

NUMERICAL SIMULATION OF GLUEY PARTICLES

ALINE LEFEBVRE¹

Abstract. We propose here a model and a numerical scheme to compute the motion of rigid particles interacting through the lubrication force. In the case of a particle approaching a plane, we propose an algorithm and prove its convergence towards the solutions to the gluey particle model described in [B. Maury, *ESAIM: Proceedings* **18** (2007) 133–142]. We propose a multi-particle version of this gluey model which is based on the projection of the velocities onto a set of admissible velocities. Then, we describe a multi-particle algorithm for the simulation of such systems and present numerical results.

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1. INTRODUCTION

Slurries, lava's flows or red cells in blood are systems made of rigid particles embedded in viscous fluids (if we consider as a first approximation that red blood cells are rigid). Such systems can also be found in industry: concrete, paper pulp or some food industry products. These systems present varieties of noticeable rheological behaviours, whose study has been the subject of a great amount of researches, with contributions coming from engineering, chemistry, physics or mathematics. The basic problem is to predict macroscopic transport properties of these suspensions – viscosity, settling velocity – from microstructures, that is to say, from the interactions between particles and from their spatial configuration.

In case of dilute suspensions, theoretical results come from neglecting near field interactions. For example, in 1906, Einstein proposed an asymptotic formula for the apparent viscosity of dilute suspensions in [10,11]. In that case, apparent viscosity only depends on the solid volume fraction. Unfortunately, agreement between such asymptotic results and experiments generally fails as soon as the solid fraction reaches a few percent. For higher solid fractions, near field interactions can not be neglected anymore and it becomes essential to take them into account. Note that, the problem of the behaviour of neighbouring particles also appears in the study of the fluid/particle system of equations modelling suspensions of particles. For example, existence of solutions to these equations has been proved as long as the distance between the particles remains strictly positive (see for example [9,33,34]). Global weak solutions have also been constructed in [12,29], supposing that solids stick after contact. However, nothing is said concerning the possibility that such a contact may occur in finite time.

The interactions between solids embedded in a viscous fluid are due to lubrication forces: for the solids to get very close, the fluid must be evacuated from the narrow gap between them, which creates a force penalizing

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¹ Laboratoire de Mathématiques, Université Paris-Sud, 91405 Orsay Cedex, France. aline.lefebvre@math.u-psud.fr

their relative motion. This force is singular in the distance and this singularity is sufficient to avoid contacts. Indeed, it has been proved in [14] that in two dimensions, a smooth particle embedded in a viscous fluid following Navier-Stokes equations can not touch a plane in finite time. This behaviour can be recovered in three-dimensions from the asymptotic expansion of the lubrication force:

$$\mathbf{F}_{\text{lub}} \sim -6\pi\mu r^2 \frac{u}{d}, \quad (1.1)$$

where μ is the viscosity of the fluid, r the radius of the particle, u its velocity and d the distance between the particle and the plane. This expansion is obtained in [7] from the exact solution in three-dimensions to the Stokes problem outside a sphere with no-slip boundary condition, and in the limit $d \ll r^2$, though the fluid is assumed to be a continuum. It has to be noticed that this expansion is valid for perfectly smooth surfaces. Using this first order approximation, we can write the Fundamental Principle of Dynamics for a particle of mass m submitted to an external force per unit mass f :

$$m\ddot{d}(t) = -6\pi\mu r^2 \frac{\dot{d}}{d} + mf(t), \quad (1.2)$$

and the fact that the maximal solution to this ODE is global and never goes to zero (contact) in finite time comes from the Cauchy-Lipschitz theorem. Similarly, in case of a fixed sphere of radius r_1 and another sphere of radius r_2 moving at velocity \mathbf{V} along the axe of the centers, the first term of the development of the lubrication force exerted on the moving particle is (see [6]):

$$\mathbf{F}_{\text{lub}} \sim -6\pi\mu \frac{r_1^2 r_2^2}{(r_1 + r_2)^2} \frac{\mathbf{V}}{d}, \quad (1.3)$$

and no contact can occur in finite time.

However, from our experience, we know that the particle should touch the plane in finite time. One of the reasons explaining this behaviour is that physical particles are not smooth. The problem of modelling rough surfaces motivated a great amount of research, in various domains. For example, in case of flows above a rough plane, experimentations and asymptotic expansions [28,35], homogenization tools [1,5] as well as Molecular Dynamics simulations [3] have been used to understand better the boundary condition to impose on the plane to model its roughness. It has been shown that one had to use slip boundary conditions on the plane, which is equivalent, in case of shear flow, to consider a shifted plane with no-slip boundary conditions. Unfortunately, understanding the behaviour of the lubrication force in case of rough solids is much more delicate. A heuristic model has been proposed in [31], saying that the lubrication force exerted on a rough particle is the one would be exerted on a shifted smooth particle:

$$\mathbf{F}_{\text{lub,rough}} \sim -6\pi\mu r^2 \frac{u}{d + d_s}, \quad (1.4)$$

where $d_s > 0$ is the length of shift. In that article, the authors suggested to take $d_s = r_s$, where r_s is the size of roughness. The existence of a shift has been confirmed by experiments [2,18]. It was also obtained using asymptotic expansions in [19], but for large distances only. More recently, thanks to experimental devices allowing to measure distances as small as roughness size, it has been shown in [36] that d_s was strictly lower than r_s . Note that, as in the smooth case, it can be proved from (1.4), that the equivalent smooth sphere can not undergo contact with the plane ($d + d_s$ doesn't go to zero in finite time). However, the real surfaces can collide (d can go to zero).

This lubrication force, while acting at microscopic level, can be very important for the macroscopic behaviour of the global system, especially in case of high density of particles. Even for Stokes flows, it induces complexity and nonlinearity. This complex link between microscopic and macroscopic levels makes it difficult to obtain

theoretical results and studying these systems requires numerical simulations. Lots of numerical tools have been developed to simulate smooth particles embedded in a Newtonian fluid. In case of dense suspensions, both far-field and near-field interactions are essential to obtain relevant simulations. For example, Stokesian Dynamics Simulations (see [4]) are based on asymptotic expansions of both long-range and short-range hydrodynamic interactions in shear flows. In this article, we are interested in another class of methods which are direct numerical simulations. They consist in solving the coupled fluid/rigid problem without any model or approximation apart from time and space discretizations. They are divided into two classes : the first one relies on a conforming mesh of the fluid domain (see *e.g.* [15,16,23]) and the second one is based on an embedding of the solid phase in a global domain covered by a cartesian mesh (see *e.g.* [13,20,27,30]). These methods enable to take into account the many-body character of the hydrodynamic interaction forces. However, because of space discretization it becomes difficult to solve the fluid in the narrow gap between neighbouring particles and to take into account with accuracy the lubrication forces. As a consequence, even if the particles are supposed to be smooth, numerical contacts can be observed in such simulations and physical reasons as well as numerical robustness make it necessary to develop specific technics to deal with these contacts.

A first idea to solve this problem is to search for a strategy allowing an accurate computation of the lubrication forces. In [15], a method based on local refinements of the space and time meshes is proposed, so that the lubrication force in the interparticle gap is taken into account with accuracy and prevents overlappings. However, the number of refinements needed is not known *a priori* and the method can become computationally heavy. Consequently, less time-consuming methods have been developed. Some of them consist in adding a short range repulsive force (see [13,27] or [37]). In [23] a minimizing algorithm is used to impose a minimal distance between the particles while, in [30], the particles are allowed to undergo slight overlappings and an elastic repulsive force is added when such overlappings are detected. All of these methods ensure numerical robustness but introduce new parameters and do not take into account the underlying physics. Another approach is to use inelastic collisions, taking advantage of what has been done for numerical simulations of granular media (see [32] for a review of numerical methods to handle rigid-body contacts in granular flows). This idea has been proposed in [16] in order to impose a minimal distance between the particles. In [24], a scheme for inelastic collisions, based on a global projection step of the velocities, has been developed for granular flows and makes it possible to handle lots of particles. This scheme has been coupled with a fluid/particle solver in [20], to avoid contacts. More physical strategies, taking the lubrication force into account, have finally been proposed. Each of them relies on the asymptotic development of the lubrication force (1.3). In [8,26], it is shown that these lubrication forces are solution to a linear system. They are computed at each time step and added to the simulations. Unfortunately, this leads to stiff systems and, whereas it better takes into account the underlying physics, contact problems still occur because of the time discretization. In [22] a method is proposed to stabilize this problem by computing accurately sensible quantities such as the interparticle distances. However, a projection step is still needed for big time steps, in order to avoid overlappings.

The purpose of this article is to propose a strategy dealing simultaneously with contacts and lubrication forces. We restrict ourself here to the study of a gluey contact model which consists in modelling lubrication forces without taking far-field hydrodynamic interactions into account. This model is based on the gluey model for smooth particles described in [25], which consists in a vanishing-viscosity limit of (1.2). We propose an algorithm for this particle/plane model and prove its convergence. We show how the model and the algorithm can be extended to rough solids. Then, we generalize it to the multi-particle case. The numerical strategy is to combine the algorithm given for the plane/particle case with the scheme proposed in [24] for inelastic collisions in granular flows. While programming this multi-particle algorithm, we watched out for dealing with contacts efficiently in order to manage to simulate collections of many particles. Numerical simulations for few thousands of gluey particles are presented in the last section. Finally, to take both far-field and near-field hydrodynamic interaction forces into account, this gluey contact model has to be coupled with a fluid/particle solver. An example of such a coupling is given in Section 2.4 in the particle/plane case.

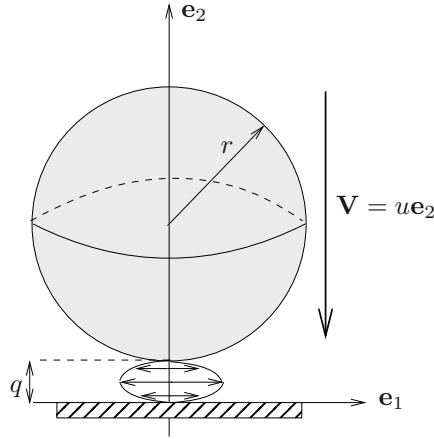


FIGURE 1. Notations.

2. SINGLE PARTICLE ABOVE A PLANE

2.1. The gluey particle model

We consider a three-dimensional smooth spherical particle moving perpendicularly to a plane (see Fig. 1). Its velocity and radius are denoted by \mathbf{V} and r respectively. Its distance to the plane is q .

The gluey particle model has been proposed in [25]. It describes, from a macroscopic point of view, the behaviour of the system near contact. It is built as the vanishing viscosity limit of the lubrication model (1.2) and relies on two states, glued ($q = 0$) or unglued ($q > 0$). These states are described by a new variable γ which stands for an adhesion potential: the more γ is negative, the more the solids are glued.

We denote by $I =]0, T[$ the time interval. The functional space $W^{1,\infty}(I)$ is the Sobolev space of functions in $L^\infty(I)$ whose time derivative is also in $L^\infty(I)$. $BV(I)$ is the space of functions in $L^\infty(I)$ with bounded variation on I . We define the dual space $\mathcal{M}(I) = (\mathcal{C}_c(I))'$ where $\mathcal{C}_c(I)$ is the space of continuous functions with compact support. To finish with notations, Π_K is the projection operator from \mathbb{R} onto $K \subset \mathbb{R}$.

