# Femtosecond Laser Inscribed Y-Branch Waveguide in Nd:YAG Crystal: Fabrication and Continuous-Wave Lasing 

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#### Abstract

Rectangular Y-branch cladding waveguides have been fabricated in Nd:YAG crystal by femtosecond laser inscription. Such novel configurations are fabricated with depth of $50 \mu \mathrm{~m}$, supporting multimode guidance in both TM and TE polarizations. Continuous wave laser oscillations at wavelength of $1.06 \mu \mathrm{~m}$ have been achieved under the optical pump at 808 nm . The maximum output power is 0.2 W with a slope efficiency of $20 \%$ in the device with splitting angle of $0.5^{\circ}$.


Index Terms-Optical waveguides, femtosecond laser inscription, waveguide lasers, Y-branch waveguides.

## I. Introduction

AS THE basic components in integrated optics, waveguides possess advantages of confinement of the light propagation compactly in small volumes, in which higher optical density could be achieved with respect to bulk materials, which is beneficial to the construction of high-performance photonic devices in small scales of dimensions [1], [2]. In active media, the compressed volume in waveguide geometries leads to high optical intensities of pump beams inside the structures, and results in laser oscillations in waveguides with reduced threshold and enhanced efficiency with respect to the bulks [3]-[5]. The femtosecond laser inscription (FLI) has been first reported to be utilized to fabricate optical waveguides in glasses in 1996 [6]. As an efficient technique for direct microprocessing of transparent dielectric materials, the FLI possesses unique 3-D capability for device production compared with other traditional waveguide fabrication techniques, such as ion exchange, ion

[^0]irradiation [7]-[9]. Focused femtosecond-laser pulses produce localized modification in micro- or sub-micrometer scales in the bulk materials. The parameters of the femtosecond laser pulses, such as wavelength, pulse energy, pulse duration, polarization as scanning speed [3], [9], [10], are critical for the refractive index modifications of the materials. Waveguides fabricated by FLI have been realized in a number of gain crystals and ceramics, e.g., rare-earth ions ( Nd or Yb ) doped neodymium doped yttrium aluminum garnet ( $\mathrm{Nd}: \mathrm{Y}_{3} \mathrm{Al}_{5} \mathrm{O}_{12}$ or $\left.\mathrm{Nd}: \mathrm{YAG}\right)$ [11]-[15], GGG [16], KGW [17], vanadate crystals $\left(\mathrm{GdVO}_{4}\right.$ and $\left.\mathrm{YVO}_{4}\right)$ [18], [19] as well as nonlinear crystals (such as $\mathrm{BiBO}_{3}$ and $\mathrm{KTiOPO}_{4}$ ) [20], [21], and in various glasses [22]. The depressed cladding waveguides confine light propagation in channels which are surrounded by numbers of low-index tracks, different from dualline waveguides which are located in the region between two filaments with reduce indices [5], [23]. In addition, in cubic crystals of YAG or GGG, the dual-line structures only support light propagating at TM polarization, whilst the cladding structures enable mode confinement at any transverse polarizations.

Nd :YAG crystal is one of the most widely used gain media for solid-state lasers for its outstanding fluorescence, thermal and mechanical properties. Depressed cladding waveguide laser have been achieved in Nd:YAG crystal and ceramics [11]-[13]. Y-branch waveguide, which could act as an optical amplifier or splitter in the integrated optical devices, have already been fabricated in Nd-doped silicate glass, $\mathrm{LiNbO}_{3}$, BK-7 glass and Yb:YAG [24]-[27]. Meanwhile, the Y-branch construction could be used for monolithically integrated optical heterodyne systems with designed for signal amplification and communication applications [24], [28], [29]. Furthermore, the Y-branch splitter serve as the basic element to realize the wavelength division multiplexing in the optical networks [28].

In this work, we report on the fabrication of rectangular Ybranch surface cladding waveguides with different splitting angles by FLI in Nd:YAG crystal. For comparison, straightforward rectangular Y-branch cladding waveguides were produced in the surface of the bulk. Continuous wave (cw) lasing experiments were taken under the direct optical pump of the structures at 808 nm .

## II. Experiments in Details

The Nd:YAG crystal sample (doped by $1 \mathrm{at} . \% \mathrm{Nd}^{3+}$ ions) was cut with sizes of $10 \times 10 \times 2 \mathrm{~mm}^{3}$. The Y-branch depressed cladding waveguides were produced by using the laser facility of the Universidad de Salamanca, Spain. A Ti:Sapphire

TABLE I
Constants of Y-Branch Cladding Waveguides

| No. | Width (single/branch sections) $(\mu \mathrm{m})$ | Depth $(\mu \mathrm{m})$ | Splitting angle $\left({ }^{\circ}\right)$ |
| :--- | :---: | :---: | :---: |
| Pr1 | $50 / 25+25$ | 50 | 2 |
| $\operatorname{Pr} 2$ | $50 / 25+25$ | 50 | 1 |
| $\operatorname{Pr} 3$ | $50 / 25+25$ | 50 | 0.5 |
| $\operatorname{Pr} 4$ | 50 | 50 | 0 |

regenerative amplifier (Spitfire, Spectra Physics, USA), delivering linearly-polarized pulses of 120 fs and 795 nm central wavelength at 1 kHz repetition rate as previous report [12], [16]-[21], was used as laser source. The maximum available pulse energy was 1 mJ . In order to get a fine control of the incident energy, it was reduced with a calibrated neutral density filter placed after a half-wave plate and a linear polarizer.

