



### **UNIVERSITI PUTRA MALAYSIA**

# HIGH-VOLTAGE IGNITION CIRCUIT FOR COMPRESSED NATURAL GAS DIRECT INJECTION ENGINE

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# HIGH-VOLTAGE IGNITION CIRCUIT FOR COMPRESSED NATURAL GAS DIRECT INJECTION ENGINE

#### **AZIMAH BINTI OMAR**

MASTER OF SCIENCE UNIVERSITI PUTRA MALAYSIA

2007



#### Dedicated to,

My beloved Mother Zaibah Endut, My loving Father Omar Ismail, My faithful sister, brothers, relatives & friends

Abstract of thesis presented to the Senate of Universiti Putra Malaysia in fulfilment of the requirement for the degree of Master of Science

HIGH-VOLTAGE IGNITION CIRCUIT FOR COMPRESSED NATURAL GAS DIRECT INJECTION ENGINE

By

AZIMAH BINTI OMAR

March 2007

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**Faculty: Engineering** 

Ignition system of an internal combustion engine is an important part of the overall

engine management system. It is a means to provide enough high-voltage, minimum

around 20 kV to form an arc across the gap of a spark plug and to control the ignition

timing. Thus, it can provide a right time to burn the air-fuel mixture inside the

engine.

With advances in technology, the ignition system has progressed from a contact point

ignition system to an electronic ignition system and then to a digital distributorless

ignition system. The increased growth of the ignition system design in both size and

complexity has brought about the need for a simple and reliable ignition system to

provide high-voltage output to be delivered to the spark plug and at the same time to

adapt with the natural gas engine environment. Therefore, with the development of

an economical and reliable ignition system, there is a growing interest in developing

digital distributorless ignition system, which is programmable making it more

flexible and superior to other conventional system.

This thesis presents the development of an ignition circuit for a coil-on plug ignition

system of a natural gas engine. The main specification of the circuit is the

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implementation of the ignition power-switching device at the primary side of the circuit to provide high switching speed to turn on and off the device. The chosen power-switching device was Insulated Gate Bipolar Transistor or IGBT, which is more suitable to be implemented inside the circuit design compared to other powerswitching devices. The selected IGBT, IRGB14C40L are specifically design for a ignition applications and small engine ignition circuit. It has low saturation voltage and high self-clamped inductive switching energy. The modelling and optimization of the ignition IGBT parameters is done in the PSPICE software to fulfill the real ignition power-switching device requirements. The other specification of the circuit design is the implementation of the snubber circuit, which can provide over-voltage protection at the primary side of the power-switching device. Finally, the testing of the circuit is done by applying a control signal at the input source terminal or at the gate terminal of the ignition IGBT. The complete circuit design is integrated with the high-voltage ignition coil and a special designed long neck spark plug for the natural gas engine purpose. The circuit has been tested to make sure it can provide the desired voltage so it can ignite the mixture of the air and compressed natural gas in the right cylinder and at the right time.

From the test results of the ignition circuit, it demonstrates that the performances of the ignition parameters such as the primary current and secondary voltage are highly affected by the device parameters like the ignition IGBT parameters, specifications of the high-voltage ignition coil as well as the control strategy of the switching-time to ignite the spark plug.

Abstrak tesis yang dikemukakan Senat Universiti Putra Malaysia sebagai memenuhi keperluan untuk Ijazah Master Sains

LITAR PENYALAAN BERVOLTAN-TINGGI UNTUK ENJIN GAS ASLI TERMAMPAT SUNTIKAN TERUS

Oleh

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Sistem penyalaan bagi enjin pembakaran dalam adalah satu bahagian penting bagi

keseluruhan sistem pengurusan enjin. Ia adalah sumber yang boleh menghasilkan

voltan cukup tinggi minimum sekitar 20 kV untuk menghasilkan arka merentasi

ruang di antara palam pencucuh serta untuk mengawal masa pembakaran. Oleh itu, ia

boleh menghasilkan masa yang sesuai untuk membakar campuran udara-bahan bakar

di dalam enjin.

Dengan kemajuan teknologi, sistem penyalaan telah berkembang dari sistem

penyalaan titik sentuh kepada sistem penyalaan elektronik kemudian kepada sistem

penyalaan digital tanpa pengagih. Perkembangan rekabentuk sistem penyalaan dari

segi saiz dan kerumitannya telah membawa kepada perlunya sistem penyalaan yang

ringkas dan mampu menghasilkan keluaran voltan-tinggi untuk dialirkan kepada

palam pencucuh dan pada masa yang sama untuk disesuaikan dengan persekitaran

enjin gas asli. Oleh itu, dengan pembangunan sistem penyalaan yang ekonomik, dan

berkemampuan, terdapat peningkatan minat dalam pembinaan sistem penyalaan

digital tanpa pengagih yang lebih fleksibel kerana diprogramkan dan lebih hebat dari

titik sentuh konvensional yang lain.

