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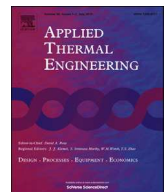
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Thermodynamic analysis and comparison of retrofitting pre-drying concepts at existing lignite power plants

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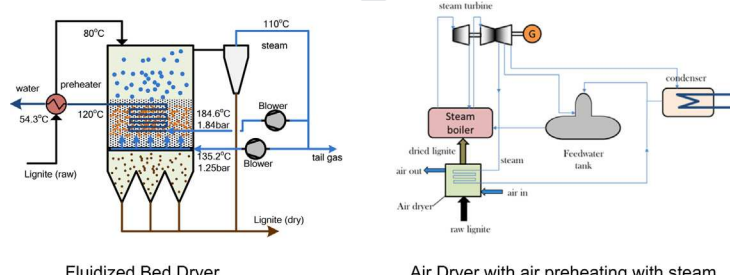
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HIGHLIGHTS

- Thermodynamic analysis of state-of-the-art lignite pre-drying options.
- Integration and optimization of the drying process for different drying methods.
- Most efficient FB drying case: recirculated steam for heating/60 °C drying temp.
- Most efficient air drying case: hot water from feed-water tank/110 °C drying temp.

GRAPHICAL ABSTRACT



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ABSTRACT

Lignite is considered as a domestic and abundant energy source for several countries. However, its high ash and moisture content have a negative effect on power plant efficiency, on cost of electricity (COE) and consequently on CO₂ emissions. The aim of the present work is the investigation and optimization of existing lignite pre-drying concepts and their improvement in terms of overall plant efficiency and integration. The main process parameters examined are the heat source for drying and the respective drying medium. In the conventional lignite drying process, hot recirculating flue gas is used as a heating medium, while in the current state-of-the-art pre-drying concepts, a fluidized bed drying system is considered. Different concepts are also examined including a) the utilization of preheated air as heating medium and b) the optimized integration of a heat pump as a heat source for the drying process. Based on the performed thermal cycle calculations, the plant efficiency increase is evaluated. The results of the study indicate that higher plant efficiency is expected, when focussing on the optimized pre-drying process scheme and its integration with the overall steam.

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1. Introduction

Coal is generally expected to continue to play a key role in the future energy mix as the most abundant and competitive fossil fuel source. Especially brown coal, as a domestic fuel for many European

countries, guarantees the efficient and cost effective power generation in the base load range. Since global climate change and the Kyoto-protocol impose a reduction of CO₂ emissions produced from fossil fuel power plants, the increase of their efficiency and the minimization of their emissions become the main challenges for power producers and manufacturers [1–4]. In the case of brown coal particularly, it is estimated that the optimization of the drying process in future brown coal power plants may lead to an efficiency increase of 4–6 percentage points [5–7]. The development of an efficient brown coal drying process is a necessary step towards

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increasing flexibility in current coal power plants [8,9] and developing the oxy fuel firing technology in future generations of brown coal power plants [10–13]. One of the brown coal pre-drying technologies is the fluidized bed drying concept with waste heat utilization (WTA-Drying). The concept has been successfully demonstrated in a pilot plant in Frechen, Germany and in a prototype fluidized bed dryer integrated in a 1000 MWe brown coal boiler in Niederaussem, Germany [14–16]. The prototype dryer has a nominal capacity of 110 t/h dry lignite and may cover the boiler's thermal input up to a thermal share of 30%. The vaporised coal moisture produced from the drying process is utilized as heating medium for feeding water in the boiler's water preheaters.

Thermodynamic studies on the integration of a lignite dryer in a Greek power plant have been carried out in the past. More specific, initial investigations on lignite pre-drying focused on the comparison of different lignite drying technologies including the conventional tubular drying concept, the fluidized bed drying (WTA) and the Mechanical and Thermal Dewatering Process (MTE) [17–19]. Definite advantages of the "WTA drying" in terms of steam cycle efficiency increase were noticed in the examination, while the complexity of the MTE process was also noticed due to the required mechanical moving parts, although the results in terms thermal efficiency increase were promising. The pressurized fluidized bed concept is also another alternative currently under investigation [20], which however is as complex as the MTE due to the sophisticated construction for attaining and preserving a high pressure. Another simpler concept followed by an American company in the Coal Creek power plant is the utilization of low temperature heat from the cooling water, to reduce lignite moisture in an air fluidized bed dryer from 38% to 29% [21,22]. The particular approach, although it does not provide the exceptional thermodynamic performance in terms of efficiency increase as the other fluidized bed drying concepts, it may be proven as cost effective due to the simpler construction and the lower operating temperatures.

Previous work was focused on the integration of the WTA drying concept in future Greek power plant with elevated steam parameters [23–26] and included also an initial economic assessment. The present work focuses again on the drying technology and the integration of the dryer in a modern steam cycle representing the state of the art for a power plant firing low rank coal. Two different types of dryers are presented and compared:

- the fluidized bed drying concept utilizing steam as a heating and fluidizing medium following the concept proposed by RWE's WTA technology, and
- the drying concept utilizing hot air as fluidizing and heating medium

It should be noted that the particular concept investigated in the present work, differs from the concept applied in the Coal Creek power plant, according to which hot water, and not hot air, is utilized as a heating medium.

