





# Combined $^{23}\text{Na}$ and $^{13}\text{C}$ imaging at 3.0 Tesla using a single-tuned large FOV birdcage coil

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**Purpose:** An unmet need in carbon-13 ( $^{13}\text{C}$ )-MRI is a transmit system that provides uniform excitation across a large FOV and can accommodate patients of wide-ranging body habitus. Due to the small difference between the resonant frequencies, sodium-23 ( $^{23}\text{Na}$ ) coil developments can inform  $^{13}\text{C}$  coil design while being simpler to assess due to the higher naturally abundant  $^{23}\text{Na}$  signal. Here we present a removable  $^{23}\text{Na}$  birdcage, which also allows operation as a  $^{13}\text{C}$  abdominal coil.

**Methods:** We demonstrate a quadrature-driven 4-rung  $^{23}\text{Na}$  birdcage coil of 50 cm in length for both  $^{23}\text{Na}$  and  $^{13}\text{C}$  abdominal imaging. The coil transmit efficiencies and  $B_1^+$  maps were compared to a linearly driven  $^{13}\text{C}$  Helmholtz-based (clamshell) coil. SNR was investigated with  $^{23}\text{Na}$  and  $^{13}\text{C}$  data using an 8-channel  $^{13}\text{C}$  receive array within the  $^{23}\text{Na}$  birdcage.

**Results:** The  $^{23}\text{Na}$  birdcage longitudinal FOV was > 40 cm, whereas the  $^{13}\text{C}$  clamshell was < 32 cm. The transmit efficiency of the birdcage at the  $^{23}\text{Na}$  frequency was  $0.65 \mu\text{T}/\sqrt{W}$ , similar to the clamshell for  $^{13}\text{C}$ . However, the coefficient of variation of  $^{23}\text{Na}-B_1^+$  was 16%, nearly half that with the  $^{13}\text{C}$  clamshell. The 8-channel  $^{13}\text{C}$  receive array combined with the  $^{23}\text{Na}$  birdcage coil generated a greater than twofold increase in  $^{23}\text{Na}$ -SNR from the central abdomen compared with the birdcage alone.

**Discussion:** This  $^{23}\text{Na}$  birdcage coil has a larger FOV and improved  $B_1^+$  uniformity when compared to the widely used clamshell coil design while also providing similar transmit efficiency. The coil has the potential to be used for both  $^{23}\text{Na}$  and  $^{13}\text{C}$  imaging.

Martin J. Graves and Ferdia A. Gallagher contributed equally to this study.

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## KEYWORDS

body imaging, carbon-13 MRI, multinuclear imaging, RF coils, sodium-23 MRI

## 1 | INTRODUCTION

Recent technical developments in the field of multinuclear MRI have improved spatial resolution within clinically feasible timescales, as well as allowing more accurate quantification of the measured signals. These developments have demonstrated a wide range of new clinical applications for carbon-13 ( $^{13}\text{C}$ ) and sodium-23 ( $^{23}\text{Na}$ ) MRI.<sup>1-7</sup> For example, there has been much recent interest in  $^{13}\text{C}$ -MRI due to the advent of hyperpolarized technologies, with particular emphasis on detecting the metabolism of hyperpolarized [1- $^{13}\text{C}$ ] pyruvate into [1- $^{13}\text{C}$ ]lactate noninvasively in tumors, the heart, and in the brain.<sup>1-3</sup> One challenging task in the field of multinuclear MRI is ensuring optimum RF coil hardware. In this work, we focus on a transmit (Tx) RF coil for both  $^{23}\text{Na}$  and  $^{13}\text{C}$  excitation.

$^{13}\text{C}$  RF coil evaluations are more challenging than those for  $^{23}\text{Na}$  due to the low natural abundance of  $^{13}\text{C}$  (~1%), the long  $T_1$  values for many  $^{13}\text{C}$  nuclei (>1.0 s for relevant molecules at 3 Tesla [T]), multiplet peaks, and the need for expensive enriched phantoms. In contrast,  $^{23}\text{Na}$ -MRI can be performed using readily available saline phantoms *in vitro*; has a short  $T_1$  (20-40 ms typical at 3.0 T<sup>8,9</sup>), which enables rapid TR; and is not affected by J-coupling. The high natural abundance of  $^{23}\text{Na}$  makes it favorable for imaging *in vivo*. Because the RF requirements for  $^{13}\text{C}$ -MRI and  $^{23}\text{Na}$ -MRI are very similar due to their gyromagnetic ratios ( $\gamma^{13}\text{C} = 10.708$  MHz/T;  $\gamma^{23}\text{Na} = 11.262$  MHz/T), the characterization of a  $^{23}\text{Na}$  abdominal Tx coil enables the assessment of a design prior to  $^{13}\text{C}$ -specific coil construction.

In addition, the small difference in the 2 Larmor frequencies yields the opportunity to evaluate the feasibility of driving the  $^{23}\text{Na}$  coil off-resonance for acquisition at the  $^{13}\text{C}$ -frequency. Such off-resonant operation has potential benefits. We have shown that the detection of the  $^{23}\text{Na}$  resonance, using a coil tuned to  $^{13}\text{C}$ , can be used to calibrate the Tx  $B_1$  and center frequency prior to hyperpolarized [1- $^{13}\text{C}$ ]pyruvate metabolism *in vivo* imaging. Such an approach could greatly improve the workflow for clinical  $^{13}\text{C}$ -hyperpolarized imaging.<sup>10</sup> Furthermore, we have previously shown that  $^{23}\text{Na}$ -MRI can be undertaken with an endorectal coil tuned to  $^{13}\text{C}$ , allowing additional and complementary  $^{23}\text{Na}$  information to be acquired during a hyperpolarized  $^{13}\text{C}$ -MRI exam of the prostate.<sup>11</sup> Therefore, as part of this work we are interested in the degradation of coil performance when using a  $^{23}\text{Na}$  coil at the nearby but off-resonant frequency of  $^{13}\text{C}$ .

An ideal Tx coil has a high  $B_1^+$  field uniformity and a low RF power consumption, which is particularly important for

imaging large FOV regions such as the thorax or abdomen. Therefore, Tx coils typically surround the body part under investigation. An ideal abdominal Tx coil would also accommodate patients with wide-ranging body habitus, which is particularly important because many pathological conditions are associated with an increased abdominal girth due to obesity, masses, or ascites. Removable volume coils are typically required for  $^{13}\text{C}$  or  $^{23}\text{Na}$  imaging to avoid disruption of the clinical hydrogen-1 ( $^1\text{H}$ )-MRI.

However, the construction of body-sized, removable coils for multinuclear MRI is challenging because the large coil size reduces Tx efficiency. Broadband RF amplifiers used for multinuclear MRI with local RF coils are supplied with only a fraction of the available power used for  $^1\text{H}$ -MRI, typically a fourth or even less. This limited available Tx power at non- $^1\text{H}$  frequencies ( $\leq 8$  kW for non- $^1\text{H}$  vs.  $> 30$  kW for  $^1\text{H}$  at 3.0 T) necessitates an optimized Tx efficiency for effective imaging and forms the basis for the work presented here, in which  $^{23}\text{Na}$  coil properties are assessed as a surrogate for evaluating  $^{13}\text{C}$  RF properties more easily than a  $^{13}\text{C}$  tuned coil. Whereas the  $B_1^+$  field shape is largely determined by coil geometry regardless of the nucleus imaged at field strengths below  $\leq 3.0$  T, the precise assessment of SNR and Tx efficiency are due to frequency dependencies of matching and tuning.

For choosing an appropriate coil design for a  $^{13}\text{C}$  abdominal Tx coil, we considered the coil designs common in the x-nuclei field, especially the clamshell coil<sup>9,12-15</sup> and various birdcage coil approaches.<sup>16-18</sup> The clamshell coil is a widely used, and the largest previously available, Tx-only system for  $^{13}\text{C}$  abdominal imaging,<sup>9,12-15</sup> which has also been used for  $^{23}\text{Na}$ -MRI at 1.5 T.<sup>13,14</sup> The clamshell consists of 2 ~30 cm Helmholtz-like loops separated by a variable distance. The 60 cm available MRI system bore diameter is further reduced by the patient table and the clamshell to 29 cm in the vertical direction and by ~45 cm in the left-right direction due to the coil support structures on one side. The requirement for separate receive (Rx) coils, which can be up to 10 cm in depth, also reduces the available volume. Furthermore, the FOV of the  $^{13}\text{C}$  clamshell is limited by the low Tx homogeneity and the limited length in the  $z$  direction. This lack of available patient space has limited which patients can be imaged when using the combination of the clamshell with both anterior and posterior Rx arrays.

