



UNIVERSITI PUTRA MALAYSIA

**AN INVESTIGATION OF COTTON/ EPOXY AND
GLASS/ EPOXYCOMPOSITE CONES SUBJECTED TO
AXIAL COMPRESSIVE LOAD**

ASAD ABDULLAH KHALID

FK 1999 38

**AN INVESTIGATION OF COTTON/ EPOXY AND
GLASS/ EPOXYCOMPOSITE CONES SUBJECTED TO
AXIAL COMPRESSIVE LOAD**

ASAD ABDULLAH KHALID

**DOCTOR OF PHILOSOPHY
UNIVERSITI PUTRA MALAYSIA**

1999



**AN INVESTIGATION OF COTTON/ EPOXY AND
GLASS/ EPOXY COMPOSITE CONES SUBJECTED TO
AXIAL COMPRESSIVE LOAD**

By

ASAD ABDULLAH KHALID

**Thesis Submitted in Fulfillment of the Requirements for the
Degree of Doctor of Philosophy in the Faculty of Engineering
Universiti Putra Malaysia**

April 1999



ACKNOWLEDGEMENTS

First of all I would like to thank my God (ALLAH) for every thing.

I would like to express my sincere gratitude and deep thanks to my supervisor Associate Professor Dr. Barkawi Bin Sahari for his kind assistance, support, advice, encouragement and suggestions throughout this work and during the preparation of this thesis.

I would like to express my appreciation to Dr. Mustafar Bin Sudin and Dr. Mageed Hammoda. Co-supervisors, for their help, suggestions and assistance during preparation of this thesis. My appreciation is also to Dr. Yousif A. Khalid for his assistance, constructive ideas and suggestions during my research projects.

I acknowledge the help from the head of mechanical and manufacturing engineering department Dr. Megat hamdan and the help from Dr. Shamsuddin Sulaiman.

Great thanks to the external examiner Prof. S. A. Meguid from the Department of mechanical Engineering / Toronto University, Canada for his effort, time spent, valid advice and thesis corrections.

Thank to Associate Prof. Baharuddin Hitam and Mr. Aznijar Ahmad for their help. Appreciation is also due to Puan Mahyon, Mr. Sharani, Mohamad Rashid, Tajul Arifin , Ahmed shaifuldeen, Zulkifli, Suliaman and Mr. John. for their help during the experimental work stage of this project.

I would like also to thank all the staff members of the UPM library for their assistance in providing the scientific papers required for this work.

Last but not least, I would like to extend my sincere appreciation to my family, my mother, sisters and my brothers.

TABLE OF CONTENTS

	Page
ACKNOWLEDGEMENTS	11
LIST OF TABLES	vii
LIST OF FIGURES	ix
LIST OF PLATES	xx
NOMENCLATURE	xxi
ABSTRACT	xxiv
ABSTRAK	xxvi
 CHAPTER	
I INTRODUCTION	1
Types of Composite Materials	2
Mechanical Behavior of Composite Materials	4
Manufacturing of Fiber Reinforced Composite Materials	6
Energy Absorption in Composite Materials	7
Objectives of this Study	9
II LITERATURE REVIEW	11
Introduction	11
Material behavior	13
Fiber	13
Matrix Materials	20
Fabrication Methods	24
Hand Lay-up	25
Filament Winding	25
Resin Transfer Molding	26
Energy Absorption	27
Calculation of Specific Energy Absorption	28
Component Behavior	31
Tubular Specimens	31
Modes of Progressive Crushing	36
Geometry Effect	40
Effect of Material Type	50
Fiber Architecture	53
Effect of Testing Conditions	57
Predicting Failure Load	62
Discussion	66
Conclusions	67
III THEORETICAL ANALYSIS	69
Stress-Strain Relation	69
Compliance Matrix for Orthotropic Materials	72
Determination of Strength and Stiffness of Composite Laminates	75

Determination of Material Properties of Orthotropic Materials.....	79	
Determination of the Longitudinal Young's Modulus E_{11}	80	
Determination of Transverse Young's Modulus E_{22}	81	
Determination of Major Poisson's Ratio ν_{12}	82	
Determination of In-Plane Shear Modulus G_{12}	83	
Determination of E_{33} , G_{13} , and ν_{23}	84	
Determination of G_{23} and ν_{23}	85	
Stress-Strain Relation for Plane Stress in an Orthotropic Material ($\theta=0^\circ$ or $\theta=90^\circ$).....	86	
Stress-Strain Relation for a Lamina of Arbitrary Orientation ($\theta \neq 0^\circ$ or $\theta \neq 90^\circ$).....	87	
Lamination Theories of a Composite material.....	90	
Classical Lamination Theory (CLT).....	90	
Effective Stiffness Theory (EST).....	92	
FEM Applications in a Composite materials.....	94	
Discussion.....	96	
IV	EXPERIMENTAL WORK	98
	Filament Winding Equipment Set-up.....	99
	Mandrels Fabrication.....	101
	Test Specimens Fabrication.....	102
	Cones Fabrication.....	102
	Moisture Absorption Specimens,	104
	Discussion.....	104
V	MATERIAL PROPERTIES TESTS.....	106
	Fiber and Matrix Properties.....	106
	Epoxy Resin Properties test.....	106
	Cotton Fiber Properties Test.....	109
	Glass Fiber Properties Test.....	110
	Composite Laminate Tensile Testing.....	112
	Cotton Fiber/Epoxy.....	113
	Glass Fiber/Epoxy.....	115
	Determination of the Composite Materials Properties.....	117
	Tensile Mechanism of failure.....	122
	Conclusions.....	124
VI	EXPERIMENTAL RESULTS	126
	Results of Cylindrical Composite	126
	Introduction.....	126
	Tube Parameter, Material and Test Conditions.....	126
	Discussion.....	132
	Conclusions.....	133
	Results of Single Composite Cones.....	133
	Introduction.....	133
	Cotton Fiber/ Epoxy Single Cones.....	134
	Glass Fiber Epoxy Single Cones.....	141
	Comparison	147

