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An all-sky radiative transfer method to predict optimal tilt and azimuth angle of a solar collector

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Abstract

This paper describes a radiative transfer method for calculating radiances in all-sky conditions and performing an integration over the view hemisphere of an arbitrary plane to calculate tilted irradiance. The advantage of this method is the combination of cloud parameters inside the radiative transfer model with a tilt procedure. For selected locations this method is applied with cloud, ozone, water vapour and aerosol input data to determine tilted irradiance, horizontal irradiance and optimal tilt angle. A validation is performed for horizontal and tilted irradiance against high-quality pyranometer data. For 27 sites around the world, the annual horizontal irradiation predicted by our model had a mean bias difference of +0.56% and a root-mean-squared difference of 6.69% compared to ground measurements. The difference between the annual irradiation estimates from our model and the measurements from one site that provides tilted irradiance were within $\pm 6\%$ for all orientations except the north-facing vertical plane. For European and African sites included in the validation, the optimal tilt from our model is typically a few degrees steeper than predictions from the popular PVGIS online tool. Our model is generally applicable to any location on the earth's surface as the satellite cloud and atmosphere data and aerosol climatology data are available globally. Furthermore, all of the input data are standard variables in climate models and so this method can be used to predict tilted irradiance in future climate

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experiments.

Keywords: radiative transfer, tilt, radiance, cloud

1 1. Introduction

The orientation of a plane solar collector such as a PV panel can be varied in the tilt and azimuth directions in order to maximise the incident irradiance. One way to accurately assess the solar resource available on a tilted plane and determine the optimum angle to orient a fixed angle PV panel in the real world, is to position pyranometers in several plane orientations and record the sum of irradiance over a sufficiently long period of time. In practice this is rarely completed, so models to predict the tilted irradiance are used.

There are two concepts fundamental to the method described. Firstly, cloud optical prop-8 erties, from satellite retrievals, are integrated into the radiative transfer (RT) calculation. 9 Secondly, tilted irradiance is derived from a surface radiance field. RT methods are frequently 10 used to model clear-sky solar irradiance (Bird and Riordan, 1986; Gueymard, 1995; Mueller 11 et al., 2004). Sometimes cloud effects are introduced as an adjustment to the clear-sky values 12 depending on satellite-derived cloud albedo (Cano et al., 1986) or tuned based on observed 13 historical ground-level irradiance (Nann and Emery, 1992). In other studies cloud effects 14 are included directly. Lohmann et al. (2006) used data from meteorological reanalyses and 15 cloud parameters from the International Satellite Cloud Climatology Project (ISCCP) with 16 a two-stream radiative transfer code to estimate surface irradiance. Deneke et al. (2008) 17 used cloud retrievals from Meteosat in combination with RT simulations to estimate solar 18 irradiance in the Netherlands. Mueller et al. (2009) used a lookup table approach for clouds 19 with transmissions pre-calculated with RT and values interpolated from the lookup table. 20 They used a cloud effective radius of 10 μ m for water droplets using the Hu and Stamnes 21 (1993) parametrisation of the phase function and did not consider ice clouds. While this 22 may be sufficient for horizontal fluxes, this approach is less accurate when calculating the 23 radiances required for the tilted irradiance. Behrendt et al. (2013) used the SOLIS clear-sky 24 model with cloud adjustment to determine the spectral effects on different PV technologies. 25 A separate run with clouds specified directly inside the radiative transfer model was per-26

formed. The difference in spectral transmission between SOLIS and the RT solution using 27 the libRadtran package (Mayer and Kylling, 2005) is about 5% in average photon energy 28 for thick cloud cover (optical depth of 60) at a solar zenith angle of 60°. More recently, the 29 UniSky simulator software (Kocifaj and Fečko, 2014; Kocifaj, 2015) includes the effects of a 30 3D cloud field to model ground-level radiances. Current satellite products often include the 31 required cloud optical properties, namely cloud phase (water or ice), cloud optical depth, 32 and cloud droplet effective radius, to allow RT simulations including clouds to be performed. 33 One motivation for inclusion of clouds inside the RT calculation is for the development of 34 solar energy models that can be applied to a wide variety of historical, current and future 35 datasets, for example meteorological reanalyses or climate models, as well as satellite obser-36 vations. Another is the spectral effects of cloud attenuation are better captured with RT 37 simulation, which is important for PV. 38

After the directional radiances have been calculated from the RT simulation, integrating 39 the radiance field over the direction of interest will provide the tilted irradiance. McArthur 40 and Hay (1981) used radiance distributions obtained from fish-eye photographs and obtained 41 agreement to $\pm 10\%$ for horizontal diffuse irradiance and $\pm 5\%$ for tilted irradiance on a south-42 facing plane, in a variety of sky conditions. Brunger and Hooper (1993) derived an empirical 43 model for the sky radiance distribution calculated from observations of clearness index (ratio 44 of surface irradiance to extraterrestrial irradiance) and zenith angle. Similarly Gueymard 45 (1987) derived the sky radiance distribution by producing different anisotropic sky radiance 46 distributions for a clear-sky and an overcast sky. The all-sky radiance distribution was 47 calculated as a weighted sum of the clear and overcast cases with cloud transmission as the 48 weighting factor. 49

Other popular anisotropic tilted irradiance models (e.g. Bugler (1977); Klucher (1979); Willmott (1982); Hay and Davies (1980); Skartveit and Olseth (1986); Reindl et al. (1990); Perez et al. (1990); Muneer (1990)) are varyingly complex functions of the horizontal diffuse and direct irradiance measurements along with solar position and panel orientation. A comparison between ten tilt models at the NREL site at Golden, Colorado, USA, found that most anisotropic models did not predict irradiance with a satisfactorily low error for tilted planes compared to the bounds of instrumental error from pyranometers (Gueymard, 2009). An intercomparison of 15 models (4 isotropic and 11 anisotropic) in Denmark, France and Spain again found that no one anisotropic model generally performed better than the others consistently when considering different cloud conditions, tilt angles and azimuth angles (Gracia-Amillo and Huld, 2013). Therefore, the continued development of tilt models for all-sky conditions is desirable.

