



RESEARCH ARTICLE

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Key Points:

- CO₂ efflux data show no pattern with latitude
- Flow intensity is a primary control on CO₂ efflux and pCO₂ a secondary control
- Water surface appearance has potential as a proxy for flow intensity aiding rapid upscaling

Supporting Information:

- Supporting Information S1

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Hydraulics are a first-order control on CO₂ efflux from fluvial systems

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Abstract Evasion of carbon dioxide (CO₂) from fluvial systems is now recognized as a significant component of the global carbon cycle. However, the magnitude of, and controls on, this flux remains uncertain, and improved understanding of both is required to refine global estimates of fluvial CO₂ efflux. CO₂ efflux data show no pattern with latitude suggesting that catchment biological productivity is not a primary control and that an alternative explanation for intersite variability is required. It has been suggested that increased flow velocity and turbulence enhance CO₂ efflux, but this is not confirmed. Here using contemporaneous measurements of efflux (range: 0.07–107 μmol CO₂ m⁻² s⁻¹), flow hydraulics (mean velocity range: 0.03–1.39 m s⁻¹), and pCO₂ (range: 174–10712 μatm) at six sites, we find that flow intensity is a primary control on efflux across two climatically different locations (where pH is not a limiting factor) and that the relationship is refined by incorporating the partial pressure of CO₂ (pCO₂) of the water. A remaining challenge is how to upscale from point to reach or river basin level. Remote imaging or river surface may be worth exploring if subjectivity in interpreting surface state can be overcome.

1. Introduction

Fluvial systems are often oversaturated with carbon dioxide (CO₂) and thus have the capacity to degas CO₂ to the atmosphere [Butman and Raymond, 2011; Melack, 2011; Billett et al., 2006]. Such evasion of CO₂ is now recognized to be a significant component of the global carbon cycle, estimated at a rate of 1.8 ± 0.25 Pg of carbon per year [Raymond et al., 2013], and its omission from carbon budget calculations may account for some of the imbalance in global estimates of carbon reservoir size and rate of transfer [Richey et al., 2002; Billett et al., 2006; Aufdenkampe et al., 2011]. While efflux estimates are becoming more precise, and a significant amount of carbon is known to be reprocessed within fluvial systems in a series of transformations and losses [Cole et al., 2007; Tranvik et al., 2009], the specific controls on CO₂ efflux and its exact magnitude remain poorly understood and quantified [Zappa et al., 2007; Alin et al., 2011; Butman and Raymond, 2011; Rasera et al., 2013] and fluvial CO₂ evasion may still be underestimated [Alin et al., 2011; Raymond et al., 2013] or overestimated [Hunt et al., 2011; Abril et al., 2015]. As such we need to better quantify and understand the controls on aquatic CO₂ degassing, particularly in systems, such as rivers and lower order streams, for which data remain sparse [Butman and Raymond, 2011; Melack, 2011; Wallin et al., 2011].

Published CO₂ efflux data show similar means and ranges from rivers across a wide latitudinal range (Figure 1 and supporting information Figure S1). This contradicts expectation of intersite variability in CO₂ efflux in response to drivers of the fluvial CO_{2(aq)} pool size, for example, soil type, geology, temperature, and river water pH (Table 1) [Rebsdorf et al., 1991; Aufdenkampe et al., 2011; Lauerwald et al., 2013]. Further, where moisture is not a limiting factor, catchment biological productivity is greater in warmer environments [Lauerwald et al., 2013; Maberly et al., 2013], and greater productivity in a catchment has been linked to increased riverine CO₂ concentrations and CO₂ efflux [Maberly et al., 2013]. Thus, in the tropics and equatorial regions CO₂ efflux from fluvial systems may be expected to be greater than at higher latitudes. However, no consistent increase in CO₂ efflux rate with decreasing latitude is observed (Figure 1), suggesting that net ecosystem productivity [e.g., Crammer et al., 1999] is not a primary control on CO₂ efflux.

Studies of the controls on oxygen aeration [e.g., Moog and Jirka, 1998; Palumbo and Brown, 2013] have shown how a range of hydraulic factors, including velocity, depth, and channel slope, can be used to produce statistical equations, which can be used to calculate the capacity for fluvial systems to absorb gas from the

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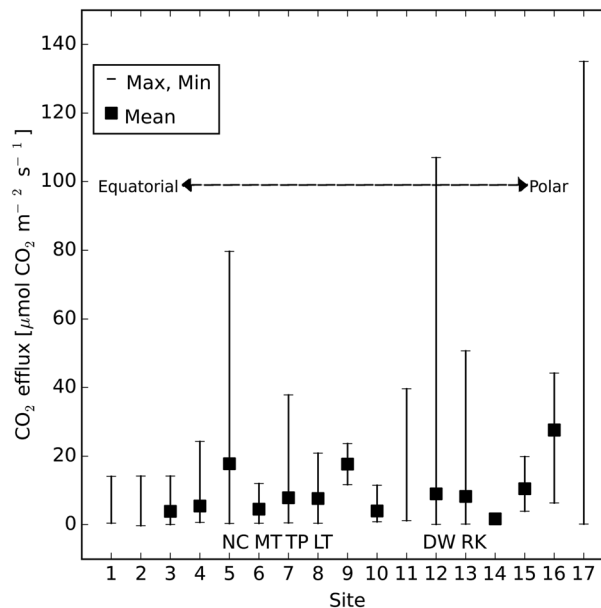


Figure 1. Global CO₂ flux rates, obtained by direct measurement from flowing water, displaying maximum, minimum, and mean CO₂ efflux values. Data sources and site references are in Table 1. Sites are ordered by latitude. Site locations shown in Figure S1.