Different configurations are examined for each basic case, depending on the heating medium source and the basic components used in the drying process. In order to have a common measure of the two different drying concepts, the thermal share of substitution of raw lignite by dry lignite was set as constant and equal to 25%. Since the air drying process usually operates in lower temperatures (50–80 °C), the drying capacity of the process (i.e. mass flow of moisture evaporated per fuel thermal input) is lower compared with the fluidized bed drying process utilizing low pressure steam bleed (drying temperature 110–130 °C). This means that the fuel input of the air drying system shall be about 10–15% higher than the steam drying system (see Fig. 1), in order to reach the same pre-dried lignite thermal share. Nevertheless as shown in

Fig. 1, the percentage of the coal mass flow to be dried compared with the total mass flow input, when keeping constant pre-dried lignite thermal share is similar for both drying technologies due to large amounts of raw coal, which are still required in the regarding co-firing cases.

2. Methodology

2.1. Drying methods

The description of the drying technologies under investigation is divided in two parts. On the one hand, the description of the drying mechanism and the configuration of each technology are presented. On the other hand, the available options for the adequate heat provision are also analyzed (heat integration with the power plant).

2.1.1. Fluidized bed dryer with steam

The WTA concept of fuel drying in a fluidized bed using steam as fluidizing medium has been described in previous studies [26,27]. The steam for the fluidization is a part of the evaporated moisture that is extracted after cyclone separation. The heat source can either be extracted steam from the steam turbine (Fig. 2a) or evaporated moisture of the fuel, recompressed and recirculated (Fig. 2b). An alternative option for the heat source is also examined in the fluidized bed dryer concept, where the heating medium is water from the feed-water tank of the facility.

2.1.2. Air dryer

The concept of air drying includes the drying of the fuel through a stream of preheated air. The air is initially preheated by a certain temperature heat source. Furthermore it heats up the fuel up to the evaporation point and absorbs the evaporated moisture, increasing its own relative humidity at the same time. This method has the advantage of allowing the drying process to be performed quickly and safely, avoiding self-ignition issues. The outlet air is saturated in most cases and cooled down, and so it cannot be used further in the process; therefore, after the lignite pre-drying, it is released to the atmosphere, following a fundamental filtering.

The aforementioned changes in the condition of air during the drying process can be displayed in a psychrometric chart in Fig. 3.

The quantity of required air and the heat consumption for the drying process has been calculated for different drying temperatures through Simprosys v3.0, a software specialized in drying processes [28]. The calculations have been performed for fuel with 25% and 35% moisture content at the air dryer outlet and the results are shown in Fig. 4.

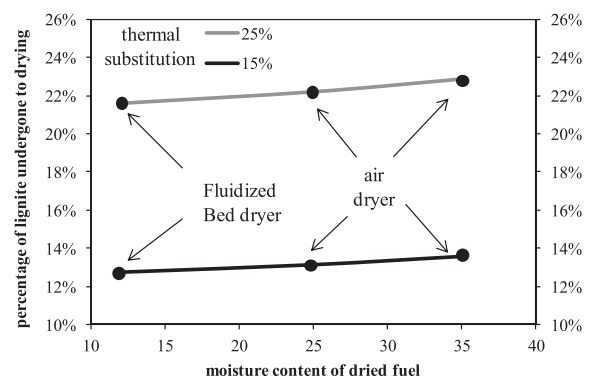


Fig. 1. Correlation of mass fraction of dried lignite to the moisture content and the drying method.

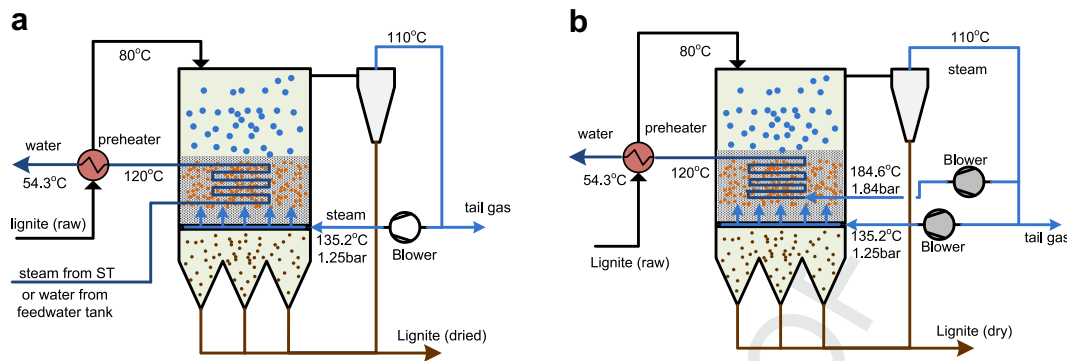


Fig. 2. a: Fluidized bed dryer system, heat medium: extracted steam from the ST or extracted water from the feedwater tank. b: Fluidized bed dryer system, heat medium: recirculating and recompressed steam.

As shown in Fig. 4, the required air flow rate for a certain moisture content in dried fuel decreases at higher inlet temperatures. Hence, the power consumptions at the air fan also drop. On the other hand, the heat duties for air heating before the dryer increase up to the temperature of 80 °C where they reach a local maximum and then they keep increasing in higher temperatures. It should be pointed out that although power requirements are higher at lower temperatures, the exergy losses are lower due to lower temperature differences between solid fuel and the incoming hot air. The determination of the dried fuel moisture content is correlated with both the heat and energy requirements for the drying process. It is observed that for temperatures greater than 140 °C both the required heat consumptions and the required amount of air tend to get stabilized.

The heat load for air preheating before it enters the air-drier can be provided by two sources:

2.1.2.1. Heat from extracted water from the feed-water tank. The feedwater tank contains water to be used for the Rankine steam cycle. A vapour stream is used there for deaeration and

heating of the boiler feedwater, which has also been preheated from the upstream preheaters. Thus, it is in appropriate conditions to be used for heating in the drying process. The stream used from the feed-water tank in the dryer returns back at the condenser and re-enters the cycle. The feedwater that is extracted from the tank is at 190 °C/12.62 bar. The drying system configuration is presented in Fig. 5. After the air preheating, the feedwater returns to the condenser and mixes with the rest condensates.

