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Development of Modular Bio-inspired Autonomous Underwater Vehicle for Close Subsea Asset Inspection

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Abstract: To reduce human risk and maintenance costs, Autonomous Underwater Vehicles (AUVs) are involved in subsea inspections and measurements for a wide range of marine industries such as offshore wind farms and other underwater infrastructure. Most of these inspections may require levels of manoeuvrability similar to what can be achieved by tethered vehicles, called Remotely Operated Vehicles (ROVs). To extend AUV intervention time and perform closer inspection in constrained spaces, AUVs need to be more efficient and flexible by being able to undulate around physical constraints. A biomimetic fish-like AUV known as RoboFish has been designed to mimic propulsion techniques observed in nature to provide high thrust efficiency and agility to navigate its way autonomously around complex underwater structures. Building upon advances in acoustic communications, computer vision, electronics and autonomy technologies, RoboFish aims to provide a solution to such critical inspections. This paper introduces the first RoboFish prototype that comprises cost-effective 3D printed modules joined together with innovative magnetic coupling joints and a modular software framework. Initial testing shows that the preliminary working prototype is functional in terms of water-tightness, propulsion, body control and communication using acoustics, with visual localisation and mapping capability.

Keywords: underwater robotics, biomimetic AUV, biomimetic propulsion, 3D seafloor reconstruction, acoustic communication

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1. Introduction

The use of offshore wind power will play an essential role in our future electricity generation. It is forecast that by 2050, 12 percent of the world's primary energy supply will come from wind energy, and 20 percent of this will come from offshore wind [1] [2]. However, ongoing wear and corrosion from the harsh sea environment drives up cost and introduces downtime to this renewable and clean energy source [3]. To ensure reliable production, regular inspection tasks during high seas up to 100m depth need to be performed in a cost effective and safe manner [4]. These tasks are currently being conducted largely using Remotely Operated Vehicles (ROVs) which generally need tethers and a human operator, or using Autonomous Underwater Vehicles (AUVs), which are limited in their accessibility and manoeuvrability [5] [6]. To extend AUV intervention ability and perform critical inspection tasks, they need to be efficient and flexible in operation. A fish-like AUV with a bending body of a spinal column design that is able to mimic propulsion techniques of living fish can provide efficient thrust at minimum swimming velocities, and higher manoeuvrability in limited spaces during

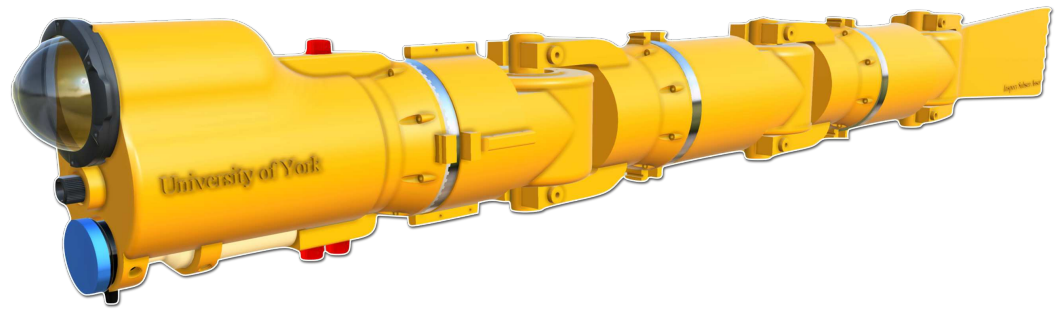


Figure 1. RoboFish CAD Model with Four modules: Head, Two Segments, and Tail

33 sensor data acquisition. RoboFish was created by the project "Autonomous Biomimetic
34 Robot-fish for Offshore Wind Farm Inspection" supported by the EPSRC Supergen
35 Renewable Energy Hub and "Innovating the Future of Bio-Inspired Autonomous, Robots
36 for Offshore Renewable Energy Inspection" supported by the White Rose University
37 Consortium. It was specifically aimed at investigating and exploiting bio-inspired
38 mobility features to facilitate autonomous inspection of offshore infrastructure, and is an
39 agile and efficient biomimetic AUV that will in the near future be able to continuously
40 inspect the foundations of offshore wind turbines and drastically reduce potential risks
41 to divers, maintenance costs, and operational constraints. RoboFish replicates the full-
42 body movement of an eel allowing greater agility and better energy efficiency in close
43 proximity to structures.

44 The understanding of fish swimming behaviours and the exploration of their bene-
45 fits and application in engineering designs is an interdisciplinary research field of signif-
46 icant and ongoing interest [7] [8] [9] [10]. Swimming robots that mimic the techniques
47 of natural swimmers promise to provide an increase in overall swimming performance
48 over conventional thruster propelled systems. Reference [11] shows that thrusters waste
49 energy by generating a vortex perpendicular to the desired thrust direction. On the
50 other hand, aquatic animals are able to efficiently produce a jet in the desired direction
51 through actively and passively controlled body motion. Based on the modular assembly
52 of identical body modules and the resulting equal mass distribution a swimming gait
53 resembling an eel is anticipated. Research into eel locomotion in Reference [12] predicts
54 swimming efficiencies of 0.5 to 0.87 depending on choice of calculation, compared to
55 thruster efficiencies of up to 0.4 in Reference [11]. Among the two main categories of
56 fish swimming, propulsion employing displacement of the centre line of the fish, the
57 so-called Body Caudal Fin (BCF), is suggested to have advantages in speed and long
58 distance travel over flapping fin propulsion of Median Paired Fin [13]. Given that the
59 target application of RoboFish is wind farm inspection, the slender body design of a BCF
60 swimmer is beneficial for the anticipated long-distance travel between wind turbines,
61 maintaining a high level of manoeuvrability through its body flexibility. This also makes
62 more complex routes available that can potentially reduce travel distance. Low noise
63 and mitigated risk of entanglement of continuously rotating parts suggests lower envi-
64 ronmental disturbance. Furthermore, the multi-actuated system allows flexibility and
65 adaptability in entering tight spaces and manoeuvring in complex environments. The
66 long body shape is also appropriate for a modular design, enabling extendibility and
67 flexibility for mission setup of different intervention tasks and increased robustness and
68 survivability in case of isolated module failures.

69 2. Motivation and Background

70 Traditionally, offshore infrastructure such as wind turbines have been inspected
71 in person by humans, with the associated risks to safety in inclement weather and
72 changing underwater conditions. More recently, automated inspection systems such as
73 drones above the water and underwater vehicles have been developed, but with limited
74 autonomy and loitering time. Human intervention to control an underwater vehicle can

75 be quite beneficial, especially during complex inspection tasks which require human
76 judgement and intuition. ROVs have been in existence since 60s [14], and received
77 international attention following the aftermath of the Deepwater Horizon disaster in
78 the Gulf of Mexico in 2010 [15]. In this disaster, human operators sent ROVs fitted out
79 with a saw and manipulators to cut and cap an oil well head at a depth of one mile. The
80 precise control, flexibility and ability to have dangerous jobs done at great depths make
81 ROVs an ideal solution for such inspection tasks in open water. ROVs enable unique
82 access to the underwater world, and can also have robotic arms for object manipulation
83 to provide a safe alternative to perform otherwise costly and dangerous tasks. Being
84 tethered, their advantage over AUVs will, however, be restricted by the complexity of
85 the underwater infrastructure.

86 Unlike ROVs, AUVs have no human intervention in their control loop and they run
87 more independently. AUVs are traditionally used to gather oceanographic data using
88 cameras, SONAR, and other sensing instruments. Using advanced control algorithms,
89 AUVs can run in an autopilot mode for hours and even days without receiving constant
90 operator guidance. REX II [16] from MIT is a unique AUV that can run autonomously and
91 through a remote operator. While loitering around autonomously, Rex II can transmit
92 video images over a wireless channel using a tethered buoy equipped with a radio
93 modem, which is also used in the manual operating mode to enable remote control by an
94 operator. Odyssey IV is an AUV with a pioneered concept known as hovering [17]. It is
95 capable of remaining stationary anywhere up to 6000 meter depth. After AUVs became
96 able to reach great depths and hover around in the oceans, the ability to operate over a
97 longer period of time and cover an extended range were the next features to improve.
98 AUVs can, otherwise, catch only brief glimpses in time and space of the underwater
99 world. Thus, a newer class of more recent AUVs such as Autosub-Long-Range [18] and
100 HUGIN-AUV [19] were developed to push beyond their powers of endurance for longer
101 ranges, and larger sensor payloads. This class of AUVs is particularly useful in offshore
102 surveying applications.

103 Although the aforementioned sophisticated AUVs are extremely capable, they are
104 not the optimal platform to operate in shallow water and inspect assets closely in critical
105 locations due to their relatively large size, unbending bodies. Because of the limitations
106 of AUVs and constraints of ROVs in certain applications, a new, low cost, bendable
107 vehicle was needed to efficiently perform research missions in shallow water and inspect
108 subsea assets. This requirement is what initiated the design for RoboFish, a low cost,
109 modular, hovering AUV or wireless ROV. The concept of a flexible subsea vehicle
110 comprising a chain of joints that are collectively able to change shape was previously
111 successfully implemented by Eelume-AS [20]. Eelume demonstrated dexterity and
112 hyper-redundancy that has not been commercially available before in the inspection,
113 maintenance and repair (IMR) applications. During IMR, the vehicle is able to transit
114 over distances and hover around using ducted lateral and vertical thrusters attached
115 along its flexible body. Unlike Eelume, RoboFish does not use any thrusters and has
116 the ability to run both autonomously and remotely controlled by means of an acoustic
117 communication system.

118 Fish-like robots have been an active research area due to the remarkable physical
119 mobility of fish in nature. A review of biomimetic robotic fish, their gaits, and actuators
120 is in [21]. The Eel gait (Anguilliform) is most suitable for the current eel-like body of
121 RoboFish and the trout gait (Subcarangiform) is more likely to show instability in this
122 kind of robot than robotic fish with a trout-like body [22]. The eel gait is used in many
123 similar robot fish and is well known in the literature. Reference [23] shows an underwater
124 snake robot named Mamba created in 2016. These long and slender robots can maneuver
125 through narrow openings and confined areas. Other related fish-like robot projects
126 include Envirobot by EPFL [24] and ACM R5 by Hirose Fukushima Robotics lab in Japan
127 [25]. The Envirobot platform has improved energy use and efficiency than this lab's
128 previous segmented anguilliform swimming robots, and uses an ARM microcontroller

129 in the head unit and additional microcontrollers in each body segment. ACM R5 was
130 developed in 2005 and to be an amphibious snake like robot that undulates its body to
131 move both on land and underwater. ACM R5 uses paddles for water locomotion and
132 passive wheels on land, and uses an advanced control system which includes a CPU, a
133 battery, and motors in each independently-operating segment. Segments communicate
134 to coordinate and identify automatically how many segments are joined, providing the
135 ability to remove, add, and exchange segments freely.

136 In this paper, we show some new features that RoboFish includes that extend
137 the state of the art. This paper is intended as a high level overview of the modular
138 RoboFish architecture which uses magnetically coupled joints to form an eel-type body.
139 We consider the way they are applied in RoboFish to be essential for fulfilling several
140 fundamental requirements that are common to many modular autonomous underwater
141 systems. These include: a single universal end to end communications system; a modular
142 control and software architecture using off the shelf parts for cost effectiveness; and
143 a physical embodiment that is 3D printable yet fully enclosed and watertight without
144 the need for rotary seals. This paper describes the first working prototype of RoboFish
145 that is equipped with an acoustic modem, a SONAR rangefinder, a camera, and uses
146 computer vision for close range navigation and inspection of structures, with the ability
147 to build complete visual models of the structure using 3D reconstruction methods. This
148 prototype is a cost effective underwater platform and could be spun out to a successful
149 commercial product.