The unknowns q and γ belong to the following functional spaces:

$$q \in W^{1,\infty}(I), \quad \dot{q} \in BV(I), \quad \gamma \in BV(I),$$

and the initial conditions are:

$$q(0) = q^0 > 0, \quad \dot{q}(0) = u^0, \quad \gamma(0) = 0.$$

In order to be able to generalize the model to the multi-particle case, we use the following second order ODE formulation of the gluey particle model proposed in [25]:

$$\dot{q}(t^+) = \Pi_{\mathcal{C}_{q,\gamma}(t)} \dot{q}(t^-), \tag{2.1}$$

$$m\ddot{q} = mf + \lambda \text{ in } \mathcal{M}(I) = (\mathcal{C}_c(I))', \tag{2.2}$$

$$\text{supp}(\lambda) \subset \{t, q(t) = 0\}, \tag{2.3}$$

$$\dot{\gamma} = -\lambda, \tag{2.4}$$

$$q \geq 0, \quad \gamma \leq 0, \tag{2.5}$$

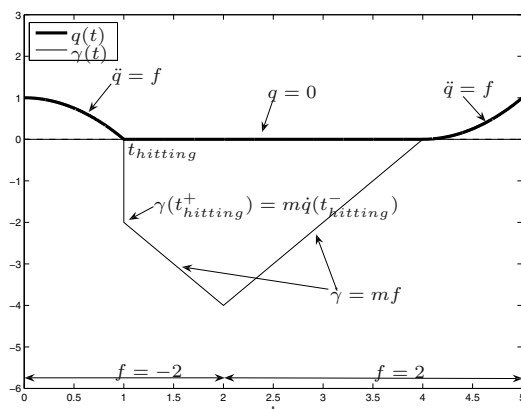


FIGURE 2. Example of solution to the gluey particle model.

where $C_{q,\gamma}(t)$ is the set of admissible velocities at time t :

$$C_{q,\gamma}(t) = \begin{cases} \{0\} & \text{if } \gamma(t^-) < 0, \\ \mathbb{R}^+ & \text{if } \gamma(t^-) = 0, \quad q(t) = 0, \\ \mathbb{R} & \text{else.} \end{cases}$$

Remark 2.1. In this formulation, \dot{q} and γ are supposed to be in $BV(I)$. In order to alleviate the notations, their differential measures have been denoted by \ddot{q} and $\dot{\gamma}$ respectively.

The behaviour of the solutions to this problem is the following. By (2.2) and (2.3), q is solution to $\ddot{q} = f$ while there is no contact ($q > 0$). Suppose a collision occurs at time t_0 , we have $\dot{q}(t_0^-) < 0$ and $\gamma(t_0^-) = 0$. Then $C_{q,\gamma}(t_0)$ is \mathbb{R}^+ and (2.1) gives $\dot{q}(t_0^+) = 0$. By (2.2), we obtain that, in the sense of distributions, λ identifies to the Dirac mass at time t_0 weighted by the velocity jump $m(\dot{q}(t_0^+) - \dot{q}(t_0^-)) = -m\dot{q}(t_0^-)$. This, together with (2.4) finally gives that γ is initialized to the value $m\dot{q}(t_0^-) < 0$. From then, while γ remains strictly negative, $C_{q,\gamma}$ is reduced to $\{0\}$ and, combining this with (2.1) gives that there is adhesion between the solids ($q = 0$). During this adhesion, \ddot{q} is zero and therefore, (2.4) associated to (2.2) gives $\dot{\gamma} = mf$. By definition of $C_{q,\gamma}$, the particle is allowed to take off when γ is back to zero. An example of such a behaviour is given in Figure 2, where the particle is pushed towards the plane until time 2 and then pulled away from it.

Remark 2.2. In [25], the author shows that, if we denote by d_μ the solution to the three-dimensional lubrication model (1.2) (where each constant is set to 1 except the viscosity):

$$\ddot{d}_\mu(t) = -\mu \frac{\dot{d}_\mu}{d_\mu} + f(t)$$

and if we set $\gamma_\mu = \mu \ln(d_\mu)$, the pair (d_μ, γ_μ) converges, when μ goes to zero, to (q, γ) solution to

$$\begin{cases} \dot{q} + \gamma = u^0 + \int_0^t f(s) ds, \\ \gamma \leq 0, \quad q \geq 0, \quad q\gamma = 0, \\ q(0) = q^0, \quad \dot{q}(0) = u^0. \end{cases} \quad (2.6)$$

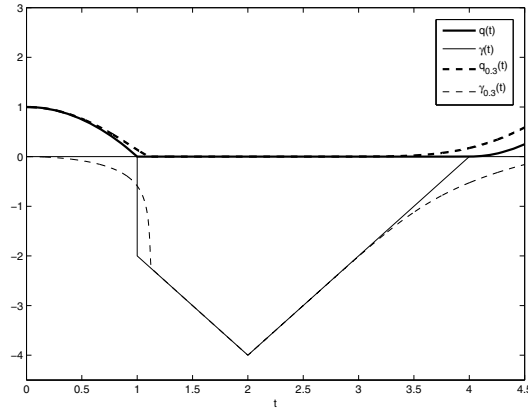


FIGURE 3. A vanishing-viscosity model.

Because of non-uniqueness of the solution to this limit problem (see [25] for a counter example), this convergence is given up to a subsequence. However, in case q has a finite number of zeros, the limit model admits a unique solution and therefore the whole sequence (d_μ, γ_μ) converges to (q, γ) . This hypothesis is verified if the external force f changes of sign a finite number of times, which is true in the test proposed in Figure 2. The convergence for that example is illustrated in Figure 3. Note that this asymptotic model (2.6) can be obtained from any lubrication model

$$\ddot{d}_\mu(t) = -\mu \dot{d}_\mu \varphi(d_\mu) + f(t)$$

where $d \mapsto \varphi(d) > 0$ and $\int_d^1 \varphi \rightarrow +\infty$ when d goes to zero. For example, the two-dimensional lubrication force, for which $\varphi(d) = 1/d^{-3/2}$ fits into this framework. Modelling gluey particles using a model that does not depend on the lubrication model and on the viscosity of the underlying fluid may be quite surprising. This unphysical behaviour will be improved in Section 2.5, when modelling roughness (see Rem. 2.15).

Remark 2.3. The second order ODE formulation (2.1)–(2.5) is formally equivalent to (2.6). Moreover, in case q has a finite number of zeros, it can be shown that (2.1)–(2.5) and (2.6) are equivalent, in the sense that a solution to one of the problem is also solution to the other (the demonstration of this result can be found in [21], p. 223).

Note that the constraint $q\gamma = 0$ is not needed anymore in (2.1)–(2.5): it can be checked that it is automatically verified using (2.3) together with the fact that γ is initialized to zero. To the contrary, the additional constraints (2.5) are necessary. Indeed, suppose that t_1 is an unsticky contact time ($q(t_1) = 0$, $\gamma(t_1^-) = 0$, $\dot{q}(t_1^-) = 0$). If the force is negative after this instant and if we do not impose $q \geq 0$, then $\gamma \equiv 0$ and $\dot{q}(t) = \int_{t_1}^t f(s)ds$ is a solution to the problem and the particle can enter the wall. Similarly, if the force is positive and if the constraint $\gamma \geq 0$ is not imposed, $q \equiv 0$ and $\gamma(t) = m \int_{t_1}^t f(s)ds$ is a solution and γ can become strictly positive.

Before proposing an algorithm to compute the solutions to this model, we make a few remarks about its interpretation and its physical relevance.

Remark 2.4 (physical interpretation). As already mentioned, a smooth particle embedded in a Newtonian fluid never touches the plane in finite time. In the context of the gluey particle model, the variable q can be seen as a macroscopic distance between the solids: it is equal to zero as soon as the solids are near contact. The new variable γ , which is obtained as the limit of $\gamma_\mu = \mu \ln(d_\mu)$, stands for the microscopic distance.

To understand the behaviour of the gluey particle system presented in Figure 2, one can consider a rigid ball falling on a table coated with a viscous fluid like honey. When the particle reaches the layer of fluid,

it instantaneously sinks in it and the depth it reaches is linked to the impact velocity. From then, the ball is glued to the layer of fluid, the macroscopic contact begins, q is set to zero and γ stores the impact velocity. As long as it is pushed, the particle sinks deeper in the fluid and gets closer to the plane (γ decreases). Then the particle is pulled. From that moment on, it smoothly moves back from the fluid (γ increases) and comes unstuck from the layer of fluid when the pulling forces have balanced the impact velocity and the pushing forces (γ reaches zero).

Note that, from (2.2), λ can be interpreted as an additional force, exerted by the plane on the particle, in order to satisfy the constraint (2.1). It follows from (2.3) that the plane is allowed to act on the particle through this force only if they are in macroscopic contact.

Remark 2.5 (radius). This gluey particle model is built in [25] as the vanishing viscosity limit of the lubrication model (1.2) where each constant except the viscosity is taken equal to 1. Taking all constants into account leads to define γ as the limit of $\gamma_\mu = 6\pi\mu \ln(d_\mu)$ and the equation governing its evolution becomes

$$\dot{\gamma} = -\frac{1}{r^2}\lambda. \quad (2.7)$$

The larger r is, the less the microscopic distance γ varies (the more it is difficult for the particle to move). Note that, provided we are only interested in the macroscopic trajectory q of the particle, the previous model (2.1)–(2.5) was valid for any radius: these trajectories only depend on the sign of γ (and not its value) which is independent of r from (2.7).

Remark 2.6 (viscous or not viscous?). Since this model is built by letting the viscosity go to zero, one may wonder whether it models viscous fluids or not. First, in our limit model, sticky collisions occur (q can reach zero), whereas smooth solids in viscous fluids can not collide. This does not limit the model, since q stands for a macroscopic distance. The fact that the lubrication forces continue to act on the solids during the macroscopic contact is taken into account through γ . The point is to know whether q reflects the macroscopic behaviour of a smooth particle embedded in a viscous fluid. To answer to this question, we consider the same experiment as in Figure 2 (pushing until time 2 and then pulling) for a particle falling on a plane coated with different viscous fluids. In Figure 4, we compare the trajectory given by the gluey particle model to the trajectories computed for these systems where the viscous fluid layer is modeled by (1.2). Of course, trajectories converge to the limit model when the viscosity goes to zero. We also observe that, from a macroscopic point of view, as long as we are interested in hitting and unsticking times, the limit model seems to agree with all trajectories. As a matter of fact, in case of smooth solids and from this macroscopic point of view, what is important is not the viscosity of the fluid but whether it is viscous or not. However, it has to be pointed out that, for small viscosities, the distances can become very small and reach domains wherein the lubrication formula (1.1) is no longer valid (fluid assumed to be a continuum, solids supposed to be smooth). Consequently, our model being based on this expansion, it shall be employed to represent the macroscopic behaviour of very viscous systems for which distances are not too small.

2.2. Numerical algorithm

We propose here an algorithm for problem (2.1)–(2.5). Let $h = T/N$ be the time step. The problem is initialized to $q^0 > 0$, $u^0 \in \mathbb{R}$ and $\gamma^0 = \lambda^0 = 0$. We denote by q^n , u^n , γ^n and λ^n the computed values of q , u , γ and λ at time t^n . We define f^n by $f^n = \frac{1}{h} \int_{t^n}^{t^{n+1}} f(s) ds$. We have to compute q^{n+1} , u^{n+1} , γ^{n+1} and λ^{n+1} .

In order to compute u^{n+1} and λ^{n+1} , we define the discrete counterpart of $C_{q,\gamma}(t^n)$ the following way:

$$\left| \begin{array}{l} K(q^n, \gamma^n) = \{v, q^n + hv \geq 0\} \text{ if } \gamma^n = 0, \\ K(q^n, \gamma^n) = \{v, q^n + hv = 0\} \text{ if } \gamma^n < 0. \end{array} \right.$$

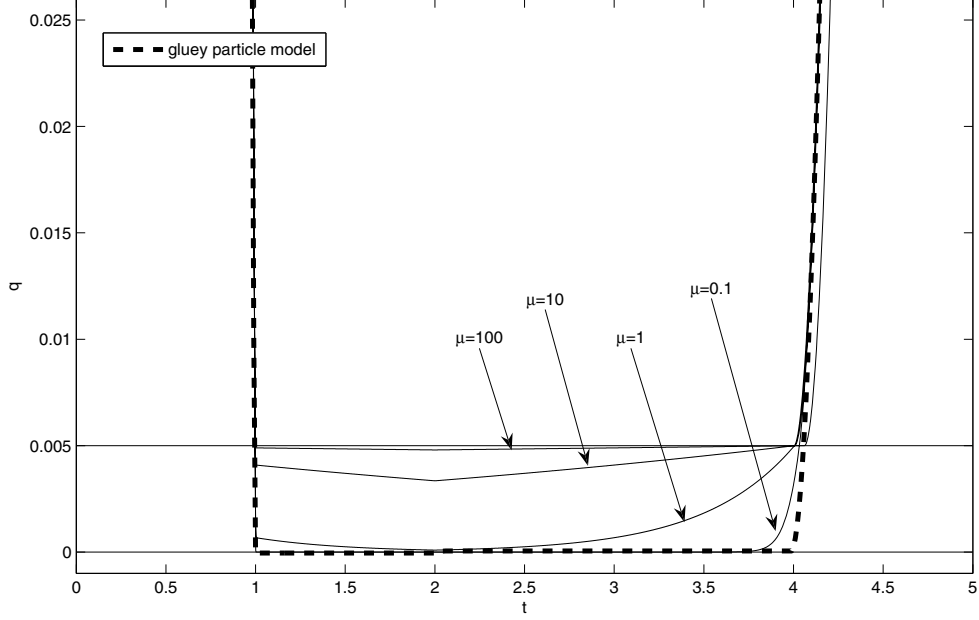


FIGURE 4. Comparison gluey particle model/layer of viscous fluid.