In this paper, the optimal tilt angle of a fixed-angle solar collector is considered. For 62 comparison with the PVGIS method, the panel is oriented towards the equator, although 63 it is also possible to optimise azimuth as shown in section 4.3. In the absence of horizon 64 obstruction, shading, or radically different morning and afternoon weather conditions, the 65 equatorial direction provides the best azimuthal alignment. The tilt angle of integration is 66 varied to find the irradiance at each angle and summed over a year of operation to determine 67 the optimal tilt. The model is tested against the tilted irradiance model in PVGIS and 68 compared to tilted irradiance measurements from NREL. 69

70 2. Determining tilted irradiance from radiances

The irradiance on a tilted plane angled at tilt β and azimuth γ is a combination of the downwards and upwards radiance fields such that the bounds of the integration is over the hemisphere with base in the plane of the solar collector (Gueymard, 1987):

$$I_T = \int_0^{2\pi} \int_0^{\theta_m} L(\theta, \phi) \cos \theta_d \sin \theta \, \mathrm{d}\theta \, \mathrm{d}\phi \tag{1}$$

where the angle between the normal of the tilted plane and the radiance direction of interestis given by

$$\cos\theta_d = \cos\beta\cos\theta + \sin\beta\sin\theta\cos(\phi - \gamma) \tag{2}$$

and the bound of the integration θ_m is in the plane of the solar collector such that

$$\theta_m = \frac{\pi}{2} - \tan^{-1}(\cos(\phi - \gamma) \tan\beta).$$
(3)

The radiance field L is calculated at a resolution of 3° in the polar direction and 10° in the 77 azimuthal direction using the DISORT radiative transfer code (Stamnes et al., 2000), as part 78 of the libRadtran package (Mayer and Kylling, 2005), with a pseudo-spherical correction to 79 improve accuracy at low solar elevations (Dahlback and Stammes, 1991). θ is the polar angle 80 and ϕ is the azimuthal angle. The radiative transfer equation is solved numerically with 81 16 streams, the minimum recommended for calculating radiances (Mayer et al., 2012). Eq. 82 (1) is approximated numerically by summing each radiance element over small solid angles 83 $\Delta\theta\Delta\phi$ such that 84

$$I_T \approx \sum_j \sum_k L(\theta_j, \phi_k) W \Delta \theta_j \Delta \phi_k \tag{4}$$

where $W = \max(0, \cos \theta_{dj} \sin \theta_j)$ to ensure only the radiances in the field of view of the solar collector are counted (McArthur and Hay, 1981). At non-zero tilts, the field of view will include some upwelling radiances from the ground which depend on the surface albedo and exclude any sky radiances emanating from directions behind the solar collector. $\cos \theta_{dj}$ is as given in eq. (2) with (θ, ϕ) replaced with (θ_j, ϕ_k) .

To perform a complete calculation line-by-line over the whole solar spectrum for 61×36 radiance directions is infeasible in terms of computational time, so the correlated-k method (Kato et al., 1999) is used to divide the solar spectrum into 32 wavelength bands with similar atmospheric absorption properties. The calculation in eq. (4) is performed for each correlated-k band and the broadband radiance for each (θ_j, ϕ_k) pair is obtained by summing up I_T for each of the 32 correlated-k bands.

The numerical approximation in eq. (4) is performed for the diffuse irradiance only. The direct normal irradiance (DNI) is simpler to calculate. From the Beer-Lambert law the DNI is

$$I_B = I_0 \exp(-m\tau) \tag{5}$$

⁹⁹ where I_0 is extraterrestrial irradiance and m is air mass. The optical depth τ describes the ¹⁰⁰ likelihood that a ray travels to the surface of the earth without being absorbed or scattered. au_{101} au is the overall sum of the optical depths of all extinction phenomena in the atmosphere, e.g. mixed gases, ozone, water vapour, aerosols and cloud droplets. For a tilted plane, the direct incident irradiance is

$$I_{BT} = I_B \cos \theta_i \tag{6}$$

where the incident angle θ_i follows a similar form to eq. (2):

$$\cos\theta_i = \cos\beta\cos\theta_z + \sin\beta\sin\theta_z\cos(\phi_a - \gamma). \tag{7}$$

¹⁰⁵ Here, θ_z is the solar zenith angle and ϕ_a is the solar azimuth angle.

The radiative transfer method bears another advantage over empirical tilt models in 106 that no assumption of the size and shape of the circumsolar region is made. When making 107 ground irradiance measurements, the direct irradiance is not usually discernible from diffuse 108 sky irradiance that has been scattered into the region of the solar disc or diffuse radiation 109 emanating from the solar region that has been caused by strongly forward scattering aerosol 110 or thin cloud. This can cause issues in calculating the direct and diffuse contributions as a 111 decision has to be made on the angular size of the circumsolar region (Blanc et al., 2014). 112 Often a half-angle of 2.5° is used with all irradiance inside this region treated as direct. In 113 our model, all scattered radiation is treated as diffuse regardless of the scattering direction 114 with the directional distribution handled by the radiance field. 115

¹¹⁶ 3. Inputs into the model

To generate the radiance field, inputs of the atmospheric state, location altitude, clouds, aerosols and surface albedo are required. Although any climate, satellite or reanalysis dataset that provides all of the necessary inputs can be used, we use the Moderate Resolution Imaging Spectroradiometer (MODIS) instrument data on the Aqua and Terra satellites for all parameters except aerosols for which we use a climatological run from a dedicated aerosol model (GLOMAP). The Terra satellite overpasses the equator at approximately 10:30 local solar time daily and the Aqua satellite overpasses at approximately 13:30 daily. Therefore,

synoptic diurnal differences between the morning and afternoon can be partially captured. 124 MODIS Level 3, 8-day mean data for ozone, water vapour, and cloud parameters (MOD08E3) 125 and MYD08E3 data series, both Collection 5.1) were used. Surface albedo was obtained 126 from the combined Terra and Aqua 16-day running mean albedo product MCD43C3, which 127 is updated every 8 days. The resolution of the atmosphere and cloud data is $1^{\circ} \times 1^{\circ}$ and 128 the albedo data is $0.05^{\circ} \times 0.05^{\circ}$. All data is freely available from the MODIS portal at 129 http://modis-atmos.gsfc.nasa.gov/. 8-day time resolution is used as a trade-off be-130 tween capturing fluctuations in weather conditions and computational efficiency. Daily and 131 monthly timesteps are also available for the Level 3 MODIS data. 132

133 3.1. Atmosphere

Well-mixed gases in the atmosphere are a source of Rayleigh scattering which is dependent on wavelength. Shorter wavelengths are scattered more strongly according to the well-known λ^{-4} relationship.

libRadtran contains the set of six standard AFGL atmospheres (Anderson et al., 1986)
which are tropical, mid-latitude summer and winter, sub-Arctic summer and winter, and
US standard. The location and time of year dictates which particular atmosphere was
selected in the calculation, however the impact of mixed gases on the final result is negligible
(Oumbe et al., 2008; Mueller et al., 2009). Ozone is a strong absorber in the ultraviolet
range and water vapour has absorption bands located throughout the near infrared, so the
total atmospheric column depth of ozone and water vapour are taken from the MODIS data.

144 3.2. Clouds

¹⁴⁵ Clouds are both the largest attenuating factor in the transmission of solar radiation and ¹⁴⁶ the source of the largest uncertainty for many regions of the world, the principal exceptions ¹⁴⁷ being in areas of high aerosol optical depth and infrequent clouds such as deserts. Both ¹⁴⁸ liquid and ice water clouds exhibit complex scattering properties. The radiative properties ¹⁴⁹ of clouds are determined by cloud droplet effective radius $r_{\rm eff}$, single scattering albedo ω , ¹⁵⁰ phase function $P(\mu)$ where μ is the cosine of the scattering angle, and the cloud water content C which is the mass of cloud droplets present in a given volume. The cloud optical depth τ_c is a function of C and r_{eff} . The single scattering albedo determines the probability that if a ray collides with a cloud droplet, it is scattered rather than absorbed. The phase function describes the directional distribution of scattering event and hence is important in determining the final diffuse irradiance field.

