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# Numerical study of neutron beam divergence in a beam-fusion scenario employing laser driven ions

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### Abstract

The most established route to create a laser-based neutron source is by employing laser accelerated, low atomic number ions in fusion reactions. In addition to benefiting from the high reaction cross-sections at moderate energies of the projectile ions, the anisotropy in the neutron emission is another important feature of beam-fusion reactions. Using a simple numerical model based on neutron generation in a pitcher-catcher scenario, anisotropy in the neutron emission was studied for the deuterium-deuterium fusion reaction. Simulation results are consistent with the narrow-divergence ( $\sim 70^{\circ}$  full width at half maximum) neutron beam recently obtained from an experiment employing multi-MeV deuteron beams of narrow divergence (upto 30° FWHM depending on the ion energy) accelerated by a sub-petawatt laser pulse from thin deuterated plastic foils via the Target Normal Sheath Acceleration mechanism. By varying the input ion beam parameters, simulations show that a further improvement in the neutron beam directionality (i.e. reduction in the beam divergence) can be obtained by increasing the projectile ion beam temperature and cut-off energy, as expected from the interactions with higher power lasers at upcoming facilities.

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Keywords: laser, neutron, beam fusion

### 1 1. Introduction

Fast neutron sources driven by high-power lasers 2 have gained substantial interest over the last decades for 3 a range of potential applications in medicine [1], secu-4 rity [2, 3], material science [4] and high energy density 5 physics research [5]. Furthermore, deploying compact 6 moderators closely coupled to laser-driven fast neutrons 7 sources would allow the development of intense sources 8 of thermal and epithermal neutrons, which would ex-9 tend the range of applicability of laser-based sources. 10 With the rapid progress in laser technology, aiming to-11 wards developing higher repetition rate lasers of higher 12 powers, laser-driven neutron sources can, in principle, 13 complement the research activities currently pursued at 14

\*Corresponding author. Email address: s.kar@qub.ac.uk conventional accelerator-driven spallation sources. Although these large scale facilities produce substantially higher fast neutron fluxes, a key interest for laser-driven neutron sources lies in the neutron burst duration, which is substantially shorter than that produced at spallation facilities.

With the current laser systems, neutron yields up to of the order of  $10^{10}$  neutrons/shot have been shown experimentally ([6, 7] and references therein), by employing laser driven ions to generate neutrons from secondary catcher targets via beam-fusion reactions. In addition to the advantage of the ultra-short pulse duration, directionality/anisotropicity in the neutron emission is another important characteristic resulting from the beam-fusion reactions. The total neutron yield from a fusion reaction scales with the product of fusing ion densities and cross-section  $\sigma$ , which, for the most common reactions, reaches high values for centre-of-

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mass energy in the MeV-10s of MeV range [8]. In a 33 pitcher-catcher scenario, where neutrons are produced 34 by bombarding the laser-driven ions on a suitable con-35 verter target, anisotropy arises from the nuclear reac-36 tion kinematics, which strongly depends on the atomic 37 mass of the fusing nuclei and velocity of the projectile 38 ions [6]. In addition, the strong angular dependence 39 of the differential cross-section for light nuclei reac-40 tions helps producing neutron fluxes strongly peaked 41 along the incident ion-beam direction, even while us-42 ing moderate energy (10s of MeV) ions as acceler-43 ated at currently available laser intensities [9]. In this 44 context, fusion reactions based on low atomic mass 45 nuclei, such as <sup>7</sup>Li(p,n)<sup>7</sup>Be, <sup>9</sup>Be(p,n)<sup>9</sup>B, <sup>13</sup>C(p,n)<sup>13</sup>N, d(d,n)<sup>3</sup>He, T(d,n)<sup>4</sup>He, <sup>7</sup>Li(d,xn), <sup>7</sup>Be(d,xn), are partic-47 ularly relevant, which would not only allow obtaining 48 higher neutron yield, but higher peak flux by producing 49 a narrow cone beam of neutrons. A highly beamed neu-50 tron flux would be extremely helpful towards improving 51 transport capabilities as well as efficient moderation of 52 the neutrons to thermal and epithermal energies by us-53 ing compact, closely-coupled, directional moderators. 54

Anisotropic emission of the neutron beam is start-55 ing to be realized in experiments. In addition to 56 the anisotropicity intrinsic to the beam-fusion, as dis-57 cussed above, the neutron beam divergence from a typ-58 ical laser-driven pitcher-catcher source also depends 59 strongly on the divergence of the projectile ions - the fi-60 nal neutron beam divergence from the catcher will be a 61 convolution of the divergence of the input ion beam and 62 the neutron beam divergence expected for a collimated 63 beam of ions. 64