150 The paper is organised as follows: Section 1 is an introduction; Section 2 provides the
151 motivation and background; Section 3 discusses the system design; Section 4 describes
152 the vision system; Section 5 describes the acoustic communication system; Section 6 is
153 the locomotion control design of the RobotFish; Section 7 presents the outcomes of initial
154 testing; Section 8 presents ideas for future work; Section 9 concludes the paper.

155 3. RoboFish Design

156 Development of a modular bio-inspired autonomous underwater vehicle for close
157 subsea asset inspection is a task of extraordinary hardware and software challenges
158 (shown in Figure 1). Splitting a protective, watertight 3D printed enclosure into jointed
159 segments, collectively mimicking the motion of a fish is an example of these challenges.
160 To overcome this, innovative mechanical and electronic modular designs were created
161 as this section introduces.

162 3.1. Vehicle Requirements

163 The current RoboFish design was created within the scope of offshore wind farm
164 inspection. While the mission of RoboFish is clear, there were a number of other re-
165 quirements that had to be involved into the design such as affordability, underwater
166 docking, manoeuvrability, and acoustic remote control. To meet all the requirements, the
167 academic and industrial project partners were involved in early design meetings. The
168 following list outlines the partners that were involved in defining the current RoboFish
169 prototype's requirements.

- 170 • University of York (Intelligent Systems and Nanoscience Group and Underwater
171 Communication Group)
- 172 • University of Strathclyde (Computational Fluid Dynamics and Fluid Structure
173 Interaction Research Group)
- 174 • Supergen ORE Hub
- 175 • PicSea Ltd
- 176 • EC-OG Ltd
- 177 • Offshore Renewable Energy Catapult

178 Consulting with the aforementioned partners, the budget boundaries were defined
179 in order to avoid involving materials, features and characteristics that were beyond the
180 budget. Next, through collective research and engineering discussions, the minimum

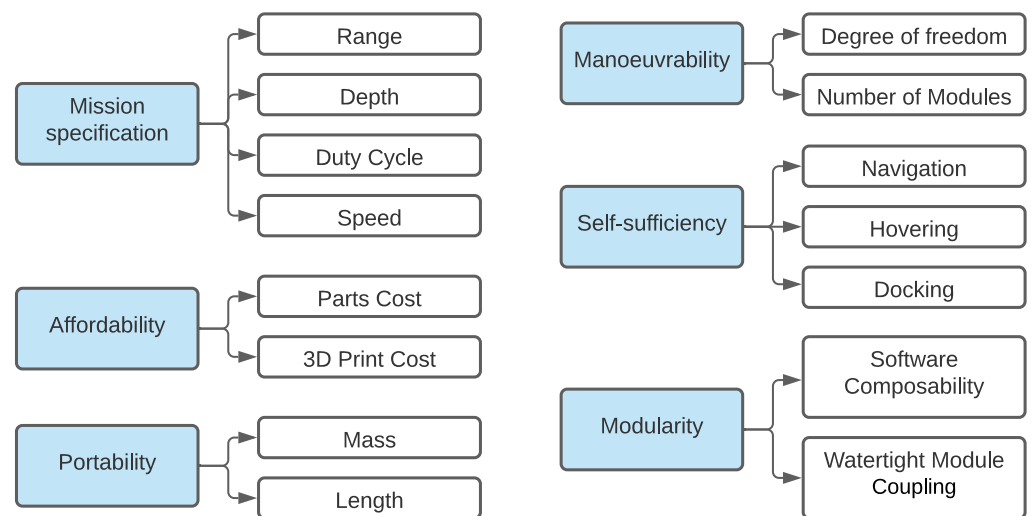


Figure 2. RoboFish's Mapping of Top-level Design Parameters to KPAs.

181 requirements to operate RoboFish in the ocean environment around wind farms was
 182 defined. Finally, the type of data required in inspection missions was decided. The
 183 primary RoboFish requirements defined in the early design stage are:

- 184 • Manoeuvrability
- 185 • Affordability
- 186 • Portability
- 187 • Modularity
- 188 • Self-sufficiency

189 3.2. Key Performance Attributes

190 Ideally, all design requirements are defined at the top-level to ensure that the
 191 mission of RoboFish is comprehensively covered. In the design process of RoboFish, the
 192 attributes that ensure meeting the minimum design requirements were further defined.
 193 This was achieved by creating Key Performance Attributes (KPAs) as depicted in Figure
 194 2. KPAs were linked to the top-level design requirements in order to determine how
 195 RoboFish would meet the overall requirements of a subsea asset inspection mission.
 196 The current RoboFish KPAs are determined based on the mission of offshore wind farm
 197 inspection and are measurable design characteristics that control the overall effectiveness
 198 of the RoboFish design. The KPAs for the current prototype are listed in Table 1. Based
 199 on the top-level design requirements, a decision matrix was created to determine the
 200 best off-the-shelf options with regards to batteries, cameras, servos and micro-controllers.
 201 Using KPAs, associated weights are used to evaluate each decision matrix. In general,
 202 the author were guided by a design philosophy that can be quoted as:

203 Design a low cost, modular AUV to perform underwater inspection around
 204 complex structures. To keep costs at minimum, off-the-shelf parts and acces-
 205 sible additive manufacturing technologies will be used. The vehicle will be
 206 easy to launch, capture videos, recharge, and return to a home location with
 207 minimum or no human intervention.

208 3.3. Mechanical Design

209 RoboFish is composed of several separate body segments with a head at one end
 210 and a caudal fin at the other end. The segments are joined together using an innovative
 211 magnetically coupled joint. This allows it to have the required multiple degrees of
 212 freedom in its agility in order to move very precisely by aiming its head and undulating

Table 1: RobotFish Key Performance Attributes (KPA's)

Attribute	Objective
Depth [m]	100
Mission Duration [hrs]	3
Weight [kg]	30
Length [m]	1.9
Duty Cycle [%]	75
Modular	Yes
Speed [knot]	0.5

213 its body. With this type of locomotion, RoboFish features greater agility in close proximity
 214 to structures compared to conventional underwater vehicles. The current RoboFish
 215 prototype is developed using off-the-shelf parts and a common 3D printing technology,
 216 i.e. Fused Deposition Modelling (FDM). The prototype currently consists of three
 217 sections due to space constraints of laboratory testing. Being modular, it is scaleable
 218 and expandable. Five sections have been created and can be assembled easily during
 219 field testing to produce longer operation time, more efficient movement and higher
 220 agility. Buoyancy control is necessary for long-term loitering capability of biomimetic
 221 vehicles, and the buoyancy control of RoboFish is currently still being refined in design
 222 as the miniaturization and pressure capability of such a buoyancy unit is a considerable
 223 challenge. To allow pitch control, one buoyancy unit will be ultimately installed in each
 224 segment of RoboFish, and they will operate independently to trim the attitude of the
 225 vehicle. The buoyancy units will draw a small amount of water from a port outside
 226 the body segment and compress the air inside to increase the mass of the segment a
 227 small amount, enough to offset the buoyancy of the vehicle for rising and diving. Roll is
 228 statically limited by placing the batteries low in the body.

229 3.3.1. Body Segment

230 This is a 3D printed enclosure using Acrylonitrile Styrene Acrylate (ASA) material.
 231 The primary part of the enclosure takes the form of cylinder of 9.3 cm internal diameter
 232 and 23.3 cm length, as shown in Figure 3. The total length of a segment can be variable
 233 with any modifications that are needed, but the length of the current configuration is
 234 43cm due to the size of the servomotors used. To reach the inside of the enclosure,
 235 O-ringed stainless steel rings with a male-to-female fit are used to hold the two parts of
 236 the enclosure together. This allows convenient disassembly while keeping the system
 237 watertight under high pressure. The enclosure is designed with a fork at one end to
 238 interlock with the rotor of the following segment, whereas the other end of the enclosure
 239 is fused to a magnetic coupling joint containing a rotor. The top of the enclosure allows
 240 wire entry via M10 penetrators, making a waterproof, high-pressure seal to pass Ethernet
 241 cable into the segment. The bottom of the segment is fitted with a M10 plugged vent,
 242 allowing trapped pressure to escape from the segment while it is being closed. This is
 243 also used for testing water-tightness on the segment using a vacuum pump inserting
 244 into the enclosure vent. Segments are joined together using a magnetic-coupling joint
 245 that allows a servo in each joint to rotate an external rotor that in turn rotates an internal
 246 rotor to move the next joint connected to the fork. Four guides with holes are built in on
 247 the outside circumference to allow the attachment of fins, ballast, or other accessories
 248 as required. Internally, components are mounted on a 3D printed mounting plate. The
 249 servo fits into a 3D printed frame moving on linear rails, working as a tilting drawer to
 250 provide the required tension for the timing belt by adjusting the sliding servo on the
 251 rails and locking it in place with two screws.

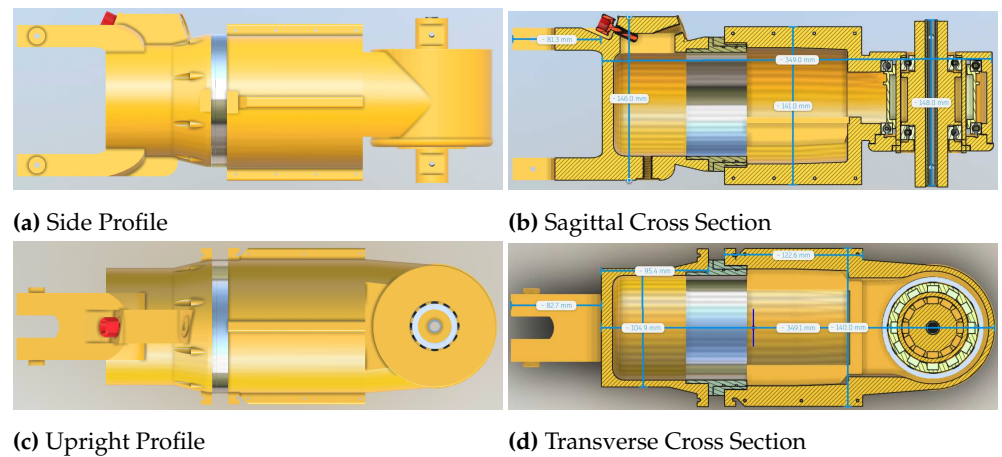


Figure 3. RobotFish Perspectives of a Segment's Cross Sections.

