11 | 5 | 2 |
| 36 | A | 4 | 36 | 15 | 3 | 4 |
| 36 | A | 4 | 36 | 14 | 3 | 4 |
| 36 | A | 4 | 36 | 8 | 6 | 4 |
| 36 | A | 4 | 36 | 7 | 6 | 4 |
| 36 | A | 4 | 36 | 4 | 6 | 3 |
| 36 | A | 4 | 36 | 8 | 6 | 3 |
| 36 | A | 4 | 36 | 4 | 6 | 4 |
| 36 | A | 4 | 36 | 6 | 6 | 3 |
| 36 | A | 4 | 36 | 6 | 6 | 4 |
| 36 | A | 4 | 36 | 7 | 6 | 3 |
| 36 | A | 4 | 36 | 14 | 3 | 3 |
| 28 | A | 3 | 48 | 5 | 6 |  |
| 28 | A | 3 | 48 | 3 | 6 | 2 |
| 28 | A | 3 | 48 | 4 | 6 | 2 |
| 28 | A | 3 | 48 | 5 | 6 | 2 |
| 28 | A | 3 | 48 | 2 | 6 | 1 |
| 28 | A | 3 | 48 | 10 | 6 | 1 |
| 28 | A | 3 | 48 | 11 | 6 | 2 |
| 28 | A | 3 | 48 | 2 | 6 | 2 |
| 28 | A | 3 | 48 | 10 | 6 | 2 |
| 27 | A | 3 | 15 | 6 | 2 | 1 |
| 27 | A | 3 | 15 | 11 | 2 | 2 |
| 27 | A | 3 | 15 | 10 | 2 | 2 |


|  |  |  |  | 氐 | 폼 | N |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | A | 3 | 15 | 7 | 2 | 2 |
| 27 | A | 3 | 15 | 6 | 2 | 2 |
| 27 | A | 3 | 15 | 3 | 2 | 2 |
| 27 | A | 3 | 15 | 2 | 2 | 1 |
| 27 | A | 3 | 15 | 11 | 2 |  |
| 27 | A | 3 | 15 | 8 | 2 | 2 |
| 12 | C | 4 | 80 | 11 | 7 | 2 |
| 12 | C | 4 | 80 | 10 | 7 | 2 |
| 12 | C | 4 | 80 | 4 | 7 | 2 |
| 12 | C | 4 | 80 | 5 | 7 | 2 |
| 12 | C | 4 | 80 | 10 | 7 | 1 |
| 12 | C | 4 | 80 | 2 | 7 | 1 |
| 12 | C | 4 | 80 | 5 | 7 |  |
| 12 | C | 4 | 80 | 2 | 7 | 2 |
| 12 | C | 4 | 80 | 3 | 7 | 2 |
| 6 | C | 2 | 24 | 13 | 7 | 2 |
| 6 | C | 2 | 24 | 12 | 7 | 2 |
| 6 | C | 2 | 24 | 9 | 14 | 2 |
| 6 | C | 2 | 24 | 8 | 14 | 2 |
| 6 | C | 2 | 24 | 4 | 14 | 2 |
| 6 | C | 2 | 24 | 3 | 14 | 2 |
| 6 | C | 2 | 24 | 3 | 14 | 1 |
| 6 | C | 2 | 24 | 13 | 7 | 1 |
| 6 | C | 2 | 24 | 8 | 14 | 1 |
| 4 | C | 1 | 13 | 3 | 15 | 2 |
| 4 | C | 1 | 13 | 3 | 15 | 1 |
| 4 | C | 1 | 13 | 4 | 15 | 2 |
| 4 | C | 1 | 13 | 9 | 15 | 2 |
| 4 | C | 1 | 13 | 14 | 8 | 2 |
| 4 | C | 1 | 13 | 15 | 8 | 1 |

## HV Failure:

Each HV failure causes the loss of $1 / 4$ of the signal on the entire readout depth of a module. Below are the effected towers due to 8 HV line failures.

|  |  | $\begin{array}{lll} 0 & 0 \\ 0 & \frac{0}{3} \\ 0 & 0 \\ 3 & 0 \end{array}$ |  | $\left.\begin{array}{\|c} \varepsilon \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 4 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ \omega \end{array} \right\rvert\,$ | $\underset{\sim}{\leftarrow}$ | $\overline{\text { I }}$ | $\begin{aligned} & \boldsymbol{0} \\ & \stackrel{e}{\mathbf{E}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 5 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 6 | 3 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 5 | 3 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 4 | 4 | 32 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 4 | 3 | 32 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 3 | 4 | 32 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 3 | 3 | 32 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 14 | 2 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 13 | 2 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 12 | 2 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 11 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 8 | 3 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 2 | 3 | 8 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 2 | 4 | 8 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 7 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 6 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 8 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 9 | 3 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 9 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 10 | 3 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 10 | 4 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 11 | 3 | 16 |
| 64 | 4 A | 2 AF14 | 2 Short | 0 | 7 | 3 | 16 |


