

1 **Enhancement of the geotechnical and geochemical properties of** 2 **gold tailings by BOF slag and class F fly ash**

3
4 **N.E. Mkhonto, Masters**

5 **Department of Chemical Engineering Technology**

6 **University of Johannesburg**

7 P.O. Box 17011, Doornfontein 2088, South Africa

8 201409446@student.uj.ac.za

9
10 **T.P. Mashifana, PhD**

11 **Department of Chemical Engineering Technology**

12 **University of Johannesburg**

13 P.O. Box 17011, Doornfontein 2088, South Africa

14 tmashifana@uj.ac.za

15
16 **N.T. Sithole, PhD**

17 **Department of Chemical Engineering Technology**

18 **University of Johannesburg**

19 P.O. Box 17011, Doornfontein 2088, South Africa

20 nastassias@uj.ac.za

21 **Abstract**

22 The aim of the study was to study if gold tailings can be stabilised by fly ash. The gold tailings
23 used in the study was the one where gold was recovered by cyanidation process. With more than
24 500 gold tailings in South Africa, which has adverse effect on the environment and human health,
25 this study provided a potential solution to deal with the tailings. Fly ash and BOF slag were
26 investigated as stabiliser to improve the properties gold tailings. Different fly ash: gold tailings:
27 BOF slag mix designs were investigated. Specimens were cast using the optimum ratio and cured
28 for 3, 7, 14, 28, 56 and 90 days to study the effect of curing time on strength development and
29 after the UCS tests the composites were characterised. The composite with 10% fly ash, 40%
30 BOF slag and 50% gold tailings showed the highest unconfined compressive strength. The
31 composite can withstand 5 wet-dry cycles. The BOF slag and FA modified GMT meet the
32 minimum strengths requirements to be classified as C4 material which can be used as subgrade
33 material.

34 **Key words:** beneficiation, gold mine tailings, slag, stabilisation

35 **Introduction**

36 Considerable volumes of waste materials generated by numerous industrial activities is disposed
37 to the environment resulting to pollution (Mashifana et al 2018). The mining sector in South
38 Africa contributes greatly to the economic development of the country. Researchers specifically
39 identified gold mining industry for over years playing a significant role in the country's economic
40 development (Schonfeld et al. 2014; Ngole-Jeme and Fantke 2017) and the production of gold
41 generates significant amount of tailings (mine residues). The impact of gold mine tailings to the
42 environment were investigated, the results showed that tailings pose serious human health risk
43 and ecological hazard through the inhalation of tailing dust and ingestion of contaminated
44 food/soil/water (Ngole-Jeme and Fantke 2017; Rudzani et al. 2017). Some residents living
45 around the tailing dams complained about wheezing chest, chronic cough, dermatitis and flu and
46 risk of long term effect such as cancer. There is a need to develop solutions that will utilise the
47 tailings and minimize the impact posed by gold tailings.

48

49 Fly ash and BOF slag as an industrial wastes were used in this study to beneficiate the gold
50 tailings. Fly ash is the by-product of coal combustion during the production of electricity and
51 it is either disposed in the landfill or stored at the power plant (Chancey et al. 2010; Xiao et al.
52 2017; Cho et al. 2019). All the three wastes utilised in this study, gold mine tailings and fly ash
53 are by-products that are readily available and are disposed in the landfill and result into
54 polluting the environmental. The materials have constituent that certify them to be used in civil
55 construction producing products at low cost and minimizing the environmental impact.

56 BOF slag is mostly used in the production of cement and road construction. Carvalho et al.
57 2017 evaluated the effect of utilizing BOF slag in the production of Portland cement.
58 Specimens were casted by adding 0, 1.8, 3.6 and 5.4% BOF slag to the slag cement. The axial
59 compressive strength was tested at 3, 7, 28 and 91 days of hydration, the specimens were also
60 characterised by setting time, hot and cold expansibility. The addition of BOF slag improved
61 the strength of the material but 5.4% addition had the greatest gain. In 2016 Santamaría et al.
62 investigated the use of fly ash and steel slag in structural mortars. Mortars were prepared using
63 steel slag to substitute aggregate and used as a cementing material and fly ash was used with
64 Portland cement. The use of steel slag with fly ash- cement appeared acceptable and the
65 strength reached about 78 MPa. The results showed that there is a potential of using steel slag
66 with fly ash in structural mortars.