$K(q^n, \gamma^n)$ is called the set of admissible velocities at time t^n . The collision law (2.1) and the Fundamental Principle of Dynamics (2.2) then become,

$$\begin{cases} u^{n+1/2} = u^n + hf^n, \\ u^{n+1} \in K(q^n, \gamma^n), \quad \frac{1}{2} |u^{n+1} - u^{n+1/2}|_m^2 = \min_{v \in K(q^n, \gamma^n)} \frac{1}{2} |v - u^{n+1/2}|_m^2, \end{cases}$$

where $(v, w)_m = (mv, w)$. Note that $u^{n+1/2}$ is the velocity the particle would have at time t^{n+1} if there were no plane. u^{n+1} is the projection of this *a priori* velocity on the set of admissible velocities $K(q^n, \gamma^n)$ for an adapted scalar product. From this projection step, arises a Lagrange multiplier, denoted by λ^{n+1} , and such that

$$m(u^{n+1} - u^{n+1/2}) = h\lambda^{n+1}.$$

This can be rewritten as

$$m \frac{u^{n+1} - u^n}{h} = mf^n + \lambda^{n+1}, \quad (2.8)$$

which is a discretization of (2.2). Note that, when $\gamma^n = 0$, λ^{n+1} is a Lagrange multiplier associated to an inequality constraint ($q^n + hu^{n+1} \geq 0$) and therefore, λ^{n+1} is positive.

Then, γ^{n+1} is given by an explicit Euler discretization of (2.4),

$$\gamma^{n+1} = \gamma^n - h\lambda^{n+1}.$$

This equation is valid while γ^{n+1} is negative. If it becomes strictly positive, it means that the particle has taken off at a time $t^* \in]t_n, t_{n+1}[$. In that instance, γ^{n+1}/m has integrated the force on $]t^*, t^{n+1}[$ instead of u^{n+1}

which was fixed to zero. Therefore, in that case, we modify u^{n+1} and γ^{n+1} the following way:

$$\text{if } \gamma^{n+1} > 0, \quad u^{n+1} = \gamma^{n+1}/m \text{ and } \gamma^{n+1} = 0.$$

Finally the position q^{n+1} is given by

$$q^{n+1} = q^n + hu^{n+1}.$$

To sum up, the algorithm is the following:

Algorithm 2.7 (particle/plane). *For all $n \geq 0$, let q^n , u^n , γ^n and λ^n be given. We define $f^n = \frac{1}{h} \int_{t^n}^{t^{n+1}} f(s)ds$.*

(1) *Computation of the a priori velocity, without taking the lubrication force into account*

$$u^{n+1/2} = u^n + hf^n.$$

(2) *Projection of the a priori velocity onto the set of admissible velocities,*

$$\bar{u}^{n+1} \in K(q^n, \gamma^n), \quad \frac{1}{2} \left| \bar{u}^{n+1} - u^{n+1/2} \right|_m^2 = \min_{v \in K(q^n, \gamma^n)} \frac{1}{2} \left| v - u^{n+1/2} \right|_m^2,$$

where $K(q, \gamma) = \{v, q + hv \geq 0\}$ if $\gamma = 0$,

$K(q, \gamma) = \{v, q + hv = 0\}$ if $\gamma < 0$.

From this projection step, we obtain λ^{n+1} .

(3) *Updating of γ ,*

$$\bar{\gamma}^{n+1} = \gamma^n - h\lambda^{n+1}.$$

(4) *Modification if unsticking,*

$$\begin{aligned} \text{if } \bar{\gamma}^{n+1} \leq 0, \quad u^{n+1} = \bar{u}^{n+1} \quad \text{and} \quad \gamma^{n+1} = \bar{\gamma}^{n+1}, \\ \text{if } \bar{\gamma}^{n+1} > 0, \quad u^{n+1} = \bar{\gamma}^{n+1}/m \quad \text{and} \quad \gamma^{n+1} = 0. \end{aligned}$$

(5) *Updating of q ,*

$$q^{n+1} = q^n + hu^{n+1}.$$

Remark 2.8 (coupling with fluid simulations). This algorithm simulates collections of gluey particles, where the lubrication force acts on the particles only if they are near to contact (macroscopic contact, $q = 0$). Let us now suppose that the particles are embedded in a viscous fluid. In that case, we have to take both short-range and long-range hydrodynamic interactions into account. To do so, a splitting method can be used to couple a fluid/particle solver with the gluey particle algorithm. We denote by \mathbf{u}^n and p^n the velocity and pressure fields into the fluid at time t^n . Let S be any fluid/particle solver: from \mathbf{u}^n , q^n and f^n , S computes the *a priori* velocities of the particles, without taking the lubrication force into account carefully. To couple the two algorithms we propose to modify step (1) of Algorithm 2.7 writing:

$$u^{n+1/2} = S(q^n, \mathbf{u}^n, f^n).$$

2.3. Convergence result

In this section, we establish a convergence result for the proposed algorithm. To do so, we are going to use the initial formulation of the gluey particle model (2.6):

$$\begin{cases} m\dot{q} + \gamma = m \left(\dot{q}(0) + \int_0^t f(s)ds \right), \\ q \geq 0, \quad \gamma \leq 0, \quad q\gamma = 0, \\ q(0) = q^0 > 0, \quad \dot{q}(0) = u^0. \end{cases}$$

We recall that h is the constant time step. We denote by q_h the piecewise affine function with $q_h(t^n) = q^n$. Similarly, γ_h is the piecewise affine function with $\gamma_h(t^n) = \gamma^n$. We denote by u_h the derivative of q_h , piecewise constant equal to u^{n+1} on $]t^n, t^{n+1}[$. Finally, we define $\lambda_h = -\dot{\gamma}_h$, piecewise constant. Note that, due to step (4), λ_h is generally not equal to λ^{n+1} on $]t^n, t^{n+1}[$. We will denote by $\tilde{\lambda}^{n+1} = -(\gamma^{n+1} - \gamma^n)/h$ its value on this interval. If the particle does not take off between times t^n and t^{n+1} , no modification is made during step (4) and we obtain $\tilde{\lambda}^{n+1} = \lambda^{n+1}$. The convergence theorem is the following:

Theorem 2.9. *Let f be integrable on $I =]0, T[$. When h goes to zero, there exists subsequences, still denoted by $(q_h)_h, (u_h)_h, (\lambda_h)_h$ and $(\gamma_h)_h, q \in W^{1,1}(I) \cap \mathcal{C}(I)$ and $\gamma \in BV(I)$ such that*

$$\begin{aligned} u_h &\longrightarrow u \text{ in } L^1(I), \\ q_h &\longrightarrow q \text{ in } W^{1,1}(I) \text{ and } L^\infty(I) \text{ with } \dot{q} = u, \\ \lambda_h &\overset{*}{\rightharpoonup} \lambda \text{ in } \mathcal{M}(I), \\ \gamma_h &\longrightarrow \gamma \text{ in } L^1(I) \text{ with } \dot{\gamma} = -\lambda, \end{aligned}$$

where (q, γ) is solution to (2.6).

Remark 2.10. Non-uniqueness for the limit problem (see Rem. 2.2) prevents from using the standard approach based on consistence and stability. Consequently, we use compactness methods and obtain convergence up to a subsequence. However, in case q has a finite number of zeros, the limit model admits a unique solution and therefore the convergence of the algorithm to problem (2.6) is proved. Moreover, in that case, since (2.1)–(2.5) and (2.6) are equivalent, Theorem 2.9 shows that Algorithm 2.7 converges to (2.1)–(2.5).

Remark 2.11. In Theorem 2.9 no hypothesis is made on the time steps: the result of convergence holds even if time steps do not reach hitting and unsticking times. In Figure 5 we consider again the case $f = -2$ on $[0, 2]$ and $f = 2$ on $[2, +\infty[$. The curves $t \rightarrow q(t)$ and $t \rightarrow \gamma(t)$ are obtained from the numerical solutions to Algorithm 2.7 for $dt = 0.03$. In that case, although hitting and unsticking times are not reached by the time steps, the numerical solutions can not be distinguished from the exact ones. Actually, the behaviour of the numerical algorithm is reasonable, even for large time steps, when the specific points can not be detected with accuracy. To illustrate this, we plot in Figure 5 the numerical solutions obtained for $dt = 0.63$. We suppose that the computation of f^n is exact for all n . We can observe that γ is exactly computed from time t^{n_1+1} and that the numerical trajectory is close to the exact one. The reason why it works is that the derivatives $\dot{\gamma}$ and \dot{q} are exactly computed, even if the specific points do not correspond to time steps. Indeed, let's denote by n_1 the numerical hitting time step ($n_1 = 2$ in our case). The particle hits the plane at $t = t^{n_1} > 1$. It is an easy computation to show that λ^{n_1} stores a part of the impact velocity and that, at the next time step, λ^{n_1+1} takes into account the missing part and is equal to $\lambda(t^{n_1+1})$. Then, for $n > n_1 + 1$ and as long as the contact exists, it is clear that $\lambda^n = \lambda(t^n)$. Consequently, although it takes two time steps long, the error on γ^n for $n \geq n_1 + 1$ is strictly caused by the Euler explicit discretization of $\dot{\gamma} = -\lambda$ (step 3 of Algorithm 2.7). In our case, since γ

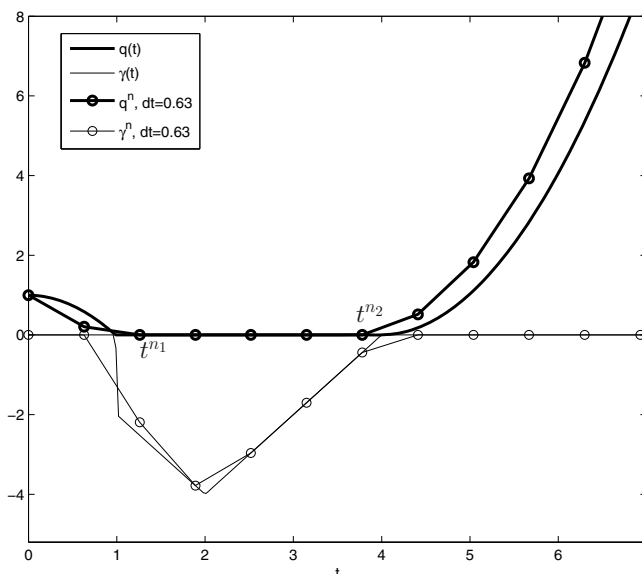


FIGURE 5. Behaviour of the numerical algorithm for large time steps.

is an affine function, it is computed exactly. Similarly, concerning the unsticking time, the velocity is exactly computed thanks to step 4: the particle unsticks at time $t^{n2} < 4$ with a corrected velocity and, as before, the exact value of the velocity is recovered at the following time step.