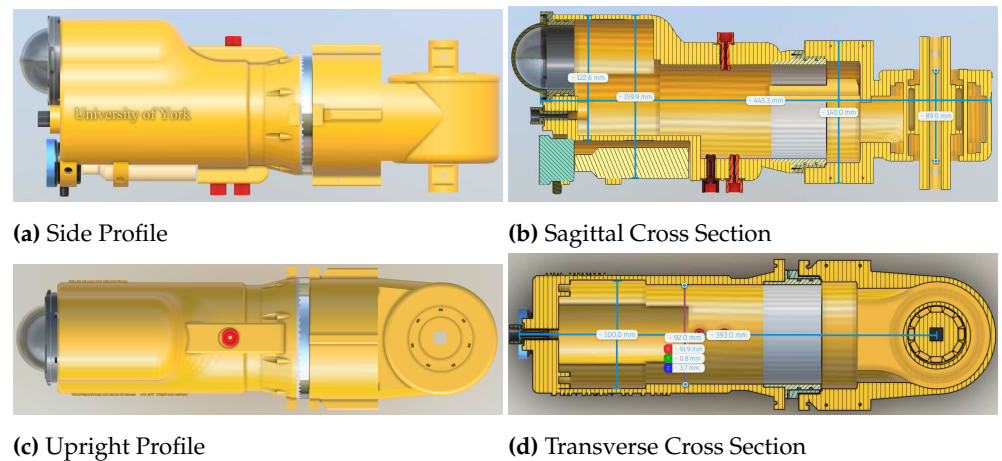


Figure 4. RobotFish Perspectives of the Head's Cross Sections

252 3.3.2. Head

253 This is a modified segment with the same 9.3cm diameter cylindrical enclosure,
 254 but with a front end that appears like a cockpit, allowing the attachment of clear acrylic
 255 dome end cap. The dome shape allows for extra room within the head for additional
 256 two or more cameras or sensors. It gives the camera a wider view than that of a flat end
 257 cap. It is very transparent and does not warp or distort camera images. The dome is
 258 fit into the head using a flange that has a double O-ring seal. Like the other segments,
 259 the head enclosure is fit with a pressure releasing vent and two cable penetrators. It is
 260 also provided with an additional M10 penetrator at the nose of the head, allowing a
 261 waterproof high-pressure seal to pass a 4-8mm tether into the head (should it be required).
 262 To mount the acoustic modem and rangefinder on the head without being obstructed, the
 263 head has an external hollow at the bottom, in which both devices are placed. Internally,
 264 like in the segment, components are mounted on a 3D printed mounting plate and a
 265 servo is fitted into a pull-on 3D printed frame (shown in Figure 4).

266 3.3.3. Tail

267 This is modelled after a caudal fin directly connected to a magnetic joint that en-
 268 ables active control of the fin motion, manoeuvrability and thrust generation for the
 269 overall body. An appropriate fin design can contribute to the overall device stability and
 270 manoeuvrability. Many species use their caudal fin as the main propulsive and manoeu-
 271 vring appendage in addition to the body. For example, almost all of the thrust comes
 272 from the caudal fin for *Thunnus albacares* and *Acanthocybium solanderi* as suggested

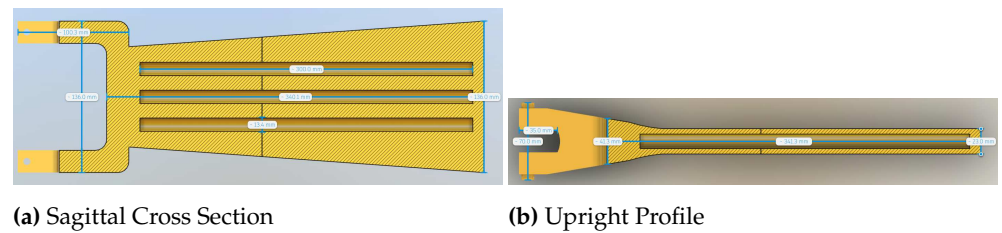


Figure 5. RobotFish Perspectives of the Tail's Cross Sections.

273 by Fierstine and Walters (1968) in [26]. Moreover, the tail may also help produce lift force
274 to balance gravity and buoyancy [27]. In the current design, the caudal fin is directly
275 attached to an actuated joint (shown in Figure 5). This makes it possible to optimise the
276 interaction between the body and tail to enhance propulsion performance and achieve
277 manoeuvrability, e.g., braking, when necessary. The caudal fin in this work has another
278 function to provide additional buoyancy by using a hollow design. In this way, the mass
279 of the caudal fin itself is decreased and it also reduces the energy consumption when the
280 joint servo actuates the rotation of the tail.

281

282 Using Computational Fluid Dynamics (CFD) techniques and Fluid Structure In-
283 teraction (FSI) numerical solvers, it was possible to numerically study the propulsion
284 performance ahead of the manufacturing stage. This provides insights into the structural
285 design and material selection. Using a fully coupled FSI numerical solver consisting of
286 a finite volume method based fluid solver and finite element method based structural
287 solver [28], a preliminary analysis was performed on the motion control of the simplified
288 system [29]. The caudal fin was simplified as a 2D cross-section in rotation locomotion.
289 The yaw angle was a result of PID control with feedback and the control objective is to
290 find the yaw angle matching with the specified steady swimming speed. Initial results
291 showed that the medium stiffness is the most favourable in terms of thrust production,
292 which provides insights into our material selection of the caudal fin and locomotion
293 parameters in the design of the AUV.

294

295 The current fin is printed with ASA materials, which are rigid, to manufacture a
296 fish-inspired tail. Subsequently, the project consortium is curious as to whether flexibility
297 can enhance thrust production and, if so, how flexible the fin needs to be to achieve the
298 most thrust improvement. For a real fish, the conformation of flexible fins would be
299 changed as the fin rays and membrane deform under hydrodynamic forces and inertial
300 force. In return, the fin deformation changes the surrounding flow field; and thus, the
301 resultant force conditions of the fin. During the dynamic interplay between the flexible
302 caudal fin and immersed fluid, the propulsive capabilities may be improved significantly
303 compared with cases when a rigid fin is adopted.

304 3.3.4. Magnetic Coupling Joint

305 This is a mechanism that mechanically joins two watertight enclosures together and
306 transmits the torque of a rotary actuator between an outer driving shaft and an inner
307 driven shaft without physical contact. This enables a servomotor in one of the enclosures
308 to actuate the other enclosure and achieve a precise control of angular position, velocity
309 and acceleration of the body. The contact-less bond is created by the magnetic attraction
310 of a number of magnetic blocks evenly distributed on the side surface of the two shafts
311 with opposite polarity. This allows the two enclosures to function like a robotic arm with
312 rotational joint motion. To keep costs to a minimum, off-the-shelf small magnetic bricks
313 were used. Figure 6 illustrates the magnetic joint's internal parts. The recent paper [30]
314 provides additional details about the implementation of RoboFish magnetic coupling
315 joints and how to maximise the transmittable torque with different numbers, types and
316 arrangement of magnetic blocks.

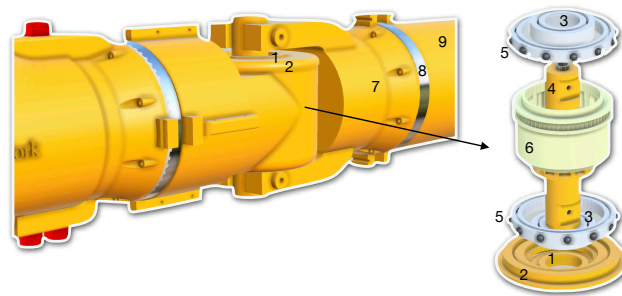


Figure 6. Body parts comprising a segment: 1- Inner joint housing lid; 2- Outer joint housing lid; 3- Zirconia ceramic bearing; 4- Driven shaft; 5- Stainless bearing; 6- Driving shaft; 7- Electronic housing; 8- Stainless male/female rings; 9- Servo housing.

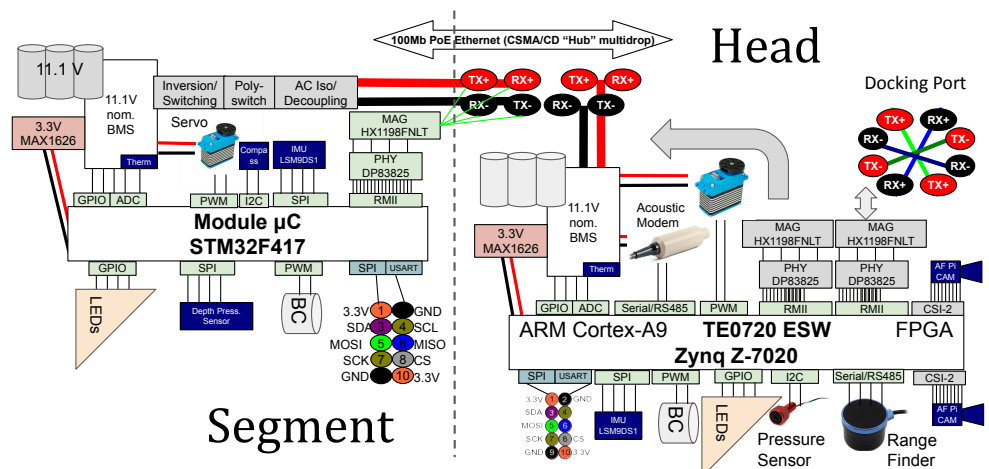


Figure 7. Simplified Electronic System Design of RoboFish; Modular Software and Hardware Architecture; Each Module is Self-contained.

317 3.4. Electronic Design

318 A simplified design schematic of the RoboFish electronic systems is shown in
 319 Figure 7. RoboFish uses a modular software and hardware architecture. Each segment is
 320 self-contained and includes self-managed battery power, internal and external sensor
 321 data, and actuator control using a low-cost microcontroller. Communications and power
 322 transfer between segments are performed through a customised 100 Mbit Ethernet bus,
 323 and it can charge autonomously underwater by docking with a source such as EC-OG's
 324 Subsea Power Hub. The head segment contains a powerful Xilinx Zynq SoC that serves
 325 as a master control node, communications router, and FPGA-accelerated vision platform
 326 with an acoustic rangefinder for position detection. While Wi-Fi communication is only
 327 available on the surface, RoboFish can also communicate at low rates underwater by an
 328 acoustic modem. It currently uses vision for close-range navigation and inspection of
 329 structures, with the ability to build complete visual models of the structure by using 3D
 330 reconstruction methods.

331 3.4.1. Requirements

332 As the RoboFish project aims to produce an autonomous agent, significant pro-
 333 cessing capabilities are required. On board real-time vision processing is required for
 334 navigation. Acoustic communication is required for feedback and issuing control com-
 335 mands during operation. Pressure sensing is required for water depth acquisition. A
 336 SONAR sensor is used for range-finding. Each of these sensory inputs are to be used as
 337 inputs to the control system of the robot. Actuation is produced using servo motors. The
 338 system of inputs and outputs is summarised in Figure 8.