For calculating radiances it is recommended to use the full Mie scattering parametrisation for liquid cloud droplets (Mayer et al., 2012) which provide ω and $P(\mu)$ as a function of wavelength. This is available as an extension to the core libRadtran package in the form of pre-calculated lookup tables generated using the Wiscombe (1980) Mie scattering code.

Ice clouds pose a particular complexity as ice crystals form in a variety of habits (shapes), 160 on which the scattering phase function is strongly dependent. Additional morphological 161 features such as surface roughness and trapped air bubbles also affect the phase function 162 (Xie et al., 2006, 2012). The cloud retrieval algorithm for Collection 5.1 in MODIS uses a 163 mixture of particle habits depending on the maximum diameter D_{max} of the ice crystals: 164 50% solid columns, 15% 3D bullet rosettes and 35% hexagonal plates for particles where 165 $60 < D_{\rm max} < 1000 \ \mu {\rm m}$, and 45% solid columns, 45% hollow columns and 10% aggregates 166 for particles where $1000 < D_{\text{max}} < 2000 \ \mu\text{m}$ (Baum et al., 2005; Menzel et al., 2010; Min-167 nis et al., 2011). A definition of 100% solid columns has been used in our model due to 168 the difficulties of mixing habit types and the fact that solid columns make up the largest 169 part of the mixture in the range of 60 $\,<\,D_{\rm max}\,<\,2000\,$ $\mu{\rm m}$ corresponding to $r_{\rm eff}$ of ap-170 proximately $20-120 \ \mu m$, encompassing the majority of ice cloud effective radius retrievals. 171 Out of the single-habit assumptions, solid columns provide the best estimates of ice water 172 content and $r_{\rm eff}$ (Baum et al., 2005). The ice scattering has been represented by a double 173 Henyey-Greenstein (DHG) phase function using the Key et al. (2002) model. The DHG is a 174 convenient simplification of the real phase function that is suitable for modelling radiances 175 due to its ability to somewhat account for the forward and backward scattering peaks better 176 than the simpler single Henyey-Greenstein (HG) phase function (Mayer et al., 2012). In 177 order to correctly model ice cloud scattering a full phase matrix scattering code should be 178

used (e.g. Baum et al. (2014)), however the number of Legendre coefficients that need to 179 be calculated for each scattering phase function make its use computationally prohibitive 180 for multiple calculations. The DHG phase function is smooth and does not include effects 181 such as the 22° and 46° halo scattering peaks present in pristine hexagonal columns and 182 plates. The roughened hexagonal column phase function has a less strong forward scattering 183 component than pristine hexagonal columns and does not exhibit a halo effect, therefore is 184 represented better by the DHG phase function. The assumption of roughened hexagonal 185 columns provides the lowest RMS error in optical depth for MODIS retrievals (Xie et al., 186 2012) adding justification for the smooth DHG phase function approximation. 187

Owing to the large uncertainties in modelling clouds in time and space, it was decided to 188 use a simplified approach with two atmospheric columns, one clear and the other overcast. 189 The resulting radiance distribution is weighted between the two situations based on cloud 190 fraction c_f . To define the cloudy column, the cloud liquid water content C_w , cloud ice water 191 content C_i (both g m⁻³), cloud fraction c_f , cloud height h, and r_{eff} are used. r_{eff} may be, and 192 usually is, different for liquid and ice droplets. Where both liquid and ice clouds are present, 193 they are aggregated into the same column to create one mixed-phase cloud. The cloud is 194 defined as having a vertical depth of 1 km except where the cloud top height is less than 195 1 km above the ground in which case it extends down to the surface. For single scattering 196 albedos $\omega \to 1$, which is the case for the majority of solar wavelengths (Hu and Stammes, 197 1993), the fraction of transmitted to incident irradiance is approximately independent of 198 the cloud geometric height. This has previously been demonstrated in RT calculations 199 (Rozwadowska, 2004; Oumbe et al., 2008). For mathematical convenience and consistency 200 with other investigations (e.g. Lohmann et al. (2006)) the somewhat arbitrary depth of 1 km 201 has been chosen. C_w , C_i , c_f and r_{eff} are all available from the MODIS data. Currently h is 202 only reported for Aqua, so cloud top pressure, which is available from both satellites, was 203 converted to height for both Terra and Aqua data using the hydrostatic equation. 204

205 3.3. Aerosols

A monthly aerosol climatology is provided by the GLOMAP model (Scott et al., 2014) at 206 a resolution of $2.8^{\circ} \times 2.8^{\circ}$, which specifies ω , the asymmetry parameter g, and aerosol optical 207 depth τ_a for 6 wavelength bands in the shortwave spectrum on 31 pressure levels. g describes 208 the mean cosine of the scattering angle from $P(\mu)$ and ranges from -1 for backscattering 209 to +1 for forward scattering. The species included are sulphate, sea-salt, black carbon and 210 particulate organic matter aerosols in four size modes. A HG phase function is specified in 211 our model, which has the large computational advantage of completely parametrising the 212 phase function by q. MODIS data for aerosol has not been used as aerosol properties are 213 not always available over land, particularly in desert regions which are important for solar 214 energy and aerosols are prevalent. 215

216 3.4. Albedo

The surface albedo is the proportion of downwards irradiance that is reflected by the earth's surface. In reality, surface albedo is a function of wavelength and solar zenith angle as direct and diffuse irradiance components have different reflectance properties. Albedo is important in the tilted irradiance calculation as it defines the amount of reflected irradiance available from the ground that is available to a solar collector. Even at zero tilts, a higher surface albedo can increase downwards irradiance due to multiple reflections between surface and atmosphere, particularly if clouds are present (Gueymard, 2009).

The black-sky and white-sky albedos are calculated from the bi-directional reflectance 224 distribution function (BRDF). Black-sky albedo is the albedo assuming all direct irradiance 225 and no diffuse irradiance and is a function of solar zenith angle, whereas white sky albedo 226 assumes a purely diffuse isotropic source and is independent of solar geometry. We have 227 used the white sky albedo in this simulation due to the solar zenith independence. Deneke 228 et al. (2008) has shown that this does not introduce significant error even in thin clouds. 229 Surface albedo is spatially and temporally variable, even throughout the course of the same 230 day (Gueymard, 2009), with the surface properties within a few metres of the solar collector 231 of greatest importance. 232

233 4. Application of the model

One year of atmosphere, cloud and albedo data from 2013 was input into the model, and the solar zenith and azimuth were calculated at the centre of each hour for the middle day in each 8 day period. The diffuse radiance field L and direct normal irradiance I_B for each hour are the outputs from libRadtran. Plane irradiance for a particular tilt and azimuth is obtained by applications of eqs. (4) and (6) and adding together the results.

