

Comparative analysis of the life cycle impact assessment of available cement inventories in the EU

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Abstract

Life Cycle Impact Assessment (LCIA) is one of basic steps in Life Cycle Assessment methodology (LCA). This paper presents a comparative study of the LCIA of different life cycle inventories (LCI) for EU cements. The analysis unit used is the manufacture of 1 kg of cement, from "cradle to gate". The impact categories considered are those resulting from the manufacture of cement and include greenhouse effects, acidification, eutrophication and summer and winter smog, amongst others.

The results of the study highlighted some inconsistencies in existing inventories. As for the LCIA, the main environmental interventions related to cement manufacture were classified and characterised and their effect on different impact categories analysed. Differences observed in evaluation of the impact of cement type were essentially related to their clinker content.

Keywords: life cycle impact assessment, life cycle assessment, life cycle inventory, cement production, system boundary, clinker

1. Introduction

Life cycle assessment (LCA) methodology is used to evaluate the impact of processes or products on the environment [1]. Fundamental to this analysis is the inclusion of every stage of a process or product's life cycle. In the case of products, every stage from the production of the raw materials to the end of their useful lives and their use and maintenance should be included. Thus, all significant environment impacts in their life cycle can be addressed.

In some cases, however, a full life cycle (cradle to grave) analysis is impossible and the analysis must terminate at an intermediate stage (cradle to gate) or begin and end at intermediate stages (gate to gate). This is the case, for example, if one analyses cement production which has multiple specific applications (beams, pillars, pavements, bridges, etc.) and therefore disallows a unique life cycle to be defined (cradle to gate).

This type of partial analysis (not cradle to grave) is useful for comparing and evaluating possible improvements in environmental behaviour as well as constructing more

complete life cycles for specific cement end-products (beams, columns, pavements etc).

One of the fundamental parts of a LCA is the undertaking of a life cycle inventory (LCI), in which the energy and materials used and wastes emitted during the manufacture of a product are identified and quantified (in solid, liquid or gas form). This typically yields a long list of environmental interventions that is difficult to manage and interpret [1-5].

These environmental interventions in the inventory are classified and characterised during the life cycle impact assessment (LCIA) stage. During this process the results are summarised into a short list of impact categories. These impact categories (such as the greenhouse effect or acidification), are much easier to interpret than the environmental interventions themselves.

An earlier paper [6] compiled and analysed LCI for EU cements and included both input and output data. The latter focused on main emissions resulting from the production of cement (CO₂, SO₂, NO_x and dust). Alternative

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techniques were used to evaluate these emissions and thus compare the results from different LCI and confirm the validity of the methodology.

Key issues in available LCI were summarised in the previous paper by the authors [6], such as a) the identification of some inconsistencies in the figures included in some of them, b) the possibility of using theoretical models to estimate some environmental interventions, c) that emissions are primarily produced during the production of clinker, and d) that the types of cement that require the least amount of energy for their production are those which use greater proportions of different types of additives.

The main objective of this paper is to undertake a comparative study of the impact assessment of the same LCI analysed in [6]. The analysis unit used was 1 kg of Portland cement, with or without some types of additives. These LCI

were obtained from references [7] and [8] and from information provided by several manufacturers and are listed in Table 1 ([9-17]. Reference [6] provides further detailed information on the source data. It should be noted that these inventories depend, among other things, on the system boundaries utilised in each case.

LCA can be undertaken by following a number of different specific methodologies [18-21] which can use different impact categories such as greenhouse effect, stratospheric ozone depletion, acidification, eutrophication or toxicity as well as have different hypotheses for evaluating their environmental impact. This paper uses the CML 1992 methodology ([18]), which is one of the most widely used and accepted in Europe and has recently been updated ([21]).

