

THE THERMAL DECOMPOSITION

of

INORGANIC SOLIDS

Thesis presented for the degree of Doctor of Philosophy

by

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# ABSTRACT OF THESIS.

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A brief outline has been given of the present knowledge of the kinetics of the thermal decomposition of inorganic solids. The isothermal decomposition of potassium metaperiodate crystals, which were 300  $\mu$  and 40  $\mu$  in linear dimensions, has been studied, together with the effects on the subsequent decomposition, of storage and pre-irradiation with ultraviolet light.

The stoichiometric equation  $2\text{KIO}_4 \longrightarrow 2\text{KIO}_3 + \text{O}_2$  accurately represented the decomposition with no detectable intermediates. The kinetics of the decomposition involved three mechanisms. Initially, there was the decomposition of external and internal crystal surfaces. This accounted for not more than 3% of the decomposition and for one half of the total reaction time. Storage for two years did not affect the rate of the initial decomposition but pre-irradiation more than doubled the rate. This was followed by the acceleration or autocatalytic stage, which was expressed in terms of a branching plane mechanism in which the planes interfere, viz.

$$\ln \frac{\alpha}{1-\alpha} = kt + C.$$

It is considered that the branching occurred along dislocations, dividing the crystal into particles which were approximately of mosaic block size. These particles then decomposed by means of a contracting sphere mechanism, giving rise to the decay stage. The maximum rate generally occurred at 50% decomposition. The effect of storage probably facilitated the branching at imperfections, while pre-irradiation appeared to increase the number of imperfections.

The activation energy for the decomposition of  $46 \pm 4 \text{ kcal mole}^{-1}$  is similar to the heat of reaction  $\text{KIO}_4 \longrightarrow \text{KIO}_3 + \text{O}$   $\Delta H = 50 \text{ kcal mole}^{-1}$ . This suggested that the activation energy is connected with the probable primary chemical step, the rupture of the iodine-oxygen bond.

The isothermal decomposition of potassium permanganate-perchlorate solid solutions has been investigated with respect to the effect of the potassium perchlorate on the potassium permanganate decomposition. The rate of the decomposition was reduced due to the change in environment of the permanganate ion. The kinetics for pure potassium permanganate appeared to be those of the branching plane mechanism, but increasing perchlorate content resulted in the kinetics for solid solutions of 75% potassium perchlorate being expressed by a power law with  $n = 2$ , which represented two dimensional bulk growth of the reaction interface. The main effect of the addition of perchlorate to the permanganate lattice was a reduction in the 'A factor' for the decomposition of the permanganate ion.





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## Preface

The thesis is concerned firstly with an investigation of the isothermal decomposition of potassium metaperiodate and secondly with that of potassium permanganate - potassium perchlorate solid solutions.



## Abstract

A brief outline has been given of the present knowledge of the kinetics of the thermal decomposition of inorganic solids. The isothermal decomposition of potassium metaperiodate crystals, which were 300  $\mu$  and 40  $\mu$  in linear dimensions, has been studied, together with the effects on the subsequent decomposition, of storage and pre-irradiation with ultraviolet light.

The stoichiometric equation  $2\text{KIO}_4 \longrightarrow 2\text{KIO}_3 + \text{O}_2$  accurately represented the decomposition with no detectable intermediates. The kinetics of the decomposition involved three mechanisms. Initially, there was the decomposition of external and internal crystal surfaces. This accounted for not more than 3% of the decomposition and for one half of the total reaction time. Storage for two years did not affect the rate of the initial decomposition but pre-irradiation more than doubled the rate. This was followed by the acceleration or autocatalytic stage, which was expressed in terms of a branching plane mechanism in which the planes interfere, viz.

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The activation energy for the decomposition of  $46 \pm 4$  kcal mole<sup>-1</sup> is similar to the heat of reaction  $\text{KIO}_4 \longrightarrow \text{KIO}_3 + \text{O} \quad \Delta H = 50$  kcal mole<sup>-1</sup>. This suggested that the activation energy is connected with the probable primary chemical step, the rupture of the iodine-oxygen bond.

The isothermal decomposition of potassium permanganate-perchlorate solid solutions has been investigated with respect to the effect of the potassium perchlorate on the potassium permanganate decomposition. The rate of the decomposition was reduced due to the change in environment of the permanganate ion. The kinetics for pure potassium permanganate appeared to be those of the branching plane mechanism, but increasing perchlorate content resulted in the kinetics for solid solutions of 75% potassium perchlorate being expressed by a power law with  $n = 2$ , which represented two dimensional bulk growth of the reaction interface. The main effect of the addition of perchlorate to the permanganate lattice was a reduction in the 'A factor' for the decomposition of the permanganate ion.

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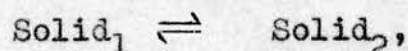
THE ISOTHERMAL DECOMPOSITION OF POTASSIUM PERMANGANATE-  
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## General Introduction

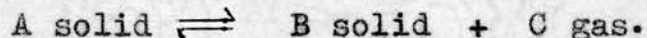
In reactions in the solid state new solid phases are produced which entail a spacial propagation of the reaction. It is this spacial aspect which characterises solid state reactions, and is an important factor in the mechanism and kinetics.

A simple solid reaction is a polymorphic transformation of the type



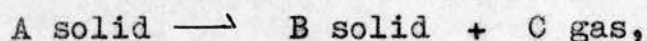
which is reversible in the case of tin<sup>1</sup> an enantiotropic change, or irreversible as in azoxybenzene<sup>2</sup> a monotropic change.

The more general class of inorganic reactions studied are of the type



Endothermic reactions of this type may be complicated by the occurrence of both dissociation and recombination processes, but the information gained about nucleation and the interface reaction is worth the experimental and theoretical complications involved. Work in this field has been restricted to the dehydration of salt hydrates and the dissociation of metal carbonates. A comprehensive review has been given by Garner<sup>3</sup>.

Irreversible exothermic decompositions,



to which category potassium metaperiodate and potassium permanganate belong, have been fairly systematically studied, especially the decomposition of azides and oxalates. The kinetics are easily followed by measuring the pressure of the



evolved gases or the loss in weight of solid A.

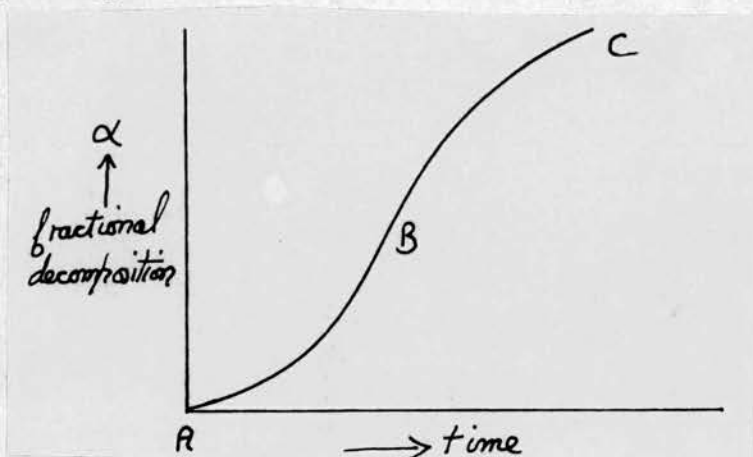
Langmuir<sup>4</sup> pointed out that when  $A \rightarrow B$  to form another phase, it is necessary that the reaction occurs only at the boundary between the two phases. The formation of a stable fragment of phase B, called a growth nucleus, involves the free energy of nucleation, and can only occur when the local fluctuations in the lattice energy of the solid are sufficient to supply the necessary activation energy. The energy required is least at imperfections in the crystal lattice such as dislocations<sup>5</sup>, grain boundaries and Smekal cracks, and at the surfaces of very small crystals. Growth of nuclei is preferred at these sites since large lattice stresses can not be supported in their vicinity. This has been experimentally shown by Hedges and Mitchell<sup>6</sup> for the photolysis of silver bromide.

When the free energy of activation of nucleus formation is substantially higher than that for growth of the nuclei, a few compact nuclei are formed; this has been observed with barium azide<sup>8</sup> and for the decomposition of hydrates<sup>9,10</sup>. On the other hand if these free energies are of the same order a large number of diffuse nuclei are formed which may not grow to visible size.

The subsequent decomposition is mainly governed by the continued production and/or growth of these nuclei. A review of the different mechanisms has been given by Jacobs and Tompkins<sup>11</sup> and by Garner<sup>12</sup>.

The pressure time curves for isothermal decompositions are generally divided into portions, (1) an acceleration stage AB and

(2) a decay stage BC.



In addition and preceding AB, an initial evolution of a small amount of gas may occur, as for example with mercury fulminate<sup>13,14,15,16</sup> and lithium aluminium hydride<sup>17</sup>. The acceleration of the reaction is due to an increase in the area of the decomposition interface with time, explained by the growth of individual nuclei and an increase in the number of these nuclei.

When nucleation is very efficient and there is a rapid coverage of the surface of the crystals with small nuclei only the decay stage is observed. This occurs in lead azide<sup>18</sup>.

Theoretical relationships between ' $\alpha$ ' and ' $t$ ', (' $\alpha$ ' = fraction decomposed at time ' $t$ '), are derived in terms of production and growth of nuclei.

Crystal imperfections can be considered as 'germ' nuclei. Their conversion into 'growth' nuclei is governed by one of two laws. (1) The rate of formation of growth nuclei decreases exponentially with time, as the number of germ nuclei are used up. (2) The rate of formation varies as a power of the time. In both cases the rate of nucleation is constant when either the

probability of a germ nucleus becoming a growth nucleus is small or when the power of the time is zero. These growth nuclei grow in either one, two or three dimensions and give rise to transformation-time equations of the form  $\alpha = At^n + B$ . This power law represents the 'normal' growth of nuclei, where 'n' is a constant composed of the dimensions of growth and rate of nucleation. The power law holds well for barium azide<sup>8,19</sup>, calcium azide<sup>20</sup>, silver oxide<sup>21,22</sup> and aged mercury fulminate<sup>16</sup>.

However this law takes no account of the ingestion of germ nuclei by growth nuclei and the effect of overlapping of the nuclei which will occur at about  $\alpha = 0.5$ . These factors were considered by Arami<sup>23</sup>, who developed an equation

$$\alpha = 1 - e^{-kt^n}$$

which should apply for both the acceleration and decay periods, although if the interface, between product and reactant collapses and each molecule has an equal chance of decomposing a unimolecular decay law will result. Erofeyev<sup>24</sup> and Mampel<sup>25</sup> have arrived at the same formula by different approaches. The Avrami equation has been successfully applied by Burgers and Groen<sup>1</sup> to the kinetics of the allotropic transformation of tin.

There is a further type of reaction where the acceleration period shows an exponential increase of ' $\alpha$ ' with time. This exponential relationship has two physical interpretations. The first involves a 'branching plate' mechanism, where the increase in the area of the interface reaction is not caused by the production and growth of nuclei, but the creation of fresh surfaces by cracking. It is considered that the product molecules



on the surfaces of the crystal produce lateral stresses, which are relieved by cracks along which nucleus formation is favoured. The reaction therefore spreads into the crystal down these crevices and covers the inner surfaces with product molecules. The cracking process is repeated on the fresh surfaces and the reaction proceeds through the solid by a system of branching planes of decomposed material. When the rate of decomposition is governed by the rate of branching an exponential law results

$$\alpha = De^{kt},$$

where  $k$  is the probability of branching. When these chains interfere it is necessary to include a further term - the probability of termination - which alters the exponential law to

$$\ln_e \frac{\alpha}{1 - \alpha} = kt + C.$$

Prout and Tompkins<sup>27</sup> were the first to apply this equation to the decomposition of potassium permanganate. It has subsequently been applied to the other alkali and alkaline earth permanganates. The Prout-Tompkins equation also holds for fresh mercury fulminate<sup>16</sup>, lead oxalate<sup>28</sup>, ammonium dichromate<sup>29</sup> and lanthanum oxalate<sup>30</sup>.

The second mechanism by which an exponential law can be explained is where nuclei are produced by diffusion of the product into the reactant, thus creating a rapid increase in the number of growth nuclei. This was first proposed by Garner<sup>31</sup> and recently developed by Hill<sup>32</sup> in his studies involving potassium permanganate.

For the decay period, a decrease in the rate with time can best be explained by a decrease in the interface area of the reaction as the decomposition progresses. A contracting-sphere is the simplest three dimensional case where the decomposition progresses from the outside of a spherical particle to the centre. This has adequately explained the results in the case of mercury oxalate<sup>33</sup> and silver oxalate<sup>34</sup>. If this interface collapses the rate will depend on the number of unreacted molecules a unimolecular decay law resulting. The latter law is modified if the unreacted molecule, before it can decompose, has to be contiguous with a product molecule. Under these conditions the pressure time relationship is the same as the Prout-Tompkins equation for the acceleration.

In many decompositions studied the age of the crystal has been found to have a marked effect. For mercury fulminate<sup>16</sup>, a chemical explanation is possible due to slow decomposition on storage at room temperature. But in general physical ageing has been observed<sup>35</sup>, the mechanism for which is not clearly defined.

Irradiation with electro-magnetic waves or high energy particles, prior to decomposition, can also produce changes in the subsequent decomposition as in silver oxalate<sup>34,36,37</sup>. This appears to be primarily due to the production of growth nuclei or points from which the Prout-Tompkins branching may take place. Herley and Prout<sup>38,39,40</sup> have made an extensive study of the effect of irradiation on the permanganates.

Measurements of electrical conductivity of solids are of qualitative value in giving an activation energy for the conduction

process, which may be compared with that for the rate determining stage of the reaction<sup>29</sup>. Its use in showing the coalescence of metallic nuclei at the maximum rate stage, when the nuclei are three dimensional has been shown for the alkaline earth azides<sup>20</sup> by Garner and Reeves. Garner and Haycock have used the conducting properties of lithium aluminium hydride<sup>17</sup> to show the initial production of  $F^{\cdot}$  centres and their diffusion from the surface into the lattice where they increase the conductivity. The association of these  $F^{\cdot}$  centres causes a sharp drop in conductivity when they form nuclei, and the conductivity then remains constant until the metallic nuclei coalesce.

Infra-red absorption measurements on the solid and the partially decomposed solid can give further evidence regarding the mechanism of the decomposition. For ammonium dichromate<sup>29</sup> the presence of an intermediate was indicated but the identity was not established.



Section IThe isothermal decomposition of potassium metaperiodate

1.

Introduction

Related salts known as the periodates are best understood as being salts of acids derived from the hypothetical iodine heptoxide by the addition of water step by step. With one molecule of water, metaperiodic acid is formed, of empirical formula  $\text{HIO}_4$ . This gives rise to potassium metaperiodate, a colourless transparent solid crystallising in tetragonal bipyramids. Mellor<sup>41</sup> in a survey of early work reports that the salt decomposes at  $570^\circ - 670^\circ\text{K}$  to give potassium iodate and oxygen. It will be shown later that the stoichiometric equation,



accurately represents the reaction with no detectable intermediates. This is an exothermic reaction with  $\Delta H = -9 \text{ kcal mole}^{-1}$  at  $298^\circ\text{K}$ , as calculated from the heats of formation of potassium metaperiodate<sup>42,43</sup> and potassium iodate<sup>42</sup>.

Potassium metaperiodate thus appears to be suitable for the study of solid state kinetics as it decomposes to give a single solid phase and one of the permanent gases.

2.

Experimental2. 1. Chemistry of the reaction

The white solid produced by the decomposition of potassium metaperiodate at  $550^{\circ}\text{K}$  was soluble in water. The addition of silver nitrate solution gave a white precipitate which was insoluble in dilute nitric acid, but soluble in dilute ammonium hydroxide solution, leaving no residue. The solid product was thus potassium iodate and as no iodide ions were observed, there is no further decomposition to potassium iodide. It was concluded that the uncondensable gas released was oxygen.

In subsection 2. 6. known amounts of the salt were decomposed and the quantity of oxygen liberated was measured. In all cases the quantity of oxygen evolved was  $0.5 \pm 0.01$  mole per mole of potassium metaperiodate. The quantity of the solid product potassium iodate corresponded to 1 mole of potassium metaperiodate. For example in run A1, 21.34 mg of  $\text{KIO}_4$  produced 20.83 mg of  $\text{KIO}_3$  giving a loss in weight of 1.51 mg. The final pressure of oxygen evolved corrected to  $273^{\circ}\text{K}$  in 6.673 l. was  $119.3 \mu$  which is equivalent to 1.50 mg of oxygen.

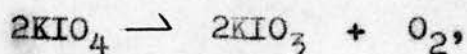
Therefore the moles of oxygen produced per mole of  $\text{KIO}_4$  was 0.505 calculated from the final pressure and 0.51 calculated from the loss in weight. This agrees with  $2\text{KIO}_4 \rightarrow 2\text{KIO}_3 + \text{O}_2$ .

X-ray powder photographs of the product were identical to those of recrystallised analar potassium iodate.

In a search for intermediate products infra-red absorption measurements (Nujol mull technique, Hilger H800 spectrophotometer)

were carried out on analar potassium metaperiodate and on samples that had been separately 0.3, 25, 50, 75 and 100% decomposed at 550°K. The relative intensities of the very strong metaperiodate ion peak<sup>44</sup> 848 cm<sup>-1</sup> decreased linearly with the percentage decomposition as the very strong iodate ion peak<sup>44</sup> 738 cm<sup>-1</sup> increased. No peaks were observed other than those of metaperiodate and iodate.

Thus the reaction is

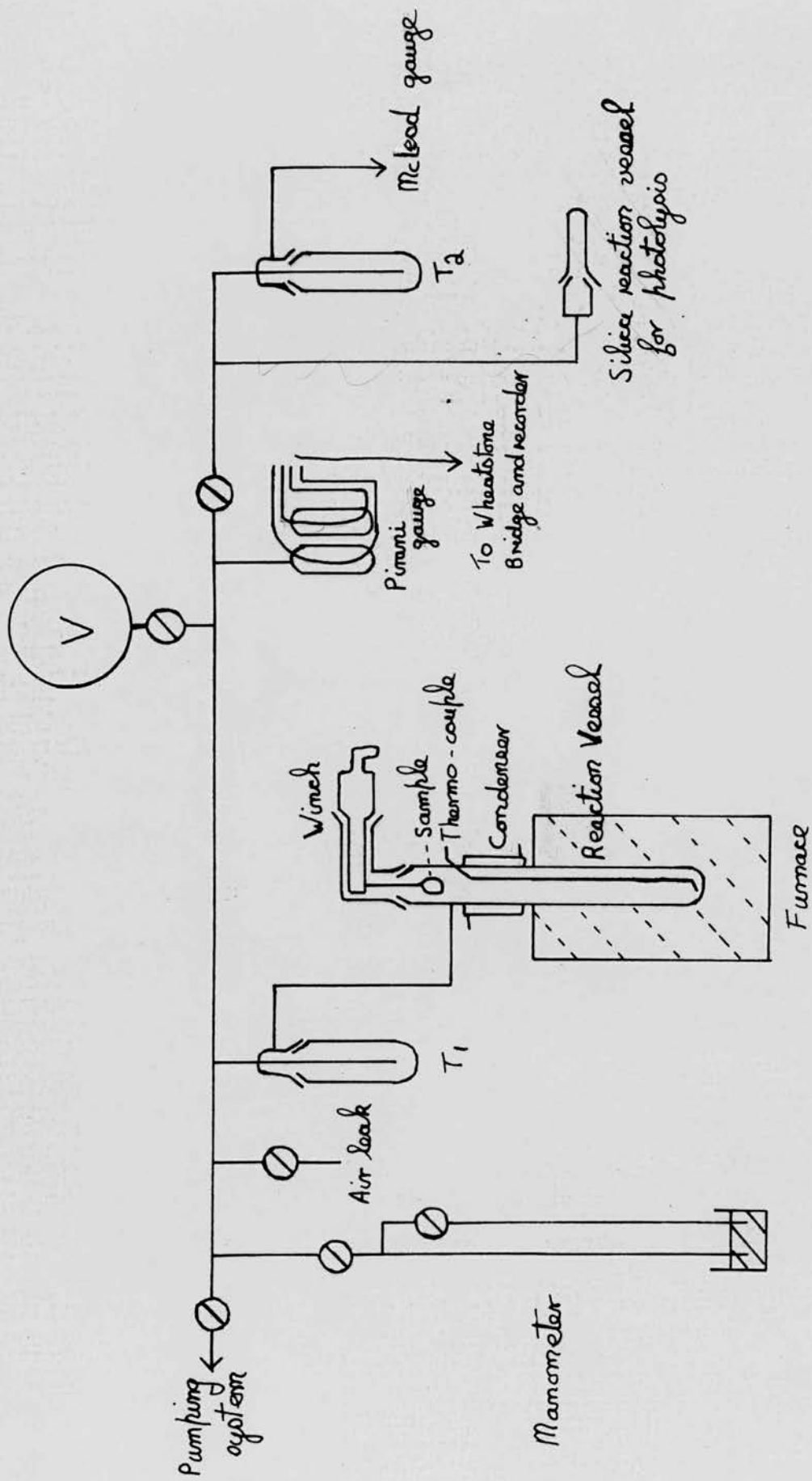


with no detectable intermediates.

## 2. 2. Apparatus and procedure

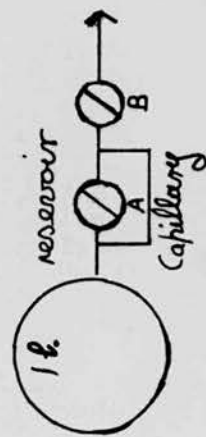
The apparatus (Fig. 1a) and experimental procedures were similar to those described by Simpson and Taylor<sup>29</sup>. Decompositions were carried out in a closed system, in which the pressure increase in a known volume, was measured by a McLeod gauge. The Pyrex reaction vessel carrying the thermal couple pocket was centrally situated in an electrically heated furnace. The sample contained in a small bucket constructed from 2 cm<sup>2</sup> of 0.0025 cm thick platinum foil, could be lowered into the furnace by means of the winch, to which the bucket was attached by a fine platinum wire. The furnace was stabilised to better than 0.1° by a Sunvic Resistance Thermometer Controller type RT2, with the A.C. mains basic power supply stabilised by a voltage stabiliser. The thermocouple with one junction at the bottom of the reaction vessel and the other held at 0° in ice, was calibrated in steps of 5° from 470° - 570°K against a standard Pt/Pt Rh thermocouple; the voltage was read to





Apparatus for pressure measurements

Fig. 1 a.



Apparatus for diffusion measurements

Fig. 1 b.

0.001 mv on a Tinsley potentiometer type 3184D.

The gases from the reaction vessel passed through trap  $T_1$  into the vacuum line. V consisted of three bulbs any of which could be connected to the vacuum line to give pressures in the desired range. The pressures were measured by a McLeod gauge measuring from  $10^{-3} \mu$  to  $1.6 \times 10^2 \mu$ .

In section II experiments on potassium permanganate were carried out in an identical apparatus, but using a pressure gauge of the compensating Pirani type. It was operated at constant voltage by a Wheatstone bridge method, the out of balance voltage being fed, through a shunt into a Sunvic recorder. A linear response was obtained up to  $10^2 \mu$ , the gauge being calibrated against a standard McLeod gauge.

The volume of each section of the system was found by expanding a known pressure of dry air from a known volume, through the air leak into each section, and measuring the resultant pressure on the manometer. From Boyle's law the volume of each section was calculated, small volumes, where necessary, being calculated from their dimensions. The volumes given in Table I are the mean of three determinations and were obtained with the reaction vessel and both traps at room temperature. The pressures read on the McLeod or Pirani gauges were converted to pressures at  $273^\circ\text{K}$  by a correction factor calculated from the respective volumes and temperatures, of the reaction vessel, of the cold traps and of the remaining volume of the system.

Table I

| Section of Thesis | Section of system                                  | Mean volume c.c. | $\frac{p_{273^{\circ}\text{K}}}{p_{\text{measured}}} =$ | correction factor |
|-------------------|--|------------------|---|-------------------|
| I                 | Reaction line<br>+ T <sub>1</sub> + T <sub>2</sub> | 608              | }   | 1.00              |
|                   | McLeod gauge                                       | 376              |   |                   |
|                   | Bulb 1   | 1100             | -   |                   |
|                   | Bulb 2   | 2303             | -   |                   |
|                   | Bulb 3   | 2335             | -   |                   |
|                   | Total volume<br>(added)                            | 6722             |   | 0.94              |
| II                | Reaction line<br>+ T <sub>1</sub> + T <sub>2</sub> | 369              |   | 1.38              |
|                   | McLeod gauge                                       | 230              |   | -                 |
|                   | Total volume<br>(added)                            | 599              |   | 1.23              |

The pumping system consisted of a glass two stage mercury diffusion pump, backed by a Speedivac rotary oil pump, the unit giving a vacuum of  $10^{-3}$   $\mu$ . Apieson 'L' grease was used for all joints and taps.

Rate of diffusion of air through the apparatus.

An attempt was made to find the maximum rates of gas evolution from the reaction vessel that could be measured on the McLeod gauge, without correction having to be applied for diffusion effects. The apparatus shown in Fig. Ia was adapted with that shown in Fig. Ib substituted for the winch. The rate of flow through the



capillary into the apparatus was controlled by the pressure in the reservoir, and the pressure in the apparatus adjusted to what was required. With tap A closed and tap B open gas (air) was allowed to flow for 3 min., tap B then closed and the pressure  $P_I$  in the McLeod gauge read. After 5 min. the pressure  $P_F$  was again measured,  $P_I - P_F$  is the error due to diffusion. The rates and pressures were varied and the following conclusions were drawn.

With bulb V closed and with the maximum rates encountered experimentally, there was no measurable difference between  $P_I$  and  $P_F$ . With the bulb V open and a rate of  $3 \mu \text{ min}^{-1}$ , when the initial pressure in the apparatus was  $50 \mu$ ,  $P_I - P_F$  was  $1 \mu$ . This represented the extreme experimental conditions and resulted in an error of 2%. For the fast runs no correction was made for this error.

As  $P_I > P_F$ , the gases entered the McLeod gauge before the volume bulbs and generally for a given rate the lowering of the initial pressure increased the error. These results were obtained with the furnace on and the cold trap 1 surrounded by liquid nitrogen; when the cold trap was removed the error was doubled due to temperature effects.

#### Experimental procedure.

With the weighed crystals (10 - 20 mg) in the platinum bucket the total volume was pumped out overnight, a vacuum of  $10^{-3} \mu$  being obtained. The system was isolated from the pumps and the taps to the volume bulbs closed. If after an hour the pressure remained below  $10^{-2} \mu$ , the sample was lowered into the furnace so that it

made good contact with the bottom of the pocket containing the thermocouple. The thermocouple indicated a maximum heating up time of 5 min and gave no evidence of self heating of the crystals during decomposition.

With liquid nitrogen surrounding  $T_1$ , the McLeod gauge measured the pressure of oxygen evolved during the decomposition, readings being taken every five minutes. When the pressure reached ca  $10^2 \mu$  the total volume of the system was used. The final pressure was recorded at least one hour after the apparent end point had been attained.

### 2. 3. Growth of Crystals

Analar potassium metaperiodate was used as the initial material. Due to its low solubility (ca 6 g.  $l^{-1}$  at  $20^\circ C$ ), difficulties were encountered in producing crystals of suitable size. The effect on a saturated solution of stirring during cooling, of the rate of cooling and evaporation, and of the time of growth, were investigated. The following procedure was finally adopted.

A saturated solution of the salt was prepared at  $60^\circ C$  from ca 6 g. and 600 ml. of dust-free distilled water, allowed to come to equilibrium at room temperatures, and then decanted into a 9 inch crystallising dish. This solution was evaporated slowly at room temperature in a draught of air, over a period of a month, fresh mother liquor being added occasionally to keep the volume ca 500 ml. The resulting crystals were dried and sieved. The largest crystals that were reasonably free from visible imperfections, such as steps on the crystal faces and occlusions, were used in the

experiments. They passed through the British Standard sieve of mesh number 52 and were held by number 60, therefore they had linear dimensions of ca 250 - 300  $\mu$ . 1 g. of crystals of these dimensions were obtained from six sets of evaporations as described above and are referred to as 'large' crystals.

'Small' crystals, that appeared under the microscope to be free from obvious imperfections, were made by the rapid cooling of a saturated solution from 90°C to room temperature. The crystals, that passed through a 300 mesh sieve, and thus had linear dimensions  $< 50 \mu$ , were used in the experiments. As the crystals did not readily pass through the sieve, and were visible under the microscope their linear dimensions were taken as ca 40  $\mu$ .

The following batches of material were prepared by the above procedures.

#### Large crystals

A material A made in diffuse light.

B material A after storage for 18 months.

C repeat of material A but made in the dark.

D material C after pre-irradiation with u.v. light as subsequently described (2. 4.).

E similar to material A but stored for 12 months.

#### Small crystals

F made as described.

G material F after storage for 24 months.

H repeat of material F.

K material H after pre-irradiation with u.v. light.



The above material was stored, until required, in the dark, in a vacuum desiccator over calcium chloride. It was experimentally determined that 300 mg. of crystals dried at  $110^{\circ}\text{C}$  for a week lost  $<0.03$  mg. in weight. Thus the water content was less than 0.01%.

The kinetic experiments performed on material A and F were started immediately after the preparation of the crystals, and extended over a period of four months, but for material C and H the experiments were concluded within three weeks.

#### 2. 4. Effect of ultraviolet irradiation and electron bombardment

The small photolytic decomposition of potassium metaperiodate, was measured using the apparatus shown in Fig. 1a. The tap between the thermal reaction vessel and the McLeod gauge was closed making the volume of the system used 500 ml. The source of the ultraviolet light was a 300 w Hanovia mercury lamp, placed 8 cm. from the vitreous silica tube. To avoid thermal effects a copper sulphate solution contained in a silica vessel was interposed between the lamp and the silica tube; this ensured that the temperature of the tube did not rise above  $35^{\circ}\text{C}$ .

Crystals were spread in a layer in the silica tube and this was attached to the apparatus. With liquid nitrogen surrounding  $\text{T}_2$ , and when a vacuum of  $0.1 \mu$  was held for 10 h., the irradiation was begun. The increase in pressure was measured over a period of 20 h. using the McLeod gauge. This procedure was repeated with crystals of varying sizes. It was concluded that the rate of evolution of gas varied with the surface area exposed to

irradiation and that the rate, corrected for a slight blank rate, was ca  $0.004 \mu \text{ h}^{-1} \text{ cm}^{-2}$  in the 500 ml. This represents ca  $1 \times 10^{-10}$  mole of oxygen  $\text{h}^{-1} \text{ cm}^{-2}$ .

After 10 h. irradiation the crystals were noticeably yellow. The colour could be destroyed by heating for 30 sec. at  $550^{\circ}\text{K}$ , or 2 h. at  $370^{\circ}\text{K}$ , or by the effect of daylight for 3 months at room temperature.

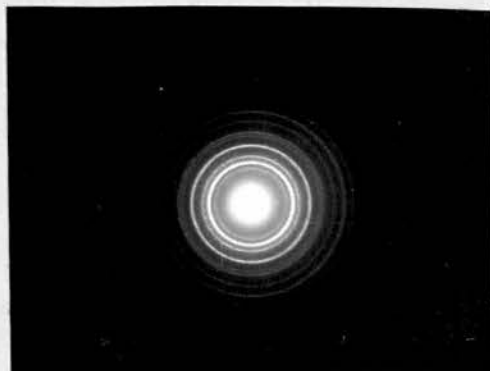
Material C, fresh large crystals, and H fresh small crystals were pre-irradiated for 18.5 h. under conditions similar to those used in the photolytic experiments. In this case the silica tube was shaken every  $\frac{1}{2}$  h. to expose fresh surfaces. The pre-irradiated material is designated D and K respectively.

It was not possible to estimate directly the volume of oxygen liberated in the above experiments due to the necessity to shake the tube, but this was found from the known rate of photolytic decomposition, and the size of the crystals. The fractional decomposition ' $\alpha$ ' after 18.5 h. irradiation for material D was ca  $5 \times 10^{-5}$  and for material K was ca  $35 \times 10^{-5}$ .

Microscopic examination of the crystals before and after irradiation failed to show any observable differences, apart from the slight yellow coloration, although the subsequent thermal decomposition (2.6) was radically altered.

Sawhill<sup>45</sup> in a detailed study of the effects of an electron beam on silver azide showed that after decomposition only silver remained and it was in two forms, randomly orientated as shown by the rings on the diffraction photograph, and highly orientated as shown by the intense arcs on the rings.

The effect of an electron beam on potassium metaperiodate was observed employing a Metropolitan Vickers Electron microscope 6. Using 50 kvolt potential and a tube current of 100  $\mu$  amp., the electrons were focused on a single crystal of ca 1  $\mu$  linear dimensions and a diffraction photograph taken.



It can be seen from the photograph that sets of rings were obtained. The two strong reflections (rings two and four as counted from the centre), are due to the (100) and (110) crystal planes in  $\text{KIO}_3$  as deduced from the structure given by Smith<sup>46</sup>, while the first and third rings are probably due to the (111) and (110) planes of  $\text{KIO}_4$ <sup>47</sup>. Diffraction photographs during the decomposition of crystals ca 0.1  $\mu$  showed rings of ca 100 spots. This is to be expected because a crystal of 0.1  $\mu$  will give rise to fewer particles than one of 1  $\mu$ . These photographs clearly show that potassium metaperiodate decomposes in an electron beam and breaks up into randomly oriented parts.



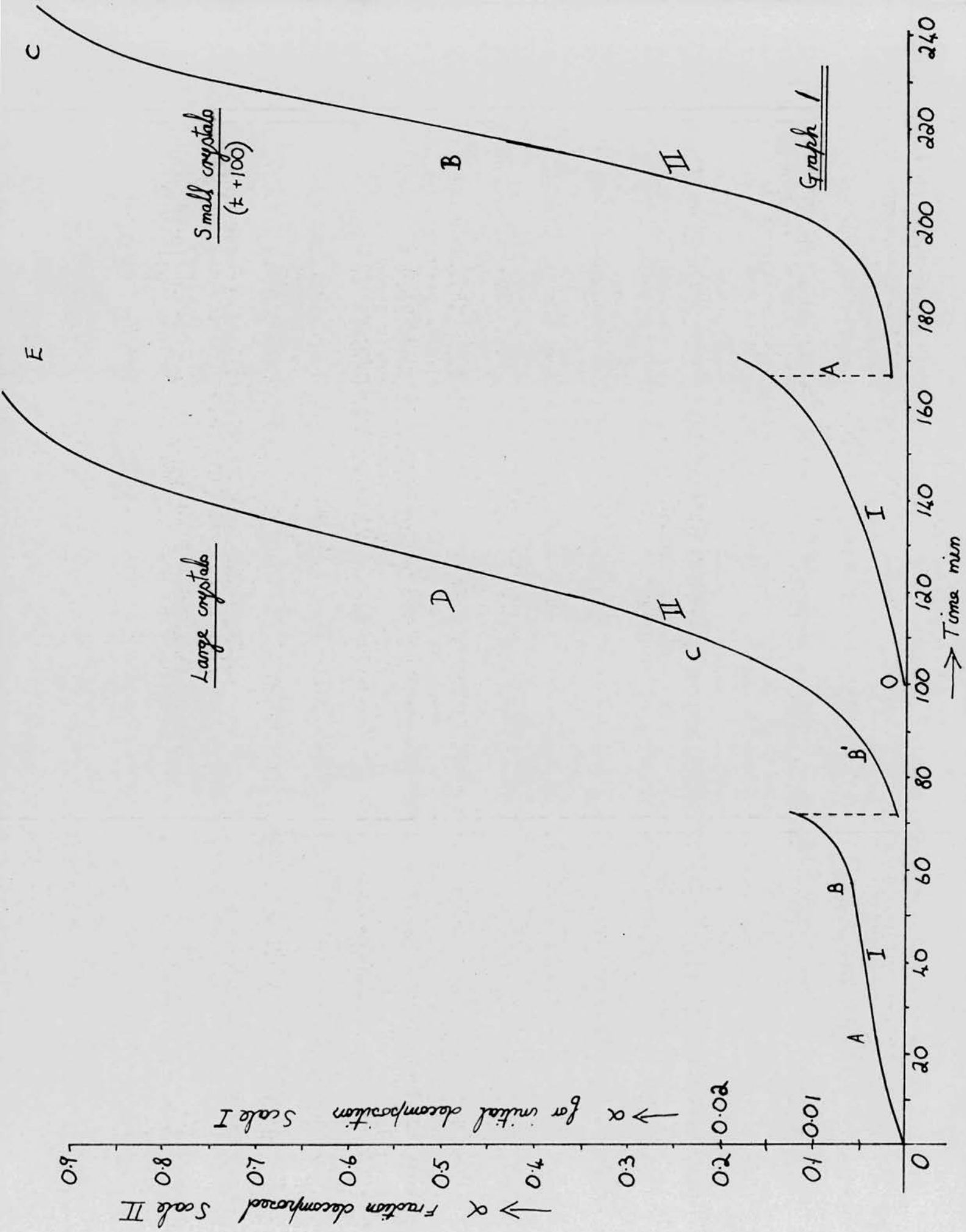
## 2. 5. Visual observations of the decomposition

When crystals of material A were heated ( $2^{\circ} - 3^{\circ}/\text{min}$ ) in air on a hot-stage microscope, white diffuse opaque centres developed, ( $510^{\circ} - 520^{\circ} \text{ K}$ ) at visible imperfections in the crystals, and by  $550^{\circ} \text{ K}$  these had spread throughout the crystals. At  $570^{\circ} \text{ K}$  the crystal broke into two or three fragments, and with the rising temperature there was rapid decrepitation. The direction of the cracking and splintering was random and bore no relationship to the crystal axes. Above  $580^{\circ} \text{ K}$  no further changes were noted, the small fragments being white and opaque.

Small crystals became gradually white in colour, but there was no sign of decrepitation. They retained their original crystal form at the end of the decomposition.

By the use of a vapour bath in place of the furnace (Fig. Ia) and a glass bucket substituted for the platinum one, a continuous observation was made on the decomposition as it progressed at a fixed temperature. For the unirradiated crystals dimethyl phthalate boiling at  $553^{\circ} \text{ K}$  was used as the liquid in the vapour bath and for the irradiated crystals ethyl cinimate boiling at  $543^{\circ} \text{ K}$ .

For the large crystals A, with reference to graph I, over the stage O - A ( $\alpha = 0.0 - 0.003$ ), there was a steady but infrequent fragmentation. For A - B ( $\alpha = 0.003 - 0.006$ ) occasional fragmentation occurred but at a quarter of the rate for OA. At the end of this stage the crystals appeared to be mainly opaque, and 90% of them were structurally intact.



Vigorous decrepitation was observed for the acceleration stage B - C ( $\alpha = 0.01 - 0.30$ ), but following this there were no further signs of fragmentation.

For the large pre-irradiated crystals D, the vigorous decrepitation did not begin until  $\alpha = \text{ca } 0.03$ , and for the intermediate stage B - B<sup>1</sup> the rate of fragmentation was the same as for OA; at B<sup>1</sup> some crystals were still intact.

The size distribution of the fragments at the end of the decomposition showed that 30% were less than 50  $\mu$ , 60% between 50 and 150  $\mu$  and 10% greater than 150  $\mu$ . It will be noted that the average dimensions of these particles is greater than that of the small crystals.

It is apparent that the clouding of the crystals as decomposition progresses is due to the formation of potassium iodate.



## 2. 6. Kinetics of the decomposition

Kinetic measurements were carried out on material A - K (2.3.) as described in the experimental procedure (2.2). The  $\alpha'$ -time curves were of the general form shown in graph 1 and were analysed in terms of the following relationships between  $\alpha'$  and  $t'$ , where  $\alpha'$  is the ratio of the pressure at time  $t'$ , to the final pressure. Thus  $\alpha'$  represents the fraction of the material decomposed at time  $t'$ .

Large crystals; material A B C D and E:

The linear relationship between  $\alpha'$  and  $t'$ , section AB, was represented by  $\frac{d\alpha}{dt} = k_1 = R_L$ , with  $\alpha_L$  the fraction decomposed at B the end of the linear stage, which occurred at ca  $\alpha = 0.005$ .

For the large pre-irradiated material D the section  $BB^1$  of the curve fitted a power law with  $n = 4$ ,  $(\alpha - \alpha_L) = k_4(t - t_0)^4$ , where  $t_0$  is the time at the start of the mechanism. From a plot of  $(\alpha - \alpha_L)^{1/4}/t$  the constants  $k_4^{1/4}$  and  $t_0$  are obtained.

The acceleration stage, BD in the case of unirradiated material and  $B^1D$  for irradiated material, is adequately fitted by the Prout-Tompkins equation corrected for the initial decomposition  $\alpha_L$ ,

$$\log_{10} \frac{\alpha - \alpha_L}{1 - \alpha} = \frac{k}{2.3}t + C_1.$$

The decay stage of the reaction DE is described in terms of a contracting sphere mechanism,

$$\alpha = 1 - [C_2 - k_3(t - t_0)]^3$$

where  $t_0$  is the time at the start of the mechanism and  $C_2$  and  $k_3$  are constants. A plot of  $(1 - \alpha)^{1/3}/t$  gives the constant  $k_3$ .

This equation is discussed later.

Small crystals; material F G H and K:

The first 2 - 3% of the reaction, stage OA, is fitted by a power law with  $n = 2$ ,  $\alpha = k_2(t - t_0)^2$ . The factor  $\alpha^{\frac{1}{2}}$  is plotted against 't' to give the constant  $k_2^{\frac{1}{2}}$ .

The acceleration stage AB and decay stage BC are fitted by Prout-Tompkins equation and the contracting sphere equation respectively, as for the large crystals. Generally the decay stage began at  $\alpha = 0.5$ .

The following tables and graphs show a cross section of the runs performed at various temperatures in the range  $529^\circ - 561^\circ$  K. The tables give the respective functions of  $\alpha$  as required by the above analysis and the graphs show the plots of the different functions.

An alternative analysis for the acceleration stage is that of a power law with  $n = 3$ , and so included in the tables is the function  $\alpha^{\frac{1}{3}}$ . The merits, graphical and kinetic, of this equation compared with the Prout-Tompkins equation, are discussed in section 3.

The following abbreviations have been used in the subsequent tables:

$$\underline{PT} = \log_{10} \frac{\alpha}{1 - \alpha} ; \quad \underline{PT}_L = \log_{10} \frac{\alpha - \alpha_L}{1 - \alpha} ; \quad \underline{PT}_P = \log_{10} \frac{\alpha - \alpha_P}{1 - \alpha} ;$$

$$\underline{\alpha}_L^{\frac{1}{3}} = (\alpha - \alpha_L)^{\frac{1}{3}} ; \quad \underline{\alpha}_P^{\frac{1}{3}} = (\alpha - \alpha_P)^{\frac{1}{3}} ; \quad \underline{\alpha}_L^{\frac{1}{2}} = (\alpha - \alpha_L)^{\frac{1}{2}} ,$$

where  $\alpha_L$  is as previously given and  $\alpha_P$  is the fractional decomposition at the end of the initial power law growth.

In 2.6.6. the constants  $k_x$  are tabulated for the various runs together with the respective Arrhenius activation energy plots.

2. 6. 1. Kinetic results for large crystals A and B

Tables 2, 3, 4 and 5 and graphs 2, 3, 4, 5 and 6 illustrate the effect of 18 months ageing on large crystals. Material A is fresh crystals, and B is the same material after storage for 18 months. The most notable features are, the much increased rate for the acceleration stage, and the onset of the decay stage at  $\alpha = 0.2$  for the aged material compared with  $\alpha = 0.5$  for the unaged. The pre-acceleration, linear stage AB, starts at ca  $\alpha = 0.002$  and continues to  $\alpha = 0.005$ ; this is little affected by ageing.

Tables 2 and 3, analysis of material A.

Tables 4 and 5, analysis of material B.

Graphs 2 and 3, the ' $\alpha$ ' - 't' curves for material A and B respectively.

Graph 4a and b, linear stage, the ' $\alpha$ ' - 't' curves showing the pre-acceleration stage of the decomposition for material A and B.

Graph 5, acceleration stage, plot of Prout-Tompkins factor for material A and B.

Graph 6, decay stage, plot of the contracting sphere factor for A and B.



Table 2. Material A. Large crystals.

| Run<br>Temp<br>$\alpha_L$<br>Time<br>min | A2<br>555.2°K<br>0.0055 |                 |                          |                            | A12<br>551.2°K<br>0.006 |                 |                          |                            |
|--|-------------------------|-----------------|--------------------------|----------------------------|-------------------------|-----------------|--------------------------|----------------------------|
|  | $\alpha \times 10^2$    | PT <sub>L</sub> | $\alpha_L^{\frac{1}{3}}$ | $(1-\alpha)^{\frac{1}{3}}$ | $\alpha \times 10^2$    | PT <sub>L</sub> | $\alpha_L^{\frac{1}{3}}$ | $(1-\alpha)^{\frac{1}{3}}$ |
| 10                                       | 0.08                    |                 |                          |                            | 0.15                    |                 |                          |                            |
| 15                                       | 0.12                    |                 |                          |                            | 0.22                    |                 |                          |                            |
| 20                                       | 0.24                    |                 |                          |                            | 0.27                    |                 |                          |                            |
| 25                                       | 0.32                    |                 |                          |                            | 0.32                    |                 |                          |                            |
| 30                                       | 0.37                    |                 |                          |                            | 0.36                    |                 |                          |                            |
| 35                                       | 0.42                    |                 |                          |                            | 0.41                    |                 |                          |                            |
| 40                                       | 0.48                    |                 |                          |                            | 0.45                    |                 |                          |                            |
| 45                                       | 0.55                    |                 |                          |                            | 0.49                    |                 |                          |                            |
| 50                                       | 0.74                    | 0.95            |                          |                            | 0.53                    |                 |                          |                            |
| 55                                       | 0.90                    | 1.66            | 0.16                     |                            | 0.59                    |                 |                          |                            |
| 60                                       | 1.77                    | 2.09            | 0.23                     |                            | 0.66                    | 0.81            | 0.087                    |                            |
| 65                                       | 3.41                    | 2.47            | 0.31                     |                            | 0.78                    | 1.20            | 0.117                    |                            |
| 70                                       | 6.33                    | 2.79            | 0.39                     |                            | 0.93                    | 1.44            | 0.140                    |                            |
| 75                                       | 10.5                    | 3.04            | 0.46                     |                            | 1.42                    | 1.88            | 0.203                    |                            |
| 80                                       | 17.7                    | 3.32            | 0.55                     | 0.94                       | 2.21                    | 2.21            | 0.252                    |                            |
| 85                                       | 26.5                    | 3.54            | 0.64                     | 0.90                       | 3.44                    | 2.47            | 0.305                    |                            |
| 90                                       | 37.0                    | 3.76            | 0.71                     | 0.86                       | 5.01                    | 2.66            | 0.353                    |                            |
| 95                                       | 52.1                    | 4.03            | 0.80                     | 0.79                       | 7.76                    | 2.88            | 0.415                    |                            |
| 100                                      | 65.1                    | 4.26            | 0.86                     | 0.71                       | 11.4                    | 3.08            | 0.476                    |                            |
| 105                                      | 79.9                    | 4.57            | 0.93                     | 0.59                       | 15.5                    | 3.24            | 0.530                    | 0.95                       |
| 110                                      | 88.3                    | 4.85            | 0.96                     | 0.50                       | 21.9                    | 3.43            | 0.597                    | 0.93                       |
| 115                                      | 94.4                    | 5.23            | 0.98                     | 0.40                       | 29.3                    | 3.62            | 0.664                    | 0.89                       |
| 120                                      |                         |                 |                          |                            | 38.1                    | 3.78            | 0.721                    | 0.86                       |
| 125                                      |                         |                 |                          |                            | 47.2                    | 3.94            | 0.775                    | 0.81                       |
| 130                                      |                         |                 |                          |                            | 58.0                    | 4.13            | 0.831                    | 0.75                       |
| 135                                      |                         |                 |                          |                            | 68.0                    | 4.32            | 0.877                    | 0.69                       |
| 140                                      |                         |                 |                          |                            | 77.6                    | 4.52            | 0.916                    | 0.61                       |
| 145                                      |                         |                 |                          |                            | 87.8                    | 4.83            | 0.955                    | 0.50                       |
| 150                                      |                         |                 |                          |                            | 94.6                    | 5.24            | 0.982                    | 0.38                       |

Table 3.

| Run<br>Temp<br>$\alpha_L$<br>Time<br>min | A21<br>545.5°K<br>0.006 |                 |                          |                            | A26<br>540.9<br>0.005 | A34<br>535.7<br>0.004 | A46<br>530.4°K<br>0.004 |
|--|-------------------------|-----------------|--------------------------|----------------------------|-----------------------|-----------------------|-------------------------|
|  | $\alpha \times 10^2$    | PT <sub>L</sub> | $\alpha_L^{\frac{1}{3}}$ | $(1-\alpha)^{\frac{1}{3}}$ | $\alpha \times 10^2$  | $\alpha \times 10^2$  | $\alpha \times 10^2$    |
| 10                                       | 0.15                    |                 |                          |                            | 0.07                  | 0.05                  | 0.02                    |
| 20                                       | 0.24                    |                 |                          |                            | 0.15                  | 0.10                  | 0.06                    |
| 30                                       | 0.32                    |                 |                          |                            | 0.18                  | 0.11                  | 0.09                    |
| 40                                       | 0.37                    |                 |                          |                            | 0.23                  | 0.14                  | 0.12                    |
| 50                                       | 0.42                    |                 |                          |                            | 0.26                  | 0.18                  | 0.15                    |
| 55                                       | 0.44                    |                 |                          |                            | 0.28                  | 0.21                  | 0.15                    |
| 60                                       | 0.47                    |                 |                          |                            | 0.30                  | 0.21                  | 0.16                    |
| 65                                       | 0.49                    |                 |                          |                            | 0.32                  | 0.22                  | 0.17                    |