239 4.1. Radiance distributions

Fig. 1 shows the diffuse radiance distributions for clear sky, overcast sky and all sky 240 (combination of clear and overcast), for a typical midday hour in northern European summer. 241 The clear-sky case includes mixed gas, water vapour, ozone and aerosol attenuation. The 242 anisotropy of clear-sky diffuse radiation due to the circumsolar region, and to a lesser extent 243 the bright section near the horizon, can be seen from fig. 1(a). If an overcast sky is assumed 244 (fig. 1(b)), it can be seen that the radiance distribution is much different, with a maximum 245 intensity between the solar position and zenith which becomes apparently uniformly less 246 intense away from this maximum towards the horizon. Fig. 1(c) shows the all-sky weighted 247 radiance distribution taking into account the cloud fraction, which for this hour was 56.4%. 248 The circumsolar peak is still apparent, but the horizon brightening contribution is hard to 249 discern and the remaining sky radiance is more isotropically distributed than in the clear-sky 250 case. 251

252 4.2. Tilted irradiance map

The radiance distributions for the same location were integrated over all polar and azimuthal alignments using eq. (4), and the direct beam included, to provide a tilted irradiance map (fig. 2). Fig. 2(a) shows that when there are no clouds, the ideal panel alignment is more or less normal to the solar beam. There is a fairly wide tolerance around the optimal position as a result of the cosine of incidence angle being approximately 1 for small incidence angles. Fig. 2(b) shows that in an overcast sky, the ideal panel alignment is horizontal and independent of the solar direction even though the corresponding radiance distribution is

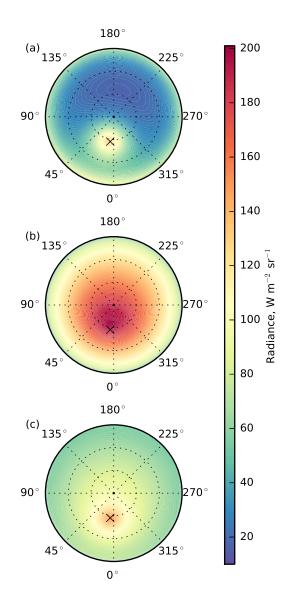


Figure 1: Radiance distributions (looking upwards). Distance from the centre represents polar angle and angular coordinate represents azimuth angle. (a) clear sky radiance distribution, (b) overcast radiance distribution (water cloud optical depth of 8.8), (c) all-sky distribution based on clear sky and cloudy sky distributions with cloud fraction equal to 56.4%. Solar position is represented by X at zenith 32.9° , azimuth 8.2° (the convention in this paper for azimuth is 0° for south, increasing clockwise).

off-zenith. In this example the optical depth of the cloud layer is 8.8, which is thick enough to obscure the solar beam (Oumbe et al., 2008) with the resulting diffuse irradiance approximately isotropically distributed. Fig. 2(c) shows the all-sky tilted irradiance map with the cloud fraction of 56.4%. The optimal tilt of the solar collector is centred around the solar position as in the clear-sky case, but with corresponding lower irradiance values.

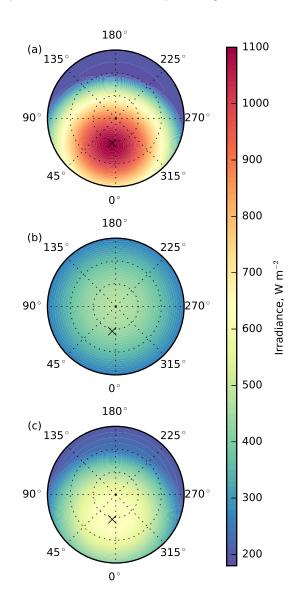


Figure 2: Tilted irradiance maps for the same location as fig. 1. Distance from the centre represents tilt angle with centre representing a horizontal alignment and the edge of the circle represents a vertical alignment. Angular coordinate represents azimuthal alignment. (a) clear sky, (b) overcast sky (water cloud optical depth of 8.8), (c) all-sky with cloud fraction equal to 56.4%. Solar position is represented by X at zenith 32.9°, azimuth 8.2°.

²⁶⁵ 4.3. Yearly tilted irradiation

Radiance distributions were obtained for each hour of the middle day for each 8 day period, and integrated using eq. (4) to produce tilted irradiance. The direct beam contribution was included. Hourly irradiance outputs were then multiplied by the number of days in each period (8, except for the last period of the year which is 5 or 6) and summed to generate the yearly irradiation. For Church Fenton weather station in the UK, the yearly irradiation map is shown in fig. 3.

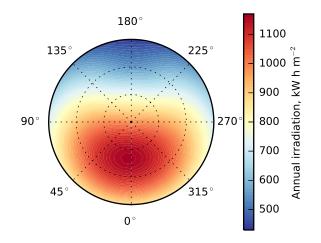


Figure 3: Angled irradiation map for Church Fenton (latitude 53.8°N, longitude 1.2°W, altitude 8 m) for the year of 2013

The optimal south-facing tilt for this location calculated using our method is 40° from 272 the horizontal. The optimal azimuthal alignment here is 6° west of south, highlighting that 273 the afternoon conditions may be clearer than the morning, although the difference in yearly 274 output between 6° and 0° is very small. A "rule of thumb" for annual optimal tilt is that 275 is should be equal to latitude on the basis that this minimises the incidence angle between 276 the solar beam and the normal to the panel surface at solar noon. For areas of the world 277 with significant cloud cover this does not hold true due to the frequent obscuring of the sun 278 by clouds. Christensen and Barker (2001) showed for the US the local clearness index could 279 be used to determine how close to latitude the optimal tilt angle β_{opt} would be with the 280 following relationship: 281

$$\beta_{\rm opt} = (0.379 + K_{\rm t,year})l - 20.6(1 - K_{\rm t,NDJ}/K_{\rm t,MJJ})$$
(8)

with l representing latitude and $K_{t,i}$ representing clearness index where for i NDJ = {November, December, January}, MJJ = {May, June, July} and year=annual. For the Church Fenton weather station in fig. 3, $l = 53.8^{\circ}$, and for 2013 $K_{t,year} = 0.424$, $K_{t,MJJ} = 0.458$ and $K_{t,NDJ} = 0.332$. These low mean clearness indices are indicative of frequently cloudy conditions. Equation (8) predicts $\beta_{opt} = 38^{\circ}$ for this station, close to the 40° calculated with the integrated radiance method. Both models suggest the optimal tilt is more horizontal than the angle of latitude at this location.

289 4.4. Treatment of broken cloud fields

As described in section 3.2, the model uses a linear combination of clear and overcast 290 radiance distributions weighted by the cloud fraction. In reality, clouds exhibit both vertical 291 and horizontal heterogeneity, and our model is a simplification of the 3D picture (Marshak 292 and Davis, 2005). The diffuse reflections from the sides of clouds, along with cloud shadowing, 293 will impact the ground-level radiance field. We therefore compare our radiance distribution to 294 that generated by the UniSky simulator software available from http://www.unisky.sav.sk 295 (Kocifaj, 2012; Kocifaj and Fečko, 2014; Kocifaj, 2015). The UniSky simulator can model 3D 296 clouds either as a regular grid, or as randomly orientated. Random clouds can be grouped 297 into a preferred sky sector, simulating the effects of a morning or evening weather front. For 298 random cloud fields, a random seed is specified on input, allowing reproducibility of random 299 simulations. 300

To keep the simulations consistent, as the two models take different parameters, a simple case is considered. We set the solar zenith angle to be 30° and azimuth to be 0°, cloud fraction 20% with base at 3 km, geometric height 1 km and optical depth 10, and perform a single monochromatic calculation at 550 nm wavelength. A generic aerosol with a Henyey-Greenstein phase function (g = 0.7), optical depth $\tau_a = 0.2$ and single scattering albedo $\omega = 0.9$ is prescribed and surface albedo is set to zero. Both models use the nadir-view cloud fraction, which is the proportion of horizontal area covered by clouds to the total area,
as viewed from a nadir-viewing instrument such as a satellite.