The aim of this study was to develop a  $^{23}\text{Na}$  abdominal Tx coil with increased available space for patients and coverage along  $z$ , as compared to the commonly used clamshell coil, with improved Tx  $B_1^+$  uniformity while maintaining Tx efficiency.  $^{23}\text{Na}$  was used as a prototype for a  $^{13}\text{C}$  Tx system due

to the higher endogenous signals available for  $^{23}\text{Na}$ . Whereas torso  $^{23}\text{Na}$  birdcage coils<sup>16-18</sup> provide a higher  $B_1^+$  uniformity and Tx efficiency over linear coils (due to quadrature polarization), they restrict patient space due to their closed designs, which are often built with 16 rungs. A design with significantly fewer rungs enables the imaging of patients with larger abdominal girth by allowing the patient to use the full width of the bore between the 2 end rings. Therefore, we decided to evaluate a birdcage design with only 4 rungs and asymmetric end rings to maintain the advantages of a birdcage coil design ( $B_1^+$  homogeneity, Tx efficiency and coverage) while overcoming these space restrictions. For the evaluation of the design, we have chosen a 4 rung  $^{23}\text{Na}$  birdcage coil. We also demonstrate the combination of  $^1\text{H}$ ,  $^{23}\text{Na}$ , and  $^{13}\text{C}$  abdominal imaging within a single setup

## 2 | METHODS

### 2.1 | $^{23}\text{Na}$ Tx/Rx volume coil

A custom-built Tx/Rx 4 rung, 50 cm long birdcage coil was designed (Figures 1 and 2) (Rapid Biomedical GmbH, Rimpar, Germany). The rungs were positioned 30 cm apart to resemble the loop size of the clamshell coil (loop diameter and distance  $\sim 30$  cm) and consist of 50 cm long, 10 mm diameter copper tubes. The end rings were adjusted to match the MRI bore and scanner table curvature for maximizing the space for the patient. The inner part of the rungs lies on a diameter of 42 cm; the coil outer diameter is 56 cm at its maximal left-to-right dimension, matching the bore size. The conductors of the end rings are printed circuit boards with 20 mm conductor width. The coil was tuned and matched

to 33.8 MHz, the  $^{23}\text{Na}$  frequency at 3.0 T. The asymmetric shape created end-ring inductance imbalances such that the coil required additional ring capacitors ( $C_L$  in Figure 1B) to keep the electrical coil symmetry for quadrature drive. The coil includes a separate  $90^\circ$  hybrid splitter for quadrature drive and a low noise preamplifier with a gain of 27 dB and a 0.9 dB noise figure. Final tuning/matching of the coil was undertaken within the scanner bore.

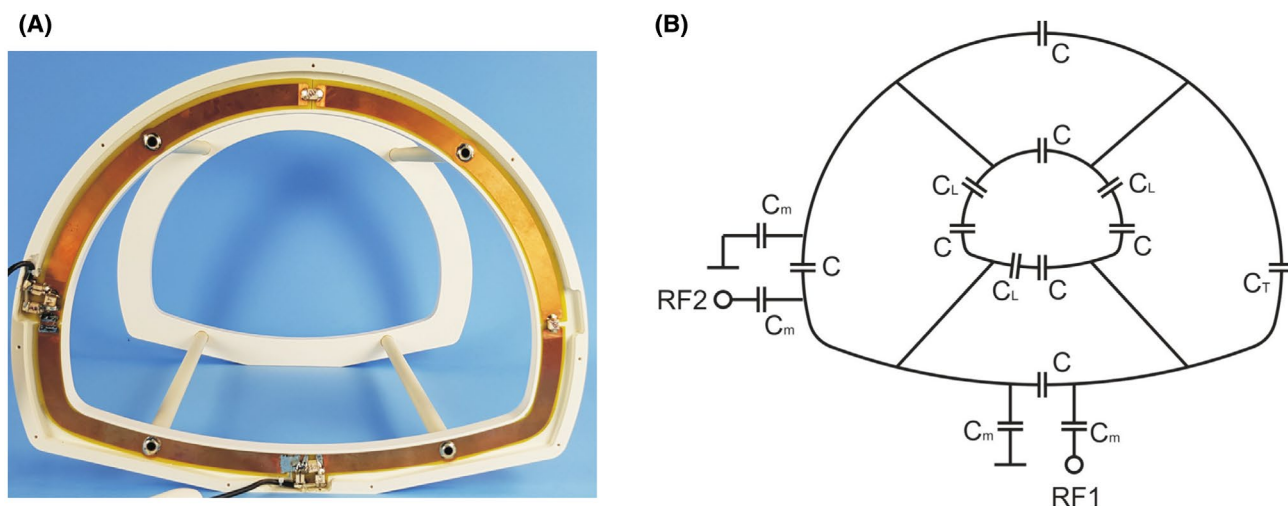
The loaded and unloaded quality (Q) factors were measured with 2 stationary decoupled magnetic field probes inside the coil from the  $-3$  dB bandwidth of S21 on a network analyzer. The load was a rectangular tub filled with 55 mM NaCl, approximately  $32 \times 22 \times 22$  cm<sup>3</sup> in dimension, containing 48 g NaCl mixed with 15 L water.

### 2.2 | 8 Channel Rx-only array

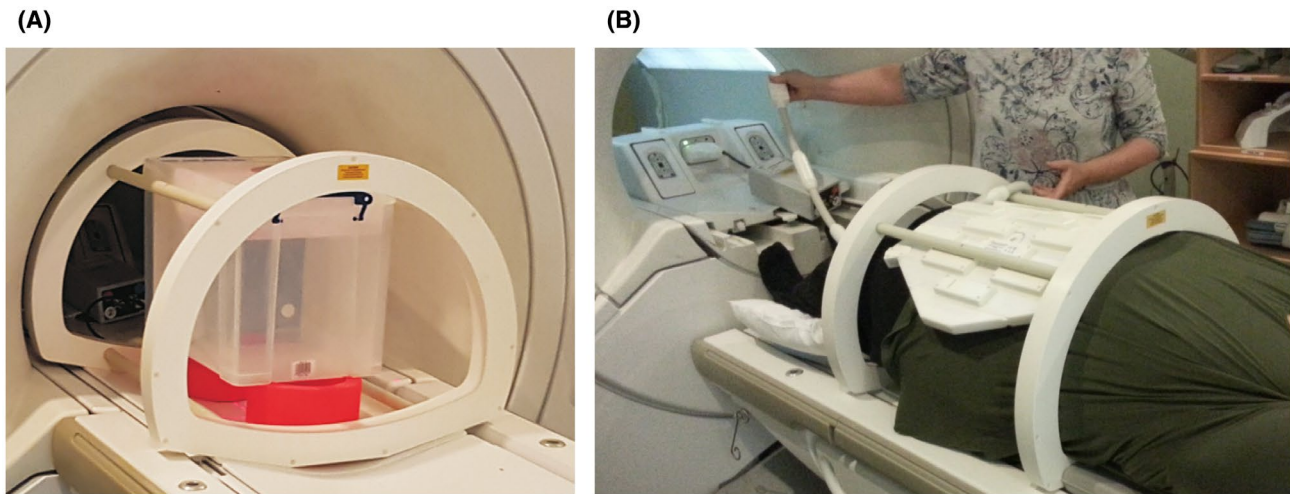
For testing the imaging performance, an 8 channel  $^{13}\text{C}$  Rx-only array—4 posterior, 4 anterior (Rapid Biomedical GmbH, Rimpar, Germany)—was used inside the  $^{23}\text{Na}$  birdcage coil. This was used for both  $^{23}\text{Na}$  and  $^{13}\text{C}$  signal reception without retuning any components. Although the birdcage coil could not be detuned during reception, the large differences between the Tx and Rx coil sizes resulted in low intrinsic coupling, hence obviating the need for active decoupling.