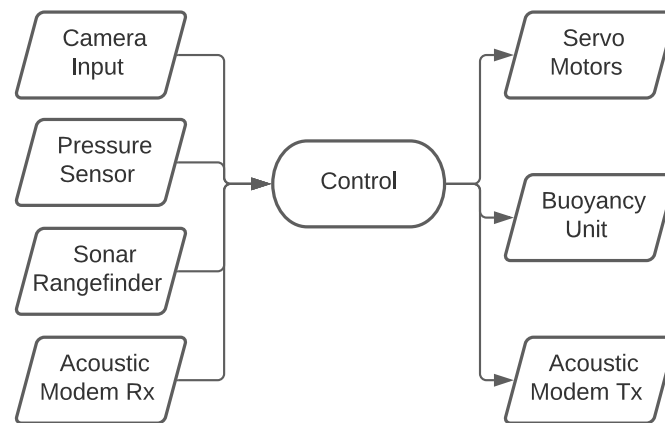


Figure 8. RoboFish Control Requirements

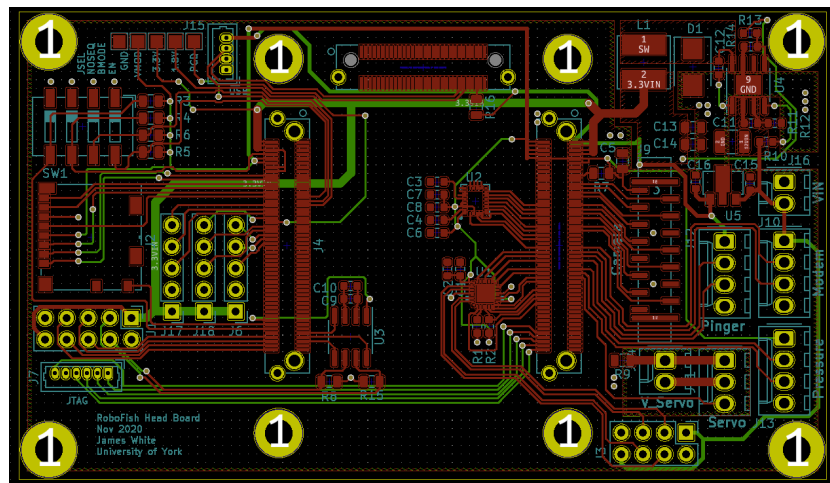


Figure 9. RobotFish Carrier Head board: a carrier PCB designed to contain all of the necessary hardware for interfacing the TE0720 SoM with the rest of RoboFish, programming the SoM and Regulating DC supplies; Either MIPI CSI-2 connector and USB is used for camera interfacing. SD card slot is provided; Either CAN or Ethernet is used for communication; LSM9DS1 IMU is used to provide orientation awareness.

339 3.4.2. Hardware choices

340 To fulfil the requirements stated in the previous section, while also making the
 341 platform upgradable in the future, the Xilinx Zynq 7000 SoC platform was chosen for the
 342 main processor of the system. The Zynq 7000 SoC is built around a hybrid processor and
 343 FPGA architecture. It consists of two ARM Cortex-A9 processor cores and Artix-7 FPGA
 344 programmable logic, with a high bandwidth AMBA AXI interface between them. This
 345 platform enables rapid development of software systems using a Linux operating system
 346 on the processor cores, with the ability to offload processor intensive tasks to the FPGA
 347 fabric. Offloading demanding tasks to the FPGA speeds up execution time for tasks like
 348 vision processing with potential power saving benefits too, which is important for a
 349 battery powered autonomous vehicle such as this. The FPGA fabric can also be used to
 350 create an inter-segment communications controller for communicating between the head
 351 and other segments without sacrificing processor time, resulting in higher-reliability
 352 communication. For the other segments in the robot, the STM32 platform was chosen.
 353 Each segment is a modular element of the system, which accelerates development and
 354 upgradability.

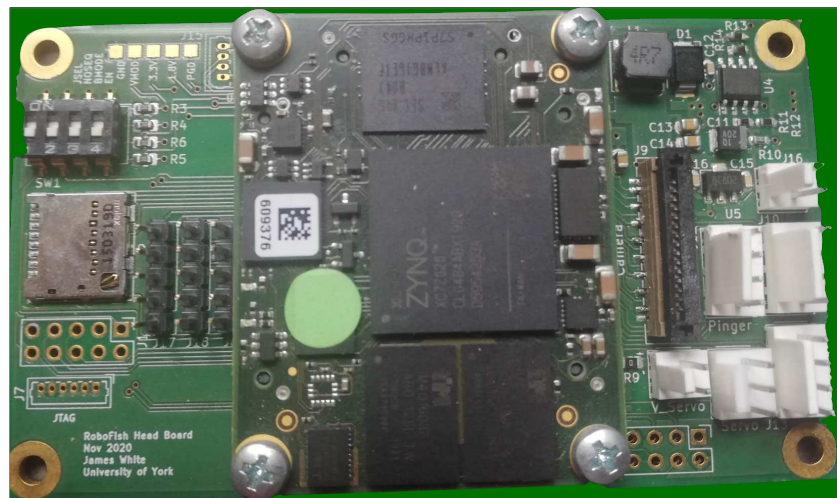


Figure 10. RobotFish Head Carrier PCB with the TE0720 SoM.

3.4.3. Hardware implementation

Head board: The head board is based around a Trenz electronic TE0720 system on Module. This module incorporates the Zynq 7020 SoC, a 1 GB DDR3 RAM, 32 MB QSPI flash for configuration, an 8 Gbyte E.MMC flash for non-volatile storage, along with the power supply and configuration electronics for the SoC. This module was chosen over creating a custom board to accelerate development and ease upgradability (shown in Figure 9). If additional processing power and FPGA fabric is required in the future, this module can be swapped for a more powerful one without affecting the carrier board.

The carrier PCB, shown in Figure-10, contains all of the necessary hardware for interfacing the Trenz SoM with the rest of Robofish, programming the SoM and regulating the battery power. Camera interfacing can be accomplished using either a MIPI CSI-2 connector or USB. An SD card slot is provided to increase onboard non-volatile storage. For communication with other modules in the system, CAN was used for initial testing, and Ethernet was chosen as the final solution. Power is transferred between modules by using a modified power-over-ethernet (PoE) methodology with the DP83825 PHY chip and HX1198FNLT transformer IC. It also contains an LSM9DS1 IMU to provide orientation awareness of the head segment. The head also interfaces with the acoustic modem and SONAR rangefinder via RS-485 bus and breaks out GPIO pins used to drive LEDs, one PWM signal that controls the servo that drives the movement of the segment, and another PWM signal to be used for a buoyancy control unit that is still in development as of this writing. A general SPI and power pin header is provided for future expansion also.

Segment board: The segment board is built around an STM32F417 Microcontroller. This serves as a networked extension to the robots capabilities in a segment. It communicates with the head board using CAN bus (initial testing) or Ethernet with PoE, and contains all of the necessary IO for any servos or sensors that may be required. It also contains an LSM9DS1 IMU for orientation awareness (shown in Figure 11), and breaks out control pins for driving LEDs and the servo and a buoyancy control unit with PWM, and the general SPI and power pin header.

4. Underwater Vision

While visual simultaneous localisation and mapping (SLAM) has seen impressive development for autonomous ground vehicles (AGVs) [31], unmanned aerial vehicles (UAVs) [32] and unmanned underwater vehicles [33], the technical challenges presented by underwater environments have hindered progress for AUVs, particularly in real-

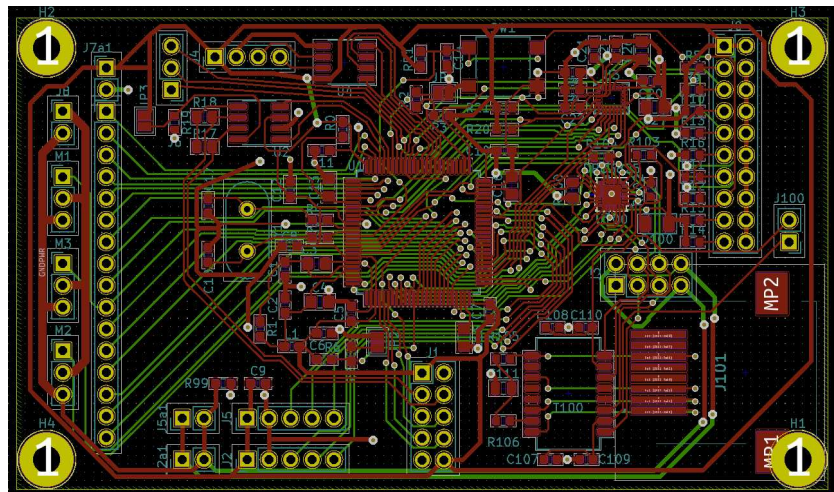


Figure 11. RobotFish Segment Board: a board designed to accommodate an STM32 F417 Microcontroller; it serves as a networked extension to communicate with the head board, and contains all of the necessary IOs for any servos or sensors, and contains an LSM9DS1 IMU.

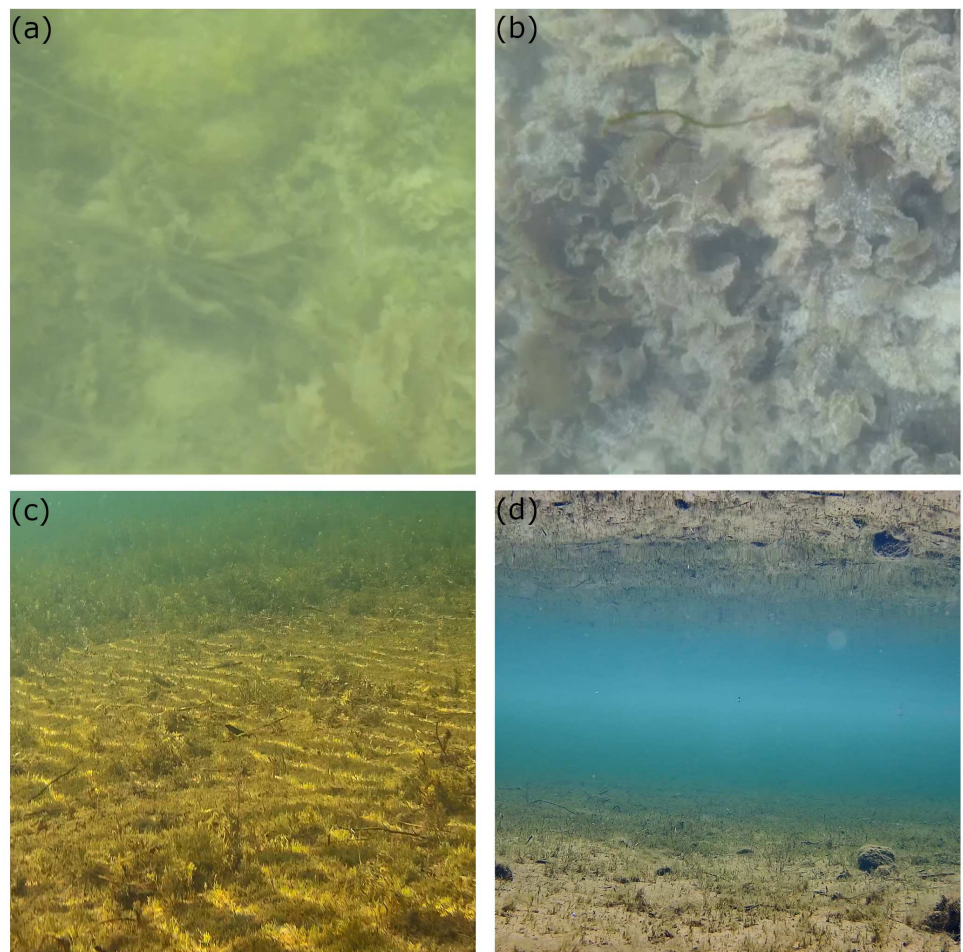


Figure 12. RobotFish Computer Vision Challenges: (a) Almost completely green image showing limited visibility, (b) floating particles in the foreground, (c) water caustics on a lake bed, created by the surface of the water, (d) total internal reflection underwater causing a mirror image of a lake bed in the water surface.

