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# The role of particle clusters on the rheology of magneto-polymer fluids and gels

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## Summary

Even in absence of cross-linking, at large enough concentration, long polymer strands have a strong influence on the rheology of aqueous systems. In this work, we show that solutions of medium molecular weight (120,000 – 190,000 g/mol) alginate polymer retained a liquid-like behaviour even for concentrations as large as 20 % w/v. On the contrary, solutions of alginate polymer of larger (and also polydisperse) molecular weight (up to 600,000 g/mol) presented a gel-like behaviour already at concentrations of 7 % w/v. We dispersed micron-sized iron particles at a concentration of 5 % v/v in these solutions, which resulted either in stable magnetic fluids or gels, depending on the type of alginate polymer employed (medium or large molecular weight, respectively). These magneto-polymer composites presented a shear-thinning behaviour that allowed injection through a syringe and recovery of the original properties afterwards. More interestingly, application of a magnetic field resulted in the formation of particle clusters elongated along the field direction. The presence of these clusters intensely affected the rheology of the systems, allowing a reversible control of their stiffness. We finally developed theoretical modelling for the prediction of the magnetic-sensitive rheological properties of these magneto-polymer colloids.

## 1. INTRODUCTION

The systems composed of polymeric chains and magnetisable particles dispersed in a liquid medium are of a high technological interest as a consequence of their soft consistency and the possibility of controlling their physical properties at a distance through magnetic fields [1]. Broadly speaking, these "smart" materials can be classified into magnetorheological fluids and magnetic gels. The former are basically suspensions of magnetisable particles in a

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liquid medium, in which polymers can be added to reach different aims, including improving the colloidal stability of the dispersed particles. From the rheological point of view, in the absence of a magnetic field, the magnetorheological fluids behave like viscoelastic liquids, achieving a reversible liquid-solid transition under the application of a magnetic field. On the other hand, magnetic gels are characterised by showing a viscoelastic solid behaviour even in the absence of an applied magnetic field. Typically, this behaviour has its origin in the formation of a cross-linked network of flexible polymer chains that retains (by absorption) a large amount of liquid. This is what is known as polymeric gel and, by extension, a magneto-polymeric gel would be one that also contains dispersed magnetic particles.

The scientific field of magneto-polymeric gels experienced in its beginnings a development similar to that of magnetorheological fluids, finding for them applications mainly in the field of magnetorheological damping. However, in the last decade, the interest for the magneto-polymeric gels has resurged with novel applications in the field of biomedicine, in parallel to the growing importance of hydrogels (i.e., gels in which water is the medium of dispersion). In biomedicine, hydrogels stand out from the rest of biomedical materials because of their mechanical, chemical and biocompatibility versatility [2]. Consequently, hydrogels have been employed in various biomedical applications, being in many cases already commercially available. The current applications range from tissue engineering, to prepare extracellular matrices for different artificial tissues, to their use as drug delivery and cell-encapsulation systems.

The dispersion of magnetic particles in polymeric hydrogels allows them to be endowed with very interesting properties from the point of view of biomedical applications. First, the presence of magnetic particles allows the visualization and monitoring of magnetic hydrogels by magnetic resonance for in vivo applications [3]. In addition, several studies indicate that, when used in tissue engineering, the magnetic material stimulates cell adhesion, proliferation and differentiation [4]. Finally, recent works of our research group show that artificial biological tissues based on magnetic hydrogels, with microstructural and mechanical properties modulated by external magnetic fields, can be prepared [5], [6]. This is a unique advantage compared to other biomaterials because it is possible to generate smart materials suitable for mimicking native tissues and, therefore, with great potential in the field of tissue engineering.

Despite the advances achieved so far in the field of magneto-polymer hydrogels, there are several aspects that need improvement. For example, from the perspective of their applications in tissue engineering, an important advance

would be that, in the absence of applied magnetic field, hydrogels could be deformable enough to be injected through small cavities [7]. In this way, the hydrogels could be implanted by simple injection (without invasive surgery) and successively, in the post-injection stage, the gels could be activated by magnetic forces at a distance, for the until their mechanical properties to be adapted to those of the native tissues that they need to mimic. In short, obtaining hydrogels with these new characteristics would be a step forward in the field of biomaterials.

With this objective (preparation of injectable hydrogels with mechanical properties controllable by magnetic fields) in mind, we aimed for the preparation of magneto-polymer composites that could present shear-thinning properties. The mechanism of the self-assembly process, due to weak physical associations, is specific to the shear-thinning system. Therefore, we tried to target the above-mentioned objective by preparing highly concentrated solutions of polymers that could demonstrate a defined gel-like character, as a consequence of the impediment of movement of the polymer chains due to their high concentration. Iron particles were subsequently dispersed in the carrier solutions in order to provide the hydrogels with responsiveness to applied magnetic fields. We explored systems consisting of alginate polymers of two different molecular weights: medium molecular weight (120,000 – 190,000 g/mol) alginate polymer, as well as larger (and also polydisperse) molecular weight (up to 600,000 g/mol) alginate polymer. As it will be shown, a gel-like behaviour was observed only in the systems prepared with the highest molecular weight alginate. Nevertheless, both systems gave rise to stable suspensions of magnetic particles with a rich (magneto)rheological behaviour.

## **2. MATERIALS AND METHODS**

### **2.1. Materials.**

As polymer material, we used sodium alginate [empirical formula  $(C_6H_7NaO_6)_n$ ], obtained from the extracellular matrix of brown macroalgae, and supplied by two different enterprises (Sigma Aldrich, USA, and BioChemica, Germany). The fundamental difference between these two samples was related to their molecular weight. Sodium alginate with molecular weight 120,000-190,000 g/mol was purchased from Sigma Aldrich, while sodium alginate with molecular weight 10,000-600,000 g/mol was purchased from BioChemica. Differences in molecular weight reflected on the viscosity of solutions ranging from 15-25 mPa·s for 1 % Sigma Aldrich sodium alginate solutions in water, to 350-550 mPa·s for similar solutions of sodium alginate from BioChemica, according to the respective

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manufacturers. We will refer to these polymer materials as low viscosity sodium alginate (LVSA) polymer and medium viscosity sodium alginate (MVSA) polymer along this paper, respectively.

We used distilled water as dispersion medium, and bare iron particles (Fe-HQ powder) supplied by BASF (Germany) as magnetic phase. This powder consisted of spherical micron-sized particles of diameter  $0.9 \pm 0.3 \mu\text{m}$ , as obtained by electron microscopy images, and showed a volumetric mass density of  $7.88 \pm 0.16 \text{ g cm}^{-3}$ , as measured by a pycnometer. The powder presented a typical paramagnetic behaviour with saturation magnetisation  $M_s = 1721 \pm 2 \text{ kA/m}$ , as measured by superconducting quantum interference device magnetometry.

## **2.2. Preparation of solutions of alginate polymer.**

Both LVSA and MVSA polymers were dissolved separately in distilled water at concentrations ranging from 5% w/v to 20% w/v. We used mechanical mixing at a speed of 3500 rpm during 10 minutes to accelerate the dissolution and homogenise the resulting alginate solutions.

## **2.3. Preparation of suspensions of magnetic particles in alginate polymer solutions.**

For the preparation of suspensions of magnetic particles, we took HQ iron particles and suspended them in the alginate solutions at a concentration of 5% v/v. The resulting mixtures were homogenised by mechanical mixing.

## **2.4. Stability of the suspensions against particle settling.**

For the evaluation of the settling behaviour of the suspensions of iron particles in alginate solutions, we placed aliquots of the samples in test tubes and waited for the appearance of a sediment/supernatant interface, due to gravitational forces.

## **2.5. Rheological characterisation of the solutions and suspensions.**

First, we determined whether the alginate polymer solutions in water behaved as fluids or gels. For this aim, we considered a rheological point of view, from which gels are characterized by values of the storage modulus ( $G'$ ) larger than the values of the loss modulus ( $G''$ ) within the linear viscoelastic region (LVR). Otherwise, we will refer to the solutions as fluid-like samples. The precise experiments (amplitude sweeps) carried out for the determination of  $G'$  and  $G''$  within the LVR are described below in details.

We determined the rheological properties under shear of both polymer solutions and iron suspensions by using a rotational(magneto)rheometer (Physica MCR 300) with a plate-plate geometry of 20 mm of diameter and at a constant temperature of  $25 \pm 0.1 \text{ }^\circ\text{C}$ .

We subjected the samples to two different kinds of experiments. Steady state measurements, where the samples were subjected to ramps of shear rate,  $\dot{\gamma}$ , of increasing value and the resulting shear stress,  $\sigma$ , and viscosity,  $\eta$ , were monitored. And oscillatory measurements, where the samples were subjected to oscillatory shear strains, monitoring the resulting oscillatory shear stress. From oscillatory measurements we obtained the values of the storage ( $G'$ ) and loss ( $G''$ ) moduli. We performed two different oscillatory tests. In the first one we subjected the samples to oscillatory shear strains of constant frequency (1 Hz) and increasing amplitude –these tests are known as amplitude sweeps and allow the determination of the extension of the LVR. Secondly, we subjected the samples to oscillatory shear strains of constant amplitude (0.1, within the LVR) and increasing frequency from 1 to 100 Hz, in order to obtain the frequency response of the samples. For iron suspensions, all kinds of measurements were carried out both in absence and in presence of the applied magnetic field. For the application of the magnetic field of different strengths, we used the commercial magneto-cell provided with the Physica MCR300 rheometer.

We also analysed the self-healing capacity of the samples, after subjecting them to a shear rate that breaks the internal structure. For this aim, we subjected the samples to oscillatory shear strain of constant amplitude within the LVR and 1 Hz of frequency, and monitored the resulting viscoelastic moduli as a function of time. At time  $t=80$  s, and for a total duration of 80 s we stopped the oscillatory shear strain and subjected the samples to shear rates of large magnitude, in order to break the internal structure of the samples. Immediately afterwards ( $t=160$  s), the shear rate was stopped and the samples were subjected again to oscillatory shear strain of constant amplitude within the LVR and 1 Hz of frequency, and the resulting viscoelastic moduli were monitored again as a function of time, to check if the rheological state previous to the large shearing was regained. For this self-healing analysis, we used a controlled-stress Haake Mars III rheometer, provided with a measuring system consisting of coaxial cylinders of 16 mm and 17 mm of internal and external diameter, respectively, where the samples were previously placed and left at rest before the experiment.