2.1.2.2. Heat from heat pump. Heat pump technology is an interesting option for effective heating near at ambient temperatures, like in air-drier case. The heat source for the inlet air temperature elevation comes from the condensation of the cooling medium. The main operating parameters of the heat pump system are summarized in Table 1.

The simulations were performed in ASPEN Plus™ in order to calculate the power consumptions and other design and other process parameter of the heat pump in each case, as cooling medium flow rate, COP and pressure ratio. The methodology for the cooling medium flow rate is correlated with the drying heating load, while the pressure ratio calculation is based on the meet of temperature approach requirements at the two heat exchangers. Two alternative options are presented for the location of the evaporator that practically imply where the cooling loads are taken from:

2.1.2.2.1. After the air dryer by cooling the out-coming (wet) air. The drying system configuration is exposed in Fig. 6.

A part of the inlet air sensible heat is provided for the latent heat of evaporation of the moisture, resulting to a lower air temperature at the exit of the dryer. This temperature and the moisture content

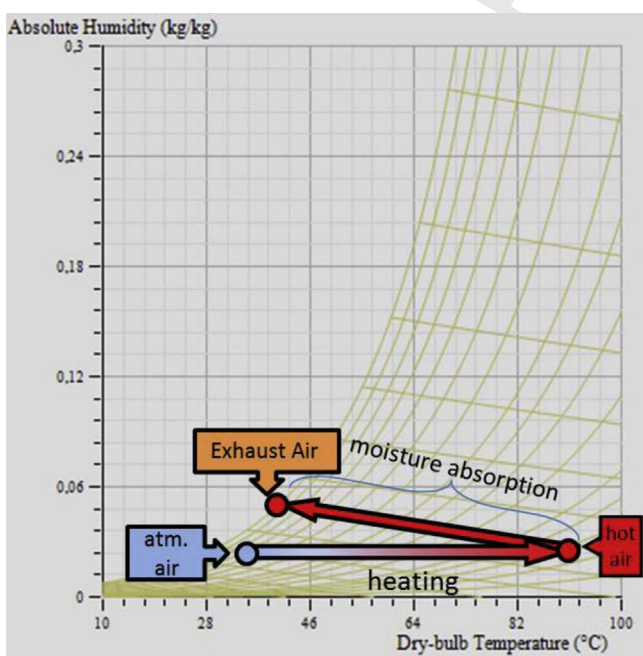


Fig. 3. Psychrometric chart with the changes of air conditions during drying.

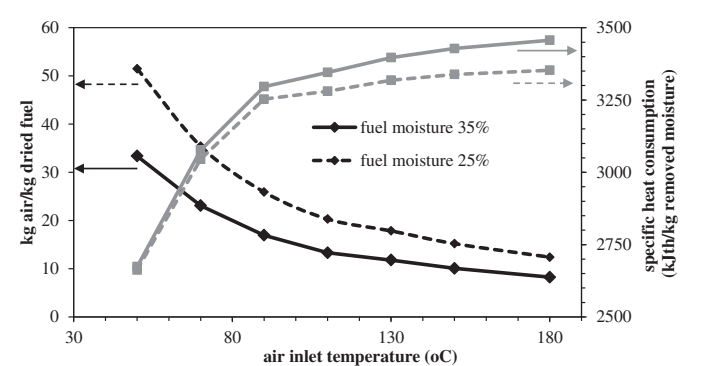


Fig. 4. Effect of air inlet temperature on the required air flow rate and the heat consumption.

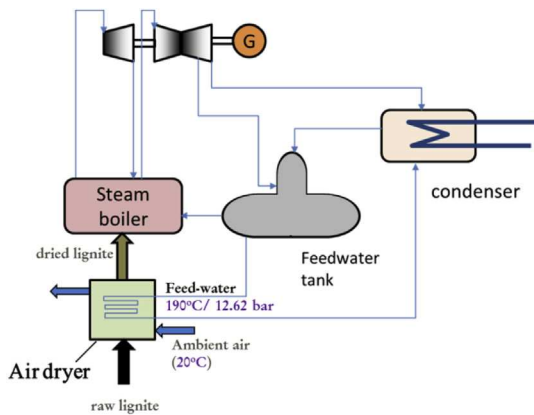


Fig. 5. Air drying cycle with feedwater as a heat source.

Table 1

Main assumptions for heat pumps modelling.

Cooling medium	R134a
Compressor isentropic efficiency	70%
Condenser temperature approach	5 °C
Evaporator temperature approach	3 °C

in the air stream determine the level of evaporation of the cooling medium, affecting the COP and the pressure ratio of the heat pumps system. The water condensation in the evaporator should be taken into account at the design of the heat exchanger. This concept has the feature that the performance of the heat pump system (COP) is independent of the ambient conditions as the levels of the operating temperatures are determined by the user.

2.1.2.2.2. *At the water cooling system before the inlet of the cooling water to the steam condenser.* In this case, the outlet temperature of the cooling water (CW) is higher than the outlet temperature of the air at the previous case, decreasing the temperature difference between condensation and evaporation (T_{hot}/T_{cold}). It is clear that the performance of the heat pumps is strongly associated with the ambient conditions, since the ambient pressure determine the steam condenser voidage and consequently, the outlet temperature of the CW. Nevertheless in the frame of this study, the ambient conditions are assumed stable and same with the reference case (15 °C, 1.01325 bar, 60% relative humidity) (Fig 7).