During the process of fabricating the Y-branch depressed cladding waveguides, the pulse energy was set to $15 \mu \mathrm{~J}$ and the laser beam was focused with a $40 \times$ microscope objective (N.A. $\sim 0.6$ ) at a depth of $50 \mu \mathrm{~m}$ beneath one of the $10 \times 10 \mathrm{~mm}^{2}$ surfaces. The sample was scanned at a constant velocity of $500 \mu \mathrm{~m} / \mathrm{s}$ in the direction paralleled to the $10-\mathrm{mm}$ edge, producing a damage line along the sample. The procedure was repeated at different depths of the sample, following the desired rectangular geometry with a lateral separation of $3 \mu \mathrm{~m}$ between each two adjacent tracks. Under these conditions, rectangular-shape structures were achieved, and the parameter of the novel structures could be found in Table I. The length of the single section and the branch section are 3.5 and 6.5 mm , respectively. According to the micromachining parameters, the volume ration between the two branch sections is about $1: 1$. The splitting angle $\theta$ of the configurations $\operatorname{Pr} 1-\operatorname{Pr} 3$ was arranged from $0.5^{\circ}$ to $2^{\circ}$. For comparison, straightforward depressed cladding waveguide ( $\operatorname{Pr} 4$ ) was manufactured in the bulk materials under the same situation. Microscope images of the Y-branch cladding waveguides (input face, top surface and output face) are shown in Fig. 1(a)-(c).

With the measurement of the N.A. of the waveguides and the formula reported in [30], the maximum changes of refractive index of the waveguides was estimated to be $3.4 \times 10^{-3}$. In spite of the method itself being a rough estimation, this value was in good agreement with those of other cladding waveguides. Afterwards, the back-reflection method was used to measure the losses of the waveguides at wavelength of 632.8 nm with a $\mathrm{He}-\mathrm{Ne}$ laser as the light source at room temperature [31]. The propagation loss of the straightforward waveguide was about $1.1 \mathrm{~dB} / \mathrm{cm}$. The endface coupling experiments with a $1.06-\mu \mathrm{m}$ solid-state laser were performed and the output power of the Y-branch constructions ( $\mathrm{Pr} 1-\mathrm{Pr} 3$ ) was nearly the same to that of the straightforward waveguide $\operatorname{Pr} 4$, which was mainly due to the similar guiding volume. Compared with the losses of the straightforward cladding structure, additional losses from the Y-branch splitting geometry is negligible, which means lossless splitting structures were produced by femtosecond laser writing in this work.

A wavelength-tunable cw Ti:Sapphire laser (Coherent MBR PE, USA) generating a polarized light pump beam at 808 nm was


Fig. 1. Microscope images of the input face (a), top surface (b) and output face (c) of the Y-branch cladding waveguides in Nd:YAG crystal; (d) cw laser modal profiles at 1064 nm collected from the structures at TM polarization. (e) Schematic diagram of the Y-branch splitter configuration, $\theta$ is the splitting angle. (f) Schematic diagram of the experimental setup for the cw waveguide laser oscillation in the Y-branch cladding waveguides.
used in the end pumping system to performed the cw Y-branch waveguide laser-operation experiments as shown in Fig. 1(f). Spherical convex lens with a focal length of 25 mm was used to couple the pump laser beam into the guiding structures. A $20 \times$ long working distance microscope objective (N.A. $=0.4$ ) was used to collect the generated waveguide lasers and an IR CCD camera to image the laser beam profiles through an aperture. A spectrometer was used to analyze the emission spectra of the pump source and the generated laser beam.

## III. Results and Discussion

During the endface coupling experiments for light transmissions at wavelength of $1.06 \mu \mathrm{~m}$, modal profiles of output laser at TM polarization were measured. As shown in Fig. 1(d), the laser modal profiles are not at fundamental modes or single modes as reported previously [12]. This is mainly caused by the edge of the rectangle structures, which is not as smooth as the circular structures. The $1.06-\mu \mathrm{m}$ light propagation in Y-branch waveguides was simulated by the well-known Rsoft software and shown in Fig. 2 [32]. The left, middle and right figures are corresponding to the Y-branch waveguides with splitting angles of $2^{\circ}, 1.5^{\circ}$ and $0.5^{\circ}$, respectively. The sources were set as Gaussian beams and the lengths of the waveguides were set to be 10 mm that are in good agreement with the structure fabricated by FLI. From the simulated images, disordered modes could be found which is also confirmed in the cw laser modal profiles displayed in Fig. 1(d).