### 2.3 | $B_1$ Phantom measurements for $^{23}\text{Na}$ , $^{13}\text{C}$ , and $^1\text{H}$

Tx efficiency and  $B_1^+$  field uniformity was evaluated for both frequencies:  $^{23}\text{Na}$  and  $^{13}\text{C}$  for the  $^{23}\text{Na}$  birdcage and  $^{13}\text{C}$  for



**FIGURE 1** (A) Photograph of the  $^{23}\text{Na}$  birdcage coil with the cover removed. (B) Circuit design showing the capacitors for tuning and matching, for which  $C$  is the capacitance for a symmetric birdcage tuned to 33.8 MHz and  $C_L$  has been added to achieve electrical symmetry. RF coupling occurs at the RF1 and RF2 ports. The capacitors were:  $C = 41$  pF,  $C_L = 160$  pF, and  $C_m = 38$  pF for tuning/matching to 33.8 MHz inside the bore.  $^{23}\text{Na}$ , sodium-23



**FIGURE 2** (A) The  $^{23}\text{Na}$  4-rung birdcage coil with saline phantom constructed for testing. (B) A female subject is shown inside the  $^{23}\text{Na}$  birdcage, with a flexible  $^{13}\text{C}$  receive array, demonstrating the possibility of using this system on a 118 kg volunteer.  $^{13}\text{C}$ , carbon-13

the  $^{13}\text{C}$  clamshell. Tx efficiency and  $B_1^+$  maps acquired during phantom imaging were used to evaluate the safety of volunteer scanning through global-specific absorption rate (SAR) calculations and observing local RF hot spots.

$^{23}\text{Na}$ - $B_1^+$  maps were obtained using the double angle mapping method with the 15 L NaCl phantom.  $B_1^+$  maps were acquired with the birdcage coil in Tx/Rx mode at 2 flip angles ( $45^\circ$  and  $90^\circ$ ) using a 3D cones gradient echo (GRE) sequence: TR = 250 ms; TE = 455  $\mu\text{s}$ ; pulse width = 500  $\mu\text{s}$ ; delay 205  $\mu\text{s}$ ; voxel size =  $6.1 \times 6.1 \times 6.1 \text{ mm}^3$ ; FOV = 42 cm; averages = 16; interleaves = 196; readout duration = 30 ms; scan time = 10 min 24 s; and bandwidth  $\pm 125 \text{ kHz}$ .

The surface temperatures of the coils were measured with an infrared thermometer (PRO 8861, RS Components, UK) before and after the same 3D cones sequence but using the full available power: TR = 100 ms and flip angle =  $90^\circ$ , averaged for  $\sim 10 \text{ min}$ .

$^{13}\text{C}$ - $B_1$  maps were acquired using a double angle mapping in a 32 cm sphere of silicone oil (GE Healthcare, Waukesha, WI). Slices were excited with spectral-spatial pulses: nominal flip angles  $60^\circ$  and  $120^\circ$ ; FOV = 48 cm; TR = 5 s; and 128 averages.  $^{13}\text{C}$ - $B_1$  variation along the bore was measured by moving a 5 cm surface Rx coil along the  $z$  axis of a large rectangular phantom containing doped silicone oil; followed by maximizing the signal; and then using a 2 ms long,  $90^\circ$  hard pulse to measure the overall signal decrease, which was considered to be the relative  $B_1^+$  change.

In order to ensure safety during  $^1\text{H}$  imaging using the MRI system body coil, the interactions with the  $^{23}\text{Na}$  removable birdcage coil were assessed by  $^1\text{H}$ - $B_1^+$  field measurements on 2 adjacent rectangular ( $32 \times 22 \times 18 \text{ cm}^3$ ) phantoms containing dimethyl silicone fluid, gadolinium, and pink colorant<sup>19</sup> (GE 283, GE Healthcare). The phantoms were placed close to the rungs to replicate maximum local  $^1\text{H}$ - $B_1^+$  distortion. The 2D  $^1\text{H}$ - $B_1^+$  maps were acquired using a Bloch-Siegert method

with a spoiled GRE sequence: TR = 29 ms; TE = 13.2 ms; flip angle =  $20^\circ$ ;  $3.75 \times 3.75 \text{ mm}^2$ ; FOV = 48 cm; 20 slices with 10 mm thickness; and  $\pm 16 \text{ kHz}$  bandwidth. To further improve safety during human imaging, the pulse widths were doubled compared to typical  $^1\text{H}$  sequences, which reduces SAR by a factor of 2. After phantom validation, the Tx flip angle was slowly increased during the initial in vivo experiments while ensuring that the subject did not experience any excess heat.

## 2.4 | Calibration measurements

Bloch-Siegert calibration scans were performed on 6 normal volunteers (5 male/1 female; ages =  $38 \pm 13$  years; body mass index [BMI] =  $25 \pm 3 \text{ kg/m}^2$ ) to obtain the center frequency and the power required for a nominal  $90^\circ$  pulse. The forward transmission (S21) was also measured between the  $0^\circ$  and  $90^\circ$  coil ports to evaluate quadrature stability. The Tx gain is reported in centibels (cB), whereas RF measurements are reported in decibels (dB) as per vendor and community naming conventions, respectively.

## 2.5 | Normal volunteer imaging

After safety was assured, imaging was performed on a single, normal volunteer (male, [body mass index] =  $28 \text{ kg/m}^2$ ) using a 3T MRI system (MR750, GE Healthcare) and following written informed consent and ethical approval (Hertfordshire Research Ethics Committee REC ref 08/H0311/117, IRAS 161555). Before imaging at the  $^{13}\text{C}$  or  $^{23}\text{Na}$  frequency, the default eddy current correction values were modified for the nucleus of interest.<sup>20</sup> Matched 2D GRE single-shot spiral images were obtained using a nominal  $60 \times 60$  point readout for  $^{13}\text{C}$  and  $^{23}\text{Na}$ : TR = 250 ms ( $^{13}\text{C}$ ) and 150 ms

( $^{23}\text{Na}$ ); TE = 12 ms and 0.70 ms; flip angle =  $70^\circ$ ; voxel size =  $8 \times 8 \times 80 \text{ mm}^3$  ( $^{13}\text{C}$ ) and  $8 \times 8 \times 40 \text{ mm}^3$  ( $^{23}\text{Na}$ ); FOV = 48 cm; averages = 128; and bandwidth =  $\pm 125 \text{ kHz}$ . The  $^{13}\text{C}$  data were acquired with spectral-spatial excitation at the frequency of a natural abundance fat peak.

Fat and water were imaged with the  $^1\text{H}$  body coil using a 3D in- and out-of-phase spoiled GRE: TR = 4.0 ms; TE = 1.1 ms (in)/2.2 ms (out); flip angle =  $15^\circ$ ; matrix size =  $256 \times 192 \times 120$ ; voxel size =  $1.9 \times 1.9 \times 5.0 \text{ mm}^3$ ; and partial phase sampling of 70%. To limit the possibility of excess patient heating during  $^1\text{H}$  imaging, only a single GRE sequence was scanned, and only after the results of phantom experiments.

3D cones  $^{23}\text{Na}$  GRE images were acquired: TR = 100 ms; TE = 705  $\mu\text{s}$ ; pulse width = 1.0 ms; delay = 205  $\mu\text{s}$ ; flip angle =  $70^\circ$ ; voxel size =  $4 \times 4 \times 8 \text{ mm}^3$ ; FOV = 48 cm; 1402 interleaves; readout duration = 30 ms; and bandwidth =  $\pm 83 \text{ kHz}$ . The number of averages was 5 with the phased array, and 4 with the body coil only, resulting in total scan time of 11 min 42 s and 9 min 21 s, respectively. This difference in averages results in an 11% ( $= \sqrt{\frac{5}{4}}$ ) SNR increase.

## 3 | RESULTS

### 3.1 | Bench measurements

The S11 of the loaded coil at either  $^{23}\text{Na}$  birdcage port ( $0^\circ$  and  $90^\circ$ ) was  $-34 \text{ dB}$ , and S21 between the 2 ports was  $-25 \text{ dB}$  at  $^{23}\text{Na}$  frequency. The S11 was  $-16 \text{ dB}$  at the  $^{13}\text{C}$  frequency. The unloaded Q factor was  $\sim 800$  and decreased to  $\sim 25$  when loaded with the 15 L NaCl phantom. Coupling with the MRI system caused a  $\sim 2.6 \text{ MHz}$  frequency shift.