and so greater gas efflux [Jonsson *et al.*, 2008]. In the ocean and lakes, wind drag on the water surface creates surface waves [Liss and Merlivat, 1986; Wanninkhof, 1992; Bock *et al.*, 1999; Hofmann *et al.*, 2008] and so enhances diffusion and increases gas fluxes. Wind plays the same roles in rivers as in the ocean and lakes, but this effect is spatially and temporally restricted. In estuaries and large rivers, wind can be the dominant physical control on gas exchange, but upstream in smaller channels, such as mainly measured here, stream characteristics which control the hydraulic properties of the flow are more significant [Alin *et al.*, 2011]. The interaction of downslope flow of water and channel roughness generates turbulence within the water column and energy dissipation in the form of surface waves when the flow reaches a critical state [Gordon *et al.*, 2004] disrupting the surface boundary layer. It has been observed that high turbulent energy during high river flow enhances fluvial gas evasion [Hope *et al.*, 2001; Billett *et al.*, 2006; Billett and Moore, 2008; Butman and Raymond, 2011; Wallin *et al.*, 2011; Raymond *et al.*, 2013; Rasera *et al.*, 2013], but the nature of this effect has not been confirmed by direct, contemporaneous measurements of flow state and CO₂ efflux.

Given the strong rationale for how hydraulic characteristics may influence the rates of riverine CO₂ effluxes, and the homogeneity observed in measured CO₂ efflux globally (Figure 1), we designed a research program to assess the importance of flow hydraulics on CO₂ efflux. As climate change is projected to change regional hydrology, including seasonality, [e.g., Gloor *et al.*, 2013; Charlton and Arnell, 2014] understanding whether flow characteristics exert a physical control on efflux rate is required to measure the impact of climate change on CO₂ feedback processes.

Here at sites in two distinct climatic and hydrological regions, we assess whether flow intensity (a generic term which describes one or more of the measures of flow strength including mean flow velocity, bed shear stress, turbulent stress, and flow state) is a primary control on CO₂ efflux through simultaneous field measurements of CO₂ efflux, flow hydraulics, and other environmental descriptors. We explore an approach for supporting upscaling from point to provide catchment scale (or larger) flux estimates.

2. Materials and Methods

Our field sites vary in location, size, and catchment characteristics, and sampling has been carried out over several years, thus capturing a range of seasons and flow conditions. Within each site, measurement locations were chosen to ensure that a range of flow intensities were included.

atmosphere. While these studies provide understanding of gas fluxes, there is a range of forms of the predictive relationships and recognition that existing approaches are restricted by the range of flow depths and velocities for which gas transfer data are available and by the quality of the overall database [Palumbo and Brown, 2013]. In essence, gas transfer across the air-water interface occurs by molecular diffusion [Moog and Jirka, 1999], at a rate controlled by the concentration gradient. The rate of diffusion is also controlled by the thickness of the surface concentration boundary layer, i.e., the mean distance over which the gas concentration varies from the surface to nearly the bulk value [Moog and Jirka, 1999], and so thicker boundary layers reduce the rate of diffusion. Processes that disrupt the boundary layer therefore facilitate faster diffu-

Table 1. Global CO₂ Efflux Rates From Flowing Water^a

| Site Code | Site | Location | Catchment | Time Period | Method | Min.; Max. Efflux | Mean; Median Efflux | Mean (Min.; Max.) pCO ₂ | Source |
|-----------|--------------------|----------|--|---------------|--------|-------------------------|---------------------|------------------------------------|---------------------------|
| DW | Drumtee Water | Scotland | Agriculture/peat | 6/12 to 12/13 | FC | 0.07; 107 | 9.00; 2.59 | 1136 (174; 2678) | This study |
| RK | River Kelvin | Scotland | Urban | 6/12 to 12/13 | FC | 0.16; 50.7 | 8.25; 4.68 | 1112 (301; 1956) | This study |
| MT | Main Trail | Amazon | Rainforest | 2/11 to 5/12 | FC | 0.40; 12.0 | 4.54; 4.61 | 2451 (1256; 4205) | This study |
| NC | New Colpita | Amazon | Rainforest | 2/11 to 5/12 | FC | 0.33; 79.7 | 17.8; 13.2 | 6163 (2399; 10712) | This study |
| LT | La Torre | Amazon | Rainforest | 2/11 to 5/12 | FC | 0.40; 20.9 | 7.64; 6.65 | 2277 (742; 4397) | This study |
| TP | Tambopata | Amazon | Rainforest/ | 2/11 to 5/12 | FC | 0.50; 37.8 | 7.87; 6.48 | 1577 (813; 2965) | This study |
| 1 | Amazon Basin | Brazil | Agriculture/mining | 7/06 to 5/07 | FC | 0.41; 14.1 ^z | - | - | Rasera et al. [2008] |
| 2 | Amazon Basin | Various | Agroecosystems | 1/06 to 12/10 | FC, CP | -0.2; 14.2 ^z | - | -(259; 7808) ^x | Rasera et al. [2013] |
| 3 | Amazon | Various | Various | 6/04 to 1/07 | FC | 0.04; 14.2 | 3.90; - | 3317 (619; 12616) | Alin et al. [2011] |
| 4 | Mekong basins | Various | Various | 6/04 to 1/07 | FC | 0.67; 24.3 | 5.45; - | 3353 (141; 9569) | Large Rivers ^x |
| 9 | Amazon Basin | Brazil | Gneiss bedrock | 1/07 to 1/08 | FC | 11.7; 23.7 ^z | 17.7; - | -(6491; 14976) | Small Rivers ^y |
| | | | Oxisol soil | | | | | | Neu et al. [2011] |
| 10 | Mer Bleue Peatland | Canada | Peatland | 4/05 | FC | 0.82; 11.5 | 3.99; - | - | Billett and Moore [2008] |
| | Mer Bleue Peatland | Canada | Peatland | 4/05 | FC | 0.20; 1.84 | 0.80; - | - | Flowing water |
| | Mer Bleue Peatland | Canada | Peatland | 4/05 | FC | 0.20; 11.5 | 2.39; - | -(3850; 8630) | Open water |
| 11 | Black Burn | Scotland | Peatland | 1/05-8/05 | FC | 1.17; 39.6 | - | - | All data |
| 14 | Brocky Burn | Scotland | Mixed ^b | 3/97 to 8/98 | CC, GT | 0.25; 3.20 | 1.70; - | 424 (-; -) | Billett et al. [2006] |
| 15 | Brocky Burn | Scotland | Mixed | 3/97 to 8/98 | CC, GT | 3.91; 19.9 | 10.5; - | 1361 (-; -) | Hope et al. [2001] |
| 16 | Brocky Burn | Scotland | Mixed | 3/97 to 8/98 | CC, GT | 6.33; 44.2 | 27.6; - | 2674 (-; -) | Lower reaches |
| 17 | Krycklan Catchment | Sweden | Podzol soil and glaciofluvial sediment | 06 to 07 | FC | 0.16; 135 | - | -(713; 6253) | Middle reaches |
| | | | | | | | | | Upper reaches |
| | | | | | | | | | Wallin et al. [2011] |