2.1.2.3. *Heat from steam turbine extraction.* This case uses steam from an intermediate steam turbine extraction to heat the air for the air-drying. The configuration is the same with the case in which water from the feedwater tank is used, with the exception that here the heating medium is steam. The temperature and pressure level of the steam extraction varies, depending on the targeted drying temperature, but for the cases examined in this study, they

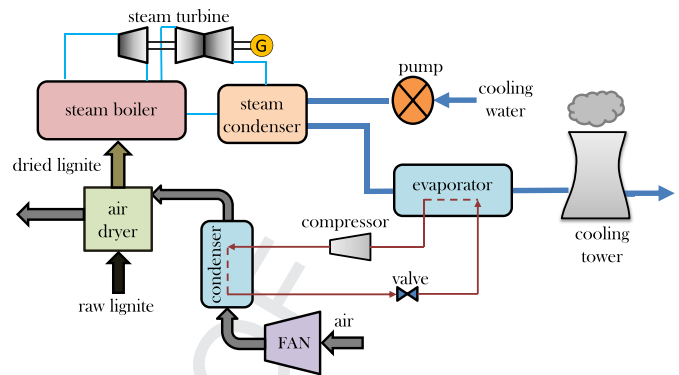


Fig. 7. Heat pump integrated with the air dryer – coupled with the CW system.

generally range between 280 and 380 °C and 4.8–11.2 bar, respectively. The layout of the air drying cycle using steam as a heat source can be seen in Fig. 8.

2.2. Reference plant description

The effect of pre-drying and the optimization of the drying method will be evaluated through thermal cycle modelling calculations in a lignite-fired power plant. The plant layout used for the investigation is typical for the state-of-the art steam cycle to be applied for low rank coal utilization. The estimated net efficiency rate is 39.6%. The nominal electric power is 586 MW_e with one reheat steam cycle and seven water preheaters with steam extraction from the steam turbine (ST). The superheated steam parameters are 610 °C/280 bar, while the reheated parameters are 620 °C/60 bar. The main characteristics of the fuel and the reference plant are summarized below (Tables 2 and 3 respectively) and a detailed flowsheet diagram of the considered steam cycle as modelled in Gatecycle™ 6.1 is presented in Fig. 9a. The energy balance for the reference case is depicted through the Sankey diagram in Fig. 9b.

2.3. Case description

2.3.1. Fluidized bed dryer cases

In all the fluidized bed dryer cases, dry lignite with 12% moisture is used. The ultimate and proximate analysis of the fuel is given in Table 4.

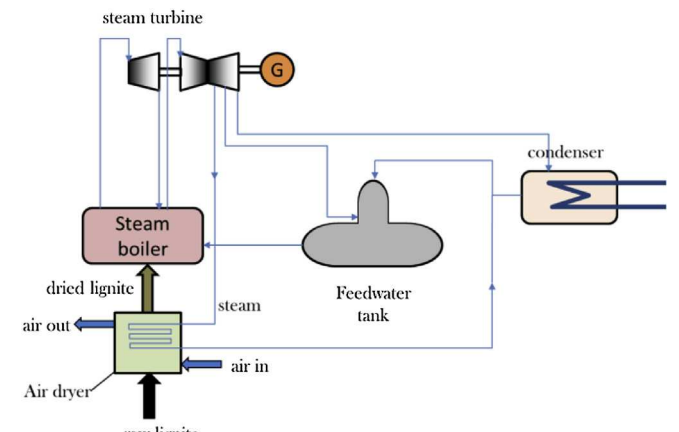


Fig. 8. Air drying cycle with steam as a heat source.

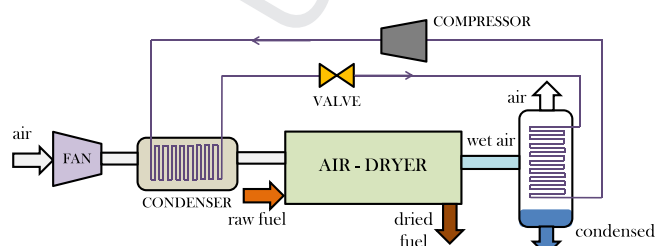


Fig. 6. Heat pump integrated with the air dryer – decoupled with the rest power plant.

Table 2
Raw lignite characteristics.

Ultimate analysis (% dry basis)				
C	H	N	O	S
38.08	3.08	1.28	22.41	0.96
Proximate analysis (% , a.r.)				LHV (MJ/kg, dry)
Moisture	Ash	Volatiles	Fixed carbon	14.41
53.2	16.0	17.0	13.8	

The fluidized bed drying cases examined are the following:

1 Drying using low enthalpy extracted steam

Steam from the LP stage of the Steam turbine is used (29.7 kg/s, 300 °C, 5.96 bar). The steam delivers its heat in the fluidized bed dryer and the condensate returns in the cycle through the water preheater before the feedwater tank. The evaporated moisture from the fuel can be used as a heating medium for an extra, parallel water preheater, saving steam extractions for heating in the existing preheaters.

2 Drying using vaporized moisture recirculation

In this case, evaporated moisture of the fuel, recompressed and recirculated is used both as a fluidizing and a heating medium. This system works decoupled from the rest of the facility, without an interaction and impact on the steam cycle. The only parameter influenced in the steam boiler is the fuel.

Table 3
Reference power plant main characteristics.

Thermal input (MW _{th})	1481.5
Raw fuel flow rate, kg/s	272.2
Superheated steam flow rate, kg/s	492.7
Reheated steam flow rate, kg/s	396.8
Gross power production, MW _e	624.8
Net power production, MW _e	586.2
Net electric efficiency, % LHV basis	39.57
Specific CO ₂ emissions, kg CO ₂ /kWh _{e, net}	0.903

3 Drying using feeding water

As previously described, feedwater from the tank (117 kg/s, 190 °C/12.62 bar) is used in this case as a heating medium in the dryer and returns back at the condenser, re-entering the cycle.