390 time applications. Many unique visual phenomena affect underwater images such as
 391 wavelength-dependent attenuation, floating particles and bubbles, underwater caustics
 392 in shallow water, varying lights and shadows, moving flora and fauna and refractions
 393 through thick glass housing needed for waterproofing camera systems [34] [35], some
 394 examples of which are shown in Figure 12.

395
 396 In the RoboFish project, the research aimed to test current state-of-the-art SLAM
 397 algorithms on underwater visual datasets and to quantify performance and suitability of
 398 those algorithms for use with low-cost Raspberry Pi cameras. To achieve this a graphical
 399 user interface (GUI) was developed in Python and OpenCV [37] to enable the real-time
 400 modification of popular feature matching algorithm parameters whilst providing visual
 401 feedback on performance and an estimation of the camera's 3D trajectory using visual
 402 odometry (VO). The most suitable parameters and image processing algorithms were
 403 then determined and implemented in a modified version of ORB SLAM 2 [31].

404
 405 The GUI was built in Python using the Matplotlib library. It was decided that only
 406 ORB [38] and BRISK [39] feature matching algorithms would be tested, however the
 407 design enables the addition of SIFT [40] and SURF [41] feature detectors with only minor
 408 modifications. Figure 13 shows the GUI. It enables the adjustment of either ORB or
 409 BRISK parameters in real-time via sliders and buttons, with the effects of these changes
 410 visible both qualitatively in the overlaid video feeds and quantitatively in the graphs.
 411 Parameters can also be set prior to a test and it enables a previous tests' data to be
 412 displayed simultaneously on the graphs allowing comparisons of performance for each
 413 test. The camera's position is estimated using VO, the implementation of which was
 414 based closely on PySLAM [42].

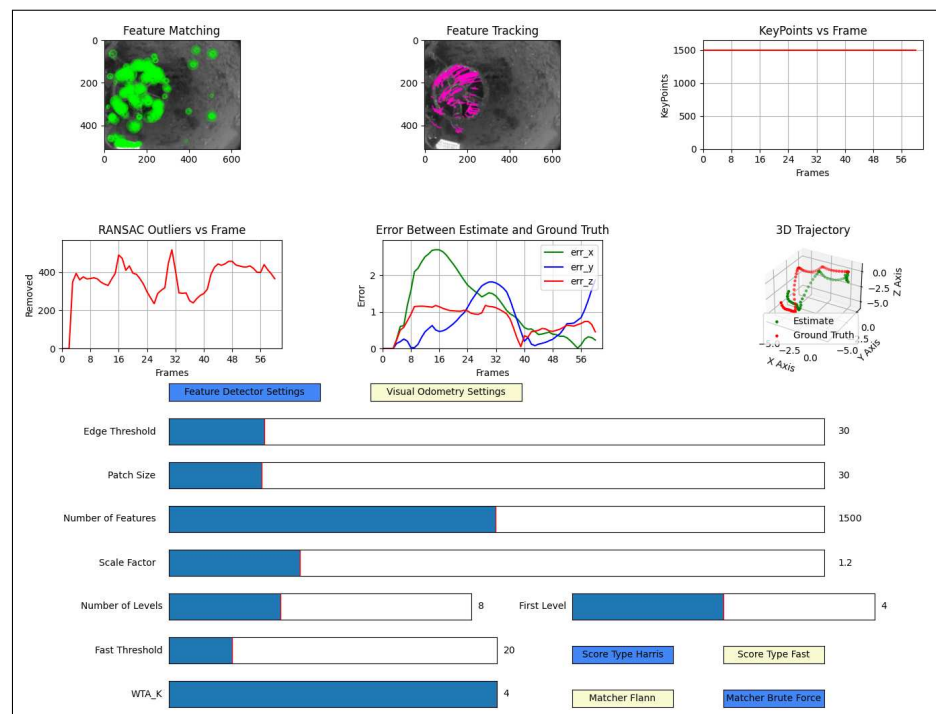


Figure 13. Python Matplotlib GUI showing the statistics of ORB features on the AQUALOC harbor-sequence-02 dataset [36] and including the video feed overlaid with ORB features: "3D Camera Trajectory" on the bottom right showing the structure-from-motion "ground truth" for comparison; "Sliders and Buttons" on the bottom enabling adjustment of ORB and VO settings in real-time.

415 5. Acoustic Communication

416 The RoboFish-specific powerful Xilinx Zynq SoC acts as a minicomputer on board
417 processing a number of operations, one of which is communication. A half-duplex 64bps
418 acoustic modem, called Water Linked M64 Acoustic Modem [43], is used to provide
419 low-rate communications at medium range (i.e. 200 meter) for remote control, telemetry,
420 and inter-vehicle coordination. This self-contained modem supports omnidirectional
421 operation, which keeps the data link stable even when the RoboFish is in motion. It
422 is programmed with a packet-based protocol with extensive use of error detection to
423 enable a highly robust transmission at very low power consumption. It communicates
424 via a serial 115200 baud UART 3.3V interface with the SoC board. Its small size enables
425 easy integration in the RoboFish head. The Xilinx Zynq SoC includes an FPGA which
426 will be used for acceleration of inter-vehicle communication architectures, protocols, and
427 applications for efficient RoboFish swarm communication networks in the future.

428
429 An interactive Python GUI, shown in Figure 14, was developed to run the RoboFish
430 manually from a distance using the acoustic modem. The modem has a configurable
431 data link and is interfaced using a lightweight API, on which the GUI design is based.
432 The default serial protocol is documented in Reference [44]. This document describes
433 the modem's Data Link Layer protocol. With this protocol, packets are sent to and
434 received from the modem with serial communication commands taking this format
435 115200 8-N-1 (payload size is 8 bytes). A Python script was put together to enable
436 sending and receiving these commands to the modems through the serial port. The
437 commands can be sent as a string represented by descriptive variable names or the GUY.
438 By configuring the modem that is installed in RoboFish as a receiver and the topside
439 modem as a transmitter, an operator can send these predefined commands to control
440 RoboFish manually over the acoustic channel if required. Through this GUI, the operator

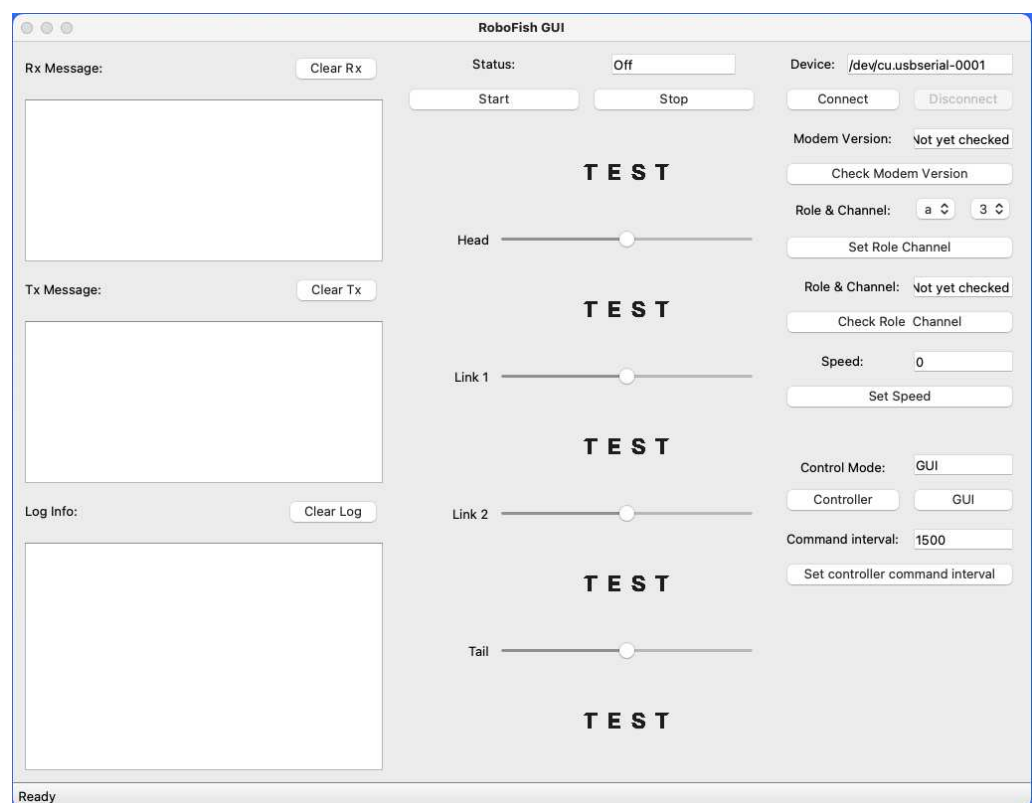


Figure 14. Python GUI for RobotFish Enabling Easier Interact with the RoboFish Acoustic Modem based on its API: works as a messaging application to remotely change parameters and control RoboFish over an acoustic channel.

441 can primarily control the degree of freedom for each joint by sending over acoustically
442 the required angle from the topside computer to RoboFish. Besides, the GUI enables
443 remote ON/OFF control, steering, selection of communication channel and displays
444 notifications received from RoboFish in humanly readable format for the operator.

445
446 In addition the acoustic modem, RoboFish uses Ping SONAR Altimeter and Echo-
447 sounder [45] that is a single-beam echo-sounder with a maximum range of 30m, a beam
448 width of 30deg and a maximum depth rating of 300m. It is connected to the RoboFish's
449 SoC through a serial connection using one of its Serial/UART ports. Distances read by
450 this Rangefinder can be read from a user interface running on the operator's computer.

451 6. Locomotion Control

452 Biological fish in nature repeat the same locomotion pattern for swimming to move
453 forward straight over a given period, it is possible to construct a precise mathematical
454 model through analytical approaches because its locomotion involves hydrodynamics
455 and kinematics [46]. However, for real-time control with microcontroller hardware, a
456 simpler parametric control method is sought. Using hydrodynamic analysis, control pa-
457 rameters that produce stable locomotion are produced for two approaches to locomotion
458 that are currently being tested, as follows.

459 6.1. Conventional Control

460 The first step of most conventional control design procedures is to establish the
461 mathematical model of the dynamic system, which is a set of ordinary differential equa-
462 tions [47]. The RoboFish has multiple joints and strong influences from the operational
463 environment. The control problem for stabilising the attitude and maximising the for-
464 ward velocity using the causal fin is high dimensional and underactuated. Designing a
465 controller taking into account the full nonlinear dynamics is challenging. The second step
466 is obtaining an approximate model for each operation scenario, i.e., the forward swim-
467 ming or the turning manoeuvre. This step is frequently performed using the feedback
468 linearization procedures [48]. Recently, reinforcement learning provides a promising
469 performance to deal with nonlinearity directly with less conservative design problems
470 [49]. The third step is to design a controller for the linearized system using linear control
471 design procedures, e.g., LQR (Linear Quadratic Regulator), PID (Proportional Integral
472 Derivative) [50]. There are several attempts to combine reinforcement learning with
473 conventional control [51] [52]. The combined methods would provide the capabilities
474 to exploit the nonlinearity in the nonlinear region and provide stability assurance in
475 the linear domain. Internal uncertainties and external disturbances would deteriorate
476 the stability and the performance. An external disturbance observer is combined in the
477 last step of the control design [53], and finally, the robustness analysis is performed [54].
478 In summary, the first control method implemented on RoboFish will be a conventional
479 controller combining linearization with reinforcement learning.