Active decoupling ( $\Delta\text{S21}$  acquired with dual pickup loop) of any Rx loop of the  $^{13}\text{C}$  array was better than 30 dB (active coil  $-36 \text{ dB}$  vs. deactivated coil  $-75 \text{ dB}$ ) at  $^{13}\text{C}$  frequency when measured with 2 external decoupled magnetic probes. At the  $^{23}\text{Na}$  frequency, each of the  $^{13}\text{C}$  array loops showed a  $\Delta\text{S21}$  of  $\sim 16 \text{ dB}$  ( $-44 \text{ dB}$  to  $-60 \text{ dB}$ ). Pre-amplifier decoupling was 14 dB ( $-38 \text{ dB}$  to  $-52 \text{ dB}$ ) for  $^{13}\text{C}$  and 4 dB ( $-47 \text{ dB}$  to  $-51 \text{ dB}$ ) for  $^{23}\text{Na}$ .

### 3.2 | Tx properties

The Tx efficiency of the  $^{23}\text{Na}$  birdcage at the  $^{23}\text{Na}$  frequency was  $0.65 \mu\text{T}/\sqrt{\text{W}}$  and for the  $^{13}\text{C}$  clamshell coil at the  $^{13}\text{C}$  frequency was  $0.63 \mu\text{T}/\sqrt{\text{W}}$ . The power consumption of the  $^{23}\text{Na}$  birdcage was increased by a factor of 2 when being driven off-resonant at the  $^{13}\text{C}$  frequency, resulting in a decrease of Tx efficiency by a factor of 1.4.

Figure 3 shows  $^{23}\text{Na}$  flip angle ( $\propto B_1^+$ ) maps in 3 directions, with the phantom positioned as shown in Figure 2A. The mean flip angle was  $90^\circ \pm 16^\circ$ , or coefficient of variation

= 18%, as measured throughout the entire central axial slice of the phantom for the  $^{23}\text{Na}$  birdcage. Within the same phantom slice, 30% of the  $^{23}\text{Na}$  birdcage voxels had a  $B_1$  between 100 and 120% of the mean, and 60% between 80 and 100%.<sup>10</sup>

A central axial map (Figure 3A) demonstrates nonuniformity at the periphery of the  $^{23}\text{Na}$  birdcage FOV with up to a 50% increase in  $^{23}\text{Na}-B_1^+$  in 2 regions near the coil rungs, although this is not observed in either central sagittal or coronal images.

Figure 4A,B show  $^{13}\text{C}-B_1^+$  maps acquired with the clamshell coil. The coefficient of variation was 28% over the central slice, and 18% of its voxels were between 100 and 120% of the mean  $B_1^+$ . Thirty percent of its voxels were within 80% and 100% of its mean  $B_1^+$ .

Figure 5 compares the  $B_1^+$  falloff in the craniocaudal direction of both the  $^{23}\text{Na}$  birdcage for  $^{23}\text{Na}$  using the 32 cm long saline phantom, and  $^{13}\text{C}$  clamshell for  $^{13}\text{C}$  using a 5 cm loop adjusted in its longitudinal position along a silicone oil phantom. The  $^{23}\text{Na}$  birdcage has lost less than 10% of its maximum  $B_1^+$  at 16 cm at the edge of the phantom, for which the  $^{13}\text{C}$  clamshell was 35% below its maximum.

The regions of interest of the  $^1\text{H}-B_1^+$  maps are shown in Figure 6 with the phantoms immediately above the rungs. The relative mean  $^1\text{H}-B_1^+$  using the standard body coil of  $100 \pm 11\%$  when the  $^{23}\text{Na}$  birdcage was in the bore increased to  $192\% \pm 2\%$  when the  $^{23}\text{Na}$  birdcage was removed when measured without additional Tx power readjustment. After recalibration using automatic prescan adjustment, the body coil had a relative mean  $^1\text{H}-B_1^+$  of  $100\% \pm 2\%$ . When the  $^{23}\text{Na}$  birdcage was in place, the relative  $^1\text{H}-B_1^+$  decreased by 50% near the birdcage rungs, whereas just outside birdcage the  $^1\text{H}-B_1^+$  was nearly twice the nominal value.

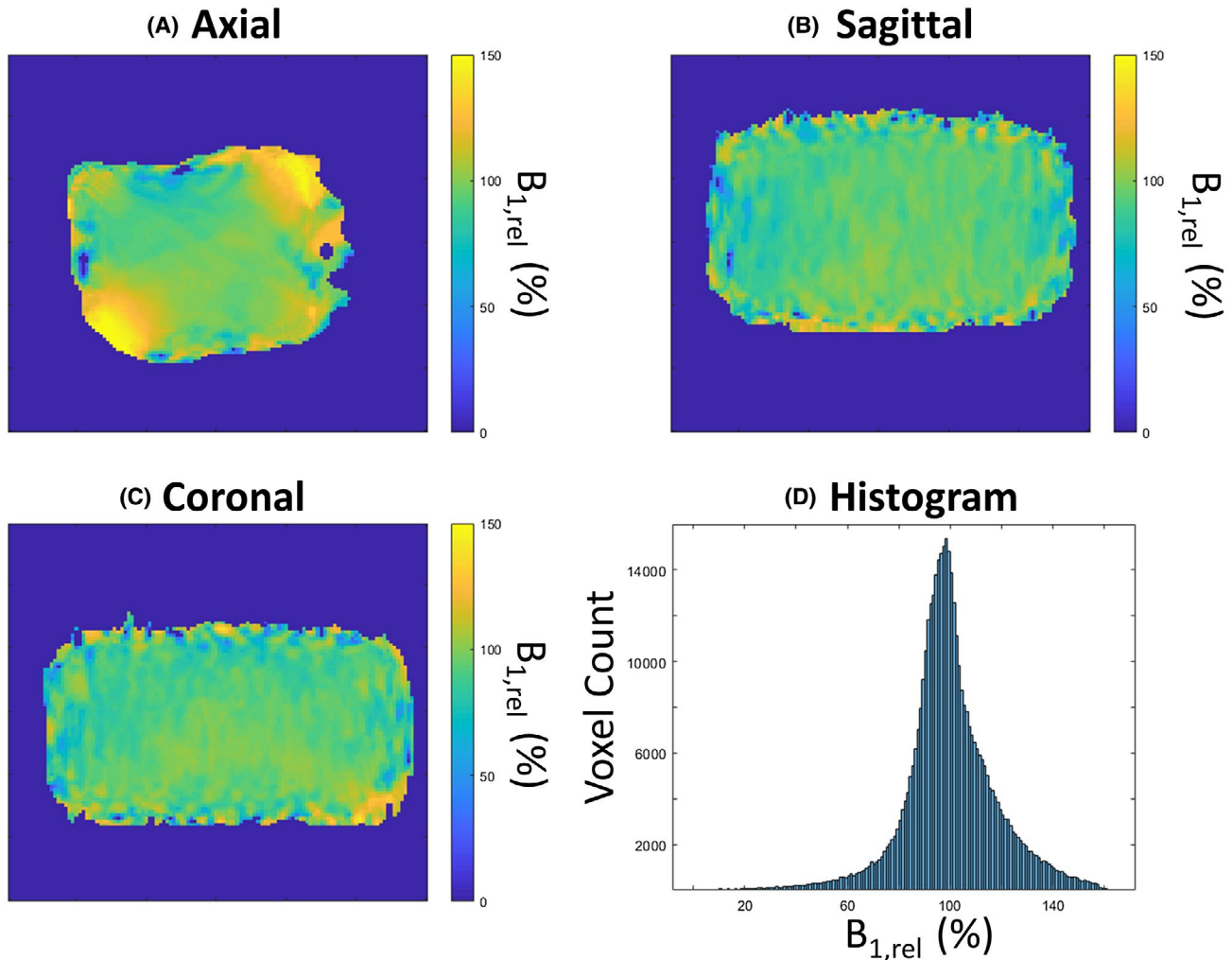
No portion of the  $^{23}\text{Na}$  birdcage had a temperature change of more than  $1^\circ\text{C}$  after sodium phantom studies.

### 3.3 | Noise correlation

Figure 7 shows the noise correlation between all the Rx elements of the  $^{13}\text{C}$  array, measured at both frequencies with the subject in place. The noise correlations were  $< 10\%$  between any 2 coils at either frequency. The correlations were not a constant ratio between the 2 frequencies, which suggests that the coil elements have mild frequency-dependent responses, which can similarly be observed by the lower off-resonant preamplifier decoupling.