Proof of Theorem 2.9. To begin, note that a discrete form of the Fundamental Principle of Dynamics (2.2) is verified:

$$\forall n, \quad m \frac{u^{n+1} - u^n}{h} = m f^n + \tilde{\lambda}^{n+1}. \quad (2.9)$$

Indeed, in case the particle does not take off between times t^n and t^{n+1} , the equality follows from (2.8), together with $\tilde{\lambda}^{n+1} = \lambda^{n+1}$. If the particle takes off, it comes from (2.8) and step 4 of the algorithm.

The proof will be divided into 4 steps.

(1) **Convergence of q_h and u_h**

Lemma 2.12. $(u_h)_h$ is bounded in $L^\infty(I)$.

Proof. In case the particle does not take off, the projection step (2) gives

$$|u^{n+1}| = |\bar{u}^{n+1}| \leq |u^{n+1/2}| \leq |u^n| + h|f^n|.$$

In the other case, it can be proved that $u^{n+1}\tilde{\lambda}^{n+1} \leq 0$ and combining this with (2.9) gives the same result. By summing up all these inequalities we obtain

$$|u^{n+1}| \leq |u^0| + \int_0^T |f|,$$

and the result follows from definition of u_h . □

Lemma 2.13. $(u_h)_h$ is bounded in $BV(I)$.

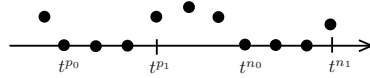


FIGURE 6. Proof of Lemma 2.13: notations.

Proof. By Lemma 2.12, the result will follow provided we prove $\text{Var}(u_h)$ is bounded independently from h , where

$$\text{Var}(u_h) = \sum_{n=1}^{N-1} |u^{n+1} - u^n|.$$

To check this, we first split the sum and consider the sums between indexes p_1 and n_1 where t^{p_1} and t^{n_1} are successive unsticking times (see Fig. 6):

$$\text{Var}_{[t^{p_1}, t^{n_1}]}(u_h) = \sum_{n=p_1}^{n_1-1} |u^{n+1} - u^n|.$$

The total variation of u_h is made of a sum of such terms.

The idea behind the above decomposition is that, at each unsticking time t^{p_1} , the velocity of the particle is small and that its variations over $[t^{p_1}, t^{n_1}]$ only depend on the integral of f over the same interval. These terms will be summed up to obtain a bound on the total variation.

More precisely, the bound for $\text{Var}_{[t^{p_1}, t^{n_1}]}(u_h)$ can be found by analysing each jump $|u^{n+1} - u^n|$, paying attention to what happens at time t^n (hitting time, sticking time, unsticking time).

First, note that the particle can stick to the plane during a single time step ($n_1 = n_0 + 1$) or during more than one instant ($n_1 > n_0 + 1$ and $u^n = 0$ for $n \in [n_0 + 1, n_1 - 1]$). In both of these cases, we can show that

$$\text{Var}_{[t^{p_1}, t^{n_1}]}(u_h) \leq \sum_{n=p_1}^{n_0-2} |u^{n+1} - u^n| + 2|u^{n_0}| + |u^{n_0-1}| + |u^{n_1}|. \quad (2.10)$$

To obtain a bound on the variation of u_h , it remains to bound each term in the right-hand side of this inequality. First, for $n \in [p_1, n_0 - 2]$, the constraint is not activated when computing u^{n+1} and therefore $\tilde{\lambda}^{n+1} = \lambda^{n+1} = 0$. From this, together with (2.9), we have

$$p_1 \leq n \leq n_0 - 2 \implies |u^{n+1} - u^n| = h|f^n|.$$

Then, we study u^{n_1} , which corresponds to an unsticking time. Combining (2.9) with the fact that $u^{n_1} \tilde{\lambda}^{n_1} \leq 0$ and with $u^{n_1} > 0$ we obtain

$$u^{n_1} \leq u^{n_1-1} + hf^{n_1-1}.$$

In the case the particle only sticks to the plane during a single time step, u^{n_1-1} is negative. On the other case, u^{n_1-1} is zero. In both cases, we can write

$$0 < u^{n_1} \leq hf^{n_1-1}.$$

To finish, it remains to study u^{n_0} and u^{n_0-1} . Using the fact that, for all n , $|u^{n+1}| \leq |u^n| + h|f^n|$ (see previous lemma) we obtain

$$|u^{n_0}| \leq |u^{p_1}| + \sum_{n=p_1}^{n_0-1} h|f^n|.$$

Since p_1 is an unsticking time, the same argument as the one we used for u^{n_1} gives $0 < u^{p_1} \leq hf^{p_1-1}$ and then

$$|u^{n_0}| \leq \sum_{n=p_1-1}^{n_0-1} h|f^n|.$$

Similarly, we have

$$|u^{n_0-1}| \leq \sum_{n=p_1-1}^{n_0-2} h|f^n|.$$

Putting these inequalities all together in (2.10) we finally prove

$$\text{Var}_{[t^{p_1}, t^{n_1}]}(u_h) \leq 4 \int_{t^{p_1-1}}^{t^{n_1}} |f(s)| ds.$$

Summing up all these contributions and the bounding terms, we obtain

$$\text{Var}(u_h) \leq u^0 + 8 \int_0^T |f(s)| ds,$$

and $\text{Var}(u_h)$ is bounded independently from h as required. \square

Lemma 2.13, together with the compact embedding of $BV(I)$ in $L^1(I)$ gives (up to a subsequence)

$$u_h \longrightarrow u \text{ in } L^1(I) \text{ with } u \in BV(I), \quad (2.11)$$

$$q_h \longrightarrow q \text{ in } W^{1,1}(I) \text{ with } \dot{q} = u.$$

Uniform convergence of q_h to q then follows from the continuous embedding of $W^{1,1}(I)$ in $L^\infty(I)$:

$$q_h \longrightarrow q \text{ in } L^\infty(I). \quad (2.12)$$

Finally, since q_h is positive, we have $q \geq 0$ everywhere.

(2) Convergence of γ_h

Lemma 2.14. $(\lambda_h)_h$ is bounded in $L^1(I)$.

Proof. By (2.9) and the fact that $\tilde{\lambda}^0 = 0$ we get

$$\int_0^T |\lambda_h| \leq m \text{Var}(u_h) + \|f\|_{L^1(I)}.$$

The result follows by combining this with Lemma 2.13. \square

By Lemma 2.14, $(\lambda_h)_h$ is bounded in $\mathcal{M}(I)$, which implies that there exists a subsequence and $\lambda \in \mathcal{M}(I)$ such that

$$\lambda_h \xrightarrow{*} \lambda \text{ in } \mathcal{M}(I).$$

Moreover, combining Lemma 2.14 with $\dot{\gamma}_h = -\lambda_h$ it comes that $(\gamma_h)_h$ is bounded in $BV(I)$. This, together with compact embedding of $BV(I)$ in $L^1(I)$, implies that there exists a subsequence and $\gamma \in BV(I)$ such that

$$\gamma_h \longrightarrow \gamma \text{ in } L^1(I) \text{ and a.e.} \quad (2.13)$$

Since γ_h is negative, it follows from this convergence result that so is γ . Finally, since $\dot{\gamma}_h = -\lambda_h$, we can check that $\dot{\gamma} = -\lambda$ in $\mathcal{M}(I)$.

(3) **Continuous FPD**

We are now going to prove that $m\dot{q} + \gamma = m \left(\dot{q}(0) + \int_0^t f(s)ds \right)$ almost everywhere on I .

In order to do so, the first step is to prove that (2.2) is verified in the sense of distributions. From (2.9) it follows that

$$\forall \varphi \in \mathcal{D}(I), \quad \langle m\dot{u}_h, \varphi \rangle = \sum_{n=1}^{N-1} mh f^n \varphi(t^n) + \sum_{n=1}^{N-1} h\tilde{\lambda}^{n+1} \varphi(t^n). \quad (2.14)$$

We are going to pass to the limit in this equation. By (2.11), $\langle m\dot{u}_h, \varphi \rangle$ converges to $\langle m\dot{u}, \varphi \rangle$. To study the first term of the right-hand side, we write

$$h \sum_{n=1}^{N-1} f^n \varphi(t^n) = \int_0^T f(s)\varphi(s)ds + \sum_{n=1}^{N-1} \int_{t^n}^{t^{n+1}} f(s) [\varphi(t^n) - \varphi(s)] ds - \int_{t^0}^{t^1} f(s)\varphi(s)ds.$$

The convergence to zero of the sum over n comes from uniform continuity of φ . Combining this with $|t^1 - t^0| = h$ gives

$$\sum_{n=1}^{N-1} mh f^n \varphi(t^n) \longrightarrow m \int_0^T f(s)\varphi(s)ds \text{ when } h \rightarrow 0.$$

The argument for the last term is similar. We write

$$\sum_{n=1}^{N-1} h\tilde{\lambda}^{n+1} \varphi(t^n) = \int_0^T \lambda_h(s)\varphi(s)ds + \sum_{n=1}^{N-1} \int_{t^n}^{t^{n+1}} \lambda_h(s) [\varphi(t^n) - \varphi(s)] ds - \int_{t^0}^{t^1} \lambda_h(s)\varphi(s)ds.$$

The convergence to zero of the sum over n comes from uniform continuity of φ and Lemma 2.14, and the last term is equal to zero for all h . This, together with Lemma 2.14 gives

$$\sum_{n=1}^{N-1} h\tilde{\lambda}^{n+1} \varphi(t^n) \longrightarrow \langle \lambda, \varphi \rangle = -\langle \dot{\gamma}, \varphi \rangle \text{ when } h \rightarrow 0.$$

Finally, passing to the limit in (2.14) we obtain

$$\langle m\ddot{q} - \dot{\gamma}, \varphi \rangle = \langle mf, \varphi \rangle, \quad \forall \varphi \in \mathcal{D}(I),$$

as required.

Then, by density of $\mathcal{D}(I)$ in $\mathcal{C}_0^0(I)$ and the fact that $m\dot{q} - \gamma$ is in $BV(I)$, we get

$$m\ddot{q} - \dot{\gamma} = mf \text{ in } \mathcal{M}(I).$$

Integrating this equality over $[0, t[$ (Stieltjes integral of BV functions) we obtain

$$(m\dot{q} - \gamma)(t^+) - (m\dot{q} - \gamma)(0^-) = \int_0^t mf,$$

and the result follows from this, by using $\gamma(0^-) = 0$ and a.e. continuity of $m\dot{q} - \gamma$.

(4) **Proof of $q\gamma = 0$**

To prove that (q, γ) is solution to (2.6), it remains to show that $q\gamma = 0$ almost everywhere. For all n we have $q^n \gamma^n = 0$. However, $q_h \gamma_h$ is not identically equal to zero. We build new functions \tilde{q}_h and $\tilde{\gamma}_h$, piecewise constant, with respective values q^n and γ^n on $]t^n, t^{n+1}[$. We now have $\tilde{q}_h \tilde{\gamma}_h = 0$ and simple computations give

$$\|\tilde{q}_h - q\|_{L^\infty(I)} \leq \|\tilde{q}_h - q_h\|_{L^\infty(I)} + \|q_h - q\|_{L^\infty(I)} \leq h \|u_h\|_{L^\infty(I)} + \|q_h - q\|_{L^\infty(I)}$$

and

$$\|\tilde{\gamma}_h - \gamma\|_{L^1(I)} \leq \|\tilde{\gamma}_h - \gamma_h\|_{L^1(I)} + \|\gamma_h - \gamma\|_{L^1(I)} \leq \frac{h}{2} \|\lambda_h\|_{L^1(I)} + \|\gamma_h - \gamma\|_{L^1(I)}.$$

Combining the first inequality with Lemma 2.12 and (2.12) gives uniform convergence of \tilde{q}_h to q . Putting together the second inequality, Lemma 2.14 and (2.13), we see that $\tilde{\gamma}_h$ converges to γ in $L^1(I)$ which implies that the sequence converges up to a subsequence almost everywhere on I . Finally, letting h go to zero in $\tilde{q}_h \tilde{\gamma}_h = 0$ gives $q\gamma = 0$ almost everywhere as required.