67 Li et al. 2018 prepared fly ash- slag-carbide binder for application in mine backfilling. The
68 optimum composite was composed of 62% fly ash, 20% slag, 10% compound activator and
69 8% carbide slag. Compressive strength of 1.64- 4.14 MPa was obtained at 28 days hydration.
70 The cost of the backfill was found to be 20% lower compared to the one with Portland cement
71 alone. Researchers have used BOF slag and fly ash for cement production and the use of BOF
72 slag with fly ash to stabilise tailings is not explored. This study focused on using waste to
73 beneficiate waste in order to produce products that can be used for building purposes.

74 **Materials and methods**

75 The gold tailings were collected from Pan African Resources Mine in Barberton, Mpumalanga
76 (South Africa). Fly ash was collected from Eskom, Camden power station in Ermelo (South
77 Africa). The BOF slag was collected at Vaal, Arcelo Mittal. The materials were then
78 characterised for chemical composition using X-ray Fluorescence (XRF). The standard
79 compaction tests were conducted to determine the Optimum Moisture Content (OMC) and

80 Maximum Dry Density (MDD) on the composites of fly ash: BOF slag: gold mine tailings
 81 (10:40:50, 20:30:50, 30:20:50, 40:10:50 & 25:25:50).

82 The specimens were compacted at their OMC and MDD using 50x50x50mm³ moulds. The
 83 specimens were sealed in a plastic for curing periods of 3, 7, 14, 28, 56 and 90 days at room
 84 temperature in order to study the strength development with curing time. The unconfined
 85 compressive strength (UCS) was measured using a UCS machine with a loading rate of 15
 86 kN/min.

87

88 Results and discussion

89 Table 1 present the chemical composition of the materials

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Table 1: XRF analysis of the raw materials

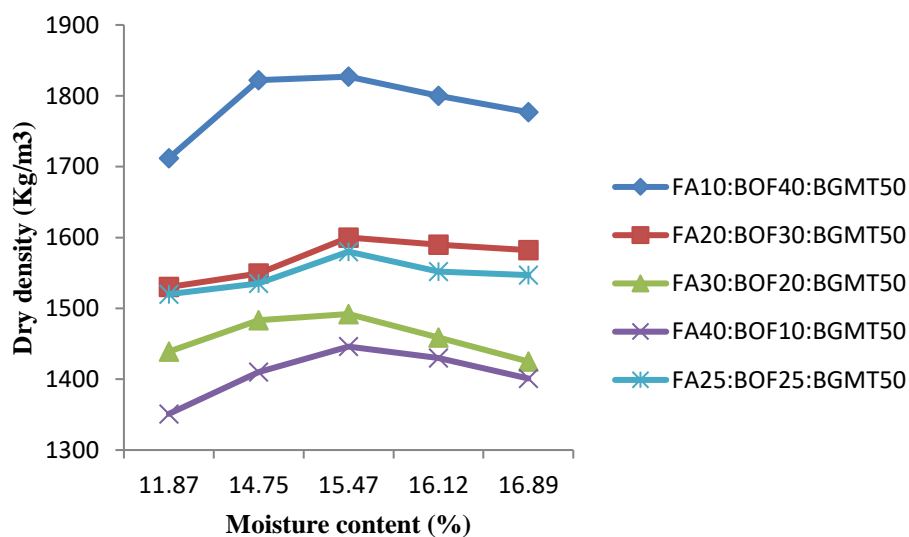
Materials	CaO	Al ₂ O ₃	MgO	SiO ₂	MnO	Fe ₂ O ₃
GT	9.17	11.25	4.64	48.08	0.32	14.87
BOF	47.50	4.20	3.62	10.15	3.94	27.73
FA	10.52	19.43	1.39	46.57	0.12	15.58

91 GT = gold tailings, BOF = basic oxygen furnace, FA = fly ash

92 The elemental compositions of the materials are presented in table 1. The predominant
 93 compounds in gold tailings are silicon oxide 48.08%, iron oxide 14.87%, alumina 11.25% and
 94 calcium oxide 9.17%. The main constituents of BOF slag are CaO (47.50%), Fe₂O₃ (27.73%)
 95 and SiO₂ (10.15%), the high proportion of CaO is attributed to lime that is added in the furnace
 96 in order to remove unwanted chemicals and iron that was not recovered when steel was made
 97 from the molten iron (Yildirim and Prezzi 2011; Jiang et al. 2018). Fly ash is mainly
 98 distinguished by the CaO (10.52%) content from the chemical composition presented in table
 99 1 it is evident that a class F fly ash was used in this study as the proportion of CaO is less than
 100 25%.