|  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



|  |  | $\begin{array}{ll} 0.0 \\ \frac{8}{0} & \frac{0}{7} \\ 3 & \vdots \\ 3 & i \end{array}$ |  | $\begin{aligned} & \varepsilon \\ & \frac{\varepsilon}{0} \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \infty \end{aligned}$ |  | $\overline{\mathrm{x}}$ | $\begin{aligned} & \mathscr{0} \\ & \stackrel{\text { en }}{\mathbf{Z}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 12 | 4 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 13 | 4 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 14 | 4 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 3 | 7 | 4 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 3 | 8 | 4 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 4 | 7 | 16 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 4 | 8 | 16 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 5 | 8 | 16 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 11 | 8 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 5 | 7 | 16 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 11 | 7 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 10 | 8 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 10 | 7 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 9 | 8 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 9 | 7 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 8 | 8 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 8 | 7 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 7 | 8 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 6 | 8 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 6 | 7 | 8 |
| 76 | 4 A | 28 AR33 | 3 Short | 0 | 7 | 7 | 8 |


|  |  |  |  |  | $\stackrel{\mathbb{1}}{\underset{\sim}{x}}$ | $\overline{\mathrm{I}}$ | $\stackrel{\text { e }}{\stackrel{\text { ¢ }}{\text { L }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 6 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 3 | 6 | 32 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 2 | 6 | 8 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 6 | 6 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 5 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 5 | 6 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 4 | 5 | 32 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 3 | 5 | 32 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 14 | 3 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 13 | 3 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 12 | 3 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 11 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 7 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 4 | 6 | 32 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 7 | 6 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 2 | 5 | 8 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 8 | 6 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 8 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 9 | 6 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 9 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 10 | 6 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 10 | 5 | 16 |
| 80 | 4 C | 11 AF04 | 2 Short | 0 | 11 | 6 | 16 |


|  | Issue FEB=1, CAL=2, HV_Pin=3,HV_Line=4 Cryostat | $\left\|\begin{array}{ll} 0 & 0 \\ 0 & \frac{0}{0} \\ 0 & \sum \\ 3 & \sum \end{array}\right\|$ |  | $\begin{aligned} & \varepsilon \\ & \frac{\varepsilon}{0} \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \infty \\ & \infty \end{aligned}$ | 氐 | $\overline{\mathrm{I}}$ | $\begin{gathered} \boldsymbol{e} \\ \frac{\stackrel{e}{5}}{\mathbf{Z}} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 11 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 5 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 5 | 16 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 4 | 15 | 32 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 4 | 16 | 32 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 3 | 15 | 32 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 3 | 16 | 32 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 14 | 8 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 13 | 8 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 12 | 8 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 6 | 16 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 6 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 2 | 15 | 8 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 2 | 16 | 8 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 7 | 16 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 7 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 8 | 16 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 9 | 16 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 9 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 10 | 16 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 10 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 8 | 15 | 16 |
| 82 | 4 C | 24 AF25 | 2 Short | 0 | 11 | 16 | 16 |


|  | Issue $\mathrm{FEB}=1, \mathrm{CAL}=2, \mathrm{HV}$ _Pin $=3, \mathrm{HV}$ _Line $=4$ Cryostat | $\left\|\begin{array}{ll} 0 \\ 0 & \frac{0}{0} \\ 3 & 0 \\ 3 & \sum \end{array}\right\|$ |  |  | $\underset{\underset{y}{*}}{\stackrel{y}{2}}$ | $\overline{ \pm}$ | $\stackrel{\text { er }}{\stackrel{\text { er }}{ \pm}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 5 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 12 | 5 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 13 | 5 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 3 | 10 | 32 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 2 | 10 | 8 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 4 | 10 | 32 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 6 | 10 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 5 | 10 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 11 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 14 | 5 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 4 | 9 | 32 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 8 | 10 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 3 | 9 | 32 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 2 | 9 | 8 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 7 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 6 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 8 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 9 | 10 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 9 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 10 | 10 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 10 | 9 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 11 | 10 | 16 |
| 83 | 4 C | 29 CF31 | 2 Short | 0 | 7 | 10 | 16 |


|  |  | 뀽 | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ | $\begin{aligned} & \frac{0}{3} \\ & \frac{0}{0} \\ & \sum \end{aligned}$ | N |  |  | $\stackrel{\varangle}{\underset{w}{4}}$ | $\overline{\mathrm{I}}$ | $\begin{aligned} & \stackrel{\infty}{\mathbf{\omega}} \\ & \stackrel{\Delta}{\mathbf{Z}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 13 | 8 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 14 | 8 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 3 | 16 | 4 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 3 | 15 | 4 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 4 | 16 | 16 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 4 | 15 | 16 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 12 | 8 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 5 | 15 | 16 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 8 | 16 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 5 | 16 | 16 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 11 | 15 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 11 | 16 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 10 | 15 | 8 |
| 91 |  | C |  | CR32 |  | Short | 0 | 10 | 16 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 9 | 15 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 8 | 15 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 7 | 15 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 7 | 16 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 6 | 15 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 6 | 16 | 8 |
| 91 |  | C | 32 | CR32 |  | Short | 0 | 9 | 16 | 8 |

## HV Pins disconnected:

26 pins were disconnected causing the average loss of $1 /(4 \times$ Ntiles $)$ in signal. The following table give the list of all affected towers and the value of Ntiles.