### 3.4 | Calibration measurements

The calibration scans on normal volunteers demonstrated the following results: center frequency =  $33,799,288 \pm 7 \text{ Hz}$ ; Tx gain =  $186 \pm 10 \text{ cB}$ ; and  $|\text{S21}|$  was  $12.4 \pm 0.9 \text{ dB}$  (mean  $\pm$



**FIGURE 3** (A-C)  $^{23}\text{Na}$ - $B_1$  maps of the 15 L NaCl phantom along each orthogonal direction acquired using dual angle mapping and a saline phantom. (D) Histogram of the flip angles throughout the phantom.

SD). There were no linear correlations between any combination of body mass index, center frequency, or Tx power ( $P$  values  $> .25$ ).

### 3.5 | Imaging

The small number of rungs enabled the possibility of imaging a large volunteer (Figure 2B). The limitation on patient size with this coil setup is primarily determined by the scanner bore width, unless the hips or shoulders are placed near the end ring; however, the length of the coil and the large  $z$  coverage minimize the requirement for this.

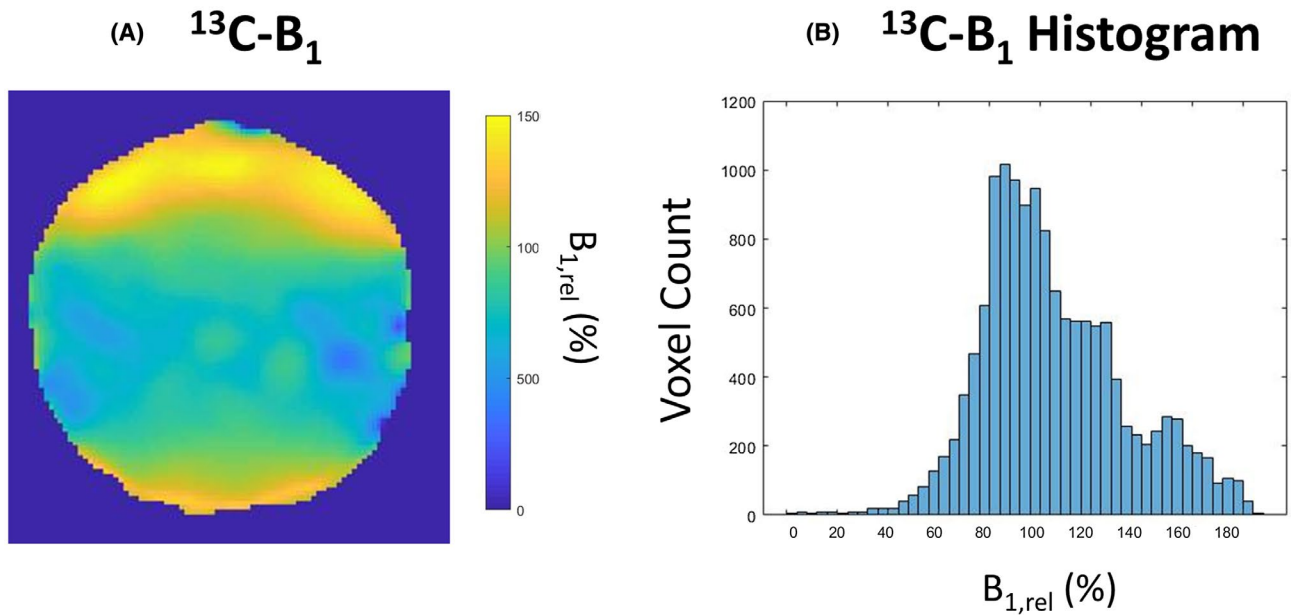
Figures 8 and 9 show in vivo  $^{23}\text{Na}$  MRI of the kidneys, liver, spleen, spine, and aorta. Figure 8 shows imaging of both the natural abundance  $^{13}\text{C}$  signal from fat and endogenous  $^{23}\text{Na}$  using the  $^{13}\text{C}$  array (Rx) with the  $^{23}\text{Na}$  birdcage (Tx). The 50 cm length of the coil allows  $^{23}\text{Na}$  imaging from the level of the heart to the pelvis, while obtaining a  $90^\circ$  flip angle with a 1 ms rectangular pulse width using an 8 kW

power amplifier. The Tx gain was 188 cB, which for a maximum Tx gain of 200 cB translates to a power used that was within 15% below the maximum. If the  $^{23}\text{Na}$  birdcage were tuned to  $^{13}\text{C}$ , we expect to have a similar power requirement.

## 4 | DISCUSSION

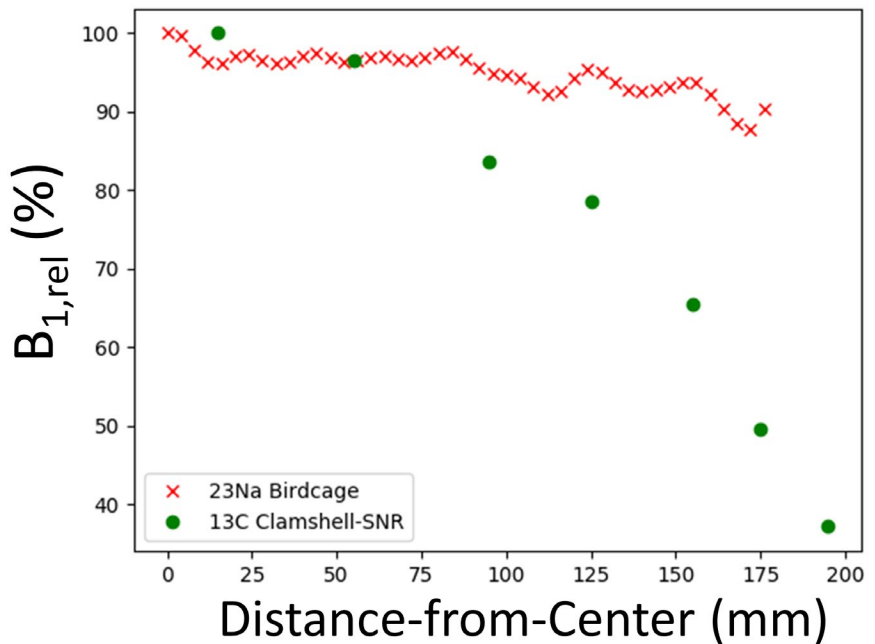
We have demonstrated the feasibility of using a  $^{23}\text{Na}$  birdcage coil for large FOV  $^{23}\text{Na}$  and  $^{13}\text{C}$  imaging within the abdomen. Our Tx coil is larger than any commercially available coils previously reported for  $^{13}\text{C}$  imaging. The insertable  $^{23}\text{Na}$  birdcage enables a craniocaudal FOV up to 48 cm, which is comparable to both conventional  $^1\text{H}$  imaging and to previously reported  $^{23}\text{Na}$  systems.<sup>16</sup>

The unloaded-to-loaded Q ratio, measured on the  $^{23}\text{Na}$  birdcage, is very high ( $> 30$ ), as occurs with large coils due to an increase of sample losses and resistance.<sup>21</sup> The drop in Q when loading the coil demonstrates that the setup is sample noise dominated, and a gain in Tx efficiency can only



**FIGURE 4** Axial clamshell  $^{13}\text{C}$ - $B_1$  map (A) and corresponding histogram (B) using a 32 cm silicone sphere phantom. The clamshell has a  $B_1$  distribution that is broader than the  $^{23}\text{Na}$  distribution and is multi-modal.