Original cement name and reference	Classification		Clinker	Origin
			(%)	
Cement Portland I [7]	Type I	Portland cement	95-100	Holland
Cement Portland [7]	Type II / A-S	Portland slag cement	80-94	Holland
Blastfurnace slag cement [7]	Type III / B	Blastfurnace cement	20-34	Holland
Cement Hoogoven I [7]	Type III / B	Blastfurnace cement	20-34	Holland
Portland ash cement [7]	Type IV / B	Pozzolanic cement	45-64	Holland
Cement CH [7,(9)]	Type I	Portland cement	95-100	Switzerland
Cement N [8,(10)]	Type I	Portland cement	95-100	Sweden
Portlandcement NL1 [8,(11)]	Type I	Portland cement	95-100	Holland
Cement S [8,12]	Type I	Portland cement	95-100	Sweden
Cement SF1 [8.13]	Type I	Portland cement	95-100	Finland
Cement SF2 [8.14]	Type I	Portland cement	95-100	Nordic Countries
Portlandcement A [8,(15)]	Type II / A-S	Portland slag cement	80-94	Austria
Portlandcement NL2 [8,(16)]	Type II / A-S	Portland slag cement	80-94	Holland
Portlandcement NL3 [8,(17)]	Type II / B-S	Portland slag cement	65-79	Holland
Blastfurnace slag cement NL1 [8,(16)]	Type III / B	Blastfurnace cement	20-34	Holland
Blastfurnace slag cement NL2 [8,(17)]	Type III / B	Blastfurnace cement	20-34	Holland

TABLE 1. LCI utilised in this paper ([6])

2. Impact assessment

The LCIA is also a fundamental stage in a LCA [1] and consists of a number of parts. In the first or classification part, each environmental intervention in the LCI is associated with the impact category or categories in which it has an effect (for example, CO₂ is associated with the greenhouse effect).

In the second or characterisation part, the relative effects of all the environmental interventions associated with each of the different impact categories are compared with

one another (for example, 1 kg of CH₄ has the same impact on the greenhouse effect as do 11 kg of CO₂). A reference unit is defined for each impact category (for example, equivalent CO₂ on the greenhouse effect) as well as the corresponding characterisation factors (11, as indicated in the case of CH₄). Additionally, there may be a later phase of normalisation, in which the results of each impact category are divided by a reference figure (for example, for the greenhouse effect, worldwide CO₂ emissions is sometimes used).

Of all the impact categories considered in the 1992 CML methodology ([18]), those that are affected by one or more of the main emissions resulting from the production of cement were the first to be analysed. In agreement with [6], these emissions are stipulated as CO₂, SO₂, NO_x and dust, which in Table 2 are presented in association with the corresponding impact categories. This Table also includes the

corresponding characterisation factors of these environmental interventions.

The impact categories are classified as global, regional or local, depending on their geographical area of impact. This sort of classification facilitates a subsequent analysis of the results and decision-making depending on the scope of the point of view adopted.

Impact area	Impact category	Airborne emissions of the system			
		CO ₂	SO ₂	NO _x	Dust
Global	Greenhouse effect	1			
Regional	Acidification		1	0.7	
	Eutrophication			1	
Local	Winter smog		1		1

TABLE 2. Initial impact categories considered in the analysis

3. Study of the global environmental impacts

3.1. Greenhouse effect

Table 3 shows the results of the greenhouse effect characterisation of the different types of cement studied. The values are expressed in grams of equivalent CO₂ per kg of cement produced.

This Table shows the relevant gas emissions related to the greenhouse effect, which, in this case, are carbon dioxide (CO₂), methane (CH₄) and nitrous oxide (N₂O), which have the corresponding characterisation factors of 1, 11 and 270 respectively. The individual contribution of each gas emitted are also shown as percentages in order to determine their relative influence on this impact category.

Of the values shown in the Table, one can deduce that the total influence of methane (CH₄) and nitrous oxide (N₂O) on the greenhouse effect is very small in comparison to the contribution of carbon dioxide (CO₂), which lies between 98.8 and 100%. This is because despite having a lower characterisation factor (1), the amount of CO₂ emitted is much higher than the other gases.

It is important to acknowledge the substantial quantitative effects of CO₂ emissions. Depending on the type of cement, these can reach values as high as 800g of CO₂ per kg of Type I cement. This data supports the opinion of the Intergovernmental Panel on Climatic Change [22], which suggests that the production of cement is a relevant industrial source of CO₂ emissions.

The variations shown between the emission values of different cements in Table 3 are due mainly to the amount of clinker in the cements. The variations in total CO₂ may be related to the type of resources utilised (mainly the fuels).