101 Standard compaction curve for different mix ratio of BOF: FA: GT

102 The maximum dry density (MDD) and optimum moisture content (OMC) of the mixtures
 103 obtained from the standard compaction test is shown in figure 1.



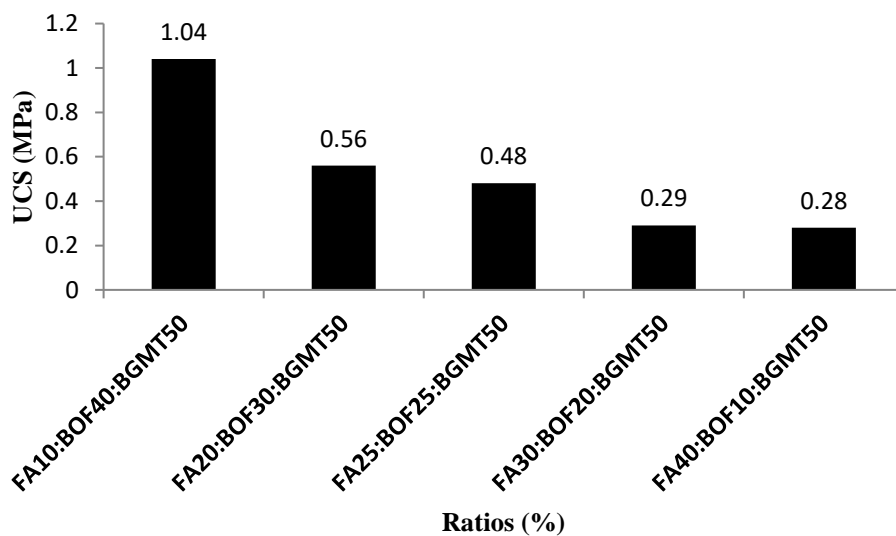
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105 Figure 1: MDD and OMC for different mix designs

106 Standard compaction test was done on the mixture of tailings, BOF slag and fly ash in order to
 107 determine the MDD and OMC. The BOF slag and fly ash content was varied between 10-40%
 108 while keeping the gold tailings constant at 50%. The OMC of the composite increase with the
 109 increasing content of fly ash and it is opposite for the BOF slag content. The MDD of composite
 110 decrease as the fly ash content increase from 10-40% at decreasing BOF slag content from
 111 1827 to 1446 kg/m³ while the MDD increases as the BOF slag content increased the results are
 112 in parallel with the previous research (Kumar and Rao 2017; Zumrawi and Babikir 2017). The
 113 behaviour of fly ash is attributed to its lower specific gravity and the smooth spherical particles
 114 that fill the voids which turn to produce denser matrix (Lee et al. 2014). The decrease in OMC
 115 is attributed by the agglomeration of particles that makes it easy to reach compaction with less
 116 water and increase in MDD is attributed by its higher specific gravity (Akinwumi 2014).

117 **Unconfined compressive strength of the different ratios**

118 Figure 2 shows the unconfined compressive strength of the different mixtures of BOF slag,
 119 gold tailings and fly ash. The obtained MDD and OMC for each mix design were used to cast
 120 and cure specimen in order to determine the best ratio that can stabilise the gold tailings. The
 121 UCS of the ratios increased with the increasing content of BOF slag and decreasing content of
 122 fly ash. The best ratio was found to be FA10: BOF40: GT50 with a UCS of 1.04MPa. The XRF
 123 analyses were conducted on the composites in order to study the influence of chemical
 124 composition on the UCS. From the chemical composition presented in table 2 increasing the
 125 BOF slag content increases the CaO content while decreasing the SiO₂ and Al₂O₃ content and
 126 in turn increase the Ca: Si ratio while decreasing the Al: Ca which are responsibly for strength
 127 gain (Sekhar and Nayak, 2019).