Environmental Effects	150
Cotton Fiber/ Epoxy Cones	154
Glass Fiber Epoxy Cones	156
Comparison	158
Discussion	161
Conclusions	163
Results of Combined Composite Cones	164
Introduction	164
Cotton Fiber/ Epoxy Multiple Cones	165
Glass Fiber/ Epoxy Multiple Cones	169
Reversed Parallel Multiple Cones	171
Discussion	173
Conclusions	175
Experimental Work Error Sources	175
VII FINITE ELEMENT RESULTS	177
Introduction	177
Cone Geometry	177
Cotton Fiber/ Epoxy Cones	178
Glass Fiber/ Epoxy Cones	179
Material Properties	179
Finite Element, Mesh, Loading and Boundary Conditions	180
Results	182
Cotton Fiber/ Epoxy	184
Glass Fiber/ Epoxy	184
Comparison of Results	185
Finite Element and Experimental results	185
Cotton fiber/ Epoxy and Glass Fiber/ Epoxy Results	193
Discussion	194
Conclusions	195
VIII DISCUSSION	196
Introduction	196
Filament Winding Machine Design	197
Factors, Parameters and Limit	197
Equipment Limitation	197
Accuracy	198
Effect of Fiber and Matrix Behavior	198
Fiber Effect	198
Matrix Effect	199
Fiber/ Matrix Volume Ratio	199
Effect of Geometry on Crushing Behavior and Energy Absorption	200
Cylinders and Cones	200
Single and Multiple Cones	201
Effect of Material on Crushing Behavior and Energy Absorption	202
Cotton Fiber/ Epoxy and Glass Fiber/ Epoxy	202
Effect of Moisture on Crushing Energy	203
Finite Element Prediction	203

Method Applied	203
Accuracy of Prediction	204
Limitation	205
IX CONCLUSIONS	206
Suggestions for Further Work	210
REFERENCES	211
APPENDIX	
A Equipment Design calculations	218
B PAFEC Finite Element Commands and Programs	226
C Finite Element Displacement Results	241
VITA	269
Papers Published From the Thesis	269

LIST OF TABLES

Table	Page
1 Mechanical Properties of Selected Natural Fibers	15
2 Mechanical Properties of Selected Man Made Fibers	18
3 Typical Compositions of three Glasses used Man Made Fibers	20
4 Typical Engineering Properties of Thermosetting and Thermoplastic Polymer Matrix Materials	21
5 Calculation Results in Carbon Fiber/ PEEK and Glass Fiber Cloth/ Epoxy Tubes with Experimental Results	64
6 Relation between the Carriage Speed and Parameters of Cotton Fiber / Epoxy Composite Cones	103
7 Relation between the Carriage Speed and Parameters of Glass Fiber / Epoxy Composite Cones	103
8 Relation between the Carriage Speed and Parameters of Cotton and Glass Fiber/Epoxy Composite Cylinders	103
9 Comparison between experimental and literature results for the fiber and epoxy mechanical properties	111
10 Uniaxial Tensile Test Results for Composite Specimens	112
11 Uniaxial Compression Test Results for Cotton Fiber/ Epoxy and Glass Fiber/ Epoxy Composite Cylinders	131
12 Uniaxial Compression Test Results for Cotton Fiber/ Epoxy Composite Cones	138
13 Uniaxial Compression Test Results For Glass Fiber/ Epoxy Composite Cones	144
14 Uniaxial Compression Test Results for Composite Cones at Different Immersion Temperatures	159
15 Uniaxial Compression Test Results for Different Cone Arrangements	172
16 Comparison between slopes for Experimental and Finite Element Results of Figure 90 (Cotton fiber/ epoxy cones, initial diameters are	