Table 3 continued

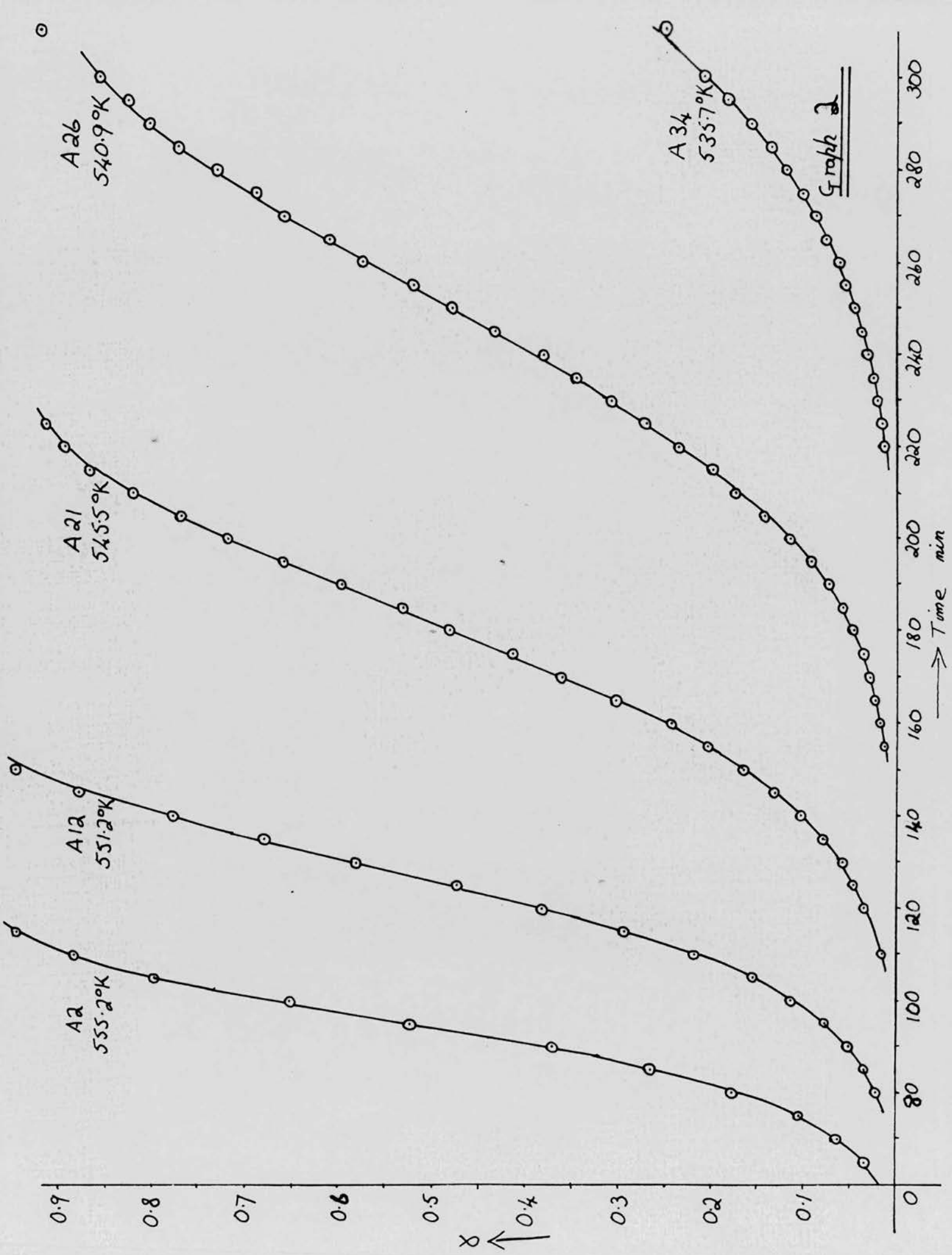
| Time<br>min | $\alpha \times 10^2$ | $PT_L$ | $A_{21}$<br>$\alpha_L^{\frac{1}{2}}$ | $(1 - \alpha)^{\frac{1}{2}}$ | $A_{26}$<br>$\alpha \times 10^2$ | $A_{34}$<br>$\alpha \times 10^2$ | $A_{46}$<br>$\alpha \times 10^2$ |
|-------------|----------------------|--------|--------------------------------------|------------------------------|----------------------------------|----------------------------------|----------------------------------|
| 70          | 0.52                 |        |                                      |                              | 0.33                             | 0.23                             | 0.18                             |
| 80          | 0.59                 |        |                                      |                              | 0.37                             | 0.25                             | 0.20                             |
| 90          | 0.68                 |        |                                      |                              | 0.40                             | 0.27                             | 0.21                             |
| 100         | 0.86                 |        |                                      |                              | 0.43                             | 0.30                             | 0.22                             |
| 110         | 1.53                 | 1.96   | 0.209                                |                              | 0.47                             | 0.32                             | 0.23                             |
| 120         | 3.46                 | 2.47   | 0.305                                |                              | 0.51                             | 0.34                             | 0.25                             |
| 125         | 4.70                 | 2.63   | 0.344                                |                              | 0.55                             | 0.36                             |                                  |
| 130         | 5.89                 | 2.75   | 0.375                                |                              | 0.59                             | 0.37                             | 0.26                             |
| 135         | 8.0                  | 2.88   | 0.423                                |                              | 0.64                             | 0.38                             |                                  |
| 140         | 10.4                 | 3.04   | 0.461                                |                              | 0.72                             | 0.40                             | 0.27                             |
| 145         | 13.1                 | 3.16   | 0.500                                |                              | 0.85                             | 0.42                             |                                  |
| 150         | 16.5                 | 3.26   | 0.542                                |                              | 0.97                             | 0.43                             | 0.28                             |
| 155         | 20.3                 | 3.38   | 0.580                                |                              | 1.29                             | 0.45                             |                                  |
| 160         | 24.2                 | 3.49   | 0.618                                |                              | 1.73                             | 0.48                             | 0.30                             |
| 165         | 30.4                 | 3.61   | 0.662                                |                              | 2.26                             | 0.51                             |                                  |
| 170         | 36.0                 | 3.72   | 0.703                                | 0.87                         | 2.94                             | 0.53                             | 0.31                             |
| 175         | 41.3                 | 3.84   | 0.741                                | 0.84                         | 3.57                             | 0.55                             |                                  |
| 180         | 47.9                 | 3.95   | 0.779                                | 0.81                         | 4.73                             | 0.59                             | 0.33                             |
| 185         | 52.9                 | 4.04   | 0.806                                | 0.79                         | 5.85                             | 0.62                             |                                  |
| 190         | 59.8                 | 4.17   | 0.840                                | 0.74                         | 7.30                             | 0.64                             | 0.34                             |
| 195         | 65.8                 | 4.28   | 0.870                                | 0.70                         | 9.2                              | 0.69                             |                                  |
| 200         | 71.8                 | 4.41   |                                      | 0.66                         | 11.5                             | 0.75                             | 0.35                             |
| 205         | 76.9                 | 4.52   |                                      | 0.62                         | 14.2                             | 0.81                             |                                  |
| 210         | 82.0                 | 4.66   |                                      | 0.56                         | 17.4                             | 0.93                             | 0.36                             |
| 215         | 85.7                 | 4.78   |                                      | 0.52                         | 19.8                             | 1.08                             |                                  |
| 220         | 89.2                 | 4.90   |                                      | 0.48                         | 23.5                             | 1.26                             | 0.38                             |
| 225         | 91.2                 | 5.02   |                                      | 0.43                         | 27.0                             | 1.66                             |                                  |
| 230         | 95.0                 | 5.28   |                                      | 0.37                         | 30.9                             | 2.10                             | 0.40                             |
| 235         |                      |        |                                      |                              | 34.5                             | 2.6                              | 0.41                             |
| 240         |                      |        |                                      |                              | 38.0                             | 3.1                              | 0.42                             |
| 245         |                      |        |                                      |                              | 43.2                             | 3.7                              | 0.43                             |
| 250         |                      |        |                                      |                              | 47.8                             | 4.6                              | 0.46                             |
| 255         |                      |        |                                      |                              | 52.0                             | 5.6                              | 0.47                             |
| 260         |                      |        |                                      |                              | 57.5                             | 6.1                              | 0.48                             |
| 265         |                      |        |                                      |                              | 61.0                             | 7.7                              | 0.50                             |
| 270         |                      |        |                                      |                              | 65.9                             | 8.8                              | 0.52                             |
| 275         |                      |        |                                      |                              | 68.9                             | 10.2                             | 0.55                             |
| 280         |                      |        |                                      |                              | 73.0                             | 12.0                             | 0.56                             |
| 285         |                      |        |                                      |                              | 77.2                             | 13.6                             | 0.58                             |
| 290         |                      |        |                                      |                              | 80.2                             | 15.8                             | 0.63                             |
| 295         |                      |        |                                      |                              | 82.6                             | 18.2                             | 0.67                             |
| 300         |                      |        |                                      |                              | 85.6                             | 20.9                             | 0.70                             |
| 310         |                      |        |                                      |                              | 92.2                             | 25.0                             | 0.83                             |
| 320         |                      |        |                                      |                              |                                  | 30.4                             | 1.00                             |
| 330         |                      |        |                                      |                              |                                  | 37.0                             | 1.20                             |
| 340         |                      |        |                                      |                              |                                  | 43.2                             | 1.70                             |

Table 4. Material B, aged material A.

| Run<br>Temp<br>$\alpha_L$<br>Time<br>min | B1<br>542.5°K<br>0.0055 |        |                            | B6<br>539.6°K<br>0.0042 |        |                                    |                            |
|--|-------------------------|--------|----------------------------|-------------------------|--------|------------------------------------|----------------------------|
|  | $\alpha \times 10^2$    | $PT_L$ | $(1-\alpha)^{\frac{1}{3}}$ | $\alpha \times 10^2$    | $PT_L$ | $\alpha_L^{\frac{1}{3}} \times 10$ | $(1-\alpha)^{\frac{1}{3}}$ |
| 5  | 0.04                    |        |                            | 0.01                    |        |                                    |                            |
| 10                                       | 0.06                    |        |                            | 0.04                    |        |                                    |                            |
| 15                                       | 0.10                    |        |                            | 0.07                    |        |                                    |                            |
| 20                                       | 0.11                    |        |                            | 0.11                    |        |                                    |                            |
| 25                                       | 0.14                    |        |                            | 0.13                    |        |                                    |                            |
| 30                                       | 0.17                    |        |                            | 0.15                    |        |                                    |                            |
| 35                                       | 0.19                    |        |                            | 0.17                    |        |                                    |                            |
| 40                                       | 0.23                    |        |                            | 0.18                    |        |                                    |                            |
| 45                                       | 0.26                    |        |                            | 0.20                    |        |                                    |                            |
| 50                                       | 0.29                    |        |                            | 0.23                    |        |                                    |                            |
| 55                                       | 0.32                    |        |                            | 0.25                    |        |                                    |                            |
| 60                                       | 0.34                    |        |                            | 0.26                    |        |                                    |                            |
| 65                                       | 0.37                    |        |                            | 0.29                    |        |                                    |                            |
| 70                                       | 0.40                    |        |                            | 0.31                    |        |                                    |                            |
| 75                                       | 0.43                    |        |                            | 0.33                    |        |                                    |                            |
| 80                                       | 0.45                    |        |                            | 0.35                    |        |                                    |                            |
| 85                                       | 0.47                    |        |                            | 0.36                    |        |                                    |                            |
| 90                                       | 0.52                    |        |                            | 0.38                    |        |                                    |                            |
| 95                                       | 0.59                    |        |                            | 0.40                    |        |                                    |                            |
| 100                                      | 0.67                    |        |                            | 0.42                    |        |                                    |                            |
| 105                                      | 0.77                    | 1.35   |                            | 0.44                    |        |                                    |                            |
| 110                                      | 0.98                    | 1.63   |                            | 0.47                    |        |                                    |                            |
| 115                                      | 1.61                    | 2.02   |                            | 0.52                    |        |                                    |                            |
| 120                                      | 3.47                    | 2.46   |                            | 0.58                    |        |                                    |                            |
| 125                                      | 9.1                     | 2.97   | 0.97                       | 0.72                    |        |                                    |                            |
| 130                                      | 17.5                    | 3.31   | 0.94                       | 0.91                    | 1.69   | 1.7                                |                            |
| 135                                      | 26.5                    | 3.54   | 0.90                       | 1.64                    | 2.09   | 2.30                               |                            |
| 140                                      | 36.3                    | 3.75   | 0.86                       | 3.07                    | 2.42   | 2.98                               |                            |
| 145                                      | 46.7                    | 3.93   | 0.81                       | 6.14                    | 2.78   | 3.85                               |                            |
| 150                                      | 55.0                    | 4.09   | 0.76                       | 11.2                    | 3.08   | 4.76                               | 0.96                       |
| 155                                      | 64.8                    | 4.26   | 0.71                       | 19.0                    | 3.36   | 5.71                               | 0.93                       |
| 160                                      | 70.8                    | 4.37   | 0.66                       | 26.7                    | 3.55   | 6.41                               | 0.90                       |
| 165                                      | 75.9                    | 4.49   | 0.62                       | 34.8                    | 3.72   | 7.01                               | 0.87                       |
| 170                                      | 81.0                    | 4.61   | 0.575                      | 43.0                    | 3.87   | 7.53                               | 0.83                       |
| 175                                      | 84.3                    | 4.71   | 0.54                       | 50.4                    | 4.00   |                                    | 0.79                       |
| 180                                      | 85.2                    | 4.74   | 0.53                       | 59.7                    | 4.17   |                                    | 0.74                       |
| 185                                      | 88.0                    | 4.85   | 0.49                       | 67.1                    | 4.30   |                                    | 0.69                       |
| 190                                      | 89.8                    | 4.94   | 0.47                       | 70.8                    | 4.38   |                                    | 0.66                       |
| 195                                      | 91.7                    | 5.04   | 0.44                       | 76.6                    | 4.51   |                                    | 0.62                       |
| 200                                      |                         |        |                            | 80.4                    | 4.61   |                                    | 0.58                       |
| 205                                      |                         |        |                            | 84.5                    | 4.73   |                                    | 0.54                       |
| 210                                      |                         |        |                            | 85.7                    | 4.77   |                                    | 0.52                       |
| 215                                      |                         |        |                            | 88.0                    | 4.83   |                                    | 0.49                       |
| 220                                      |                         |        |                            | 89.2                    |        |                                    | 0.48                       |
| 225                                      |                         |        |                            | 91.5                    |        |                                    | 0.44                       |

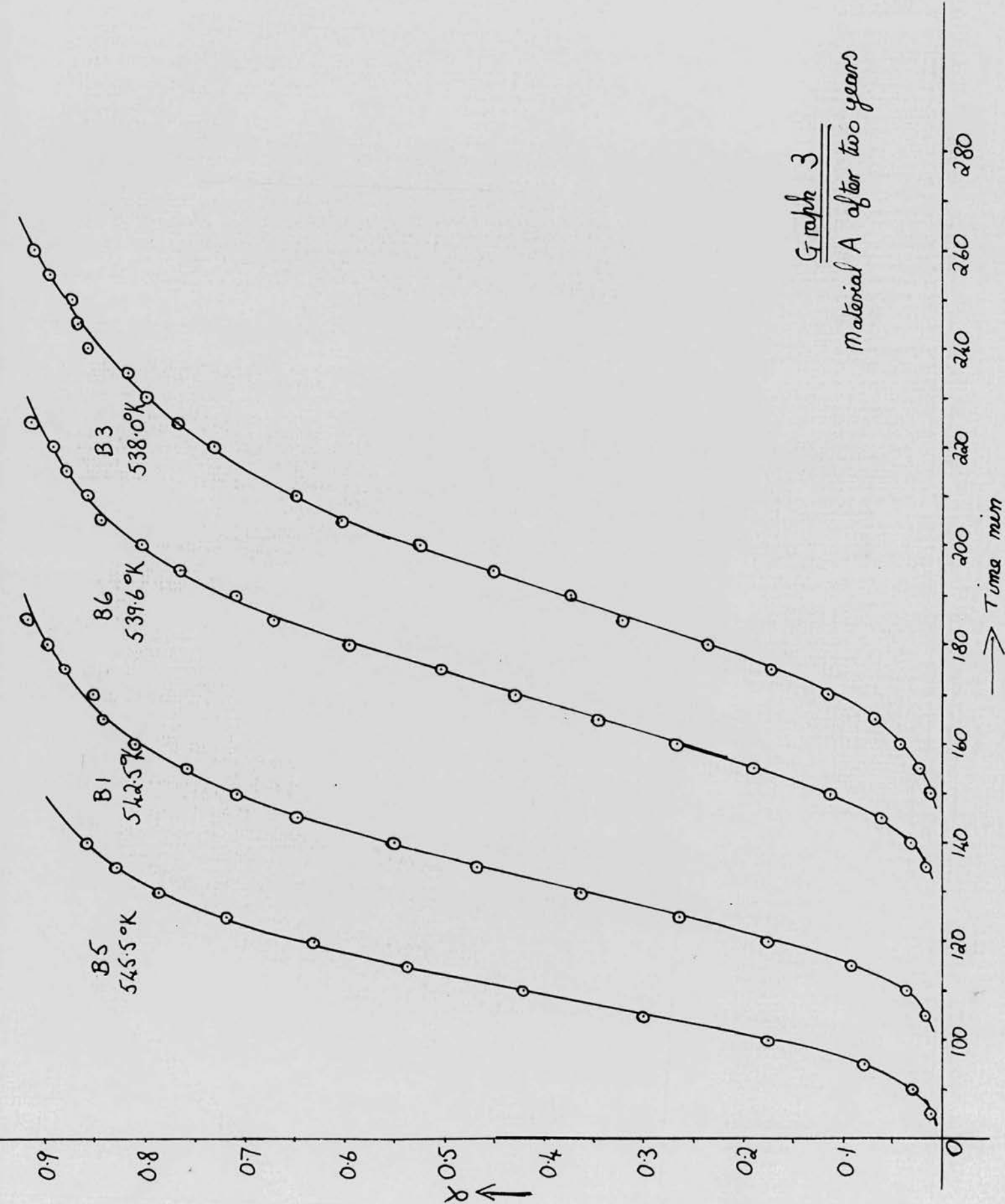






Graph 2

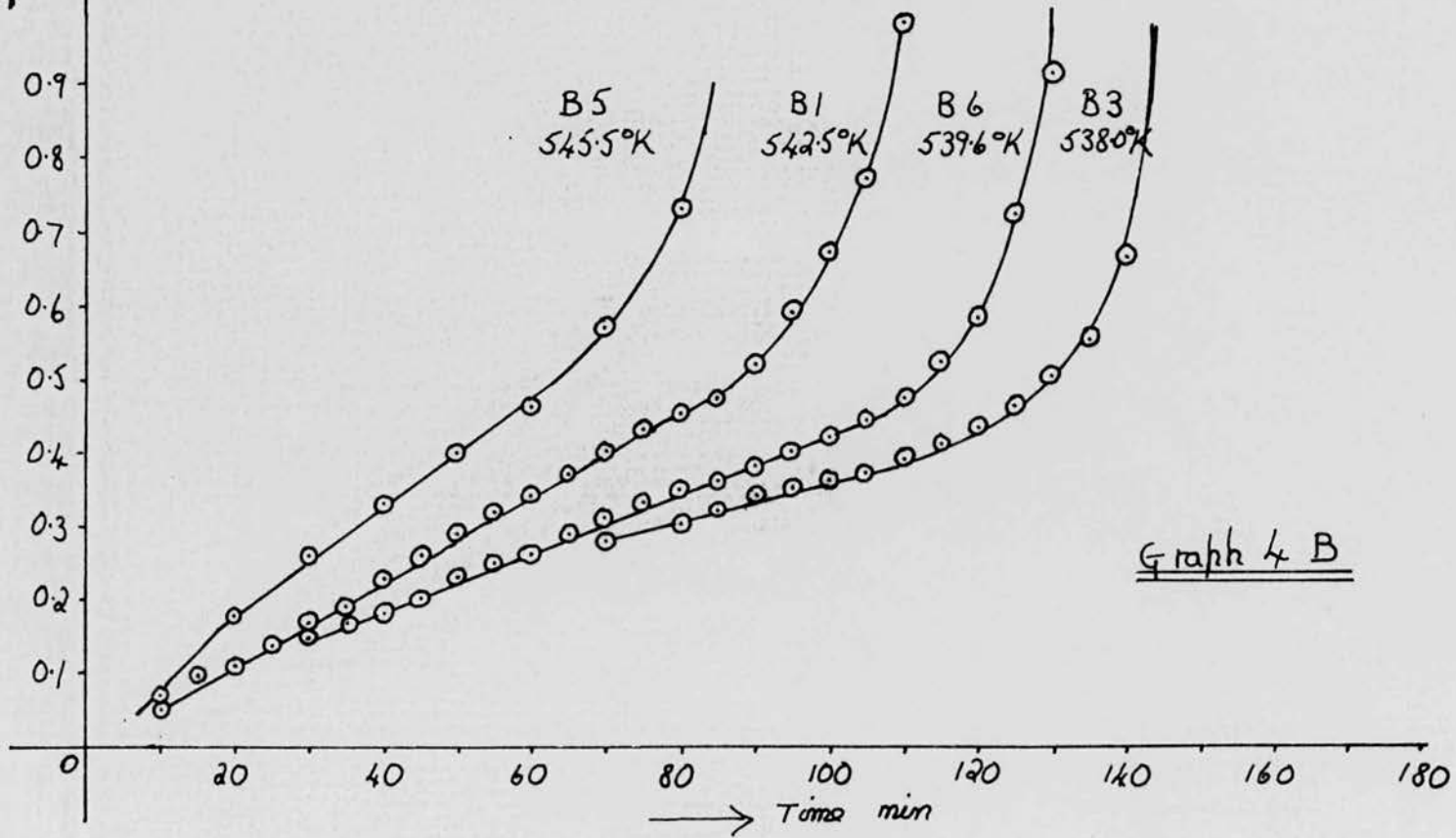
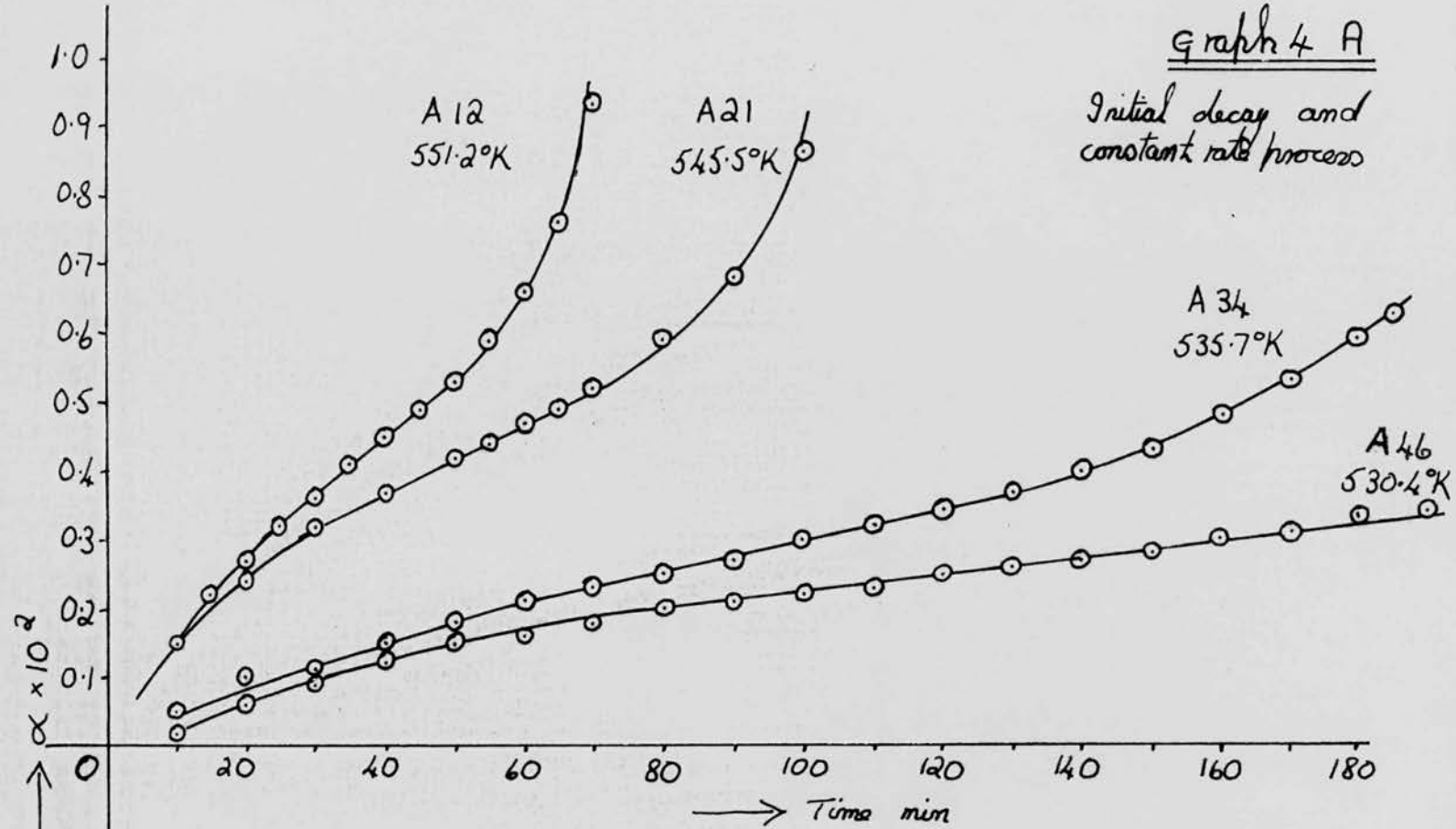
Graph 3  
Material A after two years



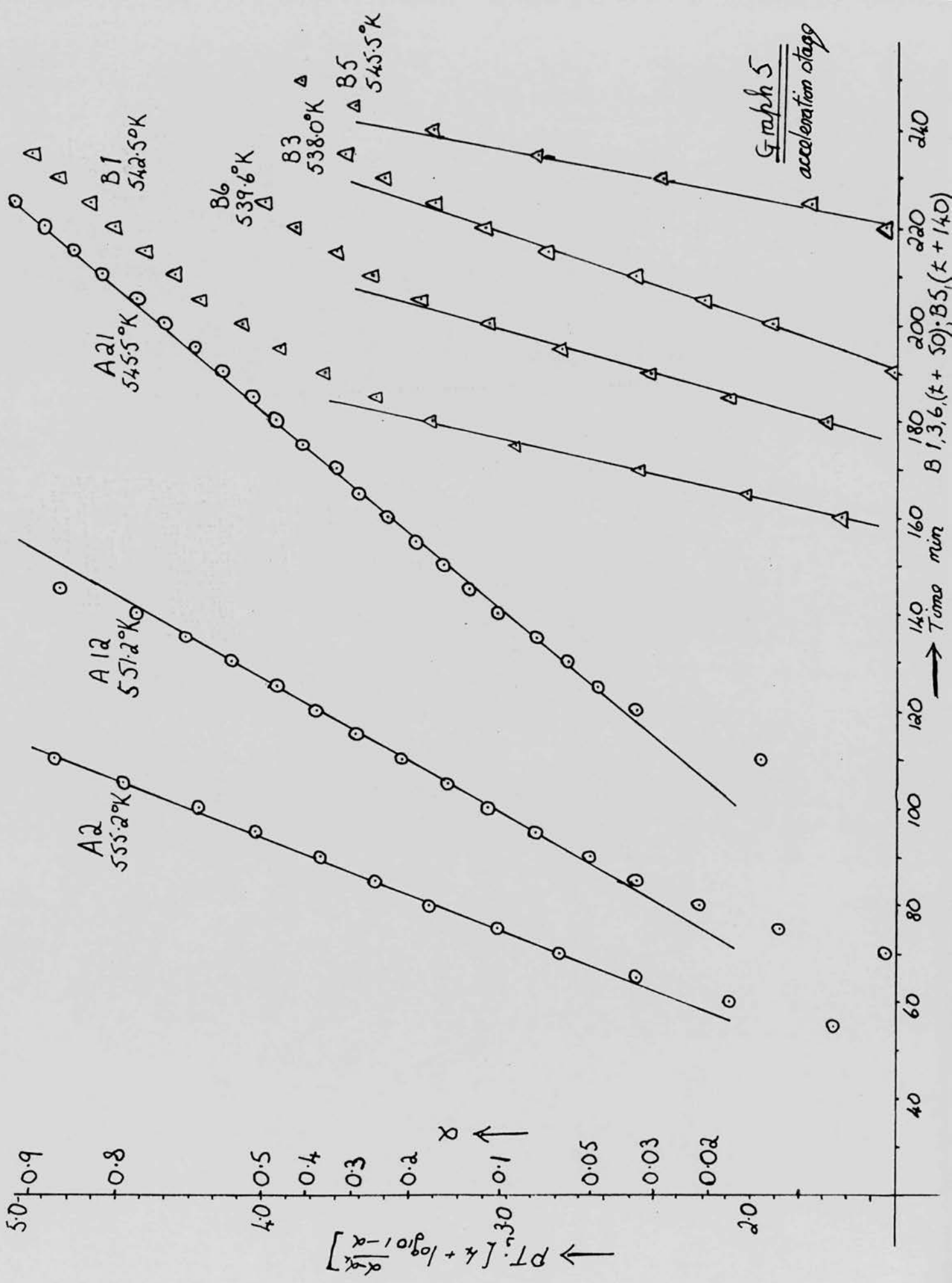


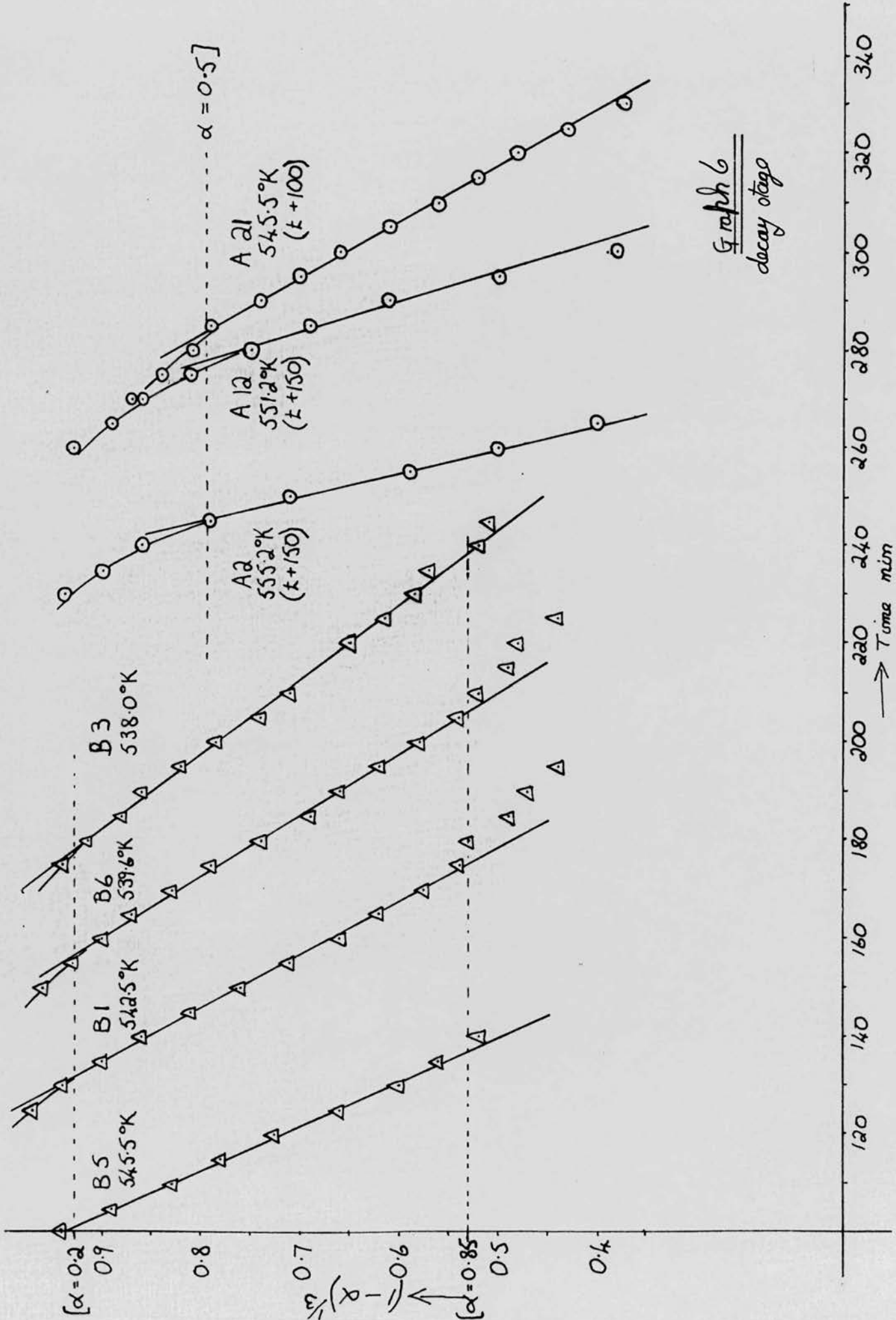
Graph 4 A

Initial decay and constant rate process



Graph 4 B





Graph 6  
decay stage



## 2. 6. 2. Kinetic results for large crystals C and D

Tables 6, 7, 8, 9 and 10 and graphs 7, 8, 9, 10, 11 and 12 illustrate the effect of 18.5 h. pre-irradiation with u.v. on the large crystals. Material C is fresh crystals, a preparation similar to A and material D is C after 18.5 h. pre-irradiation. The most notable feature is the overall increase in rate for all the stages. The decay stage begins at  $\alpha = 0.4$  compared with  $\alpha = 0.5$  for fresh material; and a power law growth has been introduced from  $\alpha = 0.005$  to  $\alpha = 0.04$ , which precedes the acceleration stage. Material C is similar to A, but with a much superior fit for the Prout-Tompkins equation at low  $\alpha$ 's.

Tables 6, 7 and 8, analysis of material C.

Tables 9 and 10, analysis of material D.

Graph 7, ' $\alpha$ ' - 't' curves for C and D.

Graph 8, linear stage, the ' $\alpha$ ' - 't' curves for material C and D showing the pre-acceleration stage of the decomposition.

Graph 9,  $\alpha^{\frac{1}{4}}/t$  for material D, showing the fit for the power law with  $n = 4$ .

Graph 10, acceleration stage, plot of Prout-Tompkins factor for material C.

Graph 11, acceleration stage, plot of Prout-Tompkins factor for material D. Note the positive deviation at low percentage decomposition due to the power law growth, which is not the case in the unirradiated material C.

Graph 12, decay stage, plot of contracting sphere factor for C and D.

Table 6. Material C. Large fresh crystals.

| Run         | C2                   |        |                          |                              | C4                   |                              |
|-------------|----------------------|--------|--------------------------|------------------------------|----------------------|------------------------------|
| Temp        | 553.8°K              |        |                          |                              | 549.8°K              |                              |
| $\alpha_L$  | 0.0051               |        |                          |                              | 0.007                |                              |
| Time<br>min | $\alpha \times 10^2$ | $PT_L$ | $\alpha_L^{\frac{1}{3}}$ | $(1 - \alpha)^{\frac{1}{3}}$ | $\alpha \times 10^2$ | $(1 - \alpha)^{\frac{1}{3}}$ |
| 5           | 0.04                 |        |                          |                              | 0.10                 |                              |
| 10          | 0.14                 |        |                          |                              | 0.20                 |                              |
| 15          | 0.24                 |        |                          |                              | 0.26                 |                              |
| 20          | 0.30                 |        |                          |                              | 0.31                 |                              |
| 25          | 0.35                 |        |                          |                              | 0.36                 |                              |
| 30          | 0.38                 |        |                          |                              | 0.44                 |                              |
| 35          | 0.42                 |        |                          |                              | 0.48                 |                              |
| 40          | 0.45                 |        |                          |                              | 0.53                 |                              |
| 45          | 0.48                 |        |                          |                              | 0.59                 |                              |
| 50          | 0.51                 |        |                          |                              | 0.66                 |                              |
| 55          | 0.56                 |        |                          |                              | 0.73                 |                              |
| 60          | 0.66                 | 1.18   | 0.114                    |                              | 0.77                 |                              |
| 65          | 0.87                 | 1.56   | 0.153                    |                              | 0.86                 |                              |
| 70          | 1.14                 | 1.80   | 0.185                    |                              | 0.97                 |                              |
| 75          | 1.72                 | 2.08   | 0.230                    |                              | 1.06                 |                              |
| 80          | 2.73                 | 2.36   | 0.281                    |                              | 1.24                 |                              |
| 85          | 5.64                 | 2.73   | 0.372                    |                              | 1.44                 |                              |
| 90          | 10.6                 | 3.05   | 0.466                    |                              | 1.87                 |                              |
| 95          | 20.1                 | 3.39   | 0.581                    | 0.923                        | 2.25                 |                              |
| 100         | 32.7                 | 3.68   | 0.686                    | 0.88                         | 2.61                 |                              |
| 105         | 50.6                 | 4.00   | 0.797                    | 0.79                         | 3.51                 |                              |
| 110         | 62.4                 | 4.21   | 0.851                    | 0.73                         | 4.88                 |                              |
| 115         | 77.1                 | 4.51   |                          | 0.62                         | 6.83                 |                              |
| 120         | 86.7                 | 4.80   |                          | 0.51                         | 10.3                 |                              |
| 125         | 93.0                 | 5.12   |                          | 0.41                         | 15.4                 |                              |
| 130         |                      |        |                          |                              | 22.9                 | 0.92                         |
| 135         |                      |        |                          |                              | 32.1                 | 0.88                         |
| 140         |                      |        |                          |                              | 42.6                 | 0.83                         |
| 145         |                      |        |                          |                              | 52.9                 | 0.78                         |
| 150         |                      |        |                          |                              | 65.0                 | 0.71                         |
| 155         |                      |        |                          |                              | 73.5                 | 0.65                         |
| 160         |                      |        |                          |                              | 81.0                 | 0.57                         |
| 165         |                      |        |                          |                              | 88.9                 | 0.48                         |
| 170         |                      |        |                          |                              | 94.5                 | 0.39                         |





Table 8. Material C. Large fresh crystals.

| Run        | C1                   | C9                   |                 | C10                  |                 |                              |
|------------|----------------------|----------------------|-----------------|----------------------|-----------------|------------------------------|
| Temp       | 544.2°K              | 540.5°K              |                 | 542.1°K              |                 |                              |
| $\alpha_L$ | 0.006                | 0.0056               |                 | 0.005                |                 |                              |
| Time       | $\alpha \times 10^2$ | $\alpha \times 10^2$ | PT <sub>L</sub> | $\alpha \times 10^2$ | PT <sub>L</sub> | $(1 - \alpha)^{\frac{1}{3}}$ |
| min        |                      |                      |                 |                      |                 |                              |
| 10         | 0.05                 | 0.04                 |                 | 0.06                 |                 |                              |
| 20         | 0.19                 | 0.15                 |                 | 0.13                 |                 |                              |
| 30         | 0.27                 | 0.25                 |                 | 0.19                 |                 |                              |
| 40         | 0.34                 | 0.30                 |                 | 0.24                 |                 |                              |
| 50         | 0.39                 | 0.33                 |                 | 0.30                 |                 |                              |
| 60         | 0.42                 | 0.36                 |                 | 0.33                 |                 |                              |
| 70         | 0.47                 | 0.40                 |                 | 0.36                 |                 |                              |
| 80         | 0.51                 | 0.43                 |                 | 0.40                 |                 |                              |
| 90         | 0.56                 | 0.46                 |                 | 0.42                 |                 |                              |
| 100        | 0.62                 | 0.50                 |                 | 0.47                 |                 |                              |
| 105        | 0.67                 | 0.51                 |                 | 0.49                 |                 |                              |
| 110        | 0.71                 | 0.54                 |                 | 0.50                 |                 |                              |
| 115        | 0.80                 | 0.55                 |                 | 0.54                 |                 |                              |
| 120        | 0.91                 | 0.57                 |                 | 0.57                 |                 |                              |
| 125        | 1.03                 | 0.58                 |                 | 0.60                 |                 |                              |
| 130        | 1.23                 | 0.61                 |                 | 0.64                 |                 |                              |
| 135        | 1.50                 | 0.64                 |                 | 0.70                 |                 |                              |
| 140        | 1.75                 | 0.68                 |                 | 0.77                 | 1.43            |                              |
| 145        | 2.09                 | 0.74                 |                 | 0.88                 | 1.58            |                              |
| 150        | 2.37                 | 0.80                 | 1.35            | 1.01                 | 1.71            |                              |
| 155        | 3.59                 | 0.90                 | 1.54            | 1.16                 | 1.82            |                              |
| 160        | 4.44                 | 1.00                 | 1.64            | 1.36                 | 1.93            |                              |
| 165        | 5.86                 | 1.08                 | 1.72            | 1.60                 | 2.04            |                              |
| 170        | 7.9                  | 1.20                 | 1.81            | 1.90                 | 2.15            |                              |
| 175        | 10.5                 | 1.37                 | 1.91            | 2.28                 | 2.25            |                              |
| 180        | 14.1                 | 1.53                 | 1.99            | 2.60                 | 2.32            |                              |
| 185        | 18.3                 | 1.68                 | 2.05            | 3.47                 | 2.47            |                              |
| 190        | 23.2                 | 2.44                 | 2.27            | 4.30                 | 2.60            |                              |
| 195        | 28.3                 | 2.63                 | 2.32            | 5.60                 | 2.74            |                              |
| 200        | 35.9                 | 3.08                 | 2.40            | 7.74                 | 2.89            |                              |
| 205        | 42.9                 | 3.63                 | 2.49            | 10.4                 | 3.04            |                              |
| 210        | 48.5                 | 4.52                 | 2.60            | 12.4                 | 3.14            |                              |
| 215        | 55.6                 | 5.56                 | 2.71            | 16.6                 | 3.28            |                              |
| 220        | 63.2                 | 6.95                 | 2.83            | 20.3                 | 3.40            |                              |
| 225        | 69.2                 | 8.6                  | 2.93            | 24.9                 | 3.51            |                              |
| 230        | 74.3                 | 10.9                 | 3.06            | 29.6                 | 3.61            |                              |
| 235        | 80.8                 | 13.6                 | 3.17            | 35.1                 | 3.72            | 0.868                        |
| 240        | 87.0                 | 16.5                 | 3.28            | 40.3                 | 3.82            | 0.848                        |
| 245        | 88.9                 | 19.9                 | 3.38            | 47.4                 | 3.95            | 0.810                        |
| 250        | 93.5                 | 23.7                 | 3.48            | 53.7                 | 4.06            | 0.776                        |
| 260        |                      | 33.0                 | 3.68            | 63.5                 | 4.23            | 0.718                        |
| 270        |                      | 42.6                 | 3.86            | 74.2                 | 4.45            | 0.641                        |
| 280        |                      | 52.3                 | 4.03            | 82.8                 | 4.67            | 0.561                        |
| 290        |                      | 62.0                 | 4.21            | 89.5                 | 4.92            | 0.472                        |
| 300        |                      |                      |                 | 93.3                 | 5.14            | 0.406                        |

Table 9. Material D. Fresh large pre-irradiated crystals.

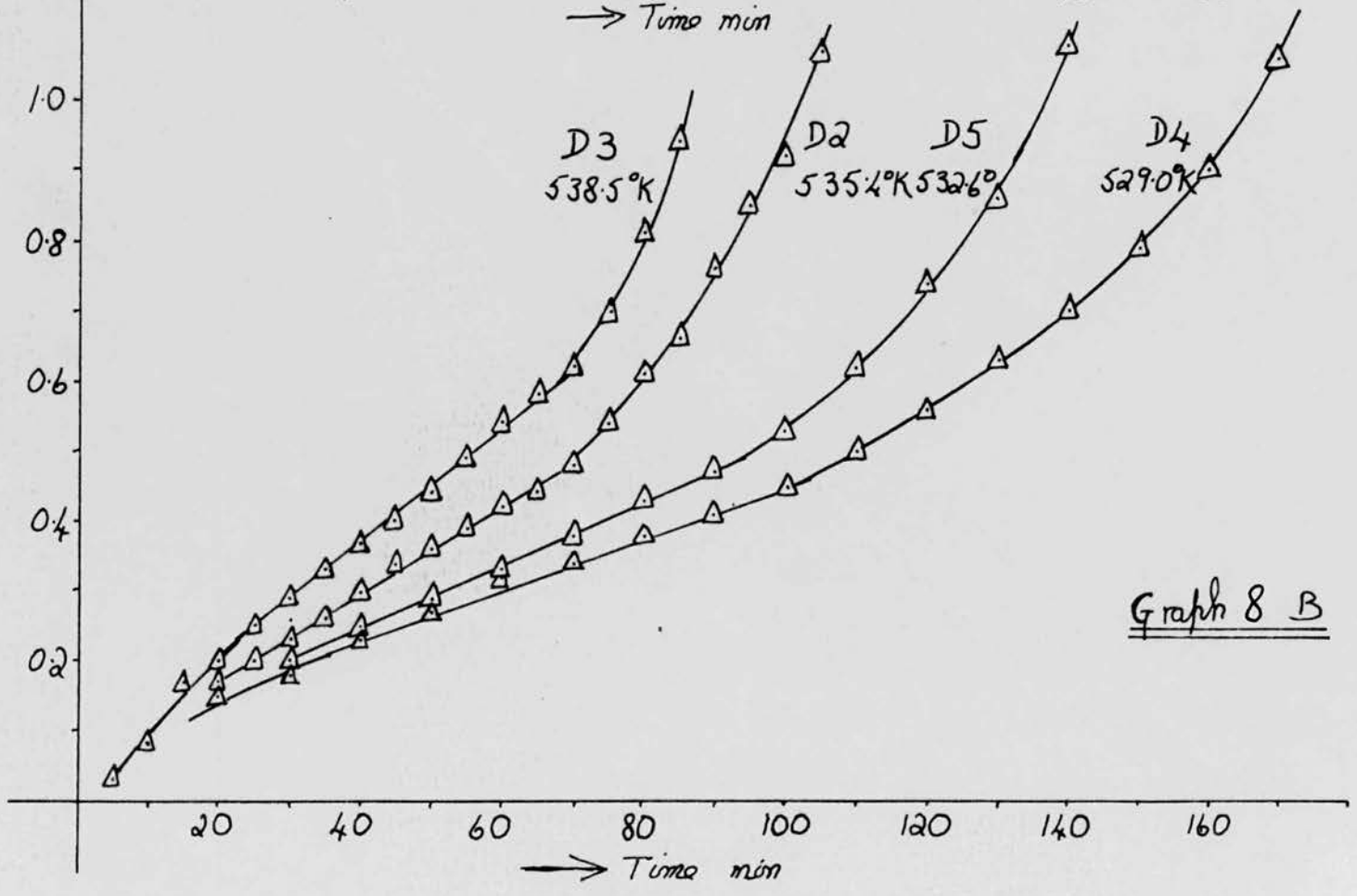
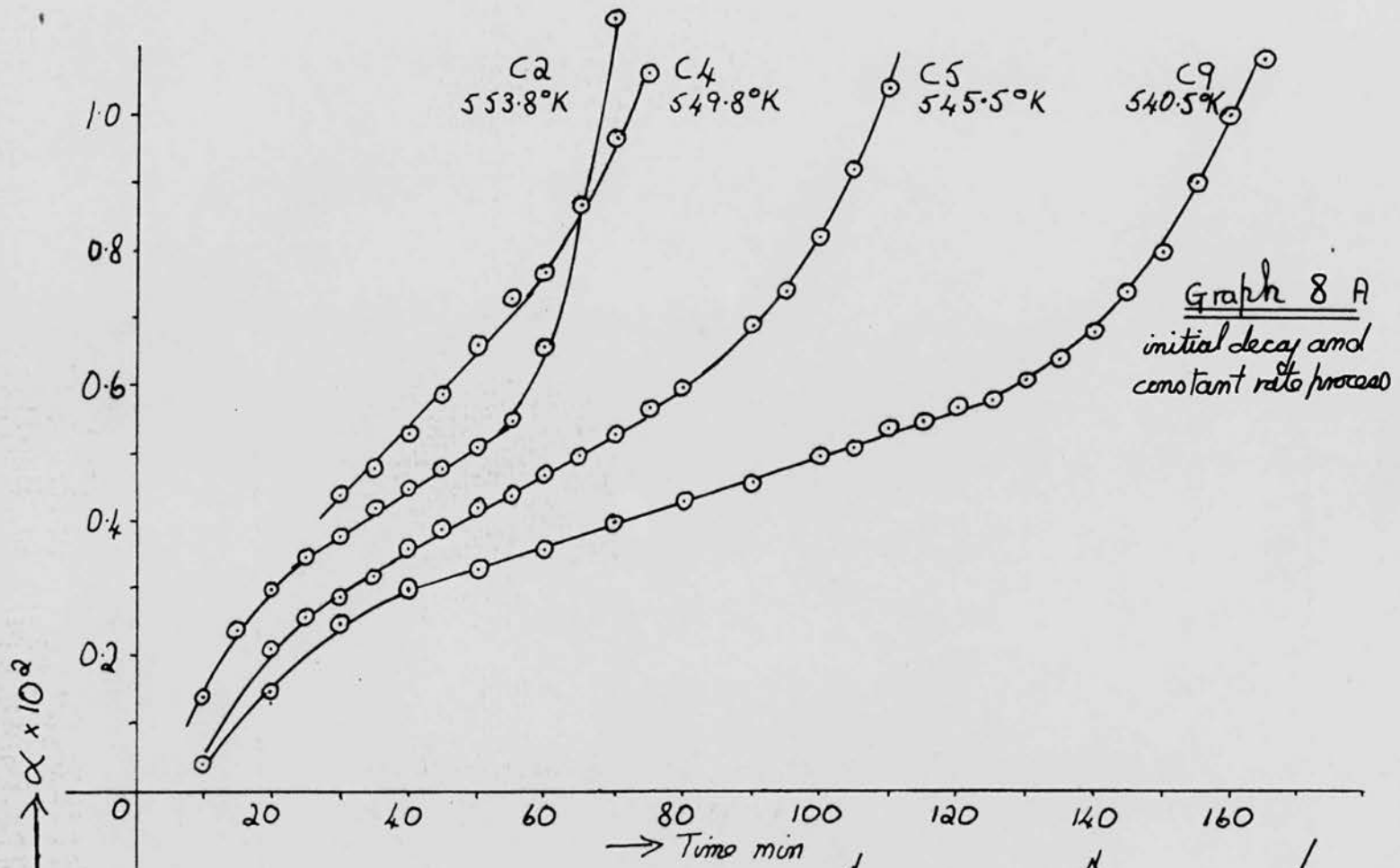
| Run         | D3<br>538.5°K<br>$\alpha_L$ 0.006 |                      | D2<br>535.4°K<br>0.0045 |                                    |                      | D1<br>541.8°K<br>0.0052 |                                    |                                    |
|-------------|-----------------------------------|----------------------|-------------------------|------------------------------------|----------------------|-------------------------|------------------------------------|------------------------------------|
| Time<br>min | $\alpha \times 10^2$              | $\alpha \times 10^2$ | $PT_L$                  | $\alpha_L^{\frac{1}{4}} \times 10$ | $\alpha \times 10^2$ | $PT_L$                  | $\alpha_L^{\frac{1}{4}} \times 10$ | $\alpha_p^{\frac{1}{3}} \times 10$ |
| 5           | 0.03                              | 0.03                 |                         |                                    | 0.04                 |                         |                                    |                                    |
| 10          | 0.08                              | 0.08                 |                         |                                    | 0.11                 |                         |                                    |                                    |
| 15          | 0.17                              | 0.16                 |                         |                                    | 0.19                 |                         |                                    |                                    |
| 20          | 0.20                              | 0.17                 |                         |                                    | 0.26                 |                         |                                    |                                    |
| 25          | 0.25                              | 0.20                 |                         |                                    | 0.30                 |                         |                                    |                                    |
| 30          | 0.29                              | 0.23                 |                         |                                    | 0.36                 |                         |                                    |                                    |
| 35          | 0.33                              | 0.26                 |                         |                                    | 0.40                 |                         |                                    |                                    |
| 40          | 0.37                              | 0.30                 |                         |                                    | 0.47                 |                         |                                    |                                    |
| 45          | 0.40                              | 0.34                 |                         |                                    | 0.52                 |                         |                                    |                                    |
| 50          | 0.44                              | 0.36                 |                         |                                    | 0.59                 |                         |                                    |                                    |
| 55          | 0.49                              | 0.39                 |                         |                                    | 0.63                 |                         |                                    |                                    |
| 60          | 0.54                              | 0.42                 |                         |                                    | 0.75                 |                         | 2.2                                |                                    |
| 65          | 0.58                              | 0.44                 |                         |                                    | 0.92                 |                         |                                    |                                    |
| 70          | 0.62                              | 0.48                 |                         |                                    | 1.14                 | 1.79                    | 2.8                                |                                    |
| 75          | 0.70                              | 0.54                 |                         |                                    | 1.37                 | 1.93                    | 3.0                                |                                    |
| 80          | 0.81                              | 0.61                 |                         | 2.0                                | 1.68                 | 2.06                    | 3.3                                |                                    |
| 85          | 0.94                              | 0.66                 |                         |                                    | 2.15                 | 2.21                    | 3.6                                |                                    |
| 90          | 1.09                              | 0.76                 |                         | 2.4                                | 2.77                 | 2.35                    | 3.9                                |                                    |
| 95          | 1.24                              | 0.85                 |                         |                                    | 3.65                 | 2.49                    | 4.2                                |                                    |
| 100         | 1.51                              | 0.92                 |                         | 2.6                                | 5.87                 | 2.75                    | 4.8                                | 2.9                                |
| 105         | 1.77                              | 1.07                 |                         |                                    | 10.0                 | 3.03                    | 5.6                                | 4.0                                |
| 110         | 2.17                              | 1.24                 |                         | 3.0                                | 18.6                 | 3.34                    | $(1-)^{\frac{1}{3}}$               | 5.3                                |
| 115         | 2.60                              | 1.43                 |                         |                                    | 31.1                 | 3.64                    | 0.88                               | 6.5                                |
| 120         | 3.26                              | 1.66                 |                         | 3.3                                | 43.2                 | 3.87                    | 0.83                               | 7.35                               |
| 125         | 4.61                              | 1.98                 | 2.18                    |                                    | 56.0                 | 4.10                    | 0.76                               | 8.1                                |
| 130         | 7.9                               | 2.30                 | 2.27                    | 3.7                                | 69.5                 | 4.35                    | 0.67                               |                                    |
| 135         | 10.5                              | 2.72                 | 2.36                    |                                    | 77.7                 | 4.53                    | 0.61                               |                                    |
| 140         | 17.2                              | 3.23                 | 2.44                    | 4.1                                | 83.5                 | 4.69                    | 0.55                               |                                    |
| 145         | 25.8                              | 4.52                 | 2.63                    |                                    | 87.5                 | 4.82                    | 0.50                               |                                    |
| 150         | 36.9                              | 5.46                 | 2.73                    | 4.7                                |                      |                         |                                    |                                    |
| 155         | 46.7                              | 6.83                 | 2.83                    | 5.0                                |                      |                         |                                    |                                    |
| 160         | 55.6                              | 9.45                 | 2.99                    |                                    |                      |                         |                                    |                                    |
| 165         | 65.1                              | 14.2                 | 3.20                    |                                    |                      |                         |                                    |                                    |
| 170         | 73.0                              | 19.7                 | 3.38                    | $(1-)^{\frac{1}{3}}$               |                      |                         |                                    |                                    |
| 175         | 78.0                              | 26.9                 | 3.56                    | 0.90                               |                      |                         |                                    |                                    |
| 180         | 82.3                              | 35.0                 | 3.74                    | 0.87                               |                      |                         |                                    |                                    |
| 185         | 85.1                              | 44.1                 | 3.89                    | 0.82                               |                      |                         |                                    |                                    |
| 190         | 86.5                              | 52.0                 | 4.04                    | 0.77                               |                      |                         |                                    |                                    |
| 195         | 89.4                              | 59.9                 | 4.17                    | 0.74                               |                      |                         |                                    |                                    |
| 200         | 91.5                              | 67.2                 | 4.30                    | 0.69                               |                      |                         |                                    |                                    |
| 205         |                                   | 73.6                 | 4.43                    | 0.64                               |                      |                         |                                    |                                    |
| 210         |                                   | 77.2                 | 4.54                    | 0.61                               |                      |                         |                                    |                                    |
| 215         |                                   | 81.4                 | 4.63                    | 0.57                               |                      |                         |                                    |                                    |