Despite the fact that Type I cements typically have a CO₂ emission of 800 g per kg of cement, quoted figures can be as low as 354.70 g per kg, as shown for the Cement Portland I [7]. The variation may be due to the fact that, for Cement Portland I, some of the emissions caused by the production of clinker are being omitted (perhaps only those associated with the fuel are considered), either because a certain proportion of these emissions are for some reason omitted from the inventory, or due to variations in definition of the system boundaries. This is confirmed by the fact (as is shown in [23]) that The Netherlands, the country of origin of this cement, has only one furnace producing clinker and three plants producing cement, all of which should yield very similar results (compare Cement Portland I with Portland Cement NL1 [8, 16]).

The principal source of variation in the results for the remaining types of cements is the amount of clinker in each. The inconsistencies between some of the results have already been analysed in [6] and are due to several factors including the definition of system boundaries and numerical errors. In cement types that incorporate high percentages of pozzolanic or cementitious additions (such as blast furnace slag or fly ashes), for example, Type III cements, the CO₂ emission reductions can be of the order of 60-70% compared to corresponding Type I cements.

Type	Cements	CO ₂	CH ₄	N ₂ O	Total
I	Cement Portland I	354.70 (100%)	0.00062 (0%)	-	354.70 (100%)
	Cement CH	810.00 (100%)	-	-	810.00 (100%)
	Cement N	813.00 (99.5%)	3.44 (0.5%)	0.60 (0%)	817.04 (100%)
	Portlandcement NL1	853.00 (100%)	-	-	853.00 (100%)
	Cement S	805.00 (99.6%)	3.3 (0.4%)	0.000039 (0%)	808.30 (100%)
	Cement SF1	780.00 (98.9%)	8.25 (1.1%)	0.00057 (0%)	788.25 (100%)
	Cement SF2	812.70 (98.8%)	9.93 (1.2%)	0.016 (0%)	822.65 (100%)
II	Cement Portland	918.30 (99.8%)	-	1.84 (0.2%)	920.14 (100%)
	Portlandcement A	586.00 (100%)	-	-	586.00 (100%)
	Portlandcement NL2	807.00 (100%)	-	-	807.00 (100%)
	Portlandcement NL3	289.00 (100%)	-	-	289.00 (100%)
III	Cement Hoogoven I	221.70 (100%)	0.00069 (0%)	-	221.70 (100%)
	Blast furnace slag cement	334.10 (98.9%)	-	3.85 (1.1%)	337.95 (100%)
	Blastfurnace slag cement NL1	212.00 (100%)	-	-	212.00 (100%)
	Blastfurnace slag cement NL2	134.00 (100%)	-	-	134.00 (100%)
IV	Cement Portlandash	692.90 (99.7%)	-	1.82 (0.3%)	694.72 (100%)

TABLE 3. Characterisation of the cements studied with respect to the global greenhouse effect (in grams of equivalent CO₂ per kg of cement and relative percentage)

3.2. Other sources of global environmental impact

As for other sources of global environmental impact (such as the contribution to the stratospheric ozone depletion), the production of cement does not have significant effects.

4. Study of the regional environmental impact

Some of the emissions caused by the production of cement have regional effects, such as acidification and eutrophication. As shown in Table 2, the main emissions resulting from the production of cement that contribute to these processes are sulfur dioxide (SO₂) and nitrogen oxides (NO_x). However, as these are among the

environmental interventions in the inventories, other influential emissions have also been included in this study, such as hydrochloric acid (HCl), ammonia (NH₃), total nitrogen (N-tot) and the chemical oxygen demand (COD), which comes from the energy production.

Characterisation factors are taken from Table 4 [18]. The reference units are the equivalent sulfur dioxide (SO₂) for acidification and the equivalent phosphatic compound (PO₄) for eutrophication.

Both of these impact categories are analysed in the following sections.

Emission	Acidification	Eutrophication
NH ₃ (ammonia)	1.88	0.33
HF (fluorhydric acid)	1.60	--
HCl (hydrochloric acid)	0.88	--
NO ₂ or NO _x (nitrogen oxides)	0.70	0.13
SO ₂ or SO _x (sulphur dioxide)	1.00	--

TABLE 4. Characterisation factors used for acidification and eutrophication

4.1. Acidification

The results that correspond to this impact category (in reference units) for all the cements studied are shown in Table 5. This Table also shows the breakdown of the total emission into percentages by type of emission, so as to show the relative implication of each.