This completes the proof of Theorem 2.9. \square

2.4. Validation: coupling with a fluid/particle solver

We consider the experiment described in Section 2 and suppose there are no inertia. The radius and the mass of the particle are taken equal to 1 and the viscosity of the fluid is $\mu = 3$. The external force is $f(t) = -2$ until time 2 and $f(t) = 2$ if $t > 2$. The balance of forces on the particle reads

$$\forall t, \quad F_{\text{lub}}(q(t), u(t)) + f(t) = 0, \quad (2.15)$$

where $F_{\text{lub}}(q, u)$ is the lubrication force exerted on the particle situated above the plane at distance q , with velocity u .

2.4.1. Computation of a reference solution

To obtain a reference solution we have to solve (2.15) as accurately as possible. To do so, we first chose $\bar{u} = -1$ and write

$$u(t) = \alpha(t) \bar{u}.$$

Then, using the linearity of the lubrication force with respect to the velocity, (2.15) becomes

$$\alpha(t) F_{\text{lub}}(q(t), \bar{u}) + f(t) = 0. \quad (2.16)$$

To compute the solution of (2.16), we choose the following time discretization

$$\left| \begin{array}{l} q^n \text{ given,} \\ \alpha^{n+1} \text{ solution to } \alpha^{n+1} F_{\text{lub}}(q^n, \bar{u}) + f^n = 0, \\ u^{n+1} = \alpha^{n+1} \bar{u}, \quad q^{n+1} = q^n + h u^{n+1}, \end{array} \right.$$

where h is the constant time-step. These computations can be achieved, provided we know the map $q \rightarrow F_{\text{lub}}(q, \bar{u})$ for the given velocity $\bar{u} = -1$ and $q \in [0, 1]$.

In order to compute this map, we begin with computing $F_{\text{lub}}(q_k, \bar{u})$ where $(q_k)_{k=1 \dots M}$ is a regular subdivision of interval $[0, 1]$. This is done, for each q_k , solving the Stokes problem in the fluid with the Dirichlet boundary condition \bar{u} on the particle and then, computing the corresponding force $F_{\text{lub}}(q_k, \bar{u})$ exerted by the fluid on the particle. The computations are carried out in tree-dimensions using an axisymmetric formulation and the Finite-Element solver `FreeFem++`¹. On the left side of Figure 7, we plot the numerical results obtained (circles).

¹F. Hecht and O. Pironneau, <http://www.freefem.org>.

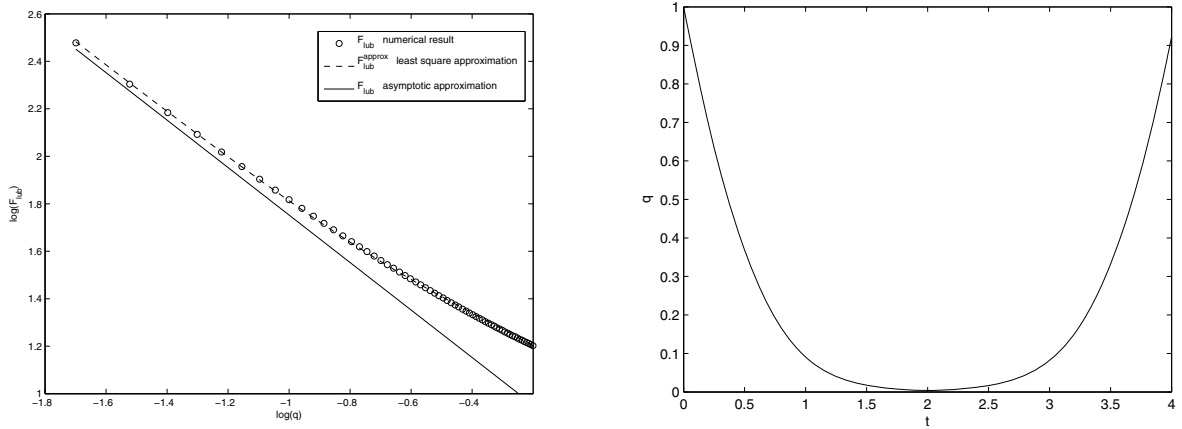


FIGURE 7. Approximation of the lubrication force (left) and reference solution (right).

They agree with the asymptotic expansion (1.1) for small distances (solid line). Finally, the map $q \rightarrow F_{\text{lub}}(q, \bar{u})$ is approximated on $[0, 1]$ by a function of the following type

$$F_{\text{lub}}^{\text{approx}}(q, \bar{u}) = \frac{\delta_{-1}}{q} + \delta_0 + \delta_1 q + \delta_2 q^2 + \delta_3 q^3,$$

where the $(\delta_i)_i$ are determined using a least square approximation of the numerical results. The approximating function is plotted on the left side of Figure 7 (dashed line).

The reference solution can then be computed using the suggested algorithm. The trajectory obtained is plotted against time on the right side of Figure 7.

2.4.2. The fluid/particle solver

We now want to observe the influence of the method employed to deal with contacts in fluid/particle simulations. To do so, we use the fluid/particle solver implemented with **FreeFem++** and described in [20].

It consists in a method to simulate the motion of rigid particles in a Newtonian fluid. The rigid motion is enforced by penalizing the strain tensor on the rigid domain. The physics behind this method is to consider the rigid domain as a fluid with infinite viscosity. This leads to a generalized Stokes formulation on the whole domain (fluid + rigid). This approach allows us to use cartesian meshes and consequently, it can easily be implemented from Finite Element Navier-Stokes/Stokes solvers. In order to obtain three-dimensional results, we implemented an axisymmetrical version of this algorithm with **FreeFem++**.

2.4.3. Numerical results

Because of the cartesian mesh and the time discretization, the fluid/particle solver described in the previous subsection doesn't take into account the near-field hydrodynamic interactions with accuracy. We study here its coupling with two methods to deal with contacts: the inelastic contact model and the gluey contact model.

In Figure 8, we plot the solution given by the solver for the mesh size $\delta x = r/10$ (dashed line). We can observe that the particle remains glued. Indeed, due to the space discretization, the characteristic function representing the rigid particle ends up with touching the boundary of the domain and the Dirichlet boundary condition prevents it from taking off. Consequently, it is necessary to deal with the problem of contact and to prevent the characteristic function from intersecting the boundary of the domain. Two methods are tested: the fluid/particle solver is coupled with an inelastic contact algorithm and with the gluey contact model. The coupling is performed using the splitting strategy described in Remark 2.8. In each case, the constraint for

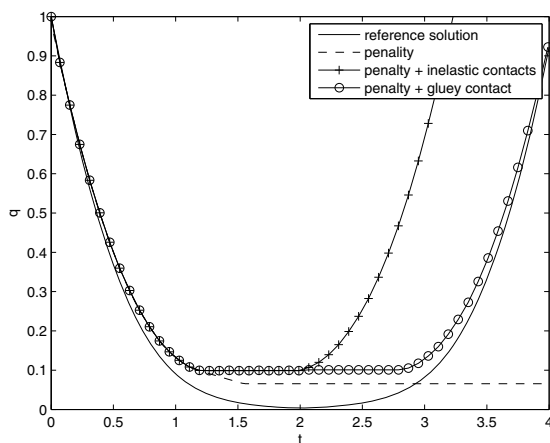
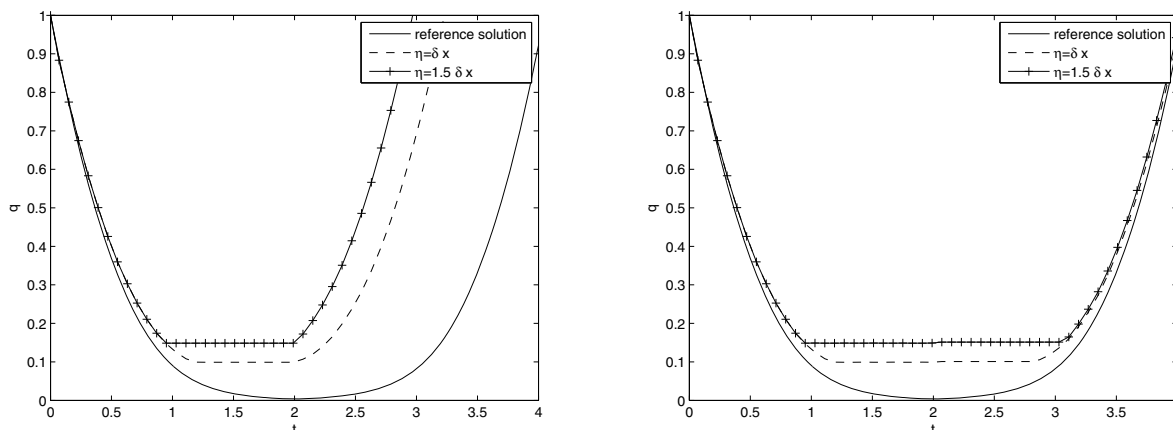


FIGURE 8. Comparison of the numerical solutions for different contact models.


 FIGURE 9. Impact of η on the numerical solution for inelastic (left) and gluey (right) contact.

the distance is set to $q \geq \eta$ with $\eta = \delta x$. The numerical results are compared in Figure 8. We observe that, for the inelastic model (solid line with crosses), the particle takes off as soon as it is pulled. To the contrary, using the gluey contact model (solid line with circles), the particle remains glued and the trajectory finally joins up with the reference one. This is a validation of the gluey particle model and it emphasizes the necessity to take the lubrication force into account when dealing with contacts.

We observe in Figure 9 the behaviour of the two contact models with respect to the parameter η which is the minimal distance allowed between the particle and the plane. We can see that the trajectories obtained for different η (greater than δx) separates after unsticking time when using the inelastic contact model (left side of the figure). This is due to the fact that, for this model, the particle unsticks as soon as it is pulled. To the contrary, the gluey particle model is not so sensible to parameter η (right side of the figure).

To finish, we study the impact of the mesh size on the results. As already mentioned, δx can not be chosen independently of η : we need $\delta x \leq \eta$ in order to avoid non-natural sticking due to the space discretization of

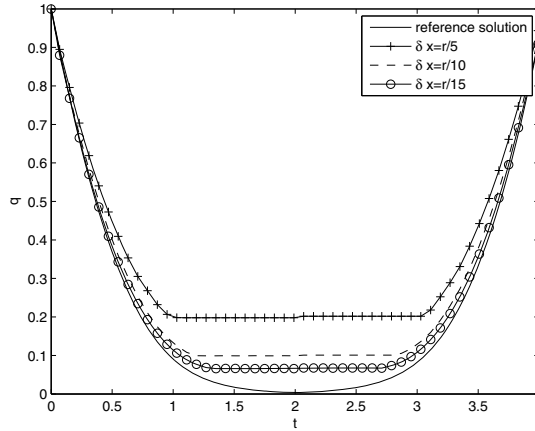


FIGURE 10. Impact of δx on the numerical solution for the gluey contact model, in the case $\eta = \delta x$.

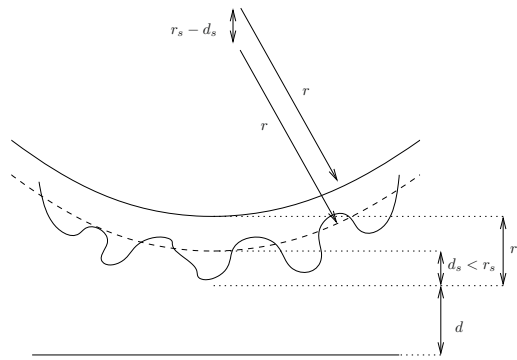


FIGURE 11. Equivalent smooth sphere.

the characteristic function. In Figure 10, we plot the trajectories obtained in the case $\delta x = \eta$, for different δx . As expected, when δx goes to zero, the numerical solution approaches the reference one.

2.5. Extension to rough solid surfaces

As described in the introduction, the lubrication force exerted on a rough sphere situated at distance d from a plane shall be modelled by:

$$\mathbf{F}_{\text{lub,rough}} \sim -6\pi\mu r^2 \frac{u}{d + d_s},$$

with $d_s < r_s$, r_s being the size of the roughness. Comparing this formula with the asymptotic expansion in case of a smooth sphere:

$$\mathbf{F}_{\text{lub}} \sim -6\pi\mu r^2 \frac{u}{d},$$

this force can be seen as the one that would be exerted on a smooth sphere situated at distance $d + d_s$ from the same plane (see Fig. 11).