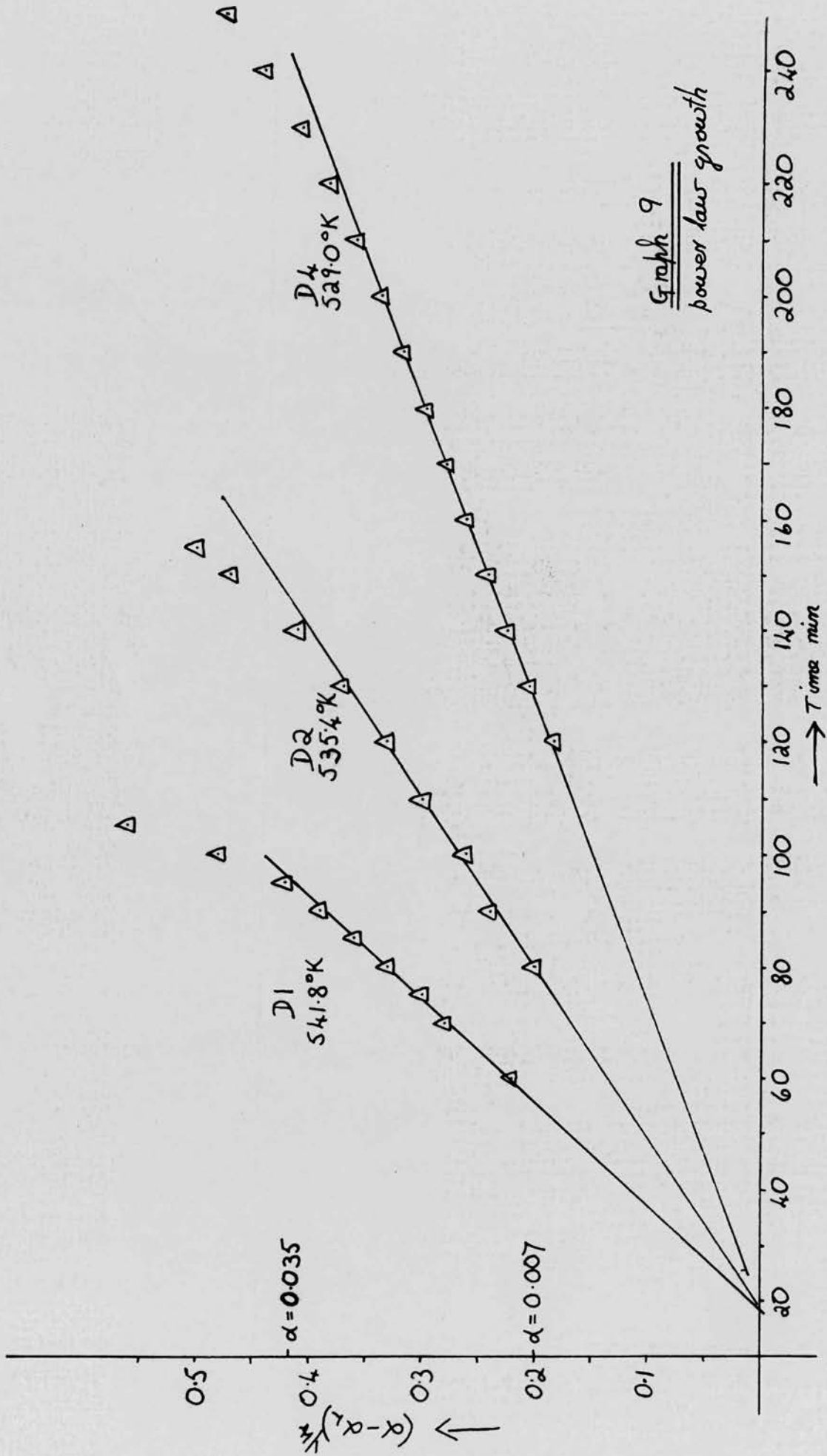
Table 10. Material D. Fresh large pre-irradiated crystals.

| Run         | D6<br>531.0°K<br>$\alpha_L$ 0.0055 |                      | D4<br>529.0°K<br>0.0045 |                                    |                                    | D5<br>532.6<br>0.005 |        |                            |  |
|-------------|------------------------------------|----------------------|-------------------------|------------------------------------|------------------------------------|----------------------|--------|----------------------------|--|
| Time<br>min | $\alpha \times 10^2$               | $\alpha \times 10^2$ | $PT_L$                  | $\alpha_L^{\frac{1}{4}} \times 10$ | $\alpha_P^{\frac{1}{3}} \times 10$ | $\alpha \times 10^2$ | $PT_L$ | $(1-\alpha)^{\frac{1}{3}}$ |  |
| 10          | 0.06                               | 0.09                 |                         |                                    |                                    | 0.08                 |        |                            |  |
| 20          | 0.13                               | 0.15                 |                         |                                    |                                    | 0.18                 |        |                            |  |
| 30          | 0.16                               | 0.18                 |                         |                                    |                                    | 0.20                 |        |                            |  |
| 40          | 0.20                               | 0.23                 |                         |                                    |                                    | 0.25                 |        |                            |  |
| 50          | 0.24                               | 0.27                 |                         |                                    |                                    | 0.29                 |        |                            |  |
| 60          | 0.28                               | 0.32                 |                         |                                    |                                    | 0.33                 |        |                            |  |
| 70          | 0.33                               | 0.34                 |                         |                                    |                                    | 0.38                 |        |                            |  |
| 80          | 0.37                               | 0.38                 |                         |                                    |                                    | 0.43                 |        |                            |  |
| 90          | 0.42                               | 0.41                 |                         |                                    |                                    | 0.47                 |        |                            |  |
| 100         | 0.45                               | 0.45                 |                         |                                    |                                    | 0.53                 |        |                            |  |
| 110         | 0.50                               | 0.50                 |                         |                                    |                                    | 0.62                 |        |                            |  |
| 120         | 0.55                               | 0.56                 |                         | 1.83                               |                                    | 0.74                 |        |                            |  |
| 130         | 0.63                               | 0.63                 |                         | 2.05                               |                                    | 0.86                 |        |                            |  |
| 140         | 0.74                               | 0.70                 |                         | 2.25                               |                                    | 1.08                 |        |                            |  |
| 150         | 0.86                               | 0.79                 |                         | 2.41                               |                                    | 1.30                 |        |                            |  |
| 160         | 1.02                               | 0.90                 |                         | 2.61                               |                                    | 1.68                 |        |                            |  |
| 170         | 1.26                               | 1.06                 |                         | 2.79                               |                                    | 2.20                 |        |                            |  |
| 180         | 1.53                               | 1.24                 |                         | 2.98                               |                                    | 3.07                 |        |                            |  |
| 190         | 1.96                               | 1.47                 |                         | 3.18                               |                                    | 4.00                 | 2.58   |                            |  |
| 200         | 2.80                               | 1.74                 |                         | 3.38                               |                                    | 5.85                 | 2.73   |                            |  |
| 205         | 3.04                               | 1.93                 |                         |                                    |                                    | 7.16                 | 2.85   |                            |  |
| 210         | 3.48                               | 2.12                 |                         | 3.59                               |                                    | 8.65                 | 2.95   |                            |  |
| 215         | 3.78                               | 2.36                 |                         |                                    |                                    | 13.5                 | 3.17   |                            |  |
| 220         | 4.32                               | 2.57                 |                         | 3.82                               |                                    | 18.0                 | 3.33   |                            |  |
| 225         | 5.13                               | 2.94                 |                         |                                    |                                    | 23.6                 | 3.48   |                            |  |
| 230         | 6.28                               | 3.22                 |                         | 4.07                               |                                    | 30.3                 | 3.63   | 0.89                       |  |
| 235         | 8.0                                | 3.66                 |                         |                                    |                                    | 36.0                 | 3.75   | 0.86                       |  |
| 240         | 10.4                               | 4.22                 | 2.59                    | 4.40                               |                                    | 43.0                 | 3.87   | 0.83                       |  |
| 245         | 14.0                               | 4.83                 | 2.65                    |                                    | 2.40                               | 49.7                 | 3.99   | 0.795                      |  |
| 250         | 17.7                               | 5.51                 | 2.73                    | 4.74                               | 2.71                               | 55.4                 | 4.09   | 0.76                       |  |
| 255         | 23.0                               | 6.67                 | 2.82                    |                                    | 3.18                               | 62.0                 | 4.21   | 0.724                      |  |
| 260         | 28.4                               | 8.4                  | 2.94                    |                                    | 3.67                               | 66.2                 | 4.29   | 0.70                       |  |
| 265         | 34.1                               | 9.9                  | 3.01                    |                                    | 4.02                               | 71.5                 | 4.39   | 0.66                       |  |
| 270         | 39.7                               | 12.6                 | 3.14                    |                                    | 4.51                               | 75.5                 | 4.49   | 0.63                       |  |
| 275         | 45.0                               | 15.6                 | 3.25                    | $(1-\alpha)^{\frac{1}{3}}$         | 4.96                               | 78.6                 | 4.56   | 0.60                       |  |
| 280         | 51.1                               | 18.8                 | 3.35                    |                                    | 5.36                               | 81.4                 | 4.64   | 0.57                       |  |
| 285         | 55.8                               | 23.6                 | 3.48                    | 0.914                              | 5.88                               | 84.1                 | 4.72   | 0.54                       |  |
| 290         | 62.1                               | 27.5                 | 3.56                    | 0.90                               | 6.28                               |                      |        |                            |  |
| 300         | 71.0                               | 37.0                 | 3.76                    | 0.855                              | 6.94                               |                      |        |                            |  |
| 310         | 77.7                               | 47.3                 | 3.95                    | 0.81                               | 7.60                               |                      |        |                            |  |
| 320         | 84.0                               | 58.1                 | 4.13                    | 0.75                               |                                    |                      |        |                            |  |
| 330         | 88.0                               | 65.9                 | 4.28                    | 0.70                               |                                    |                      |        |                            |  |
| 340         | 91.0                               | 74.3                 | 4.44                    | 0.64                               |                                    |                      |        |                            |  |
| 350         |                                    | 79.1                 | 4.58                    | 0.59                               |                                    |                      |        |                            |  |
| 360         |                                    | 84.5                 | 4.66                    | 0.54                               |                                    |                      |        |                            |  |



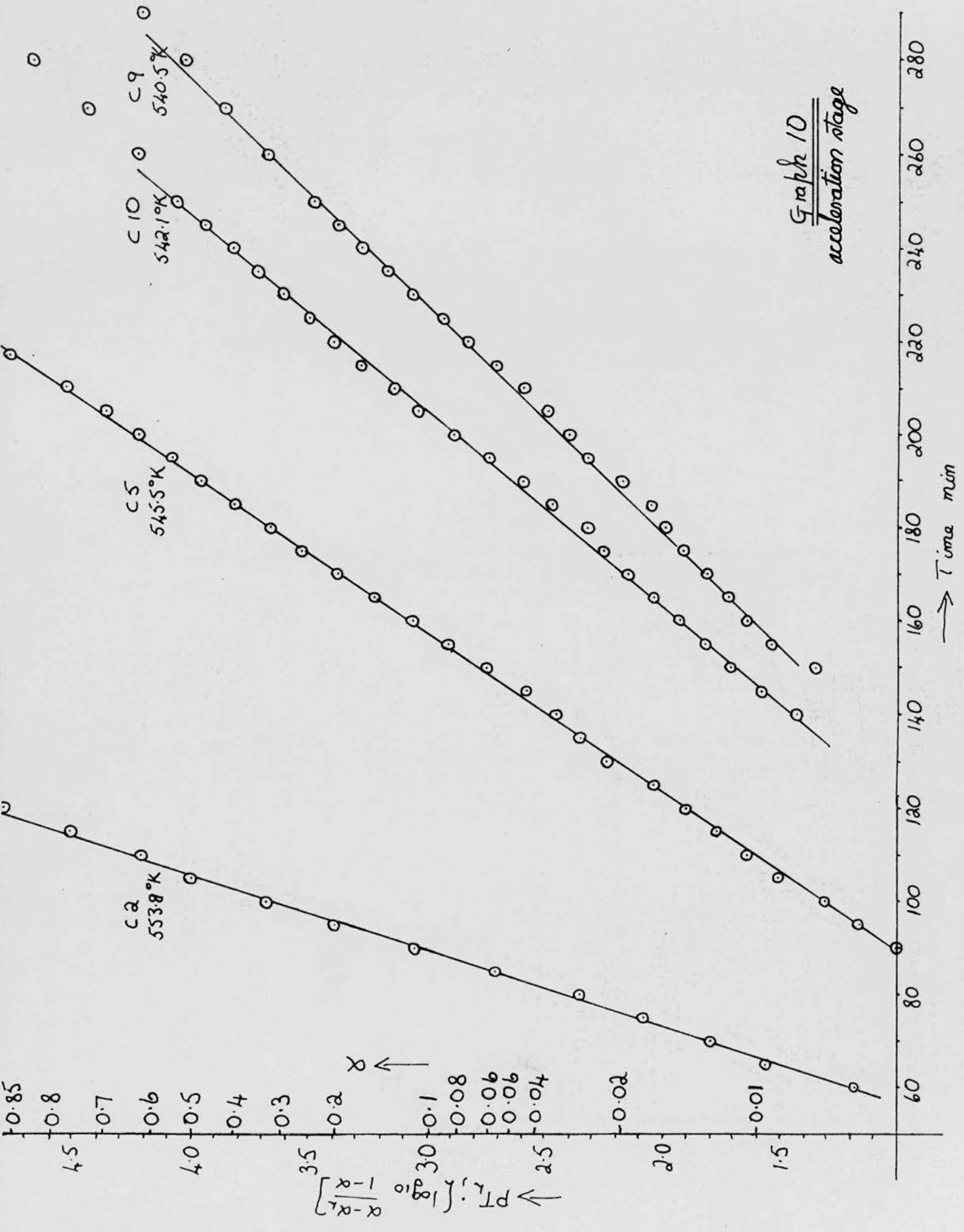




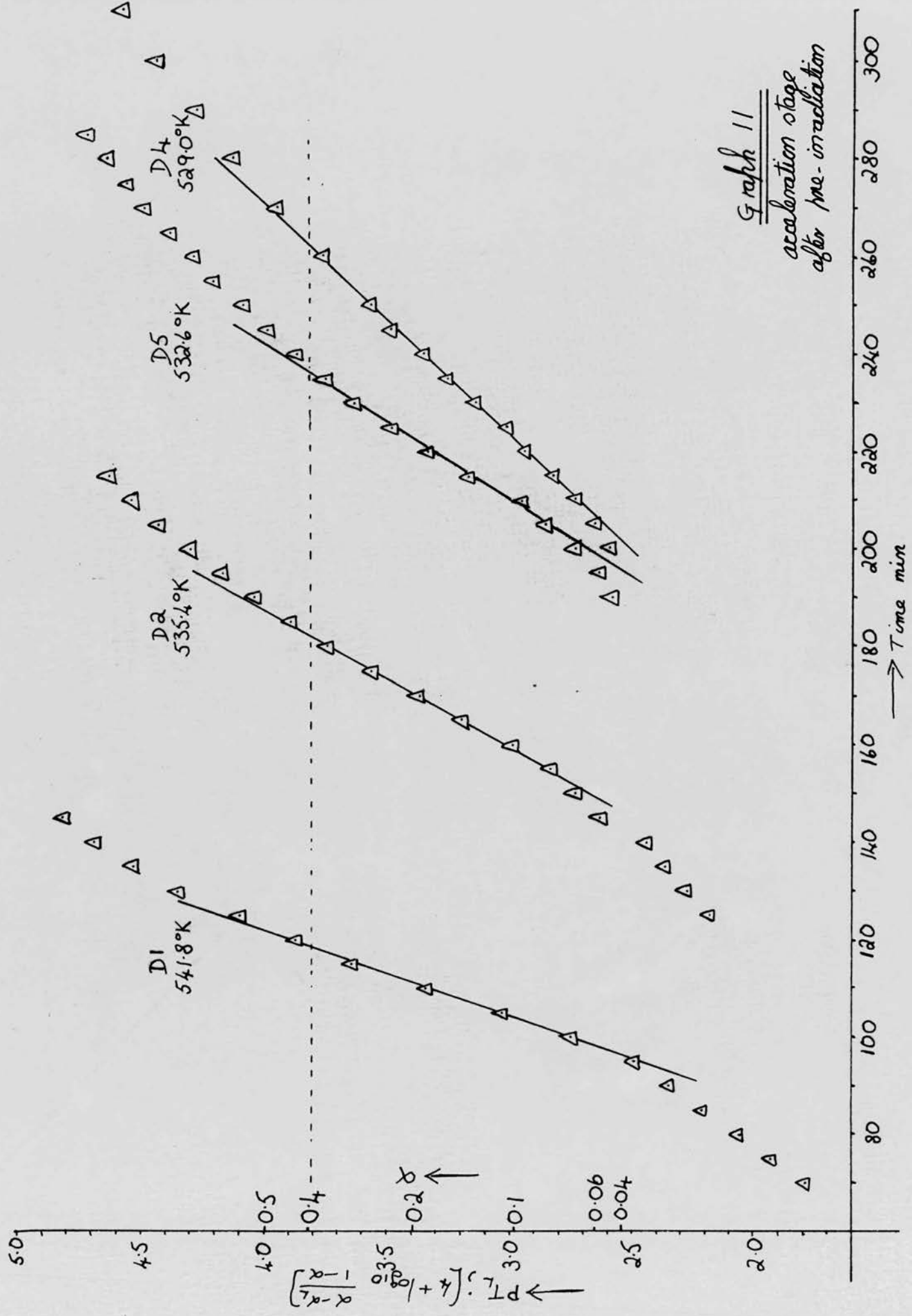


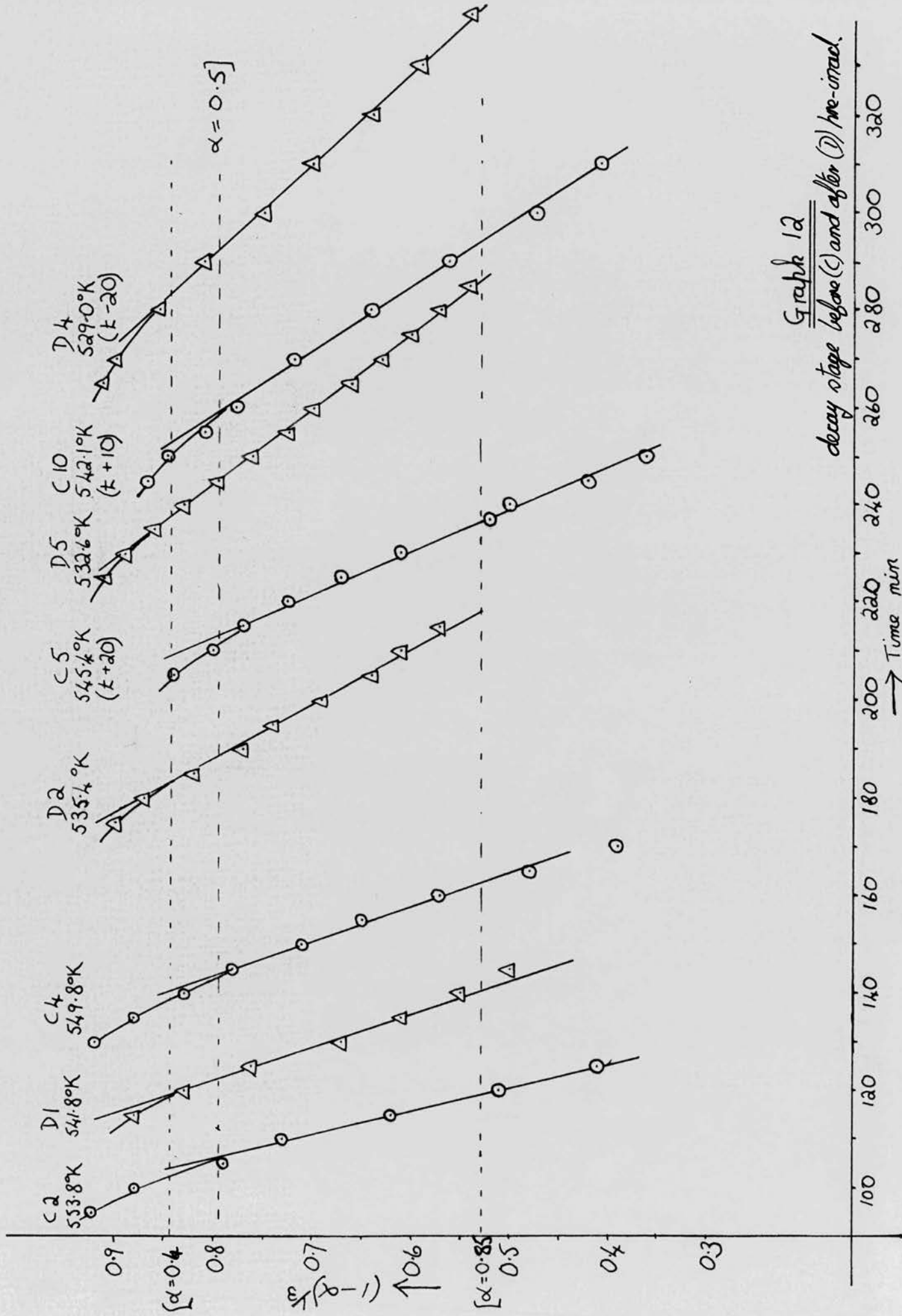


Graph 10  
acceleration stage



Graph 11  
acceleration stage  
after pre-irradiation





Graph 12  
 decay stage before (C) and after (D) pre-irrad.



2. 6. 3. Kinetic results for large crystals E with varying times of pre-irradiation.

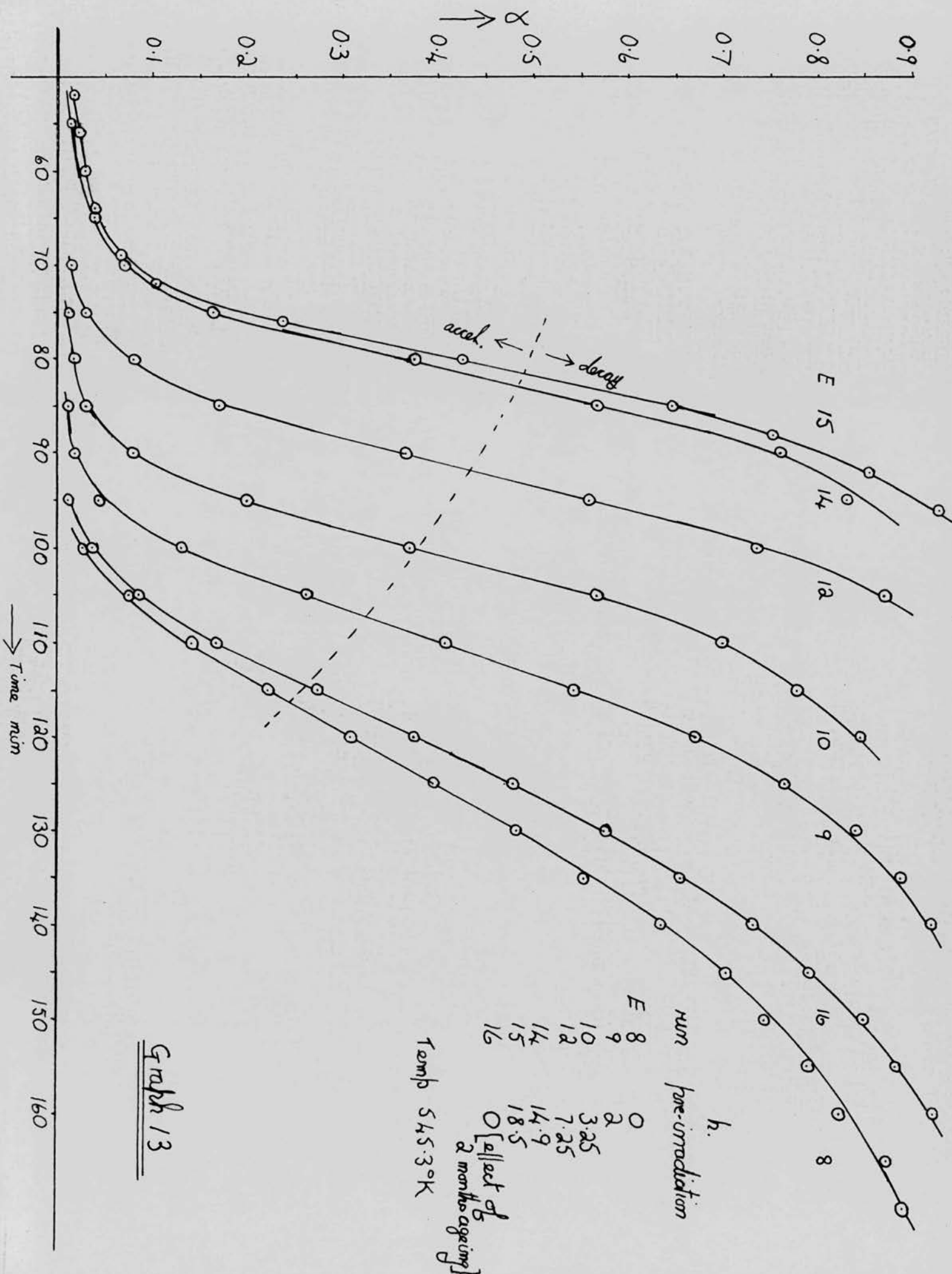
Material E is similar to A but has been stored for a year. Run E8 is for the unirradiated material and E16 shows the effect of a further 2 months storage. Runs E9 - 15 illustrate the effect of varying times of pre-irradiation with u.v. under similar conditions to those described in 2.4. The most notable feature is the extension of the acceleration stage from  $\alpha = 0.2$  to  $\alpha = 0.4$ , together with a much increased rate of decay and the introduction of the initial power law.

Table 11, analysis of material E.

Graph 13, ' $\alpha$ ' - 't' curves for material E.

Graph 14, graphical analysis of runs E8, 9, 15.





Graph 13





2. 6. 4. Kinetic results for small crystals F and G

Tables 12, 13, 14 and 15 and graphs 15, 16, 17 and 18, illustrate the effect of two years ageing on the small crystals. Material F is fresh crystals and G is the same material after storage for two years. The most notable feature is an increase in the rate of the acceleration stage. For both F and G the initial power law growth continues to ca  $\alpha = 0.03$  and the large negative values of 't<sub>0</sub>' are to be noted. The acceleration stage in both cases ceases at  $\alpha = 0.5$ .

Tables 12, 13 and 14, analysis of material F.

Tables 14 and 15, analysis of material G.

Graph 15, the ' $\alpha$ ' - 't' curves for F and G.

Graph 16a and b, plot of  $\alpha^{1/2}/t$  showing the fit for the power law with  $n = 2$ , for F and G.

Graph 17, acceleration stage, the plot of the Prout-Tompkins factor for F and G. In F23 and 28 a correction has been made for the initial power law growth; this has improved the fit for the lower values of ' $\alpha$ '.

Graph 18, decay stage, the plot of the contracting sphere factor for F and G.

Table 12. Material F. Fresh small crystals.

| Run<br>Temp<br>$\alpha_p$<br>Time<br>min | F14<br>551.2°K<br>0.035 |                                  |      | F3<br>555.2°K                      |                      |                                  | F9<br>560.6°K |                      |
|--|-------------------------|----------------------------------|------|------------------------------------|----------------------|----------------------------------|---------------|----------------------|
|  | $\alpha \times 10^2$    | $\alpha^{\frac{1}{2}} \times 10$ | PT   | $\alpha_p^{\frac{1}{3}} \times 10$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$ | PT            | $\alpha \times 10^2$ |
| 5  | 0.08                    | 0.30                             |      |                                    | 0.06                 | 0.25                             |               | 0.08                 |
| 10                                       | 0.21                    | 0.46                             |      |                                    | 0.22                 | 0.47                             |               | 0.28                 |
| 15                                       | 0.30                    | 0.56                             |      |                                    | 0.38                 | 0.62                             |               | 0.42                 |
| 20                                       | 0.41                    | 0.64                             |      |                                    | 0.56                 | 0.75                             |               | 0.70                 |
| 25                                       | 0.56                    | 0.74                             |      |                                    | 0.79                 | 0.89                             |               | 1.03                 |
| 30                                       | 0.70                    | 0.84                             |      |                                    | 0.99                 | 0.99                             |               | 1.46                 |
| 35                                       | 0.90                    | 0.92                             |      |                                    | 1.33                 | 1.15                             |               | 2.00                 |
| 40                                       | 1.07                    | 1.03                             |      |                                    | 1.64                 | 1.28                             |               | 2.69                 |
| 45                                       | 1.3                     | 1.14                             |      |                                    | 1.98                 | 1.41                             |               | 3.60                 |
| 50                                       | 1.59                    | 1.26                             |      |                                    | 2.39                 | 1.55                             |               | 5.70                 |
| 55                                       | 1.89                    | 1.37                             |      |                                    | 2.88                 | 1.70                             |               | 12.2                 |
| 60                                       | 2.22                    | 1.49                             |      |                                    | 3.58                 | 1.89                             |               | 31.6                 |
| 65                                       | 2.58                    | 1.61                             |      |                                    | 4.46                 | 2.12                             | 2.84          | 61.2                 |
| 70                                       | 2.96                    | 1.72                             |      |                                    | 6.45                 |                                  |               | 85.5                 |
| 75                                       | 3.41                    | 1.85                             |      |                                    | 10.0                 |                                  | 3.00          | 97.0                 |
| 80                                       | 3.97                    | 1.99                             | 2.62 |                                    | 19.4                 | $(1-\alpha)^{\frac{1}{3}}$       | 3.38          |                      |
| 85                                       | 4.87                    | 2.21                             | 2.71 |                                    | 37.8                 | 0.85                             | 3.78          |                      |
| 90                                       | 5.98                    |                                  | 2.80 |                                    | 58.4                 | 0.75                             | 4.14          |                      |
| 95                                       | 8.1                     |                                  | 2.95 | 2.76                               | 73.0                 | 0.65                             | 4.40          |                      |
| 100                                      | 12.7                    | $(1-\alpha)^{\frac{1}{3}}$       | 3.16 | 4.06                               | 87.5                 | 0.50                             | 4.84          |                      |
| 105                                      | 20.5                    | 0.93                             | 3.41 | 5.25                               | 96.3                 | 0.33                             | 5.42          |                      |
| 110                                      | 30.9                    | 0.88                             | 3.65 | 6.29                               |                      |                                  |               |                      |
| 115                                      | 43.7                    | 0.83                             | 3.89 | 7.22                               |                      |                                  |               |                      |
| 120                                      | 57.5                    | 0.75                             | 4.13 | 8.01                               |                      |                                  |               |                      |
| 125                                      | 71.2                    | 0.66                             | 4.39 | 8.67                               |                      |                                  |               |                      |
| 130                                      | 82.2                    | 0.56                             | 4.66 |                                    |                      |                                  |               |                      |
| 135                                      | 90.0                    | 0.46                             | 4.95 |                                    |                      |                                  |               |                      |
| 140                                      | 97.2                    | 0.30                             | 5.54 |                                    |                      |                                  |               |                      |



Table 13. Material F. Fresh small crystals.

| Run<br>Temp<br>$\alpha_p$<br>Time<br>min | F28<br>540.9°K<br>0.033 |                                  |                 |                          | F35<br>535.7°K       |                                  | F43<br>530.4°K       |                                  |
|--|-------------------------|----------------------------------|-----------------|--------------------------|----------------------|----------------------------------|----------------------|----------------------------------|
|  | $\alpha \times 10^{-2}$ | $\alpha^{\frac{1}{2}} \times 10$ | PT <sub>p</sub> | $\alpha_p^{\frac{1}{3}}$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$ |
| 10                                       | 0.15                    | 0.39                             |                 |                          | 0.12                 | 0.34                             | 0.08                 |                                  |
| 20                                       | 0.20                    | 0.45                             |                 |                          | 0.25                 | 0.5                              | 0.14                 | 0.37                             |
| 30                                       | 0.31                    | 0.56                             |                 |                          | 0.33                 | 0.57                             | 0.19                 | 0.43                             |
| 40                                       | 0.44                    | 0.66                             |                 |                          | 0.40                 | 0.63                             | 0.24                 | 0.49                             |
| 50                                       | 0.57                    | 0.76                             |                 |                          | 0.49                 | 0.70                             | 0.28                 | 0.53                             |
| 60                                       | 0.74                    | 0.86                             |                 |                          | 0.59                 | 0.77                             | 0.34                 | 0.58                             |
| 70                                       | 0.94                    | 0.97                             |                 |                          | 0.67                 | 0.82                             | 0.42                 | 0.65                             |
| 80                                       | 1.15                    | 1.07                             |                 |                          | 0.71                 | 0.88                             | 0.47                 | 0.69                             |
| 90                                       | 1.37                    | 1.17                             |                 |                          | 0.92                 | 0.96                             | 0.53                 | 0.73                             |
| 100                                      | 1.59                    | 1.26                             |                 |                          | 1.03                 | 1.01                             | 0.61                 | 0.78                             |
| 110                                      | 1.92                    | 1.38                             |                 |                          | 1.23                 | 1.11                             | 0.68                 | 0.82                             |
| 120                                      | 2.18                    | 1.48                             |                 |                          |                      |                                  | 0.79                 | 0.89                             |
| 130                                      | 2.52                    | 1.59                             |                 |                          | 1.55                 | 1.24                             | 0.85                 | 0.92                             |
| 140                                      | 2.88                    | 1.70                             |                 |                          | 1.74                 | 1.32                             | 0.96                 | 0.98                             |
| 150                                      | 3.33                    | 1.82                             |                 |                          | 1.93                 | 1.39                             | 1.01                 | 1.02                             |
| 160                                      | 4.05                    | 2.01                             | 1.87            | 1.96                     | 2.14                 | 1.46                             | 1.16                 | 1.08                             |
| 165                                      | 4.33                    |                                  | 2.01            | 2.17                     |                      |                                  |                      |                                  |
| 170                                      | 4.80                    |                                  | 2.18            | 2.47                     | 2.38                 | 1.54                             | 1.32                 | 1.15                             |
| 175                                      | 5.32                    |                                  | 2.33            | 2.71                     |                      |                                  |                      |                                  |
| 180                                      | 6.00                    |                                  | 2.46            | 3.08                     | 2.54                 | 1.59                             | 1.38                 | 1.17                             |
| 185                                      | 7.28                    |                                  | 2.63            | 3.42                     |                      |                                  |                      |                                  |
| 190                                      | 8.7                     |                                  | 2.78            | 3.78                     | 2.82                 | 1.68                             | 1.50                 | 1.22                             |
| 195                                      | 11.0                    |                                  | 2.94            | 4.25                     |                      |                                  |                      |                                  |
| 200                                      | 14.5                    | =====                            | 3.11            | 4.82                     | 3.07                 | 1.75                             | 1.64                 | 1.28                             |
| 205                                      | 17.4                    |                                  | 3.24            | 5.20                     |                      |                                  |                      |                                  |
| 210                                      | 22.6                    | $(1-\alpha)^{\frac{1}{3}}$       | 3.38            | 5.78                     | 3.40                 | 1.84                             | 1.84                 | 1.35                             |
| 215                                      | 27.6                    |                                  | 3.53            | 6.24                     |                      |                                  |                      |                                  |
| 220                                      | 33.3                    | 0.87                             | 3.65            | 6.69                     | 3.70                 | 1.92                             | 1.86                 | 1.36                             |
| 225                                      | 38.9                    | 0.85                             | 3.76            | 7.09                     |                      |                                  |                      |                                  |
| 230                                      | 44.4                    | 0.82                             | 3.87            | 7.43                     | 3.90                 | 1.97                             | 2.08                 | 1.44                             |
| 235                                      | 51.2                    | 0.79                             | 4.00            | 8.00                     |                      |                                  |                      |                                  |
| 240                                      | 57.8                    | 0.75                             | 4.11            | 8.17                     | 4.62                 | 2.14                             | 2.24                 | 1.50                             |
| 245                                      | 63.5                    | 0.71                             | 4.22            |                          |                      |                                  |                      |                                  |
| 250                                      | 69.4                    | 0.67                             | 4.33            |                          | 5.14                 | <u>2.27</u>                      | 2.40                 | 1.55                             |
| 255                                      | 75.1                    | 0.63                             | 4.46            |                          |                      | PT                               |                      |                                  |
| 260                                      | 80.5                    | 0.58                             | 4.58            |                          | 6.48                 | 2.84                             | 2.59                 | 1.61                             |
| 265                                      | 84.4                    | 0.54                             | 4.72            |                          |                      |                                  |                      |                                  |
| 270                                      | 88.5                    | 0.49                             | 4.87            |                          | 8.92                 | 2.99                             | 2.78                 | 1.67                             |
| 275                                      | 92.5                    | 0.42                             | 5.08            |                          |                      |                                  |                      |                                  |
| 280                                      | 94.8                    | 0.37                             | 5.25            |                          | 12.6                 | 3.18                             | 2.94                 | 1.71                             |
| 290                                      |                         |                                  |                 |                          | 18.0                 | 3.34                             | 3.18                 | 1.78                             |
| 300                                      |                         |                                  |                 |                          | 24.0                 | 3.50                             | 3.40                 | 1.84                             |
| 310                                      |                         |                                  |                 |                          | 31.6                 | 3.67                             | 3.70                 | 1.92                             |
| 320                                      |                         |                                  |                 |                          | 40.5                 | 3.82                             | 4.11                 | 2.03                             |
| 330                                      |                         |                                  |                 |                          | 48.5                 | 3.98                             | 4.69                 | 2.16                             |

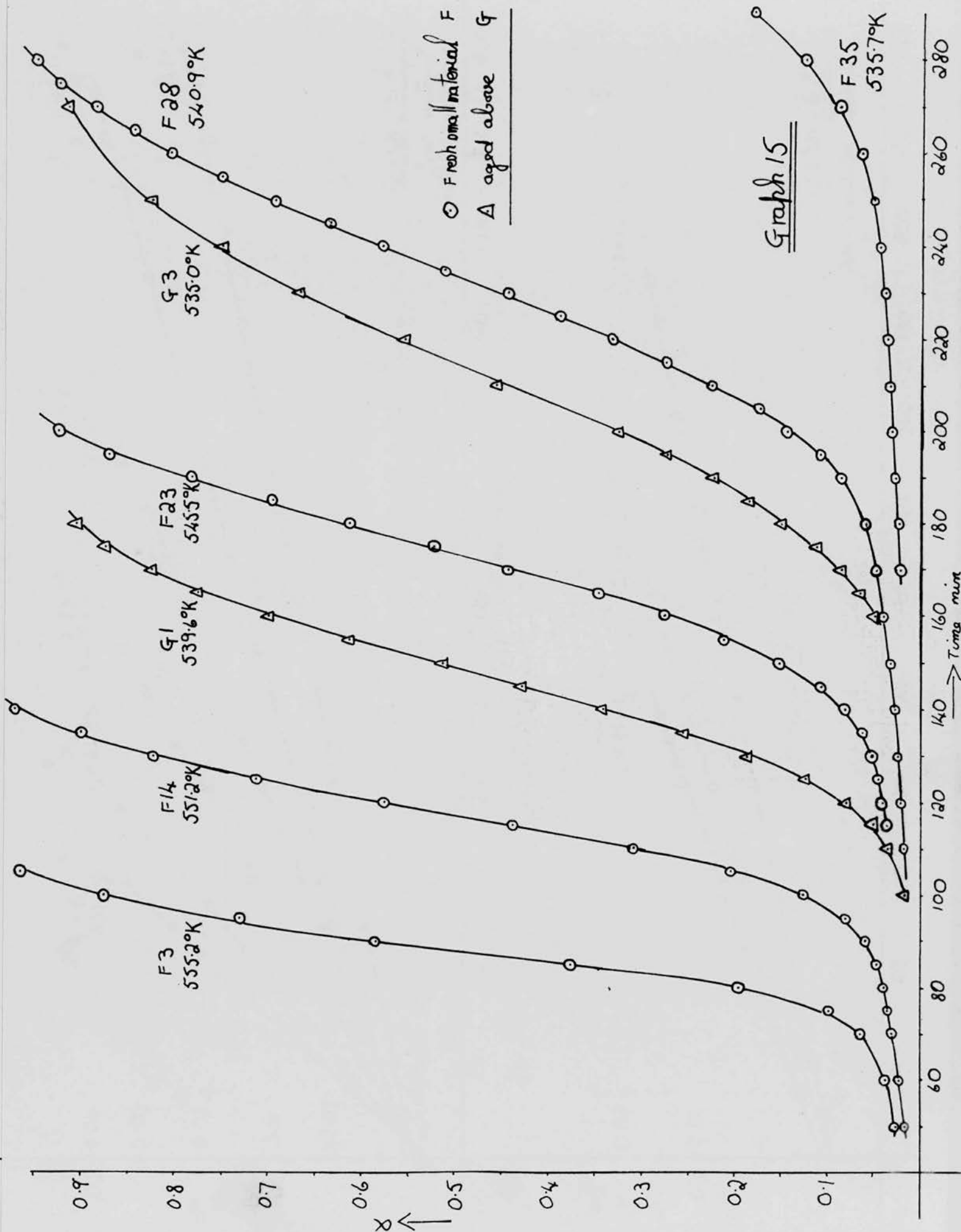
Table 14. Material F and G.

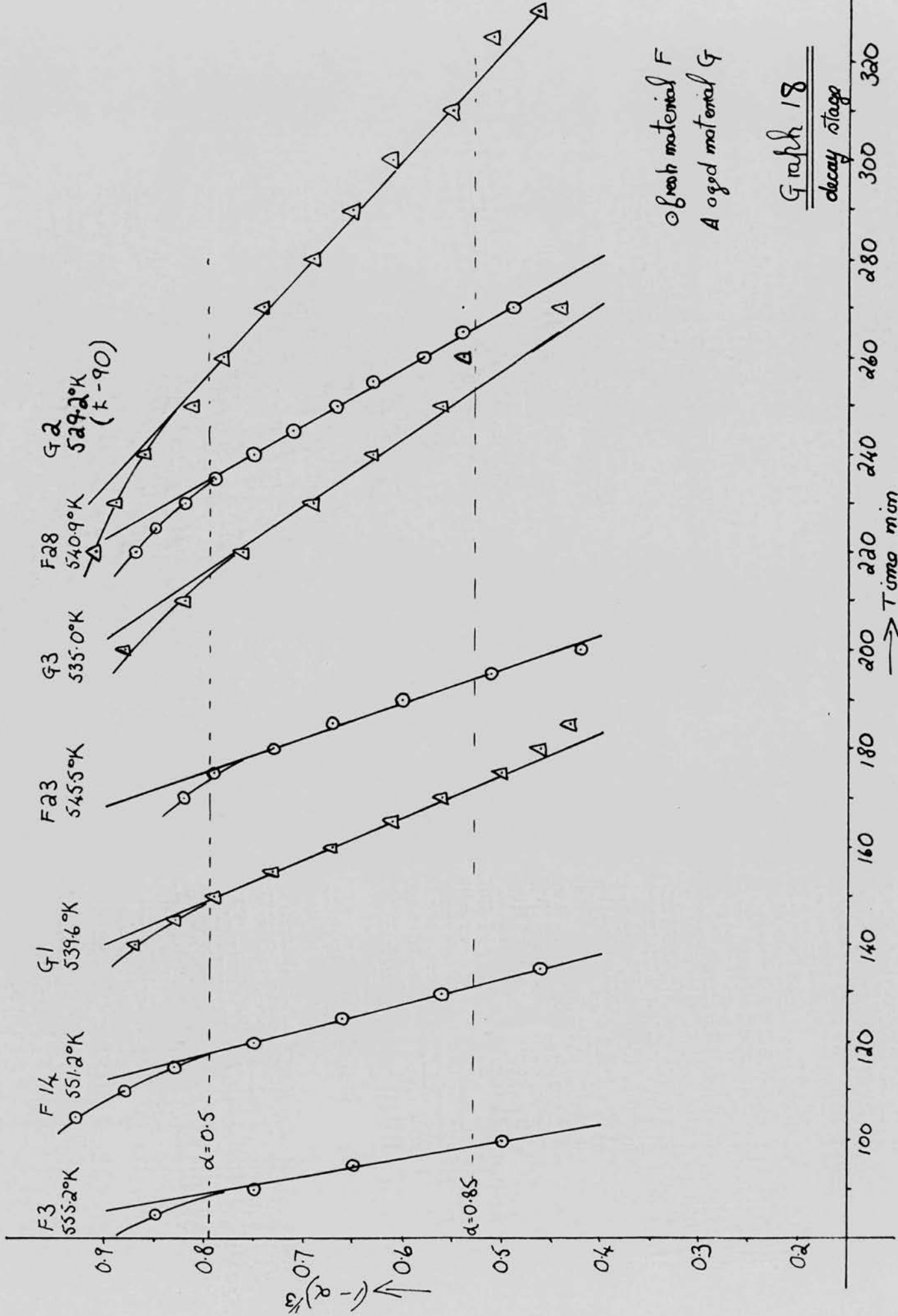
| Run<br>Temp<br>$\alpha_p$<br>Time<br>min | F23<br>545.5°K<br>0.035 |                                  |                 |                                    | G1<br>539.6°K        |                                  |      |
|--|-------------------------|----------------------------------|-----------------|------------------------------------|----------------------|----------------------------------|------|
|  | $\alpha \times 10^2$    | $\alpha^{\frac{1}{2}} \times 10$ | PT <sub>P</sub> | $\alpha_p^{\frac{1}{3}} \times 10$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$ | PT   |
| 5  | 0.09                    |                                  |                 |                                    | 0.11                 | 0.34                             |      |
| 10                                       | 0.17                    | 0.41                             |                 |                                    | 0.20                 |                                  |      |
| 15                                       | 0.21                    | 0.46                             |                 |                                    | 0.21                 | 0.46                             |      |
| 20                                       | 0.28                    | 0.53                             |                 |                                    | 0.26                 | 0.50                             |      |
| 25                                       | 0.33                    | 0.57                             |                 |                                    | 0.31                 | 0.55                             |      |
| 30                                       | 0.47                    | 0.68                             |                 |                                    | 0.36                 |                                  |      |
| 35                                       | 0.54                    | 0.73                             |                 |                                    | 0.43                 | 0.66                             |      |
| 40                                       | 0.68                    | 0.82                             |                 |                                    |                      |                                  |      |
| 45                                       | 0.79                    | 0.89                             |                 |                                    | 0.55                 | 0.74                             |      |
| 50                                       | 0.96                    | 0.98                             |                 |                                    |                      |                                  |      |
| 55                                       | 1.07                    | 1.03                             |                 |                                    |                      |                                  |      |
| 60                                       | 1.28                    | 1.13                             |                 |                                    | 0.74                 | 0.81                             |      |
| 65                                       | 1.42                    | 1.19                             |                 |                                    | 0.83                 | 0.91                             |      |
| 70                                       | 1.54                    | 1.24                             |                 |                                    | 0.91                 | 0.95                             |      |
| 75                                       | 1.68                    | 1.29                             |                 |                                    | 1.01                 | 1.00                             |      |
| 80                                       | 1.90                    | 1.38                             |                 |                                    | 1.1                  | 1.05                             |      |
| 85                                       | 2.13                    | 1.46                             |                 |                                    | 1.2                  | 1.09                             |      |
| 90                                       | 2.34                    | 1.53                             |                 |                                    | 1.31                 | 1.14                             | 2.12 |
| 95                                       | 2.56                    | 1.60                             |                 |                                    | 1.45                 | 1.20                             | 2.16 |
| 100                                      | 2.83                    | 1.68                             |                 |                                    | 1.83                 | 1.35                             | 2.26 |
| 105                                      | 3.08                    | 1.75                             |                 |                                    | 2.30                 | 1.52                             | 2.37 |
| 110                                      | 3.32                    | 1.82                             |                 |                                    | 3.40                 |                                  | 2.55 |
| 115                                      | 3.70                    | 1.92                             |                 |                                    | 5.11                 |                                  | 2.73 |
| 120                                      | 4.04                    | 2.01                             | 1.70            |                                    | 8.0                  |                                  | 2.93 |
| 125                                      | 4.66                    | 2.16                             | 2.06            | 2.23                               | 12.5                 |                                  | 3.15 |
| 130                                      | 5.41                    |                                  | 2.31            | 2.67                               | 18.8                 |                                  | 3.36 |
| 135                                      | 6.44                    |                                  | 2.50            | 3.09                               | 25.6                 | $(1 - \alpha)^{\frac{1}{3}}$     | 3.54 |
| 140                                      | 8.22                    |                                  | 2.71            | 3.61                               | 34.2                 | 0.87                             | 3.72 |
| 145                                      | 10.9                    |                                  | 2.92            | 4.20                               | 42.9                 | 0.83                             | 3.87 |
| 150                                      | 15.3                    |                                  | 3.14            | 4.90                               | 51.3                 | 0.79                             | 4.02 |
| 155                                      | 21.3                    | $(1 - \alpha)^{\frac{1}{3}}$     | 3.35            | 5.62                               | 61.3                 | 0.73                             |      |
| 160                                      | 27.6                    |                                  | 3.52            | 6.17                               | 70.0                 | 0.67                             |      |
| 165                                      | 34.9                    |                                  | 3.69            | 6.80                               | 77.4                 | 0.61                             |      |
| 170                                      | 44.3                    | 0.82                             | 3.84            | 7.42                               | 82.5                 | 0.56                             |      |
| 175                                      | 52.3                    | 0.78                             | 4.00            | 7.93                               | 87.5                 | 0.50                             |      |
| 180                                      | 61.3                    | 0.73                             | 4.14            | 8.33                               | 90.5                 | 0.46                             |      |
| 185                                      | 69.5                    | 0.67                             | 4.29            |                                    | 92.0                 | 0.43                             |      |
| 190                                      | 78.1                    | 0.60                             |                 |                                    |                      |                                  |      |
| 195                                      | 87.0                    | 0.51                             |                 |                                    |                      |                                  |      |
| 200                                      | 92.5                    | 0.42                             |                 |                                    |                      |                                  |      |

Table 15. Material G. Aged small crystals.

| Run<br>Temp<br>$\alpha_P$<br>Time<br>min | G2<br>529.2°K<br>0.024 |                                  |      | G3<br>535.0°K                      |                      |                                      |      |
|--|------------------------|----------------------------------|------|------------------------------------|----------------------|--------------------------------------|------|
|  | $\alpha \times 10^2$   | $\alpha^{\frac{1}{2}} \times 10$ | PT   | $\alpha_P^{\frac{1}{3}} \times 10$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$     | PT   |
| 10                                       | 0.09                   | 0.30                             |      |                                    | 0.12                 | 0.34                                 |      |
| 20                                       | 0.14                   | 0.37                             |      |                                    | 0.18                 | 0.43                                 |      |
| 40                                       | 0.24                   | 0.49                             |      |                                    | 0.37                 | 0.61                                 |      |
| 60                                       | 0.35                   | 0.59                             |      |                                    | 0.58                 | 0.76                                 |      |
| 80                                       | 0.46                   | 0.68                             |      |                                    | 0.82                 | 0.90                                 |      |
| 100                                      | 0.61                   | 0.78                             |      |                                    | 1.12                 | 1.06                                 |      |
| 110                                      | 0.70                   | 0.84                             |      |                                    | 1.28                 | 1.13                                 |      |
| 120                                      | 0.77                   | 0.88                             |      |                                    |                      |                                      |      |
| 130                                      | 0.86                   | 0.93                             |      |                                    | 1.81                 | 1.35                                 |      |
| 140                                      | 0.97                   | 0.98                             |      |                                    | 2.25                 | 1.50                                 | 2.35 |
| 150                                      | 1.09                   | 1.04                             |      |                                    | 3.12                 | 1.77                                 | 2.49 |
| 155                                      | 1.15                   | 1.07                             |      |                                    | 3.86                 |                                      | 2.59 |
| 160                                      | 1.21                   | 1.10                             |      |                                    | 4.98                 |                                      | 2.70 |
| 165                                      | 1.27                   | 1.13                             |      |                                    | 6.61                 |                                      | 2.82 |
| 170                                      | 1.38                   | 1.17                             |      |                                    | 8.65                 |                                      | 2.95 |
| 175                                      | 1.45                   | 1.20                             |      |                                    | 11.3                 |                                      | 3.10 |
| 180                                      | 1.45                   | 1.20                             |      |                                    | 15.1                 |                                      | 3.25 |
| 185                                      | 1.50                   | 1.22                             |      |                                    | 18.6                 |                                      | 3.36 |
| 190                                      | 1.57                   | 1.25                             |      |                                    | 22.3                 |                                      | 3.46 |
| 195                                      | 1.64                   | 1.28                             |      |                                    | 27.4                 |                                      | 3.58 |
| 200                                      | 1.72                   | 1.31                             |      |                                    | 32.7                 | $(1 - \alpha)^{\frac{1}{3}}$<br>0.88 | 3.71 |
| 210                                      | 1.90                   | 1.38                             |      |                                    | 45.6                 | 0.82                                 | 3.92 |
| 220                                      | 2.09                   | 1.45                             | 2.32 |                                    | 55.4                 | 0.76                                 | 4.10 |
| 230                                      | 2.38                   | 1.54                             | 2.38 |                                    | 66.6                 | 0.69                                 | 4.30 |
| 240                                      | 2.81                   | 1.67                             | 2.46 | 1.58                               | 75.0                 | 0.63                                 | 4.48 |
| 250                                      | 3.54                   | 1.88                             | 2.55 | 2.29                               | 82.4                 | 0.56                                 | 4.67 |
| 260                                      | 4.80                   |                                  | 2.71 | 2.88                               | 85.1                 | 0.53                                 | 4.76 |
| 270                                      | 6.69                   |                                  | 2.85 | 3.50                               | 91.3                 | 0.44                                 | 5.02 |
| 280                                      | 9.7                    |                                  | 3.03 | 4.18                               |                      |                                      |      |
| 290                                      | 13.3                   |                                  | 3.18 | 4.79                               |                      |                                      |      |
| 300                                      | 18.0                   | $(1 - \alpha)^{\frac{1}{3}}$     | 3.33 | 5.38                               |                      |                                      |      |
| 310                                      | 23.5                   | 0.91                             | 3.49 | 5.95                               |                      |                                      |      |
| 320                                      | 29.7                   | 0.89                             | 3.63 | 6.49                               |                      |                                      |      |
| 330                                      | 37.0                   | 0.86                             | 3.78 | 7.02                               |                      |                                      |      |
| 340                                      | 45.1                   | 0.82                             | 3.91 | 7.53                               |                      |                                      |      |
| 350                                      | 52.3                   | 0.78                             | 4.04 | 7.94                               |                      |                                      |      |
| 360                                      | 59.4                   | 0.74                             | 4.17 |                                    |                      |                                      |      |
| 370                                      | 67.0                   | 0.69                             | 4.29 |                                    |                      |                                      |      |
| 380                                      | 72.5                   | 0.65                             | 4.42 |                                    |                      |                                      |      |
| 390                                      | 76.8                   | 0.61                             | 4.52 |                                    |                      |                                      |      |
| 400                                      | 83.1                   | 0.55                             | 4.70 |                                    |                      |                                      |      |
| 415                                      | 86.7                   | 0.51                             | 4.81 |                                    |                      |                                      |      |
| 420                                      | 90.1                   | 0.46                             | 4.96 |                                    |                      |                                      |      |







○ Fresh material F  
 △ aged material G

Graph 18  
decay stage

### 2. 6. 5. Kinetic results for small crystals H and K

Tables 16, 17 and 18 and graphs 19, 20, 21 and 22 illustrate the effect of 18.5 h. pre-irradiation with u.v. on the small crystals. Material H is fresh crystals similar in preparation to material F, and K is H after pre-irradiation. The most notable feature is the overall increase in the rate of decomposition. For both H and K, the initial power law growth extends to ca  $\alpha = 0.02$  and the acceleration stage ceases at  $\alpha = 0.5$ . Material H is similar to F for both the acceleration and decay stages, but the rate for the initial power law growth is less.