For all kind of rheological experiments, results shown in this manuscript for each experimental condition represent the average of separate measurements; for at least 3 aliquots of each sample.

## **2.6. Optical microscopy of internal structure of suspensions.**

For the investigation of the microstructure of the suspensions of iron particles, we used optical microscopy connected to a CCD camera. We performed observations both in the absence and presence of the applied magnetic field.

### 3. EXPERIMENTAL RESULTS

#### 3.1. Stability of the suspensions against particle settling.

The colloidal stability was studied by monitoring, through direct observation, the appearance and evolution of phase separation in suspensions contained in test tubes (Figure 1).

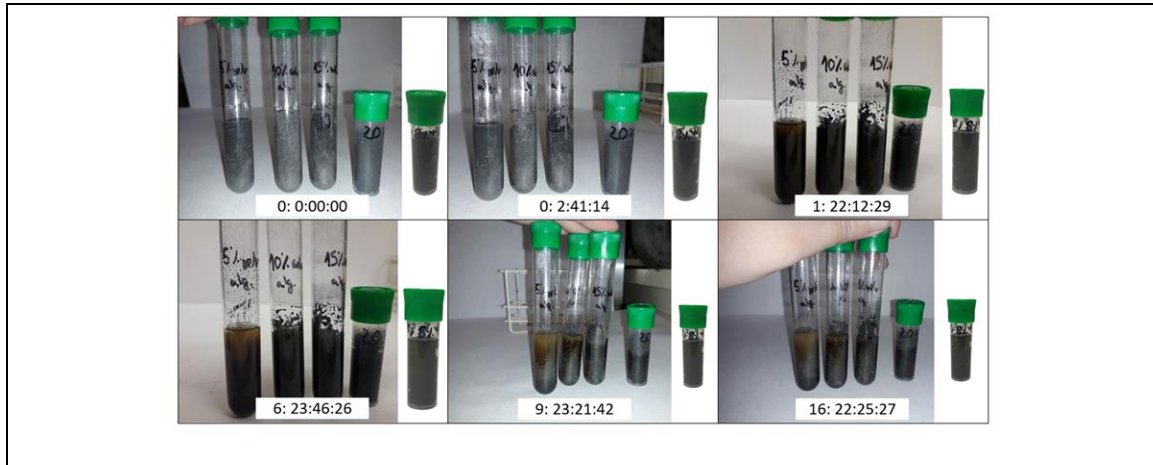


Figure 1. Images of suspensions of iron particles (5% v/v) in solutions of alginate polymer at different times after preparation as indicated (days: hours: minutes: seconds). In each image, from left to right samples corresponding to the following concentrations of alginate polymer are seen: 5% w/v of LVSA polymer; 10% of LVSA polymer; 15% of LVSA polymer; 20% of LVSA polymer; 8% of MVSA polymer.

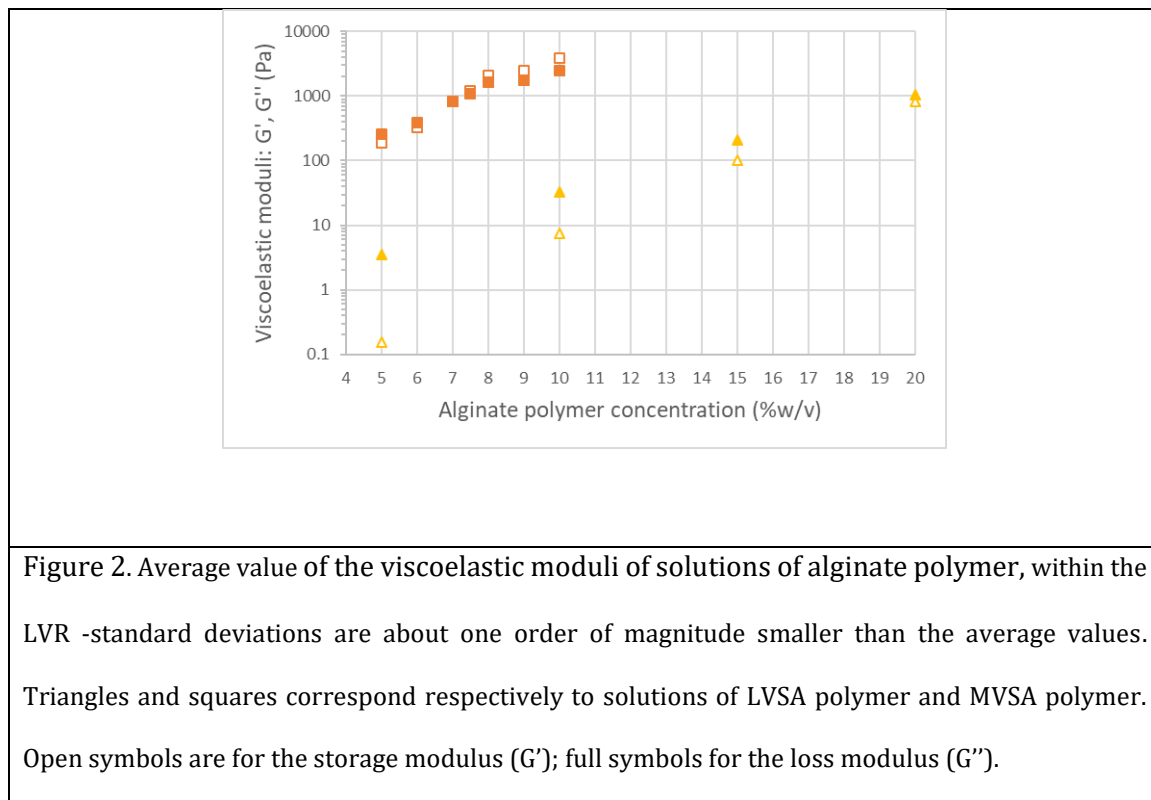
As observed, particle settling with appreciable phase separation appeared in suspensions of iron particles in LVSA polymer for concentration of polymer up to 15% w/v, whereas no signs of phase separation were observed even after 16 days of rest, for a LVSA polymer concentration of 20% w/v. As expected, the smaller the concentration of LVSA polymer, the faster was the phase separation. For suspensions of iron particles in MVSA polymer, no phase separation was observed for the total duration of the observations, already for a polymer concentration as low as 8 % w/v.

#### 3.2. Rheological characterization of the solutions and suspensions.

##### A. Analysis of fluid-like/gel-like behaviour of the solutions of alginate polymer.

We checked if solutions of LVSA polymer and MVSA polymer presented a fluid-like or gel-like behaviour. For this aim, we first subjected the samples to oscillatory strains of fixed frequency and increasing amplitude (amplitude

sweeps), and from these curves (not shown here for brevity) we determined the extension of the LVR. Then, we took the average value of both  $G'$  and  $G''$  corresponding to the LVR. The obtained results are plotted in Figure 2 as a function of alginate concentration, for both LVSA and MVSA.



As observed, for both LVSA and MVSA polymer solutions, the loss modulus ( $G''$ ) and the storage modulus ( $G'$ ) increased strongly with polymer concentration. For LVSA polymer, the loss modulus ( $G''$ ) was higher than the storage modulus ( $G'$ ) for the whole range of concentrations under study (up to 20% w/v), and thus we can conclude that LVSA polymer solutions showed a fluid-like behaviour. Note nevertheless that the difference between  $G''$  and  $G'$  diminished with polymer concentration, and at the highest LVSA polymer concentration (20% w/v), the value of  $G'$  almost reached that of  $G''$ . On the other hand, for MVSA polymer solutions, although the loss modulus was higher than the storage modulus at polymer concentration smaller than 7% w/v, a cross-over of these magnitudes took place for higher polymer concentration. Thus, we can conclude that, for concentrations higher than 7.5% w/v, the storage modulus dominated over the loss modulus and, consequently, the solutions presented a gel-like behaviour –note that the standard deviations are smaller than the differences between  $G'$  and  $G''$  for this range of concentrations of MVSA polymer.



This gel-like behaviour was certainly responsible for the stability against particle settling observed in Figure 1 for suspensions of iron particles in MVSA polymer solutions. In the case of LVSA polymer solutions, the increase in the loss (viscous) modulus with concentration of polymer justifies the progressive diminution of settling inferred from observations in Figure 1.

In what follows, and in view of the existence of two different behaviours for polymer solutions (fluid-like for LVSA polymer and low concentration of MVSA polymer, and gel-like for medium-to-high concentration of MVSA polymer), we will restrict the samples studied in this work to those described in Table I.

### B. Analysis of the steady state rheology in the absence of applied magnetic field.

From steady state measurements, we obtained the viscosity as a function of the shear rate (Figure 3). As expected, the viscosity of the LVSA polymer solutions increased strongly with the concentration of alginate polymer. Also, for a given concentration of LVSA polymer, a shear-thinning phenomenon was observed, which was characterised by a decrease of the viscosity as the value of the shear rate increased. This shear-thinning phenomenon was found to be relatively stronger at higher concentrations of polymer. With respect to the solution of MVSA polymer, it showed the largest values of viscosity at low shear rate, even though its relatively low polymer concentration, with respect to solutions of LVSA polymer. In addition, this sample showed the strongest shear-thinning behaviour, as anticipated by its gel-like behaviour, demonstrated by data of Figure 2.