An additional parameter used in UniSky is the cloud reflectance. This is not supplied explicitly in our model but can be calculated. As cloud reflectance is dependent on optical depth, a plane-parallel cloud with $r_{\rm eff} = 10 \ \mu m$, optical depth 10, base 3 km and vertical extent 1 km, with full Mie phase function, was modelled in libRadtran. Reflectance was found to be 40.7% at 550 nm, based on the ratio of upwelling to downwelling irradiance at the top of atmosphere with molecular scattering and absorption suppressed. Clouds are modelled as spheres in UniSky; the default value of 0.5 km radius is used.

100 runs of the random cloud field in UniSky were generated with the parameters described above, with the random seed ranging sequentially from 1 to 100. Two examples of these diffuse radiance fields for sun unobscured and sun obscured are shown in fig 4. The 100 random runs could simulate a short period of time in which solar zenith angle and weather conditions remain relatively constant overlaid with a wind-driven broken cloud field. As UniSky does not include the DNI as an output (M. Kocifaj, personal communication), this was determined from eq. (5) with the total optical depth the sum of each component:

$$\tau = \tau_c + \tau_a + \tau_R \tag{9}$$

where $\tau_a = 0.2$, τ_R is the Rayleigh scattering optical depth at 550 nm of 0.1014 calculated 323 as in Kocifaj (2012) and τ_c is equal to 10 if the pixel is obscured by cloud and 0 otherwise. 324 Each of the 100 radiance fields produced by UniSky, along with the calculated beam 325 component, was numerically integrated using a south-facing plane with tilt angle running 326 from 0 to 90°. For the libRadtran run, one radiance field with cloud optical depth of 10 and 327 cloud fraction 0.2 was calculated and the numerical integration applied. The mean value 328 from the 100 UniSky runs is compared to the libRadtran output and the results for tilt angle 329 ranging from 0 to 90° facing south are shown in fig. 5. 330

In both the libRadtran and the mean of the UniSky runs, the irradiance for this situation is maximised when the tilt angle is 29°. The effect of cloud obscurity can clearly be seen

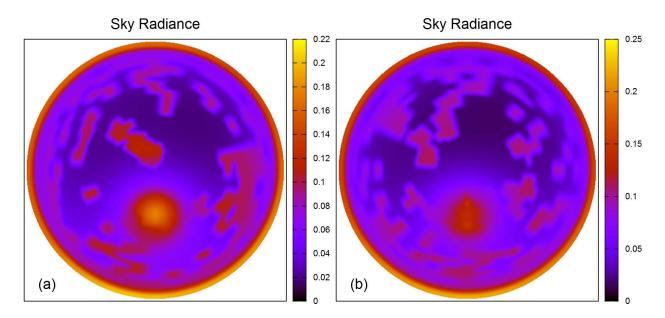


Figure 4: UniSky radiance distributions for two broken cloud regimes ($c_f = 0.2$) where (a) the sun is not obscured and (b) the sun is obscured. Units are radiance normalised to the extraterrestrial DNI [sr⁻¹].

in the bimodal character of the UniSky runs characterised by the clustering of the thin grey lines in fig. 5. When a cloud lies in front of the sun, the irradiance at optimal tilt is around 0.2 of its extraterrestrial values whereas it is close to 0.9 in the unobscured case. The majority of this effect is due to the difference in direct beam transmission between the two modes. The libRadtran method predicts a slightly higher irradiance at all tilt angles under this method compared to UniSky.

As the UniSky simulator does not include multiple scattering within clouds (M. Kocifaj, 339 personal communication), only the gaps between clouds contribute substantially to down-340 welling radiances. It is recommended (Kocifaj, 2015) to approximate a high cloud fraction 341 with an aerosol layer that represents forward scattering by cloud water droplets. Therefore, 342 for broken clouds under low cloud fraction, the good correspondence between the two models 343 for long-term irradiation totals indicates that the 3D reality can adequately simplified into 344 the 1D weighted clear/overcast simulation, although our model does not replicate an instan-345 taneous scene. For high cloud fractions, the sky diffuse radiances approach the isotropic 346 case, and the 1D approximation used in our model is well-known to be appropriate. 347

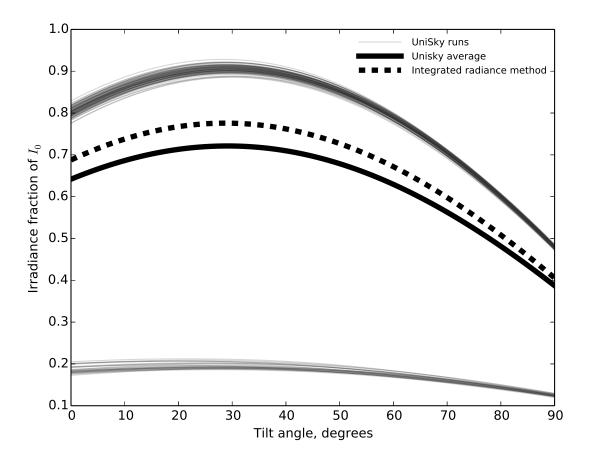


Figure 5: Plane irradiance as a function of panel tilt for 100 runs of the UniSky simulator with random cloud geometry, the UniSky average, and the 1D weighted average radiances from libRadtran, for $\theta_z = 30^{\circ}$ and $c_f = 0.2$.

348 4.5. Validation against horizontal irradiation measurements

Yearly irradiation predicted from our model using MODIS data is validated against hor-349 izontal irradiation measurements from high-quality pyranometer data and is shown in fig. 350 6. The UK Met Office MIDAS dataset (Met Office, 2012) is used for UK locations and the 351 Baseline Surface Radiation Network (BSRN) for non-UK locations (BSRN, 2015). The con-352 vention in this paper is to use the three-letter BSRN station codes in upper case for BSRN 353 stations and an upper- and lower-case abbreviation for MIDAS stations. Camborne (Cam) 354 and Lerwick (Ler) are MIDAS stations that also supply data to BSRN; at the time of writing 355 the BSRN data were not available so the MIDAS data have been used. 356

MIDAS provides hourly pyranometer measurements of global horizontal irradiance (GHI) for approximately 100 sites in the UK. The MIDAS data has passed a quality control (QC) procedure run by the UK Met Office. Five MIDAS sites were selected on the basis of wide geographical coverage within the UK and a minimal amount of missing or bad data for 2013. Where missing hours do occur in the MIDAS data, these have been replaced by the mean irradiance from the corresponding hour in the same month.