Tables 16, 17 and 18, analyses for materials H and K.

Graph 19, the ' $\alpha$ ' - 't' curves for H and K.

Graph 20a and b, plot of  $\alpha^{1/2}/t$  showing the fit for the power law with  $n = 2$ , for H and K.

Graph 21, acceleration stage, plot of the Prout-Tompkins factor for H and K.

Graph 22, decay stage, plot of the contracting sphere factor for H and K.





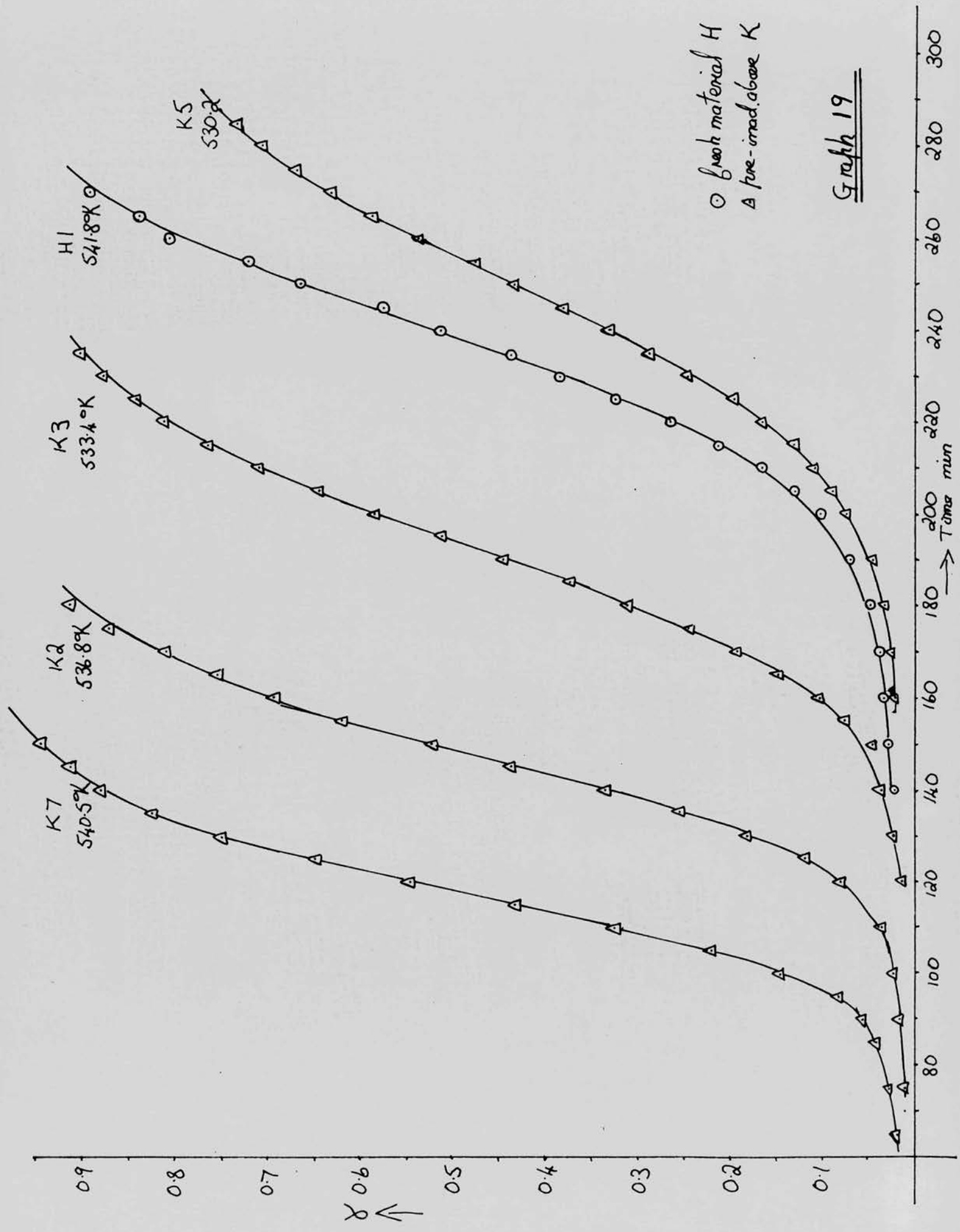
Table 17. Material H and K.

| Run<br>Temp | H1<br>541.8°K |                              |                                  | K3<br>533.4°K |                              |                                  |      | K5<br>530.2                        |                      |                                  |      |                                  |
|-------------|---------------|------------------------------|----------------------------------|---------------|------------------------------|----------------------------------|------|------------------------------------|----------------------|----------------------------------|------|----------------------------------|
|             | Time<br>min   | $\alpha \times 10^2$         | $\alpha^{\frac{1}{2}} \times 10$ | PT            | $\alpha \times 10^2$         | $\alpha^{\frac{1}{2}} \times 10$ | PT   | $\alpha_p^{\frac{1}{2}} \times 10$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$ | PT   | $\alpha^{\frac{1}{2}} \times 10$ |
| 10          | 0.05          | 0.23                         |                                  | 0.09          | 0.30                         |                                  |      |                                    | 0.09                 | 0.30                             |      |                                  |
| 20          | 0.12          | 0.35                         |                                  | 0.14          | 0.37                         |                                  |      |                                    | 0.14                 | 0.37                             |      |                                  |
| 30          | 0.19          | 0.43                         |                                  | 0.19          | 0.44                         |                                  |      |                                    | 0.19                 | 0.43                             |      |                                  |
| 40          | 0.26          | 0.51                         |                                  | 0.24          | 0.49                         |                                  |      |                                    | 0.26                 | 0.51                             |      |                                  |
| 50          | 0.36          | 0.60                         |                                  | 0.32          | 0.57                         |                                  |      |                                    | 0.33                 | 0.57                             |      |                                  |
| 60          | 0.46          | 0.68                         |                                  | 0.41          | 0.64                         |                                  |      |                                    | 0.42                 | 0.65                             |      |                                  |
| 70          | 0.60          | 0.77                         |                                  | 0.49          | 0.70                         |                                  |      |                                    | 0.51                 | 0.71                             |      |                                  |
| 80          | 0.77          | 0.89                         |                                  | 0.61          | 0.78                         |                                  |      |                                    | 0.66                 | 0.81                             |      |                                  |
| 90          | 0.94          | 0.97                         |                                  | 0.71          | 0.84                         |                                  |      |                                    | 0.74                 | 0.86                             |      |                                  |
| 100         | 1.06          | 1.03                         |                                  | 0.87          | 0.93                         |                                  |      |                                    | 0.87                 | 0.93                             |      |                                  |
| 110         | 1.25          | 1.12                         |                                  | 1.12          | 1.06                         |                                  |      |                                    | 0.98                 | 0.99                             |      |                                  |
| 120         | 1.49          | 1.22                         |                                  | 1.44          | 1.20                         |                                  |      |                                    | 1.09                 | 1.04                             |      |                                  |
| 125         | 1.64          | 1.28                         |                                  | 1.92          | 1.39                         | 2.28                             |      |                                    | 1.19                 | 1.13                             |      |                                  |
| 130         | 1.74          | 1.32                         |                                  | 2.18          |                              | 2.34                             | 2.28 |                                    | 1.27                 | 1.13                             |      |                                  |
| 135         | 1.98          | 1.40                         |                                  | 2.65          |                              | 2.42                             | 2.55 |                                    | 1.39                 | 1.21                             |      |                                  |
| 140         | 2.13          | 1.46                         |                                  | 3.54          |                              | 2.55                             | 2.94 |                                    | 1.46                 | 1.21                             |      |                                  |
| 145         | 2.50          |                              |                                  | 4.44          |                              | 2.68                             | 3.25 |                                    | 1.61                 | 1.26                             |      |                                  |
| 150         | 2.90          |                              |                                  | 5.47          |                              | 2.76                             | 3.55 |                                    | 1.59                 | 1.26                             |      |                                  |
| 155         | 3.14          |                              |                                  | 7.94          |                              | 2.94                             | 4.11 |                                    | 1.69                 | 1.43                             |      |                                  |
| 160         | 3.38          |                              |                                  | 10.4          |                              | 3.06                             | 4.55 |                                    | 2.04                 | 1.43                             |      |                                  |
| 165         | 3.69          |                              |                                  | 15.0          |                              | 3.25                             | 5.19 |                                    | 2.38                 |                                  |      |                                  |
| 170         | 3.75          |                              |                                  | 19.4          | $(1 - \alpha)^{\frac{1}{2}}$ | 3.38                             | 5.69 |                                    | 2.57                 | 1.60                             |      |                                  |
| 175         | 4.20          |                              |                                  | 24.8          |                              | 3.52                             | 6.20 |                                    | 2.92                 |                                  | 2.46 |                                  |
| 180         | 4.92          |                              | 2.71                             | 31.2          |                              | 3.66                             | 6.71 |                                    | 3.30                 |                                  | 2.52 | 2.62                             |
| 185         | 6.11          |                              | 2.81                             | 37.5          | 0.85                         | 3.78                             | 7.15 |                                    | 4.06                 |                                  | 2.62 | 2.96                             |
| 190         | 7.0           |                              | 2.88                             | 44.8          | 0.82                         | 3.91                             | 7.59 |                                    | 4.65                 |                                  | 2.69 | 3.14                             |
| 195         | 8.8           |                              | 2.98                             | 51.3          | 0.79                         | 4.02                             | 7.95 |                                    | 5.56                 |                                  | 2.77 | 3.45                             |
| 200         | 10.3          |                              | 3.06                             | 58.5          | 0.75                         | 4.15                             |      |                                    | 7.5                  |                                  | 2.90 | 3.91                             |
| 205         | 13.1          |                              | 3.18                             | 64.5          | 0.71                         | 4.26                             |      |                                    | 9.0                  |                                  | 3.01 | 4.31                             |
| 210         | 16.8          |                              | 3.30                             | 71.0          | 0.66                         | 4.41                             |      |                                    | 11.0                 |                                  | 3.10 | 4.61                             |
| 215         | 21.5          | $(1 - \alpha)^{\frac{1}{2}}$ | 3.44                             | 76.5          | 0.62                         | 4.51                             |      |                                    | 13.3                 |                                  | 3.19 | 4.90                             |
| 220         | 26.6          |                              | 3.56                             | 81.2          | 0.57                         | 4.64                             |      |                                    | 16.7                 |                                  | 3.30 | 5.34                             |
| 225         | 32.6          | 0.88                         | 3.68                             | 84.2          | 0.54                         | 4.73                             |      |                                    | 19.9                 |                                  | 3.39 | 5.69                             |
| 230         | 38.6          | 0.85                         | 3.80                             | 87.8          | 0.50                         | 4.86                             |      |                                    | 24.9                 |                                  | 3.52 | 6.16                             |
| 235         | 43.9          | 0.825                        | 3.89                             | 90.2          | 0.46                         | 4.96                             |      |                                    | 29.0                 |                                  | 3.61 | 6.54                             |
| 240         | 51.5          | 0.79                         | 4.03                             |               |                              |                                  |      |                                    | 33.3                 | $(1 - \alpha)^{\frac{1}{2}}$     | 3.70 | 6.82                             |
| 245         | 57.4          | 0.75                         | 4.13                             |               |                              |                                  |      |                                    | 38.2                 | 0.85                             | 3.79 | 7.15                             |
| 250         | 66.6          | 0.694                        | 4.30                             |               |                              |                                  |      |                                    | 43.5                 | 0.82                             | 3.89 | 7.49                             |
| 255         | 72.3          | 0.65                         | 4.42                             |               |                              |                                  |      |                                    | 47.7                 | 0.806                            | 3.96 | 7.73                             |
| 260         | 80.9          | 0.57                         | 4.63                             |               |                              |                                  |      |                                    | 54.0                 | 0.77                             | 4.07 | 8.07                             |
| 265         | 84.0          | 0.54                         | 4.72                             |               |                              |                                  |      |                                    | 58.9                 | 0.74                             | 4.16 |                                  |
| 270         | 89.6          | 0.47                         | 4.93                             |               |                              |                                  |      |                                    | 63.2                 | 0.72                             | 4.23 |                                  |
| 275         | 96.4          | 0.33                         |                                  |               |                              |                                  |      |                                    | 67.0                 | 0.69                             | 4.31 |                                  |
| 280         |               |                              |                                  |               |                              |                                  |      |                                    | 70.8                 | 0.66                             | 4.38 |                                  |
| 285         |               |                              |                                  |               |                              |                                  |      |                                    | 73.5                 | 0.64                             | 4.44 |                                  |

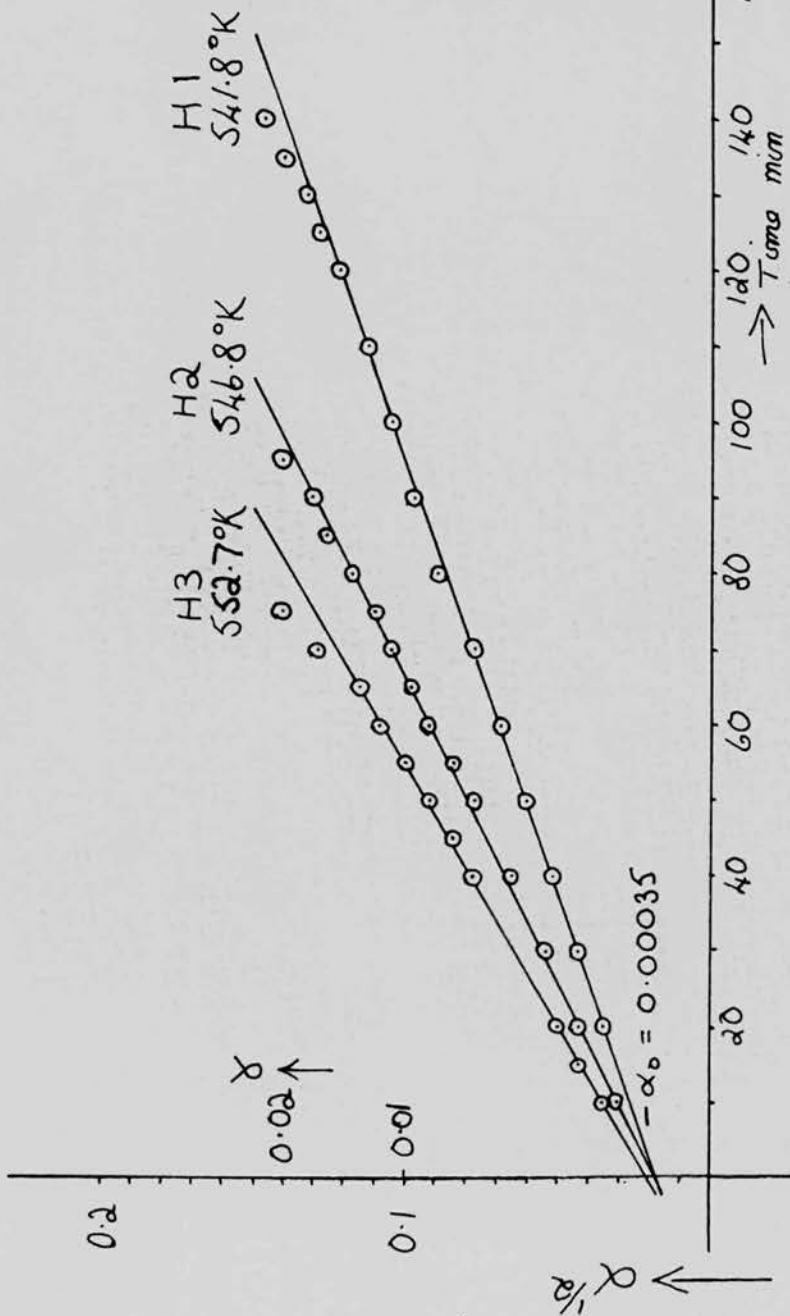
Table 18. Material K. Fresh small crystals pre-irradiated.

| Run<br>Temp<br>$\alpha_P$<br>Time<br>min | K2<br>536.8°K<br>0.013 |                                  |      | K7<br>540.5°K                      |                      |                                  |      |
|--|------------------------|----------------------------------|------|------------------------------------|----------------------|----------------------------------|------|
|  | $\alpha \times 10^2$   | $\alpha^{\frac{1}{2}} \times 10$ | PT   | $\alpha_P^{\frac{1}{2}} \times 10$ | $\alpha \times 10^2$ | $\alpha^{\frac{1}{2}} \times 10$ | PT   |
| 5  | 0.08                   | 0.28                             |      |                                    | 0.13                 | 0.36                             |      |
| 10                                       | 0.11                   | 0.33                             |      |                                    | 0.22                 | 0.47                             |      |
| 15                                       | 0.16                   | 0.40                             |      |                                    | 0.33                 | 0.57                             |      |
| 20                                       | 0.21                   | 0.46                             |      |                                    | 0.42                 | 0.65                             |      |
| 25                                       | 0.24                   | 0.49                             |      |                                    | 0.50                 | 0.71                             |      |
| 30                                       | 0.31                   | 0.56                             |      |                                    | 0.59                 | 0.77                             |      |
| 35                                       | 0.36                   | 0.60                             |      |                                    | 0.74                 | 0.86                             |      |
| 40                                       | 0.42                   | 0.66                             |      |                                    | 0.88                 | 0.94                             |      |
| 45                                       | 0.48                   | 0.69                             |      |                                    | 1.08                 | 1.04                             |      |
| 50                                       | 0.55                   | 0.74                             |      |                                    | 1.21                 | 1.10                             |      |
| 55                                       | 0.61                   | 0.78                             |      |                                    | 1.43                 | 1.20                             |      |
| 60                                       | 0.71                   | 0.84                             |      |                                    | 1.67                 | 1.29                             |      |
| 65                                       | 0.80                   | 0.89                             |      |                                    | 1.94                 | 1.39                             |      |
| 70                                       | 0.91                   | 0.96                             |      |                                    | 2.28                 | 1.51                             |      |
| 75                                       | 1.04                   | 1.02                             |      |                                    | 2.67                 | 1.63                             |      |
| 80                                       | 1.19                   | 1.09                             |      |                                    | 3.06                 | 1.74                             |      |
| 85                                       | 1.39                   | 1.18                             |      |                                    | 4.10                 |                                  |      |
| 90                                       | 1.53                   | 1.24                             |      |                                    | 5.54                 |                                  | 2.77 |
| 95                                       | 1.91                   | 1.38                             | 2.28 |                                    | 8.2                  |                                  | 3.00 |
| 100                                      | 2.18                   | 1.48                             | 2.34 |                                    | 14.6                 |                                  | 3.23 |
| 105                                      | 2.80                   |                                  | 2.46 | 2.35                               | 22.0                 | $(1 - \alpha)^{\frac{1}{2}}$     | 3.45 |
| 110                                      | 3.64                   |                                  | 2.58 | 2.98                               | 32.6                 | 0.88                             | 3.68 |
| 115                                      | 6.00                   |                                  | 2.81 | 3.68                               | 43.3                 | 0.83                             | 3.88 |
| 120                                      | 8.09                   |                                  | 2.94 | 4.14                               | 54.6                 | 0.77                             | 4.08 |
| 125                                      | 12.0                   |                                  | 3.13 | 4.79                               | 65.0                 | 0.70                             | 4.27 |
| 130                                      | 18.2                   | $(1 - \alpha)^{\frac{1}{2}}$     | 3.35 | 5.56                               | 75.0                 | 0.63                             | 4.48 |
| 135                                      | 25.6                   |                                  | 3.52 | 6.27                               | 82.5                 | 0.56                             | 4.67 |
| 140                                      | 33.7                   | 0.87                             | 3.71 | 6.89                               | 88.0                 | 0.49                             | 4.86 |
| 145                                      | 43.7                   | 0.82                             | 3.89 | 7.53                               | 91.2                 | 0.46                             | 5.02 |
| 150                                      | 52.4                   | 0.78                             | 4.10 | 8.01                               | 94.5                 | 0.38                             | 5.23 |
| 155                                      | 62.1                   | 0.72                             | 4.21 | 8.48                               |                      |                                  |      |
| 160                                      | 69.4                   | 0.67                             | 4.35 |                                    |                      |                                  |      |
| 165                                      | 75.5                   | 0.63                             | 4.49 |                                    |                      |                                  |      |
| 170                                      | 81.0                   | 0.575                            | 4.63 |                                    |                      |                                  |      |
| 175                                      | 87.1                   | 0.505                            | 4.88 |                                    |                      |                                  |      |
| 180                                      | 91.4                   | 0.44                             | 5.03 |                                    |                      |                                  |      |

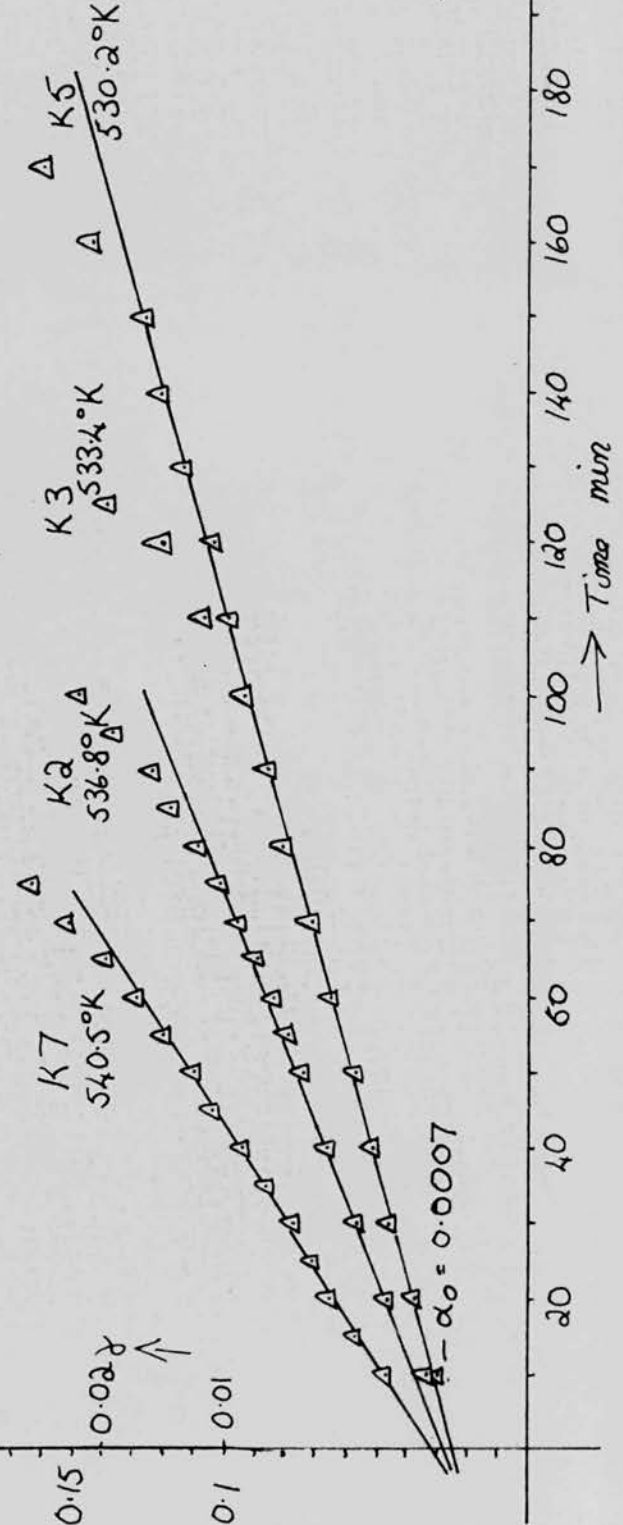


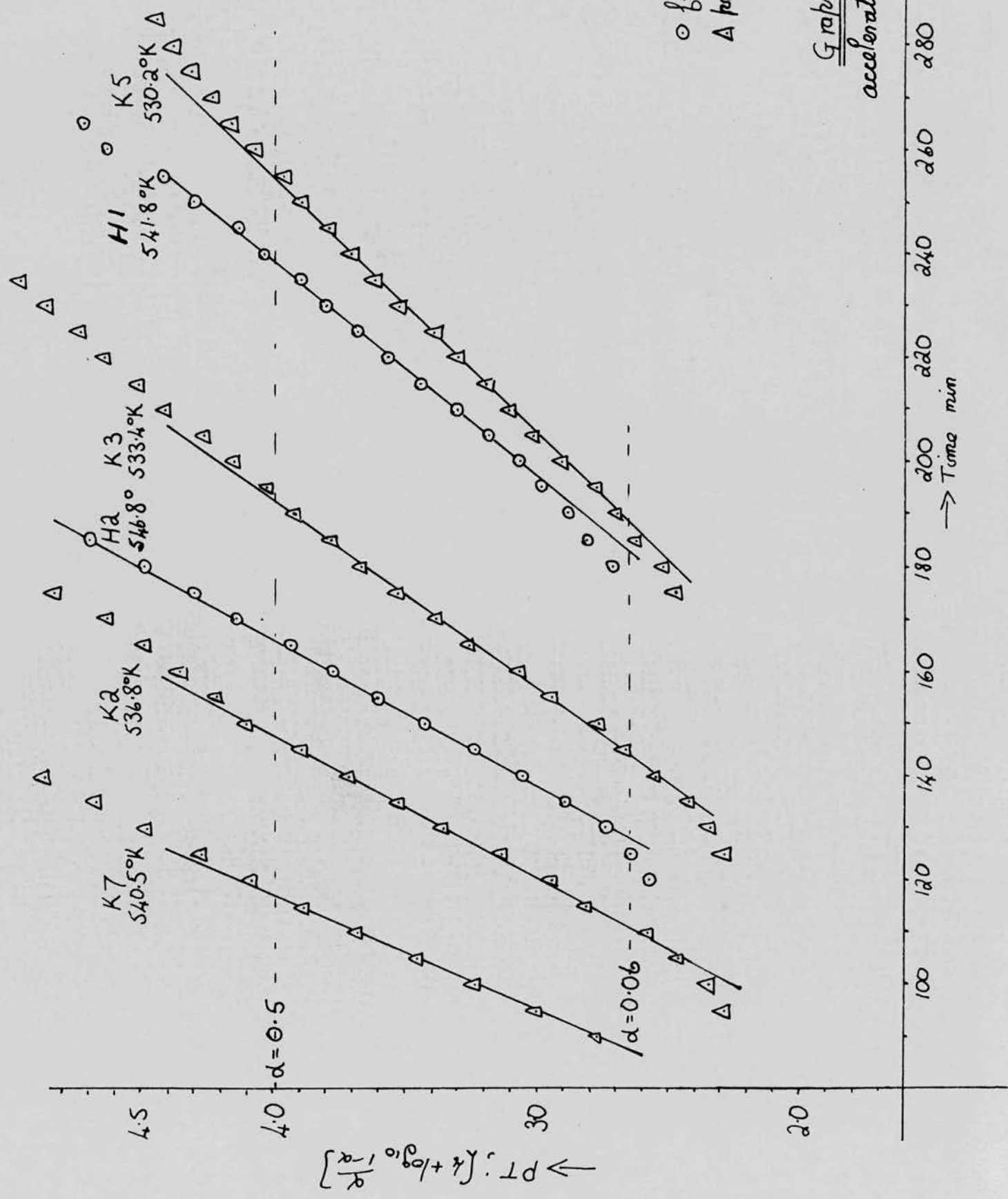


Graph 20A  
fresh material H  
initial power law



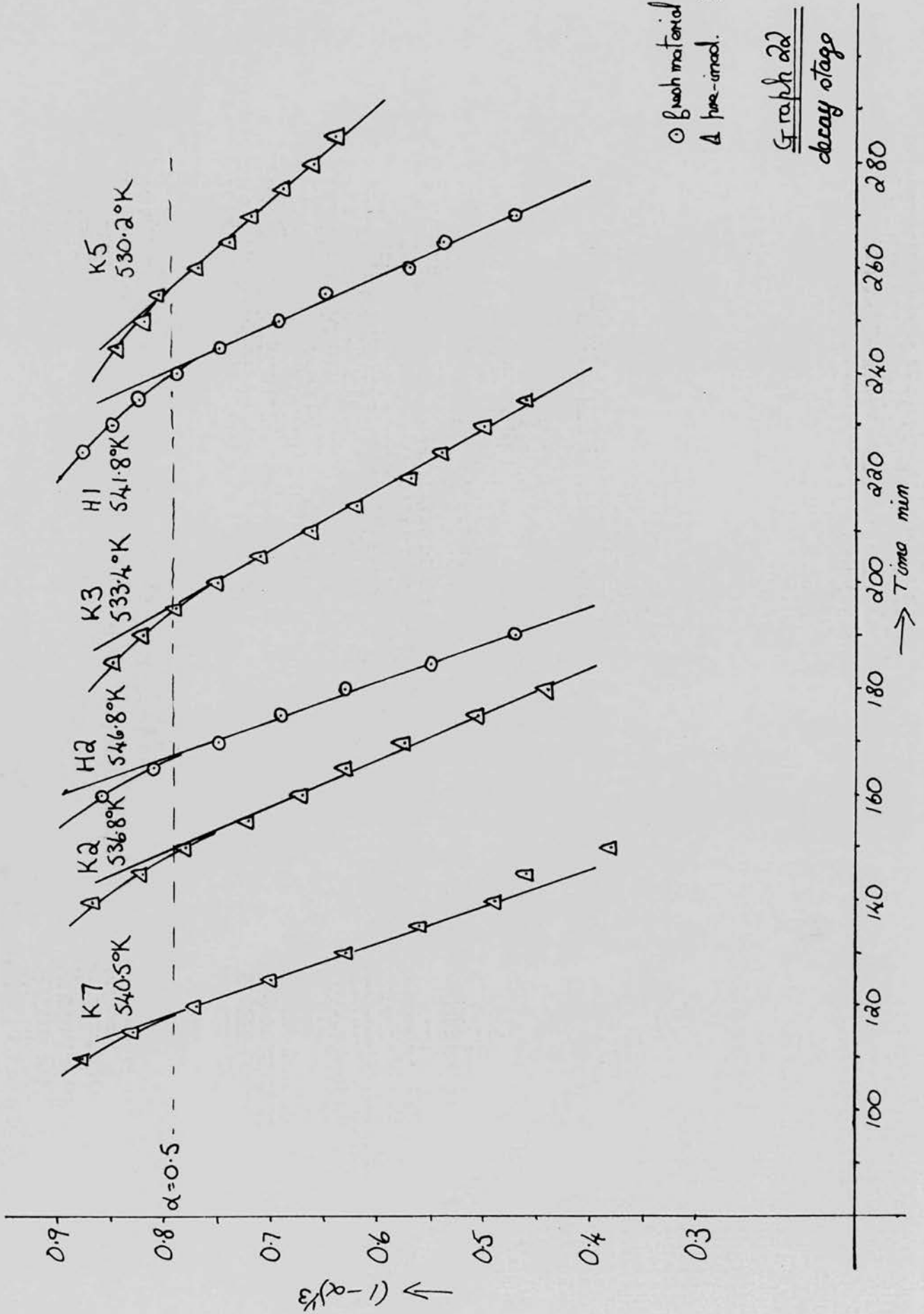
Graph 20B  
aged material K





Graph 21  
acceleration stage





### 2. 6. 6. Tables and graphs of rate constants

In tables 19 - 26 the rate constants for the various runs described in section 2.6.1 - 2.6.5 are tabulated, together with the respective temperatures.

$R_I$  is the initial rate,  $\frac{d\alpha}{dt}$ , for section OA, (Graph I, following page 19). It was found by measuring the initial slope of the ' $\alpha$ ' - ' $t$ ' curves.

$R_L$  is the constant rate for the linear stage AB in terms of  $\frac{d\alpha}{dt}$  from the equation  $\alpha = k_1 t + C$ ; thus  $R_L$  is equal to  $k_1$ .

$k_2^{\frac{1}{2}}$  and  $t_0$  are the constants from the equation  $\alpha = k_2(t - t_0)^2$  representing the initial power law growth for the small crystals.

$k_4^{\frac{1}{4}}$  is the constant from the equation  $(\alpha - \alpha_L) = k_4(t - t_0)^4$  representing the power law introduced by the pre-irradiation for the large crystals.

$k$  is the Prout-Tompkins branching coefficient from the equation  $2.3 \log_{10} \frac{\alpha}{1 - \alpha} = kt + C_1$ .

$R_M$  is the maximum rate of decomposition as measured from the ' $\alpha$ ' - ' $t$ ' curves.

$k_3$  is the constant from the contracting sphere equation  $\alpha = 1 - [C - k_3(t - t_0)]^3$ .

Table 19. Rate constants for material A, large fresh crystals.

| Run | Temp<br>T°K | $\frac{1}{T} \times 10^3$ | $R_I \times 10^5$ | $R_L \times 10^5$ | $R_M \times 10^3$ | $k \times 10^2$ | $k_3 \times 10^3$ |
|-----|-------------|---------------------------|-------------------|-------------------|-------------------|-----------------|-------------------|
| A 8 | 560.6       | 1.784                     | 27                | 19                | 38                | 15              | 27                |
| 2   | 555.2       | 1.801                     |                   | 11                | 30                | 12              | 20                |
| 12  | 551.2       | 1.814                     | 18                | 8.2               | 20                | 7.9             | 17                |
| 13  | 551.2       | 1.814                     |                   | 9.0               | 19                | 8.2             | 16                |
| 21  | 545.5       | 1.833                     | 18                | 5.0               | 12.0              | 5.5             | 8.8               |
| 22  | 545.5       | 1.833                     | 10                | 6.1               | 12.3              | 5.3             | 8.8               |
| 26  | 540.9       | 1.849                     | 6.1               | 3.3               | 8.8               | 3.8             | 5.6               |
| 29  | 540.9       | 1.849                     | 5.5               | 2.9               | 8.2               | 3.7             | 6.1               |
| 34  | 535.7       | 1.867                     | 3.6               | 2.0               | 5.9               | 2.9             | 3.7               |
| 42  | 530.4       | 1.885                     | 3.2               | 1.3               | -                 | -               | -                 |
| 46  | 530.4       | 1.885                     | 3.4               | 1.3               | -                 | -               | -                 |

Table 20. Rate constants for material B, material A aged.

|     |       |       |  |     |    |     |     |
|-----|-------|-------|--|-----|----|-----|-----|
| B 5 | 545.5 | 1.833 |  | 7.0 | 24 | 23  | 11  |
| 1   | 542.5 | 1.843 |  | 5.5 | 20 | 21  | 9.1 |
| 6   | 539.6 | 1.853 |  | 4.0 | 16 | 16  | 7.8 |
| 3   | 538.0 | 1.859 |  | 2.6 | 14 | 13  | 6.7 |
| 2   | 537.4 | 1.861 |  | 2.5 | 14 | 14  | 6.6 |
| 4   | 531.3 | 1.882 |  | 2.1 | 8  | 6.2 | 4.3 |

Table 21. Rate constants for material C, large fresh crystals.

| Run | Temp<br>T <sup>o</sup> K | $\frac{1}{T} \times 10^3$ | $R_L \times 10^5$ | $R_M \times 10^3$ | $k \times 10^2$ | $k_3 \times 10^3$ | $k_4^{\frac{1}{4}} \times 10^3$ |
|-----|--------------------------|---------------------------|-------------------|-------------------|-----------------|-------------------|---------------------------------|
| C 2 | 552.8                    | 1.809                     | 6.6               | 29                | 13.5            | 21                | -                               |
| 4   | 549.8                    | 1.819                     | 11                | 21                | 9.1             | 15.4              | -                               |
| 7   | 547.8                    | 1.826                     | 6.3               | 18                | 8.4             | 13                | -                               |
| 5   | 545.5                    | 1.833                     | 5.7               | 16                | 6.9             | 12                | -                               |
| 1   | 544.2                    | 1.838                     | 4.4               | 14                | 5.7             | 9.1               | -                               |
| 10  | 542.1                    | 1.845                     | 3.3               | 11                | 5.5             | 7.7               | -                               |
| 3   | 541.0                    | 1.848                     | 3.2               | 9.6               | 4.9             | 7.8               | -                               |
| 9   | 540.5                    | 1.850                     | 3.2               | 9.5               | 4.8             | 6.0               | -                               |

Table 22. Rate constants for material D, material C pre-irradiated.

|     |       |       |      |    |      |      |     |
|-----|-------|-------|------|----|------|------|-----|
| D 1 | 541.8 | 1.846 | 10.2 | 26 | 13.4 | 14.0 | 5.5 |
| 3   | 538.5 | 1.857 | 8.0  | 20 | 10.8 | 10.1 | 4.3 |
| 7   | 537.6 | 1.860 | 7.6  | 19 | 12.3 | 10.0 | 4.0 |
| 2   | 532.6 | 1.866 | 6.1  | 17 | 8.3  | 8.8  | 3.3 |
| 5   | 531.0 | 1.877 | 4.5  | 13 | 7.3  | 6.6  | 2.7 |
| 4   | 529.0 | 1.890 | 3.6  | 10 | 4.7  | 5.5  | 1.9 |



Table 23. Rate constants for material F, small fresh crystals.

| Run | Temp<br>$T^{\circ}\text{K}$ | $\frac{1}{T} \times 10^3$ | $k_2^{\frac{1}{2}} \times 10^4$ | $t_0$<br>min | $R_M \times 10^3$ | $k \times 10^2$ | $k_3 \times 10^3$ |
|-----|-----------------------------|---------------------------|---------------------------------|--------------|-------------------|-----------------|-------------------|
| F 9 | 560.6                       | 1.784                     | -                               | -            | 62                | -               | -                 |
| 3   | 555.2                       | 1.801                     | 27                              | 8            | 40                | 18              | 30                |
| 14  | 551.2                       | 1.814                     | 21                              | 10           | 27                | 11              | 19                |
| 20  | 545.5                       | 1.833                     | 15                              | 15           | 18                | 8.4             | 13                |
| 23  | 545.5                       | 1.833                     | 14                              | 17           | 19                | 9.2             | 14                |
| 27  | 540.9                       | 1.849                     | -                               | -            | 11                | 5.5             | 9.0               |
| 28  | 540.9                       | 1.849                     | 10                              | 23           | 12                | 6.2             | 8.6               |
| 35  | 535.7                       | 1.867                     | 7.5                             | 42           | 8.0               | 3.7             | 6.2               |
| 43  | 530.4                       | 1.885                     | 5.0                             | 51           | -                 | -               | -                 |

Table 24. Rate constants for material G, material F aged.

|     |       |       |     |    |     |     |      |
|-----|-------|-------|-----|----|-----|-----|------|
| G 1 | 539.6 | 1.853 | 9.0 | 35 | 17  | 9.6 | 11.5 |
| 3   | 535.0 | 1.869 | 7.0 | 32 | 12  | 6.0 | 7.1  |
| 2   | 529.2 | 1.890 | 5.0 | 50 | 8.0 | 3.7 | 4.5  |

Table 25. Rate constants for material H, fresh small crystals.

| Run | Temp<br>T°K | $\frac{1}{T} \times 10^3$ | $k_2^{\frac{1}{2}} \times 10^4$ | $t_0$<br>min | $R_M \times 10^3$ | $k \times 10^2$ | $k_3 \times 10^3$ |
|-----|-------------|---------------------------|---------------------------------|--------------|-------------------|-----------------|-------------------|
| H 3 | 552.7       | 1.809                     | 17                              | 13           | 36                | 13.8            | 20.0              |
| 2   | 546.8       | 1.829                     | 12                              | 14           | 20                | 8.2             | 14.0              |
| 1   | 541.8       | 1.847                     | 8.5                             | 20           | 14                | 5.6             | 10.0              |

Table 26. Rate constants for material K, material H pre-irradiated.

|     |       |       |      |    |      |      |     |
|-----|-------|-------|------|----|------|------|-----|
| K 1 | 541.3 | 1.847 | 16   | 12 | 23   | 12.0 | 8   |
| 7   | 540.5 | 1.850 | 16   | 20 | 21.3 | 10.6 | 14  |
| 4   | 539.7 | 1.853 | 11.5 | 22 | 20.3 | 10.2 | 13  |
| 9   | 539.8 | 1.853 | 11.5 | 20 | 20.3 | 10.1 | 13  |
| 2   | 536.8 | 1.863 | 10.0 | 28 | 17   | 8.4  | 11  |
| 3   | 533.4 | 1.875 | 8.0  | 34 | 14   | 6.4  | 8.7 |
| 5   | 530.2 | 1.886 | 6.8  | 35 | 10.5 | 4.6  | 5.6 |
| 8   | 529.8 | 1.888 | 5.5  | 50 | 9.2  | 4.8  | 6.0 |

In the following graphs 23 to 27, the Arrhenius activation energy plots are shown for the various temperature dependent constants given in tables 19 to 26. The activation energies have been mainly estimated from materials A and F, as the experiments in these cases covered a wide temperature range. The activation energies obtained from materials B, C, D, G, H and K could not be distinguished experimentally from those of A and F.

These graphs clearly illustrate the effect of ageing and pre-

irradiation on the rate of decomposition. As previously noted, ageing of both large and small crystals only materially increases the rate of the acceleration stage, although there is a small increase in the rate for the pre-acceleration and decay stages. On the other hand pre-irradiation of large and small crystals, materially increases the rate of all the stages of the decomposition.

The differences between material A and C and between F and H is small, indicating reasonable reproduceability of different batches that were made under similar conditions.

The following activation energies apply to the different stages:

For the large crystals the value is

ca 45 kcal mole<sup>-1</sup> for the initial decomposition (stage OA, graph 1) as found from graph 23,

50 ± 5 kcal mole<sup>-1</sup> for the initial linear decomposition (stage AB) from the values of  $R_L$  as found from graph 23,

46 ± 4 kcal mole<sup>-1</sup> for the power law growth introduced by pre-irradiation (stage BB<sup>1</sup>), as found from graph 24. This is obtained from values of  $k_4^{\frac{1}{4}}$  and is thus the value for the linear progression of the interface, assuming the same activation energy for growth and activation.

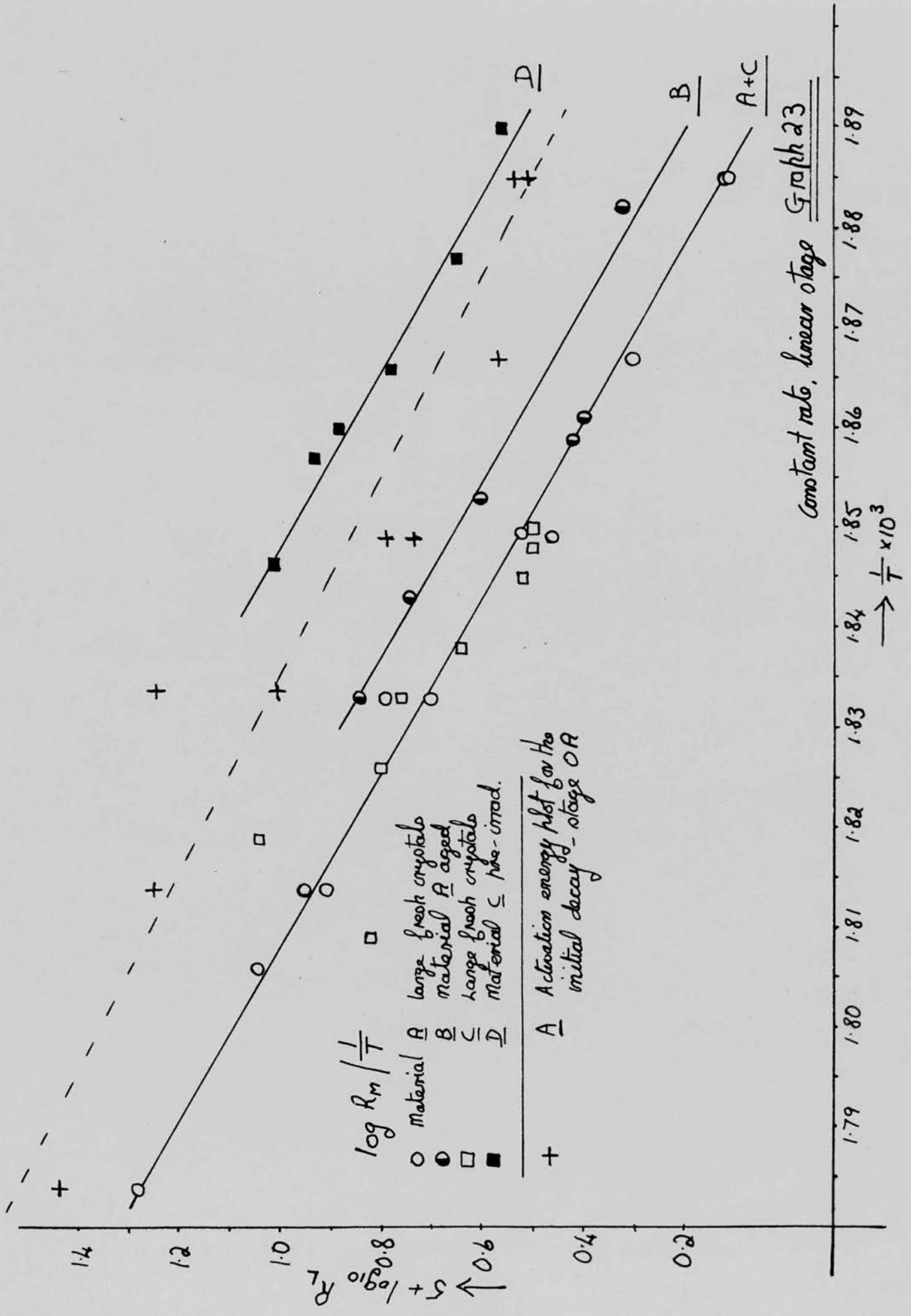
For the small crystals the value is

41 ± 4 kcal mole<sup>-1</sup> for the initial power law growth as found from graph 24. This is obtained from values of  $k_2^{\frac{1}{2}}$  and applies to the linear progression of the interface.

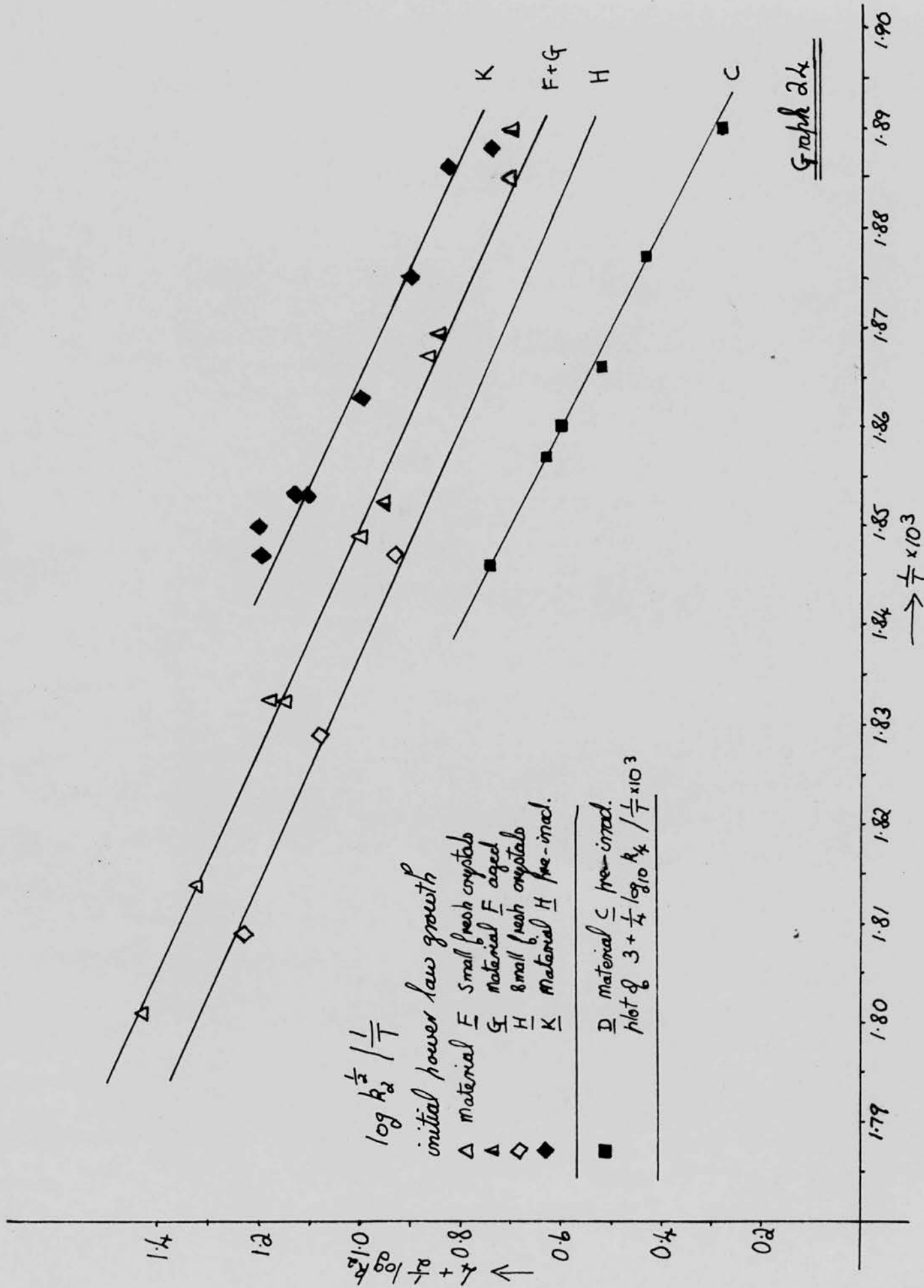
For both the large and small crystals the value is

46 ± 4 kcal mole<sup>-1</sup> from the maximum rate values,  $R_m$ , (graph 26) and from the Prout-Tompkins 'k' (graph 25) for the acceleration stage; also from the rate constant 'k<sub>3</sub>' (graph 27) for the decay stage which is by means of the contracting sphere mechanism.