The main emissions of SO₂ and NO_x during the production of cement occur during the high-energy combustion of fossil fuels used to produce clinker and those used by mechanical equipment and vehicular transport. However SO₂ emissions also occur when clays are used as raw materials in the production of clinker and the fraction of SO₂ not chemically combined is emitted into the atmosphere.

The total emission (in g of equivalent SO₂ per kg of cement) depends on the type of cement and ranges between 2 and 3 for Type I, between 1 and 2 for Type II, and has values lower than 1 for Types III and IV. These results are logical in the light of their high dependence on clinker content.

In Table 5, one can see the high proportion of total acidification that is typically caused by NO₂ emissions (in g of equivalent SO₂), which result from using fossil fuels in the clinker furnace, machinery and vehicles. The contributions of HCl and NH₃ emissions, which are only included in some inventories, are practically negligible.

The inclusion of the latter two environmental interventions in some inventories and not in others can be due to the fact that they were only deemed to be significant in some of the studies, or because different criteria were used to define their system boundaries. This last possibility would be another example of the heterogeneity of existing inventories.

4.2. Eutrophication

Eutrophication is a consequence of, among other things, the emission of nitrogen oxides (NO_x), which produces an enrichment of nutrients in aquatic reserves and agricultural

soils. During the manufacture of clinker and cement, nitrogen oxides (NO_x) are emitted, whose origin lies primarily in the type of fuel used in obtaining the clinker and in the production of electrical energy ([6]). There are other relevant emissions in the system being studied, such as ammonia (NH₃), total nitrogen (N-tot) and the chemical oxygen demand (COD).

Table 6 shows the results for the characterisation (in mg of equivalent PO₄ per kg of cement) and the percentages that each emission represents in relation to the total. These results show that the principal source in this case is the emission of NO_x, and that other emissions are negligible.

The results in Table 6, as expected, depend on the type of cement and furthermore, on the type of clinker. Thus, for Type I cement, the results for the characterisation ranged from 250-350 mg of equivalent PO₄, whilst for Type II, the range was 125-250, and for Type III, 50 and 125.

The observed differences between some of the cements of similar Type are considered to be due to errors in the environmental interventions or in how the inventories defined their system boundaries, as stated in [6]. For example, in the case of Cement Portland I, which has a lower than average equivalent PO₄ (124.38mg), mistakes were detected in its inventory, as mentioned before. Thus, the inventory probably omitted a considerable amount of the NO_x emitted in the cradle to gate analysis of this cement.

These results suggest that a cement plant producing 1 million tonnes of cement a year releases 0.5 kg of phosphorus per hectare (assuming an influence distance of about 35 km – 20 miles - surrounding the cement plant), which is in line with the values set by the European Environment Agency [24] for the industrialised countries of Western Europe.

Type	Cements	SO ₂	NO _x	HCl	NH ₃	Total
I	Cement Portland I	0.43 (39%)	0.67 (61%)	0.000019 (0%)	-	1.10 (100%)
	Cement CH	0.60 (30%)	1.40 (70%)	-	-	2.00 (100%)
	Cement N	0.67 (31%)	1.46 (69%)	-	0.000010 (0%)	2.13 (100%)
	Portlandcement NL1	0.08 (4%)	1.81 (96%)	-	-	1.89 (100%)
	Cement S	0.45 (25%)	1.36 (75%)	-	-	1.81 (100%)
	Cement SF1	0.63 (20%)	2.59 (80%)	-	-	3.22 (100%)
	Cement SF2	1.33 (39%)	2.07 (61%)	-	-	3.40 (100%)
II	Cement Portland*	1.16 (35%)	2.17 (65%)	-	0.00036 (0%)	3.33 (100%)
	Portlandcement A	0.12 (10%)	1.10 (90%)	-	-	1.22 (100%)
	Portlandcement NL2	0.09 (4%)	2.07 (96%)	-	-	2.16 (100%)
	Portlandcement NL3	0.98 (67%)	0.49 (33%)	-	-	1.47 (100%)
III	Cement Hoogoven I	0.51 (59%)	0.35 (41%)	0.000015 (0%)	-	0.86 (100%)
	Cement blast furnace slag*	0.58 (43%)	0.77 (57%)	-	0.00076 (0%)	1.35 (100%)
	Blastfurnace slag cement NL1	0.03 (5%)	0.60 (95%)	-	-	0.63 (100%)
	Blastfurnace slag cement NL2	0.43 (61%)	0.28 (39%)	-	-	0.71 (100%)
IV	Cement Portlandash*	0.90 (36%)	1.63 (64%)	-	0.00025 (0%)	2.53 (100%)

* This inventory also states the presence of negligible amounts of fluorhydric acid (HF).