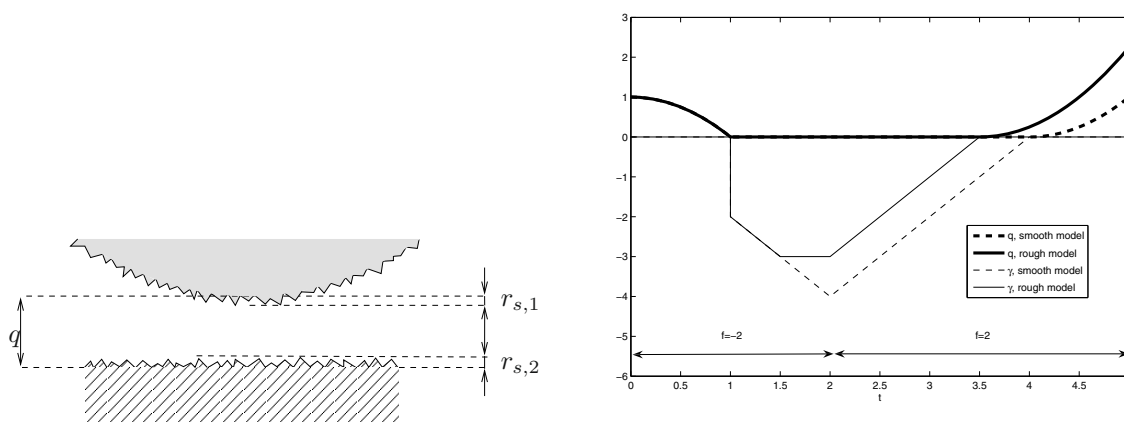


FIGURE 12. Rough solids: notations (left) and gluey particle model (right).

Consequently, d can go to zero and the roughness of the sphere and the plane can collide. As soon as such a collision occurs, there exists a solid/solid contact and the lubrication force does not act anymore on the solids.

We propose, in the following, a heuristic model for rough solid surfaces. Consider a rough sphere situated above a rough plane. We denote the size of their roughness by $r_{1,s}$ and $r_{2,s}$ respectively (see the left side of Fig. 12). The rough solids are modelled by equivalent shifted smooth ones. The shift is chosen to be equal to the size of the roughness. The action of the lubrication force on these smooth solids is modelled using the gluey contact model, which is slightly modified to take roughness into account. Indeed, as soon as the distance between the equivalent solids is equal to $r_{1,s} + r_{2,s}$, the contact becomes a real solid/solid contact (tops of roughness collide). During this contact, the distance is constant and equal to $r_{1,s} + r_{2,s}$ and the lubrication forces do not act anymore on the particle. To model such a behaviour, which is linked to the real distance and not to the macroscopic one, it suffices to recall that γ is the limit of $\gamma_\mu = 6\pi\mu \ln(d_\mu)$ and can be seen as the microscopic distance between the solids. The fact that the distance between the smooth solids can't go below $r_{1,s} + r_{2,s}$ is expressed in the limit model by:

$$\gamma \geq \gamma_{\min} = 6\pi\mu \ln(r_{s,1} + r_{s,2}).$$

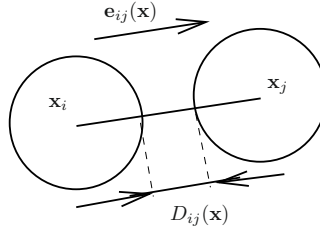
The trajectory computed for this model is plot on the right side of Figure 12, in the case $\gamma_{\min} = -3$. To understand this behaviour, as in the smooth case, let's consider a ball falling on a table coated with a viscous fluid (see Rem. 2.4). As before, at time 1, q is set to zero and γ stores the impact velocity. From then, since it is pushed, the particle gets closer to the plane and γ decreases. At time 1.5, γ reaches γ_{\min} , which means that, due to roughness, the solids collide. Then, even if it is pushed, the real distance (and γ) remains constant. From time 2, the particle is pulled and moves back from the fluid (γ increases) until it unsticks when γ is back to zero. We can observe that the rough particle takes off before the smooth one.

Contrary to what has been said in Remark 2.5 for the smooth case, it is now important to know the value of γ in order to truncate it. Therefore, it is essential to take the radius into account in its evolution and to use equation (2.7) in the gluey particle model:

$$\dot{\gamma} = -\frac{1}{r^2}\lambda.$$

In that case, the trajectory of the particle depends on r .

Remark 2.15. The smooth gluey particle model led to unphysical behaviours, independent of the initial lubrication model, the viscosity and the radius (see Rems. 2.2 and 2.5). Taking into account roughness makes it possible to come back to more physical behaviours. For example, the bigger is the viscosity, the lower is γ_{\min} and consequently, the longer lasts the contact.

FIGURE 13. Particles i and j : notations.

From an algorithmic point of view, this rough model can easily be taken into account in Algorithm 2.7 by changing step (3) in

$$\gamma^{n+1} = \gamma^n - \frac{h}{r^2} \lambda^{n+1},$$

where r is the radius of the sphere and by adding the following (4b) step:

$$\text{if } \gamma^{n+1} < \gamma_{\min}, \quad \gamma^{n+1} = \gamma_{\min}.$$

3. MULTI-PARTICLE CASE

3.1. Modelling

We generalize the gluey particle model (2.1)–(2.5) to the multi-particle case. We consider a system of N spherical particles in three-dimensions. \mathbf{x}_i stands for the position of the center of particle i in \mathbb{R}^3 and $\mathbf{f}_i \in \mathbb{R}^3$ for the external force exerted on it. Let $\mathbf{x} \in \mathbb{R}^{3N}$ be defined by $\mathbf{x} = (\dots, \mathbf{x}_i, \dots)$ and $\mathbf{f} \in \mathbb{R}^{3N}$ by $\mathbf{f} = (\dots, \mathbf{f}_i, \dots)$. We denote by D_{ij} the signed distance between particles i and j , and \mathbf{e}_{ij} by $\mathbf{e}_{ij}(\mathbf{x}) = (\mathbf{x}_j - \mathbf{x}_i) / \|\mathbf{x}_j - \mathbf{x}_i\|$ (see Fig. 13). We define M as the mass matrix of dimension $3N \times 3N$, $M = \text{diag}(\dots, m_i, m_i, m_i, \dots)$. Vector $\mathbf{G}_{ij} \in \mathbb{R}^{3N}$ is the gradient of distance D_{ij} with respect to the positions of the particles:

$$\mathbf{G}_{ij}(\mathbf{x}) = \nabla_{\mathbf{x}} D_{ij}(\mathbf{x}) = (\dots, 0, \underset{i}{-\mathbf{e}_{ij}(\mathbf{x})}, 0, \dots, 0, \underset{j}{\mathbf{e}_{ij}(\mathbf{x})}, 0, \dots, 0)^t.$$

In that context, there are $N(N-1)/2$ pair of particles and we denote by $\boldsymbol{\gamma} = (\dots, \gamma_{ij}, \dots) \in \mathbb{R}^{N(N-1)/2}$ the associated sticking variables: γ_{ij} is strictly negative if particles i and j are glued. Then, using the fact that $\frac{dD_{ij}(\mathbf{x})}{dt} = \mathbf{G}_{ij}(\mathbf{x}) \cdot \dot{\mathbf{x}}$, we define the following space of admissible velocities:

$$C_{\mathbf{x}, \boldsymbol{\gamma}}(t) = \left\{ \mathbf{V} \in \mathbb{R}^{3N} \text{ s.t. } \left\{ \begin{array}{l} \mathbf{G}_{ij}(\mathbf{x}) \cdot \mathbf{V} = 0 \text{ if } \gamma_{ij}(t^-) < 0 \\ \mathbf{G}_{ij}(\mathbf{x}) \cdot \mathbf{V} \geq 0 \text{ if } \gamma_{ij}(t^-) = 0, D_{ij}(t) = 0 \end{array} \right. \right\}.$$

To finish with notations, we denote by $\boldsymbol{\lambda} = (\dots, \lambda_{ij}, \dots) \in \mathbb{R}^{N(N-1)/2}$ the vector made of the Lagrange multipliers associated to these $N(N-1)/2$ constraints.

The multi-particle model is the natural counterpart of the particle/plane one:

$$\left\{ \begin{array}{l} \mathbf{x} \in (W^{1,\infty}(I))^{3N}, \quad \dot{\mathbf{x}} \in (BV(I))^{3N}, \quad \gamma \in (BV(I))^{N(N-1)/2}, \quad \boldsymbol{\lambda} \in (\mathcal{M}(I))^{N(N-1)/2}, \\ \dot{\mathbf{x}}(t^+) = P_{C_{\mathbf{x},\gamma}(t)} \dot{\mathbf{x}}(t^-), \\ M\ddot{\mathbf{x}} = M\mathbf{f} + \sum_{i < j} \lambda_{ij} \mathbf{G}_{ij}(\mathbf{x}), \\ \text{supp}(\lambda_{ij}) \subset \{t, D_{ij}(t) = 0\} \text{ for all } i, j, \\ \dot{\gamma} = -\boldsymbol{\lambda}, \\ D_{ij} \geq 0, \quad \gamma_{ij} \leq 0 \text{ for all } i, j, \\ \mathbf{x}(0) = \mathbf{x}^0 \text{ st. } D_{ij}(0) > 0 \text{ for all } i, j, \quad \dot{\mathbf{x}}(0) = \mathbf{u}^0, \quad \gamma(0) = 0_{\mathbb{R}^{N(N-1)/2}}. \end{array} \right. \quad (3.1)$$

Remark 3.1. The Lagrange multiplier λ_{ij} , associated to the constraint between particles i and j , is activated (non zero) only if these particles are in contact. The additional force due to this contact is equal to $\lambda_{ij} \mathbf{G}_{ij}(\mathbf{x})$. From the expression of $\mathbf{G}_{ij}(\mathbf{x})$, we get that this force only concerns the particles involved in the contact: it is equal to $-\lambda_{ij} \mathbf{e}_{ij}(\mathbf{x})$ on particle i and $\lambda_{ij} \mathbf{e}_{ij}(\mathbf{x})$ on particle j .

Remark 3.2 (roughness and radius). As for the particle/plane case (see Sect. 2.5), roughness can be taken into account by imposing a threshold on γ :

$$6\pi\mu \ln(r_{i,s} + r_{j,s}) \leq \gamma_{ij} \text{ for all } i, j,$$

where $r_{l,s}$ is the size of roughness of particle l . As noticed in the particle/plane case, it is now important to take the radius of the particles into account in the evolution of γ . To do so, in the same way as in the particle/plane case, we come back to the way the gluey particle model has been built and take into account all the constants involved in the first order asymptotic development of the lubrication force exerted between two particles (1.3). We obtain the following evolution equation for γ :

$$\dot{\gamma} = -R\boldsymbol{\lambda},$$

where R is the diagonal matrix of dimension $N(N-1)/2$ with coefficients $R_{ij,ij} = (r_i + r_j)^2 / (r_i^2 r_j^2)$.

3.2. Algorithm

Let h be the time step. We denote by $\mathbf{V}^n = (\dots, \mathbf{V}_i^n, \dots) \in \mathbb{R}^{3N}$ the approximated velocities of the particles at time $t^n = nh$. Let \mathbf{x}^n , γ^n and $\boldsymbol{\lambda}^n$ be the respective approximations of \mathbf{x} , γ and $\boldsymbol{\lambda}$ at time t^n .