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 129 **Figure 2: UCS of the composites**

130 Table 2 present the XRF analysis of different mixtures and ratios of Ca: Si & Al: Ca for the
 131 mixtures

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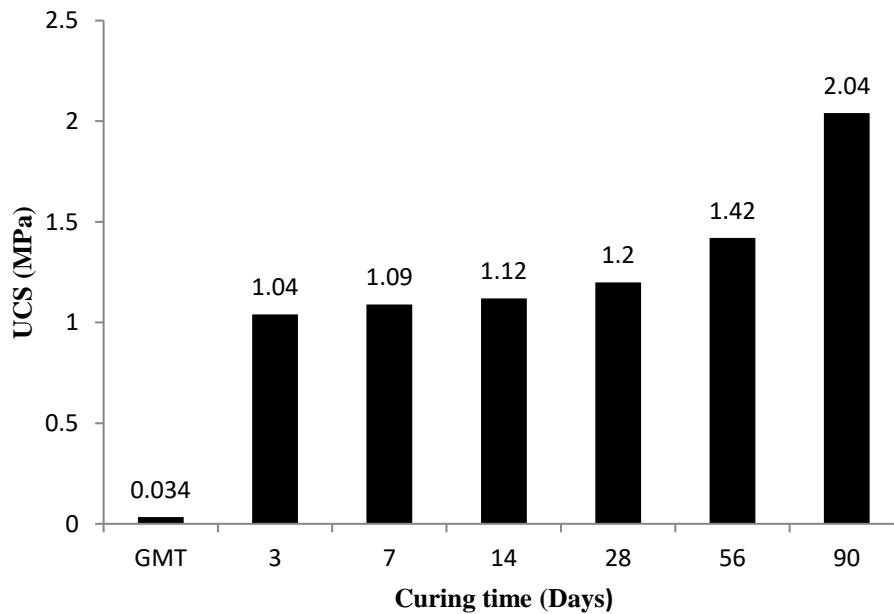
Table 2: XRF analysis and ratios of Ca: Si & Al: Ca

Composites	10B:40FA:50GT	20B:30F:50GT	25B:25FA:50GT	30B:20FA:50GT	40B:10FA:50GT
CaO	11.83	14.22	15.56	16.60	17.70
SiO ₂	43.70	42.09	40.51	39.99	39.11
Al ₂ O ₃	17.64	16.48	15.54	14.85	12.77
Ratios of Ca:Si and Al: Ca for the composites					
Ca: Si	0.27	0.34	0.38	0.42	0.45
Al: Ca	1.49	1.16	0.99	0.89	0.72

136

137 **Strength development of the optimum composite**

138 Figure 3 shows the strength development of the optimum ratio of BOF slag, fly ash and gold
 139 tailings over time. The UCS of the composite increased with the curing time. The UCS
 140 significantly increased by 40% from 1.04MPa at 3 days curing period to 1.42MPa after 56 days
 141 of curing. The obtained results are in parallel with other researches (Li et al., 2018; Jiang et al.,
 142 2018; Santamaría et al., 2016; Wang et al., 2018). The strength gain of BOF slag and fly ash
 143 stabilised composites is attributed by materials cementious structure which is caused by the
 144 product of hydration reaction, pozzolanic and crystallisation (Rabbani et al., 2012). The
 145 chemical compositions were used to study its influence on the UCS of the composites over
 146 time as Sekhar and Nayak, 2019 stated that Ca: Si and Al: Ca can be used to justify strength
 147 development. The increase in Ca and decrease in Al confirms the strength gain as the trend
 148 confirms the production of cementious compounds (CAH and CSH) (Sekhar and Nayak,
 149 2019). The strength gain is attributed to increase in Ca: Si and decrease in Al: Ca which is
 150 confirmed in table 3 (Sekhar and Nayak 2019; Jha and Sivapullaiah, 2014).