	respectively 96, 92 and 93 mm. fiber orientation angle=90°).....	188
17	Comparison between slopes for Experimental and Finite Element Results of Figure 91. (Cotton fiber/ epoxy cones, initial diameters are respectively 96, 92 and 93 mm. fiber orientation angle=80°).....	188
18	Comparison between slopes for Experimental and Finite Element Results of Figure 92. (Cotton fiber/ epoxy cones, initial diameters are respectively 118, 135 and 174 mm. fiber orientation angle=90°).....	189
19	Comparison between slopes for Experimental and Finite Element Results of Figure 93. (Cotton fiber/ epoxy cones, Initial diameters are respectively 118, 135 and 174 mm. fiber orientation angle=80°).....	189
20	Comparison between slopes for Experimental and Finite Element Results of Figure 93. (Glass fiber/ epoxy cones, initial diameters are respectively 96, 92 and 93 mm. fiber orientation angle=90°).....	192
21	Comparison between slopes for Experimental and Finite Element Results of Figure 94. (Glass fiber/ epoxy cones, initial diameters are respectively 96, 92 and 93 mm, fiber orientation angle=80°).....	192
22	Comparison between slopes for Experimental and Finite Element Results of Figure 95. (Glass fiber/ epoxy cones, initial diameters are respectively 118, 135 and 174 mm, fiber orientation angle=90°).....	193
23	Comparison between slopes for Experimental and Finite Element Results of Figure 96. (Glass fiber/ epoxy cones, initial diameters are respectively 118, 135 and 174 mm. fiber orientation angle=80°).....	193

LIST OF FIGURES

Figure		Page
1	Schematic Illustration of Four Stages of Deformation of Fibers, Matrix, and Composite.....	12
2	Relationship between the Strength of Natural Fibers and their Contents and Microfibril angle.....	15
3	Chemical Structure of Celulose.....	17
4	Typical Load- Displacement Curve for a Progressively Crushed Composite Tube.....	29
5	Typical Load- Displacement curve for a Progressively Crushed Composite Cone (Cone angle=22°)	31
6	Schematic Representation of Progressive Folding.....	33
7	Typical Load-Displacement Curve for Progressive Folding I: Fold Initiation, II: Progressive Folding, III: Compaction.....	33
8	Typical Load- Displacement Curve of a Square- Ended Tube of a Brittle Composite Material in Axial Compression	34
9	Schematic Representation of Progressive Crushing. a: Tube with Chamfer at One End, b: Partially Crushed Tube, c: Fully Crushed Tube with Debris Compacted Inside Preventing Further Crushing.....	35
10	Typical Load- Displacement Curve of Tube with Chamfered End Undergoing Progressive Crushing; I: Formation of Crush Zone, II: Progressive Crushing, III: Compaction of Debris.....	36
11	Schematic Representation of Formation of a Splaying Mode Crush Zone Based on Microscopic Examination of Polished Sections....	37
12	Polished Section Through Crush Zone Showing Remains of Debris Wedge and Center-Wall Crack.....	37
13	Schematic Representation of Formation of a Fragmentation - Mode Crush Zone Based on Microscopic Examination of Polished Section....	38
14	Polished Cross-section Through Crush Zone of Woven Glass Cloth/ Epoxy Resin Tube.....	38

15	Variables Influencing the Specific Energy Absorption of the Composite Material.....	39
16	Variation of Specific Energy Absorption with (t/ D ₁).....	40
17	Geometry and Notation of the Conical Shell.....	46
18	Collapse of Thin-Walled $\theta=22^{\circ}$ Cone by Folding.....	49
19	Load-Displacement Curve of Cone Shown in Figure 2.16, t=1.5 mm... .	49
20	Effect of Fiber Orientation on Specific Crushing Stress For Glass Fiber/ Polyester Resin Tubes Crushed at 0.2 mm/s	54
21	Crushing test for composite tube.....	.
22	Fracture aspect and Load-displacement curve in square ended tube....	64
23	Fracture aspect and Load-displacement curve in tapered tube.....	64
24	Initial Mesh in FEM Analysis for Splaying Mode... .	.
25	Assumption in FEM Analysis of Predicted Mean Crushing Load.....	65
26	Component of Stress and Strain in a Rectangular Cartesian Coordinate System.....	70
27	Distinction between ν_{12} and ν_{21}	74
28	Uniaxial Loading in 1-Direction.....	77
29	Uniaxial Loading in 2-Direction.....	77
30	Uniaxial Loading at 45° to the 1-Direction.....	78
31	Torsion Tube Test.....	78
32	Representative Volume Element Loaded in 1-Direstion	80
33	Representative Volume Element Loaded in 2-Direstion.....	81
34	Representative Volume Element Loaded in Shear.....	82
35	Shear Deformation of a Representative Volume Element.....	83
36	Equality in 2 and 3-Direction for Uniformly Distributed Unidirectional Fibers.....	85