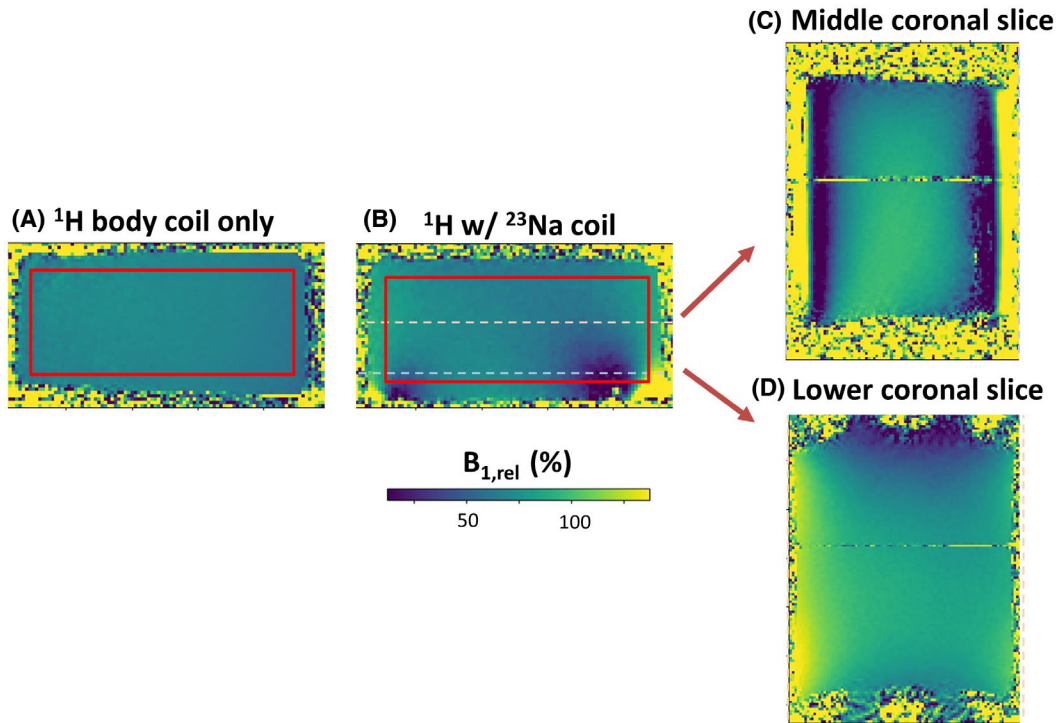
**FIGURE 5** The relative  $B_1$  along the  $z$  axis from the center of the phantom for both the  $^{23}\text{Na}$  birdcage at  $^{23}\text{Na}$  frequency and the  $^{13}\text{C}$  clamshell at  $^{13}\text{C}$  frequency, demonstrating greater consistency for the birdcage.



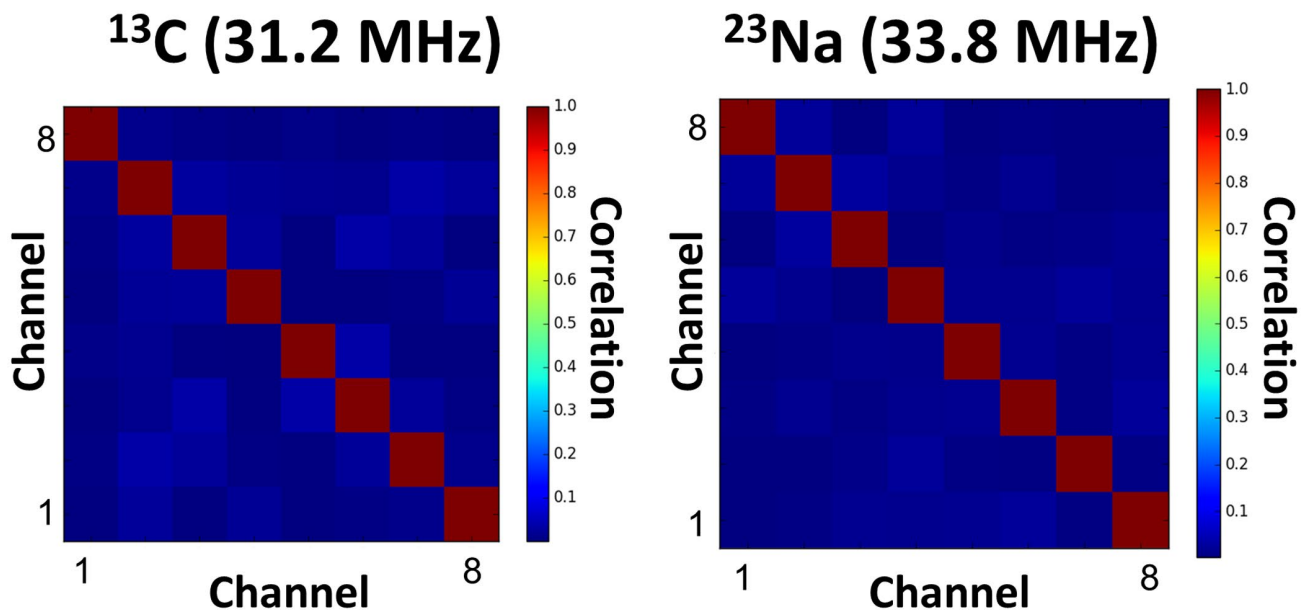
be achieved by changing the  $z$  coverage of the coil. The Tx efficiencies of both birdcage and clamshell coils are similar at their optimized frequencies. Both coils have a similar cross-section in the axial plane, with the birdcage being ~67% longer. The expected drop of 23% in Tx efficiency due to additional length is compensated by the gain in quadrature (40%). Therefore, a  $90^\circ$  flip angle was achievable with a hard pulse width of 1.0 ms and  $< 8$  kW power, which is often difficult to achieve with a large linear clamshell coil due to the higher nonuniformity and SAR. Whereas shorter pulse

durations are desirable for  $^{23}\text{Na}$  imaging, a 1.0-ms pulse is a simple number that is useful for comparisons, especially considering the RF amplifier power limitations. The pulse duration could not be shortened by more than 0.2 ms (eg, below 0.8 ms) due to insufficient Tx to achieve the desired flip angles.

The Tx efficiency demonstrated here was favorable compared to the reported Tx efficiency of a  $^{23}\text{Na}$  abdominal birdcage reported by Wetterling et al. (0.5 ms block pulse,  $90^\circ$ , 1200 V,  $0.24 \mu\text{T}/\sqrt{\text{W}}$ )<sup>17</sup>. The lower Tx efficiency of



**FIGURE 6** Axial proton  $B_1$  maps of 2 large 12.7 L phantoms acquired using the standard  $^1\text{H}$  body coil: (A) without the  $^{23}\text{Na}$  coil inside the system and (B-D) with the  $^{23}\text{Na}$  coil inside the system. (A) Demonstration of a uniform  $B_1$  field without the insert. (B-D) Demonstration of  $^1\text{H}$  shielding immediately near the  $^{23}\text{Na}$ -coil rungs. Images (C) and (D) show 2 parallel coronal slices, with a split occurring between the phantoms. The red boxes in (A) and (B) indicate the regions of interest used for calculation. The dashed lines in (B) indicate the 2 orthogonal slices shown in (C) and (D).  $^1\text{H}$ , hydrogen-1