Tesis ini mempersembahkan pembinaan litar penyalaan bagi sistem penyalaan gelung di atas palam untuk enjin gas asli. Spesifikasi utama bagi litar ini adalah pelaksanaan peranti suis-kuasa penyalaan pada bahagian utama litar untuk menghasilkan laju pensuisan yang tinggi bagi menghidupkan dan mematikan peranti tersebut. Peranti suis-kuasa yang dipilih adalah 'Insulated Gate Bipolar Transistor' atau IGBT, yang lebih sesuai untuk dilaksanakan pada rekabentuk litar berbanding dengan peranti-peranti suis-kuasa yang lain. IGBT yang dipilih iaitu IRGB14C40L, adalah direka khas bagi aplikasi pencucuhan dan litar pencucuh enjin sederhana. Ia mempunyai voltan tepu yang rendah dan kebolehan mengapit yang tinggi bagi tenaga pensuisan aruhan. Pemodelan dan pengoptimuman bagi parameter-parameter IGBT penyalaan ini dilakukan di dalam perisian PSPICE untuk memenuhi keperluan sebenar peranti suis-kuasa penyalaan. Spesifikasi lain bagi rekabentuk litar adalah pelaksanaan litar 'snubber' yang boleh memberi perlindungan daripada lebihanvoltan di bahagian utama peranti suis-kuasa. Akhirnya, pengujian ke atas litar dilakukan dengan mengaplikasikan isyarat kawalan pada terminal sumber masukan atau pada terminal get IGBT penyalaan. Rekabentuk litar yang lengkap diintegrasikan dengan gelung pencucuh bervoltan-tinggi dan palam pencucuh yang direka khas mempunyai leher yang panjang bagi kegunaan enjin gas asli. Litar ini telah diuji untuk memastikan ianya boleh menghasilkan voltan yang dikehendaki untuk menyalakan percampuran udara dan gas asli termampat di dalam silinder sebenar dan pada masa yang sesuai.

Daripada keputusan eksperimen litar penyalaan, ia menunjukkan prestasi parameterparameter penyalaan seperti arus utama dan voltan sekunder adalah lebih diakibatkan oleh parameter peranti seperti parameter-parameter IGBT penyalaan, spesifikasi gegelung penyalaan bervoltan tinggi serta strategi kawalan masa-penyuisan untuk menyalakan palam pencucuh.

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I certify that an Examination Committee has met on 10 March 2008 to conduct the final examination of Azimah binti Omar on her degree thesis entitled "High-Voltage Ignition Circuit for Compressed Natural Gas Direct Injection (CNGDI) Engine" in accordance with Universiti Pertanian Malaysia (Higher Degree) Act 1980

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#### **DECLARATION**

I declare that the thesis is my original work except for quotations and citations, which have been duly acknowledged. I also declare that it has not been previously



and is not concurrently, submitted for any other degree at Universiti Putra Malaysia or at any other institution.