37	Unidirectionally Reinforced Lamina	87
38	Helically Wound Fiber-Reinforced Circular cylindrical Shell.....	88
39	Positive Rotation of Principal Material Axis From Arbitrary xy Axis... .	88
40	Laminate Geometry.....	91
41	Filament Winding Equipment Set-up	100
42	Load-Extension Relation for the Matrix (Epoxy Resin With Hardener)	108
43	Load-Extension Relation for Cotton Fiber.....	110
44	Load-Extension Relation for Glass Fiber.... .	111
45	Tensile Test Load-Displacement Relation for Cotton Fiber/ Epoxy Specimen with a Fiber Orientation Angle of; a. 0° , b. 90°	114
46	Tensile Test Load-Displacement Relation, for Glass Fiber/ Epoxy Specimen with a Fiber Orientation Angle of; a. 0° , b. 90°	117
47	Load-Displacement Relation for Cotton Fiber/ Epoxy Composite Cylinders (a. $D_l = 97.4$ mm, b. $D_l = 116.2$ mm).....	128
48	Load-Displacement Relation for Glass Fiber/ Epoxy Composite Cylinders (a. $D_l = 97.4$ mm, b. $D_l = 116.2$ mm).	129
49	Specific Energy Absorption Vs. Diameter for Composite Cylinders (fiber orientation angle= 90° , $D_1=97.4$ mm, $D_2=116.2$ mm).....	131
50	Load-Displacement Relation for Cotton Fiber/ Epoxy Cones (Fiber orientation angle= 90° , initial diameters are respectively 96, 92 and 93 mm).....	136
51	Load-Displacement Relation for Cotton Fiber/ Epoxy Cones (Fiber orientation angle= 80° , initial diameters are respectively 96, 92 and 93 mm.....	136
52	Load-Displacement Relation for Cotton Fiber/ Epoxy Cones (Fiber orientation angle= 90° , initial diameters are respectively 118, 135 and 174 mm).....	137
53	Load-Displacement Relation for Cotton Fiber/ Epoxy Cones (Fiber orientation angle= 80° , initial diameters are respectively 118, 135 and 174 mm).....	137

54	Specific Energy Absorption Vs. Crush Distance for Cotton Fiber/ / Epoxy Cones (Fiber orientation angle=90°, initial diameters are respectively 96, 92 and 93 mm).....	139
55	Specific Energy Absorption Vs. Crush Distance for Cotton Fiber/ / Epoxy Cones (Fiber orientation angle=80°, initial diameters are Respectively 96, 92 and 93 mm).....	140
56	Specific Energy Absorption Vs. Crush Distance for Cotton Fiber/ / Epoxy Cones (Fiber orientation angle=90°, initial diameters are respectively 118, 135 and 174 mm).....	140
57	Specific Energy Absorption Vs. Crush Distance for Cotton Fiber/ / Epoxy Cones (Fiber orientation angle=80°, initial diameters are respectively 118, 135 and 174 mm).....	141
58	Load-Displacement Relation for Glass Fiber/ Epoxy Cones (Fiber orientation angle=90°, initial diameters are respectively 96, 92 and 93 mm).....	142
59	Load-Displacement Relation for Glass Fiber/ Epoxy Cones (Fiber orientation angle=80°, initial diameters are respectively 96, 92 and 93 mm).....	142
60	Load-Displacement Relation for Glass Fiber/ Epoxy Cones (Fiber orientation angle=90° , initial diameters are respectively 118, 135 and 174 mm).....	143
61	Load-Displacement Relation for Glass Fiber/ Epoxy Cones (Fiber orientation angle=80°, initial diameters are respectively 118, 135 and 174 mm).....	143
62	Specific Energy Absorption Vs. Crush Distance For Glass Fiber/ / Epoxy Cones (Fiber orientation angle = 90°, initial diameters are respectively 96, 92 and 93 mm).....	145
63	Specific Energy Absorption Vs. Crush Distance for Glass Fiber/ Epoxy Cones (Fiber orientation angle = 80°, initial diameters are respectively 96, 92 and 93 mm).....	145
64	Specific Energy Absorption Vs. Crush Distance for Glass Fiber/ Epoxy Cones (Fiber orientation angle = 90°, initial diameters are Respectively respectively 118, 135 and 174 mm).....	146
65	Specific Energy Absorption Vs. Crush Distance for Glass Fiber/ Epoxy Cones (Fiber orientation angle=80°, initial diameters are respectively 118, 135 and 174 mm).....	146

66	Load-Displacement Relation for Cotton and Glass Fiber/ Epoxy Cones (Fiber orientation angle=90°, cone angle=5°, initial diameter=96 mm)....	148
67	Specific Energy Absorption Vs. Crush Distance for Composite Cones (Fiber orientation angle=90°, cone angle=5°, initial diameter = 96 mm).....	148
68	Variation of Apparent Weight Gain (M_a), Net Weight Gain (M_g), and Weight Loss (M_L) with Immersion Time (Days) for Cotton Fiber/ Epoxy..	151
69	Variation of Apparent Weight Gain (M_a), Net Weight Gain (M_g), and Weight Loss (M_L) with Immersion Time (Days) for Glass Fiber/ Epoxy...	152
70	Variation of Moisture Content (M_g) with Immersion Time (Days) for Cotton Fiber/ Epoxy.....	152
71	Variation of Moisture Content (M_g) with Immersion Time (days) for Glass Fiber/ Epoxy.....	153
72	Moisture Content Vs. Temperature Relation for Cotton Fiber/ Epoxy....	153
73	Moisture Content Vs. Temperature Relation for Glass Fiber/ Epoxy.....	154
74	Load-Displacement Relation for Cotton Fiber/ Epoxy Cones.....	155
75	Specifi Composite Cones.....	156
76	Load-Displacement Relation for Glass Fiber/ Epoxy Composite Cones.....	157
77	Energy Absorption Vs. Crush Distance for Glass Fiber/ Epoxy Composite Cones.....	158
78	Variation of Energy Absorption with Immersion Temperature.....	161
79	Geometry and Dimensions of the Combined Composite Cones and Cylinders.....	165
80	Load - Displacement Relation for Two Cotton Fiber / Epoxy Cones (Fiber orientation angle=90°, cone angle=5°, initial diameter=96 mm)....	166
81	Specific Energy Absorption Vs. Crush Distance for Two Cotton Fiber/ Epoxy Combined Cones (Fiber orientation angle=90°, cone angle=5°, initial diameter = 96 mm).....	168
82	Load - Displacement Relation for Two Glass Fiber / Epoxy Cones (Fiber orientation angle=90°, cone Angle=5°, initial diameter=96 mm)....	170