2.3.2. Air drying cases

In the air drying cases, dry lignite is used with i) 35% and ii) 25% moisture content. For both of the above cases, the following cases are distinguished, depending on the medium providing heat to the drying air as they were described above:

- hot water from feed-water tank
- heat pumps – decoupled
- heat pumps – coupled with cooling water
- steam from steam turbine extraction

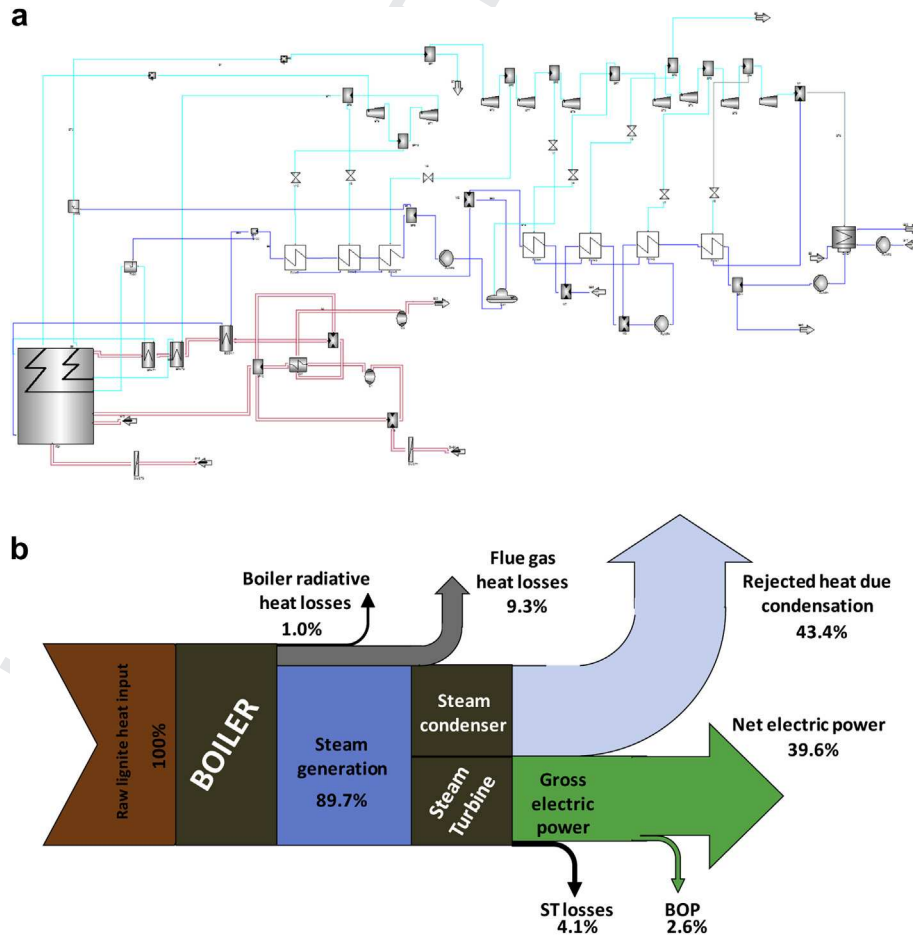


Fig. 9. a: Flow chart of the examined steam cycle in GateCycle™ in % of the Boiler Heat Input (on an LHV basis). b: Sankey diagram of the Reference lignite power plant.

Table 4
Dried lignite characteristics for both moisture contents.

Ultimate analysis (same for both case as it is in % dry basis)				
C	H	N	O	S
38.08	3.08	1.28	22.41	0.96
Proximate analysis (% a.r.)				
Moisture	Ash	Volatiles	Fixed carbon	LHV (MJ/kg, raw)
12	30.09	31.97	25.95	12.38
25	25.64	27.24	22.12	10.19
35	22.22	23.61	19.17	8.51

Finally, the influence of drying air temperature is also investigated as a parameter. In the cases examined, three representative temperatures were selected, 60 °C, 110 °C, 140 °C.

For the FD fan it is assumed it has a 70% isentropic efficiency and a 40 mbar pressure increase. The ultimate and proximate analysis of the fuel for these cases is given in Table 4.

The characteristics of the test cases that are under investigation are summarized in Table 5. The thermal substitution for all cases is assumed 25%.

3. Results and discussion

The results of the performed investigation are presented in the following analysis. What is mainly focused is the attitude of the drying technologies under investigation at the total net efficiency from a thermodynamic and economic point of view. Furthermore the impact of various parameters like dried fuel moisture content and the selection of the heat source on the performance of the power system are also examined.

3.1. Fluidized bed dryer cases

The basic results of the cases with the fluidized bed dryer are summarized in Table 6.

A comparison between the net electric efficiency of the plant for each case can be seen in Fig. 10. The results reveal that the fluidized bed drying technology concept is an interesting option for retrofitting drying as the efficiency of the plant increases more than 1.3%. Case 2 representing the fluidized bed dryer with steam recirculation has the greatest efficiency. In other words, it is more preferable to use dedicated compressors for steam compression than to extract steam or feedwater from the steam cycle. The water flow rate at case 3 is six times greater than the other two cases. This fact leads to larger heat exchanger inside the dryer occupying more space inside the bed, making the fluidization more difficult.