|  | 岕 |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  |  | $\left\|\begin{array}{l} \frac{\pi}{0} \\ \stackrel{\rightharpoonup}{0} \\ 2 \\ 0 \\ 0 \end{array}\right\|$ | $\left.\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 3 \end{aligned} \right\rvert\,$ |  | $\begin{aligned} & \text { J } \\ & \text { U } \\ & \text { O} \end{aligned}$ | N | $\stackrel{\leftarrow}{\leftarrow}$ | $\overline{\mathrm{I}}$ | $\frac{\mathscr{y}}{\frac{0}{\bar{z}}}$ | $\stackrel{\text { ¢ }}{ \pm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 2 | 10 | 8 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 2 | 9 | 8 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 3 | 9 | 32 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 3 | 10 | 32 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 4 | 10 | 32 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 4 | 9 | 32 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 5 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 5 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 6 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 6 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 7 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 7 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 8 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 8 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 9 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 9 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 10 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 10 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 11 | 9 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 11 | 10 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 12 | 5 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 13 | 5 | 16 | HEC1 |
| 39 | 3 | A | 5 | 22 | PAD2 | 2 | 14 | 5 | 16 | HEC1 |


|  | Issue FEB=1, CAL=2, HV_Pin=3,HV_Line=4 |  | $\begin{aligned} & 8 \\ & \frac{8}{0} \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \text { J } \\ & 0 \\ & \text { 팅 } \end{aligned}$ | N | $\underset{\sim}{\leftarrow}$ | $\overline{\mathrm{I}}$ | $\begin{aligned} & \text { en } \\ & \frac{\stackrel{\omega}{\bar{Z}}}{} \end{aligned}$ | ¢ ¢ ¢ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 2 | 11 | 8 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 2 | 12 | 8 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 3 | 12 | 32 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 3 | 11 | 32 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 4 | 11 | 32 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 4 | 12 | 32 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 5 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 5 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 6 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 6 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 7 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 7 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 8 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 8 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 9 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 9 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 10 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 10 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 11 | 11 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 11 | 12 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 12 | 6 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 13 | 6 | 16 | HEC1 |
| 40 | 3 | A | 6 | 21 | EST2 | 2 | 14 | 6 | 16 | HEC1 |


|  |  | $\begin{aligned} & \text { T⿳亠丷厂囗十 } \\ & \stackrel{0}{0} \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $\begin{array}{\|c} 9 \\ 8 \\ 0 \\ 3 \end{array}$ |  | $\begin{aligned} & \overrightarrow{7} \\ & 0 \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ | N | $\stackrel{\varangle}{\leftrightarrows}$ | 픔 | $\begin{gathered} \boldsymbol{e} \\ \stackrel{e}{\bar{\Sigma}} \end{gathered}$ | $\begin{aligned} & \Phi \begin{array}{l} \Phi \\ \vdots \\ \stackrel{\otimes}{3} \end{array} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 2 | 8 | 16 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 2 | 7 | 16 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 3 | 8 | 16 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 3 | 7 | 16 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 4 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 4 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 5 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 5 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 6 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 6 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 7 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 7 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 8 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 8 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 9 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 9 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 10 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 10 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 11 | 8 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 11 | 7 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 12 | 4 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 13 | 4 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 14 | 4 | 8 | HEC1 |
| 41 | 3 | A | 12 | 5 | EST2 | 1 | 15 | 4 | 8 | HEC1 |


|  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |  | N | $\stackrel{\mathbb{~}}{\underset{山}{4}}$ | 픔 |  | $\stackrel{\text { ® }}{\stackrel{\text { ® }}{3}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 2 | 14 | 8 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 2 | 13 | 8 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 3 | 13 | 32 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 3 | 14 | 32 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 4 | 13 | 32 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 4 | 14 | 32 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 5 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 5 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 6 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 6 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 7 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 7 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 8 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 8 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 9 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 9 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 10 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 10 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 11 | 13 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 11 | 14 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 12 | 7 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 13 | 7 | 16 | HEC1 |
| 42 | 3 | A | 15 | 22 | EST2 | 2 | 14 | 7 | 16 | HEC1 |


|  |  | $\left\|\begin{array}{l} \vec{\pi} \\ \frac{\pi}{0} \\ 0 \\ 0 \\ 0 \end{array}\right\|$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  | $\begin{aligned} & \stackrel{7}{J} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | 氐 | $\overline{\mathrm{I}}$ | $\begin{gathered} \text { e } \\ \stackrel{\omega}{\bar{Z}} \end{gathered}$ | $\begin{aligned} & \bar{\otimes} \\ & \stackrel{\otimes}{3} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 2 | 1 | 8 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 2 | 2 | 8 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 3 | 2 | 32 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 3 | 1 | 32 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 4 | 2 | 32 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 4 | 1 | 32 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 5 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 5 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 6 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 6 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 7 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 7 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 8 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 8 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 9 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 9 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 10 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 10 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 11 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 11 | 2 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 12 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 13 | 1 | 16 | HEC1 |
| 43 | 3 | A | 17 | 14 | EST2 | 2 | 14 | 1 | 16 | HEC1 |


|  | 岕 |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  |  | $\begin{array}{\|l\|} \hline \frac{\pi}{0} \\ \stackrel{y}{0} \\ \stackrel{0}{0} \\ \hline \end{array}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ |  |  | N | $\stackrel{\varangle}{\leftrightarrows}$ | $\overline{\mathrm{I}}$ | $\begin{aligned} & \dot{0} \\ & \frac{0}{\bar{\Sigma}} \end{aligned}$ | ¢ $\stackrel{\text { ¢ }}{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 3 | 6 | 4 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 3 | 5 | 4 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 4 | 5 | 16 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 4 | 6 | 16 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 5 | 5 | 16 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 5 | 6 | 16 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 6 | 6 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 6 | 5 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 7 | 5 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 7 | 6 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 8 | 5 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 8 | 6 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 9 | 6 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 9 | 5 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 10 | 6 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 10 | 5 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 11 | 6 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 11 | 5 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 12 | 3 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 13 | 3 | 8 | HEC2 |
| 45 | 3 | A | 3 | 8 | EST1 | 3 | 14 | 3 | 8 | HEC2 |