TABLE 5. Characterisation of the different types of cement in terms of the regional impact of acidification (in grams of equivalent SO₂ per kg of cement)

5. Local impact

Dust in the air can cause respiratory problems in humans, livestock and wildlife. These effects are included in the impact category referred to as winter smog which is one consequence of particulate air pollution by SO₂, dust and soot (the by-products of combustion).

Table 7 shows the results corresponding to this impact category for each of the cements studied. This shows the effects of individual emissions (in g of equivalent suspended particle matter – SPM - per kg of cement) as well as the total effect. A characterisation factor 1 was adopted for all emissions.

The results of Table 7 show that soot has a negligible influence and that there is very high variation in the inventoried results for SO₂ and dust. Again, this is most likely to be due to

inconsistencies in the boundaries conditions used when compiling the inventories [6].

Considering absolute values, it should be noted that the values for Cement Portland I, Portlandcement NL1, Portlandcement NL3, Cement Hoogoven I and Blast furnace slag cement NL2 were two orders of magnitude higher than those of the other cements (0.25-1.50g equivalent SPM per kg of cement). These results could be due to errors in the inventories, in which case further emphasis is placed on the need to standardise inventory methodology, or to the effect of some initial stages of the life cycle analysed (for instance energy production) or to the possibility that inappropriate dust filters were used at the production plant. The latter seems highly unlikely, due to the acute environmental sensitivity of the countries from which these cements came.

Type	Cements	NO _x	NH ₃	N-tot	COD	Total
I	Cement Portland I	124.38 (100%)	-	-	-	124.38 (100%)
	Cement CH	260.00 (100%)	-	-	-	260.00 (100%)
	Cement N	271.70 (100%)	0.002 (0%)	0.023 (0%)	-	271.70 (100%)
	Portlandcement NL1	335.40 (100%)	-	-	-	335.40 (100%)
	Cement S	252.20 (100%)	-	-	-	252.20 (100%)
	Cement SF1	481.00 (100%)	-	0.029 (0%)	0.010 (0%)	481.04 (100%)
	Cement SF2	383.50 (100%)	0.021 (0%)	0.014 (0%)	0.0049 (0%)	383.54 (100%)
II	Cement Portland	403.01 (100%)	0.060 (0%)	-	-	403.07 (100%)
	Portlandcement A	204.10 (100%)	-	-	-	204.10 (100%)
	Portlandcement NL2	383.50 (100%)	-	-	-	383.50 (100%)
	Portlandcement NL3	91.78 (100%)	-	-	-	91.78 (100%)
III	Cement Hoogoven I	65.86 (100%)	-	-	-	65.86 (100%)
	Cement blast furnace slag	142.48 (100%)	0.13 (0%)	-	-	142.61 (100%)
	Blastfurnace slag cement NL1	110.50 (100%)	-	-	-	110.50 (100%)
	Blastfurnace slag cement NL2	51.87 (100%)	-	-	-	51.87 (100%)
IV	Cement Portlandash	302.38 (100%)	0.040 (0%)	-	-	302.42 (100%)

TABLE 6. Characterisation of the different types of cement in terms of the regional effect of eutrophication (in milligrams of equivalent PO₄ per kg of cement)

6. Other characterised environmental impacts stemming from minor emissions

The results shown in [6] demonstrate the existence of other emissions that, though of lesser magnitude, may have a significant impact on some impact categories. This section examines some of these that have both regional implications, such as the photochemical ozone formation (summer smog), and local implications, such as heavy metals or carcinogens. These have been characterised using the factors in Table 8.

It is important to note that these emissions stem mainly from energy-producing processes, in particular electricity production and the refining of primary fuels (petroleum, coal, etc.). These, despite the environmental effects that they entail within the system boundaries of cement manufacture (cradle to gate), generally affect areas that are not local to the cement plant.