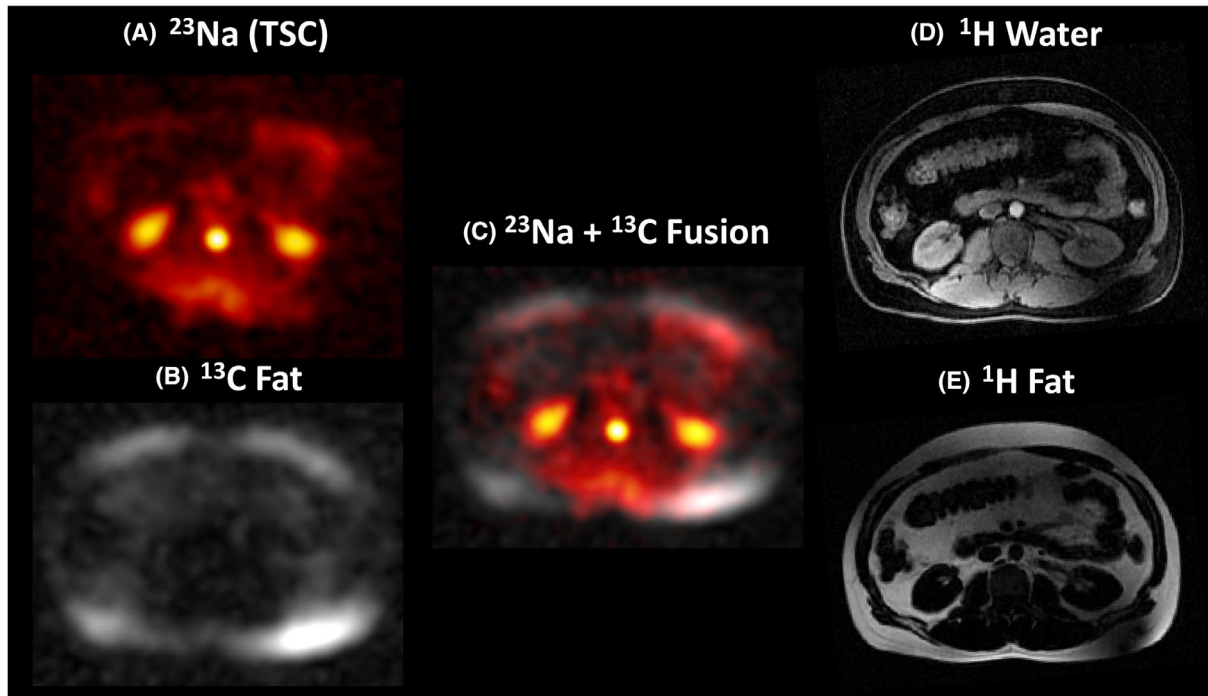


**FIGURE 7** Noise correlation matrices of the 8channel  $^{13}\text{C}$  array, measured at 32.1 MHz for  $^{13}\text{C}$  and at 33.8 MHz for  $^{23}\text{Na}$ . The noise correlation between any 2 coils was  $< 10\%$  at either frequency, suggesting the coils are decoupled.

Wetterling et al. is mainly due to the routing of RF power for  $^{23}\text{Na}$  and suboptimal quadrature performance due to the elliptical shape of their birdcage coil (personal communication

with the authors). The Tx efficiency of our  $^{23}\text{Na}$  birdcage at the off-resonant  $^{13}\text{C}$  frequency decreased by 30% but still allowed acceptable  $^{13}\text{C}$  imaging. Because the decreased Tx





**FIGURE 8** Axial images of the abdomen showing: (A) sodium images, and (B) natural abundance  $^{13}\text{C}$  from fat using the same spiral GRE pulse sequence with the  $^{23}\text{Na}$  birdcage coil as the transmit coil and the  $^{13}\text{C}$  8 channel array as the receive coil with the volunteer in the same position. (C) A fusion image showing  $^{23}\text{Na}$  signal overlaid onto the  $^{13}\text{C}$  fat images, which is used here to evaluate both nuclei. Corresponding (D) water and (E) fat images acquired with the  $^1\text{H}$  body coil and the  $^{23}\text{Na}$  birdcage in place using in- and out-of-phase fat/water imaging. GRE, gradient echo

efficiency does not influence the SNR of an additional  $^{13}\text{C}$  Rx coil (as long as the required flip angles can be achieved), such a single tuned coil is capable of exciting both  $^{23}\text{Na}$  and  $^{13}\text{C}$  in a single setup as part of a multinuclear scan.

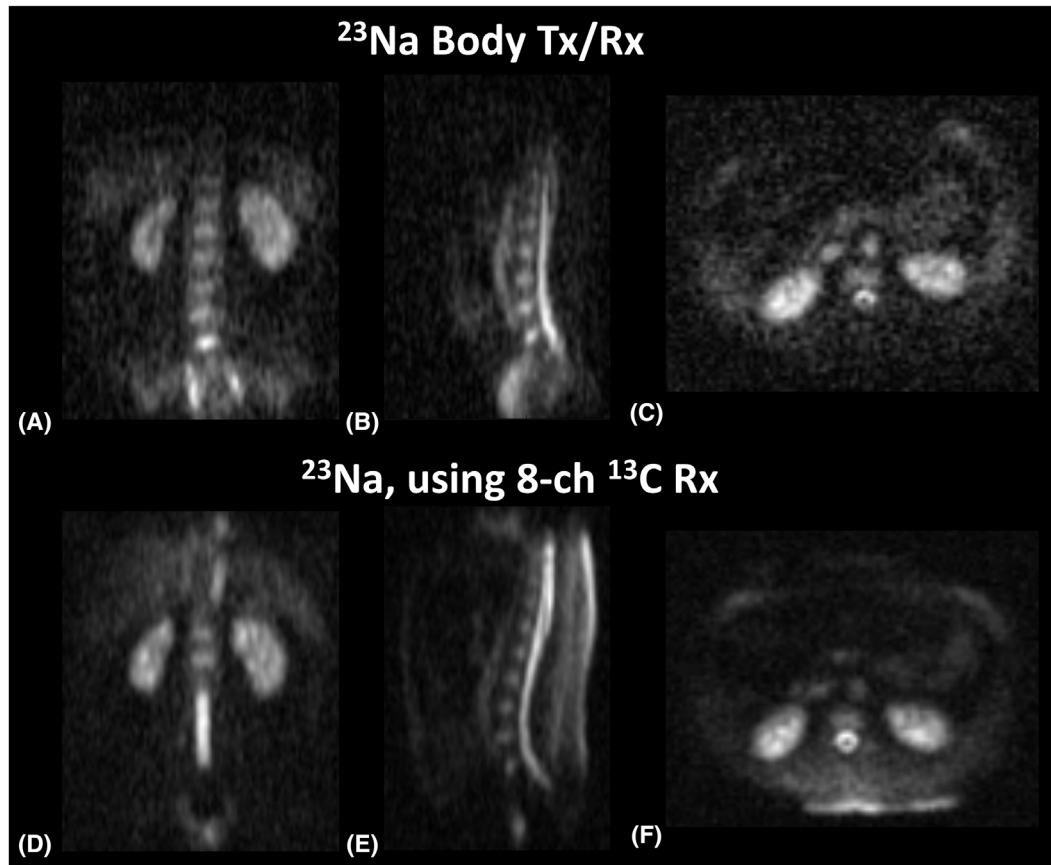
The  $^{23}\text{Na}$  birdcage also enables higher uniformity, showing half the  $B_1^+$  coefficient of variation and a more symmetrical distribution on a histogram of  $B_1^+$  values. The circular polarization of the  $^{23}\text{Na}$  birdcage improves field uniformity by adding an orthogonal field pattern that is complementary to a linearly driven coil and compensates for design intrinsic  $B_1^+$  field nonuniformities due to imperfect tuning. The  $^{13}\text{C}$ - $B_1$  maps of the  $^{13}\text{C}$  clamshell coil show an hourglass-shaped field pattern. Even with only 4 rungs, the periphery of the  $^{23}\text{Na}$ -FOV does not demonstrate severe  $B_1^+$  changes ( $< 50\%$  increases).  $B_1^+$  uniformity simplifies quantitative imaging, improves safety assessments, and can improve SNR when combined with Rx-only coils.

The bore diameter is a limiting factor when accommodating large patients within an MRI system. However, diameter alone is not the only geometric factor that determines patient comfort within a coil: the 4 rung birdcage that we demonstrate here is less restrictive than a clamshell coil design or a 16 rung birdcage (see Figure 2), enabling larger patients to be imaged and more comfortably positioned. Future iterations of this coil will incorporate a split design for easier patient positioning.<sup>22,23</sup> The increase in  $z$  length from 30 cm to 50 cm

provides the coverage required for whole abdominal imaging that is not possible with the clamshell design, which is in widespread use.

Because the  $^{23}\text{Na}$  birdcage is present in the bore during transmission of both  $^{23}\text{Na}$  and  $^1\text{H}$ , the safety of the coil with regard to RF deposition for all frequencies must be considered. The reduction of  $^1\text{H}$ - $B_1^+$  field of the integrated  $^1\text{H}$  body coil when the  $^{23}\text{Na}$  birdcage is placed inside the bore shows that the  $^{23}\text{Na}$  birdcage has an RF shielding effect. The shielding results in a twofold lower  $B_1^+$  field amplitude and therefore E-field at this frequency. Substantial  $^1\text{H}$ - $B_1^+$  field inhomogeneities were not observed close to the rungs or rings internal to the  $^{23}\text{Na}$  birdcage, which might have been a sign for local SAR hot spots. The  $^1\text{H}$ - $B_1^+$  was increased by 50% immediately external to the coil near its rungs such that increased  $^1\text{H}$ -SAR must be considered at this point for ensuring patient safety. We restricted our  $^1\text{H}$  sequences to a GRE sequence to improve safety, which has over sixfold lower SAR than conventional steady-state fast spin echo sequences.