|  | 息 |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| \# 등 응 은 | $t=$ ou! $7^{-} \wedge H^{\prime} \varepsilon=u!d^{-} \wedge H^{\prime} \tau=7 \forall O^{\prime}$ ' $=9 \exists \exists$ ənss। | $\begin{aligned} & \frac{\pi}{0} \\ & \stackrel{\pi}{0} \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \mathrm{J}_{1} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | 氐 | 픔 | $\begin{gathered} \stackrel{e}{e} \\ \frac{\stackrel{1}{\mathbf{Z}}}{2} \end{gathered}$ | $\stackrel{\text { ¢ }}{ \pm}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 4 | 5 | 4 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 4 | 6 | 4 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 5 | 6 | 16 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 5 | 5 | 16 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 6 | 5 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 6 | 6 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 7 | 6 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 7 | 5 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 8 | 5 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 8 | 6 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 9 | 6 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 9 | 5 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 10 | 6 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 10 | 5 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 11 | 6 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 11 | 5 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 12 | 3 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 13 | 3 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 14 | 3 | 8 | HEC2 |
| 47 | 3 | A | 27 | 11 | EST2 | 4 | 15 | 3 | 8 | HEC2 |


| \# E © 은 ㅇ | Issue FEB=1, CAL=2, HV_Pin=3,HV_Line=4 |  | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{3} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | $\underset{山}{\overleftarrow{~}}$ | $\overline{\mathrm{x}}$ | $\begin{aligned} & \stackrel{0}{\omega} \\ & \frac{\mathbf{E}}{\mathbf{Z}} \end{aligned}$ | $\begin{aligned} & \Phi \\ & \stackrel{\Phi}{\boldsymbol{\omega}} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 2 | 15 | 16 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 2 | 16 | 16 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 3 | 15 | 16 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 3 | 16 | 16 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 4 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 4 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 5 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 5 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 6 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 6 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 7 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 7 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 8 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 8 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 9 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 9 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 10 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 10 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 11 | 15 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 11 | 16 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 12 | 8 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 13 | 8 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 14 | 8 | 8 | HEC1 |
| 48 | 3 | C | 8 | 8 | PAD2 | 1 | 15 | 8 | 8 | HEC1 |


|  | Issue $\mathrm{FEB}=1, \mathrm{CAL}=2, \mathrm{HV}$ Pin=3,HV Line=4 | 뀽 | $\begin{aligned} & 0.0 \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \text { J } \\ & 0 \\ & \text { İ } \\ & 0 \end{aligned}$ | N | 氐 | $\overline{\text { 픈 }}$ | $\frac{\stackrel{0}{\mathbf{E}}}{\frac{1}{\mathbf{Z}}}$ | $\begin{aligned} & \Phi \\ & \stackrel{\otimes}{3} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 2 | 8 | 16 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 2 | 7 | 16 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 3 | 7 | 16 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 3 | 8 | 16 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 4 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 4 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 5 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 5 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 6 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 6 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 7 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 7 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 8 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 8 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 9 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 9 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 10 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 10 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 11 | 8 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 11 | 7 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 12 | 4 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 13 | 4 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 14 | 4 | 8 | HEC1 |
| 50 | 3 | C | 28 | 6 | EST1 | 1 | 15 | 4 | 8 | HEC1 |


|  | $\stackrel{7}{\\|}$ |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| $\#$ \# 응 은 ㅇ | $\text { Issue } \mathrm{FEB}=1, \mathrm{CAL}=2, \mathrm{HV} \text { _Pin=3,HV_Line=4 }$ | $\begin{aligned} & \stackrel{+}{0} \\ & \stackrel{N}{0} \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \frac{8}{0} \\ & \$ \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{U} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | 氐 | $\overline{\text { 픈 }}$ |  | ¢ $\stackrel{\text { ® }}{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 2 | 15 | 8 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 2 | 16 | 8 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 3 | 16 | 32 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 3 | 15 | 32 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 4 | 16 | 32 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 4 | 15 | 32 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 5 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 5 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 6 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 6 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 7 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 7 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 8 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 8 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 9 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 9 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 10 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 10 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 11 | 16 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 11 | 15 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 12 | 8 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 13 | 8 | 16 | HEC1 |
| 52 | 3 | C | 32 | 22 | PAD1 | 2 | 14 | 8 | 16 | HEC1 |


| \# E 응 은 |  | $\begin{aligned} & \frac{\pi}{0} \\ & \stackrel{\text { den }}{0} \\ & \text { ? } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 3 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \tilde{J}^{0} \\ & \stackrel{0}{0} \end{aligned}$ | N | 氐 | 폼 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 4 | 6 | 4 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 4 | 5 | 4 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 5 | 5 | 16 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 5 | 6 | 16 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 6 | 5 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 6 | 6 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 7 | 5 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 7 | 6 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 8 | 5 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 8 | 6 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 9 | 5 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 9 | 6 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 10 | 5 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 10 | 6 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 11 | 6 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 11 | 5 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 12 | 3 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 13 | 3 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 14 | 3 | 8 | HEC2 |
| 53 | 3 | C | 3 | 14 | EST2 | 4 | 15 | 3 | 8 | HEC2 |