83	Specific Energy Absorption Vs Crush Distance for Two Glass Fiber/ Epoxy Combined Cones (Fiber orientation angle=90°, cone angle=5°, initial diameter ~ 96 mm)	170
84	Load-Displacement Relation for Two Composite Cones Arranged in a Reversed Parallel Case (Fiber orientation angle=90°, cone angle=5°, initial diameter =96 mm)	172
85	Specific Energy Absorption Vs Crush Distance for Two Composite Cones arranged in a Reversed Parallel Case (Fiber orientation angle=90°, cone angle=5°, initial diameter = 96 mm)	173
86	Geometry and Dimensions of Composite Cones	178
87	Mesh and Boundary Conditions of Composite Cones	181
88	Deformed Shape of a three-dimensional Composite Cone Sample	182
89	Original and Deformed Shape of Cotton and Glass Fiber/ Epoxy Composite Cones (Load=24 KN)	183
90	Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90, initial diameters are respectively 96, 92 and 93 mm)	186
91	Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80, initial diameters are respectively 96, 92 and 93 mm)	186
92	Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90, initial diameters are respectively 118, 135 and 174 mm)	187
93	Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80, initial diameters are respectively 118, 135 and 174 mm)	187
94	Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90, initial diameters are respectively 96, 92 and 93 mm)	190
95	Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80, initial diameters are respectively 96, 92 and 93 mm)	190

96 Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90, initial diameters are respectively 118, 135 and 174 mm)	191
97 Experimental and Finite Element Results for the Elastic Region of the Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80, initial diameters are respectively 118, 135 and 174 mm)	191
98 Series of Pulleys to Control Winding Speed	218
99 Guide Pulley and Guide Pulley Stand Connections	219
100 Forces on Guide Pulley	221
101 Forces on Guide Pulley Shaft	222
102 Rectangular Weld	224
103 Circular Weld	224
104 Forces on the Guide Pulley Stand	224
105 Tension Device Forces	225
106 Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90°, initial diameters are respectively 96, 92 and 93 mm)	242
107 Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80°, initial diameters are respectively 96, 92 and 93 mm)	242
108 Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90°, initial diameters are respectively 118, 135, and 174 mm)	243
109 Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80°, initial diameters are respectively 118, 135, and 174 mm)	243
110 Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=90°, initial diameters are respectively 96, 92, and 93 mm)	244

111	Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=80°, initial diameters are respectively 96, 92, and 93 mm).....	245
112	Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=90°, initial diameters are respectively 118, 135, and 174 mm).....	245
113	Load-Displacement Relation for Surface Nodes of Cotton Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=80°, initial diameters are respectively 118, 135, and 174 mm).	246
114	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone Angle=5°, fiber orientation angle=90°, initial diameter=96 mm).....	247
115	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone Angle=10°, fiber orientation angle=90°, initial diameter=92 mm)....	247
116	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone Angle=20°, fiber orientation angle=90°, initial diameter=93 mm)... .	247
117	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=5°, fiber orientation angle=80°, initial diameter=96 mm).....	248
118	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=10°, fiber orientation angle=80°, initial diameter=92 mm) ..	248
119	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=20°, fiber orientation angle=80°, initial diameter=93 mm)....	248
120	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=5°, fiber orientation angle=90°, initial diameter=118 mm)...	249
121	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=10°, fiber orientation angle=90°, initial diameter=135 mm)... .	249
122	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=20°, fiber orientation angle=90°, initial diameter=174 mm)... .	249
123	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=5°, fiber orientation angle=80°, initial diameter=118 mm).....	250
124	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=10°, fiber orientation angle=80°, initial diameter=135 mm)....	250
125	Side Nodes Displacement in Y-Direction for Cotton Fiber/ Epoxy Cones (Cone angle=20°, fiber orientation angle=80°, initial diameter=135 mm)....	250