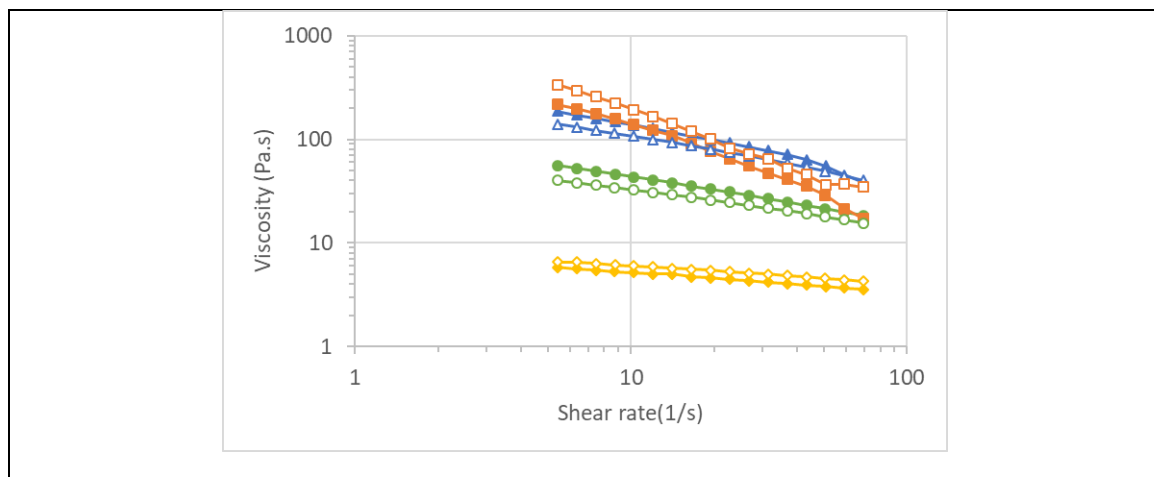


Figure 3. Viscosity as a function of shear rate for solutions of alginate polymer (open symbols) and suspensions of iron particles in alginate polymer solutions (full symbols): unfilled diamond / filled diamond: samples 0Fe-10LVSA/5Fe-10LVSA; unfilled circle / filled circle: samples 0Fe-

15LVSA/5Fe-15LVSA; unfilled triangle / filled triangle: samples 0Fe-20LVSA/5Fe-20LVSA; unfilled square / filled square: samples 0Fe-8MVSA/5Fe-8MVSA.

When magnetic particles were added to the solutions of sodium alginate, similar trends to those exhibited by the solutions of sodium alginate were obtained (Figure 3). Furthermore, the values of the viscosity for each given value of the shear rate were not much affected by the introduction of the particles, with respect to those of solutions of sodium alginate. This result was expected since in the absence of interaction between particles and polymers, the presence of 5 % v/v of particles only induces a limited modification of the viscosity, according to Batchelor's formula [8]. Nevertheless, to investigate better the effect of iron particle concentration, we studied the viscosity of 10% alginate solutions for increasing concentrations of iron particles (up to 20% v/v of iron particles – results not shown here) and we observed an increase in viscosity with increasing concentration of iron particles. Note that the effect of particle concentration in the viscosity of fluids and gels has been extensively investigated from both experimental and theoretical points of view in previous works, [8],[9], [10], [11].

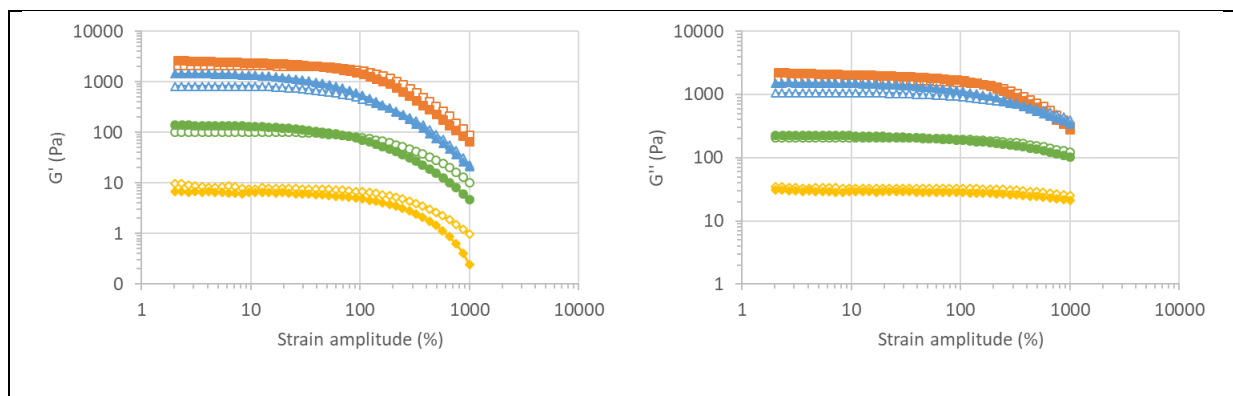


Figure 4. Viscoelastic moduli as a function of shear strain amplitude for fixed frequency of 1 Hz, for solutions of alginate polymer (open symbols) and suspensions of iron particles in alginate polymer solutions (full symbols): unfilled diamond / filled diamond: samples 0Fe-10LVSA/5Fe-10LVSA; unfilled circle / filled circle: samples 0Fe-15LVSA/5Fe-15LVSA; unfilled triangle / filled triangle: samples 0Fe-20LVSA/5Fe-20LVSA; unfilled square / filled square: samples 0Fe-8MVSA/5Fe-8MVSA. (a) Storage modulus ( $G'$ ); (b) loss modulus ( $G''$ ).

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### C. Analysis of the dynamic (oscillatory) state rheology in the absence of applied magnetic field.

We subjected the samples to oscillatory shear strains of constant frequency,  $f$ , (1 Hz) and increasing amplitude, as well as to oscillatory shear strains of constant amplitude,  $\gamma$ , and increasing frequency (Figures 4 and 5). For samples based on LVSA polymer (both the solutions and the suspensions) the loss modulus ( $G''$ ) was higher than the storage modulus ( $G'$ ), which is typical of a liquid-like system (Table II). Nevertheless, as the concentration of LVSA polymer within the solution increased, the values of  $G'$  increased faster than those of  $G''$ , and for the higher concentration under study (20 %) both the storage and the loss modulus were within the same order of magnitude. On the other hand, for the samples based on MVSA polymer (both the solution and the suspension)  $G'$  dominated over  $G''$  (Table II), i.e. a gel-like behaviour was obtained.

Another feature observed in Figure 4 is the fact that both  $G'$  and  $G''$  presented approximately constant values at low strain amplitude (something that defines the LVR), while showing decreasing trends at large amplitude (above 100 % of strain amplitude), with the drop more acute for  $G'$  than for  $G''$ . Concerning the dependence of these quantities with strain frequency within the LVR, as demonstrated by Figure 5, in all cases both  $\log G'$  and  $\log G''$  increased almost linearly with  $\log f$ , a characteristic that is typical of solutions of polymers measured at low to medium frequency [12]. Note at this point that the linear trends in double logarithmic scale observed in Figure 5 imply a power law dependence of the viscoelastic moduli with the frequency. We have calculated the exponent of this power law dependence and we obtained values in the approximate ranges 0.6 – 0.7 (for both  $G'$  and  $G''$ ) for samples based on LVSA, and values of approximately 0.25 (for  $G''$ ) and 0.44 (for  $G'$ ) for samples based on MVSA. Note that typically  $G'$  is constant at low frequency for highly cross-linked systems, such as rubber [12]. On the contrary, for concentrated polymer liquids  $G'$  scales with  $f^2$  and  $G''$  with  $f$  in the limit of low frequency [12].

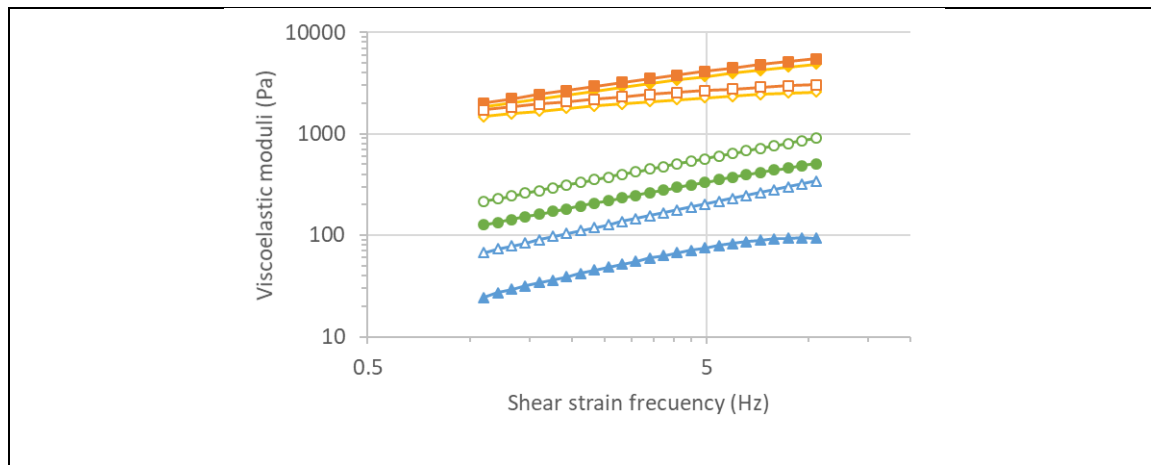


Figure 5. Viscoelastic moduli as a function of shear strain frequency for fixed shear strain amplitude within the LVR, for solutions of alginate polymer and suspensions of iron particles in alginate polymer solutions: unfilled triangle / filled triangle: sample 0Fe-15LVSA; unfilled circle / filled circle sample 5Fe-15LVSA; unfilled diamond / filled diamond: samples 0Fe-8MVSA; unfilled square / filled square sample 5Fe-8MVSA. Full symbols represent values of the storage modulus ( $G'$ ); open symbols values of the loss modulus ( $G''$ ).

As for the comparison between results for solutions and suspensions, as observed (Figures 4 and 5), the introduction of a content of 5% v/v of iron particles within the formulation provokes in general some enhancements of the values of  $G'$  and  $G''$  (Figure 3).