^aEfflux in $\mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1}$, pCO₂ in μatm . Site codes correspond to Figure 1 and locations displayed in Figure S1. Method codes: FC = floating chamber, CP = water/atm pCO₂ difference and gas transfer velocity, CC = CO₂ concentration of the water, GT = gas tracer. ^xRivers > 100 m wide. ^yRivers < 100 m wide. ^zMin. and max. efflux calculated using standard deviations. ^bMixed: Granite bedrock, glacial drift, and organic soils.

2.1. Field Study Sites

Measurements were made in two catchments in the UK and one in the Peruvian Amazon. The UK measurements were made in two rivers with different land uses and catchment sizes, the River Kelvin (RK) and Drumtee Water (DW). The Kelvin (sampling site 55°52'06"N, 4°17'16"W; 18 m above sea level (asl)) is a 335 km² semiurban (23%) catchment, containing agricultural land (70%) and some forestry (6%), with a maximum elevation within the catchment of 510 m. Measurements were made within a 30 m reach, 1.2 km upstream of the confluence with the River Clyde Estuary, where bankfull width is 15–20 m and bed sediment is large pebbles and patches of exposed bedrock. Drumtee Water (sampling site 55°41'16"N, 4°23'37"W; 197 m asl) is a headwater, 9.6 km², peat-dominated catchment where the land use is rough grazing and maximum elevation within the catchment is 260 m. Measurements were made in a 19 m reach, where the channel is 4–5 m wide. These two drainage systems were sampled between June 2012 and December 2013 (number of samples: RK 83 and DW 79).

In the Amazon, measurements were made in four fluvial systems draining tropical rainforest in the Tambopata National Reserve (12°50'00"N, 69°17'45"W; 200 m asl), Madre de Dios region, Peru (for site map see *Viherrmaa et al.* [2014]). The sites ranged from small streams draining the local forest area to large rivers. Main Trail (MT) has a catchment of ~5 km² and was only active during the rainy season, being fed by surface runoff and throughflow. New Colpita (NC) is a perennial small stream draining 7 km². In both cases, channels were 4–7 m wide at sampling locations, width varying with season and corresponding stage height. La Torre river (LT) drains an area of 2000 km², and the channel is 40–80 m wide at the sampling point, which is located close to the confluence with Tambopata river (TP). TP has a 14,000 km² catchment extending to the foothills of the Andes, and the channel at the sampling point was ~200 m wide. TP catchment contains some small-scale agriculture and gold mining, but all four catchments are predominantly rainforest. The Amazonian sites were sampled between February 2011 and May 2012 with sampling campaigns including both wet and dry seasons and targeting the associated different water levels and flow conditions (number of samples: MT 42, NC 46, LT 37, and TP 26).

2.2. CO₂ Efflux

In all cases CO₂ efflux was quantified from measuring the rate of CO₂ accumulation in a floating chamber of known volume (0.0029 m³) [Frankignoulle, 1988] using a Licor (LI-840A) infrared CO₂/H₂O gas analyzer (for configuration see supporting information Figure S2). CO₂ accumulation was measured over 4 min and repeated three times. CO₂ flux was calculated using equation (1) [Frankignoulle, 1988; Rasesa et al., 2008]:

$$F_{\text{CO}_2} = \left(\frac{\delta \text{CO}_2}{\delta t} \right) \left(\frac{V}{RTS} \right) \quad (1)$$

where F_{CO_2} is the flux ($\mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1}$), $\delta \text{CO}_2 / \delta t$ is the slope of CO₂ accumulation in the chamber ($\mu\text{atm s}^{-1}$), V is the chamber volume (m³), R is the gas constant ($\text{m}^3 \text{atm K}^{-1} \text{mol}^{-1}$), T is the air temperature (K), and S is the surface area of the chamber at the water surface (m²).