Table 5

Test cases.

a/a	Drying technology	Drying temperature	Dried fuel moisture	Heat source
1	Fluidized bed dryer	110 °C	12%	Steam extraction from ST
2				Steam circulation
3				Hot water from feed-water tank
4	Air dryer	60 °C	35%	Hot water from feed-water tank
5				Heat pumps - decoupled
6				Heat pumps - coupled with cooling water
7		110 °C	25%	Hot water from feed-water tank
8				Heat pumps - decoupled
9				Heat pumps - coupled with cooling water
10		140 °C	25%	Hot water from feed-water tank
11				Steam from ST
12				Hot water from feed-water tank
13				Steam from ST

Table 6
Main results of the fluidized bed dryer cases.

Cases	1	2	3
Dried fuel moisture (%)	12%	12%	12%
Total fuel (kg/s)	260.37	260.37	260.37
Dried fuel (kg/s)	29.91	29.91	29.91
Steam generation (kg/s)	497.8	497.76	497.79
Heat for drying (MW _{th})	77.65	77.65	77.65
Dryer energy duty (MW _e)	2.11	5.75	2.11
Fluidization medium low rate (kg/s)	70.7	70.7	70.7
Heating medium flow rate (kg/s)	29.7	21.9	117.1
Gross power output (MW _e)	622.05	634.02	619.57
Net power output (MW _e)	582.07	590.24	579.49
Net electrical efficiency (%)	41.07%	41.65%	40.89%
Δeff. (%)	+1.50%	+2.07%	+1.32%

3.2. Air dryer cases

The basic results of the cases with the air dryer are summarized in Table 7.

According to Table 7, in this initial assessment the air dryer concept has in general terms a small beneficial impact on plant performance for the air inlet temperature of 60 °C. This is mainly attributed to the power consumption at the air drying fans and the energy penalty for the air heating; for the cases 4 and 7, the gross power output drops, due to the extraction of large quantity of water (around 15% of the total water) for air heating. Although the steam production is not affected the gross output decreases because more steam is extracted from the turbines for the feedwater LP pre-heating. As it is seen, extracted feedwater from the tank is the best option as a heat provider to the air, for certain dried fuel moisture content. For the cases employing heat pumps (5, 6, 8, 9), extra power consumptions for heat pump operation (i.e. cooling medium compression) further deteriorates the efficiency of the plant. It is proved that the best option for the evaporation of the cooling medium is by coupling with the cooling water after the steam condenser, owed to the lower difference between the operating temperatures of the heat pumps that affect the pressure ratio at the cycle.

For air heating temperatures >60 °C the application of heat pumps does not operate efficiently, as the pressure ratio increases and the COP drops considerably at unacceptable levels.

On the other hand, the efficiency for air heating temperatures >60 °C (110 °C and 140 °C) is compared in the cases of feedwater and steam extraction as a heating medium. It occurs that a higher air heating temperature also leads to an efficiency improvement in these cases. The optimum case is the case of using extracted feedwater to heat air at 110 °C (case 10) which is also the optimum case

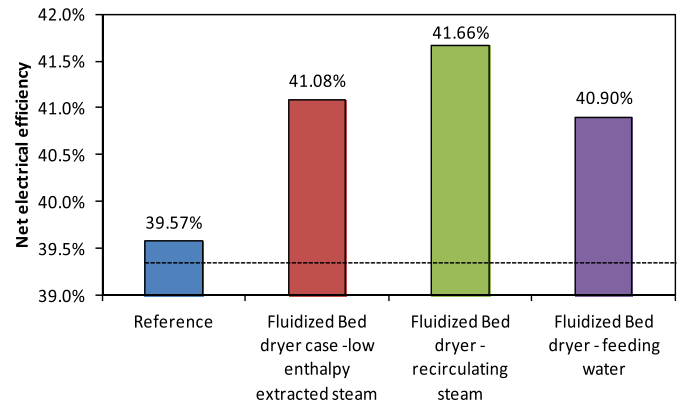
**Fig. 10.** Efficiency for the fluidized bed dryer cases compared to Reference case.

Table 7

Main results of the air dryer cases.

Cases	4	5	6	7	8	9	10	11	12	13
Dried fuel moisture (%)	35%	35%	35%	25%	25%	25%	25%	25%	25%	25%
Total fuel (kg/s)	264.59	264.59	264.59	262.36	262.36	262.36	262.36	262.36	262.36	262.36
Dried fuel (kg/s)	43.53	43.53	43.53	36.33	36.33	36.33	36.33	36.33	36.33	36.33
Steam generation (kg/s)	497.0	497.5	497.5	496.88	498.6	498.6	498.91	498.56	498.5	498.7
Air for drying (kg/s)	1274	1274	1274	1636	1636	1636	782.86	782.86	600.5	600.5
Drying temperature (°C)	60	60	60	60	60	60	110	110	140	140
Feedwater/steam for air heating (kg/s)	80.8	–	–	103.7	–	–	110.37	29.86	133.9	28.1
Heat for drying (MW _{th})	51.58	51.58	51.58	67.45	67.45	67.45	71.82	71.82	72.9	72.9
Dryer energy duty (MW _e)	5.15	5.15	5.15	6.73	6.73	6.73	3.22	3.22	2.47	2.47
Heat pumps energy duty (MW _e)	–	18.5	10.1	–	22.0	13.3	–	–	–	–
COP of heat pump	–	3.64	5.09	–	3.07	3.89	–	–	–	–
T _{hot} /T _{cold} (°C)	–	65.0/10.2	65.0/30.4	–	65.0/9.8	65.0/30.2	–	–	–	–
p _{cond} /p _{evap} (bar)	–	20.0/4.0	20.0/7.5	–	20.0/4.0	20.0/7.5	–	–	–	–
Cooling medium flow rate (kg/s)	–	345.5	347.8	–	431.6	454.4	–	–	–	–
Gross power output (MW _e)	621.652	628.78	628.78	619.94	630.35	630.35	619.11	611.17	611.53	612.05
Net power output (MW _e)	578.4	566.8	575.22	575.16	563.52	572.22	577.85	570.12	571.13	571.73
Net electrical efficiency (%)	40.16%	39.36%	39.94%	40.28%	39.46%	40.07%	40.46%	39.92%	39.99%	40.04%
Δeff. (%)	+0.6%	–0.2%	+0.4%	+0.7%	–0.1%	+0.5%	+0.89	+0.35	+0.42%	+0.47%