$^{23}\text{Na}$  sequences are SNR-efficient at very short TRs and high flip angles and therefore need consideration of SAR. Because the  $^{23}\text{Na}$  birdcage is a volume coil, whole body SAR and partial body SAR restrictions must be adhered to within the abdomen in order to confine the heating of patient tissue to an acceptable limit according to International Electrical Commission standards (60601-2-33<sup>24</sup>). The low frequency



**FIGURE 9**  $4 \times 4 \times 8 \text{ mm}^3$  3D cones imaging reformatted into: (A, D) coronal, (B, E) sagittal, and (C, F) axial  $^{23}\text{Na}$  images of a normal volunteer. (A-C) Acquired using only the  $^{23}\text{Na}$  body coil for transmit and receive, and (D-F) using the  $^{23}\text{Na}$  body coil for transmit in conjunction with a  $^{13}\text{C}$  8 channel array for  $^{23}\text{Na}$  receive. The 8channel array results in approximately twice the SNR in the kidneys, which allows easier differentiation of cortical and medullary regions.

**TABLE 1** SNRs (mean  $\pm$  SD) for  $^{23}\text{Na}$  signal in several abdominal regions in 1 volunteer, using the  $^{23}\text{Na}$  birdcage only, and using the 8-channel  $^{13}\text{C}$  array in conjunction with the  $^{23}\text{Na}$  birdcage

Region	$^{23}\text{Na}$ -SNR ( $^{23}\text{Na}$ Birdcage Tx/Rx)	$^{23}\text{Na}$ -SNR ( $^{13}\text{C}$ 8 channel Rx)	Number of Voxels
Right kidney	$10.5 \pm 1.5$	$18.0 \pm 2.4$	2153
Left kidney	$9.5 \pm 1.5$	$18.6 \pm 2.6$	2226
Liver	$2.8 \pm 1.1$	$6.0 \pm 1.4$	4519
Aorta	$13.3 \pm 2.9$	$27.5 \pm 5.0$	1251
Skin	$<1.7$	$20.2 \pm 6.7$	1339

The values shown using the birdcage have been increased by 11% to correct for differences in the number of averages.

of the  $^{23}\text{Na}$  birdcage enables the use of  $B_1^+$  maps as a proxy for simulations to estimate SAR. The  $^{23}\text{Na}$ - $B_1^+$  field increases near the rungs were sufficiently low for safe  $^{23}\text{Na}$  operation under standard limits. Theoretically, when using a similar  $B_1^+$  pulse width and shape, a birdcage can have more than twofold less SAR centrally than a linear coil (eg, the clamshell) due to quadrature operation.<sup>24</sup>

For safe operation of the  $^{23}\text{Na}$  birdcage as a Tx coil for the  $^{13}\text{C}$  Rx array, this array needs to be appropriately decoupled at each working frequency. For achieving sufficient decoupling at the  $^{13}\text{C}$  frequency, the  $^{13}\text{C}$  array incorporates actively switched  $^{13}\text{C}$  traps. Although decoupling traps are narrow band components, our tests showed that the  $\Delta S_{12}$  of the  $^{13}\text{C}$  array at the  $^{23}\text{Na}$  frequency is still sufficient to protect the array electronics from excessive  $^{23}\text{Na}$ -RF. In addition, phantom imaging did not show additional local  $^{23}\text{Na}$ - $B_1^+$  hot spots. Therefore, the  $^{13}\text{C}$  decoupling was sufficient for component protection and patient safety during both  $^{13}\text{C}$  and  $^{23}\text{Na}$ -MRI. There are confounding factors when Rx coils are used off-resonance: the decoupling strength will be lower for off-resonant traps, but a nonresonant coil will also receive lower levels of power such that the decoupling does not require the same strength.

The difference between the large resonator size of the Tx coil as compared to the smaller Rx coil elements results in a low inductive coupling; and given that the Tx coil was not detuned during Rx, the SNR is not reduced. The  $^{13}\text{C}$  array coil showed 2 to 3 times the  $^{23}\text{Na}$ -SNR within the abdomen centrally compared to the  $^{23}\text{Na}$  birdcage in Tx/Rx

mode, with even higher SNR ratios closer to the array. Qualitative results show comparable  $^{23}\text{Na}$  image quality in the kidneys when our array is compared with a 7.0T 4 channel setup.<sup>25</sup> The preamplifier decoupling at  $^{23}\text{Na}$  frequency was suboptimal due to the fact that a  $^{13}\text{C}$  Rx array was used for these experiments, although the distance between loops and geometric decoupling reduced some of the correlated noise. Our results are similar to previously published  $^{23}\text{Na}$  results using a volume and Rx coil setup<sup>16</sup> for which  $\sim 3$  times the SNR was achieved with a  $^{23}\text{Na}$  array compared to a  $^{23}\text{Na}$  volume coil.

The  $B_1^+$  field patterns at  $^{13}\text{C}$  can be assumed to be the similar as for  $^{23}\text{Na}$ -Tx.<sup>26</sup> The loaded Q factor of  $\sim 25$  results in a bandwidth of 1.2 to 1.4 MHz ( $BW = f_0/Q$ ), enabling the  $^{23}\text{Na}$  coil to cover  $^{13}\text{C}$  with 50% insertion loss, which was still sufficient for  $^{13}\text{C}$  imaging. However, for optimum performance at  $^{13}\text{C}$ , a dedicated  $^{13}\text{C}$  birdcage is preferable. The  $^{13}\text{C}$ -SNR was maintained by the dedicated  $^{13}\text{C}$  Rx array, which performed sufficiently well to obtain a natural abundance  $^{13}\text{C}$  fat image, despite its potential for electromagnetic coupling to the  $^{23}\text{Na}$  birdcage that was not detuned during Rx.

Utilizing all the capabilities of this design, we showed that combined imaging of  $^{23}\text{Na}$ ,  $^{13}\text{C}$ , and  $^1\text{H}$  was possible in this setup, as demonstrated in Figure 8. For  $^1\text{H}$ , the built-in body coil was used, whereas for  $^{23}\text{Na}$  and  $^{13}\text{C}$  imaging the  $^{23}\text{Na}$  birdcage was used for Tx and the  $^{13}\text{C}$  array was used for Rx. We have previously demonstrated the converse approach in the prostate with a  $^{23}\text{Na}$  Rx and  $^{13}\text{C}$  clamshell Tx.<sup>11</sup> This approach of merging  $^{23}\text{Na}$  and  $^{13}\text{C}$  imaging into a single-tuned coil setup that is capable of dual frequency operation is very promising for future applications of combined  $^{23}\text{Na}$  and  $^{13}\text{C}$  imaging without additional hardware costs.

Body coils been shown for other nuclei, such as  $^{129}\text{Xe}$  and  $^{31}\text{P}$ .<sup>22,23</sup>  $^{129}\text{Xe}$  imaging of the lungs follows inhalation of hyperpolarized  $^{129}\text{Xe}$ , which has a gyromagnetic ratio magnitude that is 5% higher than  $^{23}\text{Na}$ .<sup>22,23,27</sup> Integrated body coils have been shown for single-tuned  $^{31}\text{P}$  imaging at 7.0T.<sup>27</sup> An internal, integrated dual-tuned coil approach may gain several centimeters in diameter but would have reduced cranio-caudal coverage compared to our approach. The removable approach also does not require additional regulatory approval for conventional  $^1\text{H}$  imaging to prevent disruption of the integrity of existing imaging.

## 5 | CONCLUSION

We have demonstrated a 50 cm long, 4 rung  $^{23}\text{Na}$  birdcage coil with asymmetric end rings with good Tx efficiency and very high field uniformity that is also suitable for  $^{13}\text{C}$  imaging. The large cranio-caudal FOV of this  $^{23}\text{Na}$  birdcage allows coverage comparable to conventional  $^1\text{H}$  imaging. When used in conjunction with an 8 channel  $^{13}\text{C}$  Rx coil, we

demonstrated a twofold increase in  $^{23}\text{Na}$ -SNR as measured in the central abdomen, despite the  $^{13}\text{C}$  array not being tuned to  $^{23}\text{Na}$ . The  $^{23}\text{Na}$  birdcage design will be transferred to a coil optimized for  $^{13}\text{C}$  in the future and will incorporate patient access by detachable housing to enable large FOV abdominal imaging for hyperpolarized  $^{13}\text{C}$ -MRI.

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## CONFLICT OF INTEREST

Titus Lanz works for Rapid Biomedical. Dimitri Kessler receives funding from GlaxoSmithKline.

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