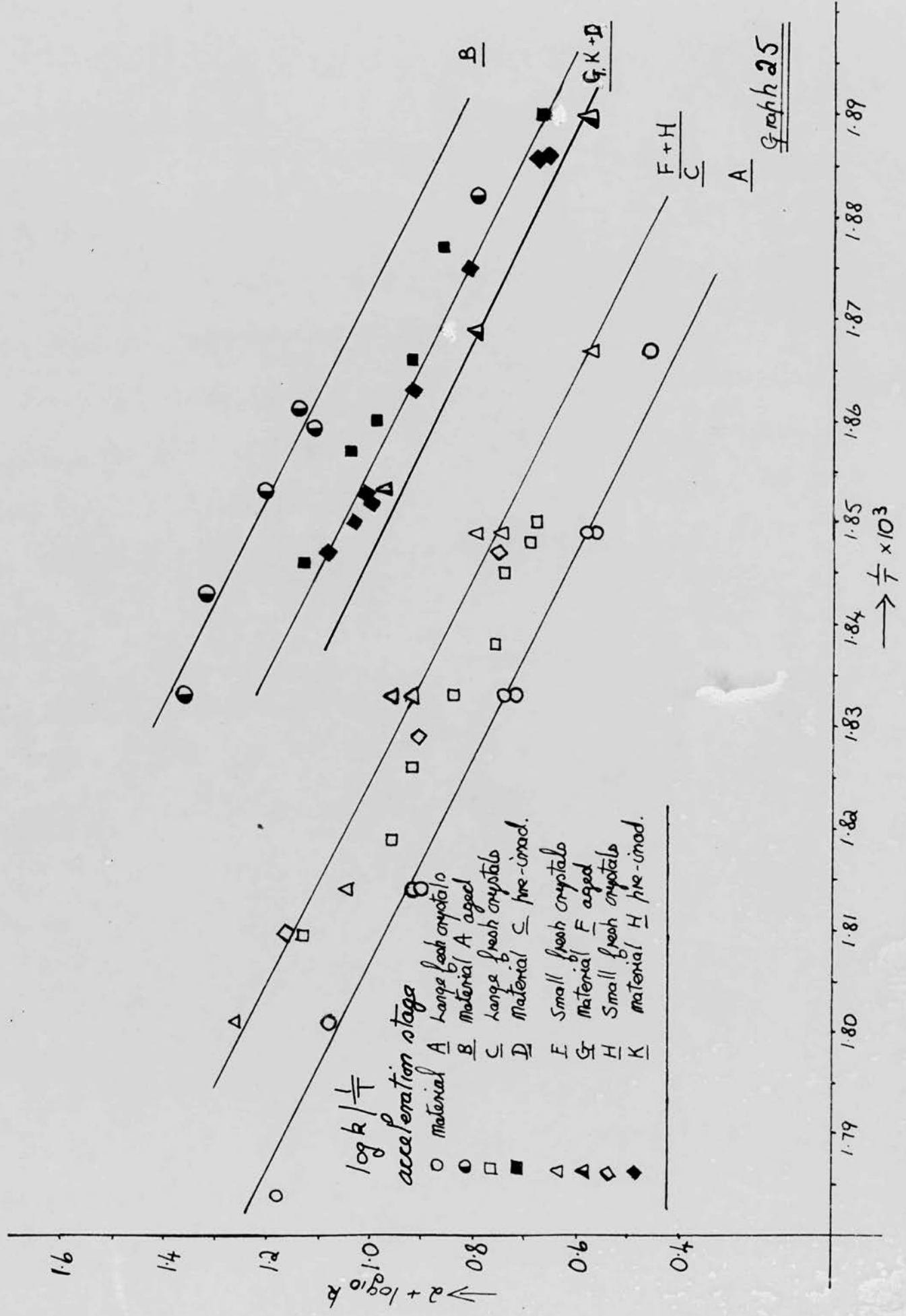


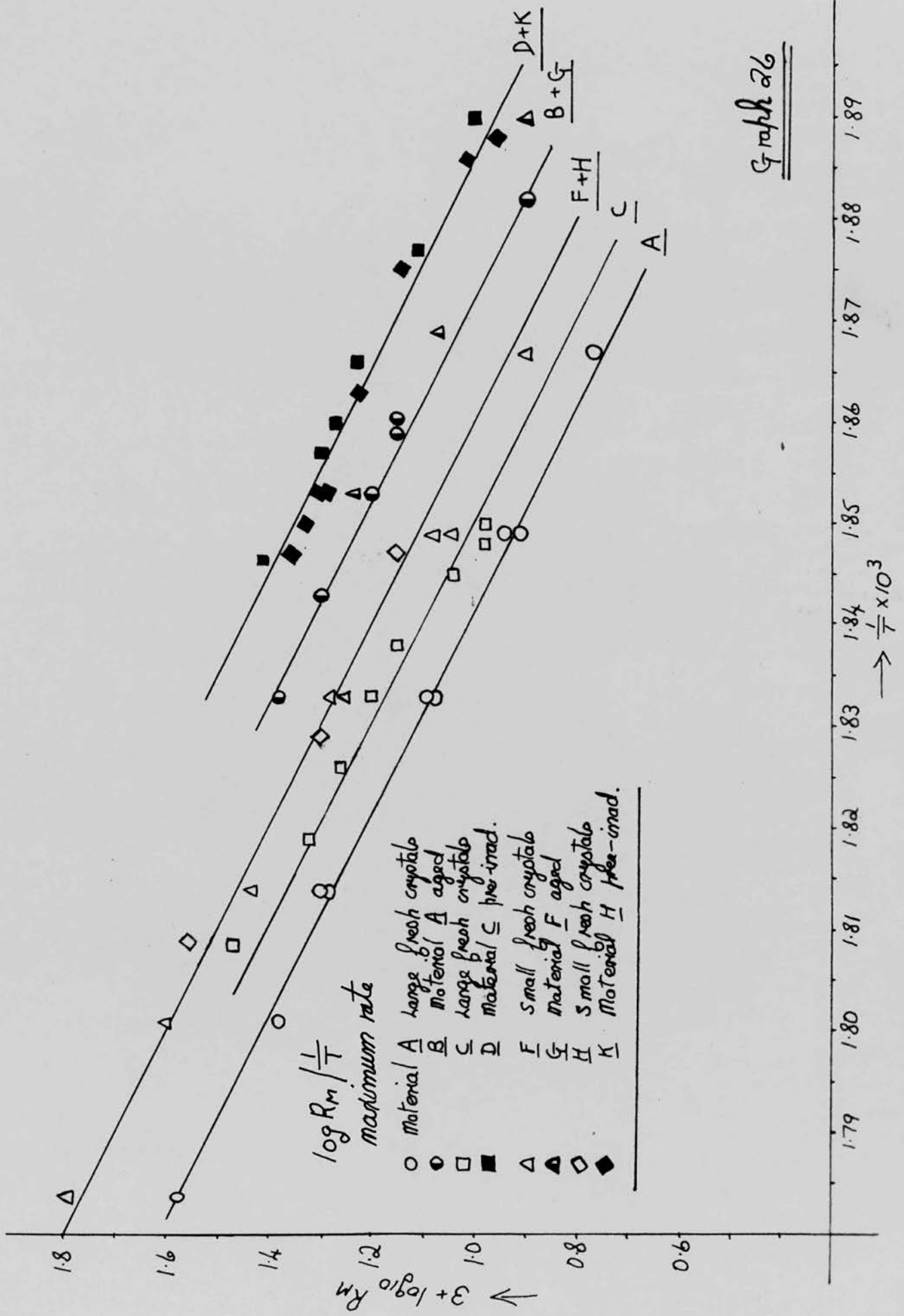




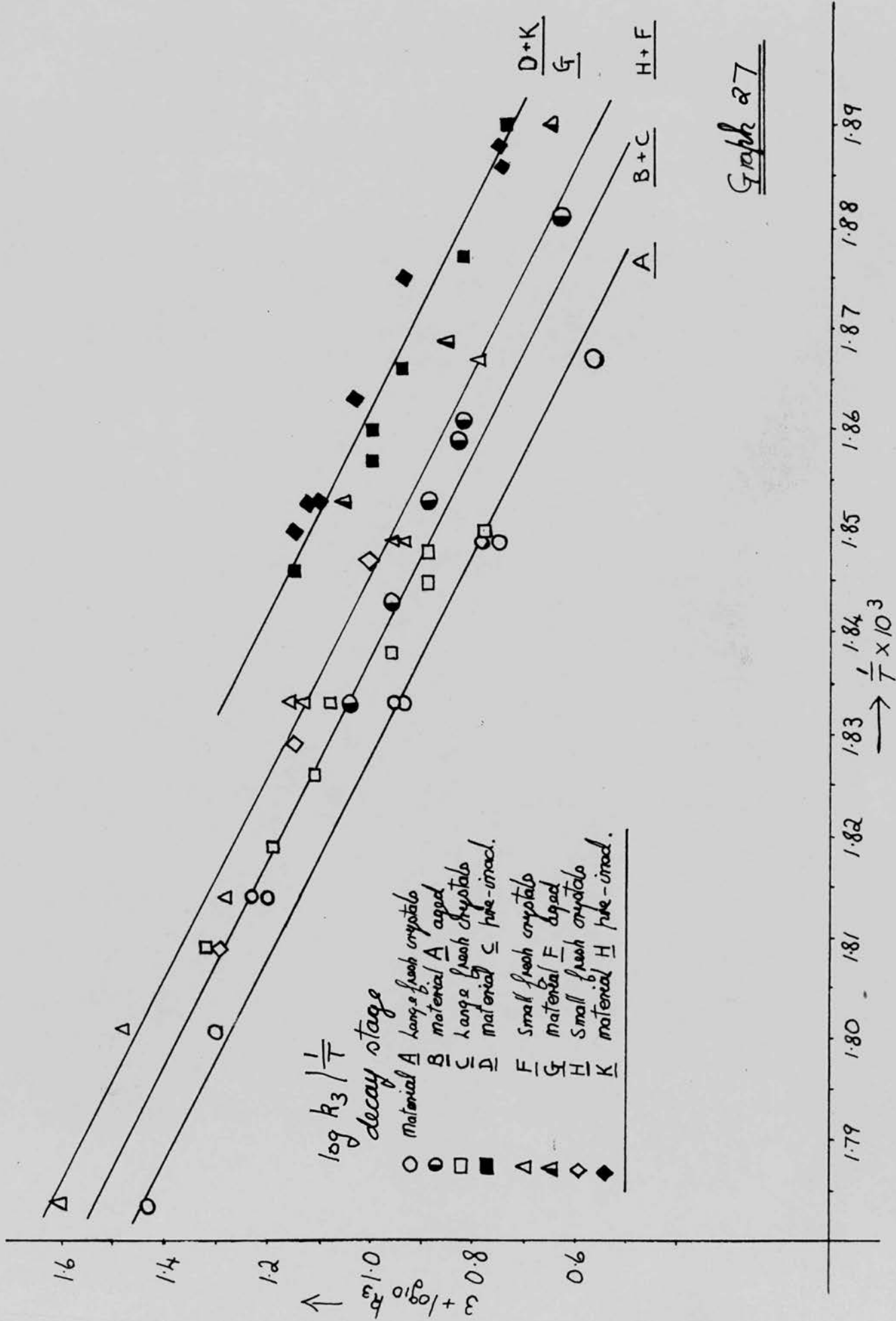


Graph 24





Graph 26



Graph 27



Finally in table 27 the rate constants are given for the runs performed on material E as described in section 2.6.3. These crystals had been stored for a year and then pre-irradiated for varying lengths of time. A graphical analysis of these results and their significance is given in the discussion.

Table 27. Rate constants for material E.

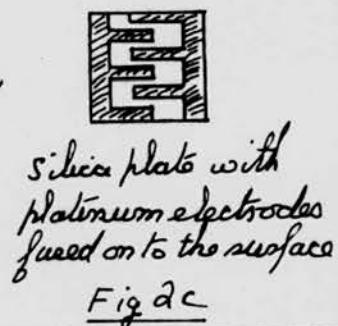
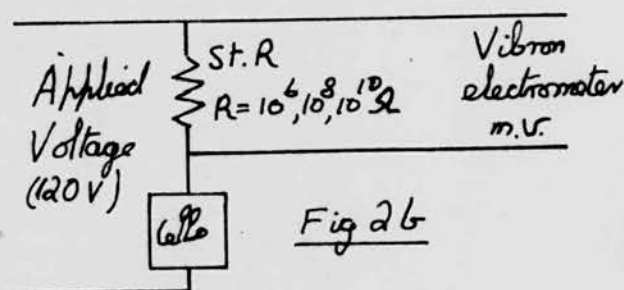
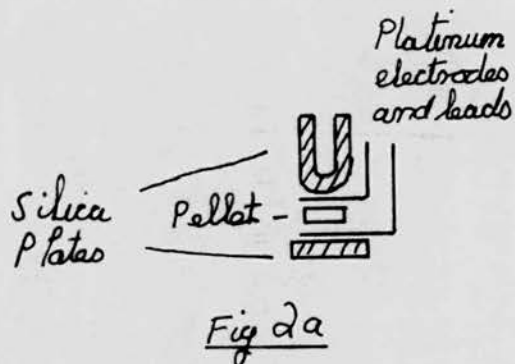
Temp 545.3°K

| Run | Time of pre-irrad. | Time at $\alpha = 0.006$ min | $R_M \times 10^3$ | $k \times 10^2$ | $k_3 \times 10^3$ | $\alpha$ at end of accel. | $k_4^{\frac{1}{4}} \times 10^3$ |
|-----|--------------------|------------------------------|-------------------|-----------------|-------------------|---------------------------|---------------------------------|
| 8   | 0                  | 87                           | 17                | 21              | 8.1               | 0.25                      | -                               |
| 16  | 0                  | 90                           | 20                | 21              | 11                | 0.25                      | -                               |
| 9   | 2                  | 75                           | 29                | 22              | 15                | 0.35                      | -                               |
| 10  | 3.25               | 65                           | 37                | 22              | 16                | 0.40                      | -                               |
| 12  | 7.25               | 60                           | 39                | 23              | 19                | 0.40                      | -                               |
| 14  | 14.9               | 40                           | 40                | 24              | 26                | 0.45                      | 6.2                             |
| 15  | 18.5               | 29                           | 45                | 24              | 27                | 0.45                      | 7.5                             |



## 2.7. Electrical conductivity measurements

For electrical conductivity measurements ground  $KIO_4$  and  $KIO_3$  were compressed at about 3 tons/sq. inch into strong hard cylindrical pellets 0.7 cm in diameter and 1 - 2 mm in height, in which spurious electrical effects due to poor contacts between individual particles<sup>48</sup> were probably minimised. A pellet was held between two 1 cm square platinum electrodes in a conductivity cell similar to that described by Jacobs<sup>49</sup>, the electrodes being insulated from the cell by means of vitreous silica plates 3 mm thick, as in Fig. 2a.



The silica plates were pressed together by means of a brass screw device, thus ensuring good contact between the platinum electrodes and the pellet surface.

The cell was hung in a pyrex reaction vessel which could be continuously evacuated by means of a three stage oil diffusion pump, backed by a rotary oil pump. The platinum leads from the platinum electrodes were led out of the reaction vessel through seals in soda

glass quickfit B7 cones. The electrical circuit used is shown in Fig. 2b; the voltage drop across the precision resistors being measured by an E.I.L. Vibron Electrometer model. This circuit measured resistances from  $10^8 - 10^{15}$  ohm.

From  $400^\circ - 490^\circ\text{K}$  the specific conductivity of pellets of  $\text{KIO}_4$  measured in vacuo after 24 h. preliminary evacuation at room temperature was given by  $\sigma = 10^0 \exp(-30000/RT)$   $\text{ohm}^{-1} \text{cm}^{-1}$ , with an error of ca  $\pm 10\%$ . A pellet made from material that had been irradiated for 50 h. as described in section 2.4. gave a similar result. For  $\text{KIO}_3$  the conductivity was given by  $\sigma = 10^{-1.8} \exp(-19000/RT)$   $\text{ohm}^{-1} \text{cm}^{-1}$  within  $\pm 10\%$  in the temperature range  $290^\circ - 490^\circ\text{K}$ . Measured resistances for pellets of  $\text{KIO}_4$  and  $\text{KIO}_3$  are given in the following table.

| Temp<br>$T^\circ\text{K}$ | Resistance (ohm) of $\text{KIO}_4$<br>pellet, 0.1 cm in height | Temp<br>$T^\circ\text{K}$ | Resistance (ohm) of $\text{KIO}_3$<br>pellet, 0.15 cm in height |
|---------------------------|--|---------------------------|---|
| 423                       | $3.4 \times 10^{14}$   | 294                       | $2.4 \times 10^{15}$  |
| 435                       | $1.0 \times 10^{14}$   | 317                       | $2.7 \times 10^{14}$  |
| 449                       | $4.8 \times 10^{13}$   | 336                       | $4.4 \times 10^{13}$  |
| 454                       | $2.4 \times 10^{13}$   | 347                       | $1.6 \times 10^{13}$  |
| 459                       | $1.4 \times 10^{13}$   | 354                       | $1.2 \times 10^{13}$  |
| 473                       | $8.0 \times 10^{12}$   | 483                       | $1.0 \times 10^{10}$  |
| 483                       | $3.5 \times 10^{12}$   |                           |   |

As the specific conductivity of  $\text{KIO}_4$  is similar to Sosman's results for vitreous silica<sup>50</sup>, it was thought that the resistances measured might have been due to the silica insulators in the cell and not to the pellet. But calculations showed that the leak resistance of



the cell was  $\frac{1}{100}$ <sup>th</sup> of the resistance of the pellet. The specific conductivity of a plate of silica glass 1 mm thick gave results in agreement with Sosman's.

For  $\text{KIO}_4$  and  $\text{KIO}_3$  both the pre-exponential factors and activation energies are reasonably characteristic of structure sensitive condition<sup>51</sup>, although the activation energy for  $\text{KIO}_4$  is slightly higher than would be expected. The extremely low conductivity of  $\text{KIO}_4$ , (the same as for vitreous silica), indicates that the movement of ions probably plays little part in the isothermal decomposition. This is supported by the conductance ( $10^{-12}$  ohm<sup>-1</sup> cm<sup>-1</sup> at 540°K) being of a similar order of magnitude to that of barium azide<sup>52</sup> and silver oxalate<sup>36</sup> at their respective decomposition temperatures. In these cases it was concluded that a mechanism of ionic transport could not be applied.

An attempt to measure the photo-conductance of a 'film' of  $\text{KIO}_4$  on a silica glass plate, with fused platinum electrodes (Fig. 2c), failed due to the resistance of the film being greater than that of the silica plate.



3.

Discussion

Darwin<sup>53</sup> was one of the first to realise that a crystal is not a perfectly ordered array of lattice points, but is in fact a mozaic structure. These minute blocks of perfect crystal, of micron dimensions, are in imperfect alignment with each other. Darwin's 'mozaic model' was required to explain the observed intensity of the X-ray diffraction spots from a crystal.

The physical picture of real crystals is now reasonably well established<sup>35</sup>, in terms of crystal dislocations and lattice defects. A comprehensive review of dislocation theory is given by Cottrell<sup>54</sup> although this mainly deals with metals. It is considered that crystals greater than ca 100  $\mu$  in linear dimensions are divided into grossly disorientated regions by subgrain boundaries that are about 10  $\mu$  apart. These boundaries are probably two dimension arrays of edges and screw dislocations, containing impurities absorbed during growth and are sites of mechanical weakness and high reactivity. The subgrains are traversed by a random network of single dislocations which delineate the crystal into irregular mozaic blocks of dimensions less than a micron.

These mozaic blocks contain further crystal imperfections - Frenkel and Schottky defects, which lead to other localized regions of disturbance.

The presence of defects is required to explain many chemical and physical phenomena in the solid state. The transport of matter depends on the existence of structural imperfections, and

many electrical and optical properties of ionic crystals are attributed directly to the presence of defects in an otherwise ordered arrangement. The dislocation theory has been confirmed in the work of Hedges and Mitchell<sup>6</sup>. They showed that the precipitation of photolytic silver in silver bromide, marked out line networks in the interior of the crystal having all the expected characteristics of a dislocation system.

It is within this framework that the kinetics of thermal decompositions have been explained, Tompkins and his co-workers setting the basis for the use of dislocation theory in their work on silver oxalate<sup>36</sup> and mercury fulminate<sup>16</sup>.

The application of the above picture to potassium meta periodate indicates that the large crystals (300  $\mu$ ) contain an extensive network of subgrain boundaries. The small crystals (40  $\mu$ ) are approximately of subgrain size and probably have none, or very few, subgrain boundaries. The subgrains will be divided into mozaic blocks by a large array of single dislocations.

The chemistry of the reaction has been shown to be simple (2.1.). From a structural point of view tetragonal  $\text{KIO}_4$ <sup>47</sup> gives rise to monoclinic (pseudocubic)  $\text{KIO}_3$ <sup>46</sup>, although Goldschmidt<sup>55</sup> reported the cubic perovskite structure. The powder photographs obtained from analar  $\text{KIO}_3$  and from the decomposition product were identical and showed marked splitting of the lines, which would not occur if the three lattice parameters were equal as in a cubic structure; thus supporting the mono-clinic (pseudo-cubic) lattice. This also allows for the existence of the iodate ion in the solid, which

could not be the case in a pure perovskite structure.

The decomposition is one of the few reported that gives a single unambiguous solid phase. Generally exothermic reactions of the type  $A_s \rightarrow B_s + C_g$ , result in the solid phase B being of uncertain composition, e.g. mercury fulminate, or having two or more components, e.g. potassium permanganate, while for the azides the solid phase is metallic. It is also worth noting that the cation  $K^+$  remains unaltered during the decomposition.

With the apparent simplicity of the chemical and physical nature of the reaction it might be expected that the kinetics would follow a straightforward course; this has not proved to be the case.

#### Kinetics of the decomposition

From the Arrhenius activation energy plots, given in 2.6.6., table 28 is constructed showing the logarithm of the rate constants at  $540^\circ K$  for the different stages in the decomposition of materials A - K. The numbers in brackets represent the relative increase in the rate constants for the pairs of material.



Table 28

| Material          | Pre-acceleration     |                                 | acceleration       |                       | decay                |                      |
|-------------------|----------------------|---------------------------------|--------------------|-----------------------|----------------------|----------------------|
|                   | $\log_{10}^{+5} R_L$ | $\frac{1}{2}\log_{10}^{+4} k_2$ | $\log_{10}^{+2} k$ | ' $\alpha$ ' at $R_M$ | $\log_{10}^{+3} R_M$ | $\log_{10}^{+3} k_3$ |
| A                 | 0.5<br>(1.4)         | -                               | 0.6<br>(4.0)       | 0.5                   | 0.9<br>(2.0)         | 0.8<br>(1.25)        |
| B<br>(aged)       | 0.65                 | -                               | 1.2                | 0.2                   | 1.2                  | 0.9                  |
| C                 | 0.5<br>(3.2)         | -                               | 0.7<br>(2.5)       | 0.5                   | 1.0<br>(2.2)         | 0.9<br>(1.6)         |
| D<br>(pre-irrad.) | 1.0                  | -                               | 1.1                | 0.4                   | 1.33                 | 1.1                  |
|                   | $\alpha_0$           |                                 |                    |                       |                      |                      |
| F                 | 0.0005               | 1.0<br>(1.0)                    | 0.75<br>(1.6)      | 0.5                   | 1.1<br>(1.4)         | 0.95<br>(1.25)       |
| G<br>(aged)       | 0.0007               | 1.0                             | 0.95               | 0.5                   | 1.25                 | 1.05                 |
| H                 | 0.00035              | 0.9<br>(1.8)                    | 0.75<br>(2.2)      | 0.5                   | 1.1<br>(1.8)         | 0.95<br>(1.4)        |
| K<br>(pre-irrad.) | 0.0007               | 1.15                            | 1.1                | 0.5                   | 1.35                 | 1.1                  |

Ageing and pre-irradiation with ultraviolet light figure prominently in the experimental work and thus a general discussion is now given of the effects.

Potassium metaperiodate does not undergo any chemical decomposition during storage, there being no visible difference between fresh and aged material for either the large or small crystals.



The different kinetics of the isothermal decomposition were the only measure of the physical changes that occurred with the passage of time.

Ageing in the case of mercury fulminate<sup>16</sup> was clearly chemical in nature, while for ammonium dichromate, Simpson, Taylor and Anderson<sup>29</sup> reported a change in the physical appearance of the crystals together with a possible loss of water, which resulted in the pre-acceleration period being reduced to zero.

For potassium metaperiodate the pre-acceleration periods are unaffected by ageing, which appears to principally affect the bulk of the decomposition (table 28), that is the acceleration and decay periods. As the water content of the crystals is less than 0.01%, it is not considered that this is responsible for the ageing effect. This was confirmed by storing aged crystals in the presence of water vapour for two weeks, after which no change was observed in the decomposition kinetics.

Ageing is probably a physical change, closely connected with imperfections, such as the system of dislocations, present in the bulk of the crystals. Tompkins and Young<sup>35</sup> have discussed the effect of physical ageing on the azides. The azides decompose by a mechanism that involves an aggregation of the cations to form a metallic nucleus, on the other hand at all stages in the decomposition of potassium metaperiodate an ionic lattice is present and the cation is unaffected by the decomposition. Their specific ideas are not applicable to potassium metaperiodate, but the concept of ageing and allied phenomena as involving lattice imperfections is of general use.

The effect of pre-irradiation with ultraviolet light on the subsequent thermal decomposition of solids is not uniform and a wide range of results have been reported. Pre-irradiation has no effect on the decomposition of potassium<sup>38</sup>, cesium<sup>62</sup> and rubidium<sup>76</sup> permanganates and on ammonium dichromate<sup>29</sup>. For mercury fulminate<sup>16</sup>, silver oxalate<sup>36,37</sup> and potassium azide<sup>58</sup> there is an appreciable photodecomposition during the pre-irradiation and the rate of the thermal decomposition is greatly increased. In the case of silver oxalate and potassium azide anionic vacancies are formed, which, at least in part, are responsible for the differences in the subsequent decomposition. This, of course, cannot occur in, what is by comparison, the insignificant photo-decomposition of potassium metaperiodate, as the metaperiodate ion is transformed into the iodate ion, an anionic vacancy is not created during the decomposition.

For potassium metaperiodate the effect is not limited to the pre-acceleration period as in lithium aluminium hydride<sup>17</sup>, but extends to all stages of the decomposition. The rate constants for the pre-acceleration and acceleration periods are substantially increased and to a lesser degree those for the decay period. The effect on the acceleration period indicates that there are changes in the bulk of the crystal, perhaps of a similar nature to those occurring during ageing.

In solution the periodate ion shows maximum absorption at 220  $\mu$ <sup>56</sup>; if this wavelength is responsible for the photolytic decomposition in the solid (2.4.), it is unlikely to penetrate a distance of more than a few lattice spacings<sup>57</sup>. The bulk

effect of the irradiation is probably due to longer wavelengths and may not then be the result of actual decomposition.

Effects associated with the yellow colouration observed after irradiation are not considered to have an effect on the subsequent decomposition<sup>58</sup> due to the rapid disappearance of the colour on heating.

It is essential to discuss the kinetics for the different materials as a unit, so that a physical picture can be developed that can accommodate both large and small crystals. As the exp. section has shown this has been achieved with the framework of the Prout-Tompkins equation for the acceleration period and the contracting sphere equation for the decay period of the reaction. These equations are considered to give the best representation of the experimental results, bearing in mind the wide diversity of materials examined.

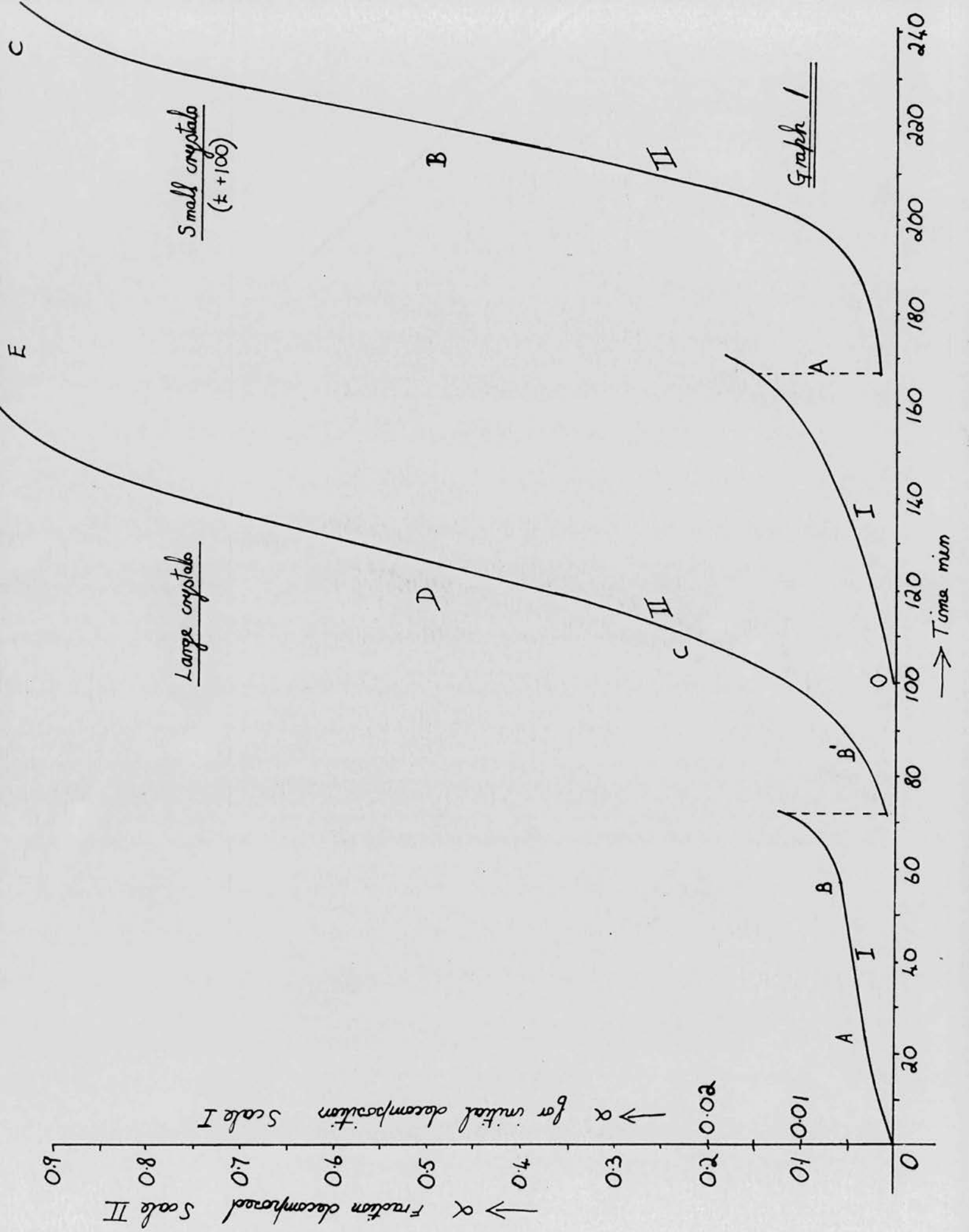
The reaction has been divided for convenience into three stages (Graph 1), firstly the pre-acceleration period, secondly the acceleration or autocatalytic period and thirdly the decay period.

(1) The pre-acceleration period

For both large and small crystals the reaction before the main acceleration stage is considered to be due to the growth of the new phase, potassium iodate, at either internal or external surfaces of the crystals.

For the large crystals visual observations (2.5.) clearly







showed a distinct change in the mechanism at the end of the linear stage AB at  $\alpha = \text{ca } 0.005$ , where vigorous decrepitation set in. Preceding AB there was an initial reaction, stage OA, which was completed at  $\alpha = \text{ca } 0.003$  and had an activation energy of approximately  $45 \text{ kcal mole}^{-1}$  indicating a chemical reaction and not the desorption of gaseous products. This is considered to be decomposition at some of the subgrain boundaries (the internal surfaces) which creates a constant area interface that progresses into the subgrains giving rise to the linear stage AB. This process would correspond to the beginning of a contracting envelope mechanism. The extent of this reaction is reasonably independent of ageing and pre-irradiation, terminating at  $\alpha = 0.005$ , but the magnitude of the rate constant  $R_L$  is substantially affected.

Materials A and C, the two similar batches of fresh crystals, have the same rate constant (see table 28) and thus a similar number of subgrain boundaries. This is not unreasonable as the crystals were prepared by the same procedure.

Ageing only slightly increases this rate and the wide scatter of points on graph 22 (2.6.6.) suggests that this is probably insignificant. Pre-irradiation more than doubled the rate and as it caused a small decomposition of the solid (2.4.) its effects seem to be, at least in part, one of nucleation at or near subgrain boundaries. The effect of irradiation in the constant rate reaction is similar to that found in thallos bromate<sup>59</sup>.

Graph II (2.6.2.) shows a positive deviation from the

Prout-Tompkins equation, for the irradiated material below

$\alpha = 0.06$ , as compared with the unirradiated as seen in graph 10, where the Prout-Tompkins acceleration period starts directly after the linear period. This combined with the visual observation that the rapid break up of the crystals did not begin until  $\alpha = 0.05$ , indicates that pre-irradiation introduces a further mechanism prior to the acceleration.

A power law with  $n = 4$ ,  $(\alpha - \alpha_L) = K_4(t - t_0)^4$  graph 9 (2.5.2.), adequately fits the results from the end of the linear period to the start of the acceleration period. As ' $t_0$ ' is approximately zero the mechanism starts from the beginning of the decomposition. This equation when interpreted within the concepts of Avrami<sup>23</sup> leads to three dimensional growth of nuclei, with a linear production of growth nuclei from germ nuclei. Thus irradiation produces germ nuclei which are converted at a constant rate to growth nuclei, by the limiting case of the exponential law<sup>60</sup> with a low probability of conversion.

Pre-irradiation of the large crystals produces two initial effects, firstly nucleation of subgrain boundaries leading to a higher rate for the linear stage due to an increased number of subgrain boundaries which decompose. This would be expected to lead to a higher value of  $\alpha_L$ , but this reaction is swamped by the second effect, viz. the power law growth from the germ nuclei. The contribution to ' $\alpha$ ' by this mechanism is small during the linear stage; for example in run D4 in the first 80 minutes the fractional decomposition due to the power law growth is 0.0002 about 10% of that from the constant rate reaction.



In turn growth from these nuclei is swamped by the Prout-Tompkins mechanism.

The surface area of the small crystals is a factor of 10 larger than that for the large crystals, for a given mass. This, combined with the probable absence of subgrain boundaries, brings into prominence the external surface.

Visual observations gave no indication as to the presence of a pre-acceleration stage. But from the appearance of the ' $\alpha$ ' - ' $t$ ' curves, for example graph 1, the first 2% of the reaction is completed in 50% of the total reaction time, a marked indication of an initial slow reaction. This is supported by the positive deviation from the Prout-Tompkins equation below  $\alpha = 0.05$  in Graphs 17 (2.6.4.) and 21 (2.6.5.).

This initial decomposition up to  $\alpha = 0.03$  was adequately fitted by a power law with  $n = 2$ , i.e.  $\alpha = k_2(t - t_0)^2$ . This process is consistent with the two dimensional growth on the surface of the crystal of a fixed number of growth nuclei present at the start of the decomposition. The large negative intercepts ' $t_0$ ' on the time axis of the plot of  $\alpha^{1/2}/t$  given in tables 23 - 26 is interpreted as due to a rapid initial growth of these nuclei as in silver oxide<sup>21</sup>, anhydrous barium, styphnate trihydride<sup>61</sup> and cesium permanganate<sup>62</sup>. The value of ' $\alpha$ ' at  $t = 0$  is  $\alpha_0 = k_2 t_0^2$ , and is a measure of the number of nuclei present.

From table 28 it is seen that the rate constant  $k_2^{1/2}$  for the normal growth of these nuclei is the same before and after ageing, that is, for materials F and G respectively, and correspondingly

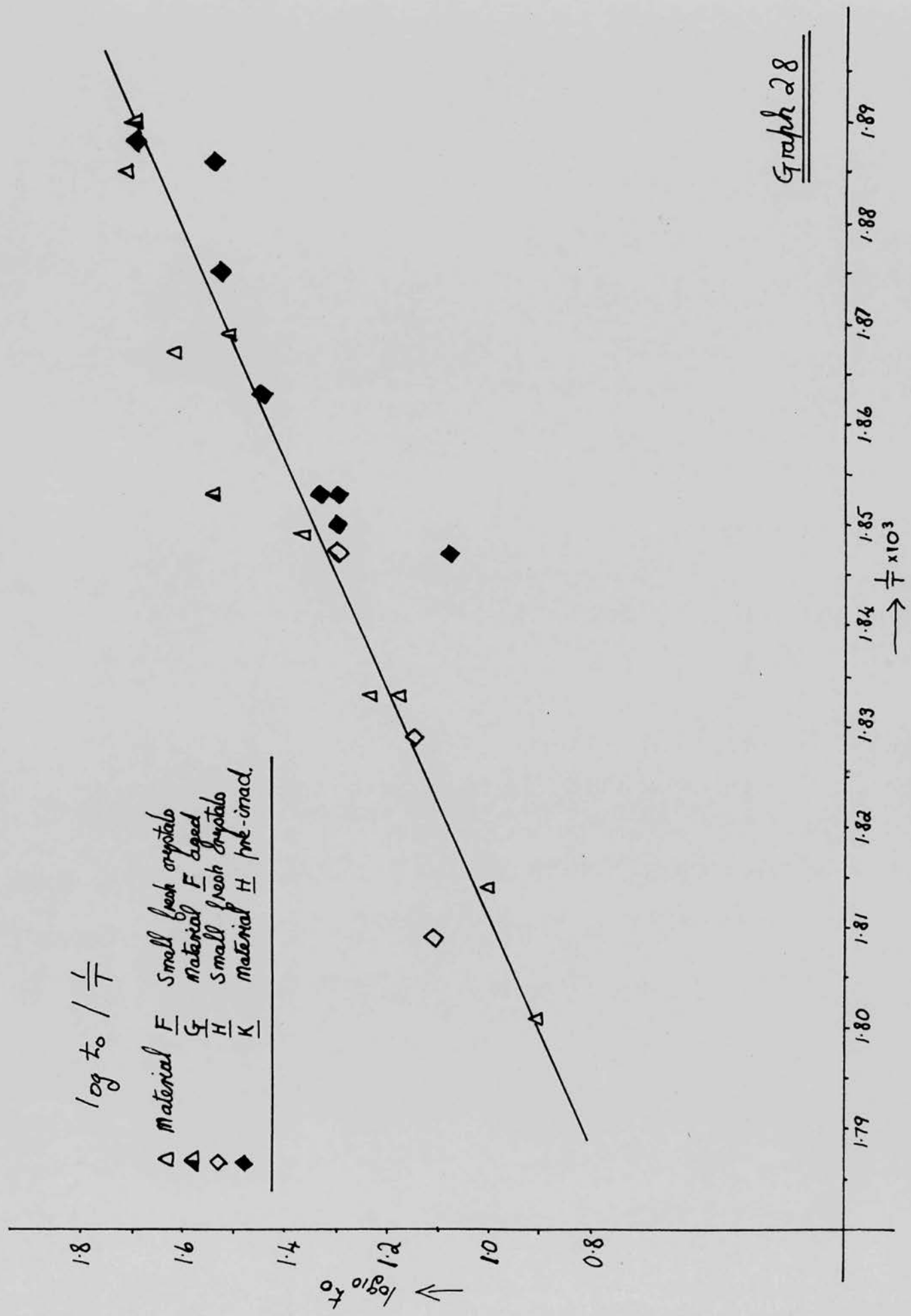
the values of  $\alpha_0$  are approximately the same. Assuming the actual rate of growth of the interface is constant regardless of ageing (this is almost certain to be true) the equivalence of the experimental rate constants entails a similar number of nuclei initially present on the surface. It is therefore concluded that the surface of the crystal is unaffected by ageing.

The rate constant for the second batch of small crystals, material H, is 20% lower than that for the first batch, correspondingly the value of  $\alpha_0$  is reduced from 0.0005 to 0.00035. Both these facts are indicative of a decrease in the number of surface nuclei in the second batch. This is not surprising as the surface of the crystals will be highly dependent on the conditions under which crystallisation took place, and although the same general procedure was used, the rate of rapid cooling was not strictly controlled.

Pre-irradiation of the fresh material increased the rate constant by about 80% and doubled the value of ' $\alpha_0$ ', this being presumably entirely due to the nucleation of the surface during irradiation. This is neatly confirmed by noting that the estimated fractional decomposition due to the irradiation, 0.00035, is identical to the increase in the value of ' $\alpha_0$ '. Thus the surface effect of irradiation is to produce growth nuclei of potassium iodate.

The constant ' $t_0$ ' represents the time of rapid growth and should be independent of the number of nuclei. To ascertain the truth of this statement the ' $\log t_0$ ' for the various materials was plotted against the reciprocal of the temperature (graph 28)





Graph 28

from which it is seen that the points lie scattered about a single line. Thus ' $t_0$ ' is independent of the number of nuclei as is expected. The activation energy deduced from the slope of this line is  $41 \pm 7$  kcal mole<sup>-1</sup> and is similar to that found for  $k_2^{\frac{1}{2}}$ , ( $41 \pm 4$  kcal mole<sup>-1</sup>). This is demanded by the constancy of  $k_2 t_0^2$ , as the number of nuclei ' $\alpha_0$ ' is not temperature dependent.

Thus ageing, pre-irradiation and mode of preparation have no effect on the rate of rapid growth, but pre-irradiation and mode of preparation do affect the number of nuclei.

The activation energy for the constant area interface reaction in the large crystals is  $50 \pm 5$  kcal mole<sup>-1</sup> which is higher than that for the bulk growth of  $46 \pm 4$  kcal mole<sup>-1</sup>. As both these values lie within the respective errors it is perhaps not a real difference. Generally the values reported in the literature for the activation energy of the pre-acceleration stage are lower than those for the acceleration stage, as is the case for the small crystals.

At the end of the pre-acceleration stage the large crystals are internally divided into subgrains by the decomposed material. On the other hand, the small crystals, which are about subgrain size, have their external surfaces covered by product. Thus the small and large crystals are in a similar physical state prior to the acceleration stage; although in the large crystals the main mass of the decomposed material is 'sandwiched' between unreacted material, while for the small crystals the product has only one

interface with the unreacted material.

(2) The acceleration period

The mechanism for the acceleration stage has to be consistent with both the pre-acceleration stage and decay stage. The decay stage for the different materials is in all cases best expressed by the contracting sphere mechanism. Thus at the end of the acceleration stage it is necessary to have small particles of periodate completely covered by reaction product.

The Prout-Tompkins equation reasonably represents the acceleration stage for large, small, fresh, aged and pre-irradiated material as seen from the respective graphs in the experimental sections 2.6.1. - 2.6.5. This equation can represent a mechanism by which the reaction spreads through the crystal by means of 'branching planes' of decomposed material as originally proposed by Prout and Tompkins<sup>27</sup> for potassium permanganate and restated by Herley and Prout<sup>62</sup> for the decomposition of cesium permanganate. The controlling factor in the rate of decomposition is the probability of branching 'k'.

Branching of the reaction interface occurs when the interface meets a dislocation in the crystal as was postulated for silver oxalate<sup>36</sup>. Equally, the stress set up at the reaction interface due partly to the different lattice dimensions of the reactant and product, cause cracking, probably at dislocations, these being points of weakness in the crystal lattice. The reaction then spreads down the cracks and the process is repeated. The branching of the interface does not continue unhindered for interference sets



in when a 'branching plane' meets a decomposed surface. The interference of the branching leads to the Prout-Tompkins equation, if there were not interference a pure exponential relationship would exist as originally put forward by Garner and Hailes<sup>14</sup>.

The branching and thus the acceleration of the reaction cannot start until the necessary stresses have been created at the interface of the two phases. Prout and Herley<sup>63</sup> have reported that the Laue photographs of partially decomposed crystals of potassium and silver permanganate show asterism of the spots. This is interpreted as demonstrating the existence of strains in the crystals, which leads to the Prout-Tompkins mechanism. The disintegration of the large crystals of potassium metaperiodate follows the same pattern as that for potassium permanganate. The decrepitation which begins at the end of the linear stage (2.5.) is probably not a necessity of the mechanism but a result of it.

For potassium metaperiodate the stresses are produced by the decomposition of the internal and external surfaces which occurs in the pre-acceleration stages. For the decomposition of anhydrous barium styphnate trihydrate, Tompkins and Young<sup>61</sup> have proposed a similar mechanism of branching of the reaction interface due to stresses set up in the early stages of the decomposition.

Decomposition via dislocations will leave the crystal at the end of the acceleration stage divided into a large number of small particles, probably about the size of mozaic blocks. As the surfaces of the particles are covered by product the contracting sphere mechanism can now operate resulting in the start of the

decay stage.

The variation in the rate constant ' $k_3$ ' for the decay stage, is solely due to the number of particles present, and thus the degree of branching, at the end of the acceleration stage. This will now be developed from first principles.

The fraction of the particles decomposed, assuming spherical symmetry is,

$$\frac{\alpha - \alpha_1}{1 - \alpha_1} = \frac{\frac{4}{3} \pi a^3 - \frac{4}{3} \pi [a - m(t - t_0)]^3}{\frac{4}{3} \pi a^3}$$

where ' $\alpha$ ' is the fraction of the crystal decomposed, as measured experimentally,

' $\alpha_1$ ' is the fraction of the crystal decomposed at the start of the contracting sphere mechanism,

' $a$ ' is the radius of the spherical particles at ' $t_0$ ' the time at the start of the contracting sphere mechanism,

' $m$ ' is the linear rate of growth of the interface into the centre of the crystal and

$$\frac{\alpha - \alpha_1}{1 - \alpha_1}, \text{ is the fraction of the } \underline{\text{spherical particle}}$$

decomposed at time ' $t$ '.

Therefore rearranging,

$$\alpha = 1 - \left[ (1 - \alpha_1)^{\frac{1}{3}} - \frac{m}{a}(1 - \alpha_1)^{\frac{1}{3}}(t - t_0) \right]^3 \quad (1)$$

$$\text{Thus } 'k_3' = \frac{m}{a}(1 - \alpha_1)^{\frac{1}{3}} \quad (2)$$

where ' $k_3$ ' was the experimentally found rate constant. If the total volume ' $V_0$ ' of the particles at ' $t_0$ ' is  $(1 - \alpha_1) V_0$  and

the number of particles is 'n', ['V' is volume of undecomposed crystals]

$$\frac{4}{3} \pi a^3 = \frac{V}{n} = \frac{(1 - \alpha_1)V}{n}$$

$$\therefore \frac{(1 - \alpha_1)^{\frac{1}{3}}}{a} = \left(\frac{4\pi}{3V}\right)^{\frac{1}{3}} n^{\frac{1}{3}} \quad (3)$$

combining equations (2) and (3)

$$k_3 = \left(\frac{4\pi}{3V}\right)^{\frac{1}{3}} m n^{\frac{1}{3}} \quad (4)$$

Thus assuming a constant rate of growth 'm' the value of 'k<sub>3</sub>' depends solely on the number of particles.

Two factors characterize the acceleration period, firstly the rate constant 'k' (the branching coefficient), and secondly the extent of the acceleration period, as given by 'α' at the maximum rate.

For both large and small fresh crystals, A C F and H, the maximum rate occurs at α = 0.5, but the value of 'k' (table 28) varies slightly. This variation in 'k' is paralleled by a similar change in the rate constant for the decay stage. This is consistent with the idea that the degree of branching governs the number of particles at the end of the acceleration stage. From the general similarities in the values of 'k' and 'k<sub>3</sub>' for these materials, the conclusion can be drawn that the mosaic dislocation structures of the small crystals resembles that of the subgrains in the large crystals.

The effect of 18 months storage on the large crystals A is



very pronounced with a 300% increase in 'k' and the maximum rate brought forward from  $\alpha = 0.5$  to 0.2, but the rate constant for the decay stage is only increased by 25%. Ageing is considered to facilitate the branching process by reducing the stresses required to form a new interface at a dislocation. Thus the crystal is broken into small particles at an earlier stage in the decomposition, as a lower degree of decomposition of the interface is required to produce the branching.

The 25% increase in the rate constant for decay indicates an increase in the number of imperfections in the lattice at which branching occurs leading to a larger number of particles in the decay stage and thus a factor rate.

The constant 'k' for the aged small crystals G is only increased by 60% as compared with that for the fresh small crystals F and H, and the constant 'k<sub>3</sub>' is increased by 25%, the maximum rate occurring at the same value of  $\alpha = 0.5$ . The increased rate of decay indicates an increase in the number of particles as in the aged large crystals and thus a larger number of imperfections have participated in the acceleration, but as this continues to  $\alpha = 0.5$  the same stresses appear to be necessary to produce the branching unlike the case of the large crystals.

The pre-irradiated large crystals D show an increase in 'k' of 150% but a slight decrease in the extent of the acceleration period, the maximum rate occurring at  $\alpha = 0.4$ . As the rate constant for decay has increased by 60%, irradiation has created branching points combined with a slight lowering of the stresses

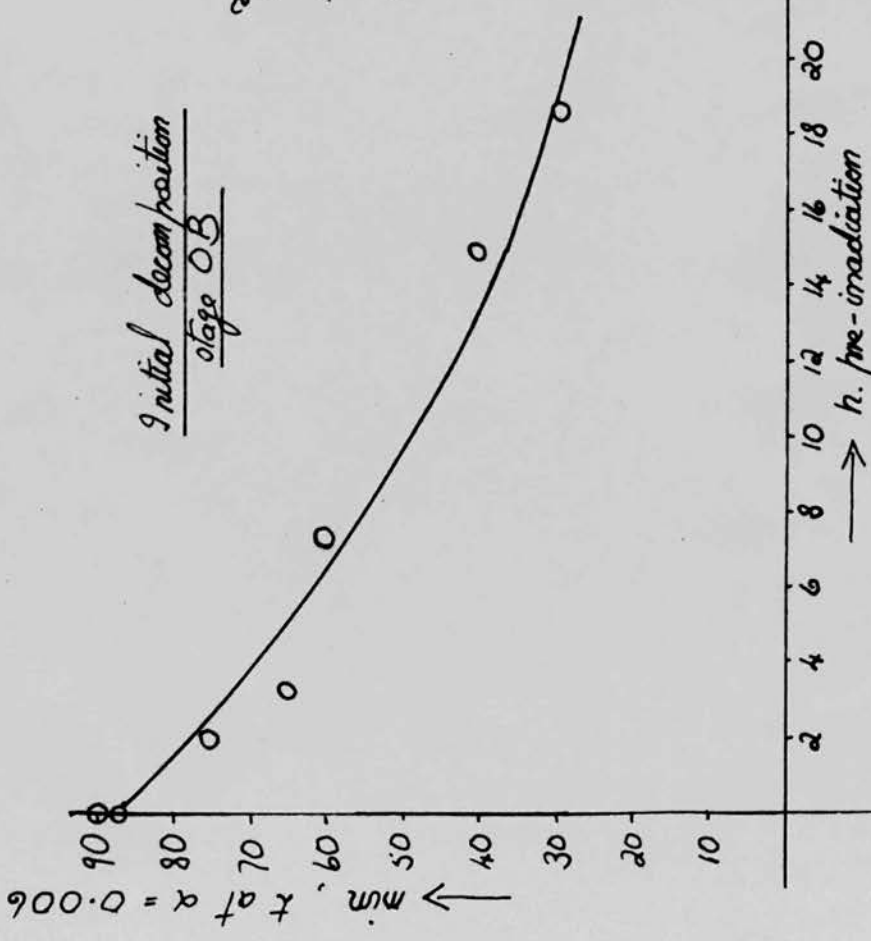
required for branching leading to an earlier maximum rate. The value of 'k' after pre-irradiation is similar to that for aged crystals, suggesting that irradiation produces imperfections of a similar nature to those present in the crystal after ageing.

The rate constants for the acceleration and decay stages of the pre-irradiated small crystals K are identical to those of the pre-irradiated large crystals. This is to be expected as the small and large crystals had identical pre-treatment. The acceleration stage for the small crystals continues to  $\alpha = 0.5$  and is not lowered as is the case for the large crystals. Thus the result of pre-irradiation of the small crystals is confined to the production of branch points, which is parallel to the limited effect of ageing in the small crystals.