480 6.2. CPG-Control

481 Traditional model based control via numerical techniques, kinematic approaches
482 and geometric approaches is not always very well suited to dynamic and changing
483 conditions [55]. Biological systems produce rhythmic patterns using a functional unit
484 called a central pattern generator. A CPG can be considered as a dedicated neural
485 mechanism involving a group of neurons that coordinately generate rhythmic signals
486 without sensory feedback [56]. While sensory feedback is needed to shape the CPG
487 signals, the CPG can run independently without input. This method is widely used for
488 the locomotion of robots such as crawling, flying, swimming, hopping, walking and
489 running. The general design of CPG-based control has been focused on three aspects:
490 CPG modelling and analysis, CPG modulation (parameter tuning and gait transition), as
491 well as CPG implementation [57].

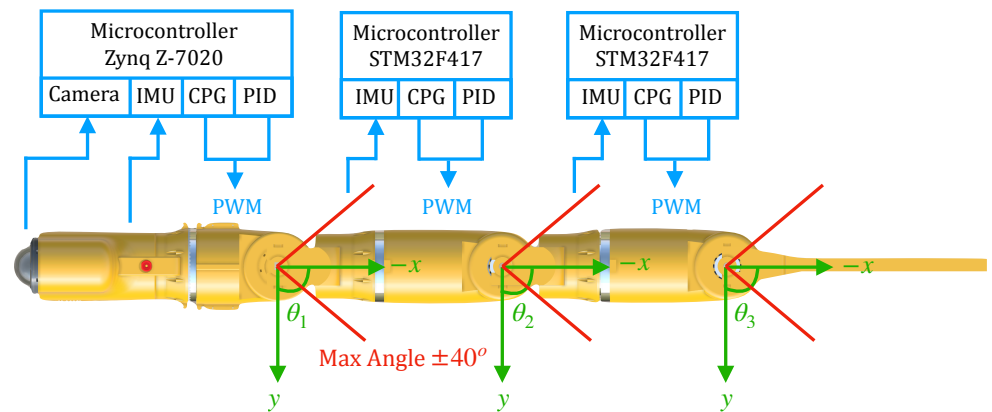


Figure 15. Locomotion Control Architecture: an example of RobotFish with three joints where θ_1 , θ_2 and θ_3 are the main parameters for locomotion control; the maximum angle of each parameter is ± 40 degree.

492 6.3. RobotFish Locomotion Control Architecture

493 In Figure 15, the RoboFish prototype is shown with its main control components. A
 494 monocular camera in the head is used for visual odometry and for detecting and tracking
 495 obstacles in the environment, with image processing running on the Zynq Z-7020 SoC in
 496 the head module. The inertial measurement units in each module of the body provide
 497 dynamic feedback from the body position. These are the main sources of sensory input
 498 for the locomotion control system. Currently, in the absence of sensory data (for example,
 499 if no visual odometry information is available), the system runs in open-loop mode, and
 500 control parameters for forward velocity and angular velocity are read directly from the
 501 desired movement commands. The output of the CPG based controller is transmitted
 502 to the servo motors in each joint via PWM signalling. The feature parameters of CPG
 503 will change the speed of the robotic fish while swimming. The power consumption of
 504 the servo motors will be recorded to compare the energy consumption corresponding to
 505 specific sets of CPG feature parameters. The modulation of the CPG will be restricted by
 506 each module's battery life. A comparison of swimming performance resulting from the
 507 conventional control methods cited, and the CPG design will be done after both control
 508 methods are implemented on RoboFish.

509 7. Initial Testing and Lessons Learned

510 The work described in this paper led to the initial testing of the first RoboFish
 511 prototype shown in Figure 16. This prototype is mechanically quite mature and had a
 512 minimum number of completed modules in the initial testing to test water-tightness
 513 in the first place. Although full autonomy has yet to be integrated into this prototype,
 514 adequate electronic parts and processing capabilities were included in the initial testing
 515 to fully program the vehicle with a basic operating system to primarily test propulsion.
 516 The computer vision system and acoustic communication system have been completed,

Table 2: List of the 3D Printer Parameters

Parameter	Value	Comment
Layer height	0.254 mm	Standard
extrusion width	0.5mm	Standard
Wall thickness	2.032 mm	To print more perimeters per layer
Solid infill	Enabled	To help preventing water ingress
Variable width fill	Enabled	To fill any small gaps
Room temperature	25 ^o	Enclosure



Figure 16. RoboFish prototype with a Head, one Segment and Tail: 3D printed in ASA and using FDM.

517 and next trials will be fully integrated into the prototype. As a proof of concept, both
518 systems were tested separately in the initial testing and they were fully operational.

519

520 *7.1. Testing Propulsion*

521 This prototype is printed in ASA, with print parameters listed in Table 2 and KPAs
522 listed in Table 1. The prototype underwent its first test outdoors in December 2020.
523 The test went well and answered a number of questions. In this test, the prototype
524 undertook some important tasks, but the test was not a very long test that examines all
525 the RoboFish features. This test was the foundation of more task-oriented trials to come.
526 The objectives of the test can be summarised as following:

- 527 • Testing water-tightness
- 528 • Testing the functionality of magnetic-coupling joints
- 529 • Testing propulsion



Figure 17. RoboFish prototype Swimming on the Surface of a Lake: two side plastic buoys were included to maintain positive buoyancy; a rope is attached to it to be dragged to the home point in the case of failure or battery recharge.

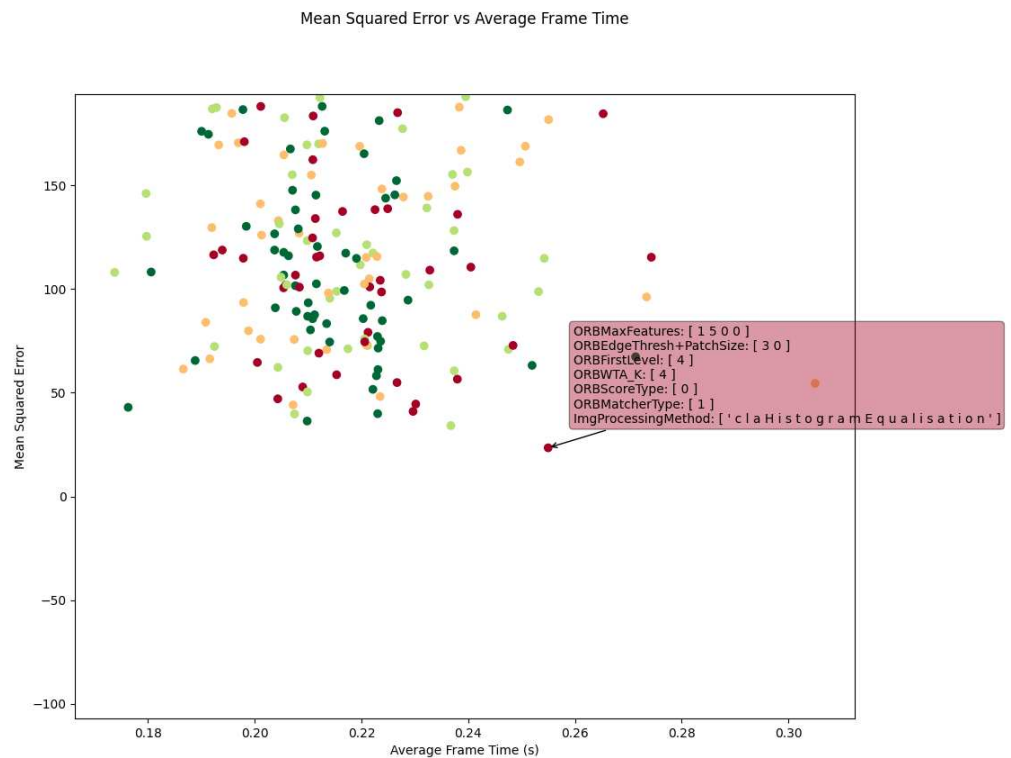


Figure 18. Results of Different Image Processing Techniques and Feature Matching Parameters on the Accuracy of VO Relative to the Structure-from-motion “ground truth”: the test with the smallest error is highlighted and the settings for that test displayed.

530 These initial trials were conducted in the University of York Campus West lake. The
 531 depths were around 1-2 m, with temperature of around 8°C, 10 mph wind speed, and
 532 poor water visibility. The prototype was put together and tested shortly on the shoreline
 533 (the lake’s edge platform) just before it was let go into water as shown in Figure 17. In
 534 one testing scenario, RoboFish was dropped slowly into the water from the platform
 535 using two ropes. To test swimming on the surface, two side plastic buoys were included
 536 to maintain positive buoyancy and good balance with the right position by preventing
 537 RoboFish from going below surface or turning upside down. With it being directed
 538 toward the centre of the lake, the Go button was pressed and RoboFish swam as expected.
 539 It was tethered to be brought back to the home point in the case of failure or untimely
 540 need for battery recharge. In another testing scenario, RoboFish was released to operate
 541 underwater. This was the first outdoor trial for RoboFish. The shallow lake seems to be
 542 an ideal place to carry out more tests to examine the functionality of control, electronic
 543 and communication. As for computer vision, the location needs to be investigated
 544 further.

545 Given that it is the first real outdoor trial, the performance of RoboFish was as good
 546 as it was predicted. Initial testing of the propulsion mechanism revealed problems with
 547 electrical connections and power cable wiring associated with batteries. To overcome this,
 548 a new battery mounting plate was designed and is currently being 3D printed to enclose
 549 all of the power network connections. The prototype is fitted out with cable penetrators,
 550 ensuring watertight connections for the discrete cable that is used for both power
 551 distribution and control signal communications between modules. In future design,
 552 plug and bulkhead socket connectors would be a better option. Also, if the modules are
 553 equipped with wireless chargers as an option it will save time, especially during testing.
 554 Improvements on its buoyancy, thrust and swimming gait can be achieved via further
 555 hydrodynamic analysis. This could involve making the head undulate less and the tail
 556 oscillate more. Adding more segments will also improve the swimming gait.

557 7.2. Testing Computer Vision

558 In order to quantify the performance of the computer vision system, a dataset with
559 ground truth was required. To the best of our knowledge, one of the only underwater
560 datasets to provide a trajectory estimate is the AQUALOC dataset. This dataset provides
561 an offline calculated structure-from-motion trajectory [36]. The assumption was then
562 made that improvements in the accuracy of the PySLAM based VO calculated using
563 ORB features would result in improvements to ORB SLAM 2. A Python script was
564 written to cycle through various OpenCV image processing techniques (e.g histogram
565 equalisation and image filtering) and multiple ORB and BRISK parameters to deter-
566 mine which combination produced the most accurate estimate of the camera's trajectory.
567 This was determined using the mean squared error between the VO estimate and the
568 structure-from-motion ground truth trajectory obtained from the AQUALOC dataset. A
569 graph of the result of these tests with the most accurate configuration selected is shown
570 in Figure 18.