|  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & 5 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | $\underset{山}{\overleftarrow{~}}$ | $\overline{\text { I }}$ | $\begin{gathered} \boldsymbol{e} \\ \frac{\stackrel{\rightharpoonup}{\mathbf{E}}}{2} \end{gathered}$ | $\begin{aligned} & \bar{\Phi} \\ & \stackrel{\otimes}{3} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 4 | 14 | 4 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 4 | 13 | 4 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 5 | 14 | 16 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 5 | 13 | 16 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 6 | 13 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 6 | 14 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 7 | 14 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 7 | 13 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 8 | 14 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 8 | 13 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 9 | 14 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 9 | 13 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 10 | 14 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 10 | 13 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 11 | 13 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 11 | 14 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 12 | 7 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 13 | 7 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 14 | 7 | 8 | HEC2 |
| 54 | 3 | C | 7 | 16 | EST2 | 4 | 15 | 7 | 8 | HEC2 |


|  | Issue $\mathrm{FEB}=1, \mathrm{CAL}=2, \mathrm{HV}$ Pin＝3，HV＿Line＝4 | T⿳一⿰工 0 0 0 0 0 | $\begin{aligned} & 0 \\ & \frac{0}{0} \\ & \vdots \end{aligned}$ |  | $\begin{aligned} & \tilde{J} \\ & \text { U } \\ & 0 \\ & 0 \end{aligned}$ | N | $\stackrel{\leftrightarrows}{\leftrightarrows}$ | $\overline{\mathrm{I}}$ | $\begin{gathered} \text { 总 } \\ \hline \mathbf{E} \\ \hline \end{gathered}$ | $\begin{aligned} & \bar{\otimes} \\ & \stackrel{\otimes}{3} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 4 | 4 | 4 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 4 | 3 | 4 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 5 | 3 | 16 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 5 | 4 | 16 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 6 | 3 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 6 | 4 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 7 | 4 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 7 | 3 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 8 | 4 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 8 | 3 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 9 | 4 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 9 | 3 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 10 | 4 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 10 | 3 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 11 | 4 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 11 | 3 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 12 | 2 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 13 | 2 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 14 | 2 | 8 | HEC2 |
| 55 | 3 | C | 10 | 15 | EST1 | 4 | 15 | 2 | 8 | HEC2 |


|  | 崱 |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| \# 등 응 은 |  |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{3} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | 氐 | 픔 | $\begin{gathered} \mathscr{0} \\ \frac{\stackrel{e}{\mathbf{z}}}{} \end{gathered}$ | $\begin{aligned} & \Phi \begin{array}{l} \Phi \\ \stackrel{\otimes}{3} \end{array} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 3 | 9 | 4 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 3 | 10 | 4 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 4 | 9 | 16 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 4 | 10 | 16 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 5 | 10 | 16 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 5 | 9 | 16 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 6 | 9 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 6 | 10 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 7 | 10 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 7 | 9 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 8 | 10 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 8 | 9 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 9 | 10 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 9 | 9 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 10 | 10 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 10 | 9 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 11 | 9 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 11 | 10 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 12 | 5 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 13 | 5 | 8 | HEC2 |
| 57 | 3 | C | 13 | 1 | PAD1 | 3 | 14 | 5 | 8 | HEC2 |


|  | Issue $\mathrm{FEB}=1, \mathrm{CAL}=2, \mathrm{HV}$ Pin=3, HV Line=4 | $\begin{aligned} & \frac{\pi}{0} \\ & \stackrel{?}{00} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \tilde{J} \\ & \text { U } \\ & 0 \\ & 0 \end{aligned}$ | N | $\underset{山}{\overleftarrow{~}}$ | $\overline{\mathrm{I}}$ |  | $\begin{aligned} & \overline{\mathbf{D}} \\ & \stackrel{\otimes}{3} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 4 | 15 | 4 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 4 | 16 | 4 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 5 | 16 | 16 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 5 | 15 | 16 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 6 | 15 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 6 | 16 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 7 | 16 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 7 | 15 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 8 | 15 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 8 | 16 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 9 | 15 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 9 | 16 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 10 | 16 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 10 | 15 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 11 | 16 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 11 | 15 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 12 | 8 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 13 | 8 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 14 | 8 | 8 | HEC2 |
| 58 | 3 | C | 16 | 16 | EST2 | 4 | 15 | 8 | 8 | HEC2 |


| \# 등 응 은 |  | $\left\lvert\, \begin{aligned} & \frac{\pi}{0} \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}\right.$ | $\left\|\begin{array}{l} 8 \\ 0 \\ 0 \\ 3 \end{array}\right\|$ |  | $\begin{aligned} & \vec{U} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | $\stackrel{\leftarrow}{\leftarrow}$ | 폼 |  | $\begin{aligned} & \bar{\otimes} \\ & \stackrel{\otimes}{\aleph} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 4 | 2 | 4 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 4 | 1 | 4 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 5 | 2 | 16 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 5 | 1 | 16 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 6 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 6 | 2 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 7 | 2 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 7 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 8 | 2 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 8 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 9 | 2 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 9 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 10 | 2 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 10 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 11 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 11 | 2 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 12 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 13 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 14 | 1 | 8 | HEC2 |
| 59 | 3 | C | 17 | 15 | EST2 | 4 | 15 |  | 8 | HEC2 |


|  | 息 |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | 息 |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