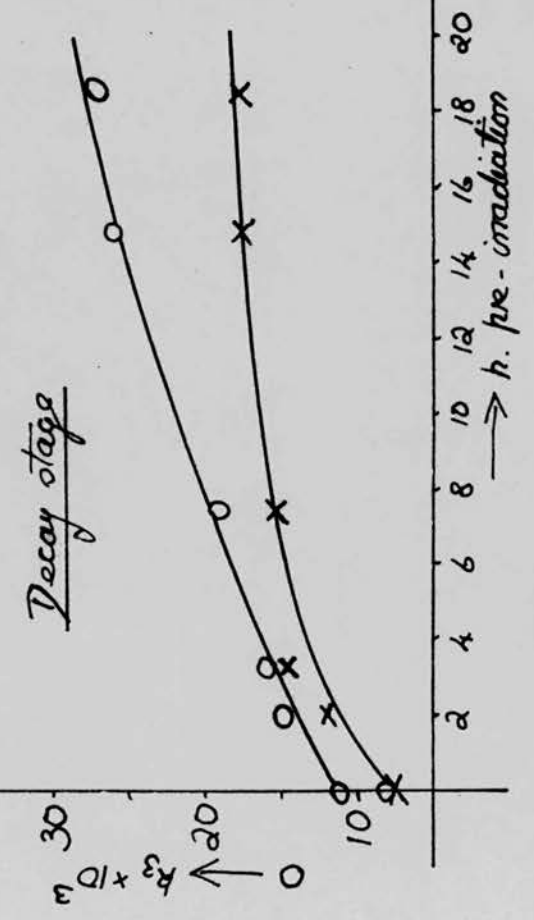
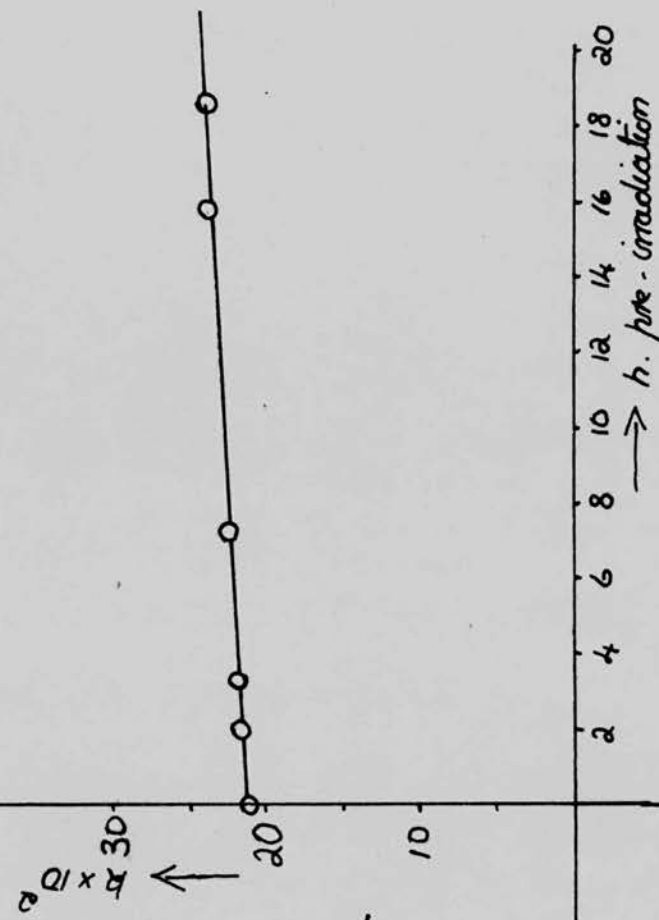
The fact that the small crystals do not appear to show a shortening of the acceleration stage after ageing and pre-irradiation, as is observed for the large crystals, is perhaps due in some measure to the actual difference in size. The small crystals are  $\frac{1}{400}$ <sup>th</sup> the volume of the large.

Material E was crystals made in a similar manner to A and C but stored for one year and then pre-irradiated for varying lengths of time. Graph 29 illustrates the effects on the subsequent decomposition as a function of the length of pre-irradiation.

The most interesting feature is that the rate of acceleration, as measured by the branching coefficient 'k', is nearly constant regardless of the length of pre-irradiation. The effects of the irradiation is to extend the acceleration stage from  $\alpha = 0.25$  to



Acceleration stage



$\alpha$  at end of accel. stage

0.5 X  
0.4 X  
0.3

Material  $\underline{E}$  crystal after storage for one year, showing the effect of varying lengths of pre-irradiation on the subsequent decomposition.



0.45 and increase the rate of decay. This fits into the previous picture that irradiation produces imperfections similar to those present in aged crystals; the resulting increase in the degree of branching leads to a larger number of particles and thus a faster rate of decay.

The time for the initial decomposition decreases with length of irradiation corresponding to the rate increases found for material D. Graph 14 (2.6.3.) illustrates that for run E 15 the power law growth has been introduced before the acceleration stage, confirming the results for material D.

### (3) The decay stage

As is observed from graphs 6 (2.2.1.), 12 (2.2.2.), 18 (2.2.4.) and 22 (2.2.5.) the decay stage is well expressed in terms of the contracting sphere equation. Although for the aged small and large crystals there is a tendency for the equation to fail at  $\alpha > 0.85$  probably due to collapse of the interface and uni-molecular decay setting in.

The particles that are created by this mechanism are formed as a result of the branching planes of the acceleration stage dividing the crystal into roughly similar particles of probably  $< 1 \mu$  - mozaic block size - with their surfaces covered by product molecules. This reaction interface then contracts into the particle with an activation energy for the linear progression of the interface of  $46 \pm 4 \text{ kcal mole}^{-1}$ , which is the same activation energy as that found for the acceleration stage. These 'mozaic blocks' contain a few or no dislocations so there

can be no increase in surface area by further branching. Thus the rate is entirely dependent on a fixed surface decreasing in area following the equation  $\frac{d\alpha}{dt} = A(1 - \alpha)^{\frac{2}{3}}$  which when integrated gives equation (1).

From a comparison of the rate constants ' $k_3$ ' for the decay stage and the value of ' $\alpha$ ' at the maximum rate, of any pair of materials, it is possible to deduce the change in the maximum rate. The rate of decomposition at the start of the decay stage is equal to the maximum rate, therefore  $R_M = \gamma a^2 n$  where ' $\gamma$ ' is a constant. Combining this with equation (3)

$$R_M = \gamma (1 - \alpha_i)^{\frac{2}{3}} n^{\frac{1}{3}} \quad (5)$$

Using the data in table 28 the maximum rates are compared for the different materials, as represented by the letters in brackets.

$$\begin{aligned} R_{M(A)}^{(B)} &= \frac{1 - \alpha_{i(B)}^{\frac{2}{3}}}{1 - \alpha_{i(A)}^{\frac{2}{3}}} \times \frac{n(B)^{\frac{1}{3}}}{n(A)^{\frac{1}{3}}} \quad (6) \\ &= \frac{1 - 0.2^{\frac{2}{3}}}{1 - 0.5^{\frac{2}{3}}} \times 1.25 \end{aligned}$$

where  $\frac{n(B)^{\frac{1}{3}}}{n(A)^{\frac{1}{3}}} = \frac{k_3(B)}{k_3(A)}$  from equation (4)

thus  $R_{M(A)}^{(B)} = 1.73.$

Table 29 gives the calculated and experimental values of this ratio.

Table 29

| Material      | Ratio of $R_M$<br>calculated from (6) | Ratio of $R_M$<br>experimental |
|---------------|---------------------------------------|--------------------------------|
| $\frac{B}{A}$ | 1.7                                   | 2.0                            |
| $\frac{D}{C}$ | 1.8                                   | 2.1                            |
| $\frac{G}{F}$ | 1.25                                  | 1.4                            |
| $\frac{K}{H}$ | 1.4                                   | 1.8                            |

The agreement between the calculated and the experimental values is within 20%. This is considered reasonable bearing in mind the assumption that the particles are spheres all of equal size. The agreement is a general indication that the mechanism proposed is along the right lines although undoubtedly not as simple.

Further confirmation that the crystals break up into small particles was obtained from X-ray powder photographs. A 'powder photograph' of the uncrushed small crystals gave as expected a few spots, but a photograph of these crystals after decomposition resulted in lines as in a normal powder photograph. The decomposed crystals had the same external form as the undecomposed (2.5.). Thus decomposition internally divides the small crystals into disorientated parts, as would have been achieved by crushing.



The acceleration stage has been expressed in terms of the Prout-Tompkins equation, but the experimental results on this stage are not entirely conclusive. The kinetics for the large crystals A is better expressed by a power law with  $n = 3$ , corrected for the initial linear growth, although after ageing (B) the Prout-Tompkins equation is probably superior, generally fitting immediately after the linear stage. The Prout-Tompkins equation as derived is only strictly applicable when the maximum rate is at  $\alpha = 0.5$ , but it reduces to  $\alpha = A \exp(kt)$  for values of ' $\alpha$ ' up to 0.2. Thus for material B it would be truer to say that there was an exponential relationship, indicating non-interference of the branching. As it has been previously argued that there are nearly the same number of branch points (imperfections) in the crystals before and after ageing, but as there is interference in fresh material and not in aged, this supports the contention that the ease of branching at these imperfections is facilitated by ageing.

In graphs 30, 31 and 32, the relative merits of the Prout-Tompkins equation and the power law with  $n = 3$ , are compared for large and small crystals before and after pre-irradiation and for the large crystals when aged. Generally the Prout-Tompkins is superior and for fresh large crystals C, the power law is not applicable.

The fit for the power law equation can be improved if the fraction subtracted from ' $\alpha$ ' is greater than that at the end of the pre-acceleration stage ( $\alpha_L$  and  $\alpha_p$  in this case), although there is little justification for this.

A power law with  $n = 3$  necessitates the formation at the

A21 Fresh large crystals

○ Prout-Tompkins factor

$$\log_{10} \frac{\alpha - \alpha_L}{1 - \alpha} / t$$

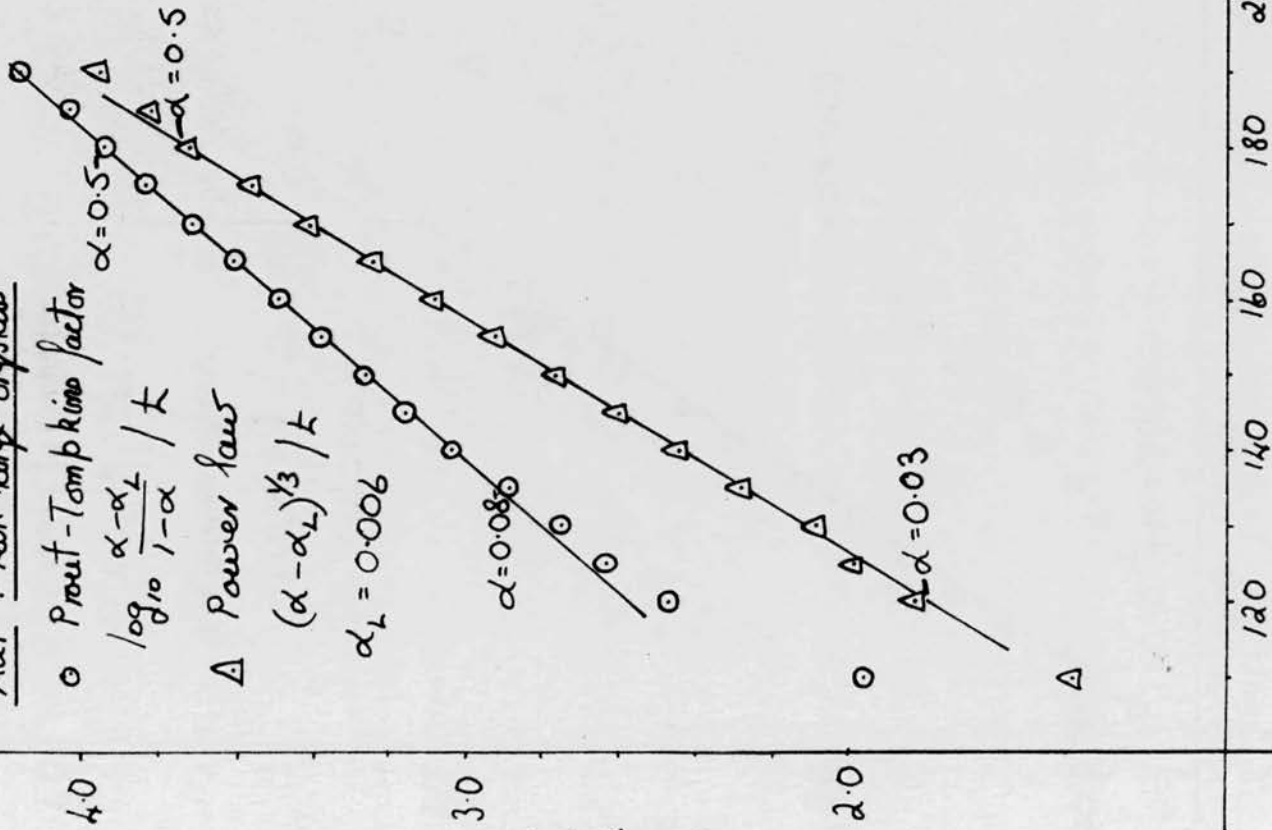
△ Power law

$$(\alpha - \alpha_L)^{1/3} / t$$

$$\alpha_L = 0.006$$

$$\alpha = 0.08$$

$$\alpha = 0.03$$



B3 Large crystals aged

○ PT factor

$$\log_{10} \frac{\alpha - \alpha_L}{1 - \alpha} / t$$

△ Power law

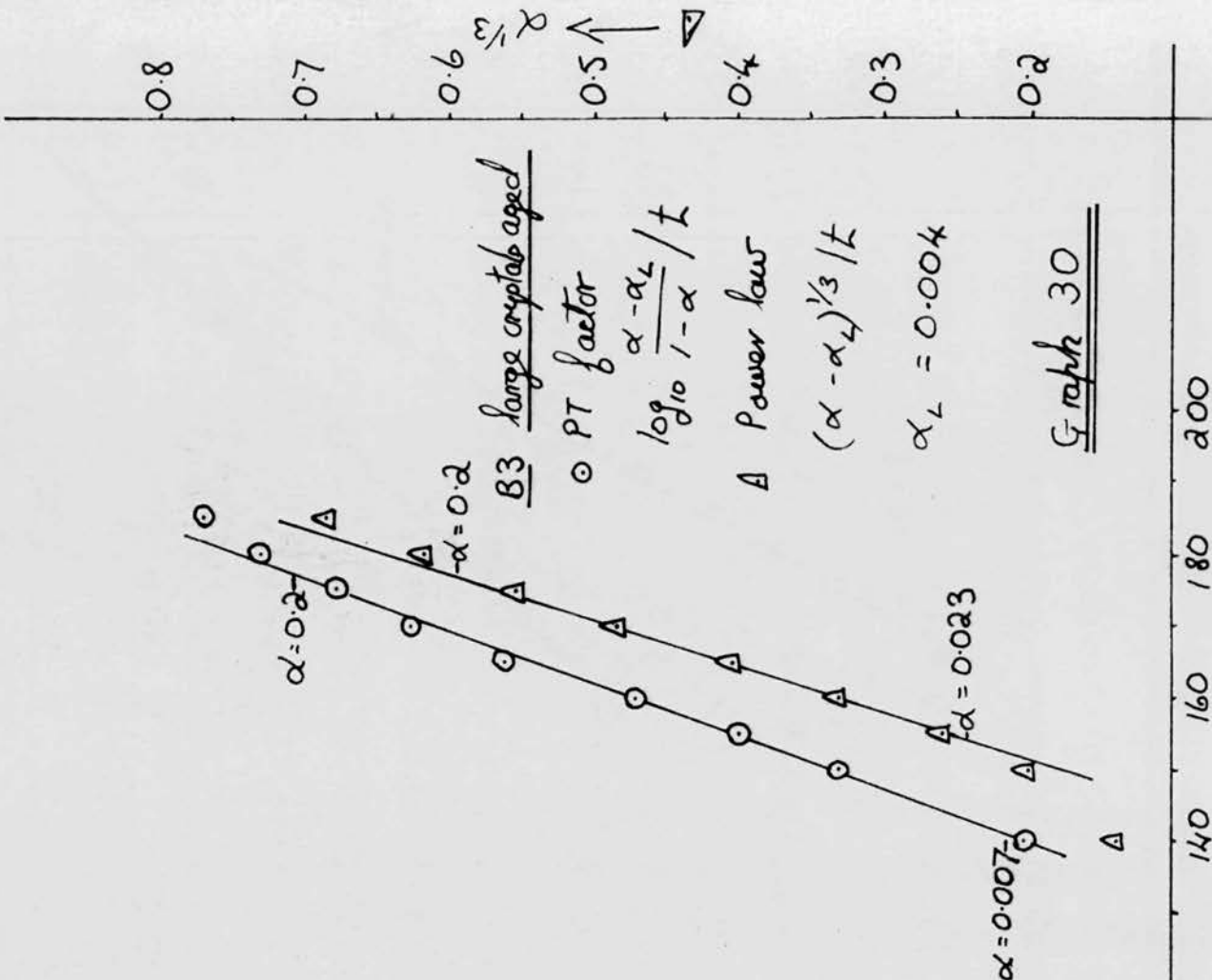
$$(\alpha - \alpha_L)^{1/3} / t$$

$$\alpha_L = 0.004$$

$$\alpha = 0.2$$

$$\alpha = 0.007$$

$$\alpha = 0.023$$



Graph 30

K3 small crystals pre-irradiated

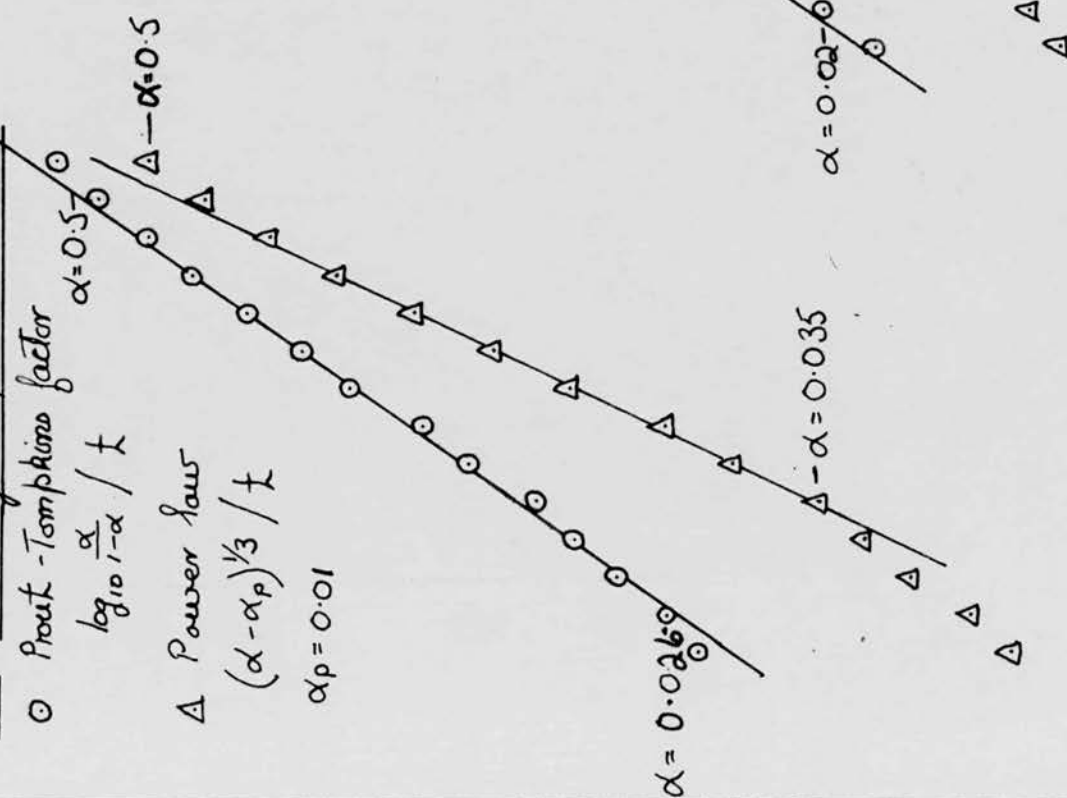
○ Prout-Tompkins factor  $\alpha = 0.5$

$\log_{10} \frac{\alpha}{1-\alpha} / t$

△ Power law

$(\alpha - \alpha_p)^{1/3} / t$

$\alpha_p = 0.01$



F28 small fresh crystals

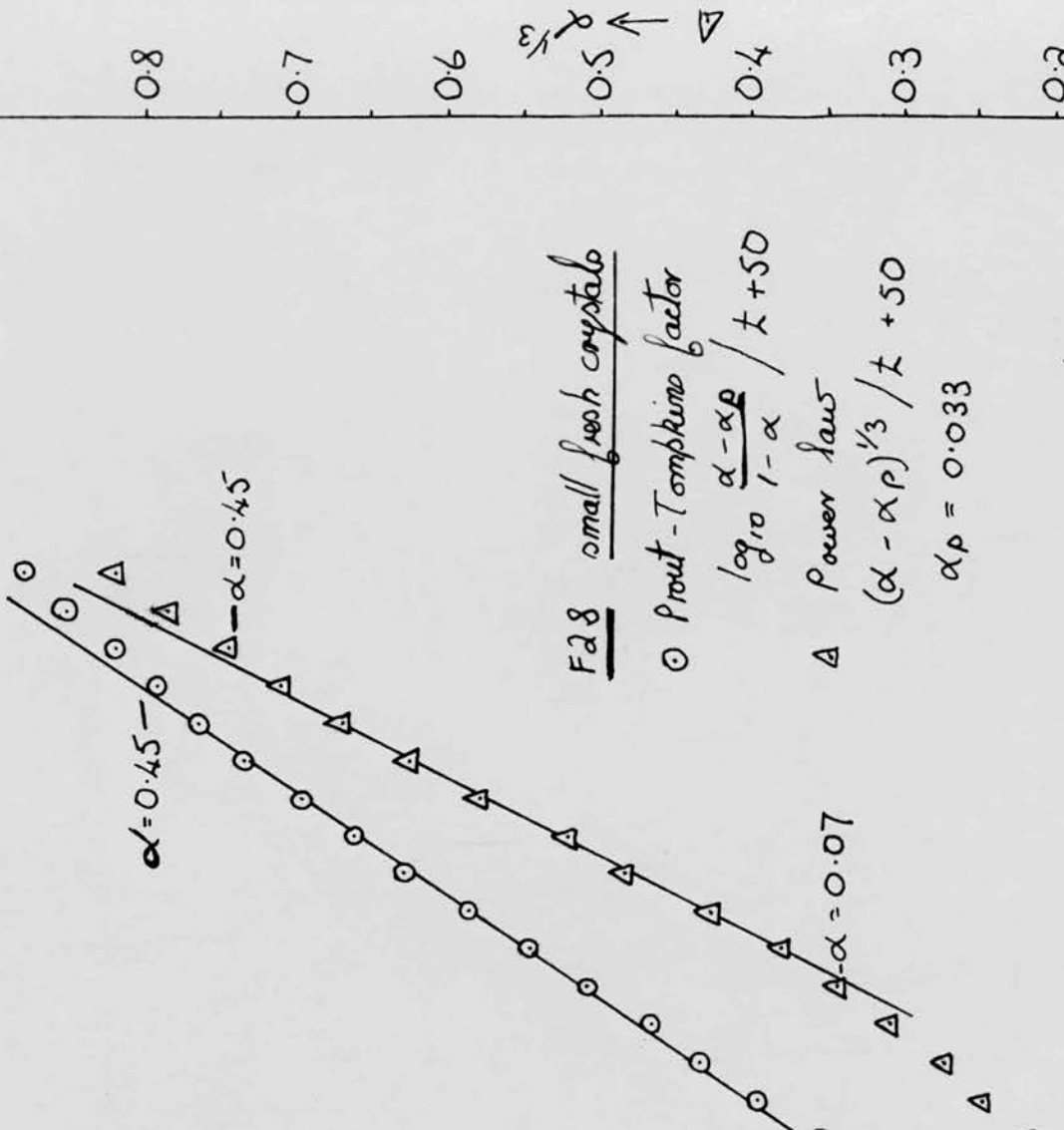
○ Prout-Tompkins factor

$\log_{10} \frac{\alpha - \alpha_p}{1 - \alpha} / t + 50$

△ Power law

$(\alpha - \alpha_p)^{1/3} / t + 50$

$\alpha_p = 0.033$



Graph 32

120 140 160 180 200 220 240 260 280 300 320 340  
 → time min



end of the pre-acceleration stage, of growth nuclei, which then grow at specific sites in the crystal and coalesce at the respective maximum rates for the different materials. If the nuclei were uniformly distributed throughout the crystal the maximum rate would always occur at the same fractional decomposition, independent of the number of nuclei. As this is not the case for large aged and pre-irradiated material, the nuclei must grow as specific sites which are decreased in number after ageing. The plot of  $\alpha^{1/3}/t$  gives intercepts on the time axis at  $\alpha = 0$  that are large and positive and correspond to the time at the end of the pre-acceleration stage. Thus all the nuclei are formed at one instant at the end of the pre-acceleration stage which is hard to visualise, more so as this constitutes one half of the total reaction time.

The Prout-Tompkins mechanism is thus preferred both from the kinetic analysis of the ' $\alpha$ ' - 't' curves and from the satisfactory manner in which the mechanism is in harmony with the overall picture of the decomposition.

In the course of the calculations the differential form of the Avrami equation  $\frac{dt}{d\alpha} (1 - \alpha) \ln(1 - \alpha) = \frac{1}{n} t$ , was considered to be a superior method of plotting the equation, compared with the normal form  $\ln [- \ln(1 - \alpha)] = n \ln t + C$ ; as it eliminates the necessity of plotting the logarithm of the time, with all the uncertainties that this involves. In run C 5 (page 30), the Avrami equation was found not to apply; the value of 'n' varied from 30 to 4 as the decomposition progressed.

Chemical mechanism of the decomposition

The overall reaction is



when this is combined with



it is found that



Thus the thermal breakdown of the metaperiodate ion into an atom of oxygen, requires approximately 50 kcal mole<sup>-1</sup> for the rupture of the iodine-oxygen bond. This is comparable to the activation energies found experimentally, suggesting that they have a direct relationship with the primary chemical act.

The kinetics of the decomposition have been explained in terms of the decomposition of an interface which increases in area due to branching during the acceleration stage and decreases in area by means of the contracting sphere mechanism during the decay stage. Two factors control the rate of the reaction, the rate of linear progression of the interface and the area of the interface. The Polanyi-Wigner equation,

$$\frac{dn}{dt} = N \nu \exp(-E/RT),$$

is an expression for the rate of decomposition of the interface where

$\frac{dn}{dt}$  is the number of molecules decomposing per second,

$N$  is the total number of molecules on the interface,

$\nu$  is the vibrational frequency responsible for the decomposition and is approximately equal to  $10^{13}$  sec<sup>-1</sup>, and  $E$  is the energy of

activation calculated from the temperature coefficient of the velocity of movement of the interface.

For the large crystals the area of the subgrain boundaries is the constant interface for the initial 'linear stage' constant rate reaction. A tentative estimate can be made of the area of the subgrain boundaries. If they are assumed to be  $10 \mu$  apart<sup>16</sup> and the crystal a cube of  $300 \mu$  in length, the area is ca  $2 \times 10^7 \mu^2$ . The area of a molecule is ca  $2 \times 10^{-7} \mu^2$  as calculated from the dimensions of the unit cell of 4 molecules with  $a = b = 5.75 \text{ \AA}$  and  $c = 12.63 \text{ \AA}$ <sup>47</sup>. Thus there are ca  $10^{14}$  molecules on the surface of the subgrain boundaries. In run A 46 (page 25) the fraction of the crystal decomposed per second was ca  $10^{-7}$  and as there are ca  $10^{17}$  molecules in a crystal (calculated from the dimensions and weight), the rate of decomposition was ca  $10^{10}$  molecules  $\text{sec}^{-1}$  at a temperature of  $530^\circ\text{K}$ . Using the Polanyi-Wigner equation with  $N = 10^{14}$ ,  $\nu = 10^{13}$ ,  $E = 50 \text{ kcal mole}^{-1}$  (page 50) and  $T = 530^\circ\text{K}$ , the rate of the reaction is equal to

$$\begin{aligned} \frac{dn}{dt} &= 10^{14} \times 10^{13} \times \exp(-50000/2 \times 530) \\ &= 10^7 \text{ molecules sec}^{-1}. \end{aligned}$$

This is not an unreasonable agreement with the experimental value of  $10^{10}$  molecules  $\text{sec}^{-1}$ , considering the approximations involved in estimating the interface area and the probable error in the activation energy. Thus the frequency factor ' $\nu$ ' would have to be  $10^{16}$  to bring the theoretical rate in line with the experimental.

The maximum rate is 300 times the constant rate for the



initial linear stage and assuming the same linear rate of progression of the interface there must have been a threehundred fold increase in the area of the interface. This is the expected increase in area if the subgrains are divided into particles 0.1  $\mu$  in linear dimensions. This is in excellent agreement with the expressed view that the Prout-Tompkins mechanism divides the crystal into small particles the size of mozaic blocks. The application of the Polanyi-Wigner equation to the beginning of the contracting sphere stage leads to the same result as found for the initial linear stage, both the rate and interface area being increased by ca 300. But the value of E is 46 kcal mole<sup>-1</sup> (page 50) so the frequency factor is  $10^{14-15}$ , which is in good agreement with the accepted value of  $10^{13}$ .

Previous applications of the Polanyi-Wigner equation to chemical reactions, as distinct from polymorphic phase changes, have been limited to endothermic reactions primarily the dehydration of salt hydrates<sup>64</sup>. It was found that when the heat of reaction was similar to the activation energy<sup>65</sup>, the frequency factor was ca  $10^{13}$  sec<sup>-1</sup>; but where the activation energy was considerably higher than the heat of the reaction the frequency factor was ca  $10^{25}$  sec<sup>-1</sup>. To explain these anomalous frequency factors the view has been put forward that a whole mozaic block undergoes instantaneous transformation on each act of excitation. This is called the Burgess and Mott trigger mechanism<sup>66</sup>.

For potassium metaperiodate the heat of reaction for the probable primary chemical step is similar to the activation energy and the frequency factors are not anomalously high. Thus the simple interfacial character of the decomposition appears to be confirmed.

## SECTION II

### The isothermal decomposition of potassium permanganate-potassium perchlorate solid solutions

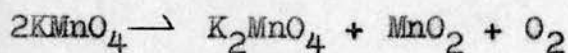
#### 1. Introduction

Greenberg and Walden<sup>69</sup> have shown that potassium permanganate and potassium perchlorate form a continuous series of solid solutions, which obey Vegard's additivity law.

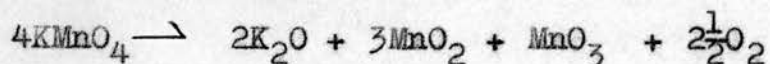
In work on the kinetics of the isothermal decomposition of the solid solutions, Hinshelwood and Bowen<sup>70, 71</sup> in 1920-21 explained the acceleration stage of the decomposition in terms of a progressive disintegration of the crystal structure with a consequent increase in the effective surface area. Solution in potassium perchlorate caused a reduction in the rate of the reaction, due to the suggested increased stability of the permanganate ion in the perchlorate lattice. They found that only the permanganate ion decomposed.

No further work appears to have been published on the decomposition of the solid solutions and the following introduction will deal with the work performed on potassium permanganate alone.

The decomposition can be represented by<sup>27</sup>



although Simchen<sup>72</sup> has reported



This can be interpreted as a further decomposition of potassium manganate into potassium oxide, manganese dioxide and oxygen.

When the decomposition is performed under isothermal conditions the addition of the products of the reaction to crystals of potassium permanganate appear to have little effect<sup>27,72,69</sup>, but using a gradually rising temperature Roginsky and Schulz<sup>73</sup> and Hill<sup>74,75</sup> observed, for iron and other oxides, a catalytic effect. This has been explained in terms of the creation of nuclei, resulting from the diffusion of ions into the lattice. This process probably has a low activation energy<sup>74</sup> and is thus effective at low temperatures.

The kinetics of the decomposition have been interpreted in various ways. Prout and Tompkins<sup>27</sup> in a study on fresh crystals, in the temperature range 473 - 493°K, found that after a linear induction period<sup>76</sup> of 4 - 5% decomposition, the reaction time curve was well fitted by the Prout-Tompkins equation. Grinding of this material in an agate mortar removed the induction period.

Erofeev and Smirmova<sup>77</sup> found that their results fitted the Avrami<sup>23</sup> equation with  $n = 4$  or  $5$ . They interpreted this as three dimensional growth and one or two 'acts' required for the formation of the nuclei. For commercial or aged material the value of 'n' was 2, representing two dimensional growth of a fixed number of nuclei. The values of 'n' were obtained by plotting  $\ln [1/(1-\alpha)]$  against  $\ln t$ , where the slope of the line was 'n'. This is an insensitive analytical method and the kinetics deduced from their results are therefore open to doubt, but the differences between fresh and aged material remain.

Similarly Roginsky and Schulz<sup>73</sup> using commercial material



fitted their results to a power law with  $n = 3$ .

Hill and Welsh<sup>78</sup> found, that for the early stages of the acceleration period for fresh material, the increase of pressure with time could best be represented by the exponential relationship  $\alpha = A \exp (kt + C)$ . This confirms the results of Prout and Tompkins, as the Prout-Tompkins equation reduces to the exponential form initially. For aged material Hill obtained poor exponential relationships, which also agrees with the previous workers' results.

Komatsu<sup>79</sup> has shown that the rate of the decomposition is dependent on the crystal size, the rate increasing with decreasing size.

Thus for a comparative study of the kinetics of decomposition of solid solutions of different compositions, it is necessary to standardise the experimental conditions. In the following work all the crystals used had linear dimensions of 300 - 500  $\mu$  and each batch of crystals was made as required and used within two weeks. The crystals used can thus be considered as fresh material.

2.

Experimental2. 1. Growth of crystals

Analar potassium permanganate and Kahlbawm's potassium perchlorate were used as starting materials. 500 ml of a saturated aqueous potassium permanganate solution at 60°C was allowed to cool to room temperature, in the dark, and then filtered through a sintered glass filter funnel. The filtrate was allowed to evaporate, in the dark, for approximately 12 hours. The supernatant liquid was decanted, the crystals rapidly dried and those of 300 - 500  $\mu$  in linear dimensions selected by sieving.

A second batch of crystals was made by the same procedure. Visual observations showed that the second batch was nearly free from external flaws, while the first batch had visible imperfections.

By use of the phase diagram for  $\text{KMnO}_4 - \text{KClO}_4 - \text{H}_2\text{O}$ , given by Greenberg and Walden<sup>69</sup>, saturated solutions were prepared such that the solid phase deposited on evaporation would have the desired percentage of potassium perchlorate. The procedure as given for potassium permanganate was then followed with the following additions. 2.5 l. of solution were prepared and not more than 1 g. of solid was allowed to crystallise out so that the composition of the solid solutions remained virtually constant, thus ensuring reasonable homogeneity of the solid solutions produced. Due to the low solubility of potassium perchlorate as compared with permanganate, the rate of evaporation was increased by evaporating in a current of air.

It was found impossible to obtain by the above procedure

crystals of low percentage potassium permanganate, that were of the required crystal size. For this case a saturated solution of the required composition at 35°C was allowed to cool to room temperature. The resulting crystals were however markedly inferior to those produced by slow evaporation.

The solid solutions were analysed for potassium permanganate by addition of excess of standard ferrous ammonium sulphate solution and back titration with standard potassium permanganate solution. The presence of potassium perchlorate was shown not to affect the results.

In this way the following batches of crystals were prepared as required. The average dimensions were 300 - 500  $\mu$ .

By slow evaporation,

- A 100 mole percent  $\text{KMnO}_4$ ,
- B 100 mole percent  $\text{KMnO}_4$ ,
- C large single crystal of  $\text{KMnO}_4$ ,
- D 89 mole percent  $\text{KMnO}_4$ ,
- E 70 mole percent  $\text{KMnO}_4$ ,
- F 52 mole percent  $\text{KMnO}_4$ .

By crystallisation from a saturated solution by cooling,

- G 25 mole percent  $\text{KMnO}_4$ .

## 2. 2. Preliminary observations

Preliminary kinetic experiments on the solid solutions were carried out in an identical manner to those described in the first section. For pure potassium permanganate (material A)



the pressure-time curve corresponded to Prout and Tompkins results for large crystals, but the volume of oxygen produced was in agreement with the results of Simchen, indicating a possible decomposition of the manganate ion. The presence of low percentages of potassium perchlorate reduced the rate of the reaction but otherwise did not effect a change in kinetics from those observed for material A. For high percentages of potassium perchlorate (material G) the Prout-Tompkins equation did not apply and the volume of oxygen released was far in excess of the value predicted by Simchen.

Potassium perchlorate decomposes in vacuo at  $800 - 820^{\circ}\text{K}$  by a complicated mechanism<sup>80</sup>. This is  $250^{\circ}$  in excess of the temperature of decomposition of material G, but it was thought likely that the manganese dioxide produced in the decomposition catalysed the decomposition of the potassium perchlorate, thus explaining the large amount of oxygen produced. This was confirmed from the analysis of the product from G which showed the presence of chloride ions. However after only 10% decomposition of G no chloride ions were detected. A 50 - 50 mixture of  $\text{KClO}_4$  and  $\text{MnO}_2$  on heating at  $570^{\circ}\text{K}$  released oxygen, but not at  $510^{\circ}\text{K}$ .

It was therefore decided to study only the first 5 - 10% of the reaction and to limit the maximum temperature to  $510^{\circ}\text{K}$ . Under these conditions only the permanganate ion decomposes, agreeing with the conclusions drawn by Hinshelwood and Bowen.

### 2. 3. Experimental procedure

The apparatus and procedure used to record the variation of pressure with time is given in section I (2.2.). The pressure was measured by means of a Pirani gauge coupled to a recorder, giving a continuous record of the pressure-time curve. Full scale deflection of 10" on the recorder represented, on the average, 7% decomposition, and as the recorder chart was subdivided into 0.1" it was estimated that the % decomposition as read from the trace was accurate to 0.02% as this represented 0.03". Thus the course of reaction through a given 1% decomposition was accurately known. A theoretical final pressure was calculated on the basis of one molecule of oxygen from two molecules of permanganate. The measured pressures were converted to the fractional decomposition ' $\alpha$ ' by dividing by the final pressure.

The rate of the reaction was determined by drawing tangents to the continuous pressure-time curve. With care this was found to be a fairly accurate procedure.

Hill and Welsh<sup>78</sup> have noted that a differential method of analysing the ' $\alpha$ ' - 't' curves avoids the use of arbitrary parameters. A plot of  $\frac{dx}{dt} / t$  and  $(\frac{dx}{dt})^2 / \alpha$  represent the power law equation with  $n = 2$  and  $3$  respectively and  $\frac{dx}{dt} / \alpha$  represents the exponential equation. In the latter case the constant obtained from the plot is independent of the estimate of the fractional decomposition, and only depends on the relative change in the pressure reading. As it was intended to examine in

detail a small fraction of the total decomposition of the solid solutions this sensitive analytical procedure was used.



## 2. 4. Kinetics of the decomposition

The typical shape of the ' $\alpha$ ' - 't' curves is shown in graph 1. For pure potassium permanganate there is an initial sigmoid section terminating at  $\alpha = 0.007$ ; this is followed by a linear stage which leads into the acceleration period. Runs D1 and F1 illustrate the effect of the potassium perchlorate; the initial decomposition as represented by the sigmoid is reduced and the linear stage is less pronounced. The overall rate of decomposition for the three examples is similar but the reaction temperature is increased as the potassium perchlorate content of the solid solutions rises. Graph 2 shows the rate-time curves for the above ' $\alpha$ ' - 't' curves. The linear stage appears as a constant rate and sometimes following this there is a linear increase in rate with time. The true acceleration stage, following either the constant or linear rate period, commences at ca  $\alpha = 0.02$ . Measurements on the decomposition did not extend past  $\alpha = 0.07$ .

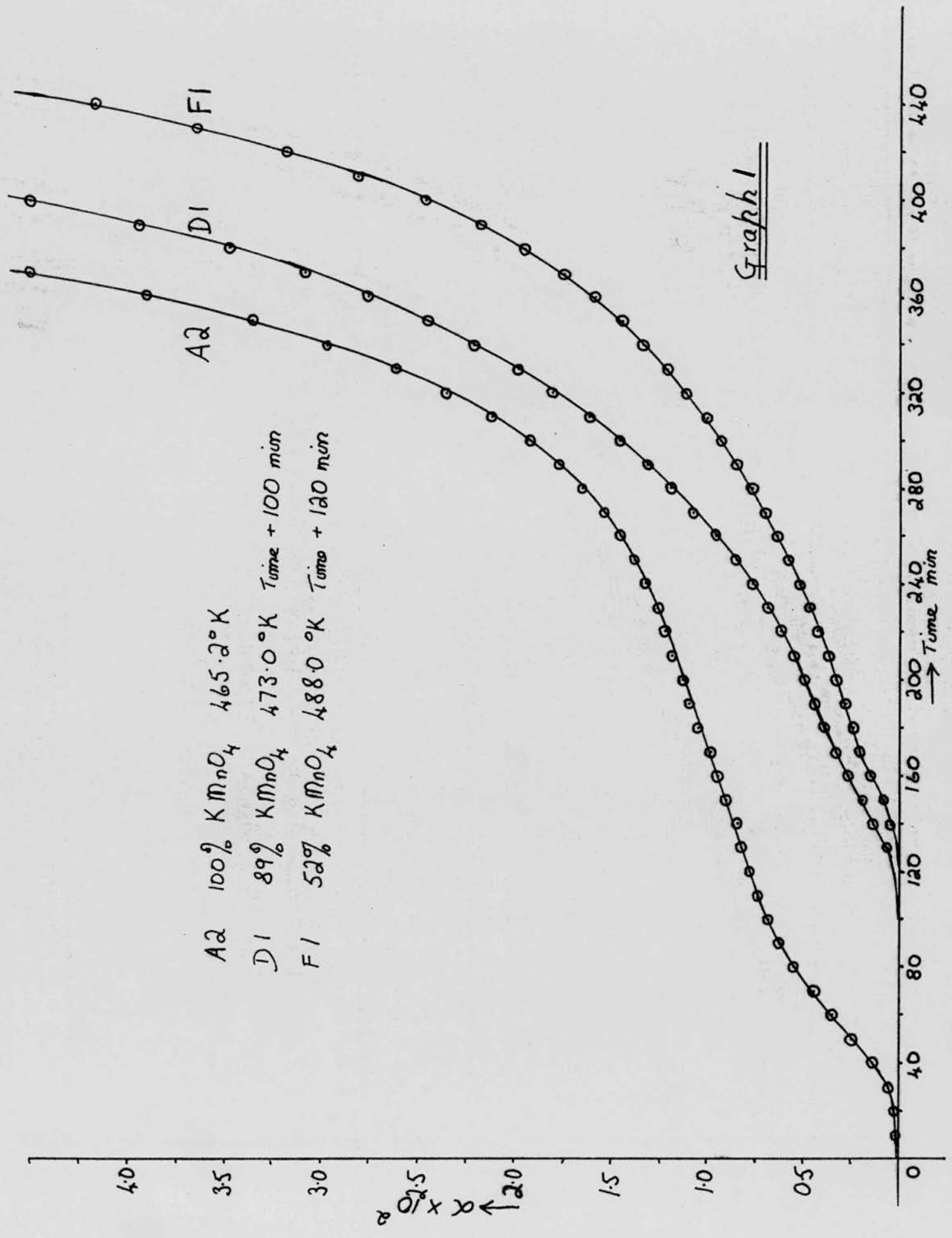
The curves have been analysed in terms of the following relationships between  $\alpha$ ,  $\frac{d\alpha}{dt}$  and t, where ' $\alpha$ ' is the ratio of the pressure at time 't' to the final pressure. Henceforth will be represented by 'R'.

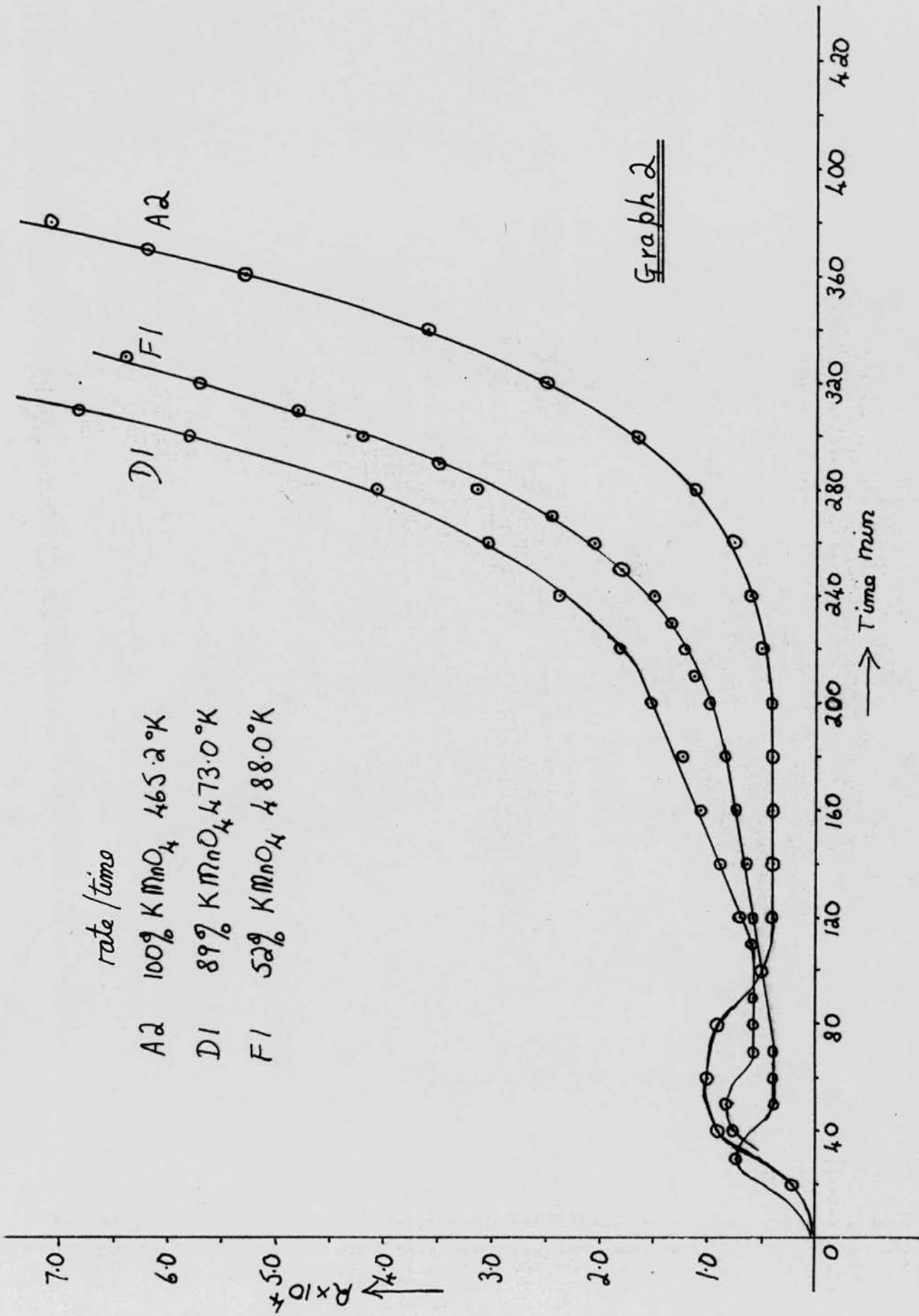
The initial sigmoid section of the curve has not been analysed in detail and the maximum rate, for this section, has been taken as a measure of the mechanism.

The linear relationship between ' $\alpha$ ' and 't' is represented by  $\alpha = k_1 t + C$ , thus  $R = k_1 = R_L$ , with  $\alpha_L$  the fraction

Graph 1

A2 100% KMnO4 465.2°K Time + 100 min  
 D1 89% KMnO4 473.0°K Time + 100 min  
 F1 52% KMnO4 488.0°K Time + 120 min







decomposed at the end of the linear stage. For the linear relationship between 'R' and 't', the equation  $\alpha \propto k_2 t^2$  represents the relationship, and is called the 't<sup>2</sup>-stage'.

The main acceleration period for the solid solutions A, B, D and E, that is those with greater than 70% potassium permanganate, followed the exponential relationship

$\alpha = A \exp(kt)$  up to  $\alpha = 0.07$  when the measurements were stopped. This agrees with the observations of Prout and Tompkins<sup>27</sup> and Hill<sup>78</sup>. The equation was plotted either in the form  $\log_{10}(\alpha - \alpha_L)/t$  or  $R/\alpha$ , and 'k' was readily found from the slope of the plots.

For the solid solution F, 52% potassium permanganate, the exponential equation for the acceleration stage was not satisfactory and a power law with  $n = 3$  found to be superior. The power law equation  $\alpha \propto k_3 t^3$  was plotted in the form  $R^2/$ . For solid solution G, 25% potassium permanganate, the acceleration stage of the reaction reduced to a power law with  $n = 2$ , as R was found to be constant.

The following tables and graphs show the majority of the runs performed at various temperatures in the range 460 - 520°K. The tables give the respective functions of ' $\alpha$ ' as required by the above analysis and the graphs show the plots of the different functions.

In 2.4.4. the constants ' $k_x$ ' are tabulated for the various runs together with the respective Arrhenius activation energy plots.

2. 4. 1. Kinetics of the decomposition for pure potassium permanganate

In tables 1, 2, 3, 4 and 5 and graphs 3A, 4 and 5, the kinetics are illustrated for pure potassium permanganate. Two batches were made, material A appeared upon visual observations to contain more surface imperfections than the second batch B.

For both A and B the initial sigmoid reaction terminates at  $\alpha = 0.006$ ; this is followed by the linear stage  $\alpha = 0.006$  to 0.012. For material A the exponential equation fitted from the end of the linear stage, but for B there was a 't<sup>2</sup>-stage' preceding the exponential relationship, which then applied from  $\alpha = 0.025$ .

The acceleration stage for A was analysed in terms of  $\log_{10}(\alpha - \alpha_L)/t$ , but for run A2,  $R/\alpha$  was also plotted. The same value of 'k' was obtained from both equations and they both fitted from

Three further runs were performed on single large crystals of approximate dimensions 1 cm x 0.1 cm<sup>2</sup>, run C3 is given as an example. The most notable features are the virtual absence of the initial sigmoid section, and the presence of a long linear stage from  $\alpha = 0.006 - 0.036$ .

Tables 1 and 2, analysis of A.

Tables 3 and 4, analysis of B.

Table 5, analysis of C.

Graph 3A, the ' $\alpha$ ' - 't' curves for the initial decomposition

showing the sigmoid and linear stages. In graph 6B (2.4.2.) the  $R/t$  curves demonstrate the ' $t^2$ -stage' for B.

Graph 4, acceleration stage for A, a plot of  $\log_{10}(\alpha - \alpha_L)/t$  illustrating the exponential relationship.

Graph 5, acceleration stage for B, a plot of  $R/\alpha$  illustrating the exponential relationship.