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152 **Figure 3: Strength development (FA 10: BOF 40: GMT 50)**

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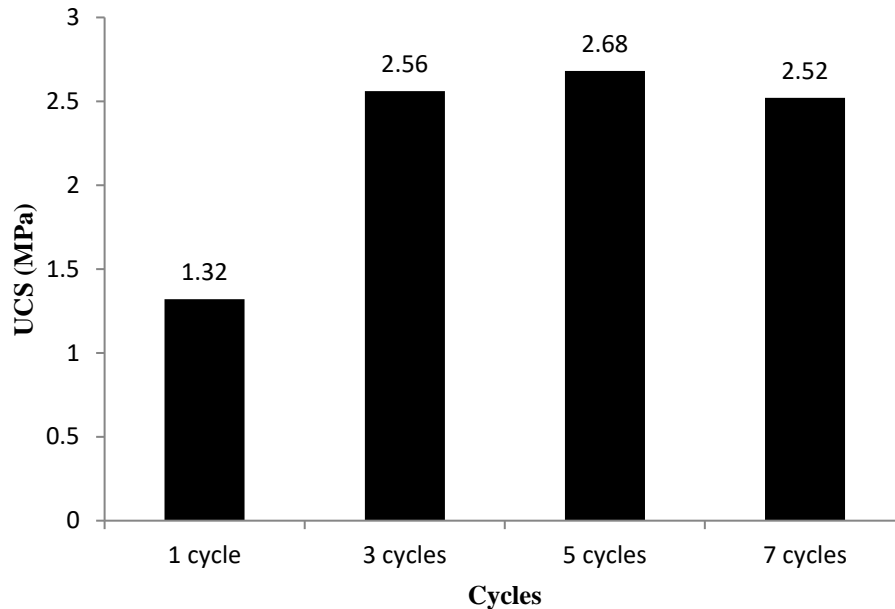
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Table 3: Ratios of Ca: Si & Al: Ca

Composites	3 days	7 days	14 days	28 days	56 days	90 days
Ca: Si	0.45	0.54	0.55	0.58	0.60	
Al: Ca	0.72	0.57	0.53	0.52	0.48	

155 Wet-dry cycles of the BOF: FA: GT composite

156 Environment plays a significant role in building and construction material especially subject to
157 weathering on wet and extreme temperatures the test had to be conducted to evaluate if the
158 composite can withstand such conditions (Zhang and Zong 2014). The results for wet-dry cycle
159 are presented in figure 4.



160

161 **Figure 4: Wet-dry cycles for the composites (FA 10: BOF 40: GMT 50)**

162 The composite FA10: BOF40: GT50 was subjected to 1, 3, 5 and 7 cycle of wet-dry and the
163 UCS results of the cycles are presented in figure 6. The highest UCS of 2.68MPa was obtained
164 after 5 wet-dry cycles, which means it can withstand over 10 days of wetting and drying without
165 losing strength but gaining. The strength loss after was obtained after 5 cycles which did not
166 show major difference.

167 Conclusions

168 The OMC of the composite increased with the increasing content of fly ash and decreased with
169 the increasing BOF slag content. The MDD of composite decreased as the fly ash content
170 increased from 10-40% while the MDD increased as the BOF slag content increased. The best
171 ratio was found to be FA10: BOF40: GT50 with a UCS of 1.04 MPa. The UCS of the composite
172 increased with the curing time. The strength gain is attributed to increase in Ca: Si and decrease
173 in Al: Ca. The optimum temperature was found to be 80°C. The composite can withstand 5 wet-
174 dry cycle

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176 References

177 Akinwumi, I. (2014). "Soil modification by the application of steel slag". *Period. Polytech.*
178 *Civ*, 58(4), 371-377.

179 Carvalho, S.Z., Vernilli, F., Almeida, B., Demarco, M. and Silva, S.N. (2017). "The recycling
180 effect of BOF slag in the Portland cement properties". *Resour. Conserv. Recy*, 127, 216-220.