for all the air-drying cases. A further increase of air heating temperature (case 12) limits the improvement of the efficiency, as the gross power output is decreased significantly due to the use of a large quantity of feedwater for air heating (around 25% of the total water), and the corresponding use of a large steam extraction quantity for the feedwater LP preheating. Steam extraction used for air heating (cases 11 & 13) presents the reverse behaviour, as in a higher temperature, the steam production is not affected but less steam extraction is required as the steam used is of a higher temperature.

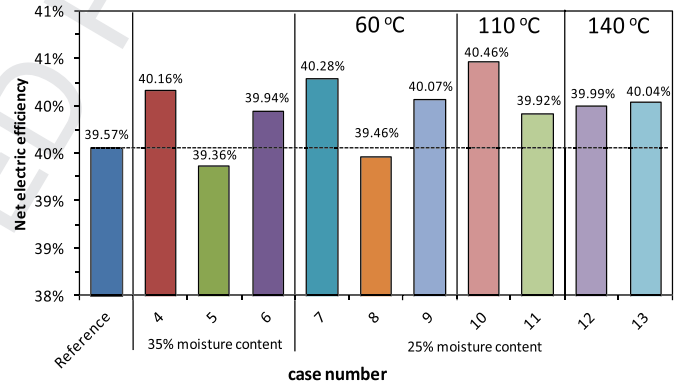
An efficiency comparison of the air drying cases (4–13) to the reference case is shown in Fig. 11.

3.3. Mass and energy balance

Selected cases representing the optimum scenarios for each pre-drying concept are presented in more detail with respect to the thermodynamic characteristics, heat and mass flows. Mass flows and other thermodynamic characteristics such as pressure and temperature are presented in Table 8 and heat streams are presented in the Sankey diagrams of Fig. 12a–d. In addition to the reference case shown in Fig. 9b, the selected cases are:

- case 2, which is the optimum fluidized bed dryer case with steam recirculation,
- case 9, which is the optimum heat pumps case (coupled with cooling water, at 60 °C drying temperature and 25% dried fuel moisture content),
- case 10, which is the optimum air dryer case with feedwater as heating medium (110 °C drying temperature) and
- case 13, which is the optimum air dryer case with steam as heating medium (140 °C drying temperature).

Several conclusions are drawn from Table 8. When the thermal share coming from pre-dried lignite is 25%, then the steam production is increased by 1% compared to the reference case. This is owed to the greater amount of available heat for steam generation, since the adiabatic temperature is greater. The steam that undergoes to phase change in the main condenser is lower in cases 10 and 13 than the other pre-drying cases. In case 10, more steam is extracted from the Low Pressure Steam Turbine for condensate water preheating, since part of the condensate is led for air preheating at the Air Dryer unit. In case 13, 28.1 kg/s steam is condensed in the air dryer preheater and not in the main condenser.

**Fig. 11.** Efficiency for the air drying cases (4–13) compared to Reference case.**Table 8**

Thermodynamic characteristics of water/steam, flue gas and heating medium flows for selected cases.

Cases		Reference	2	9	10	13
Superheated steam	m (kg/s)	492.7	497.5	498.6	496.9	498.6
	p (bar)	280	280	280	280	280
	T (°C)	610.0	610.0	610.0	610.0	610.0
Cold reheated steam	m (kg/s)	390.2	395.5	396.6	397.6	396.6
	p (bar)	64	64	64	64	64
	T (°C)	271.9	271.9	271.9	271.9	271.9
Hot reheated steam	m (kg/s)	396.8	405.3	406.4	409.3	406.3
	p (bar)	60	60	60	60	60
	T (°C)	620.0	620.0	620.0	620.0	620.0
Feedwater after condenser	m (kg/s)	316.5	336.3	322.6	297.7	295.2
	p (bar)	0.06	0.06	0.06	0.06	0.06
	T (°C)	34.9	34.9	34.9	34.9	34.9
Feedwater before ECO	m (kg/s)	492.7	497.5	498.6	496.9	498.6
	p (bar)	329.9	329.9	329.9	329.2	329.9
	T (°C)	301.3	301.3	301.3	301.3	301.3
Cooling water before cooling tower	m (kg/s)	13,650	14,875	14,354	13,262	13,397
	p (bar)	3	3	3	3	3
	T (°C)	34.0	34.0	33.2	34.0	34.0
Flue gas after LUVO	m (kg/s)	932.9	866.8	872.5	873.6	873.6
	p (bar)	0.91	0.91	0.91	0.91	0.91
	T (°C)	159.0	159.0	159.0	159.0	159.0
Heating medium for drying	m (kg/s)	–	21.9	454.4	110.4	28.1
	p (bar)	–	1.84	20.0	14	4.77
	Medium	–	Steam	R134a	Water	Steam
	T (°C)	–	184.8	65.0	195.1	286.6