571

572 It was determined that the highest accuracy was achieved when using Contrast Lim-
573 ited Adaptive Histogram Equalization (CLAHE) and an ORB feature matcher with the
574 following parameters: Edge Threshold and Patch Size of 30; Minimum FAST Threshold
575 of 30; First Level of 4; Maximum ORB Features of 1500 and all others at default OpenCV
576 values. The ORB SLAM 2 code was then modified to include CLAHE image processing
577 and the calculated ORB feature matching parameters. This was then compared against a
578 version of ORB SLAM 2 without CLAHE image processing and using ORB-SLAM 2's
579 default ORB feature matching parameters. Tests were conducted on both the AQUALOC
580 and Marine Autonomous Robotics for InterventionS MARIS [58] underwater datasets.
581 The modified ORB SLAM 2 appeared to yield improved SLAM accuracy, losing tracking
582 a reduced number of times on each dataset. ORB SLAM 2 ran at usable framerates on a
583 Raspberry Pi 4 of around 15 - 20 fps, suitable for slow moving AUVs. It is recommended
584 that ORB SLAM 2 with the provided settings be used as an initial platform on which to
585 develop further underwater visual SLAM robotic applications.

586 7.3. Testing Acoustic Communication and Ranging

587 The RoboFish prototype uses an M64 Acoustic Modem [43]. Because this modem is
588 still a Beta version during the initial testing, a number of in-water trials were conducted
589 to establish whether the two pairs RoboFish uses are working. Both modems were
590 functional and a point-to-point acoustic link was established and packets transmitted
591 over it successfully. Apart from minor issues in the beginning, mainly with wiring
592 and serial port configurations, the modem's Channel 3, which is between 93.75khz and
593 125.00khz, offered a very reliable acoustic link over 50-80m range in open water, as well
594 as inside a compact water tank of 302 litres. Channel 1 had a lower signal strength
595 causing a shorter range. Channel 4 was more unpredictable, as it worked but with a
596 shorter range and was slightly unstable. Channel 6-7 were not tested as they would give
597 a shorter range and not required at this stage. These parallel channels can be used by
598 RoboFish for networking in the future, as it is possible to switch between channels to
599 enable communication between more than two modems without packet collisions (but
600 not at the same time).

601

602 The minor wiring and interface issues were related to the 3.3V UART to USB serial
603 converter. A pair of Blue Robotics' BLUART USB to serial converters [59] were used. To
604 avoid such issues, the converter and the modem need to be common-grounded. The
605 UART TX from the modem needs to be connected to the UART RX on the converter
606 board and similarly for the RX pins. The modems need to work in water to avoid
607 unwanted overheat. A blinking light about every 2 seconds on the modem will indicate
608 it is powered, but no link is established. The head of the RoboFish is designed so that it

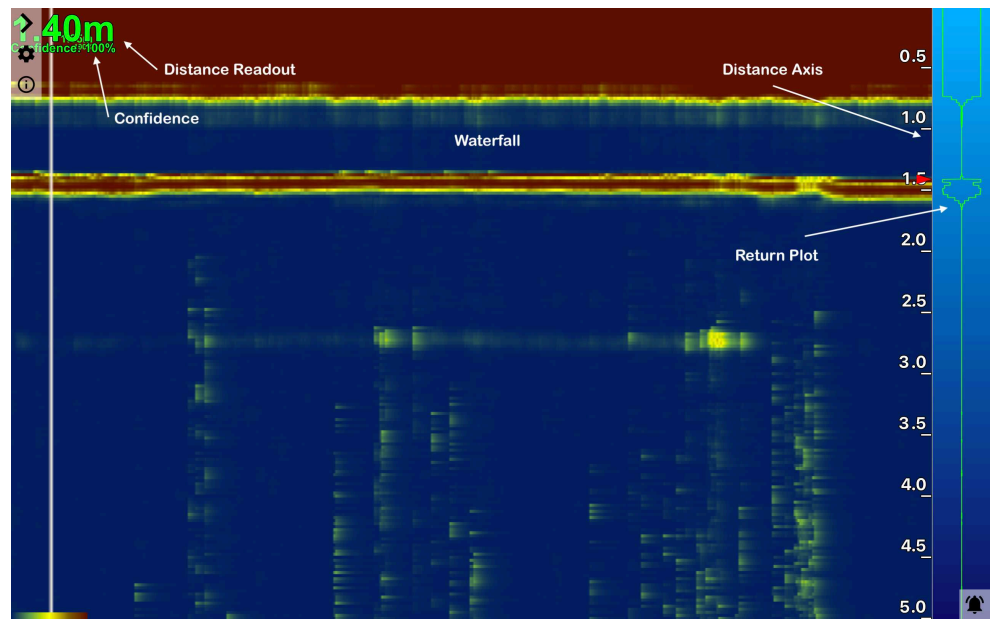


Figure 19. Ping-Viewer Interface to View and Record Ping Data showing Water Depth: consists of four important components (Distance Readout, Distance Axis; echo strength, and 3D trace presenting consecutive profile samples).

609 has the modem fitted outside.

610

611 The range finder was also tested and is currently fully operational in RoboFish.
 612 Its readings will be integrated in the final mission oriented control system. Distances
 613 read by this Rangefinder can be read from a displaying interface running on the topside
 614 computer. This window consists of four important components as shown in Figure 19:

615

- 616 • *Distance Readout:* The Distance Readout presents the distance to the target in the
 617 latest measurement. The reading that is shown in Figure 19 was the distance to the
 618 floor in a testing tank during RoboFish's initial trials. The confidence measurement
 619 for the newest range reading is presented below the distance reading and is colour-
 620 coded based on strength as follows: green = 100%, yellow = 50% and red = 0%.
- 621 • *Distance Axis:* This vertical axis represents the distance from the transducer built
 622 in the Echo-sounder. It starts from the top of the window which represents zero
 623 distance from the face of the transducer and runs down vertically with the distance
 624 to the farthest object being at the bottom. Its scale automatically adjusts to indicate
 625 a live scanning range of the rangefinder.
- 626 • *Return Plot:* The Return Plot presents the echo strength against the distance of the
 627 newest profile sample. The stronger an echo is the wider its trace appears.
- 628 • *Waterfall:* The Waterfall is a 3D trace presenting consecutive profile samples. The X
 629 axis is time; and Y axis is new distance reading shifting from right to left as a new
 630 echo arrives.

631 8. Future work

632 The RoboFish prototype is under continuing development. Future versions of a
 633 smaller size RoboFish, with particular focus on the modularity of the body design and
 634 easy connect/disconnect magnetic joints, will provide a flexible and dynamic platform
 635 for numerical data validation and experimental investigation in hydrodynamic labo-
 636 ratory testing. This will be highlighted in future projects as this work could not be
 637 done under the pandemic restrictions. Anticipated investigations include the analysis
 638 of the flow field influenced by different fin and body geometries and kinematic loco-

639 motion parameters, smart soft materials for passively deformed body parts as well as
640 analysis of different actively controlled body kinematics using linear, nonlinear and
641 CPG-based control. This will provide further insight to disseminate the hydrodynamic
642 performance under different flow conditions to prepare for application within complex
643 chaotic and harsh ocean environments. In practical sense, this will especially support
644 the targeted underwater docking, which requires accuracy and reliability of the swim-
645 ming motion. Another direction of future work is to investigate the use of networks or
646 *swarms* of RoboFish carrying out large-scale subsea monitoring or exploration missions,
647 e.g. seafloor mapping, marine archaeology. This will involve a significant challenge in
648 implementing underwater network protocols for cooperative acoustic localisation and
649 navigation, real-time remote control and data gathering from multiple RoboFish.

650 9. Conclusion

651 The work described in this paper led to the development of a fish-like AUV, namely
652 RoboFish, with a bending body that works as a spinal column and able to mimic
653 propulsion techniques of living fish. The first RoboFish prototype was built successfully
654 and was able to complete minimum lake trials. A substantial amount of knowledge
655 was gained from the construction of RoboFish about the technologies that a robotic fish
656 requires to be able to loiter with a camera around complex structures autonomously or
657 remotely controlled over an acoustic link. The use of modular electronics and actuator
658 control algorithms, the networking architecture, the 3D printing approach, and the
659 magnetic joint design are novel contributions to the state of the art that will enable new
660 opportunities. This represents opportunities for additional research arising from further
661 field tests of RoboFish and increases the likelihood of more advanced RoboFish versions.

662 **Author Contributions:** Conceptualisation, (M.P.) Mark Post and (W.G.) Wael Gorma; methodology,
663 W.G. and M.P.; software, W.G., M.P., (J.W.) James White and (J.G.) James Gardner; validation, W.G.,
664 M.P., J.W. and J.G.; formal analysis, W.G., M.P., J.W. and J.G.; investigation, W.G., M.P., J.W., (M. W.)
665 Marvin Wright, (Y.L.) Yang Luo and (J.K.) Jongrae Kim; resources, M.P., (Q.X.) Qing Xiao and (P.M.)
666 Paul Mitchell; data curation, W.G., M.P., J.W. and J.G.; writing—original draft preparation, W.G.,
667 M.P., J.W., J.G., Y.L., J.K. and (N.M.) Nils Morozs; writing—review and editing, M.P., P.M. and
668 Q.X.; visualisation, M.P.; supervision, M.P.; project administration, M.P., Q.X. and W.G; funding
669 acquisition, M.P., Q.X. and P.M.

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686 Abbreviations

687 The following abbreviations are used in this manuscript:

688

AMBA	Advanced Microcontroller Bus Architecture
AUV	Autonomous Underwater Vehicles
ASA	Acrylonitrile Styrene Acrylate
AXI	Advanced eXtensible Interface
CAN	Controller Area Network
CFD	Computational Fluid Dynamics
CSI	Camera Serial Interface
CPG	Central pattern generators
FDM	Fused Deposition Modelling
FSI	Fluid-structure interaction
FPGA	Field Programmable Gate Array
GPIO	General Purpose Input-Output
689 IC	Integrated Circuit
IMU	Inertial Measurement Unit
KPA	Key Performance Attributes
MIPI	Mobile Industry Processor Interface
ORE	Offshore renewable energy
PCB	Printed circuit board
PID	Proportional Integral Derivative
PWM	Pulse Width Modulation
ROV	Remotely Operated Vehicles
SoC	System-on-Chip
SoM	System-on-Module
SONAR	Sound Navigation and Ranging
SoC	System on a chip