2.3. Hydraulic Parameters

In the UK rivers, velocity was measured using a Valeport flowmeter with 50 mm diameter impeller, set to 60 second averaging, at 20% and 80% of the flow depth (for depth-averaged mean calculations) and a minimum of three other heights (to allow identification of outliers) within the semilogarithmic lower part of the flow profile. Mean velocity ($\bar{u} \text{ m s}^{-1}$) is an indicator of depth-averaged hydraulic conditions at the measurement point. Flow characteristics can be explored by considering the Froude (Fr) and Reynolds (Re) numbers. Fr is a depth-averaged dimensionless number that indicates the amount of surface water disturbance such as waves [Gordon et al., 2004; Allen, 1997] and so can act as a proxy for the interaction and degree of gas exchange between the water surface and the atmosphere. Reynolds number (Re) indicates the degree of turbulence and hence mixing in the water column [Gordon et al., 2004] and is an indicator of the potential transfer of CO₂-enriched water from lower in the water column and hyporheic zone (e.g., benthic recharge) [Peter et al., 2014] to the water surface. Froude and Reynolds numbers are calculated as follows:

$$a) \quad Fr = \frac{\bar{u}}{\sqrt{gH}} \quad (2a)$$

$$b) \quad Re = \frac{\bar{u}H}{\nu} \quad (2b)$$

where g is the acceleration due to gravity (m s^{-2}), H is the water depth (m), and ν is the kinematic viscosity ($\text{m}^2 \text{s}^{-1}$). Additionally at the UK sites, a qualitative visual assessment of the water surface state was undertaken; i.e., the degree of surface disturbances was estimated at the time of the CO_2 efflux measurement: “smooth” (a flat water surface), “medium” (ripples/waves with no white water) or “rough” (ripples and waves with white water) (for examples of these states see supporting information Figure S9). Wind speed was not measured, although the visual classification of water surface state incorporates the effect of wind at the water surface.

In the Amazonian streams, near-surface flow velocity is the mean of three replicates taken directly below the chamber position using a Geopacks hand-held flowmeter. Information to calculate Re and Fr was not available from the Amazon sites. As \bar{u} is highly correlated with Fr and Re , by definition, \bar{u} is used alone to indicate flow intensity for the Amazonian sites.

2.4. Water Chemistry Parameters

Water chemistry was analyzed at the time of chamber deployment to allow calculation of $p\text{CO}_2$ and exploration to find explanatory variables for CO_2 flux models. At Drumtee Water, pH was logged continuously (at 30 min resolution) with an In-Situ Inc. MP TROLL 9000 water chemistry sonde. The Troll 9000 was calibrated approximately every 4 to 6 weeks using two point calibrations from freshly prepared pH 4 and pH7 buffer solutions, and ensuring the manufacturers specified acceptable values for slope and intercept were reached. Measuring pH in situ eliminated the possibility of a delay enabling microbial action that leads to an altered sample pH [Abril *et al.*, 2015] and avoided compromising sample integrity through laboratory processes (which can alter sample pH through artificial degassing) [Herczeg and Hesslein, 1984; Abril *et al.*, 2015]; measuring pH continuously met the manufacturers pH probe minimum equilibration time specification of 20 min. For the River Kelvin our directly measured pH data were unreliable due to equipment malfunction and so pH was calculated from a linear relationship ($n = 10$; $R^2 = 0.72$) between discharge and pH fitted to data collected at a monitoring station 9 km upstream of the CO_2 measuring site (data provided by the Scottish Environmental Protection Agency, 2015). There are no significant tributaries entering between these sampling points, and similarity in water chemistry has been verified in a separate spatial sampling experiment (for details see supporting information Figure S3). At both RK and DW air and water temperature were measured using a Lilipop[®], Traceable[®], handheld thermometer.

For MT and NC, pH, conductivity and temperature were logged at 15 min resolution by an In-Situ Inc. MP TROLL 9500 data logger. For LT and TP, spot measurements of pH, conductivity, and temperature were made using a TROLL 9500 data logger at the time of CO_2 flux measurement. The TROLL was deployed for >20 min to ensure equilibration with stream water, and a maintenance regime similar to that described earlier was used.

At all sites, within 15 min of the flux measurement, water samples were collected for determining dissolved inorganic carbon concentration ([DIC]) using a headspace method [Waldron *et al.*, 2014] and analysis on a Thermo-Fisher-Scientific Gas Bench/Delta V Plus. Partial pressure of CO_2 ($p\text{CO}_2$) was calculated from the [DIC] using pH and temperature [Rebsdorf *et al.*, 1991; Stumm and Morgan, 1996]. Where pH was measured using a Troll 9000 or 9500 (DW, NC, MT, LT, and TP), uncertainty in pH is ± 0.1 pH unit according to the manufacturers specifications and 1.3% for RK indicated by the percent residuals (Figure S3). Uncertainty in [DIC] is 0.027 nM [Waldron *et al.*, 2014].