The reference units for these impact categories are equivalent ethylene (C₂H₄) for the photochemical ozone formation (summer smog), equivalent benzo(a)pyrene (B(a)P) for carcinogens and equivalent lead (Pb) for heavy metals.

6.1. Photochemical ozone formation

The photochemical ozone formation (summer smog) depends on the presence in the troposphere of oxidizing photochemical substances, such as volatile organic compounds (VOCs) and carbon monoxide (CO). The effect of solar radiation on these substances gives rise to reactions between the oxidizing photochemical compounds and hydroxyl radicals (OH[•]), in presence of NO_x, resulting in the formation of tropospheric ozone (O₃).

Type	Cements	Dust	SO ₂	Soot	Total
I	Cement Portland I	10.00 (96%)	0.43 (4%)	0.0092 (0%)	10.43 (100%)
	Cement CH	0.30 (33%)	0.60 (67%)	-	0.90 (100%)
	Cement N	0.18 (21%)	0.67 (79%)	-	0.85 (100%)
	Portlandcement NL1	7.50 (99%)	0.08 (1%)	-	7.58 (100%)
	Cement S	0.16 (26%)	0.45 (74%)	-	0.61 (100%)
	Cement SF1	0.39 (38%)	0.63 (62%)	-	1.02 (100%)
	Cement SF2	0.33 (20%)	1.33 (80%)	-	1.66 (100%)
II	Cement Portland	0.24 (17%)	1.16 (83%)	-	1.40 (100%)
	Portlandcement A	0.17 (59%)	0.12 (41%)	-	0.29 (100%)
	Portlandcement NL2	0.19 (68%)	0.091 (32%)	-	0.28 (100%)
	Portlandcement NL3	79.60 (99%)	0.97 (1%)	-	80.57 (100%)
III	Cement Hoogoven I	10.00 (95%)	0.51 (5%)	0.010 (0%)	10.52 (100%)
	Cement blast furnace slag	0.084 (13%)	0.58 (87%)	-	0.66 (100%)
	Blastfurnace slag cement NL1	0.14 (82%)	0.031 (18%)	-	0.17 (100%)
	Blastfurnace slag cement NL2	88.60 (99.5%)	0.43 (0.5%)	-	89.03 (100%)
IV	Cement Portlandash	0.18 (17%)	0.90 (83%)	-	1.08 (100%)

TABLE 7. Characterisation of the different types of cement in terms of the local impact of winter smog (in g of equivalent SPM per kg of cement)

Table 9 shows the results of these impacts, measured in mg of equivalent C₂H₄ per kg of cement. The results are highly scattered, and correlation with the cement type or definition of representative values is impossible. This fact can again be attributed, at least in part, to the criteria utilised or to the definition of the system boundaries in each case. However, it could also depend, in a decisive way, on the fuels utilised in the manufacture of clinker, some of which may lead to these sorts of emissions

It can be seen in Table 9 that there are cements whose inventories do not include the information corresponding to ozone formation (summer smog), which again calls into question

the rigour with which some of the existing inventories were designed. Furthermore, Cement SF1 (367 mg of equivalent C₂H₄ per kg of cement) and Cement blast furnace slag (364 mg of equivalent C₂H₄ per kg of cement) have values an order of magnitude higher than the rest and it is impossible to define representative values for the cements studied. The best explanation for the degree of variation shown is that the results considered in Table 9 are highly dependent on the energy sources of the system and additional information on the processes that supplied power to the cement production system is needed.

Emission	Ozone formation	Heavy metals	Carcinogens
Aldehydes	0.443	--	--
Arsenic	--	--	0.044
Benzene	0.189	--	0.00044
Benzo(a)pyrene	--	--	1.0
Cd (cadmium)	--	50	--
Cr (chromium)	--	0.2	--
CH ₄ (methane)	0.007	--	--
C _x H _y	0.398	--	--
Ethylbenzene		--	--
Phenol		0.761	--
Fluoroethane		--	--
Hg		--	1.0
Ni		--	--
PAHs		0.761	--
Pb		--	1.0
VOC		0.398	--

TABLE 8. Characterisation factors for other emissions that affect the impact categories of photochemical ozone formation, heavy metals and carcinogens.