#### D. Analysis of the steady state rheology of suspensions of iron particles in alginate solutions in the presence of applied magnetic field.

We analysed the steady state behaviour under a magnetic field. As illustrated (see Figure 6) for the sample containing 5 % v/v of iron particles in the solution of 15% w/v of LVSA polymer, there is a clear magnetorheological effect, characterised by an enhancement of both the shear stress and the viscosity for a given value of the shear rate, as the strength of the magnetic field increased. Similar curves were obtained for the other samples, not shown here for brevity.

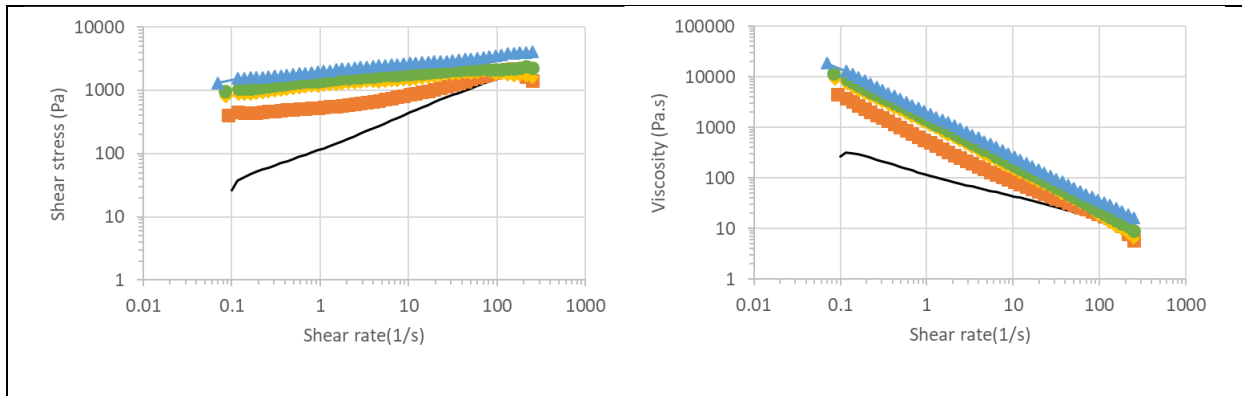


Figure 6. Shear stress (left) and viscosity (right) as a function of shear rate for sample 5Fe-15LVSA, under the application of magnetic fields of different strength,  $H$ . -:  $H=0$  kA/m; filled square:  $H=73.5$  kA/m; filled diamond:  $H=156$  kA/m; filled circle: 229 kA/m; filled triangle: 282 kA/m.

In order to better analyse the effect of the applied magnetic field on the characteristic rheological parameters of the samples, we obtained the dynamic yield stress,  $\sigma_y$ , of the samples from curves like these shown in Figure 6a, by fitting them to Bingham equation [13]:

$$\sigma = \sigma_y + \eta_p \dot{\gamma} \quad (1)$$

With  $\eta_p$  being the plastic viscosity. As observed in Figure 7, samples based on LVSA polymer did not show any yield stress in the absence of applied magnetic field, which is consistent with their liquid-like behaviour. On the contrary, the sample based on MVSA polymer presented a non-negligible yield stress in the absence of applied magnetic field, as expected for a gel-like material. Under an applied magnetic field, all samples presented a yield stress, which increased strongly with the intensity of the field. The stronger enhancement was obtained for sample 5Fe-8MVSA in spite of its gel-like behaviour in the absence of applied field. For samples based on LVSA polymer, the tunability of the rheological properties by magnetic field application was higher for the solution of 10 % of alginate than for the formulation containing 20 %, as a consequence of the stronger hindering of particle movement in the latter case due to the dense polymer chains at the microscopic level.

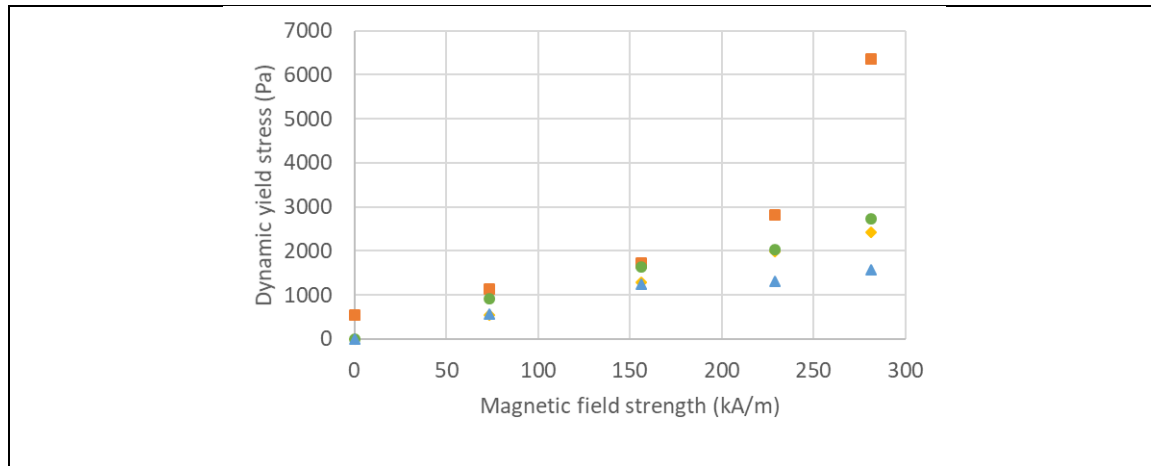


Figure 7. Dynamic yield stress as a function of the applied magnetic field strength, for suspensions of magnetic particles in solutions of alginate polymer. Filled diamond: sample 5Fe-10LVSA; filled circle sample 5Fe-15LVSA; filled triangle: samples 5Fe-20LVSA; filled square sample 5Fe-8MVSA.

#### E. Analysis of the dynamic (oscillatory) state rheology of suspensions of iron particles in alginate solutions, in the presence of applied magnetic field.

Finally, we analysed the effect of an applied magnetic field in the response of samples to oscillatory shear strains of fixed frequency (1 Hz) and step-wise increasing amplitude (Figure 8). As observed, the application of a magnetic field had a strong impact in the response of the suspensions. First, under a magnetic field, at low shear strain amplitude the storage modulus is higher than loss modulus, which is characteristic of a viscoelastic solid. The reason is the aggregation of the particles into chain-like structures under the application of a magnetic field, which gives to the samples a gel-like microstructure. Note, that for samples based on LVSA polymer, in the absence of an applied magnetic field, a viscoelastic liquid behaviour ( $G'' > G'$ ) was obtained. Another remarkable feature of Figure 8 is the fact that as the magnetic field increases, the magnitude of both  $G'$  and  $G''$  increases, as a consequence of the MR effect. Finally, we observe the appearance of a maximum in  $G''$  under a field in the range 10 to 100 % of strain. These maximums represent yielding points, for which the magnetic field-induced particle structures are broken by the applied shear.

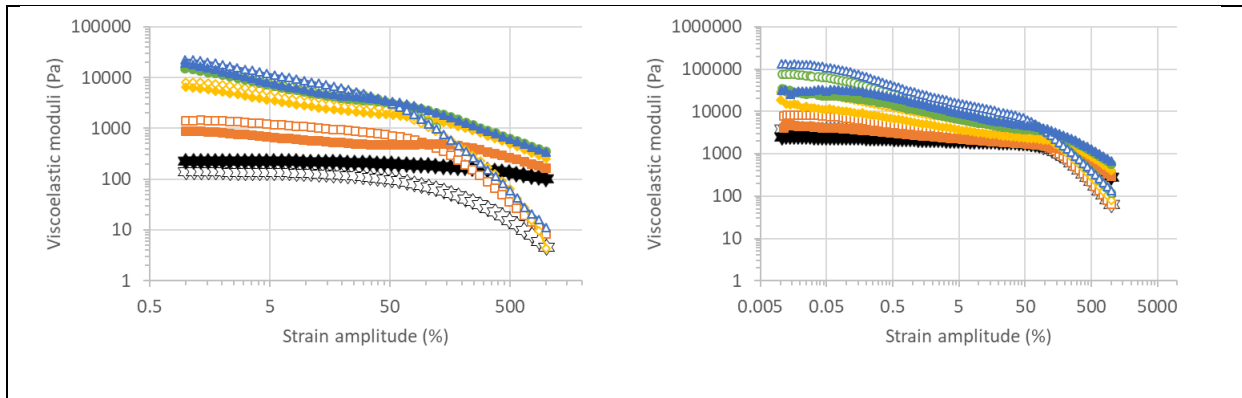
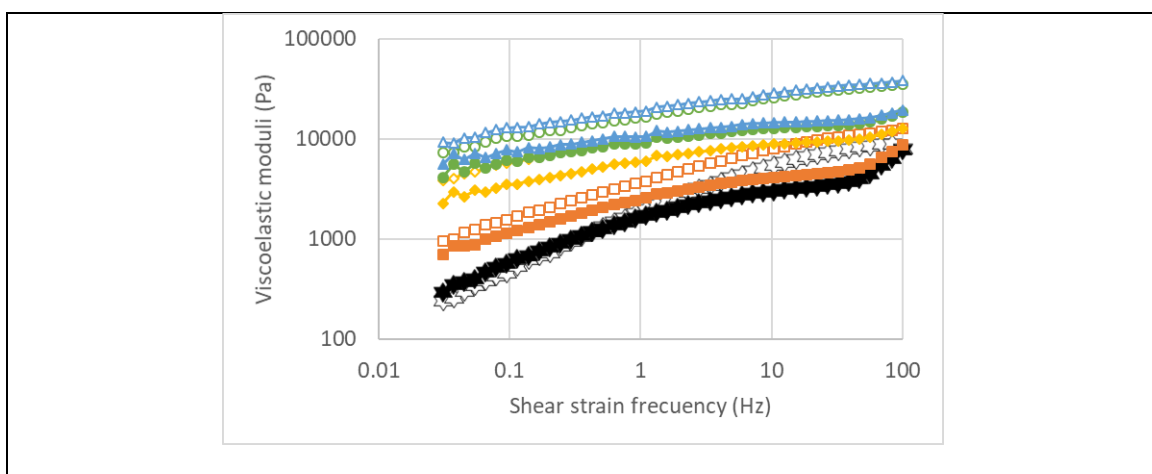


Figure 8. Viscoelastic moduli of suspensions of magnetic particles in solutions of alginate polymer, as a function of shear strain amplitude, for imposed oscillatory shear strain of fixed frequency (1 Hz), and under the application of magnetic fields of different strength:  $H$ . Unfilled star / filled star:  $H=0$  kA/m; unfilled square / filled square:  $H=73.5$  kA/m; unfilled diamond / filled diamond:  $H=156$  kA/m; unfilled circle / filled circle:  $H=229$  kA/m; unfilled triangle / filled triangle:  $H=282$  kA/m. (a) sample 5Fe-15LVSA; (b) 5Fe-8MVSA. Open symbols represent values of the storage modulus ( $G'$ ); Full symbols values of the loss modulus ( $G''$ ).