AZIMAH BINTI OMAR

Date: 20 March 2008

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# LIST OF ABBREVIATIONS

A/D Analog to Digital



AFR Air-fuel Ratio

BJT Bipolar Junction Transistor

CDI Capacitive discharge ignition

CGSO gate-source overlap capacitance

(CH<sub>3</sub>)<sub>3</sub>CSH *Tertiary*-butyl mercaptan

CH<sub>3</sub>-S-CH<sub>3</sub> Dimethyl sulfide

CH<sub>4</sub> Methane

CJC collector-base junction capacitance

CJE emitter-base junction capacitance

CNG Compressed Natural Gas

CNGDI Compressed Natural Gas Direct Injection

CO Carbon monoxide

COP Coil-on-plug

CR Compression Ratio

Cs capacitors

D ratio of time

D.C. Duty cycle

DLI Distributorless semiconductor ignition system

di/dt the rate of change of the current

dic/dt current change ratio

dv/dt the rate of change of the voltage

ECU Electronic Control Unit

EMI Electromagnetic interference

*f* frequency

GDI Gasoline Direct Injection

GM General Motors

HC Hydrocarbon

HO High Output

IANGV International Association for Natural Gas Vehicle

I<sub>c</sub> Collector current

IGBT Insulated Gate Bipolar Transistor

I/O Input/Output

*Ip* primary current

Is secondary current

IS saturation current

ISE base-emitter diode saturation current

*ja* junction to the ambient

KP transconductance

kV kilovolt

 $L_{coil}$  Coil inductance

LNG Liquefied Natural Gas

LVP Low Voltage Programming

L<sub>P</sub> primary inductance

LPG Liquefied Petroleum Gas

L<sub>sn</sub> snubber circuit inductance

L<sub>st</sub> wiring inductance

mA milliampere

MCU Microcontroller Unit

mH millihenry

mJ millijoule

ms millisecond

MPI Multi Point Injection

MOSFET Metal Oxide Semiconductor Field Effect Transistor

*n* turn ratio

NG Natural Gas

NGV Natural Gas Vehicle

NO<sub>x</sub> Nitrogen oxides

 $N_P$  Primary windings

 $N_S$  Secondary windings

*Pd* Power dissipation

PIC Peripheral Interface Controller

PWM Pulse Width Modulation

RON Research Octane Number

R<sub>P</sub> Primary resistance

RPM Revolution per Minute

R<sub>S</sub> Secondary resistance

*Rs* resistors

 $R_{\theta ja}$  thermal resistance from junction to ambient

 $R_{\theta ic}$  thermal resistance from junction to case

 $R_{\theta cs}$  thermal resistance from case to sink

 $R_{\theta sa}$  thermal resistance from sink to ambient

SCR Silicon-controlled rectifier

SI Spark Ignition

SI Semiconductor ignition

SOA Safe Operating Area

subckt Subcircuit

T period

 $T_a$  ambient temperature

 $t_{cycle}$  time to complete one cycle

TDC Top Dead Center

TI Transistorized ignition

 $T_i$  junction temperature

 $t_{on}$  time the switch is on

TS turn-off delay time

T<sub>scf</sub> Trillion standard cubic feet

VAF forward early voltage

V<sub>c</sub> Collector voltage

V<sub>ce</sub> Collector-emitter voltage

 $V_{CE(sat)}$  Collector-emitter saturation voltage

 $V_{fr}$  fall period voltage

V<sub>ge</sub> Gate-emitter voltage

V<sub>pulse</sub> Pulse Voltage

VTO threshold voltage

W<sub>s</sub> safe ignition energy

μs microsecond

 $\Delta V$  voltage oscillation



#### **CHAPTER 1**

#### INTRODUCTION

#### 1.1 Background of the Ignition System

The main purpose of an *ignition system* is to ignite the air-fuel mixture in the combustion chamber at a proper time. In order to maximize engine output efficiency, the air-fuel mixture must be ignited so that maximum combustion pressure occurs approximately at 10 degrees after Top Dead Center (TDC). However, the time from ignition of the air-fuel mixture to the development of maximum combustion pressure varies depending on the engine speed and the manifold pressure. For example, ignition must occurs earlier when the engine speed is higher and later when it is lower [1].

The development of the ignition system has moved on from the conventional contact-point ignition system to the digital distributorless ignition system. The rapid design of the system is to fulfill the ignition system requirements, together with the advancement of the current engine design. In this project, the ignition system would be installed in the Compressed Natural Gas Direct Injection or CNGDI engine. It is a new engine design technology with the modification on the combustion chamber, ignition system, injection technology, fuel system, and engine management system. Different engine design gives different engine performance. Therefore, the performance of the ignition system inside the CNGDI engine and gasoline engine has



some differences on the ignition parameters. Such critical ignition parameters are firing voltage, firing current, spark voltage, and spark duration [2].

Theoretically, the ignition voltage required by the spark plug is the maximum high-voltage necessary for spark discharge, which can exceed 60 kV. The high-voltage builds up field strength between the spark gap's electrodes, so that the spark gap is ionized and thus become conductive [2]. Unfortunately, the implementation of the GDI (Gasoline Direct Injection) ignition system inside the CNGDI engine cannot fulfill the ignition system requirement. The main factor is the changes of the engine environments when the combustion chamber is mixed-up with air-gas mixture. Natural gas needs higher firing voltage to ignite the air-gas mixture as compared with the gasoline fuel.

#### 1.2 Problem Statement

The difficulty to ignite the natural gas with low voltage comes from the effect of the contents of the natural gas. There is around 90% of methane inside the natural gas with one carbon atom and four hydrogen atoms attached together. The remainder comprises of ethane, propane, butane, and other components [3]. Meanwhile, the gasoline fuel is made up of molecules composed of hydrogen and carbon arranged in chains. It has seven to eleven carbons in each chain for the configurations of heptane, octane, nonane and decane [4].

As a comparison between methane and gasoline, the strength of the carbon-hydrogen covalent bond in methane is the strongest even compare with the other hydrocarbons,

and thus its uses, as a chemical feedstock is limited. This is the characteristic of methane, which will affect the ignition performance inside the internal combustion engine. It is also reported to have higher octane rating around 130 RON; but it does not have enough energy to ignite the air-fuel mixtures at higher compression ratio [5].

Therefore, the needs to supply high-voltage ignition system have become the main issue in the combustion and ignition process of the natural gas engines. There are two ways to get the high-voltage supply to the ignition coil, by applying the high-voltage to the primary side of the ignition circuit or switch-off the current flowing through the primary side very quickly.

The first way is not applicable, as the current in the primary circuit will rise very quickly with a large applied voltage. Consequently, the increase of the current will also saturate the transformer core at the primary side of the ignition coil. The increase of the current in a short time will finally blow the power-switching device. The second way is depending on the characteristic of the power-switching device to switch-off in limited time and the amount of voltage it can deliver.

In this project, to overcome the problem mentioned above, a high voltage circuit topology is proposed by implementing a protection circuit and suitable IGBT device, IRGB14C40L. The IGBT unit would be implemented in the electronic ignition circuit design by modelling and optimizing the parameters of the device in the PSPICE software. After that, the ignition circuit would be integrated with the microcontroller unit to control the spark timing.