Fig. 3 displays the spectrum of the pumping laser (dashed line) and output laser oscillation (solid line) when the pumping laser is above the threshold. The $808-\mathrm{nm}$ laser with the full width at half maximum (FWHM) of $\sim 0.6 \mathrm{~nm}$ is corresponding to main absorption transition of $\mathrm{Nd}^{3+}$ ions, meanwhile the generated 1064-nm laser oscillation line with a FWHM of 0.4 nm


Fig. 2. Simulated the $1.06-\mu \mathrm{m}$ transformation status in Y-branch waveguides with different splitting angle $\theta$ arranging from $2^{\circ}$ to $0.5^{\circ}$.


Fig. 3. Spectra of the pumping laser (dashed line) and output laser oscillation (solid line) when pumping laser is above the threshold at room temperature. FWHM of the lasers are 0.6 and 0.4 nm , respectively.
is corresponding to the main fluorescence of ${ }^{4} \mathrm{~F}_{3 / 2} \rightarrow{ }^{4} \mathrm{I}_{11 / 2}$ transition of $\mathrm{Nd}^{3+}$ ions.

Waveguiding laser features of the Y-branch cladding structures were calculated with consideration of the transmittance and reflectivity of the optical elements (e.g., microscope lenses) in the end-coupling experiment system. As shown in Fig. 4(a), the linearly-polarized pumping laser was changed through adjusting half-wavelength plate, and the resultant all-angle performance of the output laser collected from the cladding waveguides proves that the laser oscillations in the rectangular cavity are not influenced by the polarizations of the pumping laser. The fitting lines show the maximum output power of the $1.06-\mu \mathrm{m}$ laser when the input laser power was about 1.1 W. Difference between the output powers of lasers collected from the cladding waveguides $(\operatorname{Pr} 1-\operatorname{Pr} 4)$ is mainly owing to the splitting angles of the configurations. Despite the losses measured in the endface coupling experiment at $1.06 \mu \mathrm{~m}$ were nearly the same for the structures, the effect of the splitter junction caused in the laser oscillation could not be neglected. Fig. 4(b) displays the output powers of the active cw lasers versus the launched power at TM polarization. The slope efficiency of the output laser calculated $\left(\eta_{P r 1}, \eta_{\operatorname{Pr} 2}, \eta_{\operatorname{Pr} 3}\right.$ and $\left.\eta_{\operatorname{Pr} 4}\right)$ are $18.1 \%, 18.7 \%$, $20.2 \%$ and $22.4 \%$, respectively. Some other laser features of Y-branch rectangular cladding waveguides are depicted in Table II. The output power ratio between left and right branch are all about 49:51, which is mostly caused by the little dif-


Fig. 4. (a) All-angle performance of the output power of the active laser collected from the Y-branch waveguides ( $\operatorname{Pr} 1-\operatorname{Pr} 3$ ) and the straightforward rectangular cladding waveguide $(\operatorname{Pr} 4)$ when the launched power was 1.1 W . The incident angle of the $808-\mathrm{nm}$ laser pumping laser was changed from $0^{\circ}$ to $360^{\circ}$. (b) Output power of the collected laser as functions of the launched power. The slope efficiency of the output power were obtained after calculation.

TABLE II
Laser Performance of Y-Branch Cladding Waveguides

| No. <br> Output power ratio <br> between left and right <br> branch $(1064 \mathrm{~nm})$ | Ratio of Output <br> power compared with <br> that of Pr4 | Maximum output <br> power <br> $(\mathrm{mW})$ |  |
| :---: | :---: | :---: | :---: |
| Pr1 | $49.2: 50.8$ |  | $81.5: 100$ |
| Pr2 | $48.7: 51.3$ | Approximately 49:51 | $87: 100$ |
| $\operatorname{Pr3}$ | $48.8: 51.2$ | $92.3: 100$ | 172 |
| $\operatorname{Pr} 4$ |  | $100: 100$ | 187 |

ference of the laser cavity volume. With the splitting angle increases from $0^{\circ}$ to $2^{\circ}$, the maximum output laser power decreases from 236 to 172 mW . Meanwhile, threshold of the laser oscillation are $99,166,164$ and 231 mW , respectively. The maximum output power of the Y-branch cladding waveguide with splitting angle of $0.5^{\circ}$ is $92.3 \%$ of the straightforward cladding waveguides, which demonstrates the excellent performance of Y-branch splitter structure fabricated in Nd:YAG crystal by FLI.

## IV. CONCLUSION

We have demonstrated the fabrication of depressed cladding Y-branch waveguides in Nd:YAG crystals by the FLI. Rectangular Y-branch cladding waveguides with different splitting angles $\left(0^{\circ}, 0.5^{\circ}, 1^{\circ}\right.$ and $\left.2^{\circ}\right)$ were manufactured in the cubic Nd:YAG crystal with acceptable guiding properties. Under direct optical pump at 808 nm , the cw laser operating at 1064 nm with a maximum output powers of up to 201 mW has been obtained in the Nd:YAG Y-branch waveguide laser system with a splitting angle
of $0.5^{\circ}$. Excellent performances of the novel Y-branch waveguiding systems confirm that such promising devices could be integrated in optical devices for diverse applications.

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