We also analysed the behaviour of the samples under oscillatory shear strains of constant amplitude (within the LVR) and increasing frequency. Results are illustrated for sample 5Fe-8MVSA as an example in Figure 9. As observed, for all the values of the applied magnetic field under study, both  $G'$  and  $G''$  increased with frequency, which is typical of viscoelastic materials. It is also observed that both  $G'$  and  $G''$  increased with the intensity of the applied magnetic field.



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Figure 9. Viscoelastic moduli of sample 5Fe-8MVSA as a function of shear strain frequency, for imposed oscillatory shear strain of fixed amplitude within the LVR, and under the application of magnetic fields of different strength:  $H$ . Unfilled star / filled star:  $H=0$  kA/m; unfilled square / filled square:  $H=73.5$  kA/m; unfilled diamond / filled diamond:  $H=156$  kA/m; unfilled circle / filled circle:  $229$  kA/m; unfilled triangle / filled triangle:  $282$  kA/m. Open symbols represent values of the storage modulus ( $G'$ ); Full symbols values of the loss modulus ( $G''$ ).

Finally, and in order to better analyse the effect of the applied magnetic field, we obtained the values of the viscoelastic moduli corresponding the LVR from curves like those shown in Figure 8 (frequency 1 Hz), and plotted them as a function of the magnetic field strength (Figure 10) -note that we took the viscoelastic moduli for shear strain amplitudes of 0.05 and 0.1 respectively for MVSA and LVSA samples, as representative of the LVR. As observed, there is a strong enhancement of the viscoelastic moduli (both  $G'$  and  $G''$ ) with the increase of the magnetic field strength. This enhancement was higher for sample 5Fe-8MVSA, in spite of its gel-like behaviour in the absence of applied magnetic field. For samples based on LVSA polymer, at the highest field the stronger enhancement was obtained for the sample containing the intermediate content of alginate (15 %). A larger amount of sodium alginate very likely hindered the magnetic field-induced particle chaining, thus preventing from a strong MR effect. At the lowest value of the applied magnetic field (73.5 kA/m), no significant differences were obtained for the different samples based on LVSA polymer, very likely because the polymer prevented from strong particle chaining.



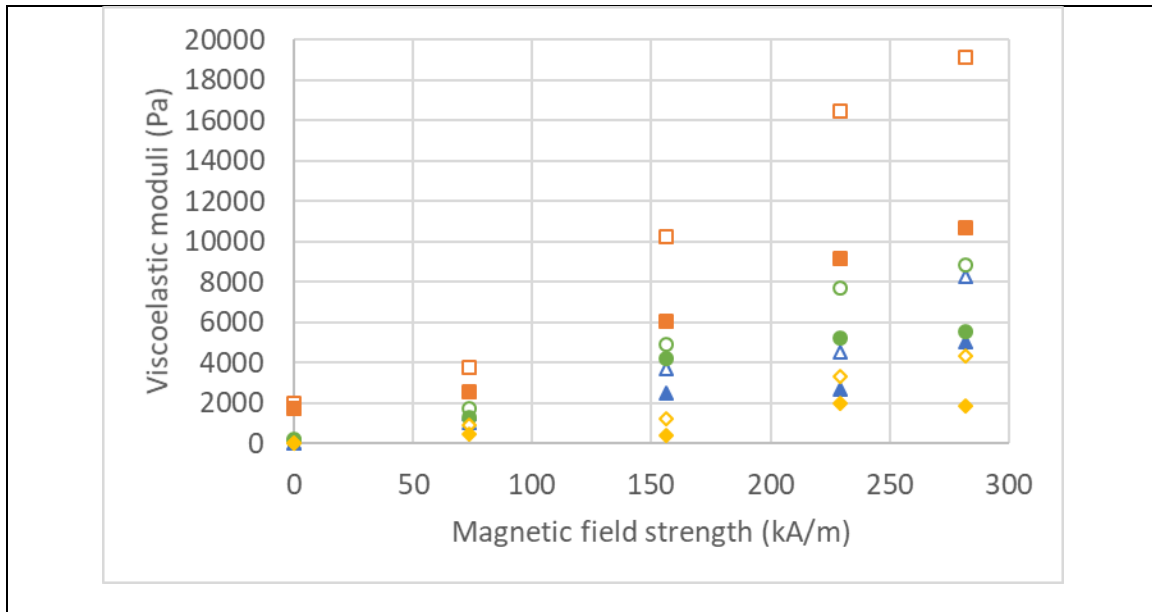


Figure 10. Values of the viscoelastic moduli corresponding to the LVR for a frequency of 1 Hz, as a function of the magnetic field strength for suspensions of magnetic particles in solutions of alginate polymer. Unfilled diamond / filled diamond: sample 5Fe-10LVSA; unfilled circle / filled circle: sample 5Fe-15VSA; unfilled triangle / filled triangle: sample 5Fe-20LVSA; unfilled square / filled square: sample 5Fe-8MVSA. Open symbols represent values of the storage modulus ( $G'$ ); Full symbols values of the loss modulus ( $G''$ ).

#### F. Self-healing behaviour.

The study of the self-healing behaviour makes sense for gel-like samples, for which a large shearing (such as the one used when injecting in biomedical applications) provokes a breakage of the internal network structure. Because of this, here we only present results for gel-like samples, i.e., samples based on MVSA polymer. As an example, Figure 11 shows the results for sample 5Fe-8MVSA, when subjected to a shear rate of  $1000 \text{ s}^{-1}$  (during the time interval 80 s – 160 s). As observed, the sample demonstrated a gel-like behaviour ( $G' > G''$ ) prior to the application of the large shear rate ( $t < 80 \text{ s}$ ). On the contrary, immediately after the application of the large shear rate ( $t \text{ approx. } 160 \text{ s}$ ), the sample demonstrated a liquid-like behaviour ( $G' < G''$ ), i.e. the internal structure (and thus the gel-like structure) was broken. Note also the large decrease of the values of the viscoelastic moduli after the large shearing. However, as the time advanced after the breakage, the gel-like behaviour was regained very quickly, accompanied by an

enhancement of the values of both  $G'$  and  $G''$ , although the values of the viscoelastic moduli measured prior to the large shearing were not recuperated for the total duration of the experiment. Similar results were obtained for other values of the applied shear rate, as well as for the gel-like samples not containing magnetic particles (0Fe-8MVSA).

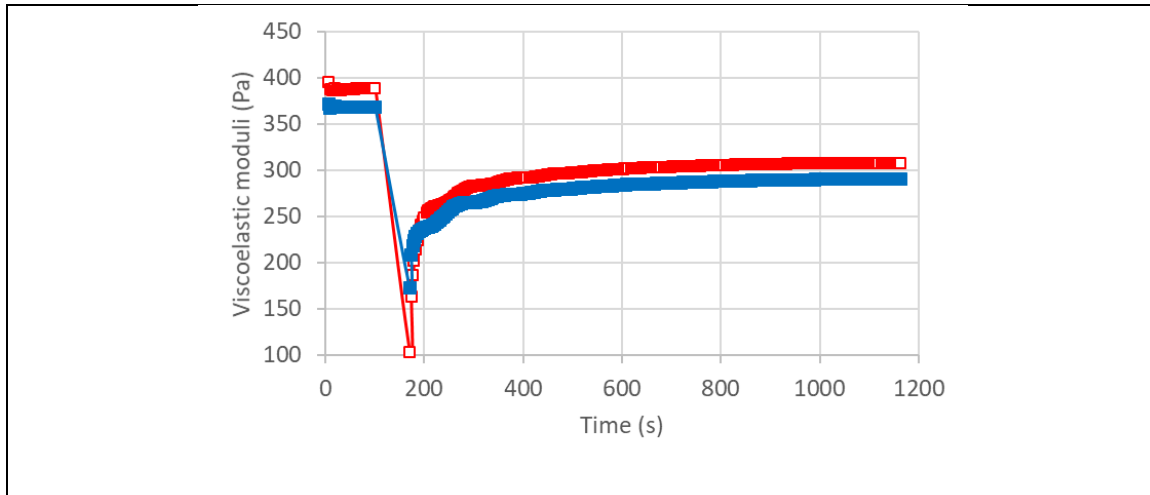


Figure 11. Self-healing study of sample 5Fe-8MVSA. The sample was subjected to a shear rate of  $1000 \text{ s}^{-1}$  during the time interval 80 s - 160 s. Before and after this time, the viscoelastic moduli resulting from an oscillatory shear strain of fixed amplitude within the LVR and 1 Hz of frequency were monitored. Open squares represent the storage modulus; full symbols the loss modulus.