2.5. Data Analysis

Data analysis was carried out using R statistical package version 3.1.0 [R Development Core Team, 2008]. Most of the measured variables were lognormally distributed (Figure 3) and were log-transformed prior to modeling. As multiple measurements were made at each site, the data show some clustering. Thus, to avoid pseudoreplication in the analysis, a linear mixed effect model was fitted to the data [Pinheiro *et al.*, 2014]. Initially, a null model with no explanatory variables was fitted to the data to investigate the influence of different levels of data structure. This showed that 2% of the variance was between regions (Amazon; UK), 12% between sites within a region, and 86% within the sites. The low between site and between region variances suggest that there was no significant systematic regional difference in efflux rate. The 86% of variance within the individual sites indicates that the differences in site characteristics (e.g., stream order) were less important than sample-to-sample variability due to variation in flow intensity and water chemistry. Further,

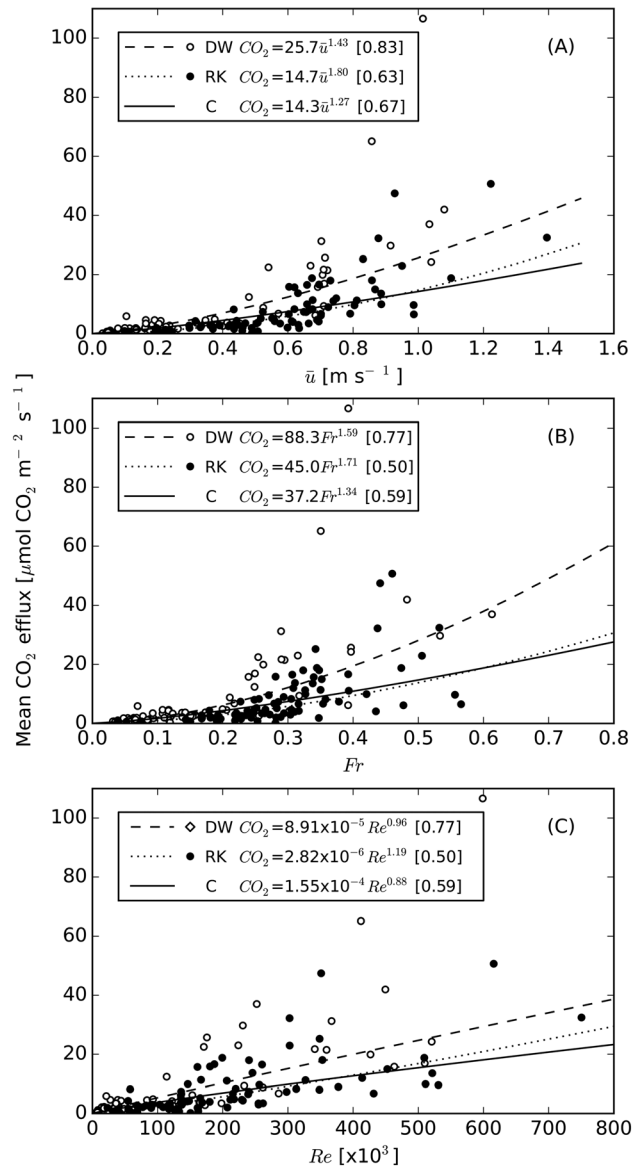


Figure 2. CO₂ fluxes related to hydraulic properties for DW and RK sites. CO₂ efflux plotted against: (a) mean flow velocity (\bar{u}), (b) Froude number (Fr), and (c) Reynolds number (Re). All show strong positive, logarithmic relationships with CO₂ efflux, with efflux rates being slightly higher and the curves slightly steeper at DW. “C” represents DW and RK combined data. All relationships were significant at $P < 0.001$. R^2 values (in square brackets) indicate that the relationship between \bar{u} and CO₂ efflux is strongest.

flow intensity available for the Amazon data, so we use mean velocity below acknowledging that this is an empirical proxy for turbulence and water surface conditions. For generality, we use the term flow intensity to encompass the combined effects of velocity, turbulence, and water surface conditions on gas transfer and exchange.

CO₂ partial pressure of the water ($p\text{CO}_2$) varied between sites, and all were within previously reported ranges [Raymond *et al.*, 2013, and references therein] (Table 1). NC had by far the highest $p\text{CO}_2$ of all the studied sites (mean 6163 μatm , maximum 10,712 μatm) with mean $p\text{CO}_2$ being 2.5–5.5 times the magnitude of that of the other sites. RK had the lowest mean and maximum $p\text{CO}_2$ (mean 1112 μatm , maximum 1956 μatm) with the maximum $p\text{CO}_2$ being lower than the minimum $p\text{CO}_2$ at NC (2399 μatm). We propagated the pH and DIC

analysis of the variance structure indicated that “site” was sufficient as a grouping factor in further analyses as regional variance was so low.

3. Results

CO₂ efflux rates ranged between 0.07 and 107 $\mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1}$ overall, with all six sites having similar CO₂ efflux ranges. Five sites had very similar mean CO₂ effluxes (range 4.54 to 9.00 $\mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1}$); however, the mean at NC was 17.8 $\mu\text{mol CO}_2 \text{ m}^{-2} \text{ s}^{-1}$, two to four times that of the other sites. Ranges and means of CO₂ efflux rates at all sites lie within the range of previously reported values (Figure 1 and Table 1).

Using pooled data from DW and RK, significant positive logarithmic correlations are found between CO₂ efflux and each of the hydraulic parameters, \bar{u} , Fr , and Re (Figure 2). Data from RK and DW overlap indicating similar controls on efflux at both sites, although with some differences in the gradients and significance levels of the relationships (Figure 2). At all six sites there was a significant positive correlation between CO₂ efflux and \bar{u} (Figure 3), although the overall relationship shows fanning at the upper end. The similarity of relationships involving \bar{u} , Fr , and Re with efflux occurs by definition, but turbulence and flow state are responsible for gas transfer within the water column and at the water-atmosphere boundary, respectively. Mean velocity empirically records these processes but is less likely to be applicable across scales than the dimensionless Fr and Re parameters. However, \bar{u} has the highest correlation with CO₂ efflux at the UK sites and is the only measure of