- 126 Side Nodes Displacement in X-Dirction for Cotton Fiber/ Epoxy Cones
(Cone angle=5°, fiber orientation angle=90°, initial diameter=96 mm)..... 251
- 127 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=10°, fiber orientation angle=90°, initial diameter=92 mm).... 252
- 128 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=20°, fiber orientation angle=90°, initial diameter=93 mm) 252
- 129 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=5°, fiber orientation angle=80°, initial diameter=96 mm)..... 253
- 130 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=10°, fiber orientation angle=80°, initial diameter=92 mm)..... 253
- 131 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=20°, fiber orientation angle=80°, initial diameter=93 mm).... 253
- 132 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=5°, fiber orientation angle=90°, initial diameter=118 mm).... 254
- 133 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=10°, fiber orientation angle=90°, initial diameter=135 mm).... 254
- 134 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=20°, fiber orientation angle=90°, initial diameter=174 mm).... 254
- 135 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=5°, fiber orientation angle=80°, initial diameter=118 mm).... 255
- 136 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=10°, fiber orientation angle=80°, initial diameter=135 mm)... 255
- 137 Side Nodes Displacement in X-Direction for Cotton Fiber/ Epoxy Cones
(Cone angle=20°, fiber orientation angle=80°, initial diameter=174 mm)... 255
- 138 Load-Displacement relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90°, initial diameters are respectively 96, 92, and 93 mm)..... 256
- 139 Load-Displacement relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80°, initial diameters are respectively 96, 92, and 93 mm)..... 257
- 140 Load-Displacement relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=90°, initial diameters are respectively 118, 135, and 174 mm)..... 257

141	Load-Displacement Relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in Y- direction, fiber orientation angle=80°, initial diameters are respectively 118, 135, and 174 mm).....	258
142	Load-Displacement Relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=90°, initial diameters are respectively 96, 92, and 93 mm).....	258
143	Load-Displacement Relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=80°, initial diameters are respectively 96, 92, and 93 mm).....	259
144	Load-Displacement Relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=90°, initial diameters are respectively 118, 135, and 174 mm).....	259
145	Load-Displacement Relation for Surface Nodes of Glass Fiber/ Epoxy Cones (Displacement in X- direction, fiber orientation angle=80°, initial diameters are respectively 118, 135, and 174 mm).....	260
146	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=90°, initial diameter=96 mm).....	261
147	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=90°, initial diameter=92 mm).....	261
148	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=90°, initial diameter=93 mm).....	261
149	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=80°, initial diameter=96 mm).....	262
150	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=80°, initial diameter=92 mm).....	262
151	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=80°, initial diameter=93 mm).....	262
152	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=90°, initial diameter=118 mm).....	263
153	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=90°, initial diameter=135 mm)...	263
154	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=90°, initial diameter=174 mm)...	263

155	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=80°, initial diameter=118 mm).....	264
156	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=80°, initial diameter=135 mm)....	264
157	Side Nodes Displacement in Y-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=80°, initial diameter=135 mm) ...	264
158	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=90°, initial diameter=96 mm).....	265
159	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=90°, initial diameter=92 mm).....	265
160	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=90°, initial diameter=93 mm).....	265
161	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=80°, initial diameter=96 mm).....	266
162	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=80°, initial diameter=92 mm)....	266
163	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=80°, initial diameter=93 mm).....	266
164	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=90°, initial diameter=118 mm).....	267
165	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=90°, initial diameter=135 mm)...	267
166	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=90°, initial diameter=174 mm)...	267
167	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=5°, fiber orientation angle=80°, initial diameter=118 mm).....	268
168	Side Nodes Displacement in X-Direction for Glass Fiber/ Epoxy Cone (Cone angle=10°, fiber orientation angle=80°, initial diameter=1	268
169	Side Nodes Displacement in X-Direction For Glass Fiber/ Epoxy Cone (Cone angle=20°, fiber orientation angle=80°, initial diameter=174 mm)...	268

LIST OF PLATES

Plate		Page
1	Filament Winding Machine Test Rig	98
2	Mandrels Fabrication	101
3	Epoxy Resin Moulds	107
4	Epoxy Resin Specimens	107
5	Cotton Fiber Tensile Test	109
6	Glass Fiber Tensile Test	111
7	Cotton Fiber/ Epoxy Specimens with 90° Fiber Orientation Angle	113
8	Cotton Fiber/ Epoxy Specimens with 0° Fiber Orientation Angle	114
9	Glass Fiber/ Epoxy Specimens with 90° Fiber Orientation Angle	116
10	Glass Fiber/ Epoxy Specimens with 0° Fiber Orientation Angle	116
11	Computerized Control Instron machine	127
12	Undeformed Shape for Composite Cylinders ($D_1=97.4$ mm, $D_2=116.2$ mm)	129
13	Deformed Shape for Composite Cylinders ($D_1=97.4$ mm, $D_2=116.2$ mm)	130
14	Composite Cones with Different Fiber Orientation Angles, Parameters, and Different Cone Angles	149
15	Crushed Composite Cones	149
16	Undeformed Shape of Composite Cones (Cone angle=5°)	160
17	Deformed Shape of Composite Cones at Different Immersion Temperatures	160
18	Undeformed Shape of the Two Combined Composite Cones Arranged in Series	167
19	Undeformed Shape of the Two Combined Composite Cones Arranged in Parallel	167
20	Deformed Shape of the Two Combined Composite Cones	174