### 3.3. Optical microscopy of the internal structure.

Finally, we analysed the internal structure of the magnetic samples by means of optical microscopy (Figure 12). As observed, some roughly spherical clusters were observed in all samples in the absence of magnetic field (parts A, C, E, G, I). These clusters should consist of magnetic particles aggregated mainly by van der Waals attraction, as well as a consequence of the remnant magnetisation. Under a magnetic field (parts B, D, F, H, J), these primary clusters should aggregate into secondary, elongated, chain-like clusters, as observed particularly in Figures 12 B and J. These chain-like clusters are less in number in those samples containing a larger amount of alginate polymer (compare Figures 12 F and H with Figures B and J), as the polymer hindered the movement of the primary clusters in response to the applied magnetic field. These results are in agreement with the results of magnetorheological experiments,

where we obtained a stronger enhancement of the rheological properties under a magnetic field for samples 5Fe-8MVSA and 5Fe-10LVSA than for those containing larger amounts of polymer.

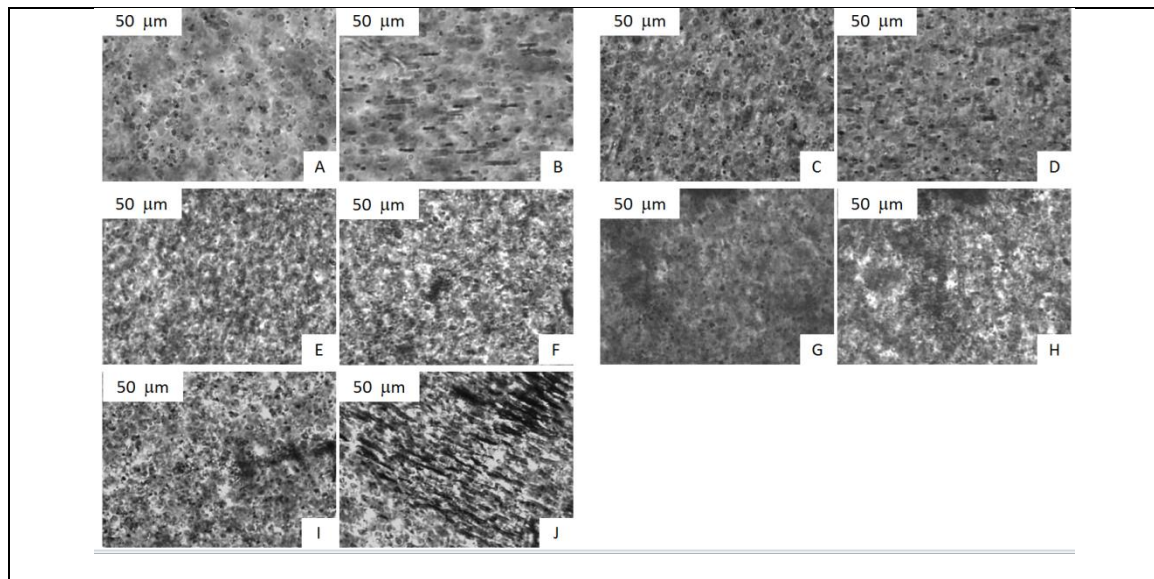


Figure 12. Images of optical microscopy of diluted suspensions of magnetic particles (about 0.2 % v/v of particles) in solutions of alginate polymer. A, C, E, G, I were taken in the absence of applied magnetic field; B, D, F, H, J were taken under the application of a magnetic field of 40 mT. Solutions of alginate polymer used as dispersing medium were as it follows: A,B: 5LVSA; C,D: 10LVSA; E,F: 15LVSA; G,H: 20LVSA; I,J: 8MVSA.

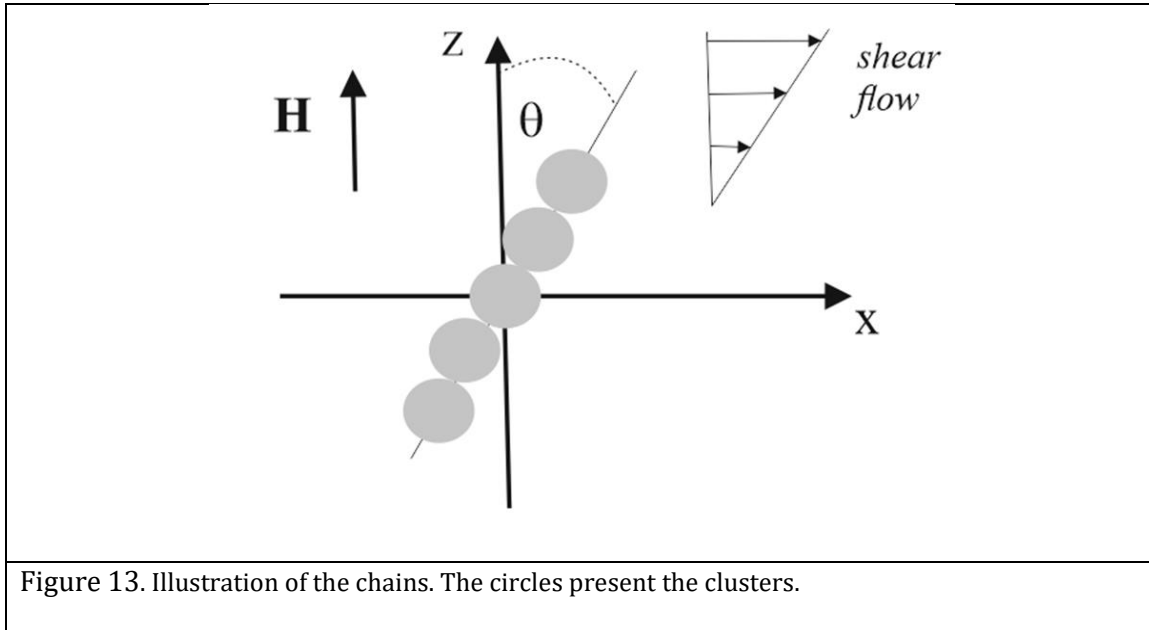
#### 4. THEORY

In this part we present a theoretical model of the observed magnetoviscous effects in the alginate suspensions, involved in the low frequency motion, which can be considered as a quay-stationary one. The model is based on observations of [10], which demonstrate that without an applied field the particles of the magnetic filler unify into dense aggregates (primary agglomerates -PA), which, in the first approximation, can be considered as spherical clusters. Under the action of applied magnetic field, these clusters magnetise and form linear chain-like aggregates. In the gelled polymer, the number of the PAs in the chain is determined by a competition between the force of magnetic attraction between the agglomerates, and the resistance to their displacement in the elastic host gel.

In a motionless liquid suspensions of magnetisable non Brownian particles (PAs), the number of particles (PAs) in the chain is, in principle, restricted only by the size of the sample. Theoretically, these chains can overlap the suspension, bridging the opposite walls of the container. If the suspension is involved in macroscopic deformation flow, the most long chains are destroyed by the viscous forces and the size of the chains is determined by competition between the forces of magnetic interparticle (interagglomerate) attraction and the destroying hydrodynamic forces [14],[15].

However, photos in Figure 12 show that, because of the high viscosity of the carrier alginate solution, the clusters do not have time to form the long chains overlapping the measuring cell. It is natural to suppose that initially, right after the field switching on, the rate of the chains formation is relatively high. Then, with depletion of the single PA concentration, the rate falls down till the neglecting values. Note that the similar time-dependence of the rate of the chains formation has been detected in computer simulations [16]. One can suppose also that the chains, which can appear for the duration of a real experiment, are significantly shorter than the maximal (stable) size of the chains, estimated in [14,15], corresponding to the given stationary shear rate of the suspension flow. That is why, in the flowing suspension, at least in the studied range of the macroscopic shear rate, these chains can be considered as undestroyed. When the shear rate exceeds some threshold value, the chains rupture. The analysis and comparison of the obtained theoretical results with the experimental ones, presented below, confirms the concept of the transition from the regimes with undestroyed to the ruptured chains.

Let us start with analysis of the suspension with undestroyed chains, corresponding to the relatively low shear rate of the suspension flow. For maximal simplification of analysis, we consider a system of identical chains, consisting of the identical spherical primary agglomerates. Like in the experiments, an external magnetic field is applied in the direction of the suspension velocity gradient. We suppose that number  $n$  of the PAs in the chain is given and does not depend on the shear rate.



We will use an approach, based on the models [10],[14],[15] of magnetic suspensions with the chains. Like in these models, suppose that they magnetically interact with the dipole-dipole way and neglect their hydrodynamic interactions.

Magnetic moment of a PA in the chain can be presented as  $m = Mv$ , where  $M$  is the chain magnetisation,  $v$  is the agglomerate volume. The magnetisation can be estimated by using the well-known Frohlich-Konnely approximations [17]

$$M = \frac{\chi_0 H_{in} M_s}{\chi_0 H_{in} + M_s} \quad (2)$$

Here  $\chi_0$  and  $M_s$  are the initial susceptibility and the saturated magnetisation of the primary agglomerate, i.e. of the chain, consisting of them;  $H_{in}$  is the mean magnetic field inside the chain. This field can be estimated as [18]

$$H_{in} = H - MN \quad (3)$$

where  $N$  is demagnetising factor of the chain,  $H$  is magnetic field in the suspension. Taking into account that the particles volume concentration in our experiments is low, the field  $H$  is approximately equal to the field external with respect to the suspension.

We estimate parameter  $N$  by using the explicit relation (see, for example. [18]) for demagnetising factor of an ellipsoid of revolution with the aspect ratio equal to the number  $n$  of the agglomerates in the chain:

$$N = \frac{1}{2(n^2-1)^{\frac{3}{2}}} \left[ n \ln \left( \frac{n+\sqrt{n^2-1}}{n-\sqrt{n^2-1}} \right) - 2\sqrt{n^2-1} \right] \quad (4)$$

Magnetic susceptibility and saturated magnetisation of the agglomerates, which appear in the alginate suspension with the internal composition similar to that in the present experiments, have been estimated in ref. [10] as:  $\chi_0 \approx 6.4$ ;  $M_s \approx 800 \text{ kA/m}$ .