BSRN provides minutely measurements of horizontal irradiance from sites globally. The 363 BSRN data also contains instances of missing records. Data gaps range from one minute to 364 several days. A QC procedure was applied to the BSRN data to fill in missing or suspect data 365 following the M7 method recommended by Roesch et al. (2011). The M7 method calculates 366 monthly 15-minute means from data where at least 3 minutes per 15-minute period exist 367 and are within the "physically possible" limit for GHI of $1.5S_0 \cos^{1.2} \theta_z + 100$ W m⁻². S_0 368 is the solar constant I_0 corrected for earth-sun distance. The monthly mean is only valid if 369 all 96 15-minute bins contain valid values. Only sites where all months of 2013 data were 370 available and passed the QC check were selected for the BSRN validation. The details of the 371 27 meteorological stations used in the validation are shown in the appendix. Solar irradiance 372 at BSRN sites is measured with a Kipp & Zonen CMP21 or CMP22 pyranometer with the 373 exception of Tamanrasset which uses the Eppley PSP, all of which are World Meteorological 374 Organisation (WMO) High Quality certified. 375

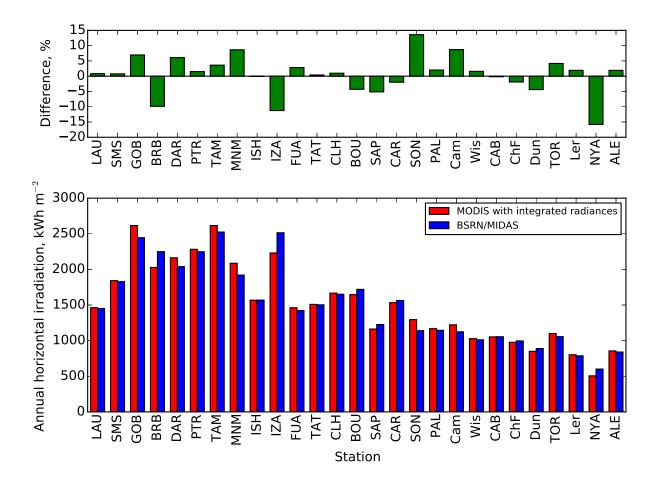


Figure 6: Validation of integrated radiance method using MODIS data against pyranometer measurements. For station names and locations please refer to Appendix.

The mean bias difference (MBD) between the annual irradiation derived from our 376 method and the pyranometer data is +0.56% and the root-mean-square difference (RMSD) 377 is +6.69%. Of the sites where our method deviates from the measured values by more than 378 10%, two (IZA and SON) are at mountaintop sites at altitudes 2373 m and 3109 m respec-379 tively. In these areas, the 1° resolution of the MODIS atmosphere data may not be large 380 enough to capture all of the micro-climatic effects in mountainous regions. As discussed by 381 Gueymard and Wilcox (2011), the spatial variation in irradiance measurements is highest in 382 coastal and mountainous areas. Clouds are particularly difficult to attribute as sometimes 383 the site location may be above the mean cloud height for the 8 day period whereas in reality 384

the station is not cloud-free for the entire 8 days. Furthermore if the cloud deck is below the station altitude, the albedo from the point of view of the pyranometer changes, and backscattering effects between the cloud layer and the atmosphere above the station can enhance the downwards radiation. It is unlikely that the MODIS albedo product includes these effects as it is calculated from clear sky scenes.

The other location with a greater than 10% absolute error, NYA, is at very high latitude 390 (78.9°N), where satellite retrievals from MODIS become less reliable. In addition, in such 391 a high-latitude site, solar declination can vary widely over the course of an 8-day period 392 in spring and autumn and as such the solar geometry used in our calculations may not 393 be representative. Interestingly, the other high latitude location, ALE in the far north of 394 Canada (82.5°N), shows a very good agreement with the model. This could be due to a 395 higher annual irradiation than NYA indicative of clearer conditions as the annual horizontal 396 irradiation at ALE is similar to that at Dun at 56.4°N. BRB, the fourth poorest site for 397 agreement with a 9.9% underestimation, suffers from a large amount of incomplete data in 398 the 2013 BSRN dataset which may result in a large error in the "measurement" value for 399 this site. BRB passes the QC test because all 96 15-minute bins are present for each month, 400 but for some months there are as little as 7 days of data present. 401

402 4.6. Results of the tilted irradiation and comparison with PVGIS

It is difficult to validate the tilted irradiation model on a global basis because there are few 403 comparable high-quality long term measurements of tilted irradiance available worldwide. 404 In section 4.7 we validate our results against data from one site. The optimal tilt angle 405 predicted by the integrated radiance model, and the irradiance predicted at this optimal 406 tilt, are compared with results from the online PVGIS solar resource estimation tool in fig. 407 7 (European Commission, 2012). PVGIS is a validated model that derives solar irradiance 408 from the Meteosat satellite cloud product and calculates tilted irradiance using the Muneer 409 model (Muneer, 1990). Additionally the PVGIS model reports GHI with a mean bias error 410 (MBE) of within $\pm 5\%$ for all but 4 BSRN and other surface irradiance measurement sites out 411 of 23 (Huld et al., 2012) whereas the Muneer (1990) tilt model gives a MBE of +5.3% and 412

root-mean-squared error (RMSE) of 9.6% for vertical, south-facing planes, with considerably
lower errors for 45° and 60° south-facing planes for the EU Joint Research Centre (JRC)
test site at Ispra, Italy. 13 of the 27 validation sites used in section 4.5 fall within the spatial
boundaries of PVGIS and have been compared in fig. 7.

The comparisons do not correspond to the same time period as the PVGIS database 417 uses data from the CM-SAF satellite products, namely Meteosat First Generation (MFG, 418 1998–2005) and Meteosat Second Generation (MSG, 2006–2011), and it is not stated which 419 particular BSRN station years are used to validate these datasets (Huld et al., 2012). Our 420 validation against BSRN and MIDAS ground stations uses 2013 data. The comparison with 421 PVGIS is not a validation of our model for this reason, but a sense-check against a widely-422 used tilted irradiance database. Nevertheless some systematic differences can be observed. 423 The top panel of fig. 7 shows that in the majority of locations our predicted annual optimal 424 tilt angle is steeper than in PVGIS, ranging from -1° at CAR and Cam to $+8^{\circ}$ at TOR. 425 Part of the differences may be due to, on average, higher GHI values predicted from our 426 model compared to PVGIS, suggesting that our model predicts a lower cloud fraction or 427 greater cloud transmission than PVGIS does in general. The effect of this is large at the 428 three low latitude sites of GOB, TAM and IZA where in each case our model predicts an 429 optimal tilt slightly steeper than the latitude location, showing the influence of the direct 430 beam and circumsolar diffuse components of solar radiation. For IZA it is interesting to note 431 that our model under-predicts GHI for the 2013 calendar year quite substantially compared 432 to the BSRN pyranometer data, whereas the PVGIS estimate is even lower (although not 433 validated against the same time period as previously mentioned). This, along with results 434 for SON reported by Huld et al. (2012) and our data shown in fig. 6, shows the difficulties 435 that both models experience in mountainous areas. 436