NOMENCLATURE

Symbol	Units
A Cross-section area	m^2
D ₁ , D ₂ Internal and External Diameters of the Section Undergoing Crush	mm
D _i Initial Diameter of the cone	mm
E Young's Modulus	GN/m^2
E _f Young's Modulus of fiber	GN/m^2
E _m Young's Modulus of Matrix	GN/m^2
E _s Specific Energy Absorption	KJ/Kg
E ₁ or E ₁₁ Longitudinal Young's Modulus (direction-1)	GN/m^2
E ₂ or E ₂₂ Transverse Young's Modulus (direction-2)	GN/m^2
E ₃ or E ₃₃ Transverse Young's Modulus in the Direction of Laminate Thickness (direction-3)	GN/m^2
E _{\text{45}} Transverse Young's Modulus at 45° to the Direction -1	GN/m^2
FEM Finite Element Method	—
G ₁₂ In-plane Shear Modulus (in the 1-2 Planes)	GN/m^2
G ₁₃ Transverse Shear Modulus (in the 1-3 Planes)	GN/m^2
G ₂₃ Transverse Shear Modulus (in the 2-3 Planes)	GN/m^2
h _C Crush Distance	mm
K Collapse Ability of the tube	—
L Length	mm
M, m mass	kg
M _a : Apparent weight gain	kg
M _g : Net weight gain	kg

M _L :	Weight loss.....	kg
N:	Rotational Speed	r.p.m
P:	Applied load	kN
\bar{P} :	Mean Crush Load	kN
PEEK:	Polyether ether keton	—
Q _{ij} :	Stiffness Matrix (i, j = 1, 2,...,6).....	—
r:	Radius	mm
S _i :	Initial Crush Distance	mm
S _{ij} :	Compliance matrix, (I, j=1,2,...,6)	—
S, S _f S _b :	Displacements at Arbitrary, Folded Zone, and at Fully Folded Tubes Respectively.....	mm
t:	Wall Thickness	mm
V:	Carriage Speed	m/s
V _f :	Fiber Volume Fraction.....	—
V _m :	Matrix Volume Fraction.....	—
W _o :	Weight of the dried specimen before immersion.....	gm
W _w :	Weight of the wet specimen after immersion.....	gm
W _d :	Weight of the dried specimen after immersion.....	gm
ε :	Strain.....	—
θ :	Fiber orientation angle Relative to a Global Laminate Axis	Degree
α :	Cone Semivertex Angle	Degree
σ :	Crush Stress	N/m ²
$\bar{\sigma}$:	Mean Crush Stress	N/m ²

$\sigma_1, \sigma_2, \sigma_3$ Normal Stress Components in the Direction of 1, 2 and 3	N/m ²
τ_1, τ_5, τ_6 Shear Stress Components in the Plane of 2-3 1-3 and 1-2	N/m ²
$\varepsilon_1, \varepsilon_2, \varepsilon_3$ Normal Strain Components in the Direction of 1, 2 and 3	N/m ²
$\varepsilon_4, \varepsilon_5, \varepsilon_6$ Shear Strain Components in the Plane of 2-3, 1-3 and 1-2	N/m ²
ρ Density of the Composite material	(kg/m ³)
$\sum ., \sum_c$ Specific Crush Stress	N m/kg
ν Poisson's Ratio	—
ν_y Poisson's Ratio for Transverse Strain in the j Direction When Stressed in the i Direction	—
ν_{12} Major Poisson's Ratio	—
ν_{13} Transverse Poisson's Ratio	—
ν_{23} Transverse Poisson's Ratio in the 2-3 Plane	—
ν_f Poisson's Ratio of Fiber	—
ν_m Poisson's Ratio of Matrix	—

Abstract of thesis presented to the Senate of Universiti Putra Malaysia in
fulfillment of the requirements for the degree of Doctor of Philosophy

**AN INVESTIGATION OF COTTON/ EPOXY AND GLASS/ EPOXY
COMPOSITE CONES SUBJECTED TO AXIAL COMPRESSIVE LOAD**

By

ASAD ABDULLAH KHALID

April 1999

**Chairman: Associate Professor Ir. Dr. Barkawi Bin Sahari,
B.Sc. (Hons), Ph.D. MIEM, P. Eng.**

Faculty : Engineering

An experimental and finite element investigation of cotton fiber/ epoxy and glass fiber/ epoxy composite cones and cylinders were carried out under axial compressive loading. A filament winding equipment have been designed and fabricated to produce the different cones and cylinders required for this project. Throughout this investigation, cones of 5°, 10° and 20° angles, for two fiber orientation angles of 90° and 80° were studied. The effect of quasi-static axial compressive load and specific energy absorption for single cylinder and cone were studied. Besides that, the effect of arrangement type for two cones on the standing load and energy absorption were also examined.

The effect of moisture absorption on the load capability and on the energy absorption of the composite cones have been carried out under axial loading. This was carried out for cones of 5° angle and 90° fiber orientation angle. Cones tested were preconditioned by total immersion in to a distilled hot water at 35 °C, 50°C, 65°C and 80°C for different periods ranging from 24 hour to saturation time.