Table 1. Material A 100%  $\text{KMnO}_4$ 

| Run                | A2                   |                               |                 |  | A4               |                      |                               |
|--------------------|----------------------|-------------------------------|-----------------|--|------------------|----------------------|-------------------------------|
| Temp<br>$\alpha_L$ | 465.2°K<br>0.011     |                               |                 |  | 458.3°K<br>0.010 |                      |                               |
| Time<br>min        | $\alpha \times 10^2$ | $\log(\alpha - \alpha_L) + 4$ | $R \times 10^3$ | $(\frac{d\alpha}{dt})^{\frac{3}{2}} \times 10^6$ | Time<br>min      | $\alpha \times 10^2$ | $\log(\alpha - \alpha_L) + 4$ |
| 10                 | 0.01                 |                               |                 |  | 40               | 0.03                 |                               |
| 20                 | 0.02                 |                               | 0.02            |  | 50               | 0.06                 |                               |
| 30                 | 0.05                 |                               |                 |  | 60               | 0.12                 |                               |
| 40                 | 0.13                 |                               | 0.09            |  | 70               | 0.16                 |                               |
| 50                 | 0.25                 |                               |                 |  | 80               | 0.22                 |                               |
| 60                 | 0.35                 |                               | 0.10            |  | 90               | 0.29                 |                               |
| 70                 | 0.44                 |                               |                 |  | 100              | 0.35                 |                               |
| 80                 | 0.54                 |                               | 0.09            |  | 110              | 0.42                 |                               |
| 90                 | 0.62                 |                               |                 |  | 120              | 0.45                 |                               |
| 100                | 0.68                 |                               | 0.05            |  | 130              | 0.50                 |                               |
| 110                | 0.73                 |                               | 0.04            |  |                  |                      |                               |
| 120                | 0.78                 |                               |                 |  |                  |                      |                               |
| 130                | 0.82                 |                               | 0.04            |  |                  |                      |                               |
| 140                | 0.84                 |                               |                 |  |                  |                      |                               |
| 150                | 0.90                 |                               | 0.04            |  | 310              | 1.02                 |                               |
| 160                | 0.94                 |                               | 0.04            |  | 320              | 1.04                 |                               |
| 170                | 0.98                 |                               |                 |  | 330              | 1.07                 |                               |
| 180                | 1.04                 |                               | 0.04            |  | 340              | 1.11                 | 1.11                          |
| 190                | 1.09                 |                               |                 |  | 350              | 1.14                 | 1.20                          |
| 200                | 1.12                 |                               | 0.04            |  | 360              | 1.17                 | 1.28                          |
| 210                | 1.18                 |                               |                 |  | 370              | 1.22                 | 1.38                          |
| 220                | 1.22                 |                               | 0.05            |  | 380              | 1.26                 | 1.45                          |
| 230                | 1.26                 |                               |                 |  | 390              | 1.31                 | 1.52                          |
| 240                | 1.32                 | 1.34                          | 0.06            | 0.45   | 400              | 1.35                 | 1.57                          |
| 250                | 1.38                 |                               |                 |  | 410              | 1.40                 | 1.62                          |
| 260                | 1.45                 | 1.54                          | 0.075           | 0.65   | 420              | 1.46                 | 1.68                          |
| 270                | 1.53                 |                               |                 |  | 430              | 1.52                 | 1.75                          |
| 280                | 1.65                 | 1.74                          | 0.111           | 1.16   | 440              | 1.59                 | 1.78                          |
| 290                | 1.77                 |                               |                 |  | 450              | 1.66                 | 1.83                          |
| 300                | 1.92                 | 1.91                          | 0.165           | 2.10   | 460              | 1.76                 | 1.89                          |
| 310                | 2.11                 |                               |                 |  | 470              | 1.85                 | 1.94                          |
| 320                | 2.35                 | 2.10                          | 0.25            | 3.94   | 480              | 1.95                 | 1.99                          |
| 330                | 2.61                 |                               |                 |  | 490              | 2.07                 | 2.04                          |
| 340                | 2.97                 | 2.27                          | 0.36            | 6.86   | 500              | 2.20                 | 2.09                          |
| 350                | 3.36                 |                               |                 |  | 510              | 2.35                 | 2.14                          |
| 360                | 3.91                 | 2.45                          | 0.53            | 12.2   | 520              | 2.51                 | 2.18                          |
| 370                | 4.51                 | 2.53                          | 0.62            | 15.4   | 530              | 2.71                 | 2.24                          |
| 380                | 5.18                 | 2.61                          | 0.71            | 18.8   | 540              | 2.97                 | 2.33                          |

linear increase  
of ' $\alpha$ ' with time

Table 2. Material A 100%  $\text{KMnO}_4$ 

| Run         | A1                   |                                | A3   |                                | A5                   |                                | A6                   |                                |
|-------------|----------------------|--------------------------------|--|--------------------------------|----------------------|--------------------------------|----------------------|--------------------------------|
| Temp        | 471.2°K              |                                | 468.3°K                                      |                                | 470.0°K              |                                | 477.8°K              |                                |
| $\alpha_L$  | 0.012                |                                | 0.012  |                                | 0.012                |                                | 0.011                |                                |
| Time<br>min | $\alpha \times 10^2$ | $\log(\alpha - \alpha_L)^{4+}$ | $\alpha \times 10^2$                         | $\log(\alpha - \alpha_L)^{4+}$ | $\alpha \times 10^2$ | $\log(\alpha - \alpha_L)^{4+}$ | $\alpha \times 10^2$ | $\log(\alpha - \alpha_L)^{4+}$ |
| 10          | 0.03                 |                                |  |                                | 0.01                 |                                | 0.04                 |                                |
| 20          | 0.10                 |                                | 0.03   |                                | 0.03                 |                                | 0.12                 |                                |
| 30          | 0.18                 |                                | 0.08   |                                | 0.09                 |                                | 0.34                 |                                |
| 40          | 0.36                 |                                | 0.20   |                                | 0.25                 |                                | 0.61                 |                                |
| 50          | 0.50                 |                                | 0.32   |                                | 0.39                 |                                | 0.77                 |                                |
| 60          | 0.62                 |                                | 0.46   |                                | 0.56                 |                                | 0.95                 |                                |
| 70          | 0.67                 |                                | 0.57   |                                | 0.67                 |                                | 1.16                 |                                |
| 80          | 0.75                 |                                |  |                                | 0.74                 |                                | 1.41                 | 1.48                           |
| 90          | 0.80                 |                                |  |                                | 0.82                 |                                | 1.67                 | 1.75                           |
| 100         | 0.87                 |                                |  |                                | 0.92                 |                                | 2.00                 | 1.95                           |
| 110         | 0.93                 |                                | linear increase<br>of ' $\alpha$ ' with time |                                | 1.02                 |                                | 2.44                 | 2.13                           |
| 120         | 1.02                 |                                |  |                                | 1.13                 |                                | 3.22                 | 2.33                           |
| 130         | 1.10                 |                                |  |                                | 1.25                 |                                | 4.55                 | 2.54                           |
| 140         | 1.19                 |                                |  |                                | 1.34                 |                                | 6.80                 | 2.76                           |
| 150         | 1.27                 |                                |  |                                | 1.46                 | 1.41                           |                      |                                |
| 160         | 1.37                 | 1.23                           |  |                                | 1.63                 | 1.63                           |                      |                                |
| 170         | 1.50                 | 1.48                           |  |                                | 1.79                 | 1.77                           |                      |                                |
| 180         | 1.70                 | 1.70                           | 1.17   |                                | 2.01                 | 1.91                           |                      |                                |
| 190         | 1.97                 | 1.89                           | 1.24   |                                | 2.21                 | 2.00                           |                      |                                |
| 200         | 2.35                 | 2.06                           | 1.33   | 1.11                           | 2.54                 | 2.13                           |                      |                                |
| 210         | 2.90                 | 2.23                           | 1.41   | 1.32                           | 3.06                 | 2.27                           |                      |                                |
| 220         | 3.67                 | 2.39                           | 1.54   | 1.53                           | 3.65                 | 2.39                           |                      |                                |
| 230         | 4.78                 | 2.55                           | 1.70   | 1.70                           | 4.65                 | 2.54                           |                      |                                |
| 240         | 6.26                 | 2.70                           | 1.89   | 1.84                           | 5.72                 | 2.65                           |                      |                                |
| 250         | 8.23                 | 2.85                           | 2.16   | 1.98                           | 7.25                 | 2.78                           |                      |                                |
| 260         | 10.6                 | 2.98                           | 2.50   | 2.11                           |                      |                                |                      |                                |
| 270         | 13.8                 | 3.10                           | 2.97   | 2.25                           |                      |                                |                      |                                |
| 280         | 19.2                 | 3.25                           | 3.56   | 2.37                           |                      |                                |                      |                                |
| 290         | 25.3                 | 3.38                           | 4.32   | 2.49                           |                      |                                |                      |                                |
| 300         | 33.0                 | 3.50                           | 5.20   | 2.60                           |                      |                                |                      |                                |
| 310         |                      |                                | 6.17   | 2.70                           |                      |                                |                      |                                |

Table 3. Material B 100%  $\text{KMnO}_4$ 

| Run         | B1                   |                 | B2                   |                 | B5                   |                 |
|-------------|----------------------|-----------------|----------------------|-----------------|----------------------|-----------------|
| Temp        | 498.2°K              |                 | 498.2°K              |                 | 486.1°K              |                 |
| Time<br>min | $\alpha \times 10^2$ | $R \times 10^3$ | $\alpha \times 10^2$ | $R \times 10^3$ | $\alpha \times 10^2$ | $R \times 10^3$ |
| 2           | 0                    |                 |                      |                 |                      |                 |
| 4           |                      |                 |                      |                 |                      |                 |
| 6           | 0.01                 |                 |                      |                 |                      |                 |
| 8           | 0.03                 |                 |                      |                 |                      |                 |
| 10          | 0.05                 |                 | 0.05                 |                 |                      |                 |
| 12          | 0.18                 |                 | 0.17                 | 0.88            |                      |                 |
| 14          | 0.39                 | 1.31            | 0.41                 |                 |                      |                 |
| 16          | 0.665                |                 | 0.70                 | 0.64            |                      |                 |
| 18          | 0.85                 | 0.81            |                      | 0.64            |                      |                 |
| 20          | 1.0                  | 0.81            | 0.96                 | 0.69            | 0.27                 | 0.62            |
| 22          | 1.18                 | 0.81            | 1.11                 | 0.79            |                      |                 |
| 24          | 1.38                 | 1.02            | 1.29                 | 0.92            |                      |                 |
| 25          |                      |                 |                      |                 |                      |                 |
| 26          | 1.59                 |                 | 1.46                 |                 |                      |                 |
| 28          | 1.85                 | 1.36            | 1.70                 | 1.16            |                      |                 |
| 30          | 2.12                 |                 | 1.94                 |                 |                      |                 |
| 32          | 2.48                 | 1.81            | 2.24                 | 1.64            |                      |                 |
| 34          | 2.87                 |                 | 2.61                 | 2.03            |                      |                 |
| 35          |                      |                 |                      |                 | 0.88                 | 0.38            |
| 36          | 3.36                 | 2.47            | 3.12                 | 2.72            |                      |                 |
| 37          |                      |                 | 3.41                 | 3.3             |                      |                 |
| 38          | 3.96                 | 3.40            | 3.76                 | 4.1             |                      |                 |
| 39          |                      |                 | 4.3                  | 5.2             |                      |                 |
| 40          | 4.78                 | 4.70            | 4.85                 | 6.4             | 1.11                 | 0.38            |
| 42          | 5.95                 | 6.70            |                      |                 |                      |                 |
| 44          |                      |                 |                      |                 | 1.32                 | 0.38            |
| 45          |                      |                 |                      |                 |                      |                 |
| 50          |                      |                 |                      |                 | 1.57                 | 0.52            |
| 55          |                      |                 |                      |                 |                      | 0.61            |
| 60          |                      |                 |                      |                 | 2.19                 | 0.72            |
| 65          |                      |                 |                      |                 | 2.56                 | 0.83            |
| 70          |                      |                 |                      |                 | 3.04                 | 0.96            |
| 74          |                      |                 |                      |                 | 3.51                 | 1.20            |
| 78          |                      |                 |                      |                 | 4.02                 | 1.40            |
| 82          |                      |                 |                      |                 | 4.70                 | 1.87            |
| 86          |                      |                 |                      |                 | 5.55                 | 2.36            |
| 90          |                      |                 |                      |                 | 6.65                 | 3.12            |
| 92          |                      |                 |                      |                 | 7.28                 | 3.6             |

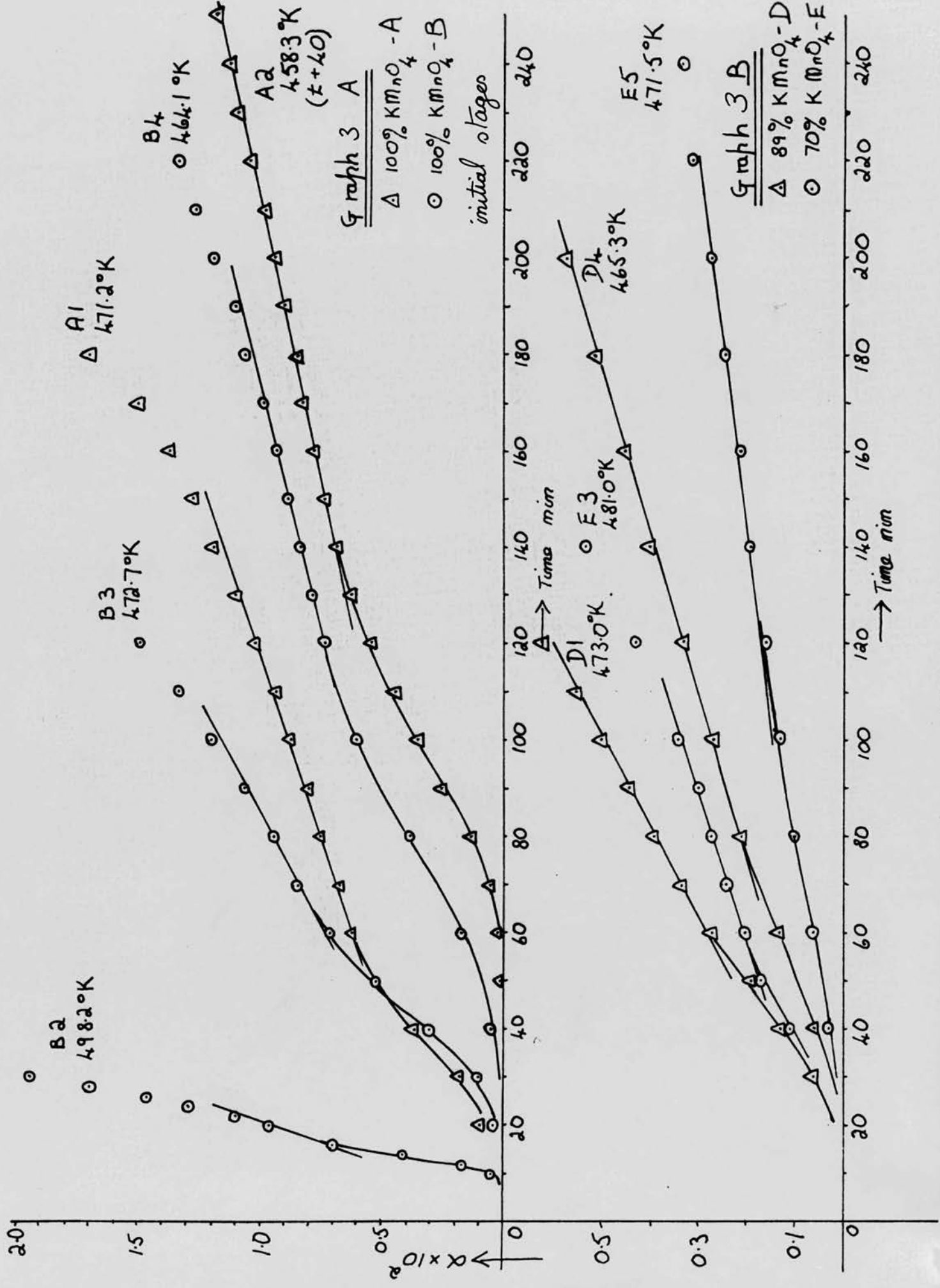


Table 4. Material B 100%  $\text{KMnO}_4$ 

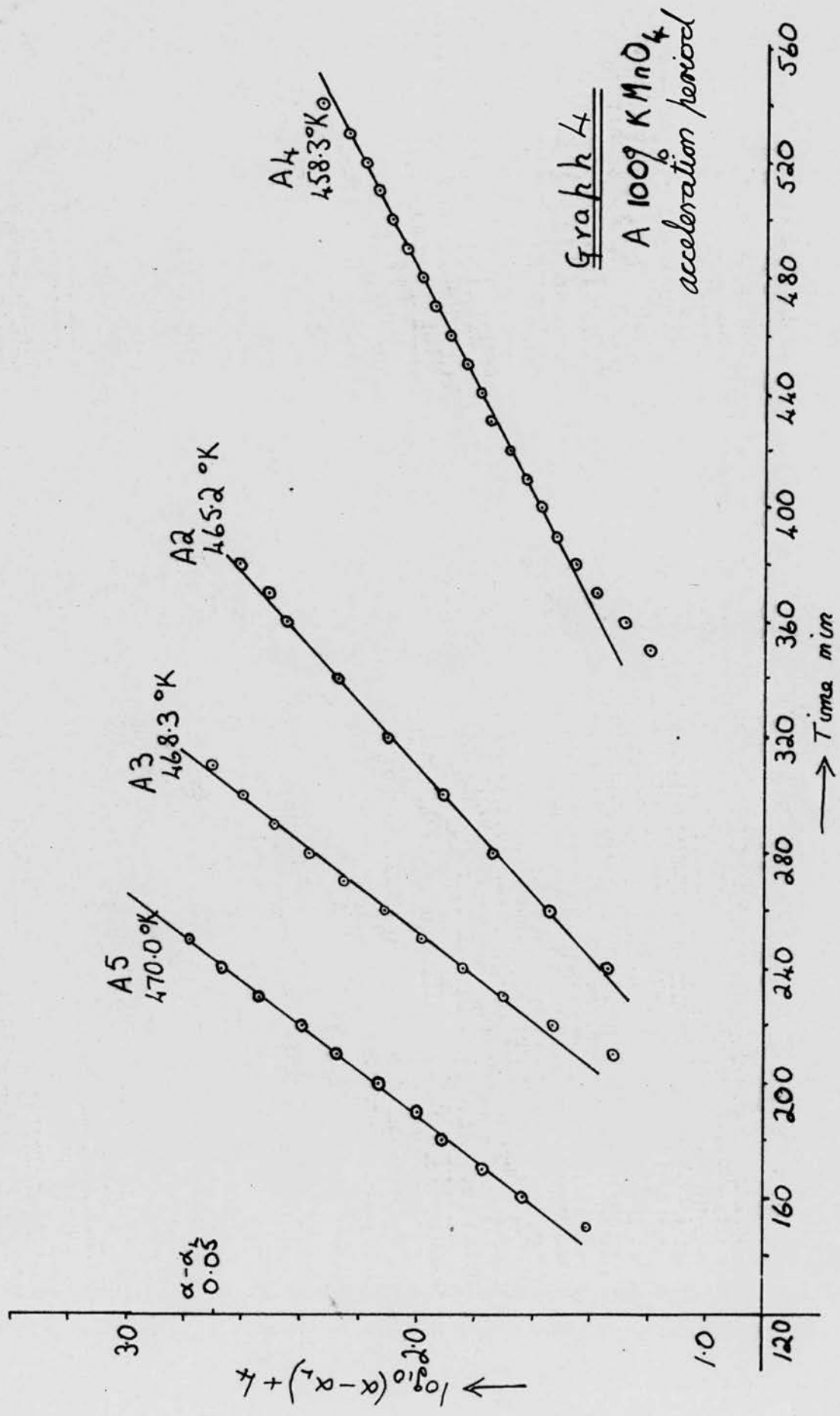
| Run         | B4                   |                 |                                 | B3                   |                 |
|-------------|----------------------|-----------------|---------------------------------|----------------------|-----------------|
| Temp        | 464.1°K              |                 |                                 | 472.7°K              |                 |
| Time<br>min | $\alpha \times 10^2$ | $R \times 10^3$ | $(R)^{\frac{3}{2}} \times 10^6$ | $\alpha \times 10^2$ | $R \times 10^3$ |
| 20          |                      |                 |                                 | 0.04                 |                 |
| 30          |                      |                 |                                 | 0.10                 |                 |
| 40          | 0.05                 |                 |                                 | 0.30                 |                 |
| 50          |                      |                 |                                 | 0.52                 | 0.26            |
| 60          | 0.17                 |                 |                                 | 0.73                 | 0.108           |
| 70          |                      |                 |                                 | 0.84                 | 0.108           |
| 80          | 0.38                 | 0.134           |                                 | 0.94                 | 0.108           |
| 90          |                      |                 |                                 | 1.08                 |                 |
| 100         | 0.58                 |                 |                                 | 1.20                 | 0.135           |
| 110         |                      |                 |                                 | 1.33                 |                 |
| 120         | 0.73                 | 0.049           |                                 | 1.49                 | 0.172           |
| 130         | 0.78                 | 0.049           |                                 | 1.64                 |                 |
| 140         | 0.83                 | 0.049           |                                 | 1.86                 | 0.210           |
| 150         | 0.88                 | 0.049           |                                 | 2.07                 |                 |
| 160         | 0.93                 | 0.049           |                                 | 2.29                 | 0.248           |
| 170         | 0.99                 |                 |                                 | 2.55                 | 0.28            |
| 180         | 1.06                 | 0.064           |                                 | 2.86                 | 0.32            |
| 190         | 1.10                 |                 |                                 | 3.18                 | 0.39            |
| 200         | 1.19                 | 0.070           |                                 | 3.63                 | 0.45            |
| 210         | 1.26                 |                 |                                 | 4.14                 | 0.56            |
| 220         | 1.33                 | 0.076           |                                 | 4.77                 | 0.69            |
| 230         | 1.41                 |                 |                                 | 5.54                 | 0.85            |
| 240         | 1.49                 | 0.087           |                                 | 6.59                 | 1.13            |
| 250         | 1.58                 |                 |                                 | 7.80                 | 1.36            |
| 260         | 1.68                 | 0.095           |                                 | 9.40                 | 1.67            |
| 270         | 1.76                 |                 |                                 |                      |                 |
| 280         | 1.88                 | 0.115           | 1.22                            |                      |                 |
| 290         | 2.01                 |                 |                                 |                      |                 |
| 300         | 2.13                 | 0.134           | 1.56                            |                      |                 |
| 310         | 2.27                 |                 |                                 |                      |                 |
| 320         | 2.42                 | 0.158           | 2.00                            |                      |                 |
| 330         | 2.59                 |                 |                                 |                      |                 |
| 340         | 2.78                 | 0.197           | 2.74                            |                      |                 |
| 360         | 3.22                 | 0.243           | 3.8                             |                      |                 |
| 380         | 3.76                 | 0.298           | 5.2                             |                      |                 |
| 400         | 4.41                 | 0.352           | 6.6                             |                      |                 |
| 420         | 5.21                 | 0.438           | 9.1                             |                      |                 |
| 440         | 6.21                 | 0.545           | 12.6                            |                      |                 |
| 450         | 6.72                 | 0.595           | 14.5                            |                      |                 |
| 460         | 7.40                 | 0.634           | 16.0                            |                      |                 |

Table 5. Material C 100%  $\text{KMnO}_4$ 

| Run         | 03                    |                 |
|-------------|-----------------------|-----------------|
| Temp        | $464.4^\circ\text{K}$ |                 |
| Time<br>min | $\alpha \times 10^2$  | $R \times 10^4$ |
| 20          | 0.12                  | 0.55            |
| 40          | 0.16                  |                 |
| 60          | 0.27                  | 0.63            |
| 80          | 0.41                  | 0.79            |
| 100         | 0.60                  | 0.84            |
| 120         | 0.79                  | 1.10            |
| 160         | 1.21                  | 1.10            |
| 200         | 1.67                  | 1.15            |
| 240         | 2.13                  | 1.18            |
| 280         | 2.63                  | 1.18            |
| 300         | 2.91                  | 1.18            |
| 320         | 3.13                  | 1.18            |
| 340         | 3.53                  | 1.18            |
| 360         | 3.62                  | 1.22            |
| 380         | 3.87                  | 1.30            |
| 400         | 4.15                  | 1.36            |
| 420         | 4.44                  | 1.58            |
| 440         | 4.80                  | 2.03            |
| 450         | 5.01                  | 2.38            |
| 460         | 5.30                  | 2.93            |
| 470         | 5.60                  | 3.2             |
| 480         | 5.95                  | 3.9             |
| 490         | 6.42                  | 4.7             |
| 500         | 6.96                  | 5.6             |
| 510         | 7.59                  | 6.5             |
| 520         | 8.4                   | 7.6             |
| 530         | 9.3                   | 8.7             |
| 540         | 10.4                  | 10.1            |
| 550         | 11.5                  | 11.2            |
| 560         | 12.8                  | 13.3            |

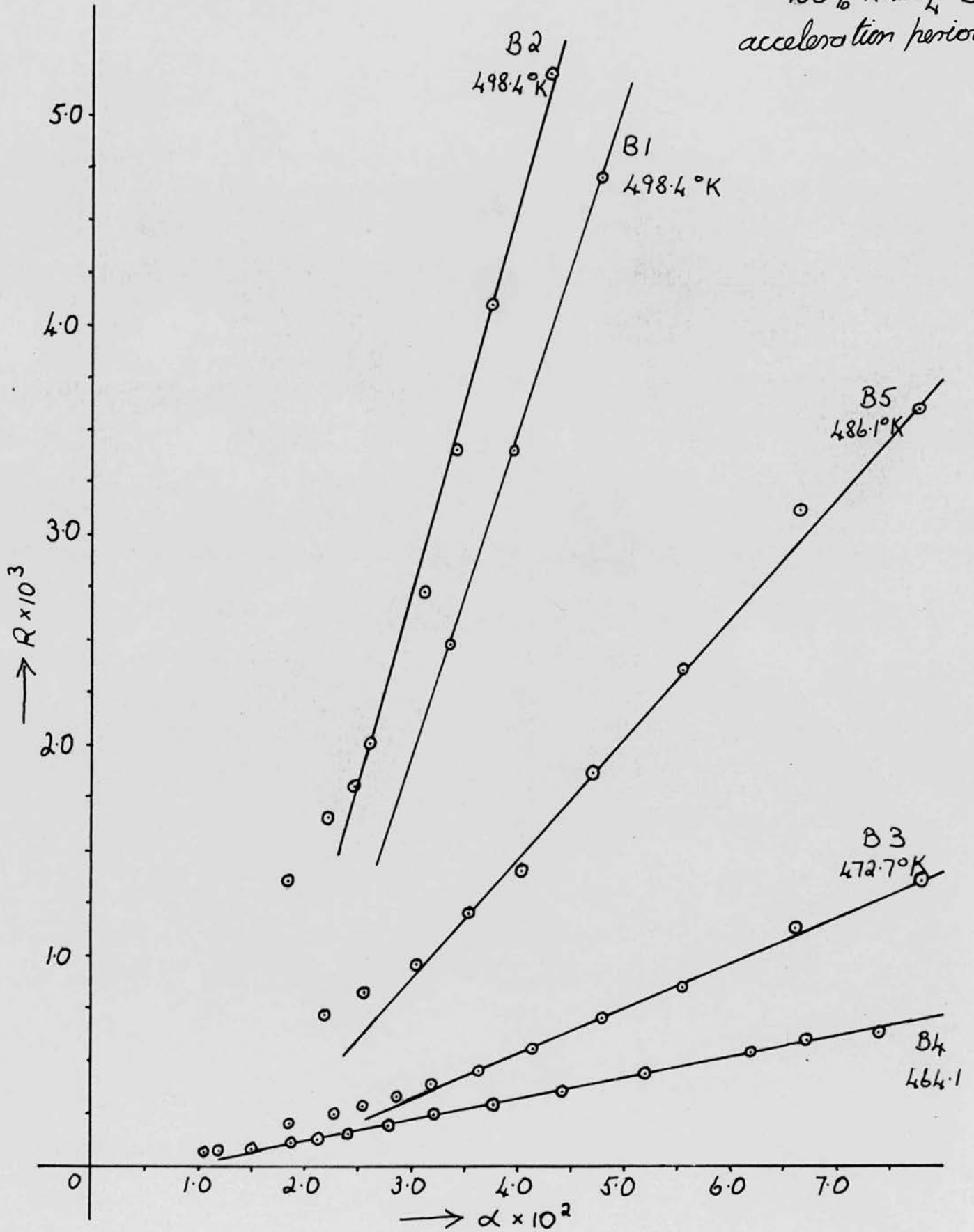






Graph 5

100%  $\text{KMnO}_4$  B  
acceleration period



2. 4. 2. Kinetics of the decomposition for solid solutions D and E

In tables 6, 7, 8 and 9 and graphs 6 and 7 the kinetics are illustrated for the decomposition of solid solutions D and E containing 89 and 70% of potassium permanganate respectively. These solid solutions show the same general features as for pure permanganate B, but with a much decreased rate of decomposition. For D the initial sigmoid stage ceases at  $\alpha = 0.003$  and the linear stage only extends from  $\alpha = 0.003 - 0.005$ , this being followed by the ' $t^2$ -stage' up to  $\alpha = 0.015$ . The acceleration stage is adequately fitted by the exponential equation from  $\alpha = 0.02$ .

For solid solution E the sigmoid stage is further reduced to  $\alpha = 0.0015$  and the linear stage is probably present from  $\alpha = 0.0015 - 0.0025$ . The ' $t^2$ -stage' extends from  $\alpha = 0.0025$  to 0.01 followed by the acceleration stage expressed by an exponential relationship but a power law with  $n = 3$  is a feasible alternative.

Tables 6, 7 and 8, analysis of solid solutions D and E.

Graphs 6A and B, ' $t^2$ -stage', a plot of the  $R/t$ , showing the linear increase in rate with time.

Graph 7, acceleration stage, a plot of the  $R/\alpha$  showing the exponential relationship. In graph 3B (2.4.1.) the ' $\alpha$ ' - ' $t$ ' curves are given for the initial decomposition, showing the sigmoid and linear stages.



Table 6. Material D 89%  $\text{KMnO}_4$ 

| Run         | D1                   |                 | D2                   |                 | D3                   |                 |
|-------------|----------------------|-----------------|----------------------|-----------------|----------------------|-----------------|
| Temp        | 473.0°K              |                 | 468.4°K              |                 | 471.6°K              |                 |
| Time<br>min | $\alpha \times 10^2$ | $R \times 10^3$ | $\alpha \times 10^2$ | $R \times 10^3$ | $\alpha \times 10^2$ | $R \times 10^3$ |
| 30          | 0.06                 |                 |                      |                 | 0.03                 |                 |
| 40          | 0.13                 | 0.077           | 0.03                 | 0.031           | 0.07                 |                 |
| 50          | 0.19                 | 0.077           | 0.08                 |                 |                      |                 |
| 60          | 0.27                 |                 | 0.13                 | 0.051           | 0.20                 | 0.062           |
| 70          | 0.33                 | 0.056           | 0.20                 | 0.047           |                      |                 |
| 80          | 0.39                 | 0.056           | 0.23                 | 0.047           | 0.28                 | 0.039           |
| 90          | 0.44                 | 0.056           | 0.28                 |                 | 0.33                 | 0.039           |
| 100         | 0.50                 |                 | 0.32                 | 0.035           | 0.37                 | 0.039           |
| 110         | 0.55                 | 0.056           | 0.35                 |                 | 0.40                 | 0.039           |
| 120         | 0.62                 | 0.069           | 0.37                 | 0.035           | 0.43                 | 0.039           |
| 130         | 0.69                 |                 | 0.42                 |                 | 0.48                 |                 |
| 140         | 0.77                 | 0.087           | 0.45                 | 0.035           | 0.54                 | 0.050           |
| 150         | 0.85                 |                 | 0.50                 |                 | 0.59                 |                 |
| 160         | 0.96                 | 0.106           | 0.54                 | 0.043           | 0.66                 | 0.060           |
| 170         | 1.07                 |                 | 0.58                 |                 | 0.72                 |                 |
| 180         | 1.19                 | 0.126           | 0.64                 | 0.052           | 0.78                 | 0.069           |
| 190         | 1.31                 |                 | 0.69                 |                 | 0.86                 |                 |
| 200         | 1.46                 | 0.151           | 0.74                 | 0.059           | 0.94                 | 0.085           |
| 210         | 1.61                 |                 | 0.79                 |                 | 1.02                 |                 |
| 220         | 1.80                 | 0.180           | 0.86                 | 0.066           | 1.12                 | 0.098           |
| 230         | 1.99                 |                 | 0.93                 |                 | 1.22                 |                 |
| 240         | 2.21                 | 0.238           | 1.00                 | 0.073           | 1.35                 | 0.125           |
| 250         | 2.45                 |                 | 1.07                 |                 | 1.47                 |                 |
| 260         | 2.76                 | 0.303           | 1.17                 | 0.088           | 1.63                 | 0.148           |
| 270         | 3.09                 |                 | 1.27                 |                 | 1.78                 |                 |
| 280         | 3.48                 | 0.407           | 1.35                 | 0.099           | 1.98                 | 0.208           |
| 290         | 3.95                 |                 | 1.46                 |                 | 2.19                 |                 |
| 300         | 4.51                 | 0.580           | 1.56                 | 0.112           | 2.45                 | 0.278           |
| 305         | 4.86                 |                 |                      |                 |                      |                 |
| 310         | 5.19                 | 0.683           | 1.70                 |                 | 2.76                 |                 |
| 315         | 5.55                 |                 |                      |                 |                      |                 |
| 320         | 5.93                 | 0.800           | 1.82                 | 0.127           | 3.11                 | 0.396           |
| 330         |                      |                 | 1.95                 |                 | 3.55                 |                 |
| 340         |                      |                 | 2.11                 | 0.147           | 4.07                 | 0.545           |
| 360         |                      |                 | 2.47                 | 0.199           | 5.36                 | 0.74            |
| 370         |                      |                 | 2.68                 |                 | 6.15                 |                 |
| 380         |                      |                 | 2.91                 | 0.24            |                      |                 |
| 390         |                      |                 | 3.18                 |                 |                      |                 |
| 400         |                      |                 | 3.45                 | 0.30            |                      |                 |
| 410         |                      |                 | 3.80                 |                 |                      |                 |
| 420         |                      |                 | 4.17                 | 0.40            |                      |                 |
| 440         |                      |                 | 5.06                 | 0.48            |                      |                 |

Table 7. Material E 70%  $KMnO_4$

| E1<br>485.5°K        |                 | E3<br>481.0°K        |                 |                                 | E4<br>489.1°K        |                 |
|----------------------|-----------------|----------------------|-----------------|---------------------------------|----------------------|-----------------|
| $\alpha \times 10^2$ | $R \times 10^4$ | $\alpha \times 10^2$ | $R \times 10^4$ | $(R)^{\frac{3}{2}} \times 10^6$ | $\alpha \times 10^2$ | $R \times 10^4$ |
| 0.11                 | 0.90            | 0.05                 |                 |                                 | 0.18                 | 0.51            |
| 0.17                 | 0.24            | 0.11                 | 0.60            |                                 | 0.22                 | 0.51            |
| 0.19                 | 0.24            | 0.17                 | 0.33            |                                 | 0.26                 | 0.51            |
| 0.20                 | 0.24            | 0.20                 | 0.33            |                                 | 0.32                 | 0.70            |
| 0.25                 | 0.38            | 0.24                 | 0.33            |                                 |                      |                 |
| 0.31                 | 0.41            | 0.27                 | 0.33            |                                 | 0.49                 | 0.79            |
| 0.35                 | 0.51            | 0.30                 | 0.33            |                                 |                      |                 |
| 0.41                 | 0.61            | 0.34                 | 0.40            |                                 | 0.69                 | 1.05            |
| 0.47                 | 0.69            |                      |                 |                                 | 0.77                 | 1.08            |
| 0.55                 | 0.79            | 0.43                 | 0.48            |                                 | 0.92                 | 1.33            |
| 0.63                 | 0.85            |                      |                 |                                 | 1.06                 | 1.60            |
| 0.72                 | 0.95            | 0.53                 | 0.54            |                                 | 1.23                 | 1.94            |
| 0.81                 | 1.04            |                      |                 |                                 | 1.43                 | 2.51            |
| 0.92                 | 1.15            | 0.64                 | 0.62            |                                 | 1.73                 | 3.34            |
| 1.04                 | 1.4             |                      |                 |                                 | 2.13                 | 4.80            |
| 1.21                 | 1.7             | 0.77                 | 0.70            |                                 | 2.78                 | 7.64            |
| 1.39                 | 2.0             |                      |                 |                                 | 3.72                 | 11.3            |
| 1.61                 | 2.4             | 0.92                 | 0.80            |                                 | 5.15                 | 17.1            |
| 1.90                 | 3.2             |                      |                 |                                 | 7.14                 |                 |
| 2.27                 | 4.4             | 1.10                 | 0.99            |                                 |                      |                 |
| 2.82                 | 5.6             |                      |                 |                                 |                      |                 |
| 3.51                 | 7.5             | 1.33                 | 1.22            | 1.33                            |                      |                 |
| 4.47                 | 9.8             |                      |                 |                                 |                      |                 |
| 5.65                 | 13.3            | 1.61                 | 1.60            | 2.00                            |                      |                 |
|                      |                 | 1.78                 |                 |                                 |                      |                 |
|                      |                 | 1.98                 | 2.15            | 3.18                            |                      |                 |
|                      |                 | 2.19                 |                 |                                 |                      |                 |
|                      |                 | 2.47                 | 3.13            | 5.64                            |                      |                 |
|                      |                 | 2.81                 | 3.70            | 7.08                            |                      |                 |
|                      |                 | 3.23                 | 4.43            | 9.26                            |                      |                 |
|                      |                 | 3.71                 | 5.43            | 12.6                            |                      |                 |
|                      |                 | 4.30                 | 6.24            | 15.6                            |                      |                 |
|                      |                 | 4.95                 | 7.20            | 19.2                            |                      |                 |

2. 4. 3. Kinetics of the decomposition of solid solutions F and G

In tables 9, 10 and 11 and graphs 8 and 9 the kinetics are illustrated for the decomposition of solid solutions F and G, containing 52 and 25% of potassium permanganate respectively. The relative fractional decomposition of the different stages in the decomposition of F is similar to E, but the acceleration stage is best represented by a power law with  $n = 3$ .

For solid solution G the sigmoid decomposition was greatly increased extending to  $\alpha = 0.01$ . This is almost certainly due to the method of preparation of the crystals, which resulted in extremely poor faces on the crystals and hence increasing the surface area. This will be discussed later. The 't<sup>2</sup>-stage' was also increased and now extended from  $\alpha = 0.01 - 0.025$ , this being followed by the acceleration stage expressed in terms of a power law with  $n = 2$ .

Tables 9, 10 and 11, analysis of solid solutions F and G.

Graph 8, acceleration stage for F, a plot of  $R^2/\alpha^3$ , showing the fit for a power law with  $n = 3$ .

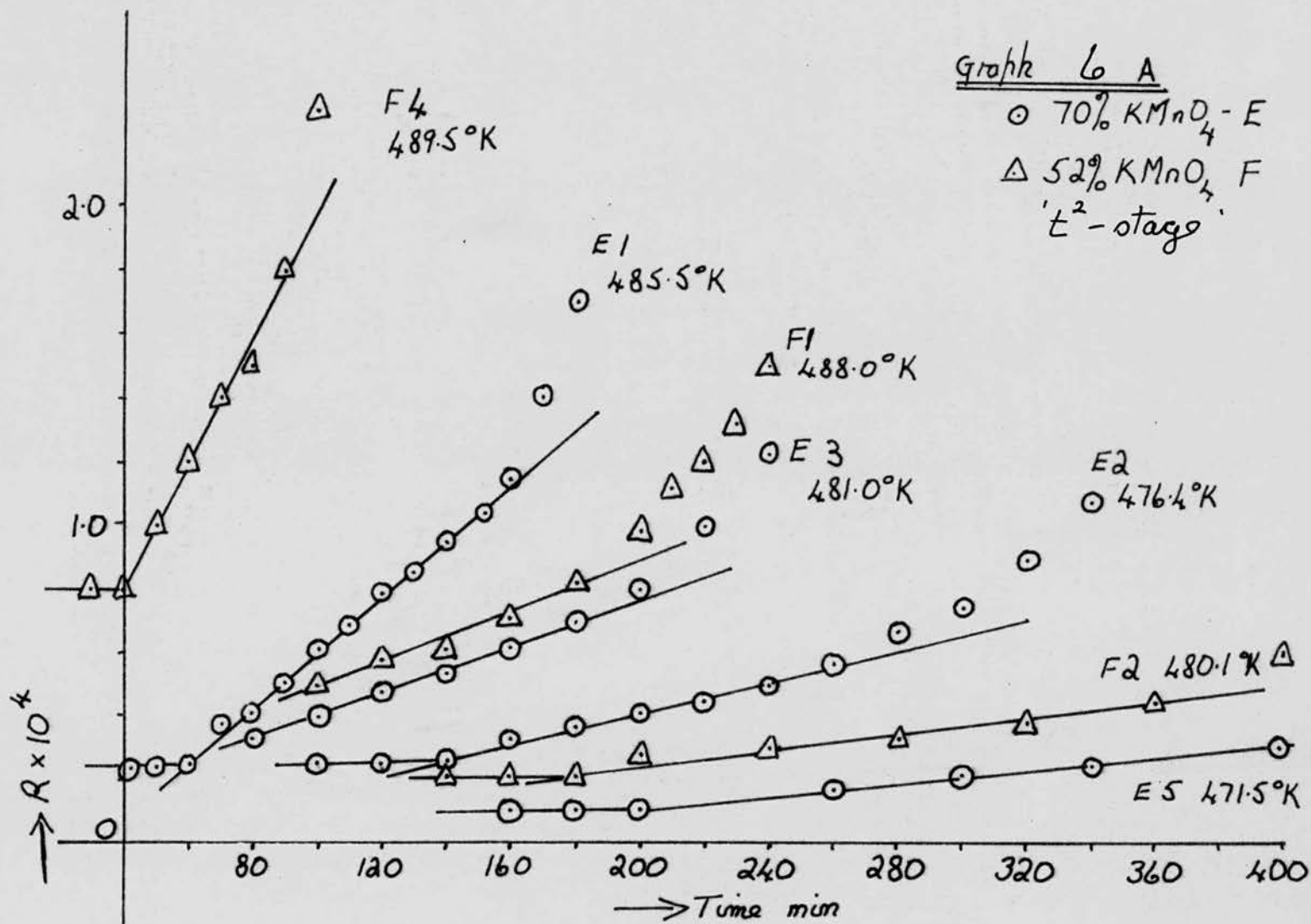
Graph 9, 't<sup>2</sup>-stage' and acceleration stage for G, a plot of  $R/t$  showing the fit for the power law with  $n = 2$ .

In graph 6A (2.4.2.) the 't<sup>2</sup>-stage' is shown for solid solution F.



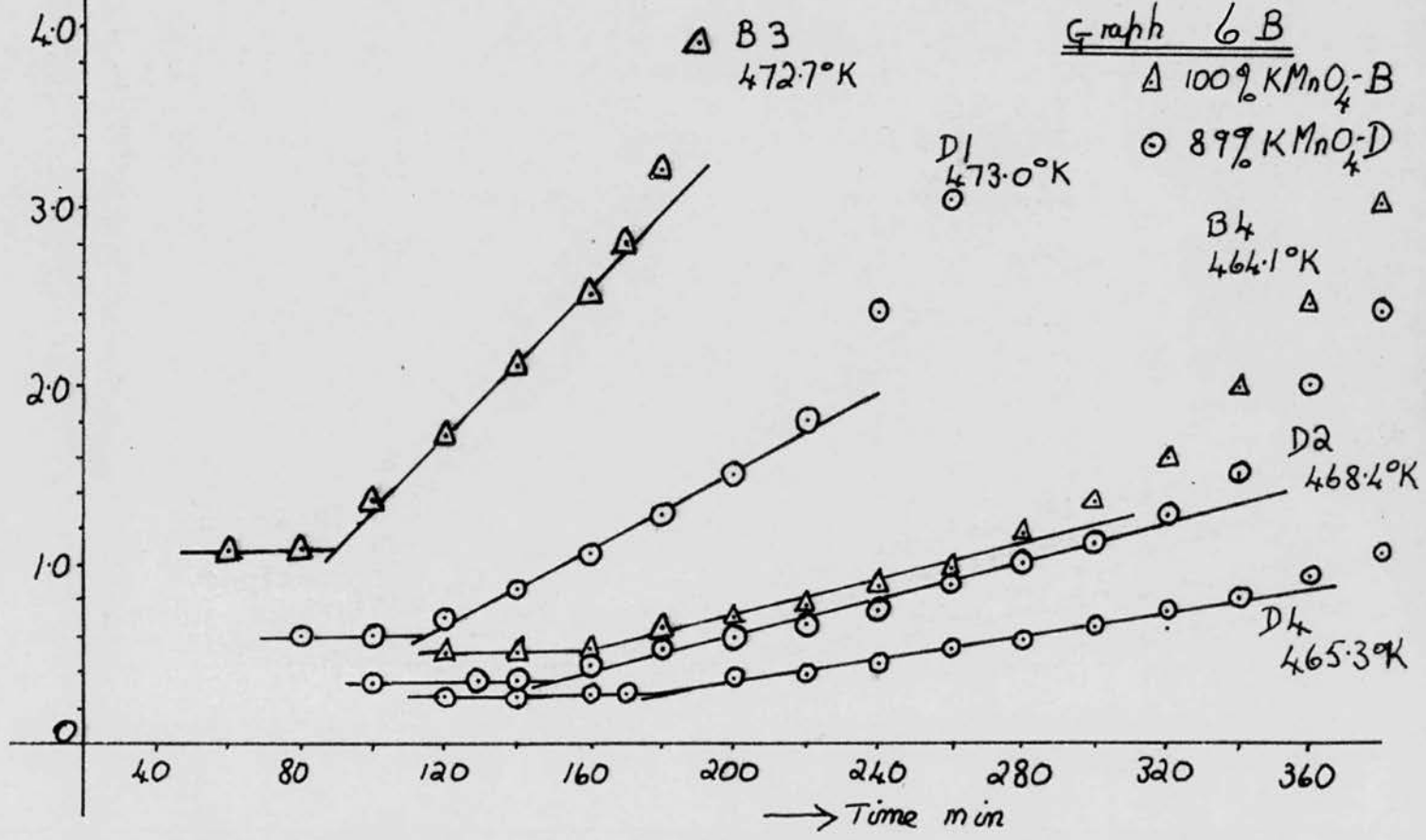
Graph 6 A

○ 70%  $KMnO_4$ -E  
 △ 52%  $KMnO_4$ -F  
 't<sup>2</sup>-stage'



Graph 6 B

△ 100%  $KMnO_4$ -B  
 ○ 89%  $KMnO_4$ -D



# Graph 7

○ 89%  $\text{KMnO}_4$ -D

△ 70%  $\text{KMnO}_4$ -E  
acceleration period

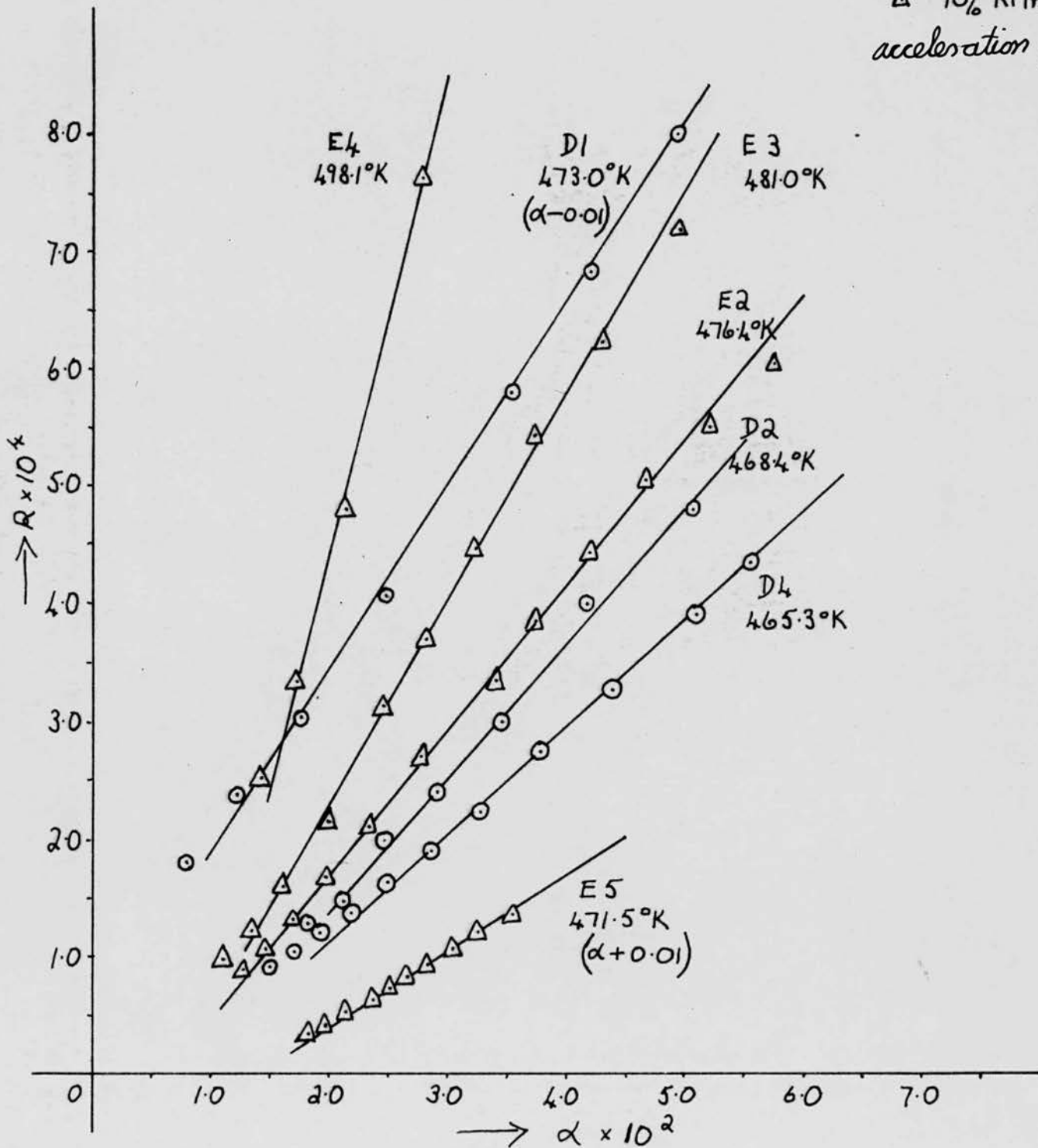


Table 10. Material F 52%  $\text{KMnO}_4$ 

| Run         | F1                   |                 |                               | F4                   |                 |                               |
|-------------|----------------------|-----------------|-------------------------------|----------------------|-----------------|-------------------------------|
|             | 488.0°K              |                 |                               | 498.5°K              |                 |                               |
| Temp        |                      |                 |                               |                      |                 |                               |
| Time<br>min | $\alpha \times 10^2$ | $R \times 10^4$ | $R^{\frac{3}{2}} \times 10^6$ | $\alpha \times 10^2$ | $R \times 10^4$ | $R^{\frac{3}{2}} \times 10^6$ |
| 20          | 0.04                 |                 |                               | 0.16                 | 2.1             |                               |
| 30          | 0.08                 | 0.72            |                               | 0.28                 | 0.8             |                               |
| 40          | 0.16                 |                 |                               | 0.39                 | 0.8             |                               |
| 50          | 0.21                 | 0.39            |                               | 0.48                 | 1.0             |                               |
| 60          | 0.24                 | 0.39            |                               | 0.60                 | 1.2             |                               |
| 70          | 0.28                 | 0.39            |                               | 0.73                 | 1.4             |                               |
| 80          | 0.33                 |                 |                               | 0.87                 | 1.5             |                               |
| 90          | 0.37                 |                 |                               | 1.03                 | 1.8             |                               |
| 100         | 0.43                 | 0.50            |                               | 1.22                 | 2.3             |                               |
| 110         | 0.47                 |                 |                               | 1.48                 | 2.8             | 4.74                          |
| 120         | 0.52                 | 0.58            | 0.44                          | 1.82                 | 4.1             | 8.3                           |
| 130         | 0.58                 |                 |                               | 2.34                 | 6.1             | 15.1                          |
| 140         | 0.64                 | 0.61            | 0.48                          | 3.08                 | 9.0             | 27.0                          |
| 145         |                      |                 |                               | 3.63                 | 11.3            | 38.0                          |
| 150         | 0.70                 |                 |                               | 4.24                 | 13.5            | 49.6                          |
| 155         |                      |                 |                               | 5.08                 | 15.9            | 63.5                          |
| 160         | 0.77                 | 0.71            | 0.60                          | 5.87                 | 17.9            | 75.7                          |
| 165         |                      |                 |                               | 6.85                 | 20.0            | 89.3                          |
| 170         | 0.85                 |                 |                               | 7.82                 | 22.6            | 107                           |
| 180         | 0.93                 | 0.82            | 0.74                          |                      |                 |                               |
| 190         | 1.00                 |                 |                               |                      |                 |                               |
| 200         | 1.11                 | 0.98            | 0.83                          |                      |                 |                               |
| 210         | 1.21                 | 1.12            |                               |                      |                 |                               |
| 220         | 1.33                 | 1.20            | 1.33                          |                      |                 |                               |
| 230         | 1.44                 | 1.32            |                               |                      |                 |                               |
| 240         | 1.59                 | 1.50            | 1.82                          |                      |                 |                               |
| 250         | 1.75                 | 1.80            |                               |                      |                 |                               |
| 260         | 1.95                 | 2.05            | 2.92                          |                      |                 |                               |
| 270         | 2.17                 | 2.46            |                               |                      |                 |                               |
| 280         | 2.47                 | 3.14            | 5.54                          |                      |                 |                               |
| 290         | 2.81                 | 3.5             |                               |                      |                 |                               |
| 300         | 3.19                 | 4.2             | 8.60                          |                      |                 |                               |
| 310         | 3.65                 | 4.8             | 10.5                          |                      |                 |                               |
| 320         | 4.18                 | 5.7             | 13.6                          |                      |                 |                               |
| 330         | 4.77                 | 6.4             | 16.1                          |                      |                 |                               |
| 340         | 5.45                 | 7.2             | 19.2                          |                      |                 |                               |
| 350         | 6.22                 | 8.0             | 22.7                          |                      |                 |                               |