The middle and bottom panels of fig. 7 shows that in every location there is a more positive difference in the irradiation at optimal tilt than the GHI between our model and PVGIS. This effect is seen even at CAR and Cam indicating a difference between the Muneer tilt model used in PVGIS and the integrated radiance method. This is emphasised by the

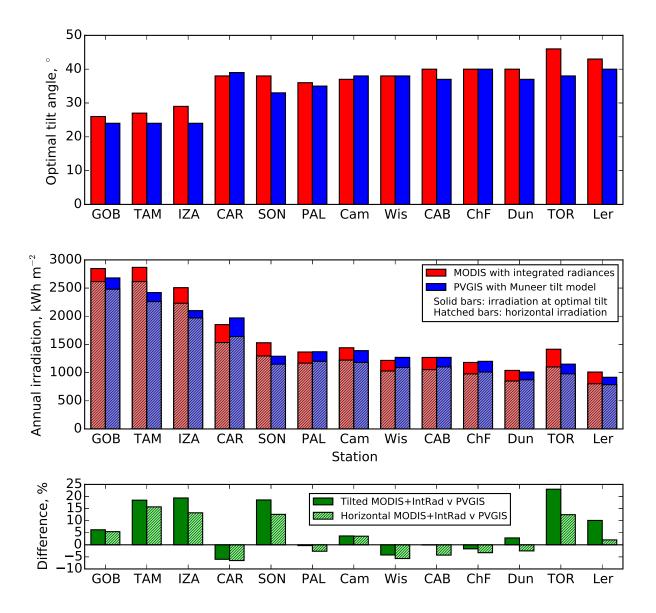


Figure 7: Comparison of integrated radiance method using MODIS data against results from PVGIS for optimal tilt angle and yearly irradiation at optimal tilt. The top figure compares optimal tilt angles between the two models, the middle figure shows irradiation at optimal tilt (solid bars) and GHI (pale hatched bars), and the bottom figure shows the differences between the two models for irradiation at optimal tilt (solid bars) and for GHI (pale hatched bars). For station names and locations please refer to table 2 in the Appendix.

⁴⁴¹ Dun site where PVGIS predicts a higher annual GHI total but lower irradiation at optimal
 ⁴⁴² tilt.

Tilt	Integrated radiance model	Eppley PSP measurements	Difference
	$(\rm kWh~m^{-2}~yr^{-1})$	$(\rm kWh~m^{-2}~yr^{-1})$	
Horizontal	1760.0	1684.2	+4.5%
$40^{\circ}\mathrm{S}$	2120.4	2010.0	+5.5%
$90^{\circ}S$	1479.3	1402.9	+5.4%
$90^{\circ}\mathrm{E}$	1085.4	1138.6	-4.7%
$90^{\circ}W$	976.7	922.2	+5.9%
$90^{\circ}N$	420.5	479.3	-12.3%

 Table 1: Validation of tilted irradiation from the integrated radiance model against ground measurements

 from NREL.

4.7. Validation against tilted irradiation measurements from the National Renewable Energy Laboratory Baseline Measurement System

The NREL Solar Radiation Research Laboratoty (SRRL) (Andreas and Stoffel, 1981) produces horizontal and tilted irradiation datasets which are available from their website at http://www.nrel.gov/midc/srrl_bms/. Tilted irradiation is measured at 40°S and at 90°S, W, E and N, using Eppley PSP pyranometers. Horizontal radiation is measured with a number of different pyranometer models. For consistency, we use the ventilated, corrected Eppley PSP horizontal irradiation measurement. The NREL site is located in Golden, Colorado, at 39.74°N, 105.18°W at an altitude of 1829 m.

The validation against the NREL station measurements is shown in table 1. The horizon-452 tal irradiation estimate from the integrated radiance model is 4.5% higher than the NREL 453 measurement using the Eppley PSP. For the 40° and 90° south-facing tilts, the relative error 454 is slightly higher but does not grow appreciably. The model captures some of the diurnal 455 variation in weather conditions at this site, as seen by the differences between east- and west-456 facing tilt estimates, however underestimates the magnitude of the diurnal variation with 457 an overestimate for the west-facing pyranometer and an underestimate for the east-facing 458 pyranometer. This may be due to the timing of the satellite overpasses, approximately 90 450

⁴⁶⁰ minutes before and after local solar noon on average, whereas east- and west-facing wall irra-⁴⁶¹ diances will be at their maximum earlier and later in the day, respectively. The north-facing ⁴⁶² estimate is considerably less good than for the other orientations, however, it is not likely ⁴⁶³ that serious consideration would be given to tilting panels poleward given the low overall ⁴⁶⁴ yield estimate.

465 5. Discussion

The integrated radiance method is possible to evaluate globally as the satellite re-466 trieval data from MODIS has global coverage. The method is applicable to any dataset 467 in which aerosol parameters, ozone, water vapour, cloud liquid water path, cloud ice wa-468 ter path and cloud fraction are available. The necessary inputs to the model also ex-469 ist in meteorological reanalysis and climate models. The aerosol parameters are avail-470 able in MODIS but often suffer from large gaps in data, so in our model they are ob-471 tained from the GLOMAP global aerosol model. Aerosol reanalysis datasets such as MACC 472 (http://apps.ecmwf.int/datasets/data/macc-reanalysis), which assimilates observa-473 tions and forecasts into a consistent gridded dataset, can be used. Thus, the integrated 474 radiance model can be used for determining a realistic optimal tilt for an arbitrary climatic 475 condition, and solar energy resource calculated on this basis. 476

It should be mentioned that MODIS satellite retrievals are not always available or are 477 of low quality. The limit of MODIS orbital tracks are at 82° N/S, and for latitudes greater 478 than 77° N/S the satellite tracks overlap. Successive retrievals may not be independent and 479 observational nadir angles may be higher towards the poles as the satellites do not overpass 480 above/below 82° N/S (Hubanks et al., 2008). On the other hand, these regions are currently 481 unimportant for solar energy generation. A more critical issue occurs when albedo values 482 are not reported over a 16-day period. As an albedo retrieval requires a cloudless scene 483 when the satellite overpasses, it is possible that there are no clear overpasses during a 16-484 day period for some parts of the world. In these cases where no albedo measurement exists 485 for a $0.05^{\circ} \times 0.05^{\circ}$ cell, the mean value from the 21×21 cells surrounding the grid square 486 $(1.05^{\circ} \times 1.05^{\circ})$ is used. In very rare cases where no 1.05° mean exists, the spectral albedo is 487

taken from the global $0.17^{\circ} \times 0.17^{\circ}$ map of 20 different surface types in the IGBP land cover dataset (Belward and Loveland, 1996).