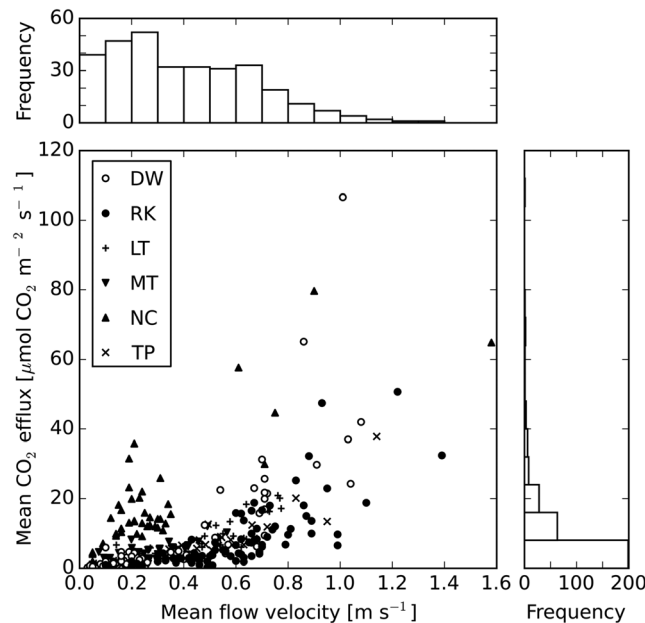


Figure 3. CO₂ efflux and mean flow velocity data from all UK and Amazonian sites. All sites follow the same trend whereby CO₂ efflux increases with flow velocity, apart from one of the Amazonian small streams (NC) where a given velocity resulted in a higher efflux rate. Both the response variable (efflux) and the explanatory variable (flow velocity) show skewed distributions and were therefore log-transformed before fitting statistical models to the data.

as explanatory variables, describes the data from all six sites (equation (3)). The residuals were randomly distributed (see supporting information Figure S5):

$$\log(F_{CO_2}) = -2.88 + 1.06 * \log(\bar{u}) + 0.77 * \log(pCO_2). \tag{3}$$

The fit had an adjusted R^2 value of 0.66 (see supporting information Figure S6), and the overall P value was highly significant (<0.001). An alternative approach fitting a model with flow: pCO_2 interaction was also tested, but the interaction term was not significant.

To account for intersite variation, a linear mixed effect model was fitted [Pinheiro and Bates, 2000], which yielded the following predictive equation based on the fixed effects:

$$\log(F_{CO_2}) = 1.43 + 1.20 * \log(\bar{u}) + 0.22 * \log(pCO_2). \tag{4}$$

Site-specific random effect terms on the intercept ranged from -0.87 to $+1.12$ (see Figure S6). In this case the flow: pCO_2 interaction term was autocorrelated with pCO_2 and could not be included in the model simultaneously. The site-specific terms reflect the magnitude of CO₂ efflux and thus are related to site-specific controls over the availability of CO₂. Four sites have effect terms that are close to zero (-0.14 to 0.01); RK has a significantly lower intercept (-0.87) and NC a significantly higher value (1.12).

The two models, equations (3) and (4), have different intercepts due to the separate site-specific component in the mixed effects model. The flow velocity coefficients (1.06 and 1.20) are similar between the models but pCO_2 has a lower coefficient in the mixed effects model (0.77 versus 0.22). This implies that some of the differences in pCO_2 values between sites (Kruskal-Wallis rank sum test, P value $\ll 0.001$) are attributed to site-specific effects, whereas the velocity differences are systematic across all sites.

Direct measurement of hydraulic properties is not always possible, so for the UK sites, the qualitative description of water surface state was used to assess the potential for rapid upscaling. Adding water surface state to the logarithmic relationships between efflux and hydraulic variables, the data separate according to the visual characterization (Figure 5). There is little separation between the medium and rough data sets, implying that moderate disturbance of the water surface disrupts the surface boundary layer.

uncertainties to calculate the uncertainty in pCO_2 ; this ranges from 14.4 to 32.8% of the pCO_2 value, and the intersite differences still exist; for example, NC is significantly different to the other sites ($P = <0.001$; for detail see supporting information Table S1 and Figure S4).

The relationship between CO₂ efflux and \bar{u} at the Amazonian sites was the same as the UK sites (Figure 3), except for at NC which has a higher rate of CO₂ efflux for a given velocity. When the influence of pCO_2 was included, by plotting efflux against the product of flow velocity and pCO_2 , data from NC and all other sites collapse onto a linear log-log relationship (Figure 4). Assumptions that all error is contained in either the product of flow velocity and pCO_2 , or flux provide constraints on the range in this relationship (Figure 4).