In this paper we show a simple model for simu-65 lating the neutron production from light nuclei reac-66 tions in a pitcher-catcher scenario, and to study the 67 effect of ion beam parameters (divergence and spec-68 trum) on the neutron generation. The neutron beam 103 69 divergence estimated by our model from  $d(d,n)^3$ He re-70 action in a beam-fusion scenario, while using laser-71 driven deuterium beam produced via the Target Normal 106 72 Sheath Acceleration (TNSA) mechanism[9], compares 107 73 well with the data obtained from a recent experiment 108 74 [6]. A systematic study show that the neutron beam di-75 vergence can be reduced significantly (to a few tens of 76 77 degrees) by increasing the input ion beam temperature, 111 which, according to the current understanding of the 112 78 TNSA mechanism, is achievable using the intense lasers 113 79 that will be available at the upcoming facilities[10, 11]. 80

# 2. Simulation design and method

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Alternative to the usual Monte-Carlo approach [12, 13] to simulate neutron generation in a beam-fusion scenario, the model described in this paper (as discussed below) takes advantage of the tabulated angularlyresolved neutron yield, that can be found in the literature, obtained for a mono-energetic, pencil beam of ions impinging onto a catcher at normal incidence. The main interaction that is taken into account in our simple model is the effect of a multi-energy, divergent beam of ions, as typically produced by the TNSA mechanism, towards the angular distribution of emitted neutrons from a secondary catcher target. The schematic of the setup used in our model is shown in Fig. 1.



Figure 1: (a) Schematic of the neutron generation process in the pitcher-catcher scheme. An ion beam is generated by the interaction of the laser with the target (pitcher), which then reaches the secondary converter (catcher), leading to the neutron emission. (b) and (c) depict the grids representing the catcher and the detector, respectively.

The input for the projectile ion beam in our model is the angularly-resolved ion spectra. This information can either be obtained numerically, by performing multi-dimensional PIC simulations of the laser-foil interaction, or experimentally, by using for example angularly distributed high-resolution Thomson Parabola Spectrometers (TPS) [14]. The angularly resolved ion spectra can be represented by a function  $\frac{d^2 N_{ion}}{dE \, d\Omega}(E, \theta, \varphi)$ , where *E* is the ion energy,  $(\theta, \varphi)$  are the angles defining the direction of a given beamlet of ion, and  $\Omega$  stands for solid angle. For simplicity, one may assume the ion beam produced by the laser-foil interaction to be cylindrically symmetrical about  $\theta$ .

The catcher in the model was designed as a two dimensional matrix ( $n_{c,x} \times n_{c,y}$  cells), where the grid size  $(dx_c \times dy_c)$  can be chosen depending on the desired resolution and accuracy, being  $dx_c = dy_c = 200 \,\mu\text{m}$  the resolution for the simulations here shown. The spectrum of ions arriving at each grid point on the catcher  $(dN_{ion,(x,y)}/dE)$  is calculated from the input ion spectrum

to the code (as mentioned above) for a given pitcher-to-115 catcher distance (l). In order to obtain the neutron flux 116 distribution across a plane parallel to the catcher, the 117 detector in the code was modelled as a two dimensional 118 array of  $n_{d,x} \times n_{d,y}$  cells of size  $dx_d \times dy_d$ . This detec-119 tor configuration mimics the response of CR39 nuclear 120 track detectors typically used in neutron generation ex-121 periments [6?, 15], allowing for a direct comparison 122 between the simulations and the experimental data. 123

Neutron generation from each grid point of the 124 catcher was calculated by using the tabulated data for 125 the angularly-resolved neutron yield, that can either be 126 found in the literature, or be obtained by running Monte 127 Carlo simulations [12, 13] for different ion energies. In 128 this paper we used the tabulated data for  $d(d,n)^{3}$ He re-129 action provided by Davis et al. [12], which was one 130 of the main reactions producing neutron in the experi-131 ment reported in [6]. The  $d(d,n)^3$ He reaction is also an 132 efficient fusion reaction for moderate-energy deuterons, 133 which is suitable for studying the effect of the input ion 134 beam spectrum and divergence on the neutron beam di-135 vergence. The tabulated neutron yield per incident ion, 136 given in Ref. [12], along different angles of neutron 137 emission and for different projectile ion energies were 138 interpolated to obtain a function  $Y_n(E, \theta')$ , where  $\theta'$  is 139 the neutron emission angle with respect to the incident 140 ion beam. Using this function, the neutron flux at a 141 given pixel of the detector  $(F_{n,(x_d,y_d)} = N_{n,(x_d,y_d)}/dx_d dy_d)$ 142 is calculated as the sum of the fluxes reaching that pixel, 143 generated at each point on the catcher. This can be ex-14 pressed mathematically as 145

$$N_{n,(x_d,y_d)} = \sum_{(x_c,y_c)} \sum_E Y_n(E,\theta'') \cdot N_{ion,(x_c,y_c)}(E)$$

where,  $\theta'' = \tan^{-1} \left( \sqrt{(x_d - x_c)^2 + (y_d - y_c)^2} / L \right)$  and *L* is 146 the catcher-to-detector distance. 147