|  | Issue $\mathrm{FEB}=1, \mathrm{CAL}=2, \mathrm{HV}$ _Pin=3,HV_Line=4 |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \stackrel{7}{0} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | N | $\stackrel{\varangle}{\mathbf{4}}$ | $\overline{\mathrm{I}}$ | $\begin{gathered} \frac{\otimes}{\mathbf{E}} \\ \frac{\Delta}{\mathbf{E}} \end{gathered}$ | ¢ $\stackrel{\text { ¢ }}{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 3 | 15 | 4 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 3 | 16 | 4 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 4 | 15 | 16 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 4 | 16 | 16 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 5 | 15 | 16 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 5 | 16 | 16 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 6 | 16 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 6 | 15 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 7 | 16 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 7 | 15 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 8 | 16 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 8 | 15 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 9 | 16 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 9 | 15 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 10 | 15 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 10 | 16 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 11 | 15 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 11 | 16 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 12 | 8 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 13 | 8 | 8 | HEC2 |
| 63 | 3 | C | 32 | 6 | EST1 | 3 | 14 | 8 | 8 | HEC2 |

## APPENDIX I

## TDR Measurements and Reconstruction of HEC Cable

## Parameters in the EC-C cold test (reproduced here from ATL-AE-

## QR-0001 v.1)

The TDR waveform displays structure that indicates the wave impedances in the line and its termination conditions. The HEC signal line (PSB to Baseplane) is a set of cables:


The measurements were done with TDS 8000 oscilloscope running in TDR mode. The instrument settings are shown in the table below. One channel (CH1) was used for all tests. The measurements were not automated, as all re-plugging operations were done manually.

| VERT | Scale <br> Offset | $100 \mathrm{mV} /$ div <br> 250 mV |  |
| :--- | :--- | :--- | :--- |
| HOR | Scale | $20 \mathrm{~ns} /$ div $\quad$ (50 for calibration |  |
| channels) |  |  |  |
|  | Offset | 21.4 ns |  |
|  | Length | 4000 samples |  |
| ACQ | Type | Average |  |
|  | N of samples | 50 |  |
|  | Stop | Condition |  |
|  | N of acquisitions | 50 |  |
| TRIG | Source | Internal |  |
|  | Frequency | 25 KHz |  |
|  | Mode | Auto |  |
| TDR | Channel | C 1 |  |
|  | Scale | V |  |

Each waveform is saved in an ASCII file with csv format. The file name reflects the board number and channel number e.g.: s1a33.txt means FEB (signal) line of FEB \#1, connector "a" (first half of FEB, "b" corresponds to the second half of FEB), channel 33. Other files are: "p" - re-measurement of signal channel, "c" calibration line, "d" - calibration line with $50 \mathrm{~ns} / \mathrm{div}$ ( 200 ns is not enough to see all
the line). There is no quadrant number in the file name because the files are grouped in four folders, one per quadrant.

There is a mismatch between in-board channels numbering and TDR file numbers. File number 01 corresponds to pin A32 of the baseplane connector while the FE boards starts with C32. Channel number (counted from 1, not 0) can be obtained from file number by applying simple odd-even transform.

There are 128 calibration lines and 768 signal lines per quadrant, so in total 3584 measurements are done. In the case that the measurement quality was in doubt, the test was repeated.

A typical oscillogram for signal line is shown below. Each part of the line can be recognized in the waveform:


Similar waveform for calibration line (from baseplane to the end of strip line):


The vertical scale, originally measured in mV , is recalculated to equivalent impedance:

$$
Z=50 \Omega \cdot \frac{V}{500 m V-V}
$$

For each cable a time window is defined as shown at the next two plots. The cable parameters are determined by analyzing data from corresponding window. The impedance of W and V cables are determined from the minimum value found in slots [ $\mathrm{t} 1, \mathrm{t} 2$ ] and [ $\mathrm{t} 2, \mathrm{t} 3$ ] respectively. For long cables: pigtail ( P ), quadrant ( Q ), calibration (C) and stripline (S) both wave impedance and serial resistivity can be reconstructed. It is done by a linear fit of the corresponding subset of points: [t4, t5] for P-cable, [t6, t7] for Q-cable, etc.


Then, the resistivity is determined from the slope of the fit line. It is measured in $\Omega / \mathrm{ns}$. The wave impedance is obtained from the value of fit function in the area of the cable start point: t 3 for pigtail, t 5 for quadrant cable, t8 for calibration cable and t10 for strip line. To obtain a better estimation of the wave impedance, the integral resistivity of all cables up to this point has been subtracted. Such subtraction is done only for Q-cables and not done for others. Therefore the reconstructed value is not exactly the cable wave impedance. It is shifted with respect to the real value by few $\Omega$. Another source of shift is the inexact definition of the cable starting point.

The length of each cable can not be accurately determined because all the lines have nearly equal impedance of $50 \Omega$. Also there is no well defined boundary between two consecutive cables because of signal slow down due to skin effect in the cables. But the total length of signal line can be easily estimated. It is done only for FEB lines where the PSB is connected. For disconnected channels it makes no sense and thus this parameter is fixed to 0 . The beginning of the chain is defined as t 1 and the end of the chain is determined in the region of 150 ns (upper plot of the last figure) when the waveform starts to rise rapidly. The end point is calculated as a point where waveform crosses the level of Q -cable impedance plus $5 \Omega$. Then the propagation time is the distance between end point and t 1 .

Other reconstructed parameters are PSB output impedance (impedance at the end of the FEB oscillogram) and strip line termination (impedance at the end of the CAL oscillogram). These values are calculated as an average over last 10-20 samplings.