A multiple regression model, with log-transformed flow velocity and pCO_2

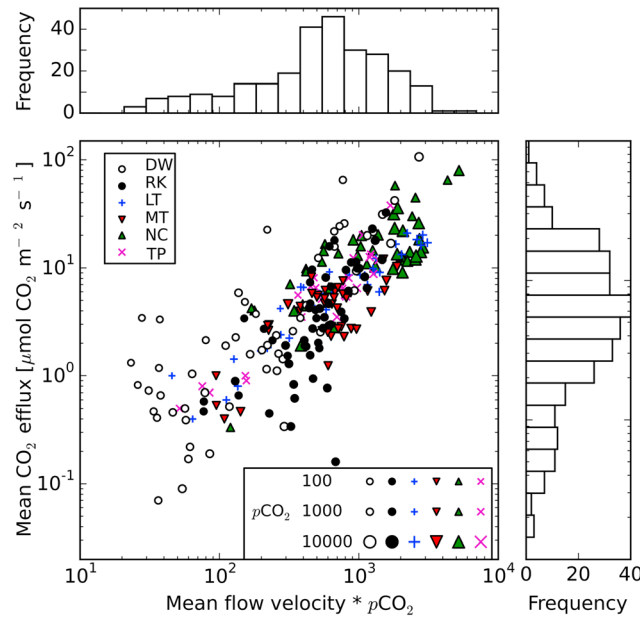


Figure 4. Data from UK (RK and DW) and Amazonian sites (MT, NC, LT, and TP) demonstrating a log-log relationship between CO₂ efflux and the product of flow velocity and pCO₂. By including the influence of pCO₂, NC falls in line with the rest of the study sites. The log-transformation produces variables that are approximately normally distributed as shown by the histograms. Symbol size is scaled by pCO₂, and site coded by color. The dashed and dotted lines are log-log regressions assuming that all error is contained in flux and the “mean flow velocity*pCO₂” product, respectively. The solid line is the bisector of these relationships and is an approximation to the functional relationship between the dependent and independent variables where both have equal proportional error.

4. Discussion

Measurements of the ranges and mean values of CO₂ efflux from rivers in contrasting climatic zones, UK (temperate) and Amazonian (tropical), show no significant differences, and all data fall within previously reported ranges that show no consistent pattern with latitude (Figure 1 and Table 1). We interpret these results as showing that ecosystem level productivity is not the primary control on CO₂ efflux and an alternative explanation for intersite variability in CO₂ efflux is required.

pH can limit CO₂ efflux through its influence on speciation of the DIC pool [Hoffmann and Schellnhuber, 2010]. At high pH, a greater proportion of the DIC pool is in the form of carbonate and bicarbonate ions, which only exist in aqueous form, and so are not available for degassing. Thus, it is possible that at higher pH the CO₂ pool size may be smaller; however, the size of the CO₂ pool is also dependent on the total DIC concentration, as it is a proportion of this. Here at the time of sampling,

the pH of all fluvial systems was rarely above pH 7; thus, in all cases, under these relatively low pH conditions, CO₂ was available for degassing.

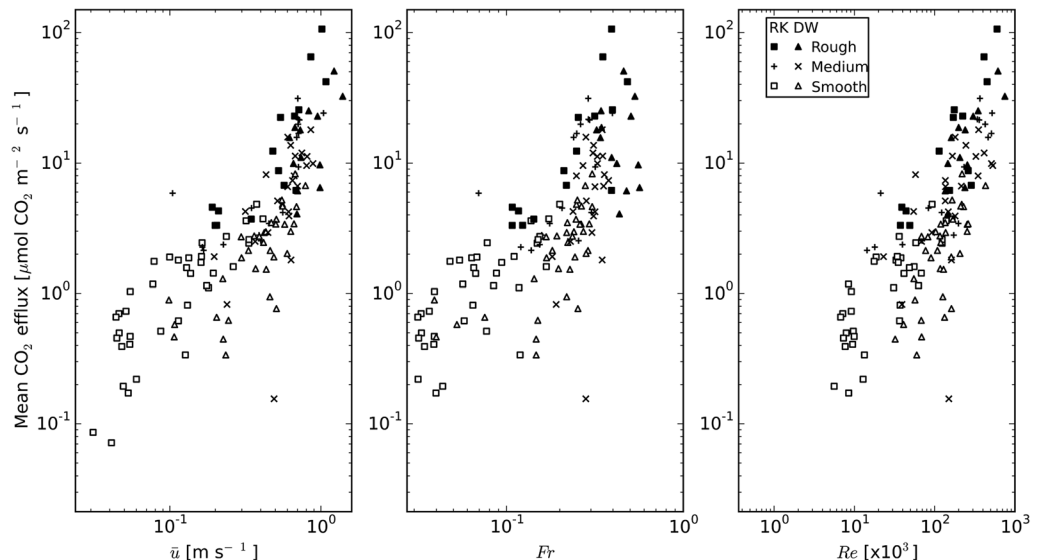


Figure 5. Separation of data by visually determined flow state in the relationships between CO₂ efflux and mean velocity, Froude number, and Reynolds number.

Within-site variability is greater than that observed between sites and is consistently related to flow hydraulics (Figures 3 and 4). Hydraulic controls over CO₂ efflux have been suggested previously [Raymond *et al.*, 2012; Wallin *et al.*, 2011], but published studies estimated this from stream slope and estimates of gas transfer velocity (k) rather than direct measurements of both flux and hydraulic variables as have been made here. When pooled CO₂ efflux data from all six sampling sites were plotted against \bar{u} , an increase in CO₂ efflux occurs as flow intensity increases regardless of climatic zone (Figure 3). CO₂ efflux should be enhanced by flow intensity because convection and turbulent mixing associated with eddies greatly enhance gas transfer across the air-water interface [Moog and Jirka, 1999; Eugster *et al.*, 2003] by repeatedly renewing the surface boundary layer with CO_{2(aq)}, maintaining a steep CO₂ concentration gradient between the water and the atmosphere [Eugster *et al.*, 2003]. It is unclear what scale of eddies are the most important to gas transfer across an air-water interface [Moog and Jirka, 1999]. However, it is thought to be a combination of large- and small-scale eddies, with the higher-frequency small-scale eddies embedded within larger eddies, carried to the surface where they renew the surface zone [Moog and Jirka, 1999], transferring CO₂ where available from the bed.