Combining eqs. (2) and (3), one gets:

$$M = \frac{b - \sqrt{b^2 - 4\chi_0^2 M_s H N}}{2N\chi_0}$$

$$b = \chi_0 H + M_s(1 + \chi_0 N) \quad (5)$$

The strong magnetoviscous effect, observed in the experiments presented in Figs. 6-10, can be provided long chains with  $n$  significantly more than one. In this case the demagnetising factor  $N$  is much less than 1, and the relation (5) gives:

$$M = \frac{\chi_0 H M_s}{\chi_0 H + M_s} \quad (6)$$

Under the action of the shear flow the chain deviates from the applied field  $H$ . This leads to appearance of a magnetic torque, which tends to return the chain in the field direction. The angle  $\theta$  of the chain deviation from the field is determined by balance of the hydrodynamic  $\Gamma^h$  and magnetic  $\Gamma^m$  torques, acting on the chains; these torques can be estimated as [14],[15]:

$$\Gamma_n^h = \frac{1}{12} \gamma \beta d^2 \cos^2 \theta n(n-1) \quad (7)$$

$$\beta = 3\pi\eta_0 d$$

$$\Gamma_n^m = -6(n-1) \frac{\mu_0 m^2}{4\pi d^3} \sin \theta \cos \theta \quad (8)$$

Here  $\mu_0$  is the vacuum magnetic permeability,  $d$  is the PA diameter,  $\eta_0$  is viscosity of the carrier liquid. In the case of the alginate suspension,  $\eta_0$  is not equal to the viscosity of the pure alginate solution without the particles (Figure 3) but, approximately, it can be estimated as viscosity of the suspension without the field (since the concentration of the particles is small). Balancing the torques (7) and (8), we come to the relation for the deviation angle  $\theta$ , shown in Figure 13:

$$\tan \theta = \frac{\pi^2}{6} \gamma \frac{\eta_0 d^6}{\mu_0 m^2} n(n+1) \quad (9)$$

The stress, produced by the chains, can be estimated as [14,15]:

$$\sigma_{ch} \approx \frac{N_{ch}}{V} |\Gamma_n^m| \quad (10)$$

where  $V$  is total volume of the suspension,  $N_{ch}$  is total number of the chains in this system.

Combining equations (8), (9) and (10), after simple transformations, one gets:

$$\begin{aligned} \sigma &\approx \sigma_{ch} + \eta_0 \dot{\gamma} \\ \sigma_{ch} &= \frac{3}{2} \Phi (n^2 - 1) \frac{\eta_0 \dot{\gamma}}{1 + (\tan \theta)^2} \end{aligned} \quad (11)$$

Here  $\Phi$  is volume concentration of the primary agglomerates,  $\eta_0 \dot{\gamma}$  is the stress in the host medium. The volume concentration  $\Phi$  of the clusters cannot be calculated theoretically; the estimate  $\Phi \approx 0.25$  was obtained in [10] by comparing the experimental and theoretical results. Note that the number  $n$  of the agglomerates in the undestroyed chain is determined by the details of kinetics of the chain formation. Analysis of this kinetics requires a special investigation that is out of the scope of the present paper. That is why we determine  $n$  as a fitting parameter from the condition of agreement between theory and experiment.

Let us consider the regime of the ruptured chains. The stress  $\sigma_{ch}$  now can be estimated by using the results of [14,15]. Assuming  $n \gg 1$ , we can present the results of [15] as

$$\sigma_{ch} = \Phi \mu_0 \frac{M^2}{36\sqrt{2}} \quad (12)$$

For small values of the shear rate  $\dot{\gamma}$ , the stress  $\sigma_{ch}$ , determined by equation (7), is less than that given by equation (8). For large  $\dot{\gamma}$ , the opposite relation takes place. Following the principle on minimum of energy dissipation in a nonequilibrium system, it is natural to suppose that the transition from the state with the undestroyed chains to the state with the ruptured chains must take place when the values of stress  $\sigma_{ch}$ , estimated by equations (11) and (12), coincide. Thus, we can present the final form for the total stress as:

$$\sigma \approx \sigma_{ch} + \eta_0 \dot{\gamma} , \quad (13)$$

$$\sigma_{ch} = \min \left( \frac{3}{2} \Phi (n^2 - 1) \frac{\eta_0 \dot{\gamma}}{1 + (\tan \theta)^2}; \Phi \mu_0 \frac{M^2}{36\sqrt{2}} \right)$$

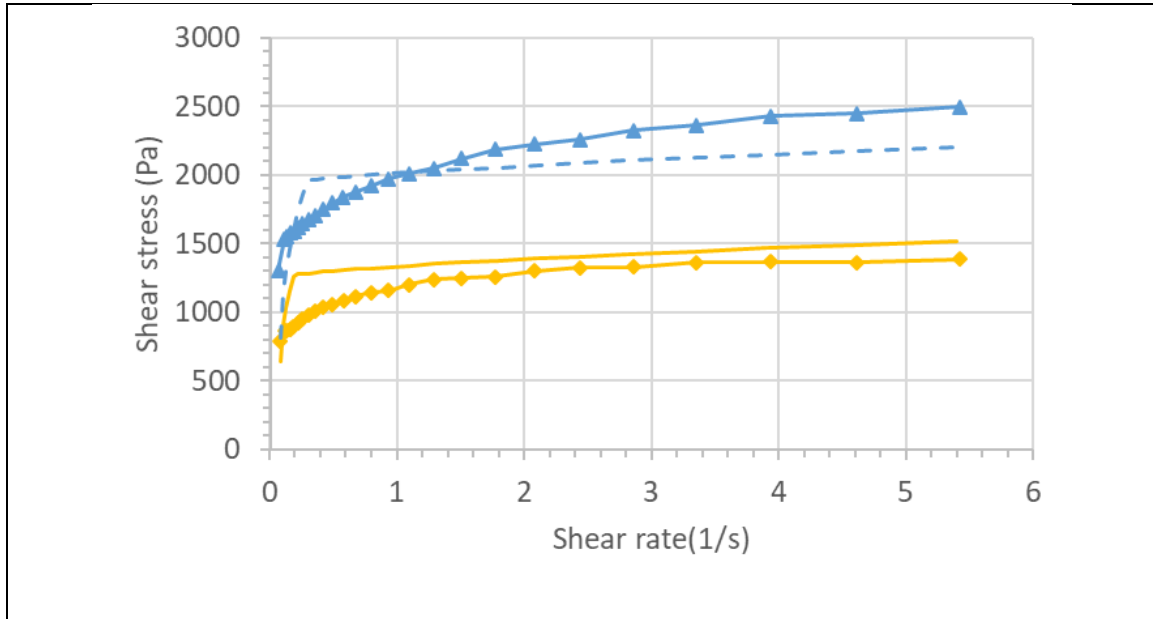


Figure 14. Theory-experiment comparison for curves of shear stress vs. shear rate, for sample 5Fe-15LVSA, under the application of magnetic fields of different strength,  $H$ : filled diamond, - :  $H=156$  kA/m; filled triangle, - - : 282 kA/m. Filled diamond, filled triangle represent experimental data; - , - - predictions of the theoretical model (Equation 13). Parameters of the system for theoretical calculations: number of primary agglomerates in the undestroyed chains obtained by fitting are  $n = 8$  and  $n = 9$  for the magnetic fields of 156 kA/m and 282 kA/m respectively; volume concentration of clusters  $\Phi = 0.25$ ; and viscosity  $\eta_0 = \sigma(H = 0)/\dot{\gamma}$ .

The fitted agglomerates volume concentration  $\Phi=0.2$  slightly differs from that  $\Phi=0.25$ , estimated in ref. [10], because the conditions of the systems synthesis have not been identical.

Results of calculations of Equation 13 are shown in Figure 14 for two values of the applied magnetic field. Experimental values are also included for comparison. As observed, the theoretical predictions reproduce the general tendency exhibited by the experimental values.

The fitting numbers  $n = 8$  and  $n = 9$  of the agglomerates in the undestroyed chains look quite reasonable from the physical point of view. The agreement between theory and experiments indicates that the proposed model is adequate, at least, in its main physical points. The dynamic yield stress  $\sigma_y$  can also be estimated, by the extrapolation of the quasi-linear parts of the theoretical curves in linear-linear scale, corresponding to large shear rates, to zero shear rate. The extrapolations gave the following theoretical values of the yield stress:  $\sigma_y \approx 1200$  Pa for  $H =$



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156 kA/m and  $\sigma_y \approx 1900$  Pa for  $H = 282$  kA/m. These results are not far from the experimental data:  $\sigma_y \approx 1629$  Pa for  $H = 156$  kA/m and  $\sigma_y \approx 2731$  Pa for  $H = 282$  kA/m.

## 5. Conclusions

We report a straightforward strategy to develop and characterise novel “smart” alginate-based fluids and gels, containing a dispersion of micron-sized Fe-HQ magnetic particles. Our study demonstrates the fabrication of magnetorheological polymer suspensions in a controlled manner and according to the physical needs in terms of colloidal stability, shear-thinning properties and viscoelastic moduli, through the modulation of the polymer concentration and molecular weight. In the presence of an applied magnetic field, we found a clear magnetorheological effect, as the viscoelastic moduli of all polymer formulations increased at increasing concentration of magnetic particles and strength of the magnetic field. Tuning the polymer concentration of the magnetorheological formulations permitted to enhance their rheological properties, by controlling the movement and the structural distribution of the magnetic particle clusters within the polymeric matrix, as demonstrated through optical microscopy evaluation. In support to our hypothesis, here we presented a theoretical model able to properly reproduce the general trend exhibited by the experimental values in the stationary regime of the suspension flow. With further improvements, the capability to master the interaction between polymeric chains, magnetic particle clusters and its distribution within the biocompatible matrices could allow the generation of novel magnetorheological fluid and gels with novel properties and with new potential applications in the field of biomedicine and tissue engineering.

## Additional Information

**Information on the following should be included wherever relevant.**

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#### **Data Accessibility**

This article has no additional data.