Mechanical properties of the composite material were evaluated experimentally by the testing of tensile specimens for composites, fiber and matrix. Another set of specimens were also tested for the moisture content effect.

Results from this study show that cylinders under axial compression tests indicate better stable crushing behavior than cones. For all cases, glass/epoxy cones or cylinders show higher absorption energy than cotton/epoxy type by 5% to 12.5% for the different cases.

It was found that a significant improvement in the crushing load and energy absorption occurs when using single cones of fiber orientation angle of 80° instead of 90° and the difference was very significant when using cones angles of 20° instead of 5°. Cones arranged in ordinary parallel stands higher load of 27.7% and higher specific energy absorption of 28.3% than similar cones arranged in series for glass/epoxy type. These percentages were 29.7% and 29.4% respectively for cotton/epoxy cones.

Comparison for load-displacement relations. were done between cones with and without moisture preconditioning. It was found that the crushing energy absorption decreases with increase in moisture content

Finite element study has also been carried out for similar cones. Surface and side nodes displacements were obtained for cotton and glass/epoxy cones under axial compression loading. The slope of the elastic region for the different cones studied was compared with the experimental results and found in the range between 1.73% to 14.44%.

Abstrak tesis dikemukakan kepada Senat Universiti Putra Malaysia
Sebagai Memenuhi keperluan untuk Ijazah Doktor Falsafah

**PENYIASATAN KEATAS KON RENCAM BENANG KAPAS/ EPOKSI
DAN KACA/ EPOKSI YANG DIBAWAH BEBAN MAMPATAN PAKSI**

Oleh

ASAD ABDULLAH KHALID

April 1999

Pengerusi: Professor Madya Ir. Dr. Barkawi Bin Sahari,
B.Sc. (Hons), Ph.D. MIEM, P. Eng.

Fakulti : Kejuruteraan

Satu eksperimen dan pengkajian unsur terhingga komposit kon dan silinder bagi gentian kapas/ epoksi dan gentian kaca/ epoksi adalah dijalankan dengan bebanan tekanan sepaksi. Peralatan belitan filamen direkabentuk dan dipasang untuk menghasilkan kon dan silinder yang berbeza yang diperlukan untuk projek ini. Melalui pengkajian ini, kon bersudut 5° , 10° dan 20° , untuk dua orientasi gantian bersudut 90° dan 80° telah dikaji. Kesan beban tekanan kuasi-statik sepaksi dan penyerapan tenaga spesifik untuk silinder tunggal dan kon telah dikaji. Selain itu, kesan dari jenis penyesuaian untuk dua kon semasa beban berdiri dan penyerapan tenaga turut diperiksa.

Kesan penyerapan kelembapan ke atas keupayaan bebanan dan penyerapan tenaga bagi kon komposit telah dijalankan di bawah beban sepaksi. Ianya dijalankan bagi kon bersudut 5° dan orientasi gentian bersudut 90° . Kon-kon yang diuji telah dirawat dengan merendam keseluruhannya ke dalam air panas pada suhu 35° , 50° , 65° dan 80° untuk jarak masa yang berbeza dari 24 jam.

Sifat-sifat mekanikal untuk bahan komposit telah dinilai secara eksperimen dengan ujian tegangan spesimen untuk komposit, gentian dan matriks. Satu set eksperimen yang lain turut diuji untuk kesan kandungan kelembapan.

Keputusan daripada kajian ini menunjukkan bahawa ujian silinder yang ditindaki mampatan sepaksi menunjukkan tingkah-laku perlanggaran stabil yang lebih baik daripada kon. Untuk kesemua kes, kon kaca/ epoksi atau silinder menunjukkan penyerapan tenaga yang lebih tinggi berbanding untuk kes yang berbeza.

Diperolehi bahawa peningkatan yang nyata di dalam beban perlanggaran dan penyerapan tenaga muncul ketika menggunakan gentian kon tunggal berorientasikan sudut 80° dibandingkan dengan 90° dan perbezaan memang jelas nyata ketika menggunakan kon bersudut 20° berbanding 5° . Kon-kon yang disusun secara selari menahan beban yang lebih tinggi sebanyak 27.7% dan penyerapan tenaga spesifik yang lebih tinggi sebanyak 28.3% daripada kon-kon yang serupa dan disusun secara bersiri bagi jenis kaca/ epoksi. Peratusan bagi kon benang kapas/ epoksi adalah 29.7% dan 29.4 % masing-masing.

Perbandingan untuk perhubungan beban-peralihan. telah dilakukan diantara kon-kon dengan dan tanpa lembapan. Telah diperolehi bahawa penyerapan tenaga perlanggaran berkurang dengan penambahan kandungan lembapan.

Kajian unsur terhingga juga dilakukan untuk kon-kon yang sama. Permukaan dan peralihan titik tepi telah diperolehi untuk benang kapas dan kon kaca/ epoksi di bawah beban mampatan sepaksi. Kecuraman kawasan elastik bagi kon berbeza yang dikaji telah dibandingkan dengan keputusan eksperimen dan diperolehi dalam nilai antara 1.73% ke 14.44%.