Of all of the sites, NC is distinctive having higher minimum, maximum and mean CO₂ efflux than the other five sites for a given flow velocity (Figure 3 and Table 1). At all six sites, mean $p\text{CO}_2$ levels showed oversaturation with respect to atmospheric CO₂ concentration, but NC had much higher $p\text{CO}_2$ levels and greater oversaturation than all the other sites (Table 1). Although data are not abundant, elevated $p\text{CO}_2$ has been previously reported to enhance CO₂ evasion [Billett and Moore, 2008]. Elevated $p\text{CO}_2$ can cause enhanced CO₂ efflux due to a greater availability of CO₂ for degassing and a steeper water-atmosphere CO₂ concentration gradient [Billett *et al.*, 2006]. Thus, it seems likely that at NC, the higher concentration of CO₂ in the water resulted in greater CO₂ efflux at a given velocity. When $p\text{CO}_2$ was included in the model for efflux, NC data aligned with the other sites (Figure 4 and supporting information Figure S7). That it was only necessary to include $p\text{CO}_2$ to align one site suggests flow intensity is the primary control on CO₂ efflux and $p\text{CO}_2$ the secondary. Our knowledge of hydrological pathways in the catchments supports this analysis, as NC is the only site with a dominant groundwater contribution to its flow. Fanning at the upper end of the relationship between CO₂ efflux and \bar{u} (Figure 3) indicates that factors that were not considered in this study may contribute to variation in CO₂ efflux, for example, the interaction of stream water with the river bed [e.g., Peter *et al.*, 2014], dissolved organic carbon concentration (as a contributor through respiration or UV oxidation to CO₂ [Cole *et al.*, 2007]), or seasonality (controlling allochthonous inputs and as a proxy for temperature, autochthonous and secondary production [e.g., Billett and Moore, 2008; Dawson *et al.*, 2009]).

These data suggest that for the range of $p\text{CO}_2$ values at the six sites, CO₂ efflux can be considered to be hydraulically limited, analogous to transport-limited solute transport in rivers; i.e., the flux of CO₂ to the atmosphere is primarily determined by turbulence and water surface disturbance which, respectively, supply CO₂ to the water surface and facilitate its transfer to the atmosphere. Figure 2 shows significant single-site relationships between efflux and flow parameters, with R^2 values 0.5–0.83. Combining data from sites introduces variation in $p\text{CO}_2$ and potentially other processes such as wind disturbing the water surface which is of more significance in larger rivers. However, introducing $p\text{CO}_2$ either as a secondary variable (equation (3)) or in a linear mixed effect model (equation (4); Figure 4) provides improved statistical significance. Where the supply of CO₂ is limited, for example, in high pH streams, we hypothesize that the relative significance of hydraulic conditions will be reduced and that additional biogeochemical parameters may need to be introduced to these explanatory models.

As yet there is no simple sensor technology to directly measure CO₂ efflux from a stream or river surface and to enable spatial and temporal upscaling, so we need to explore proxy approaches. When considering the water surface state in the relationship between CO₂ efflux and $\log \bar{u}$, $\log Fr$ and $\log Re$, the data separate according to the visual characterization of the water surface (Figure 5). The relationship between water surface state and Froude number is well known [Gordon *et al.*, 2004]: water surfaces classified as “smooth” separate by Froude number from those classified as medium and rough (supporting information Figure S8) and by definition, Fr is correlated with other measures of flow intensity. With the collection of suitable calibration data sets, visual classification data could provide estimates of Froude number. Water surface state can be measured from aerial imagery [Cox and Munk, 1954; Preisendorfer and Mobley, 1986; Gordon, 2005] and so if this visual classification method can be refined, there may be potential for using remote sensing techniques to include more accurate estimates of CO₂ evasion from low-order and/or inaccessible streams in catchment scale or global estimates of riverine CO₂.

5. Conclusion

Direct measurements of flow intensity with CO₂ efflux rates at six sites in two contrasting climatic regions show that flow intensity is a primary control on CO₂ efflux rates. Here \bar{u} has the highest correlation with CO₂ efflux but is less likely to be applicable across scales than Fr and Re , so instead we use the term flow intensity to encompass multiple measures of flow stress. The relationship between flow intensity and CO₂ efflux is refined when pCO_2 is included in the model, correcting for intersite variability. The highest CO₂ effluxes were measured when both flow velocity and pCO_2 were high. However, the highest effluxes occur over a range of velocities, suggesting that additional controls, for example, diurnal or seasonal responses or the impact of hydrological events [e.g., Peter *et al.*, 2014] also influence CO₂ efflux rates. It may be possible to refine the model by quantifying these and incorporating such controls empirically into the model.

Having confirmed the significance of hydraulic controls over CO₂ efflux, there is potential for improving both the coverage and accuracy of CO₂ efflux estimates from surface waters, overcoming limitations in understanding that support upscaling. We note that our model describes less well CO₂ efflux rates at the highest flows and so further data are required in high flow conditions to refine the model. Additionally, we lack knowledge of CO₂ recharge from the interaction of the water column with the benthic and hyporheic zones [e.g., Peter *et al.*, 2014], and how this influences the capacity to degas CO₂ needs to be considered, with a view to comparison with models that estimate CO₂ degassing at the catchment scale [e.g., Abril *et al.*, 2014]. Further, our model is unlikely to apply in conditions where CO₂ efflux is supply limited, e.g., middle to high pH systems such as glacial-melt [Thomas and Raiswell, 1984; Brown, 2002] or tufa systems [Chen *et al.*, 2004; Pedley *et al.*, 2009] where speciation of DIC can limit efflux, but flow velocity may still be high. However, to support upscaling, visual classification of water surface state shows promise but requires development and rigorous testing to reduce subjectivity and variation in the estimates.

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