In many regions, clouds are the largest input uncertainty in our model because the ra-490 diative properties of aerosols, water vapour and ozone are less significant when the entire 491 solar spectrum is considered. The direct and diffuse radiation fields are spectrally dependent 492 (Forster and Shine, 1995) and although a spectral calculation is performed and then inte-493 grated over all solar wavelengths to obtain broadband irradiance, the spectrally-dependent 494 irradiance was not considered. When applied to assessing the energy output of PV technolo-495 gies, spectral considerations have shown to be important and this could affect the optimal 496 PV tilt angle. 497

It is possible to improve the spatial and temporal resolution of the results obtained. 498 MODIS Level 3 8-day mean data has been used in this model for atmosphere and albedo. 499 Level 3 data is available daily, the use of which may improve accuracy at the expense of 500 an 8-fold increase in computational time. Greater accuracy may be obtained by using the 501 Level 2 satellite swath data, which has a nadir resolution of 1 km and will usually overpass a 502 location at least once per day, although there are small gaps in the satellite overpass tracks 503 near the equator that are not covered every day by the Level 2 or Level 3 daily data. To 504 use higher resolution data will require many more RT simulations per location per year. 505 and will need the use of pre-calculated lookup tables or a polynomial regression fit to allow 506 swifter calculation of the radiance fields. This is an area for future investigation. It is shown 507 however that for locations at low and moderate altitude and latitude, sufficient agreement 508 for horizontal and equator-facing tilts for yearly irradiation is obtained with the 8-day data. 509

510 6. Conclusion

This paper presents a computational method to calculate the all-sky irradiance on a plane of arbitrary alignment, which is globally applicable. The optimal tilt angle at a particular location is dependent on the meteorological conditions and cannot be related to a single parameter. A radiative transfer simulation is run to produce a ground-level radiance field, which is numerically integrated over the tilt angle of interest. The required inputs of cloud

liquid water path, cloud ice water path, cloud fraction, temperature, ozone, water vapour and 516 surface albedo are standard variables from satellite observations, meteorological reanalysis 517 or climate model data. We use MODIS Terra and Aqua satellite data for clouds, ozone, 518 water vapour and albedo. Aerosols are provided by the GLOMAP model but any scheme 519 that provides the aerosol phase function, optical depth and single scattering albedo can be 520 used. The horizontal irradiation predicted by our model is compared to contemporaneous 521 pyranometer data from MIDAS and BSRN and agrees to within $\pm 10\%$ for all but 3 sites 522 out of 27. The MBD between our method and BSRN/MIDAS across all sites is +0.56% and 523 RMSD is 6.69% for horizontal irradiance. 524

When validated against the NREL tilted irradiance dataset our model predicts the an-525 nual irradiation within $\pm 6\%$ for all orientations except 90°N. The magnitude of error for 526 tilted irradiance on 40° and 90° south-facing planes is similar to that for horizontal irradi-527 ance. The diurnal variation in prevaling weather conditions is partially captured by analysis 528 of the difference between east- and west-facing estimates of annual irradiation compared to 529 pyranomter measurements, although underestimated. Due to a lack of high-quality tilted 530 irradiance measurement stations, it is not possible to validate against tilted irradiance mea-531 surements globally, but the validated PVGIS model is used as a comparison. The main 532 differences between our model and the Muneer (1990) tilt model used in PVGIS are the 533 steeper optimal tilt angles and more positive relative differences between tilted irradiation 534 and horizontal irradiation. In mid-latitude and low-to-moderate altitude sites, where PVGIS 535 has been validated, the models produce similar results. In order to draw more robust con-536 clusions about the optimal tilt angle from the model, a larger network of tilted irradiance 537 measurements would be required. However, the limited model comparisons and validations 538 show that the model produces sensible results and could be applied where ground measure-539 ments of tilted irradiance are not available. Further work in this area includes accounting 540 for horizon shading, and producing a global map of optimal annual tilt. 541

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557 Appendix

Code	Station name	Country	Lat.	Lon.	Alt. (m)	Network
LAU	Lauder	New Zealand	45.045°S	169.689°E	350	BSRN
SMS	São Martinho	Brazil	$29.443^{\circ}\mathrm{S}$	$53.823^{\circ}W$	489	BSRN
GOB	Gobabeb	Namibia	$23.561^\circ\mathrm{S}$	$15.042^{\circ}\mathrm{E}$	407	BSRN
BRB	Brasilia	Brazil	$15.601^\circ\mathrm{S}$	$47.713^{\circ}W$	1023	BSRN
DAR	Darwin	Australia	$12.420^{\circ}\mathrm{S}$	$130.891^{\circ}\mathrm{E}$	350	BSRN
PTR	Petrolina	Brazil	$9.068^{\circ}\mathrm{S}$	$40.319^{\circ}W$	387	BSRN
TAM	Tamanrasset	Algeria	$22.780^{\circ}N$	$5.510^{\circ}\mathrm{E}$	1366	BSRN
MNM	Minamitorishima	Japan	$24.288^{\circ}N$	$153.983^{\circ}\mathrm{E}$	7	BSRN
ISH	Ishigakijima	Japan	24.337°N	$124.163^{\circ}\mathrm{E}$	6	BSRN
IZA	Izaña	Tenerife	$28.309^{\circ}N$	$16.499^{\circ}W$	2373	BSRN
FUA	Fukuoka	Japan	33.582°N	$130.375^{\circ}\mathrm{E}$	3	BSRN
TAT	Tateno	Japan	$36.050^\circ\mathrm{N}$	140.133°E	25	BSRN
CLH	Chesapeake Light	USA	$36.905^{\circ}\mathrm{N}$	$75.713^{\circ}W$	37	BSRN
BOU	Boulder	USA	$40.050^{\circ}\mathrm{N}$	$105.007^{\circ}W$	1577	BSRN
SAP	Sapporo	Japan	$43.060^{\circ}\mathrm{N}$	141.329°E	17	BSRN
CAR	Carpentras	France	44.083°N	$5.059^{\circ}\mathrm{E}$	100	BSRN
SON	Sonnblick	Austria	$47.054^{\circ}\mathrm{N}$	$12.958^{\circ}\mathrm{E}$	3109	BSRN
PAL	Palaiseau	France	48.713°N	$2.208^{\circ}\mathrm{E}$	156	BSRN
Cam	Camborne	UK	$50.218^{\circ}\mathrm{N}$	$5.327^{\circ}W$	87	MIDAS
Wis	Wisley	UK	$51.310^{\circ}\mathrm{N}$	$0.475^{\circ}W$	38	MIDAS
CAB	Cabauw	Netherlands	$51.971^{\circ}\mathrm{N}$	$4.927^{\circ}\mathrm{E}$	0	BSRN
ChF	Church Fenton	UK	$53.836^{\circ}\mathrm{N}$	$1.197^{\circ}W$	8	MIDAS
Dun	Dunstaffnage	UK	$56.451^{\circ}\mathrm{N}$	$5.439^{\circ}W$	3	MIDAS
TOR	Toravere	Estonia	$58.254^{\circ}\mathrm{N}$	$26.462^{\circ}\mathrm{E}$	70	BSRN
Ler	Lerwick	UK	$60.140^{\circ}\mathrm{N}$	$1.183^{\circ}W$	82	MIDAS
NYA	Ny-Ålesund	Svalbard	$78.925^{\circ}\mathrm{N}$	$11.930^{\circ}\mathrm{E}$	11	BSRN
ALE	Alert	Canada	$82.490^{\circ}N$	$62.420^{\circ}W$	127	BSRN

Table 2: List of BSRN and UKMO-MIDAS stations used in the validation and comparison.

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