#### 3. Results 148

In order to study the beamed neutron emission ob-149 served in our experiment [6] employing the petawatt 185 150 arm of the VULCAN laser at Rutherford Appleton Lab-186 151 oratory (RAL), STFC, UK[16], we used the experimen-187 152 tally measured deuteron spectrum as the input to our 188 153 model. The ion beams in the experiment were pro-154 duced by irradiating 10  $\mu$ m-thick deuterated plastic foils 155 with a p-polarised laser pulse of  $\sim 200 \,\text{J}$  energy and 156 ~ 750 fs duration, focussed down to a spot of ~  $6 \,\mu m$  192 157 (FWHM) on the target, reaching a peak intensity in ex-158 cess of  $10^{20}$  W cm<sup>-2</sup>. The ion beam spectrum was di-159 agnosed along different emission angles (-8°, 0°, 21° 160



Figure 2: (a) A typical raw data obtained by a TPS diagnosing ion spectrum along the target normal direction. (b) Angularly resolved deuteron spectrum reconstructed from the data obtained by four TPS measurements along different angles (as shown by the dashed line) with respect to the target normal direction. (c) Spatial profiles of deuteron beam for different energies at the catcher plane.

and  $32^{\circ}$ ) with respect to the target normal by employing Thomson Parabola Spectrometers (TPS)[14]. Due to the limitation of TPS in retrieving the spectrum of overlapping species, a differential filtering technique [17] was implemented to discriminate the deuterium ions from the overlapping species with equal charge-to-mass ratio, such as  $C^{6+}$  and  $O^{8+}$  originated from the target and hydrocarbon contaminant layers. A typical raw data obtained along the target normal direction is shown in Fig. 2(a). A comparison between on-axis proton and deuteron spectra obtained from the TPS data is shown in Ref. [6]. The deuteron spectra obtained from the different TPS were used to reconstruct the full beam profile, as shown in Fig. 2(b), while assuming an axissymmetrical beam profile. The data shows a divergent (~  $30^{\circ}$  FWHM, ~  $60^{\circ}$  full cone) beam of deuterons with an exponential spectrum, with the highest energies produced along the target normal direction with a narrow (~  $15^{\circ}$  full cone) beam divergence, as expected from the TNSA mechanism for such laser and target parameters [18].

The angularly-resolved deuteron spectra shown in Fig. 2(c) was used in our code to simulate the neutron generation in the catcher placed at a distance of  $l = 5 \,\mathrm{mm}$  from the ion source (which represents the point of laser interaction with the pitcher target). The flux distribution of the deuterons of different energies at the front surface of the catcher are shown in Fig. 2(c), which was obtained by using the beam profile shown in Fig. 2(b).

Despite of the moderate energies of the ions and the broad emission angle produced in the experiment, the simulation shows a directional beam-like emission of neutrons from the catcher target, as shown in Fig. 3 (showing neutron flux distribution across the detector

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plane placed at a distance L = 15 mm from the catcher), 196 with a Full Width at Half Maximum (FWHM) diver-197 gence of  $\sim 62^{\circ}$  and maximum flux along the ion beam 198 axis. The simulated neutron beam profile is similar to 199 that obtained from the experiment (FWHM of  $(70 \pm 10)^{\circ}$ 200 [6]). Since the simulated neutron beam profile was ob-201 tained by considering only the  $d(d,n)^3$ He reaction, the 202 residual difference between the simulated and exper-203 imental neutron beam profile is most likely due to a 204 range of additional nuclear reactions taking place in the 205 catcher in the latter case. As discussed in Ref. [6], due 206 to the higher flux and higher energy protons produced 207 from the pitcher target (as can be seen in Fig. 2(a)), the 208 proton-induced deuteron breakup reaction  $(d(p,n+p)^{1}H)$ 209 contributes significantly towards the total neutron yield. 210 Due to the reaction kinematics, this nuclear reaction 211 is expected to produce a narrow neutron beam diver-212 gence, similar to that obtained for the  $d(d,n)^3$ He reac-213 tion. However, a detailed simulation for the  $d(p,n+p)^{1}H$ 214 case could not be carried out due to the insufficient re-215 action cross-section available in the literature. 216

In order to study the effect of the projectile ion beam parameters on the neutron beam divergence, we car-219 ried out a set of simulations by varying the input spectrum of the ions, as expected to be produced by TNSA mechanism at different laser intensities. The ion temperature and the cut-off ion energy in the TNSA mechanism scale with the temperature of the hot electrons