The distributions of the cable parameters both for the signal and calibration lines can be found in a separate EDMS documents:
ATL-AE-QR-0003
HEC cables parameters measured with TDR in EC-C cold test
https://edms.cern.ch/file/563843/1/febhist.doc
https://edms.cern.ch/file/563843/1/calhist.doc
https://edms.cern.ch/file/563843/1/cabhist.doc

## Appendix II:

Diagrams of Connection Patch Panel to ATI, and PSB boards


Connection Patch Panel to ATI ( type 1)
$\eta=1.5-1.9$
$\eta=1.9-2.3$


Connection Patch Panel to ATI ( type 2)

$$
\eta=2.3-3.2
$$



| N | $\begin{gathered} \omega \\ 0 \end{gathered}$ | $\begin{aligned} & N \\ & \underset{\sim}{c} \\ & \hline \end{aligned}$ | $$ | $\begin{aligned} & \mathrm{N} \\ & \mathrm{~N} \\ & \mathrm{O} \end{aligned}$ | $\underset{\sim}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{N} \\ & \mathrm{O} \\ & \mathrm{G} \end{aligned}$ | $\begin{aligned} & \vec{i} \\ & \dot{G} \end{aligned}$ | $\left\lvert\, \begin{aligned} & \stackrel{\rightharpoonup}{\infty} \\ & 0 \\ & 0 \end{aligned}\right.$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\begin{array}{\|l} \vec{i} \\ \dot{\mathrm{j}} \end{array}$ | $\begin{aligned} & \vec{i} \\ & \dot{\mathrm{j}} \end{aligned}$ | $\|\overrightarrow{\mathrm{c}}\|$ | $\begin{aligned} & N \\ & \infty \\ & \hline \end{aligned}$ | $\begin{aligned} & N \\ & \cdots \end{aligned}$ | $\begin{aligned} & N \\ & \mathrm{~N} \\ & \mathrm{~N} \end{aligned}$ | $\begin{gathered} N \\ \underset{\sim}{\omega} \end{gathered}$ | $\begin{aligned} & \mathrm{N} \\ & \mathrm{~N} \\ & \mathrm{O} \end{aligned}$ | $\stackrel{N}{\sim}$ | $\begin{aligned} & \mathrm{N} \\ & \mathrm{O} \\ & \mathrm{O} \end{aligned}$ | $\begin{aligned} & \vec{i} \\ & \dot{\mathrm{v}} \end{aligned}$ | $\left\lvert\, \begin{gathered} \stackrel{\rightharpoonup}{\infty} \\ 0 \\ 0 \end{gathered}\right.$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\mid \vec{~}$ | $\left\lvert\, \begin{aligned} & \vec{~} \\ & \underset{\mathrm{G}}{ } \end{aligned}\right.$ | $\|\vec{~} \overrightarrow{\mathrm{M}}\|$ | $\underset{\sim}{\square}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| か | － | 示 | $\stackrel{\rightharpoonup}{\circ}$ | $\infty$ | の | － | N | N | $\stackrel{\rightharpoonup}{\circ}$ | $\infty$ | 0 | － | N | ज | $\stackrel{\rightharpoonup}{\omega}$ | د | $\omega$ | $V$ | $\cdots$ | $\omega$ | $\rightarrow$ | $\pm$ | $\omega$ | $v$ | cr | $\omega$ |  | \％ |
| ！ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\|\stackrel{\rightharpoonup}{\infty}\|$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\left\|\begin{array}{c} 0 \\ \infty \\ \infty \end{array}\right\|$ | $\stackrel{\rightharpoonup}{\infty}$ | $\vec{\infty} \mid$ | $\vec{\infty}$ | $\stackrel{\rightharpoonup}{\infty} \mid$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}_{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\begin{aligned} & c \\ & 0 \\ & \infty \end{aligned}$ | 픟． |
| ！ | N | N | $\stackrel{\rightharpoonup}{\infty}$ | － | － | N | $\stackrel{\rightharpoonup}{0}$ | $\infty$ | $09$ | ஷ্ষ | $\stackrel{A}{\sigma}$ | $\stackrel{\rightharpoonup}{\otimes}$ | N | N | N | $\stackrel{\rightharpoonup}{\bullet}$ | $\vec{v}$ | $\vec{v}$ | $\stackrel{\rightharpoonup}{\omega}$ | $\stackrel{\rightharpoonup}{\boldsymbol{~}}$ | $\bullet$ | $\checkmark$ | $0 \pi$ | M | $\left\lvert\, \frac{\omega}{\sigma}\right.$ | $\stackrel{\omega}{\sim}$ |  | \％ |
| $\omega$ | $\omega$ | $\omega$ | $\omega$ | N | N | N | N | $\rightarrow$ | $\rightarrow$ | $\rightarrow$ | $\checkmark$ | － | $\rightarrow$ | $\omega$ | $\omega$ | $\omega$ | $\omega$ | N | N | N | N | $\rightarrow$ | $\rightarrow$ | $\rightarrow$ | $\rightarrow$ | $\rightarrow$ |  |  |
| $\infty$ | 0 | A | N | $\infty$ | の | A | $N$ | $\infty$ | の | の | － | － | N | $\checkmark$ | cr | $\omega$ | $\rightarrow$ | $\checkmark$ | cr | $\omega$ | $\rightarrow$ | $\checkmark$ | G | O | $\omega$ | $\omega$ |  |  |