- 181 Chancey, R.T., Stutzman, P., Juenger, M.C.G. and Fowler, D.W. (2010). “Comprehensive
182 phase characterization of crystalline and amorphous phases of a class F fly ash”. *Cement.*
183 *Concrete. Res*, 40, 146-156.
- 184 Cho, Y.K., Jung, S.H. and Choi, Y.C. (2019). “Effects of chemical composition of fly ash on
185 compressive strength of fly ash cement mortar”. *Constr. Build. Mater*, 204, 255-264.
- 186 Jha, A.K. and Sivapullaiah, P.V. (2014). “Mineralogical and microstructural induced
187 compressibility behaviour of lime stabilized expansive soil”. Kathmandu, Nepal international
188 symposium geohazards: science, *Eng. Manag*, Nepal, 502–513.
- 189 Jiang, Y., Ling, T., Shi, C. and Pan, S. (2018). “Characteristics of steel slag and their use in
190 cement and concrete- A review”, *Resour. Conserv. Recy*, 136, 187-197.
- 191 Kumar, S.P. and Rao, M.K. (2017). “Utilization of pulverized steel slag for stabilization of
192 lateritic sandy soils”, *IJRASET*, 5(8), 1115-1122.
- 193 Li, C., Hao, Y. and Zhao, F. (2018). “Preparation of fly ash-granulated blast furnace slag-
194 carbide slag binder and application in total tailings paste backfill”. IOP Conference series: *Mat.*
195 *Sci. Eng.* 322, 1-5.
- 196 Lee, J.K., Shang, J.Q. and Jeong, S. (2014). “Thermo-mechanical properties and microfabric
197 of fly ash-stabilized gold tailings”. *J. Hazard. Mater*, 276, 323-331.
- 198 Mashifana, T., Okonta, F.N. and Ntuli, F., 2018. “Geotechnical properties and application of
199 lime modified phosphogypsum waste”. *Mater. Scie*, 24(3), 312-318.
- 200
- 201 Ngole-Jeme, V.M. and Fantke, P. (2017). “Ecological and human health risks associated with
202 abandoned gold mine tailings contaminated soil”. *PloS one*, 12(2), e0172517.
- 203 Rabbani, P., Daghigh, Y., Atrechian, M.R., Karimi, M. and Tolooiyan, A. (2012). “The
204 potential of lime and grand granulated blast furnace slag (GGBFS) mixture for stabilisation of
205 desert silty sands”. *J. Civ. Eng. Res*, 2(6), 108-119.
- 206 Rudzani, L., Gumbo, J.R., Yibas, B. and Novhe, O. (2017). “Geochemical and mineralogical
207 characterization of gold mine tailings for the potential of acid mine drainage in the Sabie-
208 Pilgrim’s rest goldfields South Africa”. *9th Int’l Conf. on Research in Chemical, Agricultural,*
209 *Biological & Environmental Sciences*, Parys.
- 210 Santamaría, A., Rojí, E., Skaf, M., Marcos, I. and González, J.J. (2016). "The use of
211 steelmaking slags and fly ash in structural mortars”. *Constr. Build. Mater*, 106, 364-373.
- 212 Schonfeld, S.J., Winde, F., Albrecht, C., Kielkowski, D., Liefferink, M., Patel, M., Sewram,
213 V., Stoch, L., Whitaker, C. and Schüz, J. (2014). “Health effects in populations living around
214 the uraniferous gold mine tailings in South Africa: Gaps and opportunities for research”.
215 *Cancer. Epidemiol*, 38, 628-632.
- 216 Sekhar, D.C. and Nayak, S. (2019). “SEM and XRD investigations on Lithomargic clay
217 stabilized using granulated blast furnace slag and cement”. *Inter. J. Geotec. Eng*, 13(6), 615-
218 629.
- 219 Wang, S., Wang, C., Wang, Q., Liu, Z., Qian, W., Jin, C.Z., Chen, L. and Li, L. (2018). Study
220 on cementitious properties and hydration characteristics of BOF slag”. *Pol. J. Environ. Stud*,
221 27(1), 357-364.

222 Xia, H., Wang, W. and Goh, S.H. (2017). Effectiveness study for fly ash cement improved
223 marine clay. *Construction and building materials*, 157, 1053-1064.

224 Xiao, H., Wang, W. and Goh, S.H. (2017). “Effectiveness study for fly ash cement improved
225 marine clay”. *Construction and building materials*, 157, 1053-1064.

226 Yildirim, I.Z. and Prezzi, M. (2011). “Chemical, mineralogical and morphological properties
227 of steel slag”. *Advances in civil engineering*, 2011, 1-13.

228 Zhang, S. P. and Zong, L., (2014). “Evaluation of Relationship between Water Absorption and
229 Durability of Concrete Materials”. *Advances in Materials Science and Engineering*, 1-8.

230 Zumrawi, M.M.E. and Babikir, A.A.A. (2017). “Laboratory study of steel slag used in
231 stabilizing expansive soil”. *Asian Engineering Review*, 6(1), 1-6.

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