The discretization of the continuous constraints $C_{\mathbf{x},\gamma}(t^n)$ is inspired by [24] and corresponds to a first order approximation of the constraints:

$$K(\mathbf{x}^n, \gamma^n) = \left\{ \mathbf{V} \in \mathbb{R}^{3N} \text{ s.t. } \left\{ \begin{array}{l} D_{ij}(\mathbf{x}^n) + h\mathbf{G}_{ij}(\mathbf{x}^n) \cdot \mathbf{V} \geq 0 \text{ if } \gamma_{ij}^n = 0 \\ D_{ij}(\mathbf{x}^n) + h\mathbf{G}_{ij}(\mathbf{x}^n) \cdot \mathbf{V} = 0 \text{ if } \gamma_{ij}^n < 0 \end{array} \right. \right\}.$$

Using this discrete space of admissible velocities, the time discretization of (3.1) is now a direct adaptation of Algorithm 2.7 to the multi-particle case.

Algorithm 3.3 (multi-particle). *For all $n \geq 0$, let \mathbf{x}^n , \mathbf{V}^n , γ^n and $\boldsymbol{\lambda}^n$ be given. We define $\mathbf{f}^n = \frac{1}{h} \int_{t^n}^{t^{n+1}} \mathbf{f}(s) ds$.*

(1) *Computation of the a priori velocity, without taking the lubrication force into account*

$$\mathbf{V}^{n+1/2} = \mathbf{V}^n + h\mathbf{f}^n.$$

(2) *Projection of the a priori velocity on the set of admissible velocities,*

$$\mathbf{V}^{n+1} \in K(\mathbf{x}^n, \boldsymbol{\gamma}^n), \quad \frac{1}{2} \left| \mathbf{V}^{n+1} - \mathbf{V}^{n+1/2} \right|_M^2 = \min_{\mathbf{v} \in K(\mathbf{x}^n, \boldsymbol{\gamma}^n)} \frac{1}{2} \left| \mathbf{v} - \mathbf{V}^{n+1/2} \right|_M^2.$$

From this projection step, we obtain $\boldsymbol{\lambda}^{n+1}$.

(3) *Updating of $\boldsymbol{\gamma}$,*

$$\begin{aligned} \boldsymbol{\gamma}^{n+1} &= \boldsymbol{\gamma}^n - h\boldsymbol{\lambda}^{n+1}, \\ \text{if } \gamma_{ij}^{n+1} > 0, \quad \gamma_{ij}^{n+1} &= 0. \end{aligned}$$

(4) *Updating of \mathbf{x} ,*

$$\mathbf{x}^{n+1} = \mathbf{x}^n + h\mathbf{V}^{n+1}.$$

Remark 3.4. In the same way as in Section 2.5 and Remark 2.8 for the particle/plane case, this algorithm can be extended to rough solids and coupled with fluid/particle solvers using a splitting strategy.

Remark 3.5 (obstacles). Suppose there exists N_0 fixed obstacles (walls of a box containing the particles for example). It is straightforward to add the NN_0 new constraints in $K(\mathbf{x}^n, \boldsymbol{\gamma}^n)$. Now, suppose these obstacles are moving with a prescribed velocity. We denote by \mathbf{y}^{n+1} the (known) vector giving their position at time t^{n+1} . The space of admissible velocities becomes:

$$K(\mathbf{x}^n, \mathbf{y}^{n+1}, \boldsymbol{\gamma}^n) = \left\{ \mathbf{V} \in \mathbb{R}^{3N} \text{ s.t. } \left. \begin{array}{l} \text{Pairs } (i, j) \text{ particle/particle:} \\ D_{ij}(\mathbf{x}^n) + h\mathbf{G}_{ij}(\mathbf{x}^n) \cdot \mathbf{V} \geq 0 \text{ if } \gamma_{ij}^n = 0 \\ D_{ij}(\mathbf{x}^n) + h\mathbf{G}_{ij}(\mathbf{x}^n) \cdot \mathbf{V} = 0 \text{ if } \gamma_{ij}^n < 0 \\ \text{Pairs } (i, k) \text{ particle/obstacle:} \\ D_{ik}(\mathbf{x}^n, \mathbf{y}^{n+1}) + h\mathbf{G}_{ik}(\mathbf{x}^n, \mathbf{y}^{n+1}) \cdot \mathbf{V} \geq 0 \text{ if } \gamma_{ik}^n = 0 \\ D_{ik}(\mathbf{x}^n, \mathbf{y}^{n+1}) + h\mathbf{G}_{ik}(\mathbf{x}^n, \mathbf{y}^{n+1}) \cdot \mathbf{V} = 0 \text{ if } \gamma_{ik}^n < 0 \end{array} \right\}.$$

3.3. Finding neighbours

The most time consuming step in Algorithm 3.3 is the projection step (2). It is performed using a Uzawa algorithm which imposes to run matrix/vector products involving the contacts. However, in order to simulate large collections of particles, it is essential to avoid loops over the $N(N-1)/2$ possible contacts. To do so, we notice that it is not necessary to take into account all contacts at each time-step. Indeed, two particles i and j far enough to each other at time t^n won't stick at time t^{n+1} and consequently, the corresponding constraint won't be activated (*i.e.* $\lambda_{ij}^{n+1} = 0$). We denote by D_{neigh} the distance above which we consider that two particles are not likely to touch next time-step. Then, the set of pairs of particles one has to consider at time t^n is:

$$C_{\text{neigh}}(\mathbf{x}^n) = \{(i, j) \in [1, N]^2, \quad i < j \text{ and } D_{ij}(\mathbf{x}^n) \leq D_{\text{neigh}}\}.$$

If the pair (i, j) is in the set $C_{\text{neigh}}(\mathbf{x}^n)$, we say that particles i and j are neighbours. Two particles that are not neighbours at time t^n won't stick at time t^{n+1} and consequently, one can restrict the set of constraints at time t^n to:

$$K_{\text{neigh}}(\mathbf{x}^n, \boldsymbol{\gamma}^n) = \left\{ \mathbf{V} \in \mathbb{R}^{3N} \text{ s.t., } \forall (i, j) \in C_{\text{neigh}}(\mathbf{x}^n), \left. \begin{array}{l} D_{ij}(\mathbf{x}^n) + h\mathbf{G}_{ij}(\mathbf{x}^n) \cdot \mathbf{V} \geq 0 \text{ if } \gamma_{ij}^n \geq 0 \\ D_{ij}(\mathbf{x}^n) + h\mathbf{G}_{ij}(\mathbf{x}^n) \cdot \mathbf{V} = 0 \text{ if } \gamma_{ij}^n < 0 \end{array} \right\}.$$

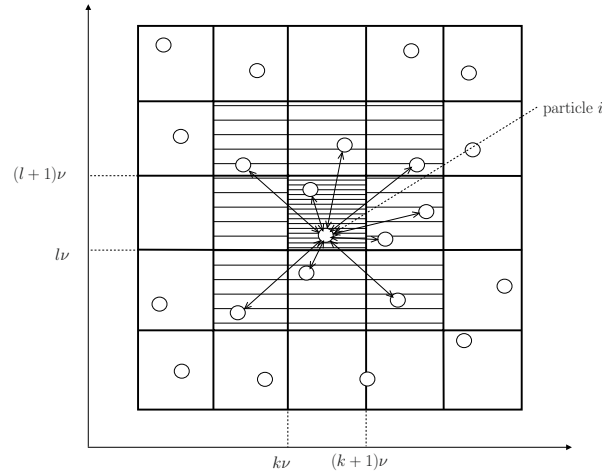


FIGURE 14. Algorithm to find neighbours: neighbouring boxes and distances actually computed.

Remark 3.6. This idea not to take into account particles far away from each other is generally used when considering particles interacting through near field interaction forces, decreasing with the distance. In that case, it consists in considering that the force is negligible above a certain distance and consequently, it is an approximation of the model. In our case, no approximation is made. Indeed, if D_{neigh} has been chosen sufficiently large, we know that the pairs of particles that are not belonging to $C_{\text{neigh}}(\mathbf{x}^n)$ won't undergo contact at time t^{n+1} and consequently, won't interact. For example, we can choose a time step in order to limit the displacement of the particles to twice their radius and then set the value of D_{neigh} to a few radiuses.

Note that this set of neighbouring particles can be used to add any short range interaction force in the simulation. For example, using the gluey particle model, two particles can interact through the lubrication force only if they undergo contact. We can chose to model the lubrication force by its asymptotic expansion when two particles are sufficiently close (*i.e.* in the set of neighbours). Then, we can deal with contacts due to the time discretization by using the gluey contact model.

To construct $C_{\text{neigh}}(\mathbf{x}^n)$ avoiding the computation of the $N(N-1)/2$ distances, we choose a bucket sorting type algorithm. It consists in dividing the computational domain into boxes of size $\nu > D_{\text{neigh}}$ and to compute distances only for pairs of particles belonging to neighbouring boxes (see Fig. 14). Note that, because of step (3), it is not sufficient to erase at each time-step the former set of neighbours and to create the new one: one has to transfer the value of γ_{ij}^n if particles i and j are in contact during these two successive time steps.

3.4. Object oriented programming method

To build this code, we chose to use the object oriented programming method for mathematical problems CsiMoon [17]. As a consequence, both numerical methods and models can be easily changed. For example, new methods can be chosen and added to the code in order to perform the projection step and to construct the set of neighbours. This programming method also allows us to take into account various models of external environment (dry environment, fluid, obstacles of different shapes...), of interparticular interactions (cohesion force...) and of contacts (inelastic, gluey model, aggregation...). This leads to a modular C++ code SCoPI², allowing Simulations of Collections of Interacting Particles. This code has already been used to simulate gluey particles, crowd motion, wet particles and red-cells (as an assembly of rigid particles).

²<http://www.math.u-psud.fr/~lefebvre/SCoPI.htm>.

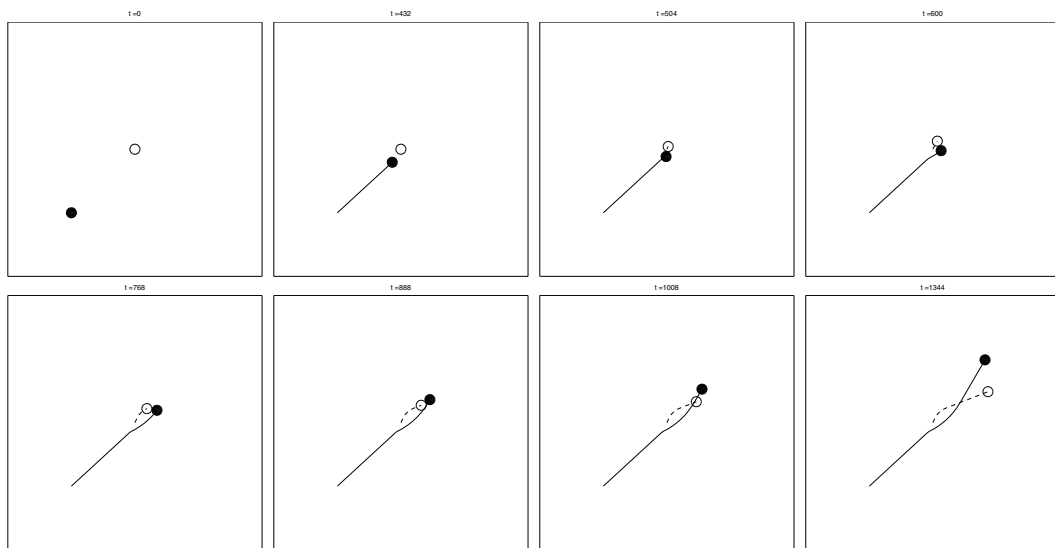


FIGURE 15. Gluey billiard: configurations and trajectories at different time steps.

4. NUMERICAL SIMULATIONS

We present in this section numerical simulations of collections of gluey particles. For visualization reasons, we only propose here two-dimensional simulations: even though the code is intrinsically three-dimensional, the motion of the particles is restricted to a vertical plane. These simulations demonstrate that the algorithm enables to take great numbers of gluey particles into account. This, together with Section 2.4, shows that coupling the gluey particle algorithm with fluid/particle solvers will make it possible to simulate dense fluid/particle flows, taking the lubrication force into account with accuracy.