6.2. Heavy metals and carcinogens

Any metal whose specific weight is higher than that of titanium (4.51gr/cm³) is considered to be a heavy metal. These are found in small quantities in raw materials such as crude oil, rock and coal. As not all the heavy metals necessarily have adverse effects on health and not all of the harmful ones have the same implications, one must use characterisation factors to analyse their effect (Table 8).

Based on the inventories used, it is suggested that these emissions originate from the energy-producing systems, as there is no evidence that they are included in the raw materials used to make cement. The highly scattered results (very different orders of magnitude) make it impossible to assign a representative value to the cement (independent of its type), since such a value depends on the type of fuels utilised, both in the energy production and in the clinker furnace.

The results for Cement CH (4.01 mg of equivalent Pb per kg of cement) are surprisingly high. This result is either an undetected error inherent to the inventory, or the consequence of using fuels with extremely high contents in heavy metals.

As for the carcinogens, the same general comments can be made as for the heavy metals in terms of the origin of the emissions. As these

results are significantly scattered and vary by orders of magnitude it is impossible to define representative values.

7. Conclusions

The characterisation of the environmental impact of manufacturing 1kg of a variety of cements, undertaken according to the LCA methodology, have led to the following conclusions:

- The errors and ambiguities of system boundaries as described in Reference [6] have again been observed. This is logical, as characterisation is a phase that takes place after an inventory is made, and which works from the environmental interventions stated in the latter. Consequently, inventories should be defined consistently, and their system boundaries must be adequately defined, structured and described.
- The contribution of carbon dioxide (CO₂) to the greenhouse effect ranges between 98.8 and 100% of the total—it is the main cause. The influences of other gases (methane, CH₄ or nitrous oxide, N₂O), are much smaller. Quantitatively, CO₂ emissions are significant and range in the order of 800 g of CO₂ in the production of 1kg of Type I cement.

Type	Cements	Regional	Local	
		Formation of ozone (mg equiv. C ₂ H ₄)	Carcinogens (mg equiv. B(a)P)	Heavy metals (mg equiv. Pb)
I	Cement Portland I	14.90	0.000021	0.0058
	Cement CH	-	0.0011	4.01
	Cement N	53.50	0.00034	0.53
	Portlandcement NL1	1.19	-	-
	Cement S	53.50	0.00034	0.53
	Cement SF1	367.00	0.0046	0.11
	Cement SF2	6.33	0.0014	0.38
II	Cement Portland	174.00	-	-
	Portlandcement A	95.50	0.00015	0.12
	Portlandcement NL2	-	-	0.013
	Portlandcement NL3	8.68	-	-
III	Cement Hoogoven I	12.70	0.000022	0.0059
	Cement blast furnace slag	363.00	-	-
	Blastfurnace slag cement NL1	-	-	0.013
	Blastfurnace slag cement NL2	3.74	-	-
IV	Cement Portlandash	182.00	-	-

TABLE 9. Characterisation of the different types of cement in terms of other categories of environmental impact considered.

- Acidification is mainly caused by SO₂ and NO_x emissions. The total acidification (in g of equivalent SO₂) depends on the type of cement (its content in clinker). These values range from 2-3 (Type I), 1-2 (Type II) and <1 (Types III and IV). NO_x emissions are the prime source of acidification, while the effect of HCl and NH₃ is practically negligible.
- The main cause of eutrophication is the emission of NO_x. The remainder of the emissions had a negligible effect on this environmental impact. The results for Type I was 250-350 mg of equivalent PO₄, whereas for Type II the values were 125-250 and for Type III, 50-125. These results mean that a cement plant that produces 1 million tonnes a year also produces a phosphorus load of approximately 0.5 kg per hectare (assuming an influence distance of about 35 km – 20 miles - surrounding the cement plant).
- For winter smog (small dust particles in suspension in the air), the main sources are SO₂, dust and soot. The results show that emissions of soot have a negligible effect and that there is a great disparity in the inventoried influences of SO₂ and dust (in percentage terms).
- In the cases of photochemical ozone formation (summer smog), heavy metals and

carcinogens, the results are highly variable and depend on the fuels and raw materials used. In most cases, emissions stem in the main from energy-producing processes and in particular the production of electricity and the refining of primary fuels (crude oil, coal, etc.). Thus, despite the environmental loads that are implied within the boundaries of the system of cement production, the processes correspond to zones that are likely not to be local to the cement plants themselves.

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