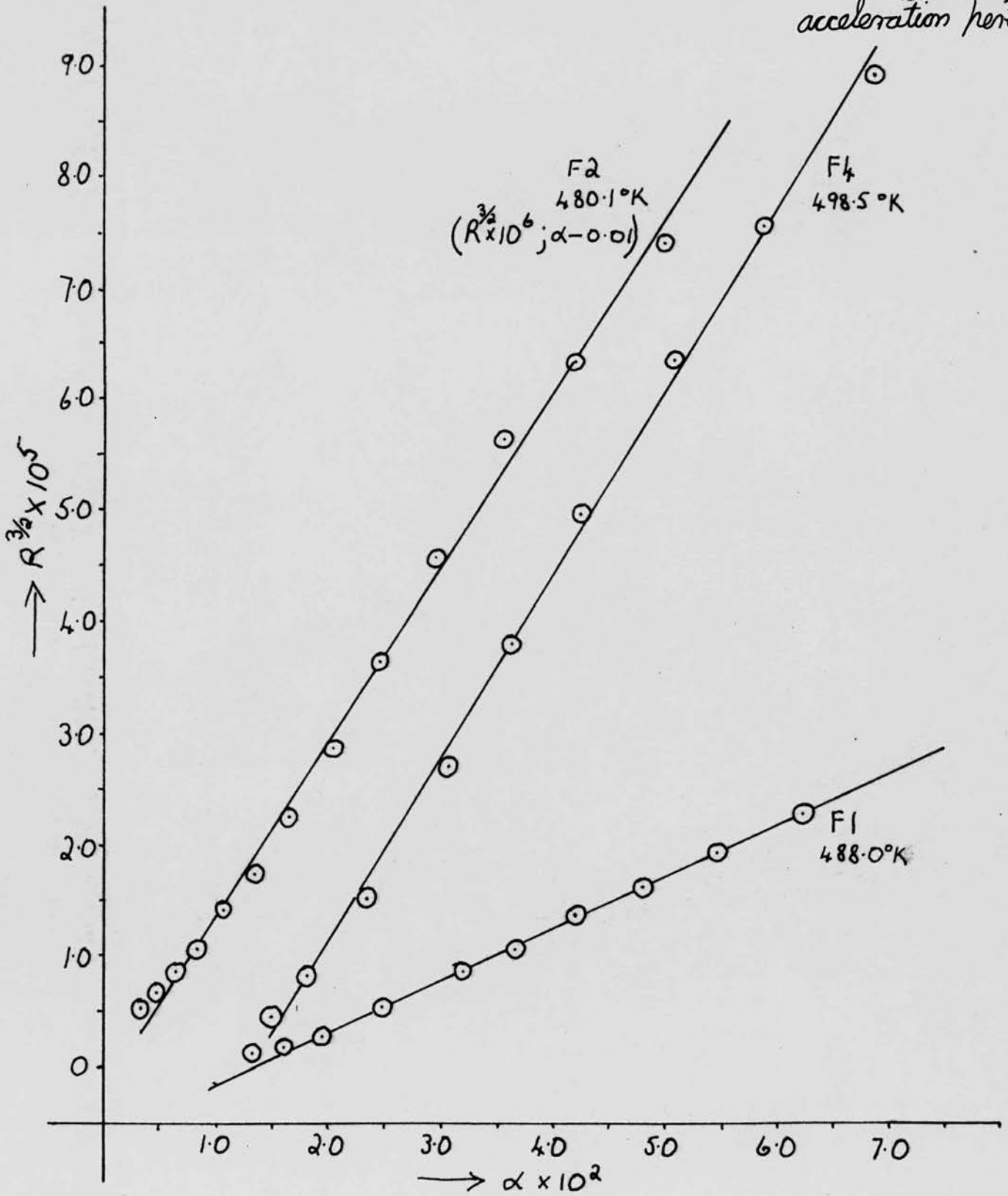


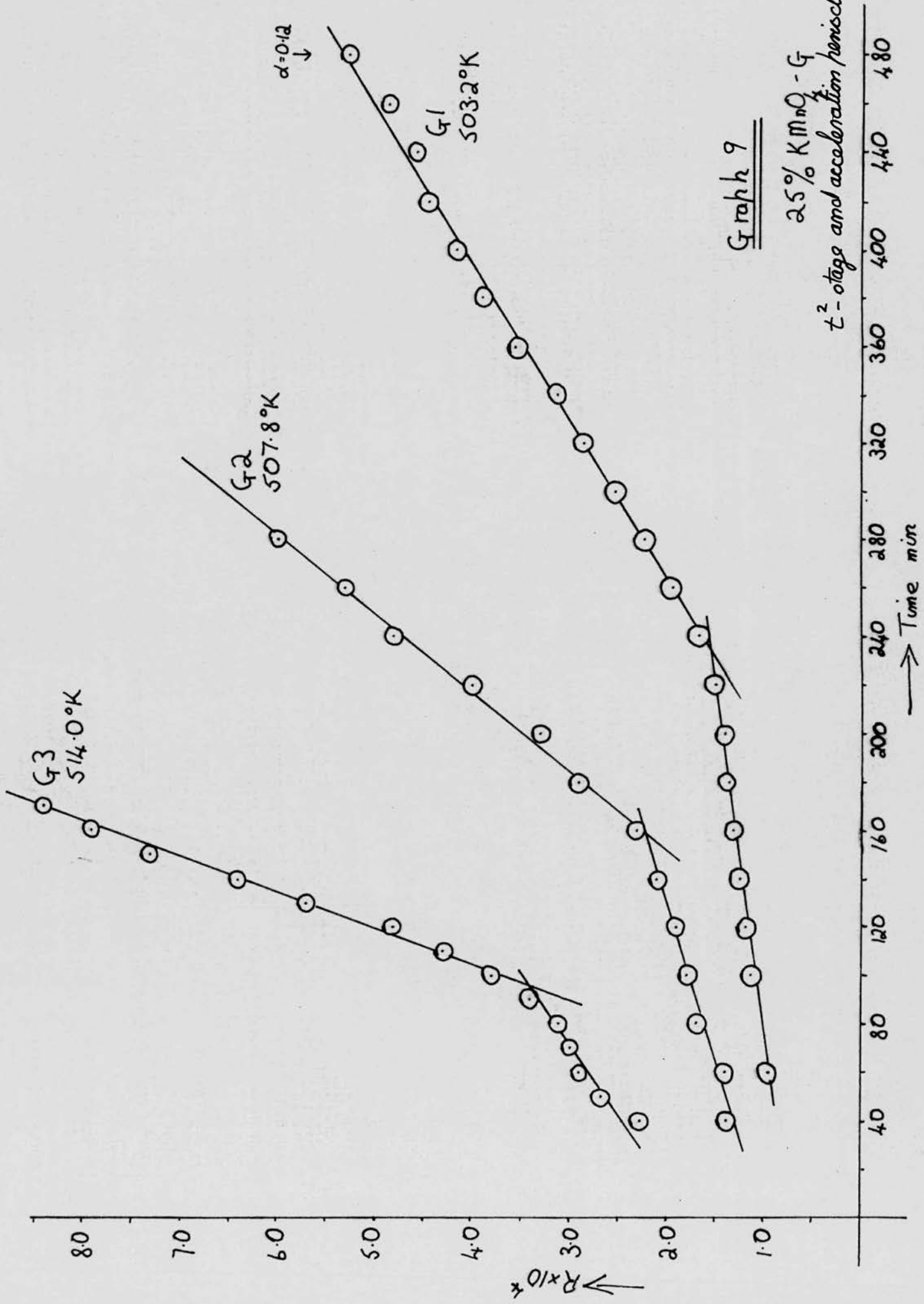
Table 11. Material G 25%  $\text{KMnO}_4$ 

| Run         | G2                   |                 |                               | G3                   |                 |
|-------------|----------------------|-----------------|-------------------------------|----------------------|-----------------|
| Temp        | 507.8°K              |                 |                               | 514.0°K              |                 |
| Time<br>min | $\alpha \times 10^2$ | $R \times 10^3$ | $R^{\frac{3}{2}} \times 10^6$ | $\alpha \times 10^2$ | $R \times 10^4$ |
| 20          | 0.50                 | 0.76            |                               | 0.50                 | 12.7            |
| 30          | 0.76                 |                 |                               | 1.00                 |                 |
| 40          | 0.92                 | 0.14            |                               | 1.24                 | 2.24            |
| 50          | 1.06                 | 0.14            |                               | 1.49                 | 2.64            |
| 60          | 1.22                 |                 |                               | 1.79                 | 2.9             |
| 70          | 1.36                 |                 |                               | 2.06                 | 3.0             |
| 80          | 1.52                 | 0.17            |                               | 2.38                 | 3.1             |
| 90          | 1.70                 |                 |                               | 2.69                 | 3.4             |
| 100         | 1.86                 | 0.18            |                               | 3.05                 | 3.8             |
| 110         | 2.05                 |                 |                               | 3.48                 | 4.3             |
| 120         | 2.22                 | 0.19            |                               | 3.93                 | 4.8             |
| 130         | 2.42                 |                 |                               | 4.42                 | 5.7             |
| 140         | 2.62                 | 0.21            |                               | 5.02                 | 6.4             |
| 150         | 2.82                 |                 |                               | 5.98                 | 7.3             |
| 160         | 3.05                 | 0.23            | 3.6                           | 6.75                 | 7.9             |
| 170         | 3.30                 |                 |                               | 7.28                 | 8.4             |
| 180         | 3.57                 | 0.29            | 4.7                           |                      |                 |
| 190         | 3.88                 |                 |                               |                      |                 |
| 200         | 4.20                 | 0.33            | 5.9                           |                      |                 |
| 210         | 4.51                 |                 |                               |                      |                 |
| 220         | 4.92                 | 0.40            | 8.0                           |                      |                 |
| 230         | 5.37                 |                 |                               |                      |                 |
| 240         | 5.82                 | 0.48            | 10.5                          |                      |                 |
| 250         | 6.63                 |                 |                               |                      |                 |
| 260         | 6.85                 | 0.53            | 12.2                          |                      |                 |
| 270         | 7.40                 |                 |                               |                      |                 |
| 280         | 8.00                 | 0.60            | 14.7                          |                      |                 |

Graph 8

52%  $\text{KMnO}_4$ -F  
acceleration period





Graph 9

25% KMnO<sub>4</sub>-G  
 t<sup>2</sup>-stage and acceleration period



2. 4. 4. Tables and graphs of rate constants

In tables 12 - 17 the rate constants for various runs described in section 2.4.1 - 2.4.3 are tabulated, together with the respective temperatures.

$\underline{R_I}$  is the maximum rate for the initial sigmoid decomposition.

$\underline{R_L}$  is the constant rate for the linear stage.

$\underline{k_2^{\frac{1}{2}}}$  is the rate constant for the 't<sup>2</sup>-stage' from the equation

$\frac{d\alpha}{dt} = 2k_2t + C$  found from the R/t curves. Thus  $\alpha \propto k_2t^2$  representing a power law with  $n = 2$ .

$\underline{k}$  is the rate constant for the acceleration stage from the equation  $\alpha = A \exp(kt)$  found from the plot of  $\frac{d\alpha}{dt} / \alpha$

$\underline{k_3^{\frac{1}{3}}}$  is the rate constant for the acceleration stage in terms of the power law growth with  $n = 3$ , if  $\alpha \propto k_3t^3$ ,  $3^{\frac{2}{3}}k_3^{\frac{1}{2}}$  is found from plotting  $(\frac{d\alpha}{dt})^{\frac{3}{2}} / \alpha$ .

$\underline{k_{22}^{\frac{1}{2}}}$  is the rate constant for the acceleration stage in terms of a power law with  $n = 2$ .

$2k_{22}$  is found from a plot of  $\frac{d\alpha}{dt} / t$  in a similar manner to  $k_2^{\frac{1}{2}}$ .

As the kinetics have been expressed in terms of ' $\alpha$ ', (the fraction of the potassium permanganate that has decomposed in a given time) the rate constants from the different solid solutions are comparable.

For material F and G the exponential equation does not apply, but  $R/\alpha$  was plotted and the value of 'k' measured at  $\alpha = 0.05$  so that the rate constants for the acceleration stage of the solid solutions could be compared on a relative basis.

Table 12. Rate constants for pure potassium permanganate A.

| Run | Temp<br>T <sup>°K</sup> | $\frac{1}{T} \times 10^3$ | $R_I \times 10^5$ | $R_L \times 10^5$ | $k_2^{\frac{1}{2}} \times 10^4$ | $k \times 10^2$ |
|-----|-------------------------|---------------------------|-------------------|-------------------|---------------------------------|-----------------|
| A 6 | 477.8                   | 2.092                     | 30                | 17.4              | -                               | 4.83            |
| 1   | 471.2                   | 2.122                     | 17.5              | 7.0               | -                               | 3.75            |
| 5   | 470.0                   | 2.130                     | 18.0              | 9.2               | -                               | 3.0             |
| 3   | 468.3                   | 2.135                     | 13.6              | 5.5               | -                               | 2.9             |
| 2   | 465.2                   | 2.150                     | 10.5              | 4.3               | -                               | 1.9             |
| 4   | 458.3                   | 2.182                     | 6.4               | 2.7               | -                               | 1.2             |

Table 13. Rate constants for pure potassium permanganate B.

|     |       |       |      |      |     |     |
|-----|-------|-------|------|------|-----|-----|
| B 1 | 498.4 | 2.007 | 131  | 81   | -   | 16  |
| 2   | 498.4 | 2.007 | 88   | 60   | -   | 18  |
| 5   | 486.1 | 2.057 | 62   | 38   | 31  | 6.5 |
| 3   | 472.7 | 2.116 | 26   | 10.8 | 8.9 | 2.2 |
| 4   | 464.1 | 2.155 | 13.4 | 4.8  | 4.5 | 1.0 |

Table 14. Rate constants for solid solution D, 89%  $KMnO_4$ .

|     |       |       |     |     |     |     |
|-----|-------|-------|-----|-----|-----|-----|
| D 5 | 478.7 | 2.091 | 11  | 7.2 | 11  | 3.6 |
| 1   | 473.0 | 2.114 | 7.7 | 5.3 | 7.8 | 1.6 |
| 3   | 471.6 | 2.120 | 6.2 | 3.8 | 7.6 | 1.6 |
| 2   | 468.4 | 2.135 | 5.0 | 3.5 | 4.7 | 1.1 |
| 4   | 465.3 | 2.149 | 4.2 | 2.8 | 3.3 | 0.9 |



Table 15. Rate constants for solid solution E, 70%  $\text{KMnO}_4$ .

| Run | Temp<br>$T^{\circ}\text{K}$ | $\frac{1}{T} \times 10^3$ | $R_I \times 10^5$ | $R_L \times 10^5$ | $k_2^{\frac{1}{2}} \times 10^4$ | $k_3^{\frac{1}{3}} \times 10^4$ | $k \times 10^2$ |
|-----|-----------------------------|---------------------------|-------------------|-------------------|---------------------------------|---------------------------------|-----------------|
| E 4 | 489.2                       | 2.045                     | 13.6              | 5.1               | 7.1                             | -                               | 4.1             |
| 1   | 485.5                       | 2.060                     | 9.0               | 4.2               | 6.6                             | -                               | 2.7             |
| 3   | 481.0                       | 2.079                     | 6.0               | 3.3               | 4.1                             | -                               | 1.7             |
| 2   | 476.4                       | 2.099                     | 3.6               | 2.6               | 3.5                             | -                               | 1.2             |
| 5   | 471.5                       | 2.123                     | 2.2               | 1.1               | 2.2                             | -                               | 0.65            |

Table 16. Rate constants for solid solution F, 52%  $\text{KMnO}_4$ .

|     |       |       |     |     |     |     |       |
|-----|-------|-------|-----|-----|-----|-----|-------|
| F 4 | 498.5 | 2.006 | 21  | 8.0 | 10  | 47  | (3.2) |
| 3   | 495.5 | 2.018 | 10  | 6.8 | 7.1 | 35  | (2.6) |
| 1   | 488.0 | 2.049 | 7.2 | 3.9 | 4.5 | 20  | (1.5) |
| 2   | 480.1 | 2.083 | 3.0 | 2.1 | 2.6 | 9.5 | (0.7) |

Table 17. Rate constants for solid solution G, 25%  $\text{KMnO}_4$ .

| Run | Temp<br>$T^{\circ}\text{K}$ | $\frac{1}{T} \times 10^3$ | $R_I \times 10^5$ | $R_L \times 10^5$ | $k_2^{\frac{1}{2}} \times 10^4$ | $k_3^{\frac{1}{3}} \times 10^4$ | $k \times 10^2$ |
|-----|-----------------------------|---------------------------|-------------------|-------------------|---------------------------------|---------------------------------|-----------------|
| G 3 | 514                         | 1.946                     | 127               | -                 | 9.1                             | 18.2                            | (1.1)           |
| 2   | 507.7                       | 1.969                     | 76                | -                 | 6.2                             | 12.3                            | (0.8)           |
| 1   | 503                         | 1.987                     | 83                | -                 | 4.1                             | 8.7                             | (0.6)           |

In graphs 10 and 11, the Arrhenius activation energy plots are shown for the various temperatures dependent constants given in tables 12 - 17.

These graphs clearly illustrate the lowering of the rate constants with the increasing percentage of potassium perchlorate in the solid solutions. From graph 10 the activation energy of the rate constant 'k' for the acceleration is ca 39 kcal mole<sup>-1</sup>, similar to the value found by Prout and Tompkins<sup>27</sup>. The solid solutions appear to have the same activation energy as for the pure potassium permanganate, although insufficient evidence is available to define clearly the activation energies.

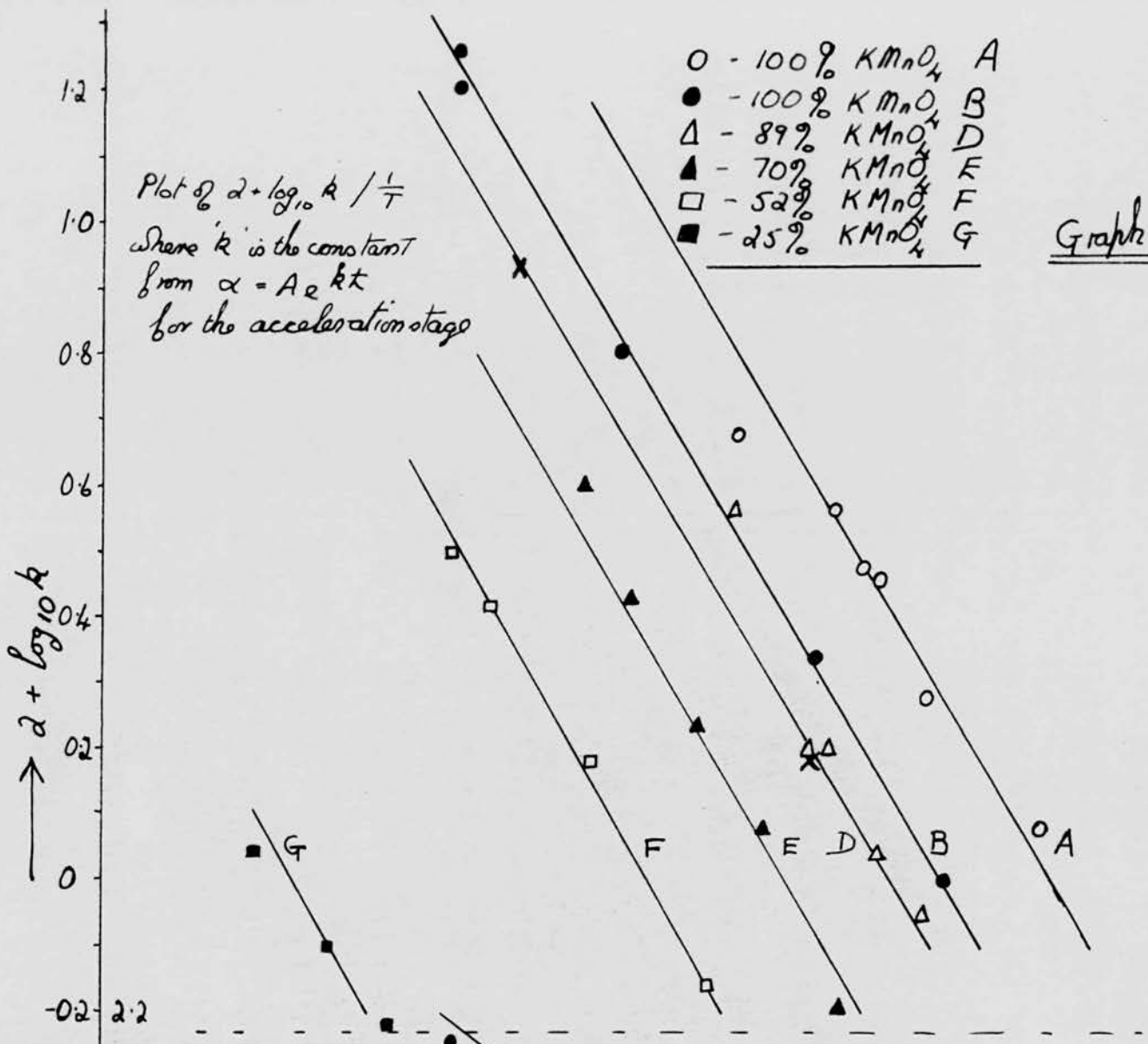
Graph 10 also illustrates the activation energy plots for 'R<sub>I</sub>', the maximum rate for the initial sigmoid decomposition. Pure permanganate (A and B) has an activation energy of 35 ± 5 kcal mole<sup>-1</sup> and there is an apparent increase for the solid solution rising to 46 ± 5 for F (52% KMnO<sub>4</sub>).

In graph 11 the plots are shown for the linear and 't<sup>2</sup>-stage', both of which have activation energies of 39 ± 6 kcal mole<sup>-1</sup>, independent of perchlorate concentration. For the linear constant rate stage Prout<sup>76</sup> reported a value of 25.5 kcal mole<sup>-1</sup> which is definitely outside the maximum error for this work.

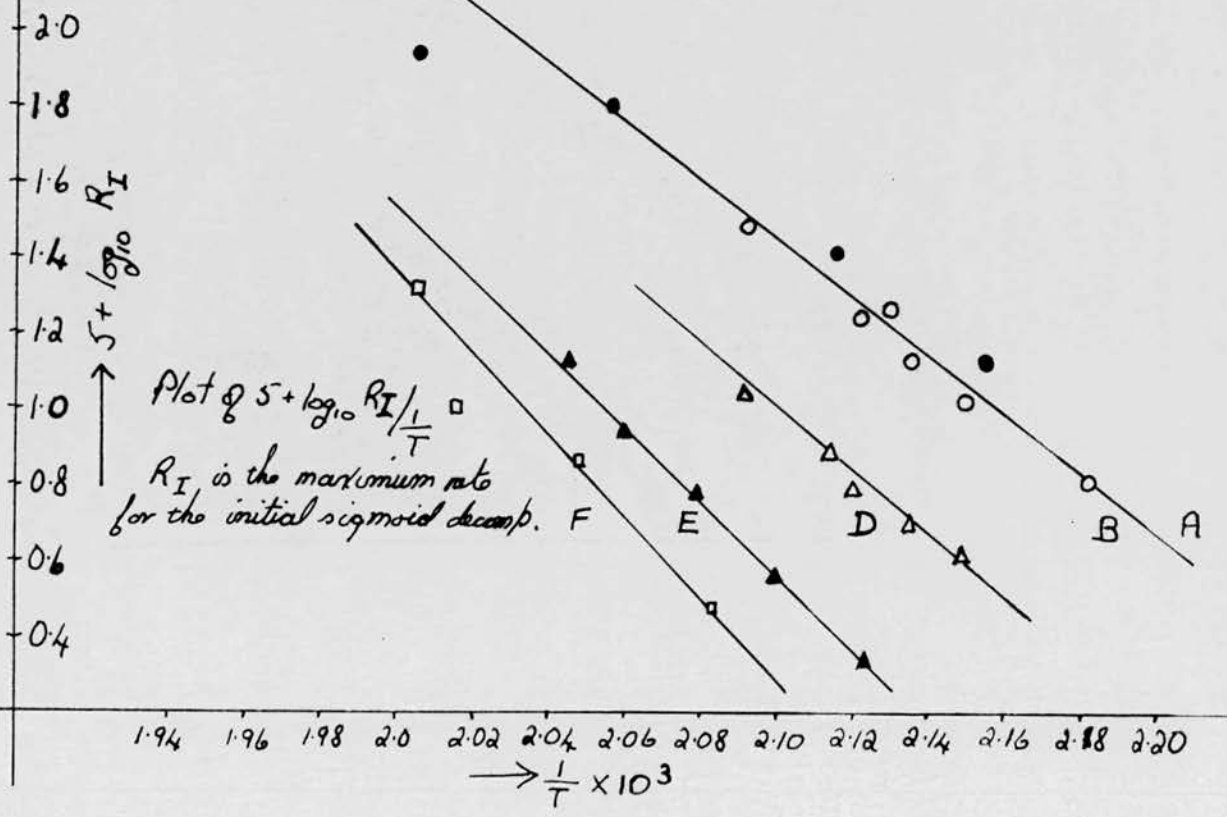
Graph 10

- O - 100% KMnO4 A
- - 100% KMnO4 B
- △ - 89% KMnO4 D
- ▲ - 70% KMnO4 E
- - 52% KMnO4 F
- - 25% KMnO4 G

Plot of  $a + \log_{10} k / \frac{1}{T}$   
 where 'k' is the constant  
 from  $\alpha = A e^{-kt}$   
 for the acceleration stage



Plot of  $5 + \log_{10} R_I / \frac{1}{T}$   
 where  $R_I$  is the maximum rate  
 for the initial sigmoidal decomp.



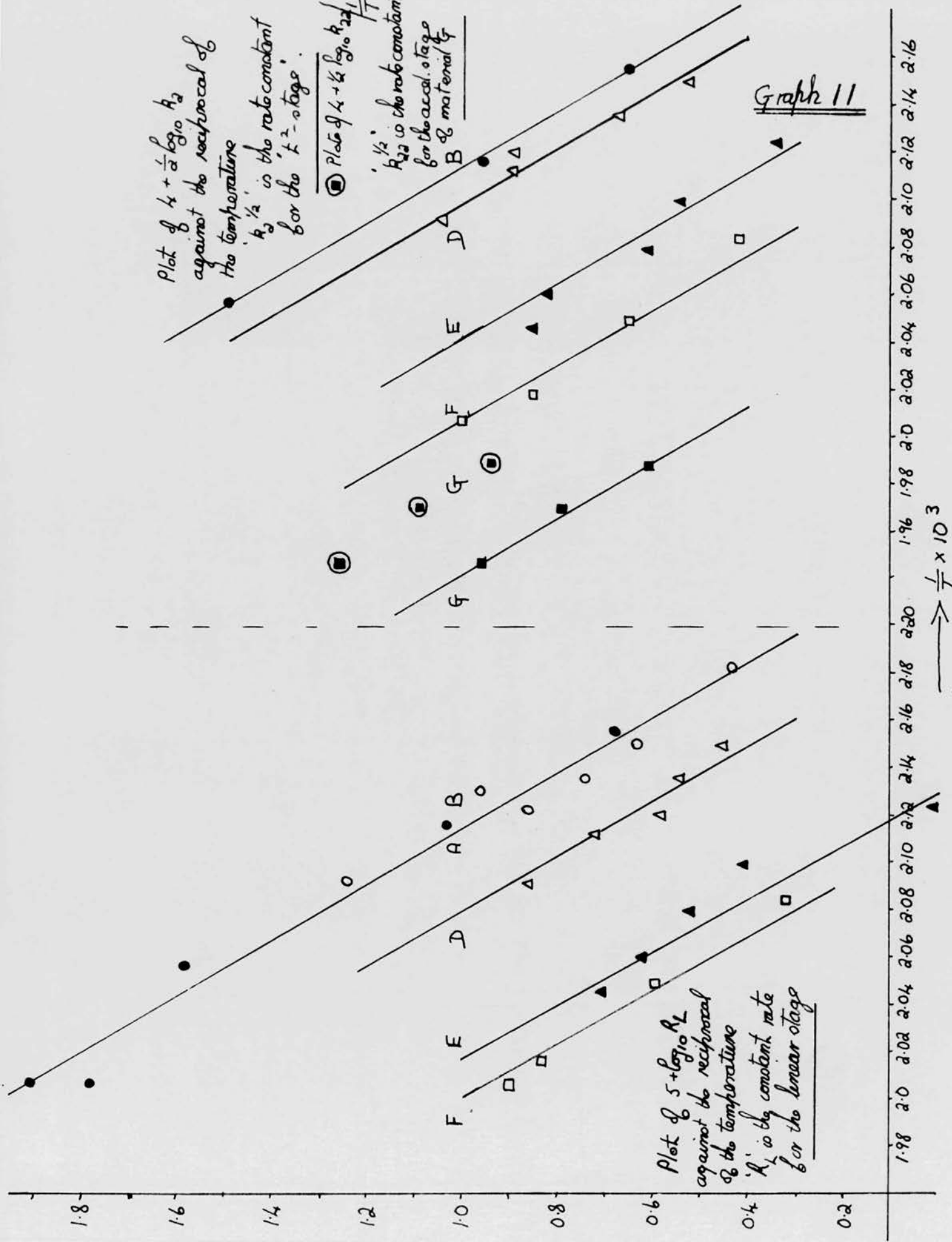


Plot of  $k + \frac{1}{2} \log_{10} k_2$   
against the reciprocal of  
the temperature

' $k_2^{1/2}$ ' is the rate constant  
for the 'k<sup>2</sup>-stage'

Plot of  $k + \frac{1}{2} \log_{10} \frac{k_2}{T}$   
' $k_2^{1/2}$ ' is the rate constant  
for the accel. stage  
of material G

Graph 11



Plot of  $5 + \log_{10} R_L$   
against the reciprocal  
of the temperature  
' $R_L$ ' is the constant rate  
for the linear stage

1.98 2.0 2.02 2.04 2.06 2.08 2.10 2.12 2.14 2.16

$\rightarrow \frac{1}{T} \times 10^3$

3.

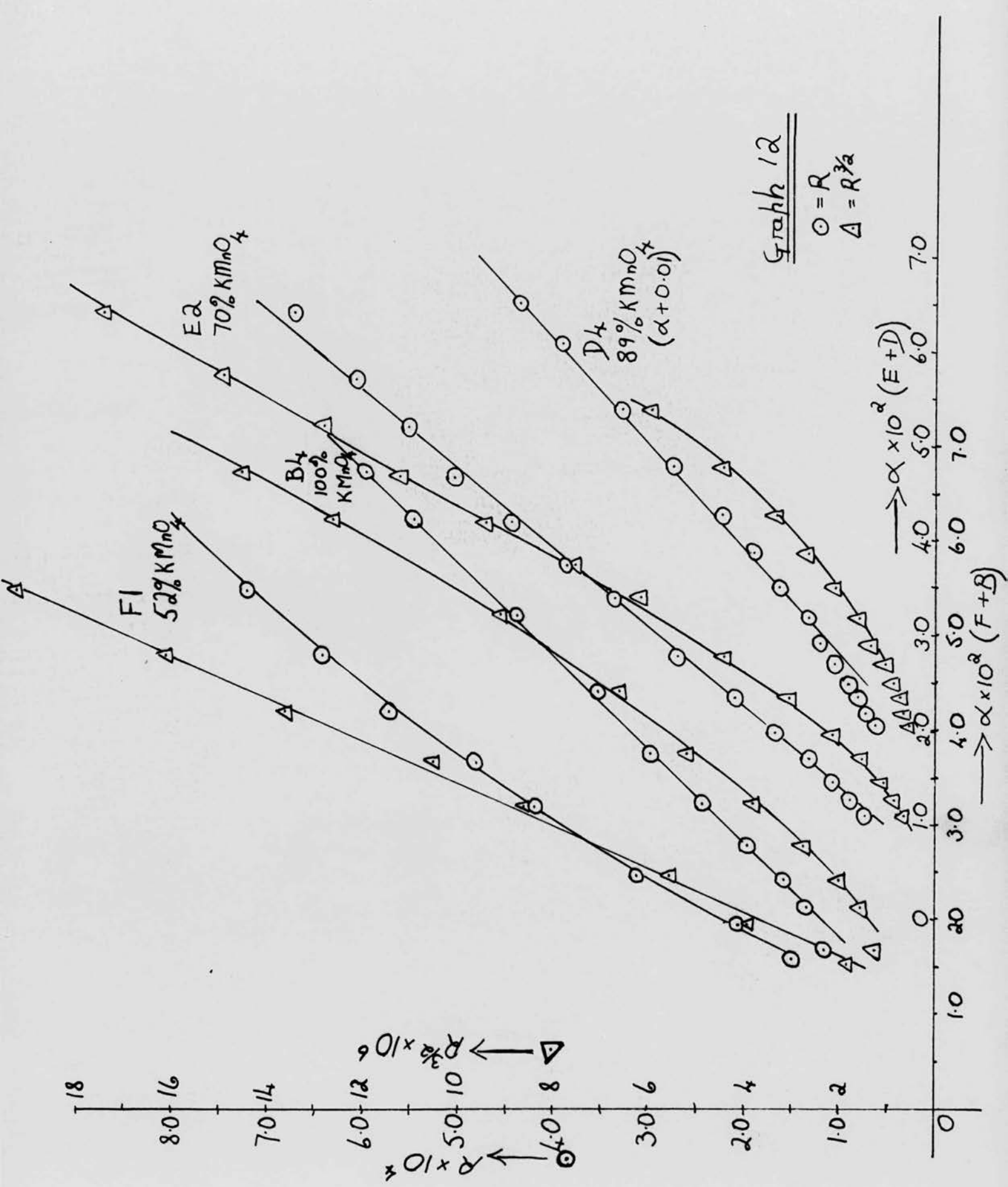
Discussion

Previous work on the isothermal decomposition of fresh large crystals of potassium permanganate has shown that the acceleration stage is best represented by an equation of the form  $\alpha = A \exp(kt)$ , at least up to  $\alpha = 0.1$ , and that this is preceded by a slow reaction<sup>27,78</sup>. The primary object of this work was to investigate the effects on the decomposition of the addition of potassium perchlorate to the potassium permanganate lattice. Hinshelwood and Bowen<sup>70,71</sup> noted that the rate of the decomposition fell, but they did not investigate any changes in the kinetics of the reaction.

Generally, all the materials showed an initial sigmoid decomposition, a linear stage and a 't<sup>2</sup>-stage' where there was a linear increase in rate with time. These three stages will be considered as the pre-acceleration period. This is followed at ca  $\alpha = 0.02$  by an acceleration stage which for the pure permanganate and the solid solutions with 89 and 72% permanganate is best expressed by the exponential relationship, but for solution F (52%  $\text{KMnO}_4$ ) a power law with  $n = 3$  is preferred.

The exponential and power law equations are compared in graph 12. For material G (25%  $\text{KMnO}_4$ ) a power law with  $n = 2$  is satisfactory as there is a linear increase in rate with time graph 9 (2.4.3.) .

The various rate constants are compared in table 18, which is constructed from graphs 10 and 11. The logarithms of the rate constants at 490°K are tabulated, together with the ratio





of the rate constants for the solid solutions compared with those for pure permanganate B. This ratio represents the relative lowering of the rate constants due to the presence of the perchlorate. In graph 13 this ratio is plotted against the mole percent of potassium permanganate in the solid solutions.

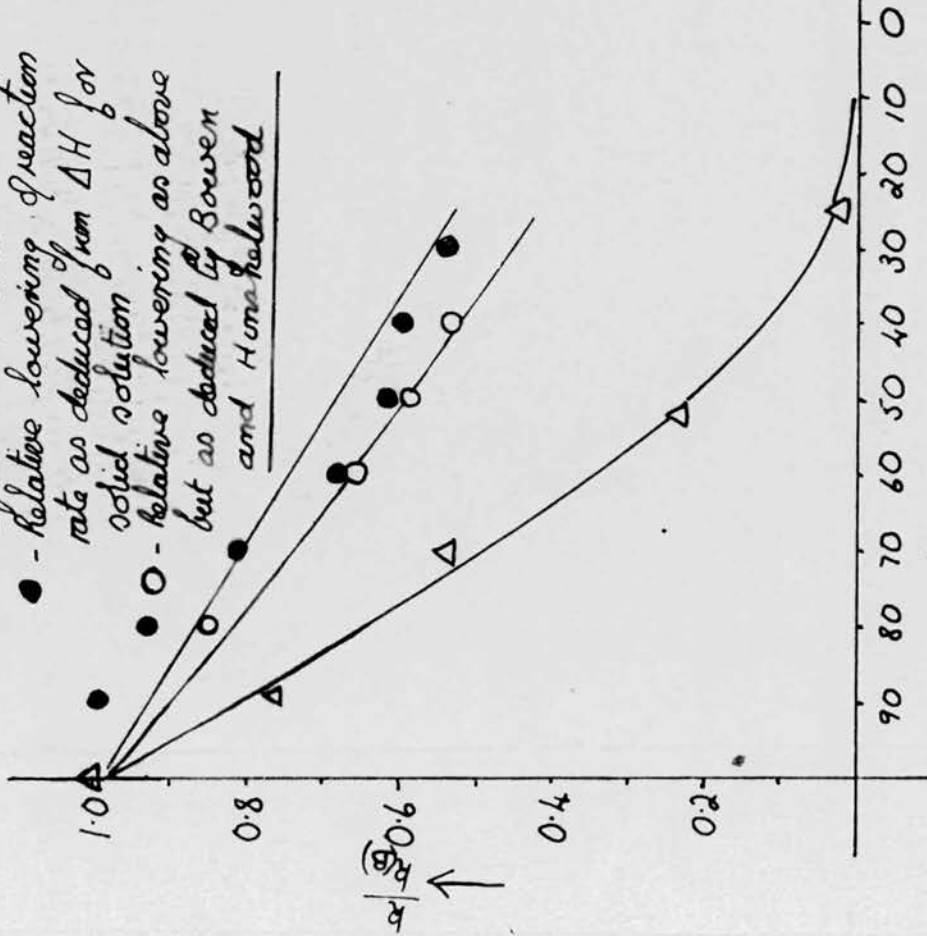
Table 18

| M | $\log_{10} \frac{R_I}{5}$ | $\frac{R_I}{R_I(B)}$ | $\log_{10} \frac{R_L}{5}$ | $\frac{R_L}{R_L(B)}$ | $\frac{1}{2} \log_{10} \frac{k_2}{4}$ | $\frac{k_2}{k_2(B)}$ | $\frac{1}{2} \log_{10} \frac{k}{2}$ | $\frac{k}{k(B)}$ |
|---|---------------------------|----------------------|---------------------------|----------------------|---------------------------------------|----------------------|-------------------------------------|------------------|
| A | 1.9                       | 1.0                  | 1.62                      | 1.0                  | -                                     | -                    | 1.25                                | 1.9              |
| B | 1.9                       | 1.0                  | 1.62                      | 1.0                  | 1.62                                  | 1.0                  | 0.95                                | 1.0              |
| D | 1.5                       | 0.39                 | 1.33                      | 0.51                 | 1.49                                  | 0.74                 | 0.83                                | 0.76             |
| E | 1.1                       | 0.16                 | 0.80                      | 0.15                 | 1.0                                   | 0.24                 | 0.58                                | 0.54             |
| F | 0.9                       | 0.10                 | 0.65                      | 0.10                 | 0.7                                   | 0.12                 | 0.22                                | 0.23             |
| G | -                         | -                    | -                         | -                    | 0.15                                  | 0.03                 | -0.70                               | 0.02             |

The relative decrease in the pre-acceleration rate constants ( $R_L, R_I, k_2^{\frac{1}{2}}$ ) show the same pattern of a rapid lowering for the first 20 - 30% of perchlorate; this probably indicates that the three stages are involved with the same mechanism. For the acceleration period the effect of the perchlorate on the rate constant 'k' is less pronounced suggesting a different mechanism is involved. This is not unreasonable if the acceleration period involves the bulk of the crystal and the pre-acceleration the external and internal surfaces, as was the case for potassium metaperiodate.

$\Delta - \frac{k}{k(B)}$  is the rate constant for the acceleration, from the equation  $\alpha = A e^{\frac{E}{RT}}$

- - Relative lowering of reaction rate as deduced from  $\Delta H$  for solid solution
- - Relative lowering as above but as deduced by Bowen and Hammett



Graph 13

← mole percentage of potassium permanganate

- $\frac{R_I}{R_I(B)}$  for the maximum rate of the initial sigmoid decomposition
- $\frac{R_L}{R_L(B)}$  for the constant rate of the linear stage
- $\frac{k_2^{1/2}}{k_2^{1/2}(B)}$  for the 't<sup>2</sup>-stage'

The pre-acceleration period

The initial sigmoid decomposition that extended to  $\alpha = 0.006$  for the pure permanganate A and B was not present in the ' $\alpha$ ' - ' $t$ ' curve of a single large crystal (C 3, page 117), indicating a dependence on surface area. A similar initial sigmoid decomposition was found in ground barium permanganate but was not present for whole crystals<sup>40</sup>. This probably represents the decomposition of active spots on the surface and some of the subgrain boundaries, which creates a constant area interface that progresses into the subgrains giving rise to the linear stage. The value of ' $\alpha$ ' at the end of the sigmoid stage decreases with increasing permanganate content (graph 3, 2.4.1.) due perhaps to a decrease in the number of active spots on the surface. Solid solution G (25%  $\text{KMnO}_4$ ) is anomalous as the sigmoid extends to  $\alpha = 0.01$ ; this is probably due to the greatly increased surface area produced by the rapid crystallisation resulting in an increase in the number of active centres.

The linear stage is followed by a ' $t^2$ -stage' (graph 6) in all cases except pure permanganate A. The linear stage represents decomposition into the subgrains as was postulated for potassium metaperiodate, but if at the same time the decomposition spreads down undecomposed subgrain boundaries, the area of the interface will increase linearly with time giving rise to ' $t^2$ ' kinetics. This is a similar mechanism to that proposed by Tompkins and Young<sup>81</sup> for the dehydration of barium styphnate monohydrate. The addition of perchlorate to the lattice lowers the initial sigmoid decomposition which probably entails a decrease in the number of



subgrain boundaries that have initially decomposed, and thus the boundaries decompose simultaneously with the linear growth into the subgrains which results in the 't<sup>2</sup>-stage'. For solid solutions F and G (52 and 52% KMnO<sub>4</sub>) the linear stage has virtually disappeared and thus the 't<sup>2</sup>-stage' starts directly after the initial surface decomposition.

#### Acceleration period

If the acceleration period is interpreted in terms of the Prout-Tompkins mechanism the pre-acceleration period produces the strains along the internal surfaces that cause the branching<sup>27,62,61</sup>. The reduced values of 'k' (table 18) for the solid solutions may be due to (1) fewer imperfections at which branching occurs, (2) lower stresses at the interface of the reactant and products. As these are solid solutions the number of imperfections should be reasonably constant, so probably the second effect predominates.

For the solid solutions the product of the permanganate decomposition is embedded in potassium perchlorate, and as the perchlorate crystal lattice is identical to that of the solid solutions, the higher the percentage of perchlorate present the closer the structure of the product (including the perchlorate) will be to that of the solid solution. Thus the higher the percentage of perchlorate the lower the stress between the reactant and product. For  $\frac{[ClO_4^-]}{[MnO_4^-]}$  of 0,  $\frac{1}{9}$ ,  $\frac{3}{7}$  (AB, D and E) there is a linear decrease in 'k' with respect to the  $[ClO_4^-]$ , in agreement with the theory. The situation arises when the probability of

branching ceases to control the rate of the reaction and individual nuclei become of importance leading to three dimensional growth (F). When each permanganate ion is surrounded by a high proportion of perchlorate ions (3:1 in G) a coherent interface becomes impossible to maintain and two dimensional growth appears to apply with the reaction perhaps spreading in some sort of zig-zag fashion throughout the lattice. Thus the environment of the permanganate ion governs the kinetics of the decomposition.

The decomposition of pure permanganate A and B are identical for the initial sigmoid and linear stages, but the rate constant 'k' for A is 90% greater than that for B. This fact combined with the absence of a 't<sup>2</sup>-stage' and the inferior external form of the crystals A indicates an increased density of dislocations leading to a higher rate of branching that can start directly after the linear stage. The value of 'k' found by Prout and Tompkins<sup>27</sup> for large single crystals corresponds to the value for D (89% KMnO<sub>4</sub>). As the crystals used in the present experiments are about  $\frac{1}{50}$ <sup>th</sup> the size of those used by Prout and Tompkins a slower rate is to be expected according to Komatsu's general observations<sup>78</sup>. Boldyrev and Zakharov<sup>82</sup> have reported that the rate of decomposition of potassium permanganate varies for the different crystal faces, so both the size and shape affect the rate of decomposition.

Hill<sup>32</sup> has suggested, as an alternative explanation for the exponential acceleration of the decomposition, that nuclei are created by the diffusion of the product into the unreacted lattice. This is to some extent supported by the observations



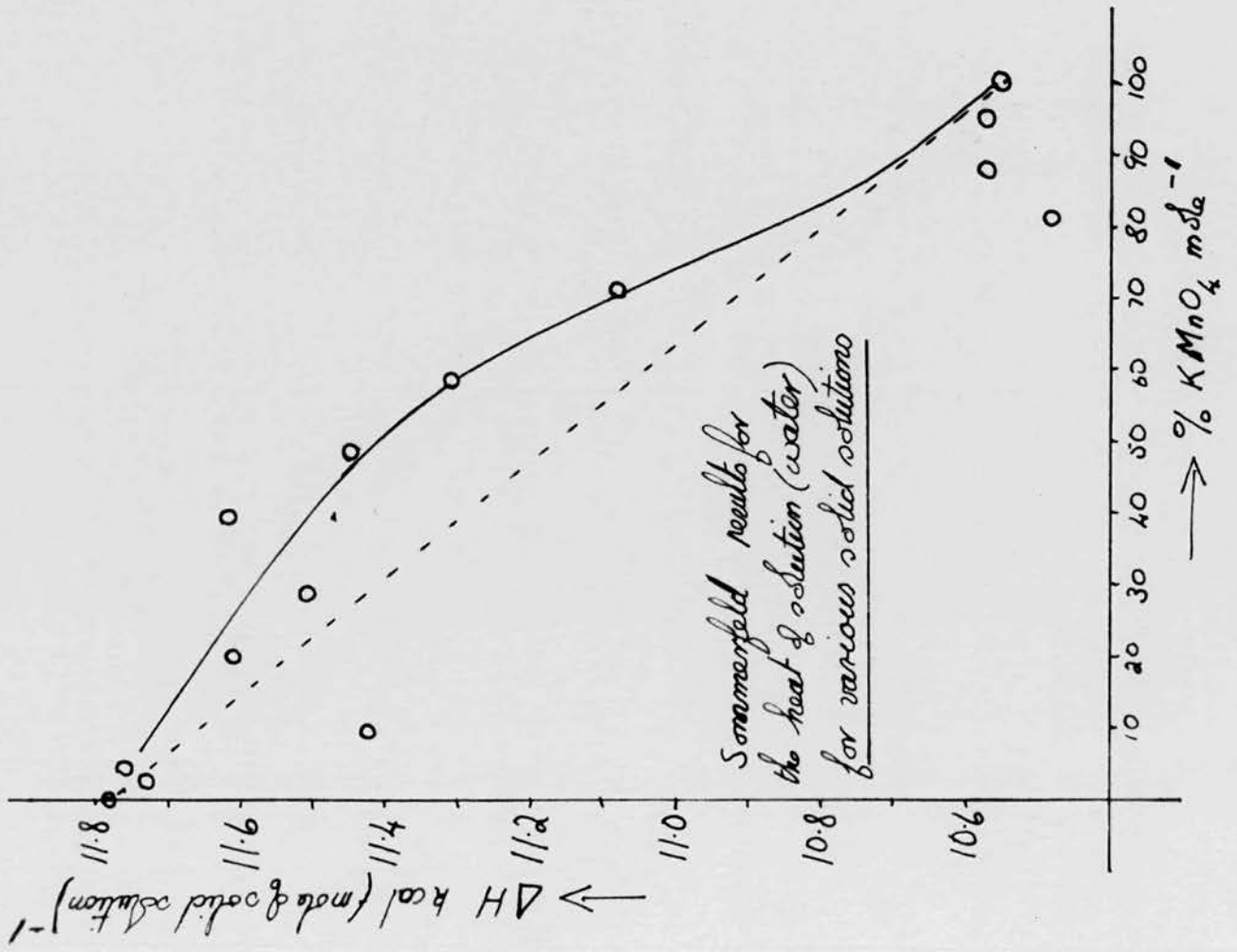
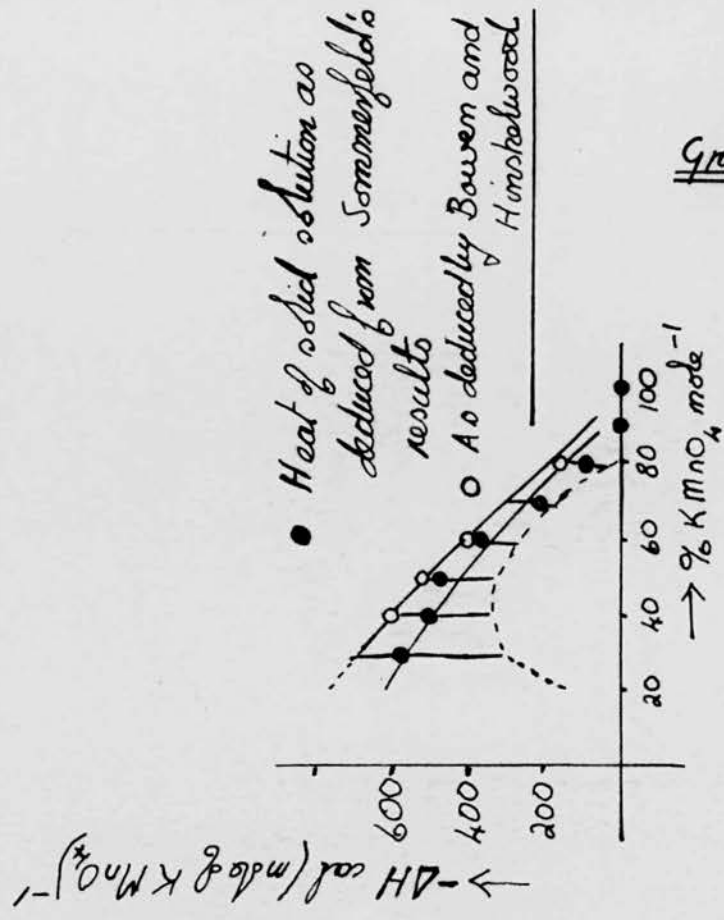
of Hill and Wallace on the diffusion of molybdenum through the dislocation network of potassium permanganate<sup>83</sup>. The presence of perchlorate ions would not be expected to affect materially the diffusion of the product through the lattice as they are similar to permanganate ions. Thus the kinetics of the decomposition of the solid solutions should not be affected by the perchlorate content, which was not found to be the case.

Diffusion as a means of creating nuclei can be combined with the Prout-Tompkins mechanism by considering diffusion along the dislocations as included in the concept of branching. If the reaction interface branches when it meets a dislocation, the prior nucleation of the dislocation by diffusion, will perhaps assist the branching.

The lowering in the rate of the decomposition has been primarily explained in terms of a decrease in the rate of increase of the reaction interface, i.e. a change in the pre-exponential factor of the Arrhenius equation. Hinshelwood and Bowen<sup>71</sup> considered that the change in rate was due to an increase in activation energy as a result of the added stability of the permanganate ion in the perchlorate lattice. This was deduced from the heats of solution (water) of the solid solutions as given by Sommerfeld<sup>84</sup>. His results are shown in graph 14, the dotted line representing the additive heats of solution of potassium permanganate and potassium perchlorate, and the circles the heats of solution of the solid solutions. The heats of solution are slightly higher than the purely additive effect due



Graph 14



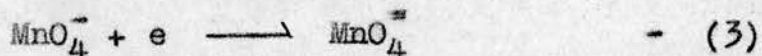
to the heat of solid solution. The values of the heat of solid solution per mole of potassium <sup>permanganate</sup> cannot be stated precisely due to the wide scatter of the points, and may lie anywhere within the dotted lines shown in graph 14.

Hinshelwood assumed that a change in the activation energy of the permanganate ion was caused by a difference in surroundings and was equal to the heat given out when passing from one surrounding to another. The relative rates of decomposition for different solid solutions can thus be calculated from the heats of permanganate/perchlorate. In graph 13 the relative decrease in rates are plotted, illustrating that the expected decrease in activation energies is insufficient to explain the decrease in rate.

The effect of the perchlorate ion on the acceleration period (the bulk effect) is mainly one of alteration in kinetics leading to a change in 'A factor', although the increase in activation energy will contribute to the decrease in rate. For the pre-acceleration period the rate constants are sharply decreased for only a small percentage of perchlorate and this may be due to a higher concentration of perchlorate at the surface and subgrain boundaries than in the bulk of the crystal. There would thus be less permanganate to decompose in the early stages. This necessitates a preferential adsorption of perchlorate at the main boundaries of the crystal during crystallisation.

The actual mechanism of the decomposition of the permanganate ion is probably complex and is not one of simple thermal breakdown as may be the case for the metaperiodate ion. Smirnova<sup>85</sup> has

suggested the following mechanism,



From his previous results<sup>77</sup> he has deduced, on somewhat dubious grounds, activation energies for the various steps and has shown that step one is the difficult stage. The first step is presumed to occur at the surface; the electron which is liberated moves in a conduction band until it is trapped by a permanganate ion. This mechanism allows for the production of manganate ions in the bulk of the crystal. The theory is plausible but the experimental grounds on which it is based are flimsy.

The conductivity of a single crystal of potassium permanganate was measured in the range 300 - 400°K by the same procedure as was used in section I (2.7.). The conductivity of the crystal could approximately be expressed by  $\sigma = 10^{-2} \exp(-10000/RT) \text{ ohm}^{-1} \text{ cm}^{-1}$ , giving a conductivity of  $10^{-7} \text{ ohm}^{-1} \text{ cm}^{-1}$  at 470°K. This is a high conductivity which perhaps supports the mechanism proposed by Smirnova. The photoconductance of potassium permanganate would perhaps throw further light on the mechanism of decomposition.



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