4.1. Gluey billiard

We consider two spherical smooth particles with radius $r = 0.02$ moving on a plane. Their initial positions are $(0, 0)$ and $(-0.25, -0.25)$. The particle situated at the origin is supposed to be immobile at the beginning and the second one is thrown on it with initial velocity equal to $0.2 * (0.25, (0.25 - r))$. The time step is $h = 0.5r$. The configurations obtained with Algorithm 3.3 are given in Figure 15 at different time steps. At impact time, the particles stick together and they remain stuck until the centrifugal force balances the impact velocity.

4.2. Gluey lotto: influence of roughness

The aim of this simulation is to observe the influence of roughness on the behaviour of multi-particle systems governed by the gluey particle model. We consider a two-dimensional “gluey lotto” made of 160 particles in a squared rotating mixer operator. The side length of the box is 0.5 and the radiuses of the particles are taken between 0.007 and 0.015. All particles have the same mass $m = 1$ and the gravity constant g is taken equal to 10. The 80 particles initially situated in the left compartment of the box are black and the 80 other ones are white. We represent side by side in Figure 16 the configurations obtained at different time steps for $\gamma_{\min} = 0$ on the left (inelastic contacts), $\gamma_{\min} = -1$ in the middle (gluey rough particles) and $\gamma_{\min} = -\infty$ on the right (gluey smooth particles). In case of smooth particles, the heaps of particles take off from the wall when they are at the top of the box: as suggested by the particle/plane model, they take off only when the gravity has balanced the forces it has itself exerted to push the particles on the bottom wall. In the rough case, they take off earlier.

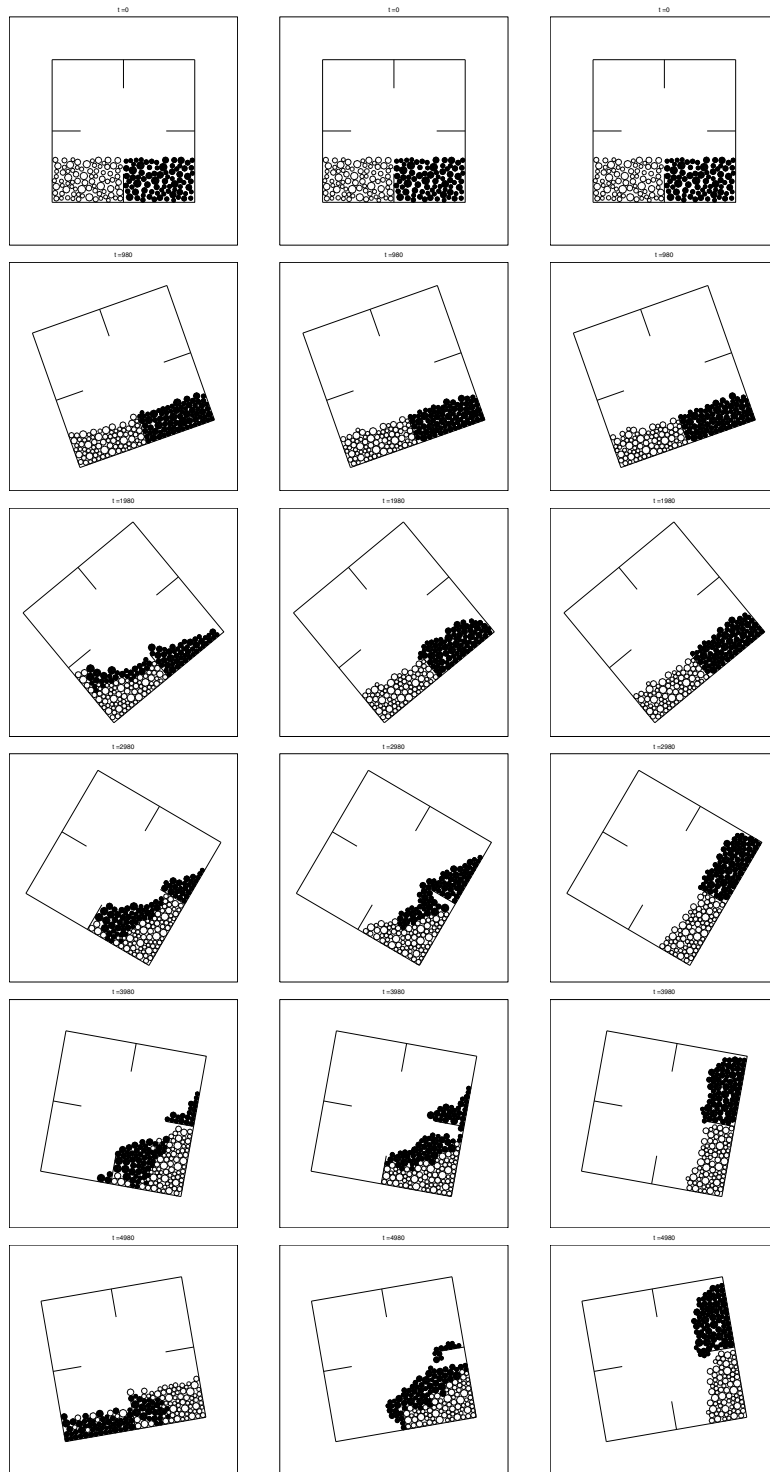


FIGURE 16. Gluey lotto: configurations at different time-steps for $\gamma_{\min} = 0$ on the left (inelastic contacts), $\gamma_{\min} = -1$ in the middle (gluey rough particles) and $\gamma_{\min} = -\infty$ on the right (gluey smooth particles).

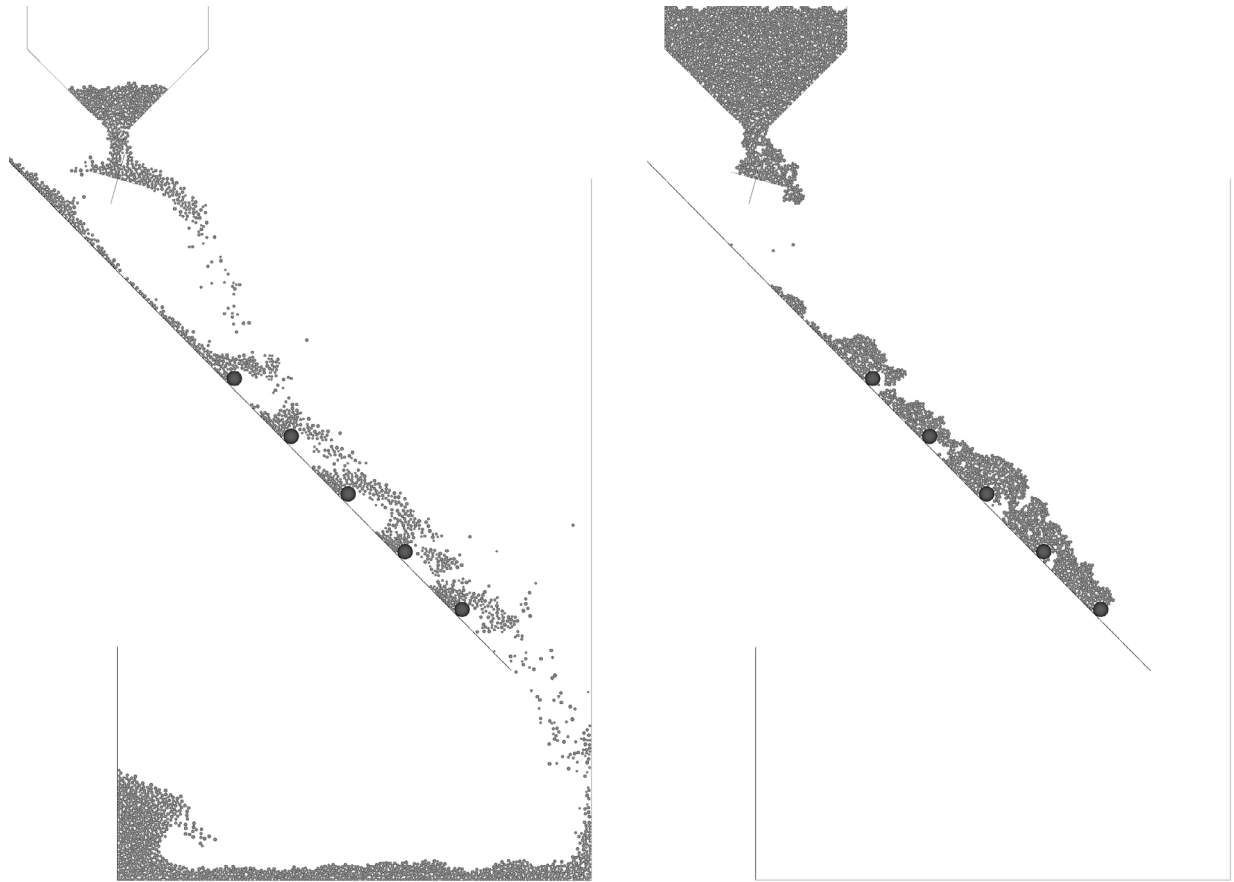


FIGURE 17. Snapshot of two-dimensional simulations, 3000 particles: dry (left) and viscous (right) simulations at time-step $n = 14\,226$.

4.3. Sedimentation of 3000 gluey particles

We consider 3000 gluey particles sedimenting under gravity with radii between 0.015 and 0.025. They are initially situated above a funnel (random sample of positions) with velocity equal to zero. All the particles have the same mass $m = 2$ and the gravity g is taken equal to 10. Below the funnel, a wheel rotates around its axis with angular velocity $\omega = -2$ and throws the particles on a leaning fixed plane situated below it. Then, the particles slip along the plane and finally fall in a container. Some spherical obstacles of radius $r = 0.1$ are fixed on the plane to slow the particles movement. A threshold is imposed on γ ($\gamma \geq -10$) to model roughness. The code also allows us to model dry granular flow involving inelastic contacts. In Figure 17 we compare the configurations obtained at the same time-step for simulations using the inelastic contact model and the previous gluey one.

Finally, we plot in Figure 18 the values of γ for a given configuration of the gluey simulation (zoom on the wheel). For each contact, a tube is plotted between the two involved particles and, the larger is γ_{ij} (*i.e.* the more the particles are glued), the darker is the grey. We can see the network of the forces leading to a packed configuration in the funnel. The particles are smoothly unsticking from each other when leaving the wheel.

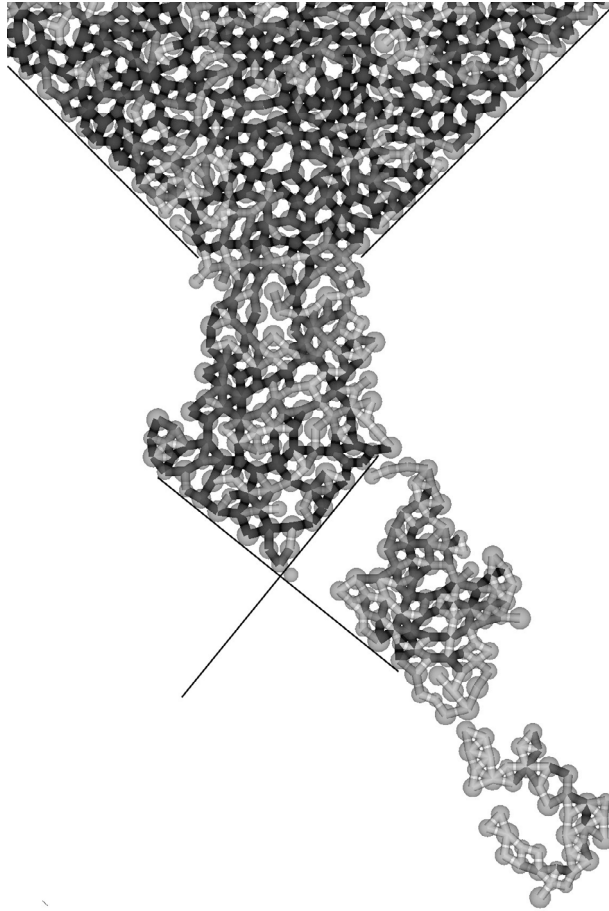


FIGURE 18. Snapshot of a two-dimensional gluey simulation, 3000 particles: configuration and values of γ at time-step $n = 14\,226$.

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