#### **Competing Interests**

We declare we have no competing interests.

#### **Authors' Contributions**

William R Suarez-Fernandez: substantial contributions to acquisition of data; drafting the article; final approval of the version to be published.

Giuseppe Scionti: substantial contributions to conception and design; revising the article critically for important intellectual content; final approval of the version to be published.

Juan DG Duran: substantial contributions to conception and design, and analysis and interpretation of data; revising the article critically for important intellectual content; final approval of the version to be published.

Andrey Yu Zubarev: substantial contributions to conception and design, and analysis and interpretation of data; revising the article critically for important intellectual content; final approval of the version to be published.

Modesto T Lopez-Lopez: substantial contributions to conception and design, analysis and interpretation of data; drafting the article; final approval of the version to be published.

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## Tables

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Table I. Experimental systems for which the rheological properties were thoroughly investigated in the present work.

Sample name	Iron particle(HQ type) concentration	Alginate polymer type / concentration	Carrier liquid	Rheological nature
0Fe-10LVSA	0% v/v	LVSA / 10% w/v	Water	Fluid-like
0Fe-15LVSA	0% v/v	LVSA / 15% w/v	Water	Fluid-like
0Fe-20LVSA	0% v/v	LVSA / 20% w/v	Water	Fluid-like
0Fe-8MVSA	0% v/v	MVSA / 8% w/v	Water	Gel-like
5Fe-10LVSA	5% v/v	LVSA / 10% w/v	Water	Fluid-like
5Fe-15LVSA	5% v/v	LVSA / 15% w/v	Water	Fluid-like
5Fe-20LVSA	5% v/v	LVSA / 20% w/v	Water	Fluid-like
5Fe-8MVSA	5% v/v	MVSA / 8% w/v	Water	Gel-like

Table II. Values corresponding to the linear viscoelastic region (LVR), as obtained by oscillatory measurements of constant frequency and increasing shear strain amplitude.

Sample name	Storage modulus, $G'$ (Pa)	Loss modulus, $G''$ (Pa)	$G''/G'$ ratio
0Fe-10LVSA	$7.5 \pm 0.8$	$33 \pm 5$	$4.4 \pm 1.1$
0Fe-15LVSA	$103 \pm 12$	$210 \pm 30$	$2.0 \pm 0.5$
0Fe-20LVSA	$820 \pm 90$	$1060 \pm 120$	$1.3 \pm 0.3$
0Fe-8MVSA	$2070 \pm 240$	$1650 \pm 170$	$0.80 \pm 0.17$
5Fe-10LVSA	$6 \pm 0.5$	$29 \pm 3$	$4.8 \pm 0.9$
5Fe-15LVSA	$132 \pm 14$	$220 \pm 30$	$1.7 \pm 0.4$
5Fe-20LVSA	$1340 \pm 140$	$1500 \pm 180$	$1.1 \pm 0.3$
5Fe-8MVSA	$2350 \pm 180$	$2030 \pm 150$	$0.86 \pm 0.12$

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Table I. Experimental systems for which the rheological properties were thoroughly investigated in the present work.

Table II. Values corresponding to the linear viscoelastic region (LVR), as obtained by oscillatory measurements of constant frequency and increasing shear strain amplitude.

Figure 1. Images of suspensions of iron particles (5% v/v) in solutions of alginate polymer at different times after preparation as indicated (days: hours: minutes: seconds). In each image, from left to right samples corresponding to the following concentrations of alginate polymer are seen: 5% w/v of LVSA polymer; 10% of LVSA polymer; 15% of LVSA polymer; 20% of LVSA polymer; 8% of MVSA polymer.

Figure 2. Average value of the viscoelastic moduli of solutions of alginate polymer, within the LVR - standard deviations are about one order of magnitude smaller than the average values. Triangles and squares correspond respectively to solutions of LVSA polymer and MVSA polymer. Open symbols are for the storage modulus ( $G'$ ); full symbols for the loss modulus ( $G''$ ).

Figure 3. Viscosity as a function of shear rate for solutions of alginate polymer (open symbols) and suspensions of iron particles in alginate polymer solutions (full symbols): unfilled diamond / filled diamond: samples 0Fe-10LVSA/5Fe-10LVSA; unfilled circle / filled circle: samples 0Fe-15LVSA/5Fe-15LVSA; unfilled triangle / filled triangle: samples 0Fe-20LVSA/5Fe-20LVSA; unfilled square / filled square: samples 0Fe-8MVSA/5Fe-8MVSA.

Figure 4. Viscoelastic moduli as a function of shear strain amplitude for fixed frequency of 1 Hz, for solutions of alginate polymer (open symbols) and suspensions of iron particles in alginate polymer solutions (full symbols): unfilled diamond / filled diamond: samples 0Fe-10LVSA/5Fe-10LVSA; unfilled circle / filled circle: samples 0Fe-15LVSA/5Fe-15LVSA; unfilled triangle / filled triangle: samples 0Fe-20LVSA/5Fe-20LVSA; unfilled square / filled square: samples 0Fe-8MVSA/5Fe-8MVSA. (a) Storage modulus ( $G'$ ); (b) loss modulus ( $G''$ ).

Figure 5. Viscoelastic moduli as a function of shear strain frequency for fixed shear strain amplitude within the LVR, for solutions of alginate polymer and suspensions of iron particles in alginate polymer solutions: unfilled triangle / filled triangle: sample 0Fe-15LVSA; unfilled circle / filled circle

sample 5Fe-15LVSA; unfilled diamond / filled diamond: samples 0Fe-8MVSA; unfilled square / filled square sample 5Fe-8MVSA. Full symbols represent values of the storage modulus ( $G'$ ); open symbols values of the loss modulus ( $G''$ ).

Figure 6. Shear stress (a) and viscosity (b) as a function of shear rate for sample 5Fe-15LVSA, under the application of magnetic fields of different strength,  $H$ . -:  $H=0$  kA/m; filled square:  $H=73.5$  kA/m; filled diamond:  $H=156$  kA/m; filled circle: 229 kA/m; filled triangle: 282 kA/m.

Figure 7. Dynamic yield stress as a function of the applied magnetic field strength, for suspensions of magnetic particles in solutions of alginate polymer. Filled diamond: sample 5Fe-10LVSA; filled circle sample 5Fe-15LVSA; filled triangle: samples 5Fe-20LVSA; filled square sample 5Fe-8MVSA.

Figure 8. Viscoelastic moduli of suspensions of magnetic particles in solutions of alginate polymer, as a function of shear strain amplitude, for imposed oscillatory shear strain of fixed frequency (1 Hz), and under the application of magnetic fields of different strength:  $H$ . Unfilled star / filled star:  $H=0$  kA/m; unfilled square / filled square:  $H=73.5$  kA/m; unfilled diamond / filled diamond:  $H=156$  kA/m; unfilled circle / filled circle: 229 kA/m; unfilled triangle / filled triangle: 282 kA/m. (a) sample 5Fe-15LVSA; (b) 5Fe-8MVSA. Open symbols represent values of the storage modulus ( $G'$ ); Full symbols values of the loss modulus ( $G''$ ).

Figure 9. Viscoelastic moduli of sample 5Fe-8MVSA as a function of shear strain frequency, for imposed oscillatory shear strain of fixed amplitude within the LVR, and under the application of magnetic fields of different strength:  $H$ . Unfilled star / filled star:  $H=0$  kA/m; unfilled square / filled square:  $H=73.5$  kA/m; unfilled diamond / filled diamond:  $H=156$  kA/m; unfilled circle / filled circle: 229 kA/m; unfilled triangle / filled triangle: 282 kA/m. Open symbols represent values of the storage modulus ( $G'$ ); Full symbols values of the loss modulus ( $G''$ ).

Figure 10. Values of the viscoelastic moduli corresponding to the LVR for a frequency of 1 Hz, as a function of the magnetic field strength for suspensions of magnetic particles in solutions of alginate polymer. Unfilled diamond / filled diamond: sample 5Fe-10LVSA; unfilled circle / filled circle: sample 5Fe-15VSA; unfilled triangle / filled triangle: sample 5Fe-20LVSA; unfilled square / filled square: sample 5Fe-8MVSA. Open symbols represent values of the storage modulus ( $G'$ ); Full symbols values of the loss modulus ( $G''$ ).

Figure 11. Self-healing study of sample 5Fe-8MVSA. The sample was subjected to a shear rate of  $1000 \text{ s}^{-1}$  during the time interval 80 s - 160 s. Before and after this time, the viscoelastic moduli resulting from an oscillatory shear strain of fixed amplitude within the LVR and 1 Hz of frequency were monitored. Open squares represent the storage modulus; full symbols the loss modulus.

Figure 12. Images of optical microscopy of diluted suspensions of magnetic particles (about 0.2 % v/v of particles) in solutions of alginate polymer. A, C, E, G, I were taken in the absence of applied magnetic field; B, D, F, H, J were taken under the application of a magnetic field of 40 mT. Solutions of alginate polymer used as dispersing medium were as it follows: A,B: 5LVSA; C,D: 10LVSA; E,F: 15LVSA; G,H: 20LVSA; I,J: 8MVSA.

Figure 13. Illustration of the chains. The circles present the clusters.

Figure 14. Theory-experiment comparison for curves of shear stress vs. shear rate, for sample 5Fe-15LVSA, under the application of magnetic fields of different strength,  $H$ : filled diamond, - :  $H=156 \text{ kA/m}$ ; filled triangle, - - :  $282 \text{ kA/m}$ . Filled diamond, filled triangle represent experimental data; - , - - predictions of the theoretical model (Equation 13). Parameters of the system for theoretical calculations: number of primary agglomerates in the undestroyed chains obtained by fitting are  $n = 8$  and  $n = 9$  for the magnetic fields of  $156 \text{ kA/m}$  and  $282 \text{ kA/m}$  respectively; volume concentration of clusters  $\Phi = 0.25$ ; and viscosity  $\eta_0 = \sigma(H = 0)/\dot{\gamma}$ .