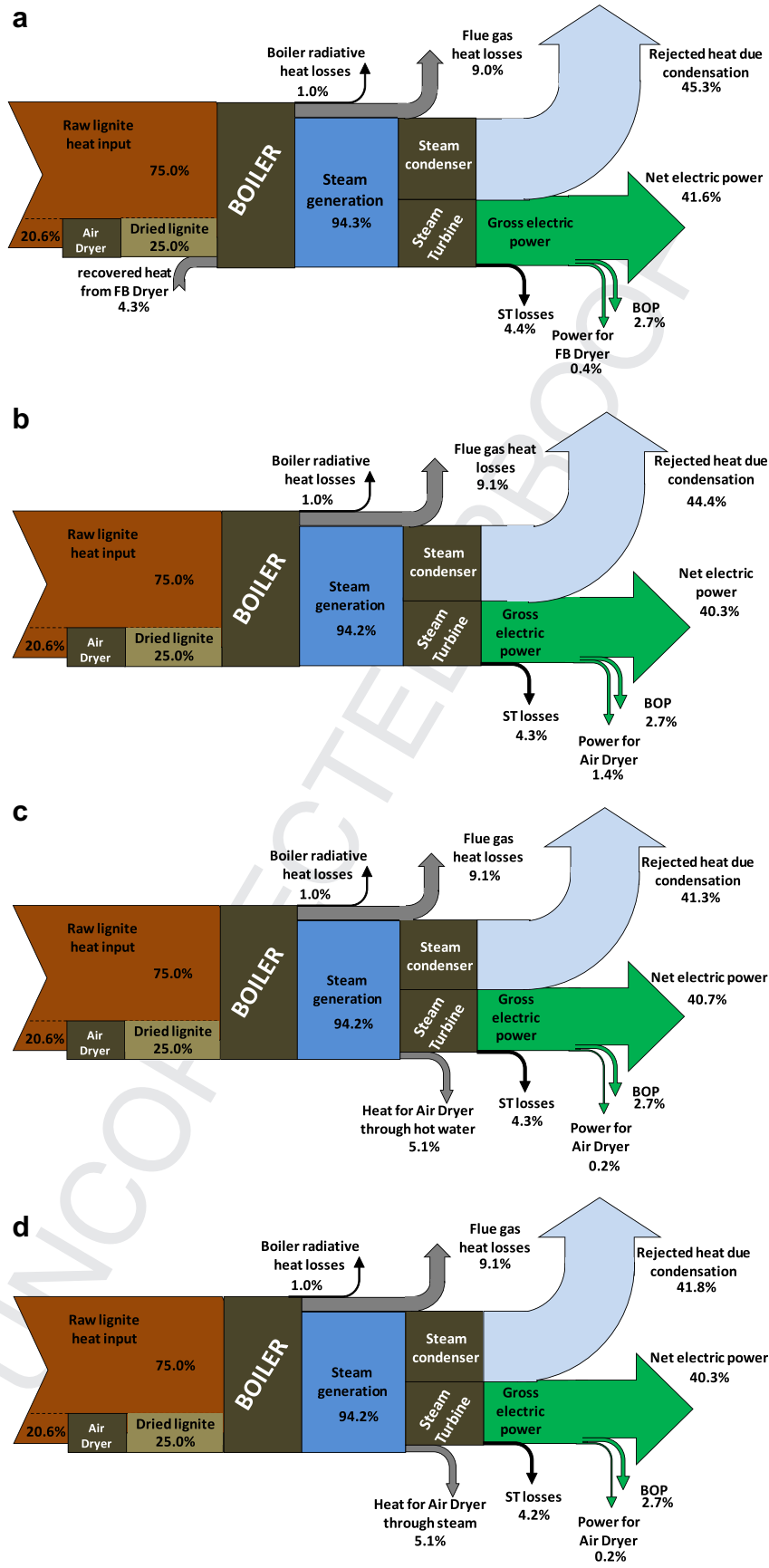


Fig. 12. a: Sankey diagram of Case 2 (FB Dryer with steam recirculation) in % of the Boiler Heat Input (on an LHV basis). b: Sankey diagram of Case 9 (Air Dryer with heat pumps) in % of the Boiler Heat Input (on an LHV basis). c: Sankey diagram of Case 10 (Air Dryer with hot water extraction) in % of the Boiler Heat Input (on an LHV basis). d: Sankey diagram of Case 13 (Air Dryer with steam extraction) in % of the Boiler Heat Input (on an LHV basis).

Consequently, the required cooling water flow rate is decreased in these two cases. In case 9, the cooling water temperature before the cooling tower is 0.8 °C less than the other cases, due to cooling from heat pump medium evaporation. This fact has an effect on the reduction of the cooling load that is should be removed in the cooling tower. A final comment on the basic streams characteristics is about the heating medium flow rates for pre-drying. In case 9 (heat pumps), the R134a flow rate is much greater compared to the other cases, resulting to higher equipment cost.

Fig. 12 depicts the Sankey diagrams for the selected pre-drying concepts. It is more than evident the fuel upgrading through pre-drying as illustrated by the reduced required heat and fuel input in the boiler.

4. Conclusions

Comparing the two drying technologies, it is concluded that the fluidized bed dryer is a more efficient option for retrofitting existing power plants. Calculations reveal that steam recirculation and condensation in the dryer is the best option to provide adequate heat for drying. Air dryer technology at low temperatures is less beneficial than the fluidized bed dryer with steam recirculation as far as total plant performance is concerned, due to the energy penalty in the fans and heat exchangers for heating and transport of air. The air drying concept is not proven yet in a large plant scale; hence additional development work is needed towards determining an optimized configuration, in order to increase its competitiveness. The additional analysis work to be carried out towards cycle optimization shall include, the utilization of the hot water extraction from the feed-water tank as a heat source for air drying. Attention should also be paid to the investigations for the impact of variations in ambient conditions, i.e. change in temperature and relative humidity on air dryer performance.

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