References

- Darwish, A.S.; Al-Dabbagh, R. Wind energy state of the art: present and future technology advancements. *Renewable Energy and Environmental Sustainability* **2020**, *5*, 7.
- Liu, P.; Barlow, C.Y. Wind turbine blade waste in 2050. *Waste Management* **2017**, *62*, 229–240.
- Pliego Marugan, A.; Garcia Marquez, F.P.; Pinar Perez, J.M. Optimal maintenance management of offshore wind farms. *Energies* **2016**, *9*, 46.
- Shafiee, M.; Sørensen, J.D. Maintenance optimization and inspection planning of wind energy assets: Models, methods and strategies. *Reliability Engineering & System Safety* **2019**, *192*, 105993.
- Mitchell, D.; Zaki, O.; Blanche, J.; Roe, J.; Kong, L.; Harper, S.; Robu, V.; Lim, T.; Flynn, D. Symbiotic System of Systems Design for Safe and Resilient Autonomous Robotics in Offshore Wind Farms. *arXiv preprint arXiv:2101.09491* **2021**.
- Hegde, J.; Utne, I.B.; Schjøberg, I. Applicability of Current Remotely Operated Vehicle Standards and Guidelines to Autonomous Subsea IMR Operations. 2015, Vol. 7, *International Conference on Offshore Mechanics and Arctic Engineering*.
- Scaradozzi, D., e.a. "BCF swimming locomotion for autonomous underwater robots: a review and a novel solution to improve control and efficiency. *Ocean Engineering* **2017**, *130*, 437–453.
- Sfakiotakis, M., e.a. Review of fish swimming modes for aquatic locomotion. *IEEE Journal of oceanic engineering* **1999**, *24*, 237–252.
- Fish, F.E. Advantages of aquatic animals as models for bio-inspired drones over present AUV technology. *Bioinspiration & biomimetics* **2020**, *15*, 025001.
- Blake, R. Fish functional design and swimming performance. *Journal of fish biology* **2004**, *65*, 1193–1222.
- Triantafyllou, M.S.; Triantafyllou, G.S. An efficient swimming machine. *Scientific american* **1995**, *272*, 64–70.
- Tytell, E.D. The hydrodynamics of eel swimming II. Effect of swimming speed. *Journal of experimental biology* **2004**, *207*, 3265–3279.
- Weihls, D. Stability versus maneuverability in aquatic locomotion. *Integrative and Comparative Biology* **2002**, *42*, 127–134.
- Christ, R.D.; Wernli Sr, R.L. *The ROV manual: a user guide for observation class remotely operated vehicles*; Elsevier, 2011.
- Macreadie, P.I.; McLean, D.L.; Thomson, P.G.; Partridge, J.C.; Jones, D.O.; Gates, A.R.; Benfield, M.C.; Collin, S.P.; Booth, D.J.; Smith, L.L.; others. Eyes in the sea: unlocking the mysteries of the ocean using industrial, remotely operated vehicles (ROVs). *Science of the Total Environment* **2018**, *634*, 1077–1091.
- Owens, D. Rex 2: Design, Construction, and Operation of an Unmanned Underwater Vehicle. PhD thesis, Massachusetts Institute of Technology, 2009.
- Brege, E.D. Design and Construction of a Low Cost, Modular Autonomous Underwater Vehicle. PhD thesis, Massachusetts Institute of Technology, 2011.
- Furlong, M.E.; Paxton, D.; Stevenson, P.; Pebody, M.; McPhail, S.D.; Perrett, J. Autosub Long Range: A long range deep diving AUV for ocean monitoring. 2012 IEEE/OES Autonomous Underwater Vehicles (AUV), 2012, pp. 1–7.
- Marthiniussen, R.; Vestgard, K.; Klepaker, R.; Storkersen, N. HUGIN-AUV concept and operational experiences to date. Oceans '04 MTS/IEEE Techno-Ocean '04 (IEEE Cat. No.04CH37600), 2004, Vol. 2, pp. 846–850 Vol.2.

20. Liljebäck, P.; Mills, R. Eelume: A flexible and subsea resident IMR vehicle. *OCEANS 2017 - Aberdeen*, 2017, pp. 1–4.
21. Raj, A.; Thakur, A. Fish-inspired robots: design, sensing, actuation, and autonomy—a review of research. *Bioinspiration & Biomimetics* **2016**, *11*, 031001.
22. Kruusmaa, M.; Toming, G.; Salumäe, T.; Ježov, J.; Ernits, A. Swimming speed control and on-board flow sensing of an artificial trout. 2011 IEEE International Conference on Robotics and Automation. IEEE, 2011, pp. 1791–1796.
23. Kelasidi, E.; Liljebäck, P. and Pettersen, K.Y.; Gravidahl, J.T. Experimental investigation of efficient locomotion of underwater snake robots for lateral undulation and eel-like motion patterns. *Robotics and Biomimetics* **2015**, *2*.
24. Bayat, B.; Crespi, A.; Ijspeert, A. Envirobot: A bio-inspired environmental monitoring platform. 2016 IEEE/OES Autonomous Underwater Vehicles (AUV), 2016, pp. 381–386. doi:10.1109/AUV.2016.7778700.
25. Yamada, H.; Chigisaki, S.; Mori, M.; Takita, K.; Ogami, K.; Hirose, S. Development of Amphibious Snake-like Robot ACM-R5. International Federation of Robotics International symposium on robotics, 2005, p. 133.
26. Fierstine, H.L.; Walters, V. Studies in locomotion and anatomy of scombroid fishes. *Biological Sciences* **1968**, p. 4.
27. Luo, Y.; Xiao, Q.; Shi, G.; Pan, G.; Chen, D. The effect of variable stiffness of tuna-like fish body and fin on swimming performance. *Bioinspiration & Biomimetics* **2020**, *16*, 016003.
28. Luo, Y.; Xiao, Q.; Shi, G.; Wen, L.; Chen, D.; Pan, G. A fluid–structure interaction solver for the study on a passively deformed fish fin with non-uniformly distributed stiffness. *Journal of Fluids and Structures* **2020**, *92*, 102778.
29. Wright, M.; Luo, Y.; Xiao, Q.; Post, M.; Gorma, W.; Durrant, A.; Yue, H. CFD-FSI Analysis on Motion Control of Bio-Inspired Underwater AUV System Utilizing PID Control. 2020 IEEE/OES Autonomous Underwater Vehicles Symposium (AUV), 2020, pp. 1–6.
30. Wright, M.; Gorma, W.; Luo, Y.; Post, M.; Xiao, Q.; Durrant, A. Multi-actuated AUV Body for Windfarm Inspection: Lessons from the Bio-inspired RoboFish Field Trials. 2020 IEEE/OES Autonomous Underwater Vehicles Symposium (AUV), 2020, pp. 1–6.
31. Mur-Artal, R.; Tardos, J.D. ORB-SLAM2: an Open-Source SLAM System for Monocular, Stereo and RGB-D Cameras **2016**. [arXiv:cs.RO/1610.06475].
32. Shang, Z.; Shen, Z. Real-time 3D Reconstruction on Construction Site using Visual SLAM and UAV **2017**. [arXiv:cs.RO/1712.07122].
33. Ferreira, F.; Veruggio, G.; Caccia, M.; Bruzzone, G. Real time optical SLAM based mosaicking for unmanned underwater vehicles. *Intelligent Service Robotics* **2012**, *5*, 55–71.
34. Akkaynak, D.; Treibitz, T. Sea-thru: a method for removing water from underwater images. Proceedings of the IEEE/CVF Conference on Computer Vision and Pattern Recognition, 2019, pp. 1682–1691.
35. Köser, K.; Frese, U. Challenges in Underwater Visual Navigation and SLAM. In *AI Technology for Underwater Robots; Intelligent Systems, Control and Automation: Science and Engineering*, Springer International Publishing: Cham, 2019; pp. 125–135.
36. Ferrera, M.; Creuze, V.; Moras, J.; Trouvé-Peloux, P. AQUALOC: An Underwater Dataset for Visual-Inertial-Pressure Localization **2019**. [arXiv:cs.CV/1910.14532].
37. Culjak, I.; Abram, D.; Pribanic, T.; Dzapo, H.; Cifrek, M. A brief introduction to OpenCV. 2012 Proceedings of the 35th International Convention MIPRO, 2012, pp. 1725–1730.
38. Rublee, E.; Rabaud, V.; Konolige, K.; Bradski, G. ORB: An Efficient Alternative to SIFT or SURF. 2011 International Conference on Computer Vision, 2011, pp. 2564–2571.
39. Leutenegger, S.; Chli, M.; Siegwart, R.Y. BRISK: Binary Robust Invariant Scalable Keypoints. 2011 International Conference on Computer Vision, 2011, pp. 2548–2555.
40. Lowe, D.G. Distinctive image features from scale-invariant keypoints. *Int. J. Comput. Vis.* **2004**, *60*, 91–110.
41. Bay, H.; Tuytelaars, T.; Van Gool, L. SURF: Speeded Up Robust Features. *Computer Vision – ECCV 2006*. Springer Berlin Heidelberg, 2006, pp. 404–417.
42. Luigi Freda. PySLAM, 2020.
43. BlueRobotics Water Linked M64 Acoustic Modem. Available online: <https://bluerobotics.com/store/comm-control-power/acoustic-modems/wl-11003-1/>. Accessed on 25 04 2021.
44. Water Linked, Modem-M64 Serial Protocol. Available online: <https://waterlinked.github.io/modems/modem-m64-protocol/>. Accessed on 25 04 2021.
45. BlueRobotics Ping Sonar Altimeter and Echosounder. Available online: <https://bluerobotics.com/store/sensors-sonars-cameras/sonar/ping-sonar-r2-rp/>. Accessed on 25 04 2021.
46. Mathieu Porez, F.B.; Ijspeert, A.J. Improved Lighthill fish swimming model for bio-inspired robots: Modeling, computational aspects and experimental comparisons. *The International Journal of Robotics Research* **2014**, *33*, 1322–1341.
47. Graver, J.G.; Leonard, N.E. Underwater Glider Dynamics and Control. 12th international symposium on unmanned untethered submersible technology. Citeseer, 2001, pp. 1742–1710.
48. Slotine, J.J.E.; Karl Herdick, J. Robust input-output feedback linearization. *International Journal of control* **1993**, *57*, 1133–1139.
49. Lillicrap, T.P.; Hunt, J.J.; Pritzel, A.; Heess, N.; Erez, T.; Tassa, Y.; Silver, D.; Wierstra, D. Continuous Control with Deep Reinforcement Learning. *arXiv preprint arXiv:1509.02971* **2015**.
50. Argentim, L.M.; Rezende, W.C.; Santos, P.E.; Aguiar, R.A. PID, LQR and LQR-PID on a Quadcopter Platform. 2013 International Conference on Informatics, Electronics and Vision (ICIEV). IEEE, 2013, pp. 1–6.
51. Yoo, J.; Jang, D.; Kim, H.J.; Johansson, K.H. Hybrid reinforcement learning control for a micro quadrotor flight. *IEEE Control Systems Letters* **2020**, *5*, 505–510.

52. Fernandez, G.I.; Togashi, C.; Hong, D.; Yang, L. Deep Reinforcement Learning with Linear Quadratic Regulator Regions. *arXiv preprint arXiv:2002.09820* **2020**.
53. Jo, N.H.; Shim, H.; Son, Y.I. Disturbance observer for non-minimum phase linear systems. *International Journal of Control, Automation and Systems* **2010**, *8*, 994–1002.
54. Kim, J.; Bates, D.G.; Postlethwaite, I. Robustness analysis of linear periodic time-varying systems subject to structured uncertainty. *Systems & control letters* **2006**, *55*, 719–725.
55. Melsaac, K.; Ostrowski, J. A Geometric Approach to Anguilliform Locomotion: Modelling of an Underwater Eel Robot. Proceedings 1999 IEEE International Conference on Robotics and Automation, 1999, Vol. 4, pp. 2843–2848.
56. Junzhi Yu, Min Tan, J.C.; Zhang, J. A survey on CPG-inspired control models and system implementation. *IEEE Transactions on Neural Networks and Learning Systems* **2014**, *25*, 441–455.
57. Crespi, A.; Lachat, D.; Pasquier, A.; Ijspeert, A. Controlling swimming and crawling in a fish robot using a central pattern generator. *Autonomous Robots* **2008**, *25*.
58. Oleari, F.; Kallasi, F.; Rizzini, D.L.; Aleotti, J.; Caselli, S. An Underwater Stereo Vision System: From Design to Deployment and Dataset Acquisition. OCEANS 2015 - Genova. IEEE, 2015, pp. 1–6.
59. BlueRobotics BLUART USB to TTL Serial and RS485 Adapter. Available online: <https://bluerobotics.com/store/comm-control-power/tether-interface/bluart-r1-rp/>. Accessed on 25 04 2021.