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| $\omega$ | $\begin{aligned} & \omega \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { A } \end{aligned}$ | $\begin{aligned} & N \\ & \underset{\sim}{\omega} \\ & \mathcal{N} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { N } \end{aligned}$ | $\underset{\sim}{N}$ | $\begin{aligned} & \mathrm{N} \\ & \mathrm{O} \\ & \mathrm{O} \end{aligned}$ | $\left\lvert\, \begin{gathered} \stackrel{\rightharpoonup}{c} \\ \dot{c} \\ \mathrm{v} \end{gathered}\right.$ | $\stackrel{\rightharpoonup}{\infty}$ | $$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\stackrel{\rightharpoonup}{\mathrm{v}}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \dot{\sim} \end{aligned}$ | $\left\lvert\, \begin{aligned} & \vec{u} \\ & \mathrm{v} \\ & \mathrm{v} \end{aligned}\right.$ | $\begin{aligned} & N \\ & \infty \end{aligned}$ | $\begin{aligned} & \mathrm{N} \\ & \hline \end{aligned}$ | $\begin{aligned} & N \\ & \underset{v}{n} \end{aligned}$ | N | $\begin{aligned} & \mathrm{N} \\ & \mathrm{~N} \\ & \mathrm{~N} \end{aligned}$ | $\underset{\sim}{N}$ | $\begin{aligned} & \mathrm{N} \\ & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\left\lvert\, \begin{array}{\|c} \mid \\ \text { e } \\ \mathrm{c} \end{array}\right.$ | $\left\lvert\,\right.$ | $\left\lvert\, \begin{aligned} & \vec{\infty} \\ & \infty \\ & \omega \\ & \omega \end{aligned}\right.$ | $\stackrel{\rightharpoonup}{\dot{v}}$ | $\stackrel{\rightharpoonup}{v}$ | $\overrightarrow{~ \stackrel{\rightharpoonup}{\mathrm{O}}}$ | $\begin{aligned} & \vec{i} \\ & \mathrm{G} \\ & \mathrm{v} \end{aligned}$ | $\underset{\sim}{\square}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | $\stackrel{\rightharpoonup}{\boldsymbol{A}}$ | へ | N | $\stackrel{\rightharpoonup}{0}$ | $\stackrel{\rightharpoonup}{0}$ | $\infty$ | $\infty$ | O) | C) | + | I | I | ! | $\stackrel{\rightharpoonup}{\omega}$ | $\stackrel{\rightharpoonup}{\omega}$ | $\underset{\sim}{ \pm}$ | $\underset{\sim}{\sim}$ | $\bullet$ | $\bullet$ | $\checkmark$ | $\checkmark$ | v | $\cdots$ | $\cdots$ | I | I | I | $\left[\begin{array}{ll} \overrightarrow{2} & 1 \\ 0 & 0 \\ 0 & 7 \end{array}\right.$ |
| $\begin{aligned} & c \\ & 1 \\ & \infty \end{aligned}$ | $\stackrel{\rightharpoonup}{\text { i }}$ | $\begin{aligned} & c \\ & 1 \\ & \infty \end{aligned}$ | $\stackrel{\rightharpoonup}{\dagger}$ | $\begin{aligned} & c \\ & 1 \\ & \infty \end{aligned}$ | $\stackrel{\rightharpoonup}{\dot{+}}$ | $\begin{gathered} c \\ 1 \\ \infty \end{gathered}$ | $\stackrel{\rightharpoonup}{\dot{+}} \mid$ | $\begin{aligned} & c \\ & 1 \\ & \infty \end{aligned}$ | $\underset{+}{\dot{+}}$ | $\stackrel{\rightharpoonup}{\mathrm{N}}$ | I | I | I | $\begin{gathered} c \\ 1 \\ \infty \end{gathered}$ | $\stackrel{\rightharpoonup}{\mathbf{+}}$ | $\begin{aligned} & c \\ & 1 \\ & \infty \end{aligned}$ | $\stackrel{\rightharpoonup}{\text { a }}$ | $\begin{aligned} & c \\ & 1 \\ & \infty \end{aligned}$ | $\stackrel{\rightharpoonup}{+}$ | $\begin{gathered} c \\ 1 \\ \infty \end{gathered}$ | $\stackrel{\rightharpoonup}{\dot{1}}$ | $\left\lvert\, \begin{aligned} & 1 \\ & 1 \\ & \infty \end{aligned}\right.$ | $\stackrel{\rightharpoonup}{+}$ | $\begin{aligned} & \text { c } \\ & \vdots \\ & \hline \end{aligned}$ | I | I | I | 흑. |
| $\underset{\sim}{N}$ | N | $\mathrm{N}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\circ}$ | $\stackrel{\rightharpoonup}{\text { a }}$ | へ | $\overrightarrow{0}$ | $\infty$ | $\begin{gathered} \infty \\ \hline 0 \end{gathered}$ | O) | I | I | I | $N$ | N | $\stackrel{\rightharpoonup}{\bullet}$ | - | $\overrightarrow{\mathrm{v}}$ | $\stackrel{\rightharpoonup}{\omega}$ | $\underset{\sim}{ \pm}$ | $\bigcirc$ | $\underset{\sigma}{V}$ | $\underset{\sim}{2}$ | $\cdots$ | I | ! | I | ²0 |
| $\omega$ | $\omega$ | $\omega$ | $\omega$ | N | N | N | N | - | - | - | $\rightarrow$ | - | - | $\omega$ | $\omega$ | $\omega$ | $\omega$ | N | N | N | N | - | - | - | $\rightarrow$ | - | $\rightarrow$ |  |
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