Figure 3: Simulated neutron beam reaching a flat detector in front of the catcher. Inset shows the lineout of the neutron beam profile across 245 the detector, which also represents the emission angle of neutrons with 246 respect to the ion beam axis. The divergence of the neutron beam (FWHM) is  $\sim 62^{\circ}$ .

produced by the interaction, which broadly scales as  $\sqrt{I_L \lambda^2}$  [9, 19, 20, 21], where  $I_L$  and  $\lambda$  stand, respectively, for the intensity and the wavelength of the incident laser. The divergence of the ions produced by the TNSA mechanism also varies within the beam depending on its energy [18] - ions with higher energy are emitted with a lower divergence. Assuming a flat-top flux profile within the ion beam divergence, and the following divergence profile as a function of ion energy (as reported for ~ps lasers in Ref. [18], which closely matches with the observed divergence shown in Fig. 2(b)),

$$\theta_D(E, E_{max}) = \begin{cases} 62 & E < E_{max}/2 \\ 107.4 - 90.9 \cdot \frac{E}{E_{max}} & E \ge E_{max}/2 \end{cases},$$
(1)

we modelled an input TNSA beam profile for our simulations as a function of laser intensity, as given by

$$\frac{d^2 N_{ion}}{dE \, d\Omega} = \left. \frac{dN_{ion}}{dE} \right|_{\substack{E < E_{max} \\ \theta < \theta_{\Omega}}} \propto \exp\left(-\frac{E}{k_B T(I_L)}\right) \tag{2}$$

A set of simulations were carried out by varying the ion beam temperature  $k_B T(I_L)$ . The cut-off energy for the deuterons as a function of laser intensities was assumed as  $E_{max}(I_L) \propto 10^{-9} \sqrt{I_L}$  MeV, where the proportionality constant was calculated using the maximum deuteron energy obtained in our experiment, shown in Fig. 2(b).

The FWHM divergence of the neutron beam obtained from the simulations is shown in Fig. 4. One can see how the neutron beam divergence reduces significantly with an increase in the ion beam temperature. While a nearly isotropic emission for low ion temperatures is produced, the neutron beam divergence can be reduced below  $50^{\circ}$  using higher power lasers than that used in our experiment. Intense lasers will produce ions at higher energies, which will provide two-fold enhancement to the on-axis neutron flux - (1) neutron yield per incident ion will increase significantly due to their deeper penetration into the catcher, (2) higher anisotropicity due to differential cross-section and kinematics (see Eq. 2 in Ref. [6]). An alternative approach for increasing the flux and energy of ions other than protons, which are preferentially accelerated by the TNSA mechanism, would be to use some special technique to eliminate the hydrogen contamination layer at the rear side of the pitcher target, such as depositing a layer of heavy water contamination for enhancing the deuteron acceleration [22].

The rate of decrease in the neutron beam divergence slows down towards the higher temperatures, as visible in Fig. 4. The nearly constant divergence of  $\sim 30^{\circ}$  obtained for the high ion temperatures is due to the, albeit

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Figure 4: Neutron beam divergence (FWHM) as a function of the 288 ion beam temperature obtained from our simulations. The blue point 289 shows the beam divergence obtained for the  $d(d,n)^3$ He reaction using the deuteron beam profile obtained from our experiment discussed 291 above.

small, intrinsic divergence ( $\sim 15^{\circ}$ ) of the highest energy 296 248 ions produced by the TNSA mechanism. This limita-297 249 298 tion in the neutron beam divergence can be easily elim-250 299 inated by focussing the ion beams on the catcher, for 251 300 example by using one of the several schemes reported 301 252 302 in literature, such as permanent/pulsed magnetic focus-253 ing devices [23, 24, 25], laser-driven micro-lens[26], 254 304 hemi-spherical targets [27], shaped targets [28] etc. Us-255 305 ing a focussed beam of ions with narrow energy band 306 256 307 can also help reducing the pulse duration of emitted fast 257 308 neutrons, as recently reported by Higginson et al. [29]. 258 309

#### 4. Conclusions 259

We presented results obtained from a numerical 260 model simulating the neutron beam generation by laser-261 320 driven ions in a pitcher-catcher scenario. Simulation re-321 262 sults are broadly consistent with the neutron beam pro-263 file observed in the experiment while using the experi-264 mentally measured ion beam profile in the simulation. 325 265 By varying the ion beam parameters, simulations pre-326 266 dict improvement in the neutron beam divergence with 267 an increase in the ion beam temperature and cut-off en-268 329 ergy, as expected from the TNSA mechanism at higher 269 330 270 laser intensities. Further experimental measurements 331 with improved ion beam parameters would be required 271 to benchmark the simulated trend for neutron beam di-272 vergence. 273

# 5. Acknowledgements

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